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U. S. Nuclear Regulatory Commission
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Subject: Docket No. 50-482: Wolf Creek Generating Station Cycle 12 Core
Operating Limits Report

Gentlemen:

Enclosed is Revision 0 of the Wolf Creek Generating Station Cycle 12 Core Operating Limits Report (COLR). This document is being submitted pursuant to Section 5.6.5 of the WCGS Technical Specifications.

If you should have any questions regarding this submittal, please contact me at (316) 364-4034, or Mr. Tony Harris at (316) 364-4038.

Very truly yours,



Richard A. Muench

RAM/rlr

Attachment
Enclosure

cc: J. N. Donohew (NRC), w/a, w/e
W. D. Johnson (NRC), w/a, w/e
E. W. Merschoff (NRC), w/a, w/e
Senior Resident Inspector (NRC), w/a, w/e

ADD1

LIST OF COMMITMENTS

The following table identifies those actions committed to by Wolf Creek Nuclear Operating Corporation (WCNOC) in this document. Any other statements in this submittal are provided for information purposes and are not considered to be commitments. Please direct questions regarding these commitments to Mr. Tony Harris, Manager Regulatory Affairs at Wolf Creek Generating Station, (316) 364-4038.

COMMITMENT	Due Date/Event
None	



**WOLF CREEK GENERATING STATION
CYCLE 12**

**CORE OPERATING LIMITS REPORT
Revision 0**

October, 2000

Prepared by:

Matthew K. Morris 9/12/2000
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Approved by:

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1.0 CORE OPERATING LIMITS REPORT

The CORE OPERATING LIMITS REPORT (COLR) for Wolf Creek Generating Station Cycle 12 has been prepared in accordance with the requirements of Technical Specification 5.6.5.

The core operating limits that are included in the COLR affect the following Technical Specifications:

- 3.1.3 Moderator Temperature Coefficient (MTC)
- 3.1.5 Shutdown Bank Insertion Limits
- 3.1.6 Control Bank Insertion Limits
- 3.2.3 AXIAL FLUX DIFFERENCE (AFD) (Relaxed Axial Offset Control (RAOC) Methodology)
- 3.2.1 Heat Flux Hot Channel Factor ($F_Q(Z)$) (F_Q Methodology)
- 3.2.2 Nuclear Enthalpy Rise Hot Channel Factor ($F_{\Delta H}^N$)
- 3.9.1 Boron Concentration

SHUTDOWN MARGIN for Specifications 3.1.1, 3.1.4, 3.1.5, 3.1.6, and 3.1.8

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the subsections below:

2.1 Moderator Temperature Coefficient (MTC)

(LCO 3.1.3)

The MTC shall be less positive than the limit provided in Figure 1.

The MTC shall be less negative than $-50 \text{ pcm}/^{\circ}\text{F}$.

(SR 3.1.3.2)

The 300 PPM MTC Surveillance limit is $-41 \text{ pcm}/^{\circ}\text{F}$ (equilibrium, all rods withdrawn, RATED THERMAL POWER condition).

The 60 PPM MTC Surveillance limit is $-46 \text{ pcm}/^{\circ}\text{F}$ (equilibrium, all rods withdrawn, RATED THERMAL POWER condition).

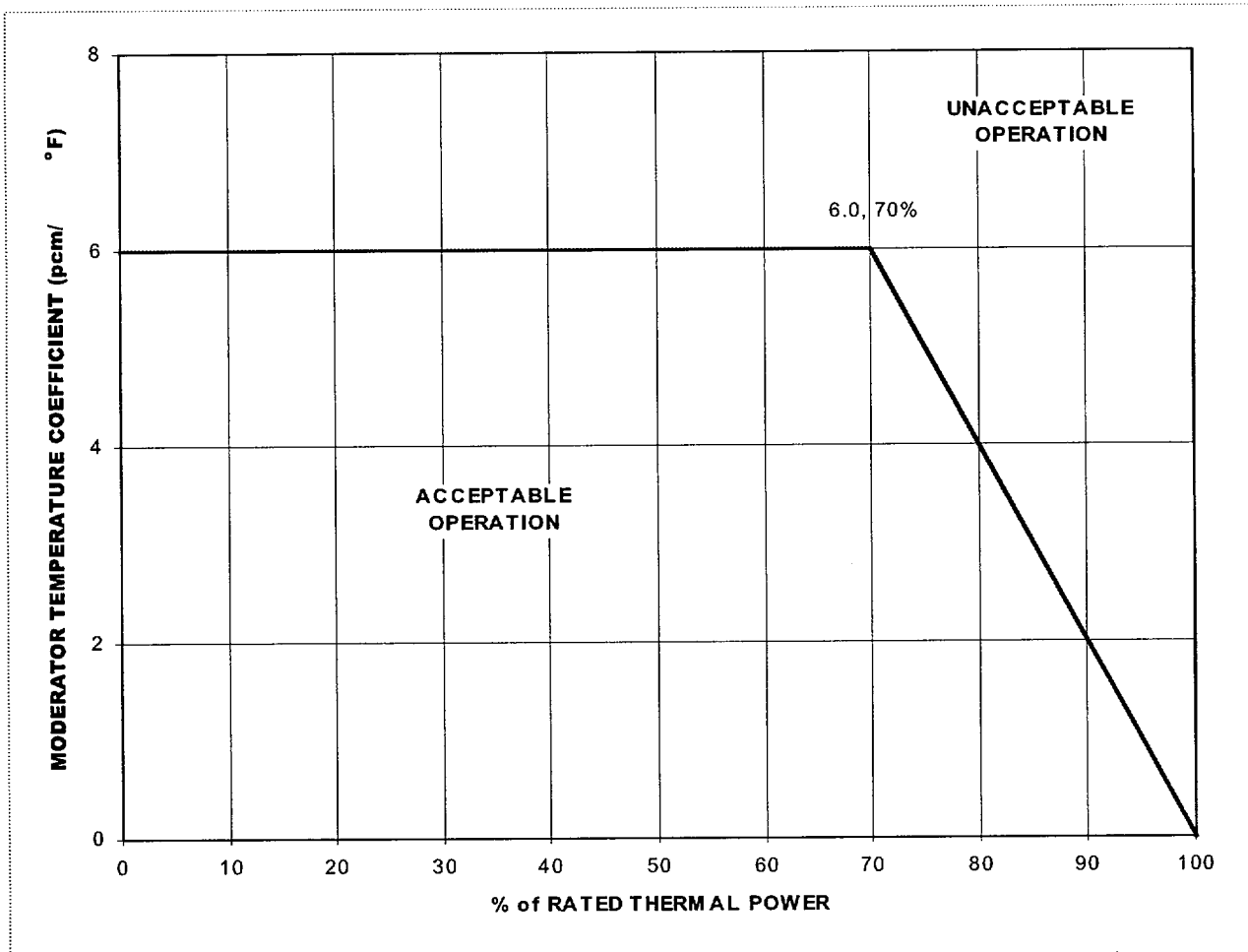


Figure 1
Moderator Temperature Coefficient Vs. RATED THERMAL POWER

2.2 Shutdown Bank Insertion Limits

(LCO 3.1.5)

The shutdown banks shall be fully withdrawn (i.e., positioned within the interval of ≥ 222 and ≤ 231 steps withdrawn).

2.3 Control Bank Insertion Limits

(LCO 3.1.6)

The Control Bank insertion, sequence, and overlap limits are specified in Figure 2.

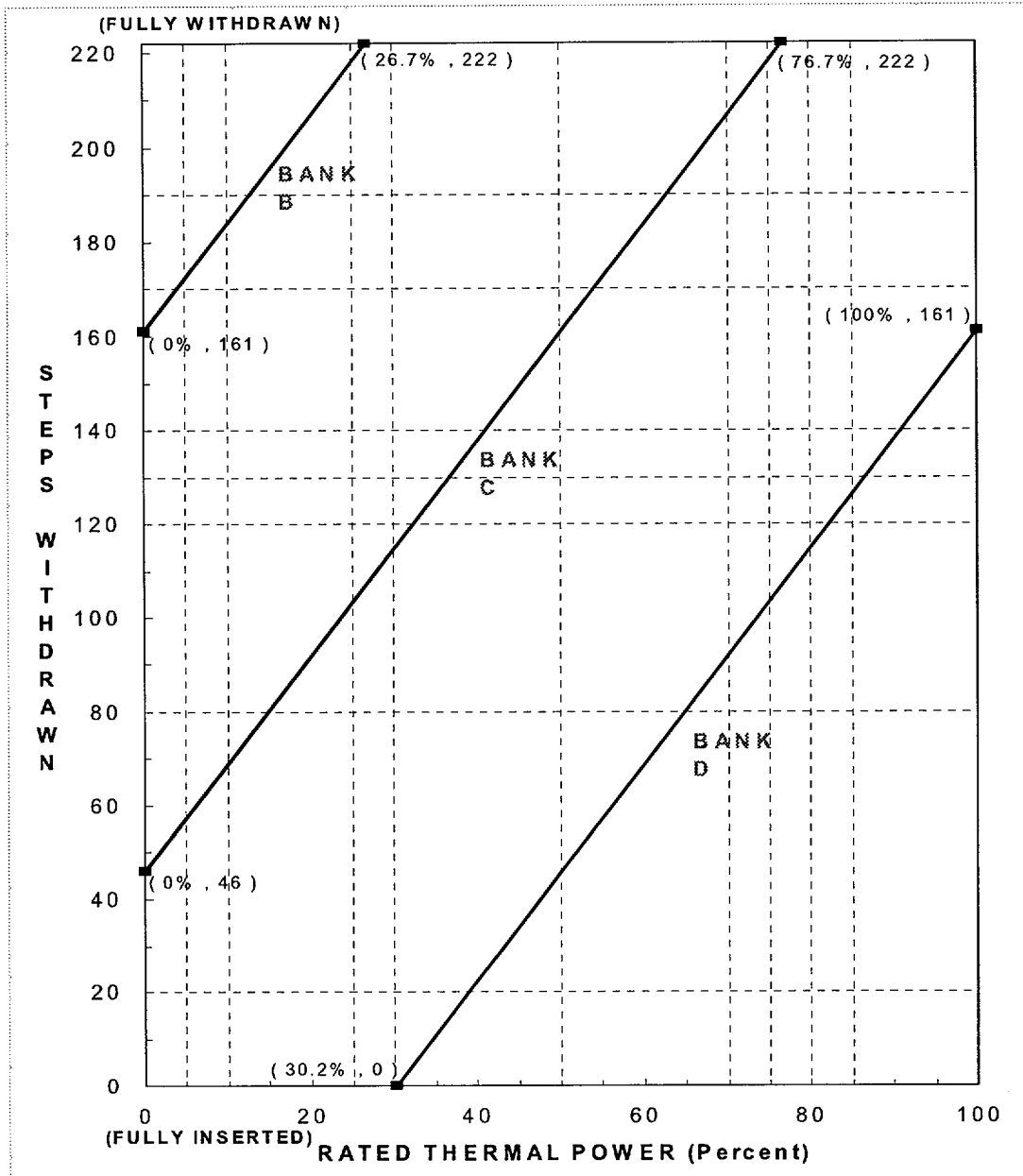


Figure 2

**Control Bank Insertion, Sequence, and Overlap Limits
Versus Thermal Power-Four Loop Operation**

Fully withdrawn shall be the condition where control banks are at a position within the interval of ≥ 222 and ≤ 231 steps withdrawn.

2.4 AXIAL FLUX DIFFERENCE (AFD) (Relaxed Axial Offset Control (RAOC)
Methodology)

(LCO 3.2.3)

The indicated AXIAL FLUX DIFFERENCE (AFD) allowed operational space is defined by Figure 3.

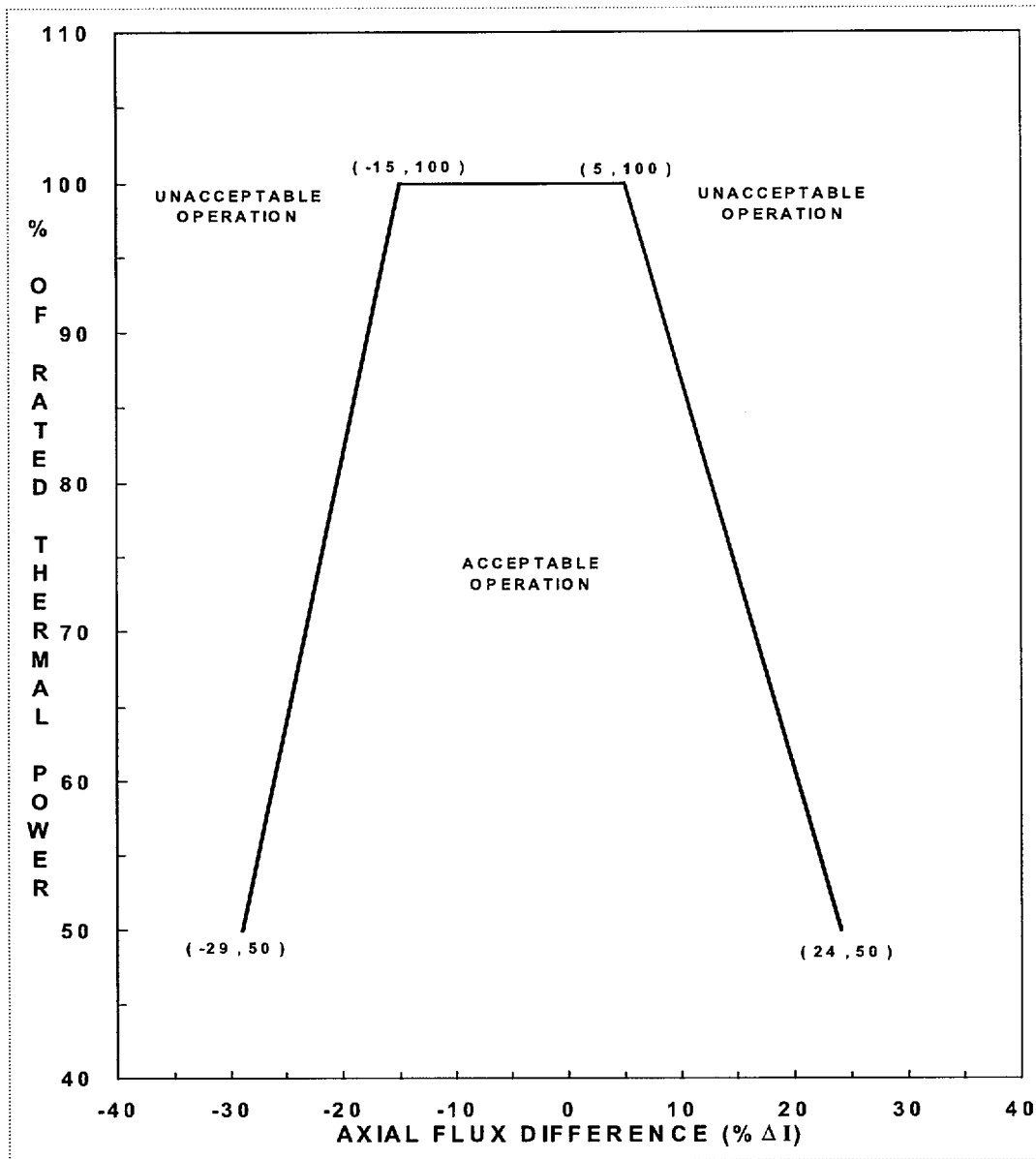


Figure 3

AXIAL FLUX DIFFERENCE Limits as a Function of
RATED THERMAL POWER

2.5 Heat Flux Hot Channel Factor ($F_Q(Z)$)(F_Q Methodology)

(LCO 3.2.1)

$$F_Q(Z) \leq \frac{CFQ}{P} * K(Z), \text{ for } P > 0.5$$

$$F_Q(Z) \leq \frac{CFQ}{0.5} * K(Z), \text{ for } P \leq 0.5$$

where, $P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}},$

$$CFQ = F_Q^{RTP}$$

$$F_Q^{RTP} = F_Q(Z) \text{ limit at RATED THERMAL POWER (RTP)}$$

$$= 2.50, \text{ and}$$

$$K(Z) = \text{as defined in Figure 4.}$$

$$F_Q^C(Z) = F_Q^M(Z)(1.03)(1.05) = F_Q^M(Z)(1.0815)$$

where, $F_Q^M(Z) =$ Measured value of $F_Q(Z)$ from incore flux map

$$F_Q^W(Z) = F_Q^C(Z) W(Z)$$

where, $W(Z)$ = a cycle dependent function that accounts for power distribution transients encountered during normal operation (see Appendix A).

(SR 3.2.1.2)

See Appendix A for:

F_Q Penalty Factor

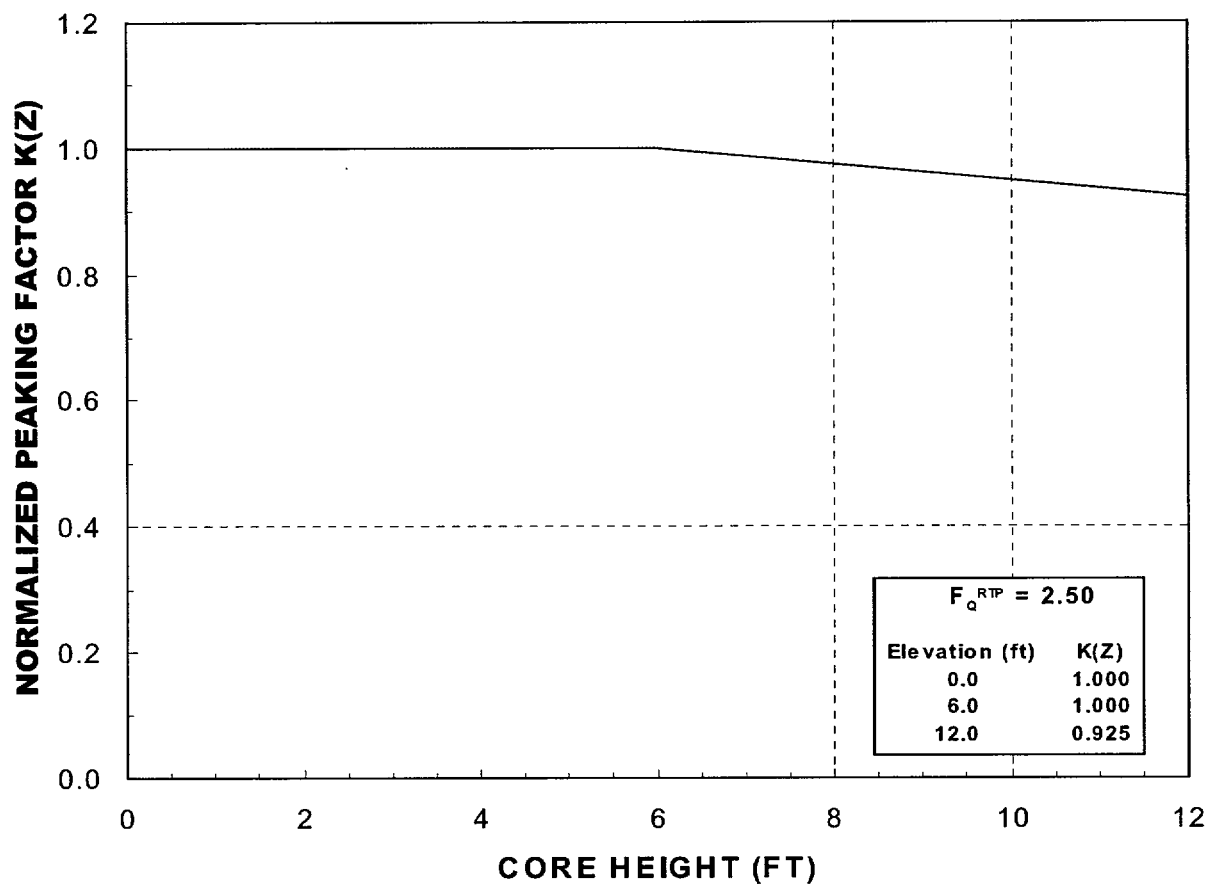


Figure 4

K(Z) - Normalized Peaking Factor Vs. Core Height

2.6 Nuclear Enthalpy Rise Hot Channel Factor ($F_{\Delta H}^N$)

(LCO 3.2.2)

$F_{\Delta H}^N$ shall be limited by the following relationship:

$$F_{\Delta H}^N \leq F_{\Delta H}^{RTP} [1.0 + PF_{\Delta H} (1.0 - P)]$$

Where,

$$\begin{aligned} F_{\Delta H}^{RTP} &= F_{\Delta H}^N \text{ limit at RATED THERMAL POWER (RTP)} \\ &= 1.586 \end{aligned}$$

$$\begin{aligned} PF_{\Delta H} &= \text{power factor multiplier for } F_{\Delta H}^N \\ &= 0.3 \end{aligned}$$

$$P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$$

$$\begin{aligned} F_{\Delta H}^N &= \text{Measured values of } F_{\Delta H}^N \text{ obtained by using the movable} \\ &\text{incore detectors to obtain a power distribution map. The} \\ &\text{measured values of } F_{\Delta H}^N \text{ shall be used since an uncertainty of} \\ &4\% \text{ for incore measurement of } F_{\Delta H}^N \text{ has been included in the} \\ &\text{above limit.} \end{aligned}$$

2.7 Boron Concentration

(LCO 3.9.1)

The refueling boron concentration shall be greater than or equal to 2300 PPM.

2.8 SHUTDOWN MARGIN

(LCO 3.1.1, 3.1.4, 3.1.5, 3.1.6, & 3.1.8)

The SHUTDOWN MARGIN shall be greater than or equal to 1300 pcm
(1.3% $\Delta k/k$).

APPENDIX A

A. Input relating to LCO 3.2.1:

$$W(Z) = \frac{F_Q(Z)^{\text{max transient}}}{F_Q(Z)^{\text{steady state}}}$$

These values are issued in a controlled report which will be provided on request.

Input relating to SR 3.2.1.2

Cycle Burnup	$F_Q^W(Z)$ Penalty Factor
0	2.00
21000	2.00

Note: All cycle burnups outside of the above table shall use a 2% penalty factor for compliance with SR 3.2.1.2. Linear interpolation should be used for intermediate cycle burnups.

Technical Specification Bases 3.4.1, Applicable Safety Analysis

Cycle 12 Safety Analysis DNB Limit 1.76

WRB-2 Design Limit DNBR 1.23