August 17, 1990

Docket No. 50-334
Serial No. BV-90-006

Mr. J. D. Sieber, Vice President
Nuclear Group
Duquesne Light Company
Post Office Box 4
Shippingport, Pennsylvania 15077

Dear Mr. Sieber:

SUBJECT: BEAVER VALLEY UNIT 1 - ISSUANCE OF AMENDMENT (TAC NO. 71869)

The Commission has issued the enclosed Amendment No. 155 to Facility Operating License No. DPR-66 for the Beaver Valley Power Station, Unit No. 1, in response to your application dated March 2, 1989, as supplemented by letter dated June 12, 1990.

This amendment revises the Appendix A Technical Specifications (TSs) relating to the reactor trip system and engineered safety features (ESF) actuation system instrumentation trip set points and allowable values. Specifically, the amendment modifies TS Tables 2.2-1 and 3.3-4.

These changes assure that the reactor trip and ESF actuation setpoints, after factoring in the revised inaccuracy allowances, remain within the limits assumed in the Final Safety Analysis Report.

A copy of the related Safety Evaluation is also enclosed. The Notice of Issuance will be included in the Commission's biweekly Federal Register notice.

Sincerely,

/s/

Albert W. De Agazio, Sr. Project Manager
Project Directorate I-4
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Enclosures:
1. Amendment No. 155 to DPR-66
2. Safety Evaluation

cc w/enclosures:
See next page

CP-1

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DATED: August 17, 1990

AMENDMENT NO. 155 TO FACILITY OPERATING LICENSE NO. DRP-66

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UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D. C. 20555

DUQUESNE LIGHT COMPANY

OHIO EDISON COMPANY

PENNSYLVANIA POWER COMPANY

DOCKET NO. 50-334

BEAVER VALLEY POWER STATION, UNIT NO. 1

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 155
License No. DPR-66

1. The Nuclear Regulatory Commission (the Commission) has found that:

   A. The application for amendment by Duquesne Light Company, et al. (the licensee) dated March 2, 1989, as supplemented June 12, 1990, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act) and the Commission's rules and regulations set forth in 10 CFR Chapter I;

   B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;

   C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations;

   D. The issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public; and

   E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.

2. Accordingly, the license is amended by changes to the Technical Specifications as indicated in the attachment to this license amendment, and paragraph 2.C.(2) of Facility Operating License No. DPR-66 is hereby amended to read as follows:

   (2) Technical Specifications

   The Technical Specifications contained in Appendix A, as revised through Amendment No. 155 , are hereby incorporated in the license. The licensee shall operate the facility in accordance with the Technical Specifications.

3. This license amendment is effective as of the date of its issuance, to be implemented within 60 days of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION

Albert W. DeAgazio for

John F. Stolz, Director
Project Directorate I-4
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Attachment:
Changes to the Technical
Specifications

Date of Issuance: August 17, 1990

ATTACHMENT TO LICENSE AMENDMENT NO. 155

FACILITY OPERATING LICENSE NO. DPR-66

DOCKET NO. 50-334

Replace the following pages of Appendix A, Technical Specifications, with the enclosed pages as indicated. The revised pages are identified by amendment number and contain vertical lines indicating the areas of change.

Remove	Insert
2-6	2-6
2-7	2-7
2-7a	2-7a
2-10	2-10
3/4 3-22	3/4 3-22
3/4 3-22a	3/4 3-22a
3/4 3-23	3/4 3-23
3/4 3-24	3/3 3-24
3/4 3-24a	3/4 3-24a

TABLE 2.2-1

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

FUNCTIONAL UNIT	TRIP SETPOINT	ALLOWABLE VALUES
1. Manual Reactor Trip	Not Applicable	Not Applicable
2. Power Range, Neutron Flux	Low Setpoint - ≤ 25% of RATED THERMAL POWER	Low Setpoint - ≤ 27.3% RATED THERMAL POWER
	High Setpoint - ≤ 109% of RATED THERMAL POWER	High Setpoint - ≤ 111.3% of RATED THERMAL POWER
3. Power Range, Neutron Flux, High Positive Rate	≤ 5% of RATED THERMAL POWER with a time constant ≥ 2 seconds	≤ 6.3% of RATED THERMAL POWER with a time constant ≥ 2 seconds
4. Power Range, Neutron Flux, High Negative Rate	≤ 5% of RATED THERMAL POWER with a time constant ≥ 2 seconds	≤ 6.3% of RATED THERMAL POWER with a time constant ≥ 2 seconds
5. Intermediate Range, Neutron Flux	≤ 25% of RATED THERMAL POWER	≤ 31.1% of RATED THERMAL POWER
6. Source Range, Neutron Flux	≤ 10^5 counts per second	≤ 1.4 x 10^5 counts per second
7. Overtemperature ΔT	See Note 1	See Note 3
8. Overpower ΔT	See Note 2	See Note 4
9. Pressurizer Pressure--Low	≥ 1945 psig	≥ 1934 psig
10. Pressurizer Pressure--High	≤ 2385 psig	≤ 2394 psig
11. Pressurizer Water Level--High	≤ 92% of instrument span	≤ 93.9% of instrument span
12. Loss of Flow	≥ 90% of design flow* per loop	≥ 89.2% of design flow* per loop

*Design flow is 88,500 gpm per loop.

TABLE 2.2-1 (Continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

FUNCTIONAL UNIT	TRIP SETPOINT	ALLOWABLE VALUES
13. Steam Generator Water Level-Low-Low	≥ 12% of narrow range instrument span-each steam generator	≥ 10.7% of narrow range instrument span-each steam generator
14. Steam/Feedwater Flow Mismatch and Low Steam Generator Water Level	≤ 40% of full steam flow at RATED THERMAL POWER coincident with steam generator water level ≥ 25% of narrow range instrument span-each steam generator	≤ 43.4% of full steam flow at RATED THERMAL POWER coincident with steam generator water level ≥ 23.1% of narrow range instrument span-each steam generator
15. Undervoltage-Reactor Coolant Pumps	≥ 2750 volts-each bus	≥ 2687 volts-each bus
16. Underfrequency-Reactor Coolant Pumps	≥ 57.5 Hz - each bus	≥ 57.4 Hz - each bus
17. Turbine Trip		
A. Auto stop oil pressure	45 psig	± 5 psig
B. Turbine Stop Valve	≥ 1% open	≥ 1% open
18. Safety Injection Input from ESF	Not Applicable	Not Applicable
19. Reactor Coolant Pump Breaker Position Trip	Not Applicable	Not Applicable
20. Reactor Trip System Interlocks		
A. Intermediate Range Neutron Flux, P-6	≥ 1×10^{-10} Amps	≥ 6×10^{-11} Amps

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

20. (Continued)

FUNCTIONAL UNIT	TRIP SETPOINT	ALLOWABLE VALUES
B. Power Range Neutron Flux, P-8	≤ 30% RATED THERMAL POWER	≤ 32.3% RATED THERMAL POWER
C. Power Range Neutron Flux, P-9	≤ 49% RATED THERMAL POWER	≤ 51.3% RATED THERMAL POWER
D. Power Range Neutron Flux, P-10 (Input to P-7)	10% RATED THERMAL POWER	≥ 7.7% and ≤ 12.3% RATED THERMAL POWER
E. Turbine Impulse Chamber Pressure, P-13 (Input to P-7)	≤ 10% of RTP Turbine Impulse Pressure Equivalent	≤ 12.3% of RTP Turbine Impulse Pressure Equivalent

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

NOTATION

NOTE 2: Overpower $\Delta T \left(\frac{1}{1+\tau_4 S}\right) \leq \Delta T_o \left[K_4 - K_5 \left(\frac{\tau_3 S}{1+\tau_3 S}\right) \left(\frac{1}{1+\tau_5 S}\right) T - K_6 \left[T \left(\frac{1}{1+\tau_5 S}\right) - T''\right] - f(\Delta I)\right]$

where:

ΔT_0	=	Indicated ΔT at RATED THERMAL POWER
T	=	Average temperature, °F
T''	=	Indicated T_{avg} at RATED THERMAL POWER $\leq$ 576.3°F
K_4	=	1.07
K_5	=	0.02/°F for increasing average temperature
K_6	=	0.00128 for $T > T''$; K_6 = (0) for $T \leq T''$
$\frac{\tau_3 S}{1+\tau_3 S}$	=	The function generated by the rate lag controller for T_{avg} dynamic compensation.
τ_3	=	Time constant utilized in the rate lag controller for T_{avg}, $-\tau$ = 10 secs.
$\frac{1}{1+\tau_4 S}$	=	Lag compensator on measured ΔT
τ_4	=	Time constant utilized in the lag compensator for ΔT, $\leq$ 2 secs.
$\frac{1}{1+\tau_5 S}$	=	Lag compensator on measured T_{avg}
τ_5	=	Time constant utilized in the lag compensator for Tavg $\leq$ 2 secs.
S	=	Laplace transform operator.
$f(\Delta I)$	=	0 for all ΔI

NOTE 3: The channel's maximum trip point shall not exceed its computed trip point by more than 3.3 percent.

NOTE 4: The channel's maximum trip point shall not exceed its computed trip point by more than 2.9 percent.

TABLE 3.3-4

ENGINEERED SAFETY FEATURE ACTUATION SYSTEM INSTRUMENTATION TRIP SETPOINTS

FUNCTIONAL UNIT	TRIP SETPOINT	ALLOWABLE VALUES
1. SAFETY INJECTION, TURBINE TRIP AND FEEDWATER ISOLATION		
a. Manual Initiation	Not Applicable	Not Applicable
b. Automatic Actuation Logic	Not Applicable	Not Applicable
c. Containment Pressure--High	$\leq$ 1.5 psig	$\leq$ 2.4 psig
d. Pressurizer Pressure-Low	$\geq$ 1845 psig	$\geq$ 1830 psig
e. Steamline Pressure-Low	$\geq$ 500 psig steam line pressure	$\geq$ 488 psig steam line pressure

TABLE 3.3-4 (Continued)

ENGINEERED SAFETY FEATURE ACTUATION SYSTEM INSTRUMENTATION TRIP SETPOINTS

	FUNCTIONAL UNIT	TRIP SETPOINT	ALLOWABLE VALUES
1.1	SAFETY INJECTION-TRANSFER FROM INJECTION TO THE RECIRCULATION MODE		
a.	Manual Initiation	Not Applicable	Not Applicable
b.	Automatic Actuation Logic Coincident with Safety Injection Signal	Not Applicable	Not Applicable
c.	Refueling Water Storage Tank Level-Low	18'8-1/2"	$\geq$ 18'2-1/2" and $\leq$ 19'2-1/2"
d.	Refueling Water Storage Tank Level - Auto QS Flow Reduction	9'6"	$\geq$ 9'0" and $\geq$ 10'0"

TABLE 3.3-4 (Continued)

ENGINEERED SAFETY FEATURE ACTUATION SYSTEM INSTRUMENTATION TRIP SETPOINTS

FUNCTIONAL UNIT	TRIP SETPOINT	ALLOWABLE VALUES
2. CONTAINMENT SPRAY		
a. Manual Initiation	Not Applicable	Not Applicable
b. Automatic Actuation Logic	Not Applicable	Not Applicable
c. Containment Pressure--High-High	≤ 8.0 psig	≤ 8.9 psig
3. CONTAINMENT ISOLATION		
a. Phase "A" Isolation		
1. Manual	Not Applicable	Not Applicable
2. From Safety Injection Automatic Actuation Logic	Not Applicable	Not Applicable
b. Phase "B" Isolation		
1. Manual	Not Applicable	Not Applicable
2. Automatic Actuation Logic	Not Applicable	Not Applicable
3. Containment Pressure--High-High	≤ 8.0 psig	≤ 8.9 psig

ENGINEERED SAFETY FEATURE ACTUATION SYSTEM INSTRUMENTATION TRIP SETPOINTS

FUNCTIONAL UNIT	TRIP SETPOINT	ALLOWABLE VALUES
4. STEAM LINE ISOLATION		
a. Manual	Not Applicable	Not Applicable
b. Automatic Actuation Logic	Not Applicable	Not Applicable
c. Containment Pressure--Intermediate-High-High	≤ 3.0 psig	≤ 3.9 psig
d. Steamline Pressure-Low	≥ 500 psig steam line pressure	≥ 488 psig steam line pressure
e. High Negative Steam Pressure Rate	≤ 100 psi with a time constant ≥ 50 seconds	≤ 127 psi with a time constant ≥ 50 seconds
5. TURBINE TRIP AND FEEDWATER ISOLATION		
a. Steam Generator Water Level High-High	≤ 75% of narrow range instrument span each steam generator	≤ 76.9% of narrow range instrument span each steam generator
6. LOSS OF POWER		
a. 1. 4.16kv Emergency Bus Undervoltage (Loss of Voltage) (Trip Feed)	≥ 75% of nominal bus voltage with a 1 ± 0.1 second time delay	≥ 73% of nominal bus voltage with a 1 ± 0.1 second time delay
2. 4.16kv Emergency Bus (Start Diesel)	≥ 83% - 12 cycles	≥ 81% of nominal bus voltage
b. 4.16kv Emergency Bus Undervoltage (Degraded Voltage)	≥ 90% of nominal bus voltage with a 90 ± 5 second time delay	≥ 88% of nominal bus voltage with a 90 ± 5 second time delay
c. 480v Emergency Bus Undervoltage (Degraded Voltage)	≥ 90% of nominal bus voltage with a 90 ± 5 second time delay	≥ 88% of nominal bus voltage with a 90 ± 5 second time delay

ENGINEERED SAFETY FEATURE ACTUATION SYSTEM INSTRUMENTATION TRIP SETPOINTS

FUNCTIONAL UNIT	TRIP SETPOINT	ALLOWABLE VALUES
7. AUXILIARY FEEDWATER		
a. Steam Generator Water Level-low-low	≥ 12% of narrow range instrument span each steam generator	≥ 10.7% of narrow range instrument span each steam generator
b. Undervoltage - RCP	≥ 2750 volts RCP bus voltage	≥ 2687 volts RCP bus voltage
c. S.I.	See 1 above (all SI Setpoints)	
d. Emergency Bus Undervoltage	≤ 3350 volts	≤ 3325 volts
e. Trip of Main Feedwater Pumps	Not Applicable	Not Applicable

UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D. C. 20555

SAFETY EVALUATION BY THE OFFICE OF NUCLEAR REACTOR REGULATION

RELATED TO AMENDMENT NO. 155 TO FACILITY OPERATING LICENSE NO. DPR-66

DUQUESNE LIGHT COMPANY
OHIO EDISON COMPANY
PENNSYLVANIA POWER COMPANY

BEAVER VALLEY POWER STATION, UNIT NO. 1

DOCKET NO. 50-334

1.0 INTRODUCTION

By letter dated March 2, 1989, and supplemented by letter dated June 12, 1990, Duquesne Light Company (the licensee) proposed certain revisions to the Technical Specifications to revise several Reactor Trip and Engineered Safety Features (ESF) Actuation System instrumentation trip setpoints and numerous allowable values for Beaver Valley, Unit 1. The revision of the Reactor Protection System and ESF trip setpoints and allowable values are based upon the results of a re-analysis of the instrument channel inaccuracies. This re-analysis was performed to update the Beaver Valley Unit 1 setpoint methodology to the same methodology used in determining Unit 2 protection setpoints.

The trip setpoints that would be revised for Unit 1 include the Turbine Impulse Chamber Pressure P-13 Interlock, the Refueling Water Storage Tank (RWST) Level-Low and auto QS flow reduction for safety injection transfer from injection to recirculation, the Containment Pressure High-High, Containment Pressure Intermediate High-High and the Emergency Buses Undervoltage settings for Degraded Voltage. In addition, numerous setpoint allowable values would be revised consistent with the calculated inaccuracies.

The methodology used is described in detail in Westinghouse WCAP-11419 "Westinghouse Setpoint Methodology for Protection Systems, Beaver Valley Unit 1" (proprietary) and WCAP-11420.

In addition to determining the required trip setpoints and allowable values, the methodology includes an optional provision for determining the OPERABILITY of a channel when its trip setpoint is found to exceed the allowable value. The licensee has elected not to incorporate this provision into the Unit 1 Technical Specifications for this revision; consequently, we did not review this feature.

2.0 EVALUATION

2.1 Setpoint Calculation Methodology

The methodology used to combine the error components for a channel is basically the appropriate statistical combination of those groups of components which are statistically independent, i.e., not interactive. Those errors which are not independent are placed arithmetically into groups. The groups themselves are independent effects and can then be systematically combined.

The methodology used for this combination is generally the square root of the sum of the squares which has been utilized in Westinghouse reports for Beaver Valley Unit 2. This technique, or other statistical approaches of a similar nature, have been used in WCAP-10395 and WCAP-8567. WCAP-8567 has been approved by the NRC staff, thus, noting the acceptability of statistical techniques for the application requested. The methodology used for this report is essentially the same as that used for V.C. Summer which was approved by the NRC in NUREG-0717, Supplement No. 4.

2.2 Sensor Allowances

Four parameters are considered to be sensor allowances -- Sensor Calibration Accuracy (SCA), Sensor Drift (SD), Sensor Temperature Effects (STE), and Sensor Pressure Effects (SPE). Of these four parameters, STE and SPE are considered to be statistically independent; SD and SCA are also statistically independent and treated as interactive which is more conservative. STE and SPE are considered to be independent due to the manner in which the instrumentation is checked, i.e., the instrumentation is calibrated and drift determined under conditions in which pressure and temperature are assumed constant. SD and SCA are considered to be interactive for the same reason that STE and SPE are considered independent, i.e., due to the manner in which the instrumentation is checked. Instrumentation calibration techniques use the same process for determining instrument drift, that is, the end result of the two is the same. When calibrating a sensor, the sensor output is checked to determine if it is representing accurately the input. The same is done for a determination of the sensor drift. Thus, it is impossible to determine the differences between calibration errors and drift when a sensor is checked for the second and subsequent times. Based on this reasoning, SD and SCA have been added to form an independent group.

2.3 Rack Allowance

Four parameters are considered to be rack allowances, Rack Calibration Accuracy (RCA), Rack Comparator Setting Accuracy (RCSA), Rack Temperature Effects (RTE), and Rack Drift (RD). Three of these parameters are considered to be interactive, RCA, RCSA, and RD, for much the same reason as described in

2.2 above. When calibrating or determining drift in the racks for a specific channel, the processes are performed at essentially constant temperature, i.e, ambient temperature. Because of this, the RTE parameter is considered to be independent of any factors for calibration or drift. As noted in 2.2, when calibrating or determining drift for a channel, the same end result is desired, that is, at what point does the bistable change state. After the initial calibration, it is not possible to distinguish the difference between a calibration error, rack drift or a comparator setting error. Based on this logic, these three factors have been added to form an independent group.

2.4 Process Allowance

The Process Measurement Accuracy (PMA) and Primary Element Accuracy (PEA) parameters are considered to be independent of both sensor and rack parameters. PMA provides allowance for the non-instrument related effects. PEA accounts for errors due to metering devices.

2.5 Combination of Error Components

The relationship between the error components and the total statistic error allowance for a channel is represented by Equation 2.1 in WCAP-11419, "Westinghouse Setpoint Methodology for Protection Systems, Beaver Valley, Unit 1." According to Equation 2.1, drift and calibration accuracy allowances are interactive and thus not independent. The environmental allowance is not necessarily considered interactive with all other parameters but it is added to the statistical sum as an additional degree of conservatism. The licensee assumes that the accuracy effect on a channel due to cable degradation in an accident environment will be less than 0.1 percent of span. This impact has been considered negligible and is not factored into the analysis. The Westinghouse setpoint methodology results in a value with a 95 percent probability with a high confidence level. By letter dated June 12, 1990, the licensee stated that the confidence level is 95 percent or better. With the exception of PMA, RD, and SD, all uncertainties assumed are the extremes of the ranges of the various parameters, i.e., are better than 2 values. Thus, the approach represented by this report is considered as conservative and follows the V. C. Summer plant setpoint methodology previously approved by the NRC.

2.6 Technical Specification Change

The setpoints for the various functions in the RPS and ESF Actuation System are determined on the basis of the trip settings assumed in the FSAR accident and transient analysis. The required settings correspond to the trip points assumed in these analyses less the required allowance for instrument inaccuracies.

An analysis has been performed to update the calculation of these instrument inaccuracies using a more current methodology for determining the required trip setting and allowable value limits. The methodology used is described in detail in Westinghouse WCAP-11419. The proposed changes to Table 2.2-1 and Table 3.3-4 revise the allowable values based on the calculation of the instrument inaccuracies using a more current methodology.

By using the methodology described in Westinghouse WCAP-11419, the plant gains added operational flexibility and yet remains within the analytical limit values accounted for in the various accident analysis. In addition, the methodology allows for a sensor drift factor and an increased rack drift factor. The proposed changes to revise the allowable values in Table 2.2-1 and Table 3.3-4 of the Beaver Valley Unit 1 Technical Specifications are based on the calculation of the instrument accuracies by using approved current methodology and are acceptable.

3.0 ENVIRONMENTAL CONSIDERATION

The amendment changes a requirement with respect to the installation or use of a facility component located within the restricted area as defined in 10 CFR Part 20. We have determined that the amendment involves no significant increase in the amounts, and no significant change in the types of any effluents that may be released offsite, and that there is no significant increase in individual or cumulative occupational radiation exposure. The staff has previously issued a proposed finding that this amendment involves no significant hazards consideration and there has been no public comment on such finding. Accordingly, this amendment meets the eligibility criteria for categorical exclusion set forth in 10 CFR 51.22(c)(9). Pursuant to 10 CFR 51.22(b) no environmental impact statement or environmental assessment need be prepared in connection with the issuance of this amendment.

4.0 CONCLUSION

We have concluded, based on the considerations discussed above, that: (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, and (2) such activities will be conducted in compliance with the Commission's regulations, and (3) the issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public.

Dated: August 17, 2990

Principal Contributor: S. Rhow