

Enclosure 2

Calculation of Atmospheric Dispersion Factors - Control Room
for SQN Units 1 & 2
(56 pages)

A Record

DEC 31 2014

Westinghouse Electric Company
 P. O. Box 355
 Pittsburgh, Pennsylvania 15230

Attention: Mr. Ronald Kucharski

Gentlemen:

SEQUOYAH NUCLEAR PLANT UNITS 1 AND 2 - NUCLEAR STEAM SUPPLY SYSTEM
 MASTER SERVICES AGREEMENT - CONTRACT NO. 4411 - LETTER N10675

PURCHASE ORDER NO. 762108 - FUEL HANDLING ACCIDENT ANALYSIS - CONTROL ROOM
 ATMOSPHERIC DISPERSION FACTOR UPDATE - N2N-081

We acknowledge receipt of the document listed below submitted by Letter TVA-14-100 and return herewith one copy marked (A), "Approved".

<u>Document No.</u>	<u>Revision</u>	<u>Title</u>
FAI/14-0989	02	Sequoyah Control Room Normal and Emergency Intake Atmospheric Dispersion Factors for Auxiliary Building Stack Release, Units 1 and 2

We note that the enclosed document has been revised to remove the proprietary data designator. We have reviewed the associated document changes and find them to be satisfactory. We have approved the document revision accordingly.

The enclosed document calculates atmospheric dispersion factors for the Sequoyah control room normal and emergency intake locations for an auxiliary building stack release using the ARCON96 analysis code and the input information provided by Letter N10665. The dispersion factors have been generated to support update of the Sequoyah fuel handing accident analysis in accordance with the subject purchase order. The limiting control room dispersion factor has been applied to the fuel handing accident analysis update as requested by Item 1 of Letter N10667.

Please contact D. M. Lafever (423-751-3340) if you have any questions or comments regarding the information included in this acknowledgement.

DEC 31 2014

Westinghouse Electric Company

Page 2

Sincerely,



William J. Pierce, Engineering Director
Sequoyah Nuclear Plant

Enclosure

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B38 141231 800

*B38 141216 800, B38 141110 800, B38 141112 800



WORLD LEADER IN NUCLEAR AND CHEMICAL PROCESS SAFETY

Report No.: FAI/14-0989

*Calculation of Atmospheric Dispersion Factors
for Sequoyah Nuclear Plant*

Revision 2

Project No.: 14-0989

APPROVED

This approval does not relieve the Contractor from any part of his responsibility for the correctness of design, details and dimensions.

Letter No. N10675

Date: December 31, 2014

TENNESSEE VALLEY AUTHORITY
SOEP (N) BY: W. J. Pierce

Submitted to:

Westinghouse Electric Company
Cranberry Twp., PA

PROJECT Sequoyah DISCIPLINE N
 CONTRACT 4411 UNIT I&2
 DESC. Control Room Dispersion Factor Calc - AB Stack Release
 DWG/DOC NO. FAI/14-0989
 SHEET - OF - REV. 02
 DATE 12/31/14 ECN/DCN - FILE N2N-081

Prepared by:
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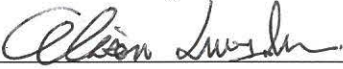
Reviewed by:
Paul McMinn

December, 2014


EDMS, WT CA-K

CALCULATION NOTE COVER SHEET (Revision 1)

SECTION TO BE COMPLETED BY AUTHOR(S):

Calc-Note Number:	<u>FAI/14-0989</u>	Revision Number:	<u>2</u>
Title:	<u>Calculation of Atmospheric Dispersion Factors for Sequoyah Nuclear Plant</u>		
Project/Subject:	<u>Sequoyah Nuclear Plant</u>	Project Number Or Shop Order:	<u>W-Sequoyah</u>
Purpose:	<u>Determine X/Q's for control room intake</u>		
Methods of Analysis*:	<u>ARCON96 under RG1.194</u>		
Acceptance Criteria*:	<u>See Section 2.2</u>		
Results Summary:	<u>See Section 1.0</u>		
*Can be N/A and/or a reference to this information in the Design Analysis can be provided.			
References of Resulting Reports, Letters, or Memoranda (Optional)			
<hr/>			
Author(s): Name (Print or Type)	Signature:	Completion Date:	
<u>Wisou Luangdilok</u>		<u>12/15/2014</u>	
_____	_____	_____	

SECTION TO BE COMPLETED BY VERIFIER(S):

Verifier(s): Name (Print or Type)	Signature:	Completion Date:	
<u>Paul B. McMinn</u>		<u>12/15/2014</u>	
_____	_____	_____	
Method of Verification:	Design Review <input type="checkbox"/>	Independent Review or Alternate Calculations <input type="checkbox"/>	Testing <input type="checkbox"/>
	3-Pass Method <input checked="" type="checkbox"/>	Other (specify): <input type="checkbox"/>	

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Responsible Manager: Name (Print or Type)	Signature:	Approval Date:
<u>Chan Y. Paik</u>		<u>12/15/2014</u>
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3-PASS VERIFICATION METHODOLOGY CHECKLIST

3-Pass Verification Review Topic	Yes	No	N/A
First Pass			
1. Were the general theme, scope of document and scope of review clear?	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Second Pass			
2. Do the references appear to be documented correctly? Is there enough information present to ensure the referenced document is retrievable?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
3. Do the acceptance criteria seem appropriate?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
4. Does the technical content of the calculation note make sense from a qualitative standpoint and are appropriate methods used?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
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5. Do the results and conclusions meet the acceptance criteria? Do the results and conclusions make sense and support the purpose of the calculation note?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
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10. Are computer code names spelled correctly? If applicable, are numerals included in the official code name as appropriate?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
11. Has the calculation note been read word-for-word, cover-to-cover?	<input type="checkbox"/>	<input checked="" type="checkbox"/>	
Reviewer Comments: The scope of this review was limited to the changes required to remove proprietary information from revision 1. This comment requires no response.			

EDITORIAL REVIEW CHECKLIST

Reviewer Name: Paul McMinn Date: 12/15/2014
Document Number: FAI/14-0989

	Yes	No	N/A
General Documents			
1. Proofread the document for general format, readability, punctuation, and grammar. Are these acceptable to you?	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
2. Is the documentation legible, reproducible and in a form suitable for archiving as a Quality Record?	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
3. Are all the pages sequentially numbered and are the document number, revision number, and appropriate proprietary classification listed on each page?	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
4. Is the Record of Revision page filled in correctly including Revision, Date, and Description of Revisions, if applicable?	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
5. Are the page numbers in the Table of Contents provided and correct?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
6. Are Acronyms defined in the document (either individually or on a separate page)?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
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12. Are all References listed referred to in the text?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
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Calc Notes			
Body of Calc Notes			
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16. Is the report revision number on each page?	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
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18. Is background information and purpose of the calculation clearly stated in the appropriate section?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
19. Have the limits of applicability been listed in the appropriate section?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
20. Are open items identified in the appropriate section and on the cover page header block?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
21. Are the Acceptance Criteria listed in the appropriate section (if applicable)?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
22. Does the Calc Note include a discussion on the methodology used?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
23. If applicable, are references to the utility, plant, unit, and cycle correct with respect to spelling and consistency of use?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
Body of Document			
24. Is the Summary of Results and Conclusions section consistent with the purpose stated and consistent with the results section?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
Computer Runs			
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29. Has the verifier provided an explanation of the method of review in the Verification Method Checklist?	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
30. Is an explanation or justification for any "NO" responses on the 3-Pass Methodology Checklist(s) presented?	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
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Additional Questions for Software Calc Notes			
32. Is the software name, version number, and system state(s) where the software was created or validated provided?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
33. Is a source code listing or reference to a controlled location of the source code included?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
34. Do the test results include the date of execution and the machine name?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
35. Do the test cases include a description of what is being tested?	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>
Editorial Reviewer Comments (if needed):			
The scope of the editorial review was limited to the changes made between revisions 1 and 2 in order to remove proprietary information.			

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1.0 Purpose and Summary

The purpose of this calculation is to determine the atmospheric dispersion factors (χ/Q [s/m^3]) for the Control Room normal and emergency intakes. The location of the source and both intakes is shown in Figure 1-1 as supplied by Reference 1.

This calculation was performed with the ARCON96 code (Reference 2). ARCON96 is an NRC accepted methodology for determining atmospheric dispersion factors χ/Q in the design basis evaluations of control room radiological analyses (Reference 3). The input parameters to the ARCON96 code were prepared according to the guidance on the use of ARCON96, as discussed in Regulatory Guide 1.194 (Reference 3).

Based on the results shown in Section 5, the recommended values for χ/Q for the Normal and Emergency Intake locations are, respectively, $2.56E-3$ [sec/m^3] and $1.57E-3$ [sec/m^3].

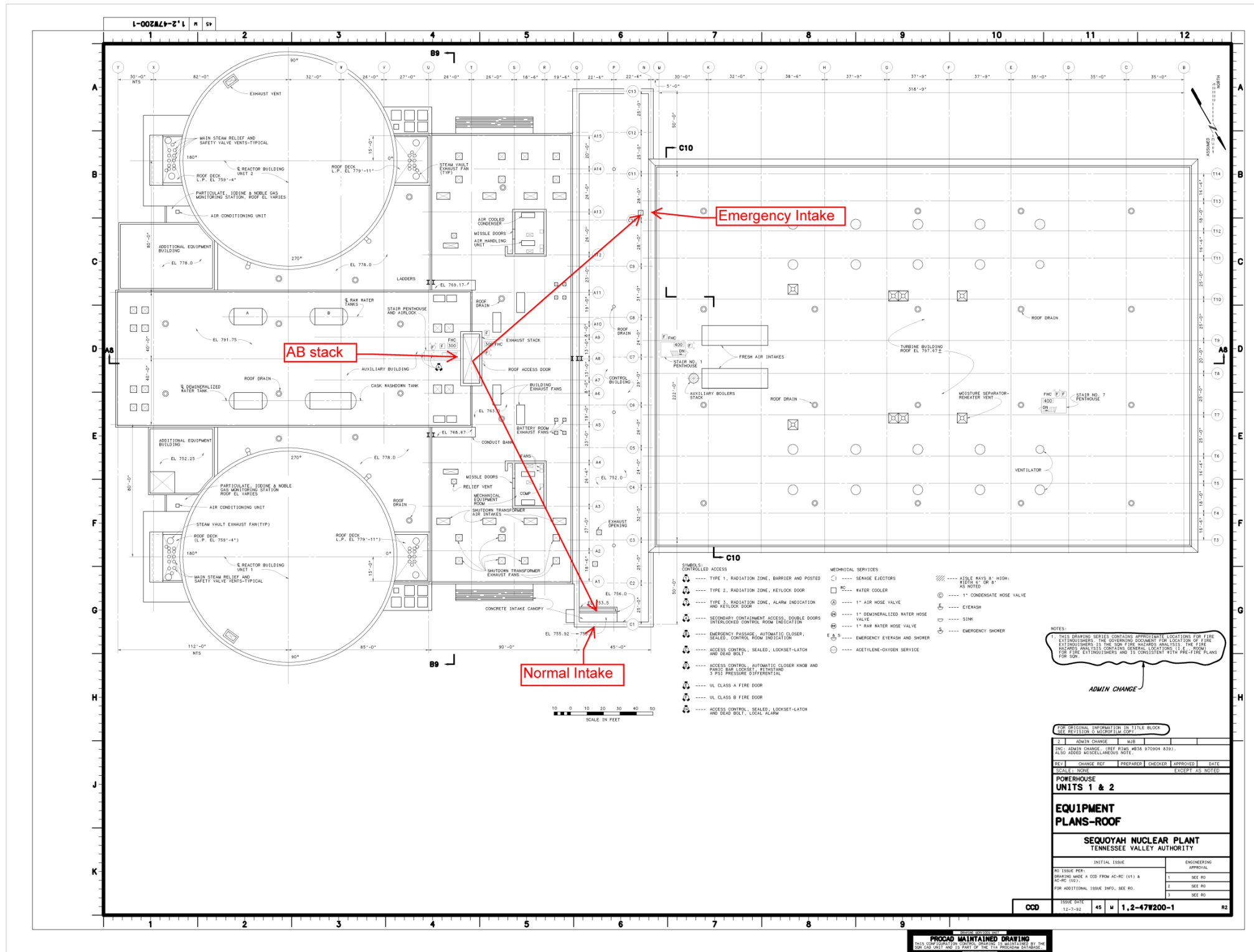


Figure 1-1 Site Arrangement for Sequoyah

2.0 Methodology

Atmospheric dispersion factors are determined with the ARCON96 code. Ten years (2004 through 2013) of site-specific meteorological data are used (Reference 1). One source and two receptors are evaluated. The receptors are the Normal Control Room Intake Vent and the Emergency Control Room Intake Vent.

All sources are treated as a point source. All releases are treated as a ground level release.

Data input to the ARCON96 code is discussed in detail in Section 3.0. The ARCON96 calculations and results are presented in Section 5.0.

2.1 ARCON96 Code

ARCON96 is a general code developed by Pacific Northwest National Laboratory for calculating atmospheric relative concentrations in plumes in building wakes under a wide range of situations. ARCON96 implements a straight line Gaussian dispersion model with dispersion coefficients that are modified to account for low wind meander and building wake effects. Hourly, normalized concentrations (χ/Q) are calculated from hourly meteorological data. The hourly values are averaged to form χ/Q 's for periods ranging from 2 to 720 hours in duration. The calculated values for each period are used to form cumulative frequency distributions and 95th percentile χ/Q values.

The May 9, 1997 version of the ARCON96 code, as described in Revision 1 of NUREG/CR-6331 (Reference 2), is an acceptable methodology for assessing control room χ/Q values for use in design basis accident (DBA) radiological analyses, subject to regulatory guidance, as discussed in U. S. NRC Regulatory Guide 1.194 (Reference 3).

The above version of ARCON96 has been obtained and maintained at FAI under the FAI quality assurance program that complies with the applicable criteria of Appendix B to 10 CFR Part 50 (Reference 4). The ARCON96 computer code was acquired from the Oak Ridge National Laboratory's Radiation Safety Information Computational Center (RSICC). ARCON96 was supplied from an external source and was placed under configuration control through FAI's procedure FAI-IG-3.5, "Dedication and Installation of External Computer Software." A validation activity was performed and documented on a PC (Intel® Core™ i7-2640M CPU) with a Microsoft Windows 7 Enterprise Version 2009 Service Pack 1 64 bit operating system (see Appendix B).

2.2 Acceptance Criteria

The acceptance criterion for determining control room χ/Q values is that the calculation is performed according to the methodology and guidelines of RG 1.194 (Reference 3).

3.0 Input to ARCON96

ARCON96 requires site specific meteorological data and plant-specific source-receptor geometric data as discussed in this section.

3.1 Meteorological Data Input

According to Position 3.1 of Reference 3, five years of Sequoyah site-specific data is a sufficiently large data set of long-term weather trends. Reference 1 provides 10 years of continuous meteorological data divided by year into the data files listed below in Table 3-1. It should be noted that 2004, 2008, and 2012 are leap years and have 24 more data points than the other years shown.

This table also provides information on the contents of the files and the number of unreadable data points. All meteorological data file contain greater than 90% usable data. This information was found by examining the *.met files and locating all entries containing a string of 9's. Such data points are excluded from processing in the ARCON96 code and represent bad data points.

Table 3-1 Meteorological Data Files

Data File Name	Description	Number of Data Points	Number of Bad Data Points (% of Total)
sqn2004.met*	2004 data file	8784	154 (1.8%)
sqn2005.met	2005 data file	8760	85 (1.0%)
sqn2006.met	2006 data file	8760	201 (2.3%)
sqn2007.met	2007 data file	8760	626 (7.1%)
sqn2008.met*	2008 data file	8784	202 (2.3%)
sqn2009.met	2009data file	8760	189 (2.2%)
sqn2010.met	2010 data file	8760	67 (0.8%)
sqn2011.met	2011 data file	8760	30 (0.3%)
sqn2012.met*	2012 data file	8784	79 (0.9%)
sqn2013.met	2013 data file	8760	199 (2.3%)

* Leap year.

The data contained in these files includes observations of wind speed, wind direction and a measure of atmospheric stability for a total of 85840 hours (not including the unreadable data points shown in the table.) Other meteorological inputs required by ARCON96 are shown below in Table 3-1. All data is supplied in Reference 1.

Table 3-2 Meteorological Input Parameters

Input Parameter	Value
Number of meteorological data files	10
Lower measurement height (m)	9.7
Upper measurement height (m)	46.4
Wind speed unit	mph

3.2 Source-Receptor Geometric Parameters

Source and receptor information is required for input. There are a number of parameters that must be calculated for individual source-receptor pairs, but there are also parameters that do not change and the same value can be used for all cases. For this analysis, only the distance to the receptor and the direction to the receptor are changed between the cases.

Table 3-3 shows a summary of input parameters related to source-receptor geometric data. All values have been supplied in Reference 1 unless noted. Two source-receptor geometric input parameters are excluded from the table: Distance and Direction. Further details are discussed in Section 3.5.

Table 3-3 Source-Receptor Geometric Data Input

Input Parameter	Discussion	Value
Release type	RG1.194 suggests that ground level release mode is appropriate for the majority of control room assessments.	Ground
Release height (m)	Calculated as mid-height of the source for each case. Value takes into account grade elevation (Reference 1)	32.5
Building area (m ²) for building wake effects	This is the vertical cross-sectional area of the Sequoyah reactor (containment) building. Calculated below in Section 3.4	1744.1
Vertical velocity (m/s)	Not used because of ground level release	0.0
Stack flow (m ³ /s)	Not used because of ground level release	0.0
Stack radius (m)	Not used because of ground level release	0.0
Control Room Intake height (m)	Control room vent intake height is the same for both intake locations.	14.3
Reference elevation difference (m)	Same reference elevation is used. There is no elevation difference. This is zero for all cases.	0.0

3.3 Dispersion Model Parameters

There are a number of dispersion model parameters used in the ARCON96 code. These parameters are referred to as "default data" in the ARCON96 user's manual (Reference 2). All of the values for these parameters have been recommended by RG-1.194 (Reference 3), as summarized below in Table 3-4:

Table 3-4 Dispersion Model Input Parameters

Input Parameter	Value
Surface roughness length (m)	0.2
Wind direction window, degrees	90
Minimum wind speed (m/s)	0.5
Averaging sector width constant	4.3
Initial diffusion coefficients (m)	0
Hours in average	Use the default values: 1, 2, 4, 8, 12, 24, 96, 168, 360, 720
Minimum number of hours	Use the default values: 1, 2, 4, 8, 11, 22, 87, 152, 324, 648

3.4 Building Area

Reference 3 suggests that the cross sectional area of the building that would have the greatest impact on building wake be used for this input. The drawings supplied in Reference 1 show that the containment structure has the greatest projected area and therefore should be used for the building area input.

The area is split between two shapes; the first is the rectangular area projected by the cylindrical containment building (Figure 3-1) and the second is the circular segment (Figure 3-2) projected from the upper containment dome. The rectangular area is calculated by using the difference in elevations shown in the drawing:

$$H = 839.0 - 705.0 = 134.0 \text{ FT}$$

The width of the rectangle is taken from the radius of the building:

$$W = 2 \times R = 2 \times 65.54167 = 131.0833 \text{ FT}$$

The area is then found to be:

$$A_R = 134.0 \times 131.0833 = 17565.167 \text{ FT}^2$$

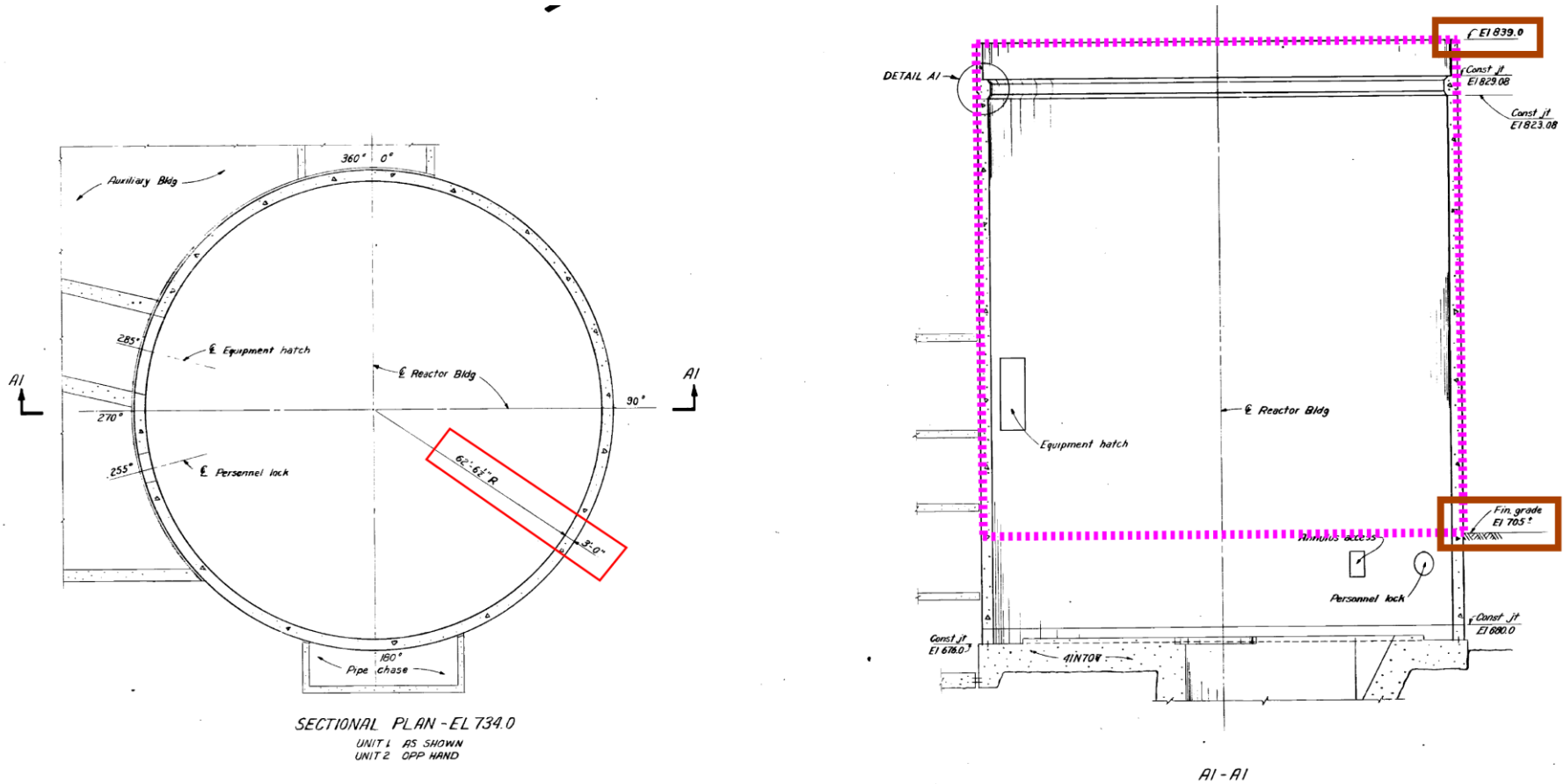


Figure 3-1 Containment Building Area – Cylindrical Building Projection

The circular segment is calculated by first calculating some simple geometric relationships, h and r from the drawings in Reference 1. The value of h is the height of the sector and is calculated based on the elevations shown in both Figure 3-1 and Figure 3-2. The value of r is the difference between the overall height of the circular sector and the distance h.

$$r = R - h$$

Where R is the radius of the circular sector. Using these values, the next step is determining the angle, θ , formed by the dome:

$$\theta = 2 \arccos\left(\frac{r}{R}\right) = 72.08^\circ$$

The area can then be found using the following relationship:

$$A_D = \frac{1}{2} R^2 (\theta - \sin \theta) = 1214.7975 \text{ FT}^2$$

The total projected area is then the sum of these:

$$A = A_R + A_D = 18779.964 \text{ FT}^2 = 1744.7 \text{ m}^2$$

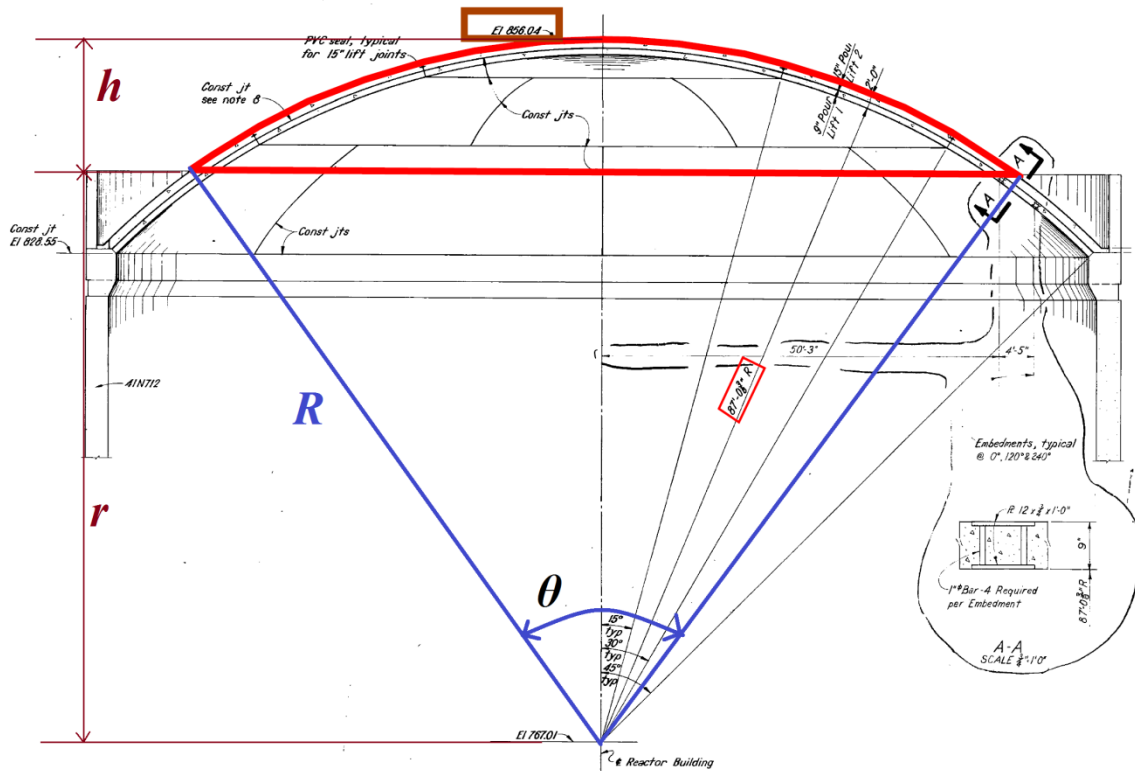


Figure 3-2 Containment Building Area – Dome Projection

3.5 Distance and Direction Input

The distances and directions calculated from plant drawings based on the definition that the source-to-receptor distance is the distance between closet points on the perimeter of the source and receptor. These points and directions are shown in the detail of the drawing supplied in Reference 1 below in Figure 3-3. The calculation of the distances and there direction are given below.

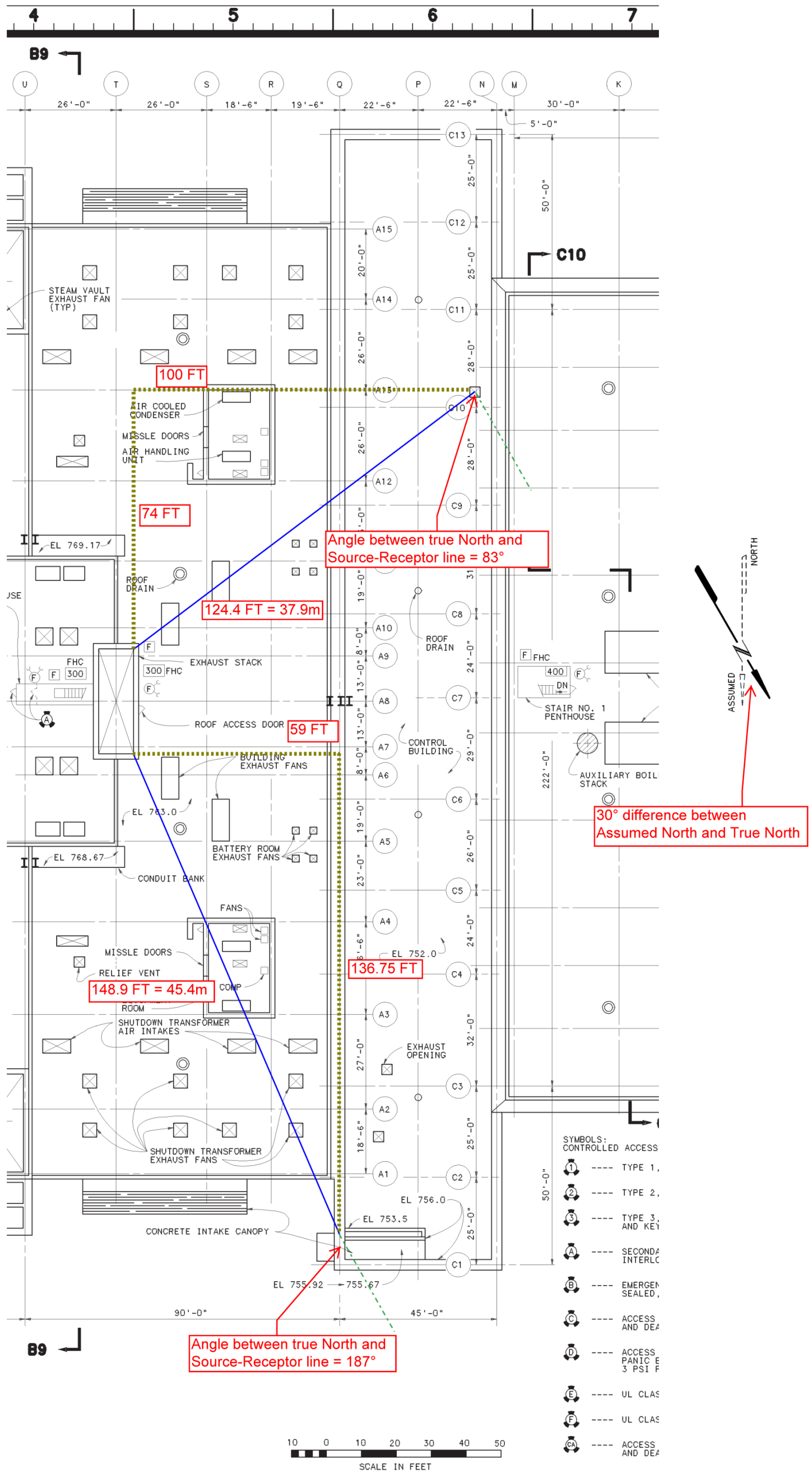


Figure 3-3 Detail from Reference 1 Drawing: Input Locations and Directions

Table 3-5 and Table 3-6 show the complete input listing for the two ARCON96 cases performed for this analysis. The cases are named for the unique direction angle for each input file as shown in the tables.

Figure 3-3 shows the locations of the release point and the two possible intake locations. The following distances and directions are calculated to augment results found by using the information supplied in Reference 1.

The horizontal distance between the release point and the intakes is calculated using the grid-like spacing indicated by the wall letters across the top of the drawing. Further adjustments are made to account for the offset between the source location and the wall grids. For the horizontal measurements, 5 FT is subtracted; the vertical direction subtracts 2 FT. For the normal location, the distances between Q-R, R-S, and S-T are used; the value being 59 FT. For the emergency intake location: N-P, P-Q, Q-R, R-S, and S-T less 4 FT from wall N for a distance of 100 FT.

Similarly, the vertical distance is calculated using the A values. Normal intake vertical distance is found using A1-A2, A2-A3, A3-A4, A4-A5, A5-A6, and A6-A7 and an estimated 16.75 FT, resulting in 136.75 FT. The emergency intake location uses A9-A10, A10-A11, A11-A12, and A12-A13: 74 FT.

From these values, the distance between the points is found using the Pythagorean Theorem and the angle between the receptors and the source is found by calculating the arctangent of the resulting triangle. For the normal intake:

$$Distance = \sqrt{59^2 + 136.75^2} = 148.9 \text{ FT} = 45.4 \text{ m}$$

$$Angle = \arctan\left(\frac{59}{136.75}\right) = 23^\circ$$

For the emergency intake:

$$Distance = \sqrt{100^2 + 74^2} = 124.4 \text{ FT} = 37.9 \text{ m}$$

$$Angle = \arctan\left(\frac{100}{74}\right) = 53^\circ$$

From Reference 3, the angle between the source and the receptor is taken from true North and is directed from the receptor to the source. Therefore, the normal intake angle must be turned 180° (to point in the proper direction) and be shifted 30° to correct toward true North. Similarly, the emergency intake must be adjusted to true North by a 30° shift. The resulting angles are 187° and 83° for the normal and emergency intakes respectively.

Table 3-5 Input for Case TVA_175 (Normal Intake Location)

	Input Parameter	Value
Meteorological	Number of meteorological data files	10
	Lower measurement height (m)	9.7
	Upper measurement height (m)	46.4
	Wind speed unit	mph
Source-Receptor Geometric	Release type	Ground
	Release height (m)	32.5
	Building area (m ²) for building wake effects	1744.7
	Vertical velocity (m/s)	0.0
	Stack flow (m ³ /s)	0.0
	Stack radius (m)	0.0
	Distance to receptor (m)	45.4
	Direction to source	187°
	Control Room Intake height (m)	14.3
	Reference elevation difference (m)	0.0
Dispersion Model	Surface roughness length (m)	0.2
	Wind direction window, degrees	90
	Minimum wind speed (m/s)	0.5
	Averaging sector width constant	4.3
	Initial diffusion coefficients (m)	0
	Hours in average	Use the default values: 1, 2, 4, 8, 12, 24, 96, 168, 360, 720
	Minimum number of hours	Use the default values: 1, 2, 4, 8, 11, 22, 87, 152, 324, 648

Table 3-6 Input for Case TVA_084 (Emergency Intake Location)

	Input Parameter	Value
Meteorological	Number of meteorological data files	10
	Lower measurement height (m)	9.7
	Upper measurement height (m)	46.4
	Wind speed unit	mph
Source-Receptor Geometric	Release type	Ground
	Release height (m)	32.5
	Building area (m ²) for building wake effects	1744.7
	Vertical velocity (m/s)	0.0
	Stack flow (m ³ /s)	0.0
	Stack radius (m)	0.0
	Distance to receptor (m)	37.9
	Direction to source	83°
	Control Room Intake height (m)	14.3
	Reference elevation difference (m)	0.0
Dispersion Model	Surface roughness length (m)	0.2
	Wind direction window, degrees	90
	Minimum wind speed (m/s)	0.5
	Averaging sector width constant	4.3
	Initial diffusion coefficients (m)	0
	Hours in average	Use the default values: 1, 2, 4, 8, 12, 24, 96, 168, 360, 720
	Minimum number of hours	Use the default values: 1, 2, 4, 8, 11, 22, 87, 152, 324, 648

3.6 Assumptions

1. Regulatory Guide 1.194 is used as guidance to the code input. All default values have been used unless noted above. Regulatory Guide 1.194 was developed in order to provide guidance on the use of ARCON96 for the calculation of χ/Q values. Therefore, for the purposes of this report, its use is justified.
2. Ground-level releases are assumed for all cases. RG 1.194 (Ref. 3) suggests that the ground-level release type is suitable for the majority of χ/Q assessments.
3. All sources are assumed to be point sources. According to RG 1.194, the use of point sources is reasonable given that the receptors are sufficiently “downwind” from the source. Given that the source-receptor distance (shortest distance is 39.5 m) for these cases is roughly an order of magnitude greater than the size of the source (approximately 7 m) (see drawings in Reference 1), it is reasonable to assume a point source.
4. The shortest source-to-receptor distances are determined from the closest point on the perimeter of the source to the closest point on the perimeter of the receptor.

4.0 References

1. TVA N10665, “Sequoyah Nuclear Plant Units 1 and 2 – Nuclear Steam Supply System Master Services Agreement – Contract No. 4411 – Letter N10665”, November 2014.
2. Ramsdell, J. V. and Simonen, C. A. Atmospheric Relative Concentrations in Building Wakes. ARCON96 Computer Code User’s Guide. s.l. : Pacific Northwest National Laboratory (PNNL), May 1997. NUREG/CR-6331, PNNL-10521, Rev. 1.
3. Nuclear Regulatory Commission (NRC). Atmospheric Relative Concentrations for Control Room Radiological Habitability Assessments at Nuclear Power Plants. June 2003. U. S. NRC Regulatory Guide 1.194.
4. Fauske & Associates, Inc. (FAI). Dedication & Installation of External or Internal FAI Generated Nonqualified Computer Software. Revision 3, 2011. FAI-IG-3.5.

5.0 Calculations and Results

The input described above in Section 3 is used to create two ASCII input files with the file extension “*.RSF”. A batch file was then created specifying the input files and calling the ARCON96 executable. A list of all computer files is given in Appendix A.

Naming convention for the input files is that the number following “TVA_” is the incident angle of receptor. This value is unique to all ARCON96 cases run for this calculation. Differences in input are described in Section 3.0.

The results of the 95th percentile χ/Q [s/m^3] values for both intake locations using TVA inputs as well as alternative inputs are summarized in Table 5-1 below. The file name for both the *.RSF and *.LOG files are also listed.

Based on the results of the ARCON96 runs, it is recommended that the following values for χ/Q should be used for dose analysis:

- Normal Intake location: 2.56E-03 [sec/m^3]
- Emergency Intake location: 1.57E-03 [sec/m^3]

Table 5-1 Summary of Results

Case Description	File Name	Averaging Period	χ/Q [s/m^3]
Intake Location: Normal Source Receptor Distance: 45.4 m Direction from Receptor to Source: 187° All other input identical.	TVA_187	0-2 hours	2.56E-03
		2-8 hours	2.20E-03
		8-24 hours	1.04E-03
		1-4 days	7.80E-04
		4-30 days	6.01E-04
Intake Location: Emergency Source Receptor Distance: 37.9 m Direction from Receptor to Source: 83° All other input identical.	TVA_083	0-2 hours	1.57E-03
		2-8 hours	6.45E-04
		8-24 hours	2.64E-04
		1-4 days	2.28E-04
		4-30 days	1.76E-04

APPENDIX A: Computer Files

Table A-1 supplies a complete list of all computer files used for this analysis. Section A.1 below also gives the complete *.LOG file output for both ARCON96 runs.

Table A-1

Item	File Name	Purpose
1	TVA_187.RSF	Input file for the Normal intake location run.
2	TVA_187.LOG	Log (results) file for the Normal intake location run.
3	TVA_083.RSF	Input file for the Emergency intake location run.
4	TVA_083.LOG	Log (results) file for the Emergency intake location run.
5	ARCON_WIN32.exe	ARCON96 Executable
6	TVA_ARCON32.BAT	Batch file used to run ARCON96
7	sqn2004.met	2004 meteorological data file
8	sqn2005.met	2005 meteorological data file
9	sqn2006.met	2006 meteorological data file
10	sqn2007.met	2007 meteorological data file
11	sqn2008.met	2008 meteorological data file
12	sqn2009.met	2009 meteorological data file
13	sqn2010.met	2010 meteorological data file
14	sqn2011.met	2011 meteorological data file
15	sqn2012.met	2012 meteorological data file
16	sqn2013.met	2013 meteorological data file

A.1 LOG File Output

TVA_187.LOG

Program Title: ARCON96.

Developed For: U.S. Nuclear Regulatory Commission
Office of Nuclear Reactor Regulation
Division of Reactor Program Management

Date: June 25, 1997 11:00 a.m.

NRC Contacts: J. Y. Lee Phone: (301) 415 1080
e-mail: jy11@nrc.gov
J. J. Hayes Phone: (301) 415 3167
e-mail: jjh@nrc.gov
L. A. Brown Phone: (301) 415 1232
e-mail: lab2@nrc.gov

Code Developer: J. V. Ramsdell Phone: (509) 372 6316
e-mail: j_ramsdell@pnl.gov

Code Documentation: NUREG/CR-6331 Rev. 1

The program was prepared for an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibilities for any third party's use, or the results of such use, of any portion of this program or represents that its use by such third party would not infringe privately owned rights.

Program Run 11/12/2014 at 08:25:01

TVA_187.LOG

***** ARCON INPUT *****

Number of Meteorological Data Files = 10

Meteorological Data File Names

sqn2004.met
sqn2005.met
sqn2006.met
sqn2007.met
sqn2008.met
sqn2009.met
sqn2010.met
sqn2011.met
sqn2012.met
sqn2013.met

Height of lower wind instrument (m) = 9.7

Height of upper wind instrument (m) = 46.4

Wind speeds entered as miles per hour

Ground-level release

Release height (m) = 32.5

Building Area (m²) = 1744.7

Effluent vertical velocity (m/s) = 0.00

Vent or stack flow (m³/s) = 0.00

Vent or stack radius (m) = 0.00

Direction .. intake to source (deg) = 187

Wind direction sector width (deg) = 90

Wind direction window (deg) = 142 - 232

Distance to intake (m) = 45.4

Intake height (m) = 14.3

Terrain elevation difference (m) = 0.0

Output file names

TVA_187.log

TVA_187.LOG

TVA_187.cfd

Minimum Wind Speed (m/s) = 0.5
 Surface roughness length (m) = 0.20
 Sector averaging constant = 4.3

 Initial value of sigma y = 0.00
 Initial value of sigma z = 0.00

Expanded output for code testing not selected

Total number of hours of data processed = 87672
 Hours of missing data = 1086
 Hours direction in window = 33711
 Hours elevated plume w/ dir. in window = 0
 Hours of calm winds = 3480
 Hours direction not in window or calm = 49395

DISTRIBUTION SUMMARY DATA BY AVERAGING INTERVAL

AVER. PER.	1	2	4	8	12	24	96	168	360	720
UPPER LIM.	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02
LOW LIM.	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06
ABOVE RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
IN RANGE	37191.	41990.	47718.	54466.	60486.	70175.	84153.	85227.	85735.	85855.
BELOW RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
ZERO	49395.	44209.	37746.	29629.	24657.	14649.	662.	32.	0.	0.
TOTAL X/Qs	86586.	86199.	85464.	84095.	85143.	84824.	84815.	85259.	85735.	85855.
% NON ZERO	42.95	48.71	55.83	64.77	71.04	82.73	99.22	99.96	100.00	100.00

95th PERCENTILE X/Q VALUES

	2.56E-03	2.49E-03	2.42E-03	2.29E-03	1.91E-03	1.46E-03	9.50E-04	8.20E-04	7.08E-04	6.47E-04
--	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------

95% X/Q for standard averaging intervals

0 to 2 hours	2.56E-03
2 to 8 hours	2.20E-03

TVA_187.LOG		
8 to 24 hours	1.04E-03	
1 to 4 days	7.80E-04	
4 to 30 days	6.01E-04	
	HOURLY VALUE RANGE	
	MAX X/Q	MIN X/Q
CENTERLINE	3.31E-03	2.34E-04
SECTOR-AVERAGE	1.93E-03	1.37E-04
NORMAL PROGRAM COMPLETION		

TVA_083.LOG

Program Title: ARCON96.

Developed For: U.S. Nuclear Regulatory Commission
Office of Nuclear Reactor Regulation
Division of Reactor Program Management

Date: June 25, 1997 11:00 a.m.

NRC Contacts: J. Y. Lee Phone: (301) 415 1080
e-mail: jy11@nrc.gov
J. J. Hayes Phone: (301) 415 3167
e-mail: jjh@nrc.gov
L. A Brown Phone: (301) 415 1232
e-mail: lab2@nrc.gov

Code Developer: J. V. Ramsdell Phone: (509) 372 6316
e-mail: j_ramsdell@pnl.gov

Code Documentation: NUREG/CR-6331 Rev. 1

The program was prepared for an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibilities for any third party's use, or the results of such use, of any portion of this program or represents that its use by such third party would not infringe privately owned rights.

Program Run 11/11/2014 at 10:46:04

***** ARCON INPUT *****

Number of Meteorological Data Files = 10
Meteorological Data File Names

TVA_083.LOG

sqn2004.met
sqn2005.met
sqn2006.met
sqn2007.met
sqn2008.met
sqn2009.met
sqn2010.met
sqn2011.met
sqn2012.met
sqn2013.met

Height of lower wind instrument (m) = 9.7
Height of upper wind instrument (m) = 46.4
Wind speeds entered as miles per hour

Ground-level release
Release height (m) = 32.5
Building Area (m²) = 1744.7
Effluent vertical velocity (m/s) = 0.00
Vent or stack flow (m³/s) = 0.00
Vent or stack radius (m) = 0.00

Direction .. intake to source (deg) = 083
Wind direction sector width (deg) = 90
Wind direction window (deg) = 038 - 128
Distance to intake (m) = 37.9
Intake height (m) = 14.3
Terrain elevation difference (m) = 0.0

Output file names
TVA_083.log
TVA_083.cfd

Minimum Wind Speed (m/s) = 0.5
Surface roughness length (m) = 0.20
Sector averaging constant = 4.3

TVA_083.LOG

Initial value of sigma y = 0.00
Initial value of sigma z = 0.00

Expanded output for code testing not selected

Total number of hours of data processed = 87672
Hours of missing data = 1086
Hours direction in window = 7383
Hours elevated plume w/ dir. in window = 0
Hours of calm winds = 3480
Hours direction not in window or calm = 75723

DISTRIBUTION SUMMARY DATA BY AVERAGING INTERVAL

AVER. PER.	1	2	4	8	12	24	96	168	360	720
UPPER LIM.	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02	1.00E-02
LOW LIM.	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06
ABOVE RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
IN RANGE	10863.	16348.	24255.	35068.	43680.	59008.	82832.	85198.	85735.	85855.
BELOW RANGE	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
ZERO	75723.	69851.	61209.	49027.	41463.	25816.	1983.	61.	0.	0.
TOTAL X/Qs	86586.	86199.	85464.	84095.	85143.	84824.	84815.	85259.	85735.	85855.
% NON ZERO	12.55	18.97	28.38	41.70	51.30	69.57	97.66	99.93	100.00	100.00

95th PERCENTILE X/Q VALUES

	1.57E-03	1.27E-03	1.05E-03	8.75E-04	6.88E-04	4.67E-04	2.88E-04	2.47E-04	2.13E-04	1.91E-04
--	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------

95% X/Q for standard averaging intervals

0 to 2 hours	1.57E-03
2 to 8 hours	6.45E-04
8 to 24 hours	2.64E-04
1 to 4 days	2.28E-04
4 to 30 days	1.76E-04

HOURLY VALUE RANGE

TVA_083.LOG		
	MAX X/Q	MIN X/Q
CENTERLINE	4.18E-03	3.72E-04
SECTOR-AVERAGE	2.44E-03	2.17E-04
NORMAL PROGRAM COMPLETION		

APPENDIX B: Software Installation and Validation

The example problems presented in Reference 2 where run on a local PC as described in Section 2.1. The log files from these runs are compared to the original log files from the distribution of ARCON96. The following printout shows the differences between corresponding log files. The only difference that is not related to I/O (i.e. run dates, leading zeroes, etc.) is example case 2. For this case, the 95th percentile value for the 8 hour averaging period is different in the last decimal (0.00177 vs. 0.00176).

```
Validation.DAT
C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>DIR
Volume in drive C is OSDisk
Volume Serial Number is A077-018D

Directory of C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE

11/11/2014  11:02 AM    <DIR>          .
11/11/2014  11:02 AM    <DIR>          ..
11/11/2014  11:00 AM    <DIR>          1997
10/29/2014  01:10 PM             480 ARCON32.BAT
03/30/2004  09:44 AM          630,784 ARCON_WIN32.exe
04/01/1995  06:00 AM          324,120 EXAMPLE.MET
03/01/2004  12:53 PM           4,829 FAI1_96.log
10/29/2014  01:10 PM          11,168 FAI1_96_2014.cfd
10/29/2014  01:10 PM           4,829 FAI1_96_2014.log
10/29/2014  01:09 PM           408 FAI1_96_2014.RSF
10/29/2014  01:10 PM          11,168 FAI2_96_2014.cfd
10/29/2014  01:10 PM           4,829 FAI2_96_2014.log
10/29/2014  01:09 PM           408 FAI2_96_2014.RSF
10/29/2014  01:10 PM          11,168 FAI3_96_2014.cfd
10/29/2014  01:10 PM           4,829 FAI3_96_2014.log
10/29/2014  01:09 PM           408 FAI3_96_2014.RSF
10/29/2014  01:10 PM          11,168 FAI4_96_2014.cfd
10/29/2014  01:10 PM           4,834 FAI4_96_2014.log
10/29/2014  01:09 PM           408 FAI4_96_2014.RSF
10/29/2014  01:10 PM          11,168 FAI5a_96_2014.cfd
10/29/2014  01:10 PM           4,829 FAI5a_96_2014.log
10/29/2014  01:09 PM           408 FAI5A_96_2014.RSF
10/29/2014  01:10 PM          11,168 FAI5b_96_2014.cfd
10/29/2014  01:10 PM           4,829 FAI5b_96_2014.log
10/29/2014  01:09 PM           408 FAI5B_96_2014.RSF
10/29/2014  01:10 PM          11,168 FAI5c_96_2014.cfd
10/29/2014  01:10 PM           4,829 FAI5c_96_2014.log
10/29/2014  01:09 PM           408 FAI5C_96_2014.RSF
10/29/2014  01:10 PM          11,168 FAI5d_96_2014.cfd
10/29/2014  01:10 PM           4,829 FAI5d_96_2014.log
10/29/2014  01:09 PM           408 FAI5D_96_2014.RSF
10/29/2014  01:10 PM          11,168 FAI5e_96_2014.cfd
```


Validation.DAT			
10/29/2014	01:10 PM	4,829	FAI5e_96_2014.log
10/29/2014	01:09 PM	408	FAI5E_96_2014.RSF
10/29/2014	01:10 PM	11,168	FAI5f_96_2014.cfd
10/29/2014	01:10 PM	4,829	FAI5f_96_2014.log
10/29/2014	01:09 PM	408	FAI5F_96_2014.RSF
10/29/2014	01:19 PM	655	FC_ARCON32.BAT
11/11/2014	11:03 AM	467	FC_ARCON32_VV.BAT
11/11/2014	09:28 AM	123	OutputTest.bat
10/29/2014	01:10 PM	11,168	PI-11A_2014.cfd
10/29/2014	01:10 PM	5,034	PI-11A_2014.log
10/29/2014	01:09 PM	576	PI-11A_2014.RSF
10/29/2014	01:10 PM	11,168	PI-11b_2014.cfd
10/29/2014	01:10 PM	5,034	PI-11b_2014.log
10/29/2014	01:09 PM	1,418	PI-11B_2014.RSF
10/29/2014	01:10 PM	11,168	PI-12a_2014.cfd
10/29/2014	01:10 PM	5,034	PI-12a_2014.log
10/29/2014	01:09 PM	576	PI-12A_2014.RSF
03/31/2004	07:59 AM	398	PI-TEST2.RSF
09/14/2000	09:09 PM	332,880	Pi93.met
09/14/2000	09:08 PM	332,880	Pi94.met
09/14/2000	09:08 PM	332,880	Pi95.met
09/14/2000	09:08 PM	332,880	Pi96.met
09/14/2000	09:07 PM	332,880	Pi97.met
10/29/2014	01:07 PM	<DIR>	PREVIOUS
11/11/2014	09:29 AM	29,641	TestData.dat
11/11/2014	11:03 AM	0	Validation.dat
	54 File(s)	2,871,128 bytes	
	4 Dir(s)	102,043,660,288 bytes free	
C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI1_96_2014.LOG 1997\EX1_96.LOG			
Comparing files FAI1_96_2014.log and 1997\EX1_96.LOG			
***** FAI1_96_2014.log			
Date: June 25, 1997 11:00 a.m.			
***** 1997\EX1_96.LOG			
Date: May 9, 1997 3:00 p.m.			

***** FAI1_96_2014.log			
Program Run 10/29/2014 at 14:10:57			
***** 1997\EX1_96.LOG			
Program Run 5/ 9/1997 at 15:03:19			

Validation.DAT		
***** FAI1_96_2014.log		
Ground-level release		
Release height (m)	=	0.0
Building Area (m^2)	=	1900.0
Effluent vertical velocity (m/s)	=	0.00
Vent or stack flow (m^3/s)	=	0.00
Vent or stack radius (m)	=	0.00
***** 1997\EX1_96.LOG		
Ground-level release		
Release height (m)	=	.0
Building Area (m^2)	=	1900.0
Effluent vertical velocity (m/s)	=	.00
Vent or stack flow (m^3/s)	=	.00
Vent or stack radius (m)	=	.00

***** FAI1_96_2014.log		
Intake height (m)	=	15.0
Terrain elevation difference (m)	=	0.0
***** 1997\EX1_96.LOG		
Intake height (m)	=	15.0
Terrain elevation difference (m)	=	.0

***** FAI1_96_2014.log		
Output file names		
FAI1_96_2014.log		
FAI1_96_2014.cfd		
Minimum Wind Speed (m/s)	=	0.5
Surface roughness length (m)	=	0.10
Sector averaging constant	=	4.0
***** 1997\EX1_96.LOG		
Output file names		
ex1_96.log		
ex1_96.cfd		
Minimum Wind Speed (m/s)	=	.5
Surface roughness length (m)	=	.10
Sector averaging constant	=	4.0

***** FAI1_96_2014.log		
Initial value of sigma y	=	0.00
Initial value of sigma z	=	0.00

Validation.DAT

***** 1997\EX1_96.LOG

Initial value of sigma y = .00
Initial value of sigma z = .00

C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI2_96_2014.LOG 1997\EX2_96.LOG
Comparing files FAI2_96_2014.log and 1997\EX2_96.LOG

***** FAI2_96_2014.log

Date: June 25, 1997 11:00 a.m.

***** 1997\EX2_96.LOG

Date: May 9, 1997 3:00 p.m.

***** FAI2_96_2014.log

Program Run 10/29/2014 at 14:10:57

***** 1997\EX2_96.LOG

Program Run 5/ 9/1997 at 15:03:28

***** FAI2_96_2014.log

Intake height (m) = 25.0
Terrain elevation difference (m) = 0.0

***** 1997\EX2_96.LOG

Intake height (m) = 25.0
Terrain elevation difference (m) = .0

***** FAI2_96_2014.log

Output file names
FAI2_96_2014.log
FAI2_96_2014.cfd

Minimum Wind Speed (m/s) = 0.5
Surface roughness length (m) = 0.10
Sector averaging constant = 4.0

***** 1997\EX2_96.LOG

Output file names
ex2_96.log

```
Validation.DAT
ex2_96.cfd
Minimum Wind Speed (m/s)      =      .5
Surface roughness length (m)  =      .10
Sector averaging constant     =      4.0
*****
***** FAI2_96_2014.log
Initial value of sigma y      =      0.00
Initial value of sigma z      =      0.00
***** 1997\EX2_96.LOG
Initial value of sigma y      =      .00
Initial value of sigma z      =      .00
*****
***** FAI2_96_2014.log
95th PERCENTILE X/Q VALUES
1.94E-03  1.93E-03  1.87E-03  1.77E-03  1.52E-03  1.10E-03
6.79E-04  5.40E-04  4.28E-04  3.28E-04
***** 1997\EX2_96.LOG
95th PERCENTILE X/Q VALUES
1.94E-03  1.93E-03  1.87E-03  1.76E-03  1.52E-03  1.10E-03
6.79E-04  5.40E-04  4.28E-04  3.28E-04
*****
C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI3_96_2014.LOG 1997\EX3_96.LOG
Comparing files FAI3_96_2014.log and 1997\EX3_96.LOG
***** FAI3_96_2014.log
Date:           June 25, 1997   11:00 a.m.
***** 1997\EX3_96.LOG
Date:           May 9, 1997    3:00 p.m.
*****
***** FAI3_96_2014.log
Program Run 10/29/2014 at 14:10:57
***** 1997\EX3_96.LOG
Program Run 5/ 9/1997 at 15:03:36
```

Validation.DAT

***** FAI3_96_2014.log

Building Area (m²) = 1730.0
Effluent vertical velocity (m/s) = 0.00
Vent or stack flow (m³/s) = 15.70

***** 1997\EX3_96.LOG

Building Area (m²) = 1730.0
Effluent vertical velocity (m/s) = .00
Vent or stack flow (m³/s) = 15.70

***** FAI3_96_2014.log

Intake height (m) = 25.0
Terrain elevation difference (m) = 0.0

***** 1997\EX3_96.LOG

Intake height (m) = 25.0
Terrain elevation difference (m) = .0

***** FAI3_96_2014.log

Output file names
FAI3_96_2014.log
FAI3_96_2014.cfd

Minimum Wind Speed (m/s) = 0.5
Surface roughness length (m) = 0.10
Sector averaging constant = 4.0

***** 1997\EX3_96.LOG

Output file names
ex3_96.log
ex3_96.cfd

Minimum Wind Speed (m/s) = .5
Surface roughness length (m) = .10
Sector averaging constant = 4.0

***** FAI3_96_2014.log

Initial value of sigma y = 0.00
Initial value of sigma z = 0.00

***** 1997\EX3_96.LOG

Initial value of sigma y = .00
Initial value of sigma z = .00

Validation.DAT

***** FAI3_96_2014.log
2 to 8 hours 8.12E-03
8 to 24 hours 4.01E-03
1 to 4 days 3.03E-03

***** 1997\EX3_96.LOG
2 to 8 hours 8.12E-03
8 to 24 hours 4.00E-03
1 to 4 days 3.03E-03

***** FAI3_96_2014.log
CENTERLINE 1.61E-02 3.99E-03
SECTOR-AVERAGE 1.12E-02 2.56E-03

***** 1997\EX3_96.LOG
CENTERLINE 1.61E-02 3.99E-03
SECTOR-AVERAGE 1.11E-02 2.56E-03

C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI4_96_2014.LOG 1997\EX4_96.LOG
Comparing files FAI4_96_2014.log and 1997\EX4_96.LOG

***** FAI4_96_2014.log

Date: June 25, 1997 11:00 a.m.

***** 1997\EX4_96.LOG

Date: May 9, 1997 3:00 p.m.

***** FAI4_96_2014.log

Program Run 10/29/2014 at 14:10:57

***** 1997\EX4_96.LOG

Program Run 5/ 9/1997 at 15:03:44

***** FAI4_96_2014.log
Release height (m) = 65.0
Building Area (m^2) = 0.0
Effluent vertical velocity (m/s) = 10.00

***** 1997\EX4_96.LOG
Release height (m) = 65.0

Validation.DAT		
Building Area (m ²)	=	.0
Effluent vertical velocity (m/s)	=	10.00

***** FAI4_96_2014.log		
Intake height (m)	=	25.0
Terrain elevation difference (m)	=	0.0
***** 1997\EX4_96.LOG		
Intake height (m)	=	25.0
Terrain elevation difference (m)	=	.0

***** FAI4_96_2014.log		
Output file names		
FAI4_96_2014.log		
FAI4_96_2014.cfd		
Minimum Wind Speed (m/s)	=	0.5
Surface roughness length (m)	=	0.10
Sector averaging constant	=	4.0
***** 1997\EX4_96.LOG		
Output file names		
ex4_96.log		
ex4_96.cfd		
Minimum Wind Speed (m/s)	=	.5
Surface roughness length (m)	=	.10
Sector averaging constant	=	4.0

***** FAI4_96_2014.log		
Initial value of sigma y	=	0.00
Initial value of sigma z	=	0.00
***** 1997\EX4_96.LOG		
Initial value of sigma y	=	.00
Initial value of sigma z	=	.00

C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI5a_96_2014.LOG 1997\EX5A_96.LOG		
Comparing files FAI5a_96_2014.log and 1997\EX5A_96.LOG		
***** FAI5a_96_2014.log		
Date:	June 25, 1997	11:00 a.m.

Validation.DAT

***** 1997\EX5A_96.LOG

Date: May 9, 1997 3:00 p.m.

***** FAI5a_96_2014.log

Program Run 10/29/2014 at 14:10:57

***** 1997\EX5A_96.LOG

Program Run 5/ 9/1997 at 15:03:54

***** FAI5a_96_2014.log

Building Area (m ²)	=	1500.0
Effluent vertical velocity (m/s)	=	0.00
Vent or stack flow (m ³ /s)	=	5.00
Vent or stack radius (m)	=	0.50

***** 1997\EX5A_96.LOG

Building Area (m ²)	=	1500.0
Effluent vertical velocity (m/s)	=	.00
Vent or stack flow (m ³ /s)	=	5.00
Vent or stack radius (m)	=	.50

***** FAI5a_96_2014.log

Intake height (m)	=	23.0
Terrain elevation difference (m)	=	0.0

***** 1997\EX5A_96.LOG

Intake height (m)	=	23.0
Terrain elevation difference (m)	=	.0

***** FAI5a_96_2014.log

Output file names
FAI5a_96_2014.log
FAI5a_96_2014.cfd

Minimum Wind Speed (m/s)	=	0.5
Surface roughness length (m)	=	0.10
Sector averaging constant	=	4.0

***** 1997\EX5A_96.LOG

Output file names
ex5a_96.log

Validation.DAT	
ex5a_96.cfd	
Minimum Wind Speed (m/s)	= .5
Surface roughness length (m)	= .10
Sector averaging constant	= 4.0

***** FAI5a_96_2014.log	
Initial value of sigma y	= 0.00
Initial value of sigma z	= 0.00
***** 1997\EX5A_96.LOG	
Initial value of sigma y	= .00
Initial value of sigma z	= .00

C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI5B_96_2014.LOG 1997\EX5B_96.LOG	
Comparing files FAI5b_96_2014.log and 1997\EX5B_96.LOG	
***** FAI5b_96_2014.log	
Date:	June 25, 1997 11:00 a.m.
***** 1997\EX5B_96.LOG	
Date:	May 9, 1997 3:00 p.m.

***** FAI5b_96_2014.log	
Program Run	10/29/2014 at 14:10:57
***** 1997\EX5B_96.LOG	
Program Run	5/ 9/1997 at 15:04:01

***** FAI5b_96_2014.log	
Building Area (m^2)	= 1500.0
Effluent vertical velocity (m/s)	= 0.00
Vent or stack flow (m^3/s)	= 5.00
Vent or stack radius (m)	= 0.50
***** 1997\EX5B_96.LOG	
Building Area (m^2)	= 1500.0
Effluent vertical velocity (m/s)	= .00

Validation.DAT		
Vent or stack flow (m ³ /s)	=	5.00
Vent or stack radius (m)	=	.50

***** FAI5b_96_2014.log		
Intake height (m)	=	23.0
Terrain elevation difference (m)	=	0.0
***** 1997\EX5B_96.LOG		
Intake height (m)	=	23.0
Terrain elevation difference (m)	=	.0

***** FAI5b_96_2014.log		
Output file names		
FAI5b_96_2014.log		
FAI5b_96_2014.cfd		
Minimum Wind Speed (m/s)	=	0.5
Surface roughness length (m)	=	0.10
Sector averaging constant	=	4.0
***** 1997\EX5B_96.LOG		
Output file names		
ex5b_96.log		
ex5b_96.cfd		
Minimum Wind Speed (m/s)	=	.5
Surface roughness length (m)	=	.10
Sector averaging constant	=	4.0

***** FAI5b_96_2014.log		
Initial value of sigma y	=	0.00
Initial value of sigma z	=	0.00
***** 1997\EX5B_96.LOG		
Initial value of sigma y	=	.00
Initial value of sigma z	=	.00

C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI5C_96_2014.LOG 1997\EX5C_96.LOG		
Comparing files FAI5c_96_2014.log and 1997\EX5C_96.LOG		
***** FAI5c_96_2014.log		
Date:	June 25, 1997	11:00 a.m.

Validation.DAT

***** 1997\EX5C_96.LOG

Date: May 9, 1997 3:00 p.m.

***** FAI5c_96_2014.log

Program Run 10/29/2014 at 14:10:57

***** 1997\EX5C_96.LOG

Program Run 5/ 9/1997 at 15:04:09

***** FAI5c_96_2014.log

Building Area (m ²)	=	1500.0
Effluent vertical velocity (m/s)	=	0.00
Vent or stack flow (m ³ /s)	=	5.00
Vent or stack radius (m)	=	0.50

***** 1997\EX5C_96.LOG

Building Area (m ²)	=	1500.0
Effluent vertical velocity (m/s)	=	.00
Vent or stack flow (m ³ /s)	=	5.00
Vent or stack radius (m)	=	.50

***** FAI5c_96_2014.log

Intake height (m)	=	23.0
Terrain elevation difference (m)	=	0.0

***** 1997\EX5C_96.LOG

Intake height (m)	=	23.0
Terrain elevation difference (m)	=	.0

***** FAI5c_96_2014.log

Output file names
FAI5c_96_2014.log
FAI5c_96_2014.cfd

Minimum Wind Speed (m/s)	=	0.5
Surface roughness length (m)	=	0.10
Sector averaging constant	=	4.0

***** 1997\EX5C_96.LOG

Output file names

Validation.DAT	
ex5c_96.log	
ex5c_96.cfd	
Minimum Wind Speed (m/s)	= .5
Surface roughness length (m)	= .10
Sector averaging constant	= 4.0

***** FAI5c_96_2014.log	
Initial value of sigma y	= 0.00
Initial value of sigma z	= 0.00
***** 1997\EX5C_96.LOG	
Initial value of sigma y	= .00
Initial value of sigma z	= .00

C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI5D_96_2014.LOG 1997\EX5D_96.LOG	
Comparing files FAI5d_96_2014.log and 1997\EX5D_96.LOG	
***** FAI5d_96_2014.log	
Date: June 25, 1997 11:00 a.m.	
***** 1997\EX5D_96.LOG	
Date: May 9, 1997 3:00 p.m.	

***** FAI5d_96_2014.log	
Program Run 10/29/2014 at 14:10:58	
***** 1997\EX5D_96.LOG	
Program Run 5/ 9/1997 at 15:04:17	

***** FAI5d_96_2014.log	
Building Area (m^2)	= 1500.0
Effluent vertical velocity (m/s)	= 0.00
Vent or stack flow (m^3/s)	= 5.00
Vent or stack radius (m)	= 0.50
***** 1997\EX5D_96.LOG	
Building Area (m^2)	= 1500.0

Validation.DAT		
Effluent vertical velocity (m/s)	=	.00
Vent or stack flow (m ³ /s)	=	5.00
Vent or stack radius (m)	=	.50

***** FAI5d_96_2014.log		
Intake height (m)	=	23.0
Terrain elevation difference (m)	=	0.0
***** 1997\EX5D_96.LOG		
Intake height (m)	=	23.0
Terrain elevation difference (m)	=	.0

***** FAI5d_96_2014.log		
Output file names		
FAI5d_96_2014.log		
FAI5d_96_2014.cfd		
Minimum Wind Speed (m/s)	=	0.5
Surface roughness length (m)	=	0.10
Sector averaging constant	=	4.0
***** 1997\EX5D_96.LOG		
Output file names		
ex5d_96.log		
ex5d_96.cfd		
Minimum Wind Speed (m/s)	=	.5
Surface roughness length (m)	=	.10
Sector averaging constant	=	4.0

***** FAI5d_96_2014.log		
Initial value of sigma y	=	0.00
Initial value of sigma z	=	0.00
***** 1997\EX5D_96.LOG		
Initial value of sigma y	=	.00
Initial value of sigma z	=	.00

C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI5E_96_2014.LOG 1997\EX5E_96.LOG		
Comparing files FAI5e_96_2014.log and 1997\EX5E_96.LOG		
***** FAI5e_96_2014.log		

Validation.DAT		
Date:	June 25, 1997	11:00 a.m.
***** 1997\EX5E_96.LOG		
Date:	May 9, 1997	3:00 p.m.

***** FAI5e_96_2014.log		
Program Run	10/29/2014	at 14:10:58
***** 1997\EX5E_96.LOG		
Program Run	5/ 9/1997	at 15:04:23

***** FAI5e_96_2014.log		
Building Area (m ²)	=	1500.0
Effluent vertical velocity (m/s)	=	0.00
Vent or stack flow (m ³ /s)	=	60.00
***** 1997\EX5E_96.LOG		
Building Area (m ²)	=	1500.0
Effluent vertical velocity (m/s)	=	.00
Vent or stack flow (m ³ /s)	=	60.00

***** FAI5e_96_2014.log		
Intake height (m)	=	23.0
Terrain elevation difference (m)	=	0.0
***** 1997\EX5E_96.LOG		
Intake height (m)	=	23.0
Terrain elevation difference (m)	=	.0

***** FAI5e_96_2014.log		
Output file names		
FAI5e_96_2014.log		
FAI5e_96_2014.cfd		
Minimum Wind Speed (m/s)	=	0.5
Surface roughness length (m)	=	0.10
Sector averaging constant	=	4.0
***** 1997\EX5E_96.LOG		
Output file names		
ex5e_96.log		
ex5e_96.cfd		

Validation.DAT		
Minimum Wind Speed (m/s)	=	.5
Surface roughness length (m)	=	.10
Sector averaging constant	=	4.0

C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI5E_96_2014.LOG 1997\EX5E_96.LOG		
Comparing files FAI5e_96_2014.log and 1997\EX5E_96.LOG		
***** FAI5e_96_2014.log		
Date:	June 25, 1997	11:00 a.m.
***** 1997\EX5E_96.LOG		
Date:	May 9, 1997	3:00 p.m.

***** FAI5e_96_2014.log		
Program Run 10/29/2014 at 14:10:58		
***** 1997\EX5E_96.LOG		
Program Run 5/ 9/1997 at 15:04:23		

***** FAI5e_96_2014.log		
Building Area (m ²)	=	1500.0
Effluent vertical velocity (m/s)	=	0.00
Vent or stack flow (m ³ /s)	=	60.00
***** 1997\EX5E_96.LOG		
Building Area (m ²)	=	1500.0
Effluent vertical velocity (m/s)	=	.00
Vent or stack flow (m ³ /s)	=	60.00

***** FAI5e_96_2014.log		
Intake height (m)	=	23.0
Terrain elevation difference (m)	=	0.0
***** 1997\EX5E_96.LOG		
Intake height (m)	=	23.0
Terrain elevation difference (m)	=	.0

***** FAI5e_96_2014.log		
Output file names		
FAI5e_96_2014.log		

Validation.DAT		
FAI5e_96_2014.cfd		
Minimum Wind Speed (m/s)	=	0.5
Surface roughness length (m)	=	0.10
Sector averaging constant	=	4.0
***** 1997\EX5E_96.LOG		
Output file names		
ex5e_96.log		
ex5e_96.cfd		
Minimum Wind Speed (m/s)	=	.5
Surface roughness length (m)	=	.10
Sector averaging constant	=	4.0

C:\LIBRARY\SEQUOYAH\DOCUMENTATION\SOFTWARE>FC FAI5F_96_2014.LOG 1997\EX5F_96.LOG		
Comparing files FAI5f_96_2014.log and 1997\EX5F_96.LOG		
***** FAI5f_96_2014.log		
Date:	June 25, 1997	11:00 a.m.
***** 1997\EX5F_96.LOG		
Date:	May 9, 1997	3:00 p.m.

***** FAI5f_96_2014.log		
Program Run 10/29/2014 at 14:10:58		
***** 1997\EX5F_96.LOG		
Program Run 5/ 9/1997 at 15:04:32		

***** FAI5f_96_2014.log		
Building Area (m^2)	=	1500.0
Effluent vertical velocity (m/s)	=	0.00
Vent or stack flow (m^3/s)	=	20.00
***** 1997\EX5F_96.LOG		
Building Area (m^2)	=	1500.0
Effluent vertical velocity (m/s)	=	.00
Vent or stack flow (m^3/s)	=	20.00

***** FAI5f_96_2014.log		
Intake height (m)	=	23.0
Terrain elevation difference (m)	=	0.0

Validation.DAT

```
***** 1997\EX5F_96.LOG
      Intake height (m)           =      23.0
      Terrain elevation difference (m) =      .0
```

```
***** FAI5f_96_2014.log
      Output file names
      FAI5f_96_2014.log
      FAI5f_96_2014.cfd
```

```
      Minimum Wind Speed (m/s)     =      0.5
      Surface roughness length (m)  =      0.10
      Sector averaging constant     =      4.0
```

```
***** 1997\EX5F_96.LOG
      Output file names
      ex5f_96.log
      ex5f_96.cfd
```

```
      Minimum Wind Speed (m/s)     =      .5
      Surface roughness length (m)  =      .10
      Sector averaging constant     =      4.0
```
