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4 DRAFT SAFETY EVALUATION BY THE U.S. NUCLEAR REGULATORY COMMISSION FOR
5
6 ANALYSIS AND MEASUREMENT SERVICES CORPORATION TOPICAL REPORT
7
8 AMS-TR-0720R1, "ONLINE MONITORING TECHNOLOGY TO EXTEND CALIBRATION
9
10 INTERVALS OF NUCLEAR PLANT PRESSURE TRANSMITTERS"
11
12 BY THE OFFICE OF NUCLEAR REACTOR REGULATION
13
14 (EPID NO. L-2020-TOP-0037)
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16

17 1.0 INTRODUCTION
18

19 By letter dated July 10, 2020 (Ref. 1), as supplemented by letter dated October 9, 2020 (Ref. 2),
20 Analysis and Measurement Services Corporation (AMS) submitted the Topical Report (TR)
21 AMS-TR-0720R1, "Online Monitoring [(OLM)] Technology to Extend Calibration Intervals of
22 Nuclear Plant Pressure Transmitters." AMS requested a formal review of the AMS OLM TR in
23 accordance with the U.S. Nuclear Regulatory Commission (NRC) TR program.
24

25 The NRC staff performed an audit (Refs. 5, 6, and 7) of the documentation materials which
26 support AMS positions and statements regarding the efficacy of OLM methodologies. The NRC
27 staff issued request for additional information (RAI) questions (Ref. 3) to obtain information
28 needed to complete this safety evaluation (SE). AMS provided the responses to these RAI
29 questions and described revisions to the AMS OLM TR in Reference 4 to address the NRC
30 staff's RAI questions.
31

32 2.0 REGULATORY EVALUATION
33

34 The NRC staff considered the following regulatory requirements and guidance in reviewing the
35 concepts presented in AMS OLM TR:
36

- 37 • Title 10 of the *Code of Federal Regulations* (10 CFR) 50.36(c)(1)(ii)(A) states that limiting
38 safety system settings are settings for automatic protective devices related to those
39 variables having significant safety functions. This clause requires that where a limiting
40 safety system setting (LSSS) is specified for a variable on which a safety limit has been
41 placed, the setting must be chosen so that automatic protective action will correct the
42 abnormal situation before a safety limit is exceeded. It also requires that the licensee
43 notify the NRC if the licensee determines that an automatic safety system does not
44 "function as required." The licensee is then required to review the matter and record the
45 results of the review.
46
- 47 • 10 CFR 50.36(c)(3) states, "Surveillance requirements are requirements relating to test,
48 calibration, or inspection to assure that the necessary quality of systems and components
49 is maintained, that facility operation will be within safety limits, and that the limiting
50 conditions for operation will be met."
51

- 10 CFR 50.55a(h), "Protection and safety systems," states the following "Protection Systems. For nuclear power plants with construction permits issued after January 1, 1971, but before May 13, 1999, protection systems must meet the requirements in IEEE Std 279-1968, "Proposed IEEE Criteria for Nuclear Power Plant Protection Systems," or the requirements in IEEE Std 279-1971, "Criteria for Protection Systems for Nuclear Power Generating Stations," or the requirements in IEEE Std 603-1991, "Criteria for Safety Systems for Nuclear Power Generating Stations, and the correction sheet dated January 30, 1995. For nuclear power plants with construction permits issued before January 1, 1971, protection systems must be consistent with their licensing basis or may meet the requirements of IEEE Std. 603-1991 and the correction sheet dated January 30, 1995.

Safety systems. Applications filed on or after May 13, 1999, for construction permits and operating licenses under this part, and for design approvals, design certifications, and combined licenses under Part 52 of this chapter, must meet the requirements for safety systems in IEEE Std. 603-1991 and the correction sheet dated January 30, 1995.

Clause 4.3, "Quality of Components and Modules," of IEEE 279-1971 states that components and modules shall be of a quality that is consistent with minimum maintenance requirements and low failure rates. Quality levels shall be achieved through the specification of requirements known to promote high quality, such as requirements for design, for the derating of components, for manufacturing, quality control, inspection, calibration, and test.

Clause 6.5.1 of IEEE 603-1991 states that means shall be provided for checking, with a high degree of confidence, the operational availability of each sense and command feature input sensor required for a safety function during reactor operation. This may be accomplished in various ways, for example:

- a) By perturbing the monitored variable,
- b) Within the constraints of 6.6, by introducing and varying, as appropriate, a substitute input to the sensor of the same nature as the measured variable, or
- c) By cross-checking between channels that bear a known relationship to each other and that have readouts available.

Clause 6.5.2 of IEEE 603-1991 states that one of the following means shall be provided for assuring the operational availability of each sense and command feature required during the post-accident period:

- a) Checking the operational availability of sensors by use of the methods described in 6.5.1.
 - b) Specifying equipment that is stable and the period of time it retains its calibration during the post-accident time period.
- Appendix A to 10 CFR Part 50, General Design Criterion (GDC) 13, "Instrumentation and control," requires that instrumentation be provided to monitor variables and systems over

1 their anticipated ranges for normal operation, for anticipated operational occurrences, and
2 for accident conditions, as appropriate, to assure adequate safety, including those
3 variables and systems that can affect the fission process, the integrity of the reactor core,
4 the reactor coolant pressure boundary, and the containment and its associated systems.
5 Appropriate controls shall be provided to maintain these variables and systems within
6 prescribed operating ranges.
7

- 8 • Appendix A to 10 CFR Part 50, GDC 20, "Protection system functions," states that the
9 protection system shall be designed a) to initiate automatically the operation of
10 appropriate systems including the reactivity control systems, to assure that specified
11 acceptable fuel design limits are not exceeded as a result of anticipated operational
12 occurrences and b) to sense accident conditions and to initiate the operation of systems
13 and components important to safety.
14

15 The following are the specific NRC guidance documents applicable to the NRC staff's evaluation
16 of the AMS OLM TR:
17

- 18 • NUREG-0800, Standard Review Plan for the Review of Safety Analysis Reports for
19 Nuclear Power Plants: LWR [Light Water Reactor] Edition, Branch Technical Position
20 (BTP) 7-12, "Guidance on Establishing and Maintaining Instrument Setpoints"
21
- 22 • Regulatory Guide (RG) 1.105 Revision 4, "Setpoints for Safety-Related Instrumentation."
23 This RG describes an approach that is acceptable to the NRC staff to meet regulatory
24 requirements to ensure that: a) setpoints for safety-related instrumentation are
25 established to protect nuclear power plant safety and analytical limits, and b) the
26 maintenance of instrument channels implementing these setpoints ensures they are
27 functioning as required, consistent with the plant technical specifications (TS).
28

29 This RG endorses American National Standards Institute (ANSI)/International Society of
30 Automation (ISA) Standard 67.04.01-2018, "Setpoints for Nuclear Safety-Related
31 Instrumentation." Among other things, the ANSI/ISA 67.04.01 standard provides criteria
32 for assessing the performance of safety related instrument channels to ensure they
33 remain capable of achieving their required safety functions in a reliable manner. This
34 performance monitoring process requires the establishment of acceptable "As-Found"
35 tolerance limits used to check whether an instrument channel is functioning as required,
36 and the establishment of acceptable "As-Left" tolerance limits used to establish the
37 maximum allowed deviation from the desired setpoint of the instrument channel and still
38 be considered as "within calibration."
39

40 The following other guidance documents provide information associated with the periodic
41 calibration of safety related instrument channels that was considered by the NRC staff during its
42 evaluation of the AMS OLM Topical Report:
43

- 44 • Generic Letter 91-04, "Changes in Technical Specification Surveillance Intervals To
45 Accommodate a 24-Month Fuel Cycle," dated April 2, 1991, provides guidance on
46 acceptable methods for licensees to justify an increase in calibration surveillance intervals
47 using as-found and as-left calibration data from past calibration surveillances.
48

- 1 • Regulatory Issue Summary (RIS) 2006-017, "NRC Staff Position on the Requirements of
2 10 CFR 50.36, 'Technical Specifications,' regarding Limiting Safety System Settings
3 during Periodic Testing and Calibration of Instrument Channels," dated August 24, 2006
4 provides regulatory clarification on NRC staff positions in terms of the appropriate
5 determination of TS-related instrument channel operability. The RIS clarifies NRC staff
6 positions about the appropriate establishment of as-found and as-left acceptance
7 tolerances.
8
- 9 • Technical Specification Task Force (TSTF) Traveler TSTF-493, Revision 4, "Clarify
10 Application of Setpoint Methodology for LSSS Functions," dated May 11, 2010, provides
11 guidance about the maintenance of instrument setpoints during periodic surveillances.
12

13 3.0 TECHNICAL EVALUATION

14
15 The NRC staff reviewed the AMS OLM TR to determine if the proposed condition based methods
16 for performing OLM can be used as an acceptable alternative means to identify whether a
17 transmitter needs to be surveilled at the next frequency-based calibration surveillance opportunity
18 as specified in plant TS surveillance requirements. Specifically, the NRC staff evaluated
19 materials referenced in the AMS OLM TR to verify that adequate evidence exists for using OLM
20 methods to determine when a calibration check, or a full calibration if necessary, is required for
21 plant pressure and differential pressure type transmitter instruments (e.g., incorporated as a
22 programmatic alternative to using a surveillance frequency as specified in the plant TS). Such
23 pressure and differential pressure transmitter type devices are typically used in nuclear power
24 plant safety applications to monitor key reactor and containment systems pressure, level, and
25 flow parameters.
26

27 3.1. Overview of the AMS OLM TR Methods

28
29 The AMS OLM TR provides a methodology for performing OLM of the output signals of pressure
30 and differential pressure transmitters. This methodology was developed to be used in nuclear
31 power plants as an analytical tool to measure sensor calibration performance during plant
32 operation between scheduled refueling outages, which are typically the times when plant TS
33 surveillance requirements for transmitters are fulfilled. The use of OLM technology enables
34 licensees to identify pressure sensors that have potential calibration performance issues during
35 plant operation rather than relying upon information gained during periodic calibration tests that
36 are performed infrequently (i.e., during refueling outages).
37

38 If a pressure or differential pressure transmitter output signal appears to deviate beyond a
39 predetermined allowable range from an average of output signals from a group of transmitters
40 measuring the same parameter, the transmitter is flagged to the analyst as needing a calibration
41 check. Calibration checks could then be scheduled and performed on those identified sensors
42 using traditional calibration procedures during a subsequent plant outage. Alternatively, careful
43 analysis of OLM data may be used to determine there is adequate evidence that a transmitter is
44 performing acceptably and does not need to be re-calibrated at the next scheduled TS
45 surveillance opportunity.
46

47 The methodology described in the AMS OLM TR includes processes for performing the following
48 activities:
49

- 1 • Establishing an OLM program and determining which plant sensors may be included in
2 the program.
- 3
- 4 • Establishing the maximum time period that a group of redundant sensors can operate
5 without at least one being calibrated as a defense against the possibility of common mode
6 drift.
- 7
- 8 • Establishing criteria for performing data acquisition during plant operation for each sensor
9 group.
- 10
- 11 • Retrieving redundant sensor measurements using the process plant computer or other
12 data acquisition system.
- 13
- 14 • Calculating the average of these process measurements and the deviation of each sensor
15 from the average.
- 16
- 17 • Establishing acceptance limits (monitoring limits) for identifying those transmitters
18 exhibiting excessive deviation from average.
- 19
- 20 • Identifying sensors that have deviated beyond predetermined monitoring limits.
- 21
- 22 • Initiating calibration activities to be performed for sensors that have exceeded OLM
23 calibration limits.
- 24
- 25 • Establishing a noise analysis methodology to enable licensees to assess the occurrence
26 of dynamic failure modes of transmitters that are not covered by the OLM process for
27 transmitter drift monitoring.
- 28

29 The AMS OLM TR is intended to be used by licensees to support plant-specific TS changes to
30 allow transition from time-based periodic calibration surveillance programs for pressure, level,
31 and flow transmitters to condition-based calibration programs based on OLM results. The TR
32 also provides licensees with guidance on how to develop procedures to detect sensing line
33 blockages (as well as other dynamic failure modes) using ~~a-the OLM-Noise~~ Aanalysis
34 technique.

35 36 3.2. Applicability of the AMS OLM TR Methods

37
38 The condition monitoring methodology described in AMS OLM TR focuses on the application of
39 OLM for monitoring calibration performance of pressure, level, and flow transmitters using
40 pressure and differential pressure type sensing devices in nuclear power plants. Therefore, the
41 applicability of this SE is limited to applications involving nuclear plant pressure, level, and flow
42 transmitters using pressure and differential pressure type sensors. The use of OLM technologies
43 for other types of sensors is not approved by the NRC in this SE and must therefore be evaluated
44 separately.

45
46 AMS OLM TR, Section 11, "OLM Implementation Methodology," includes specific steps to
47 determine which pressure, level, and flow transmitters can be included in a plant-specific OLM
48 program. This determination is based, in part, on which transmitters (i.e., make and model –
49 refers to Chapter 12) were included in prior drift studies, or a transmitter's similarity to the studied

1 transmitters. Other considerations relating to the applicability of the AMS OLM TR to a plant
2 specific application are discussed in the sections below.

3
4 3.3. Failure Mode Detection using OLM

5
6 Section 3.4 of the AMS OLM TR describes transmitter failure modes that have been experienced
7 and explains how OLM techniques can be used to identify these failures. The TR refers to two
8 failure modes and effects analyses (FMEA) that were performed by EPRI and provides
9 summaries of the main conclusions of these reports. These summaries explain that transmitter
10 failures manifest themselves by affecting transmitter calibration or response time. Both effects
11 are detectable to an extent by applying the OLM methods described in Section 11 of the AMS
12 OLM TR.

13
14 The failure modes of the following types of transmitters were considered in the referenced
15 FMEAs:

- 16
- 17 • Force Balance Transmitters
- 18
- 19 • Strain Gage Transmitters
- 20
- 21 • Capacitance Transmitters
- 22

23 A total of 35 different failure modes were identified and 31 of these failure modes were
24 determined to be identifiable by applying OLM-Drift Monitoring techniques. The failure modes
25 that are not detectable by OLM-Drift Monitoring were further analyzed as follows:

- 26
- 27 • **Change in viscosity of the fill fluid (Common to all three transmitter types)** – The TR
28 explains this failure mode is usually caused by changes in environmental conditions to which
29 the transmitter is subjected. The TR also explains that normal variations in the conditions
30 that could produce this failure mode are considered in the “design-basis” of the transmitters.
31 The TR states that “beyond-design-basis” conditions are unlikely because equipment
32 qualification (EQ) performed on safety-related transmitters would reveal such failures.
33

34 The NRC staff notes that requirements for instruments to remain functional under normal
35 operation, maintenance, testing, and postulated accident conditions, including loss-of-coolant
36 accidents are provided within GDC 4, “Environmental and dynamic effects design basis,”
37 which is applied to structures, systems, and components important to safety. It is therefore
38 reasonable to assume that environmental conditions beyond those specified in GDC 4 would
39 not be experienced for the transmitters for which OLM techniques would be applied.
40 Therefore, the failure modes associated with those conditions would not need to be
41 considered. The NRC staff also notes that current periodic calibration programs do not
42 include verification of transmitter functionality under environmental conditions that would
43 cause these failure modes.

- 44
- 45 • **Blockage of holes in the ceramic inserts used in capacitance transmitters** – This failure
46 mode is unique to Capacitance type transmitters. The AMS OLM TR explains that the
47 ceramic insert holes serve the purpose of transporting fill fluid between the isolation
48 diaphragm and the sensing diaphragm. If the flow of fluid through these holes becomes
49 restricted, then transmitter response time can degrade.

1 The NRC staff notes that current periodic calibration programs do not include verification of
2 transmitter response time functionality that would be affected by this failure mode. Though
3 an OLM-~~Drift Monitoring~~ program would not increase the ability to identify this failure mode
4 during surveillance testing, it would not reduce the ability to detect the failure mode.
5 However, Section 11.3 of the AMS OLM TR described how to assess dynamic failure modes
6 of transmitters using the ~~OLM-Noise Analysis~~ technique in addition to ~~monitoring for~~
7 ~~drift~~~~OLM-Drift Monitoring~~.
8

9 3.4. Response Time Testing using OLM

10
11 The OLM-~~Drift Monitoring~~ processes described in the AMS OLM TR have a limited ability to
12 identify transmitter response time degradation. The degree to which such degradation can be
13 identified is dependent on several factors including the rate of data collection used for OLM and
14 the dynamic characteristics of the process being measured by the transmitters.
15

16 For more dynamic processes that have a higher degrees of signal variation, OLM-~~dynamic-Noise~~
17 ~~analysis-Analysis~~ techniques can be an effective way to assess whether a transmitter response
18 has degraded. These ~~dynamic-analysis~~~~OLM-Noise Analysis~~ techniques include comparing
19 transmitter responses to process signal variations of other transmitters which are measuring the
20 same process (see AMS OLM TR, Section 11.3). The NRC staff believes that such capability to
21 detect whether a transmitter's response time is degrading is a useful indication for monitoring
22 transmitter performance between scheduled surveillance opportunities to determine whether a
23 transmitter is "functioning as required."
24

25 3.5. Response Time Safety Related Test Elimination

26
27 Many operating nuclear power plants have eliminated safety related requirements to perform
28 periodic response time (RT) testing. The justification for eliminating RT test requirements often
29 refers to the performance of periodic calibration safety related tests. Licensee's implementing
30 OLM programs should review the basis for eliminating RT tests as applicable to determine if the
31 OLM program can become a suitable substitute for the periodic calibration test programs that are
32 credited in the plant TS. The basis for RT elimination may need to be modified to credit the AMS
33 ~~OLM-Noise Analysis technique -TR program~~ in Section 11.3 in lieu of a periodic calibration
34 program.
35

36 The AMS OLM TR does not provide guidance for re-evaluating the basis for RT test elimination
37 or TS mark-ups for making changes to the basis for elimination of RT testing. Therefore, an
38 application specific action item is included to ensure that a licensee considers the effects of an
39 OLM program would have on the basis for RT testing elimination. This is applicant specific
40 action item (ASAI) 3 in Section 4.0 of this SE.
41

42 3.6. Addressing Common Mode Drift Hazards

43
44 The NRC staff recognized that OLM methods could work well to identify whether the output
45 signals of one or more transmitters out of a group of transmitters monitoring the same plant
46 process has deviated from the average of the outputs of all the transmitters in the same group.
47 However, the NRC staff was concerned that it was possible for a common mode instrument
48 performance effect to adversely impact all the transmitters within the group simultaneously, and
49 that OLM data analysis would not detect the fact that all transmitters were simultaneously being
50 affected.

1
2 Therefore, the NRC staff requested AMS to provide an evaluation of nuclear power plant industry
3 transmitter performance data that was analyzed using OLM methods to determine if there was
4 historical evidence indicating the likelihood that common mode drift effects could occur but not be
5 subsequently detected. AMS provided several examples of evaluations of OLM data collections
6 that compared the results of OLM data evaluations determining whether a transmitter appears to
7 be performing satisfactorily while in operations, against evaluations of calibration performance
8 data taken from the next scheduled calibration surveillance for those same transmitters (Refs. 4
9 and 11).

10
11 The evaluations indicated there was a very strong agreement between the two sets of data. Out
12 of hundreds of transmitter calibration performance data evaluated, only a very small number of
13 cases indicated a disagreement as to whether a transmitter remained within acceptable
14 performance requirements. None of these cases indicated that a common mode drift effect was
15 occurring among a group of transmitters monitoring the same parameter. The few cases where a
16 disagreement between OLM data analysis and traditional calibration methods existed had
17 plausible explanations as to why the disagreement occurred, and usually these were associated
18 with potential errors (e.g., imprecise calibration method or inappropriate measurement and test
19 equipment performance) in the traditional calibration method.

20
21 Further, AMS provided a summary of data analysis they performed for the Sizewell B nuclear
22 power plant located on the eastern coast of Great Britain. The Sizewell B plant has been using
23 OLM methods for identifying transmitters that need calibration checks for many fuel cycles.
24 Throughout the duration of this OLM data evaluation process there has been no evidence of
25 occurrence of common mode drift.

26
27 However, should an undetected common mode drift effect could occur, the AMS OLM TR
28 Implementation methodology includes a process for addressing the potential for mitigating the
29 effects of common mode drift among process transmitter groups. This mitigation is accomplished
30 using a calibration surveillance interval "backstop." By using this methodology, licensees will
31 analyze calibration data for common mode drift hazards and will assign shorter calibration
32 backstop intervals for process groups that appear to have greater risk of exhibiting common
33 mode drift characteristics.

34
35 Chapter ~~42-13~~ of the TR describes the method used for establishing backstop calibration
36 intervals. The NRC staff concludes that the use of this extension interval backstop approach will
37 serve to ensure that the possibility for undetectable common mode drift effects will be mitigated.
38 This is addressed as ASAI 4 in Section 4.0 below.

39 40 3.7. Maintaining Prime Standard Traceability

41
42 Instrument groups to be included in a licensee's OLM calibration program are assigned initial
43 maximum calibration intervals called backstop intervals based on available performance data for
44 the transmitters in the process group. At least one transmitter in each process group is then
45 calibrated at this interval. These maximum calibration backstop intervals can be subsequently
46 adjusted as supported by OLM performance data collected.

47
48 Chapter ~~42-13~~ of the TR describes a method for establishing backstop calibration intervals for
49 each process group of transmitters. By performing a standard calibration of one transmitter in
50 each process group at the pre-determined interval, traceability to calibration prime standards is

1 established and maintained for the instrument group.

2 3.8. Process dynamics and their effects on OLM methods

3
4 The effectiveness of OLM methods in determining transmitter responsiveness is dependent on
5 the dynamic characteristics of the process being measured. Highly stable processes may
6 therefore require higher sample rates and greater data collection requirements to establish an
7 equivalent level of confidence in transmitter responsiveness and performance when compared
8 with transmitters measuring more dynamic processes. The OLM process described in the TR
9 includes performance of an assessment of each process monitored by a group of transmitters to
10 be considered for OLM. This assessment characterizes the measured process to determine the
11 necessary sample rate and duration criteria for OLM to be applied to the group.

12
13 The OLM process states that data must be collected during startup, normal operation, and
14 shutdown periods at the highest sampling rate by which the plant computer takes data. The OLM
15 program also includes a method for determining the minimum sample rate for data collection
16 during operation that is based on the dynamic characteristics of the process being measured by
17 the instrument group. In cases where the minimum data collection rate cannot be achieved by
18 the plant computer, an alternative data acquisition system can be used. The actions for
19 performing this method are included in Chapter 11 and a description of the process for
20 determining required sample rates and durations is included in Chapter ~~12-15~~ of the TR.

21
22 3.9. Comparison of OLM Program to Periodic Calibration Program

23
24 Section 3.1, "CONVENTIONAL CALIBRATIONS VERSUS OLM," of the AMS OLM TR provides a
25 comparison between an OLM program and a conventional periodic calibration program. This
26 includes an analysis of calibration data collected from the McGuire Nuclear Power Plant over two
27 complete refueling cycles. The results of this analysis are documented in NUREG/CR-5903
28 (1993) and NUREG/CR-6343 (1995). The AMS OLM TR states that about 90 percent of plant
29 pressure, level and flow transmitters maintain their calibration for longer than a typical fuel cycle.
30 This statement is derived from calibration data showing that approximately 10 percent of the
31 transmitters that were calibrated required calibration adjustments to restore calibration to within
32 as-left tolerances.

33
34 Three calibration drift studies were referenced in the AMS OLM TR as follows:

- 35
36
- 37 • 3.3.1 EPRI TR104965 Drift Study – This study used manual calibration data from
38 eighteen nuclear power plants to support extension of calibration intervals for nuclear
39 plant pressure, level, and flow transmitters. The study used data from transmitter
40 calibration records for multiple transmitter manufacturer types.
 - 41 • 3.3.2 PWROG Drift Study to support Technical Specification Task Force - TSTF-425 –
42 This was a drift analysis performed on Westinghouse PWRs to support extending
43 transmitter calibration intervals one cycle at a time. The analysis was performed using
44 calibration records from forty-one PWR units representing three nuclear steam supply
45 system (NSSS) vendors and five transmitter manufacturers.
 - 46 • 3.3.3 Sizewell Nuclear Power Plant Drift Studies – Two drift studies were performed which
47 involved statistical analysis of manual calibration records over a seven-year period to
48 establish the drift behavior of its safety-related transmitters. This study used data from
49 five different transmitter models.
- 50

1
2 Though the objectives and conclusions of each study are unique, all of these studies showed that
3 transmitter calibration drift occurs in a random and non-biased manner and that a large
4 percentage of these transmitters do not drift enough to require calibration adjustments during a
5 single refueling interval. The data used for these studies also demonstrates that when calibration
6 drift does occur to the extent that manual calibrations are needed, the OLM techniques can be
7 used to identify the need for such calibrations.
8

9 Section 9, "OLM Implementation in U.S. Plants," of the AMS OLM TR provides an overview of
10 AMS's experience with implementing OLM programs at several operating U.S. nuclear power
11 plants. The AMS OLM TR states that together with OLM implementation at Sizewell B and
12 McGuire, these projects provide the foundation for the development of the generic OLM
13 methodology of the AMS OLM TR. Section 10 of the AMS OLM TR provides a comparison of
14 results between performing manual calibrations and performing OLM. This comparison study
15 uses calibration performance data collected from multiple plants over time period extending back
16 to the mid 1980's. The study also references several other studies conducted by EPRI, AMS,
17 and the NRC during the last 30 years.
18

19 The data from Sizewell was used to perform an objective comparative analysis between OLM
20 and manual calibration results. This analysis was possible because both calibration programs
21 were simultaneously in effect when data was obtained. The detailed results of this comparison
22 are provided in Section 10.1.3 of the AMS OLM TR and are summarized as follows:
23

- 24 1. The OLM and manual calibration results were the same for 81.8 percent of the
25 calibrations performed. This means that transmitters requiring calibration adjustments
26 could be identified in advance of the manual calibration procedure by using OLM
27 techniques.
28
- 29 2. For 17.7 percent of the calibrations, OLM identified the transmitters as having drifted
30 beyond their OLM tolerances while manual calibrations of those same transmitters
31 showed no significant drift that would have required calibration adjustment.
32
- 33 3. About 0.5 percent of the calibrations were found to be bad by manual calibrations that
34 were not identified by OLM techniques. The analysis however concluded that such
35 discrepancies are acceptable because they are an improvement over the conventional
36 practices where a higher percentage of human errors and miscalibrations would have
37 typically occurred over the same period.
38

39 The NRC staff reviewed the operational calibration and OLM data provided in the AMS
40 OLM TR and determined that OLM techniques, when implemented correctly, can provide
41 an effective means of identifying transmitter failure modes and of identifying calibration
42 shifts that require calibration adjustments to be performed. When implemented in
43 conjunction with a plant corrective action program, an OLM process can be used to
44 initiate pressure, level, and flow transmitter calibration activities in order to meet the
45 requirements of 10 CFR 50.36(c)(3) for performing tests and calibration to assure that the
46 necessary quality of systems and components is maintained, that facility operation will be
47 within safety limits, and that the limiting conditions for operation will be met.
48

1 3.10. Instrument Span Calibration and Setpoint Uncertainties

2
3 In some cases, the effective OLM span coverage can be significantly less than the calibrated
4 instrument span depending on the nature of the process being measured. It is also common for
5 the normal exercised process values to never reach or exceed the safety system setpoint value
6 during startup, shutdown, or normal plant operation. It is therefore necessary to identify and
7 address uncertainties associated with the unexercised portions of a transmitter range.

8
9 The OLM methodology in Chapter 11 of the AMS OLM TR includes actions to assess transmitter
10 exercised range with respect to the transmitter span and with respect to the safety setpoints
11 associated with the instrument. These defined processes provide a method for addressing
12 uncertainties associated with the portions of transmitter range that are not exercised during plant
13 operation with OLM.

14
15 Chapter 14 of the AMS OLM TR, "OLM Coverage of transmitter Setpoints and Range," describes
16 a process for determining if the OLM span coverage is adequate to provide assurance of
17 transmitter performance over the unexercised portions of a transmitter span. In cases where
18 adequate assurance of instrument performance cannot be demonstrated, the instrument will be
19 excluded from the OLM program and periodic time-based calibrations would continue to be
20 required for these instruments.

21
22 The NRC staff determined the processes and methods for addressing unexercised portions of
23 instrument span as outlined in Chapter 14 of the AMS OLM TR provide an acceptable means of
24 assuring safety functionality over the intended ranges of the transmitters within the OLM
25 program.

26
27 3.11. Review of Changes to Technical Specification Surveillance Requirements

28
29 AMS OLM TR, Section 11.5, and the Example TS changes in Appendix B include a definition of
30 OLM and the Bases associated with the Surveillance Requirements changes.

31
32 The proposed TS changes provide instructions for making a condition-based determination of
33 whether a calibration check must be performed for instruments that are included in a plant's OLM
34 program. The TS change guidance also includes a description of a process for extending
35 calibration intervals for the applicable instruments. The proposed processes involve use of the
36 OLM program to extend transmitter calibration intervals by using the OLM processes described in
37 the AMS OLM TR to determine the condition of the transmitters and thereby to determine when
38 CHANNEL CALIBRATION surveillances should be performed.

39
40 These proposed TS changes are examples of how an OLM program could be implemented by a
41 licensee referencing the approved AMS OLM TR with supporting justification. These TS changes
42 are however not approved changes to any TSs and the NRC staff did not review the changes as
43 allowable TS for any licensee referencing the approved AMS OLM TR.

44
45 The NRC staff did not make any conclusions regarding the acceptability of these examples, since
46 it was recognized that each licensee adopting OLM methods for flagging whether transmitters
47 need calibration checks would need to perform a plant-specific evaluation of both its existing
48 licensing basis and site-specific TSs. Licensees and applicants may propose TS changes using
49 Appendix B in the TR as a guide for the type of information needed to be addressed for TS as

1 part of its implementation of an OLM program using the 10 CFR 50.90 license amendment
2 process or 10 CFR Part 50 or Part 52 license application process.

3
4 The NRC staff examined the AMS OLM TR general processes and descriptions of TS changes
5 needed and agree that they highlight the potential use of OLM methods to justify adjustments to
6 channel calibration intervals. Each licensee will need to perform a site-specific evaluation of both
7 its licensing basis and site-specific TS to demonstrate compliance with 10 CFR 50.36. The NRC
8 staff determined that such TS changes would need to include appropriate markups of the TS
9 Bases section, the TS tables describing limiting conditions for operation and surveillance
10 requirements, and the administrative programs section. This is described in ASAI 1 in
11 Section 4.0 of this SE.

12
13 3.12. Identification and Appropriate Allocation of Calibration Uncertainty Source

14
15 The OLM methods described in the AMS OLM TR involve collection of instrument loop data
16 using plant computer systems or other data collection instruments. In some cases, these data
17 acquisition systems measure instrument loop output signals instead of direct transmitter signals.
18 For such cases, the measured calibration uncertainties include calibration uncertainties of all
19 instruments in the loop being monitored and not only uncertainties of the transmitter. To account
20 for multiple instruments being used to support the transfer of transmitter signal data from the
21 transmitter to the data collection system, all calibration errors identified using OLM should be
22 initially attributed to the transmitter until testing or analysis can be performed to determine the
23 sources of calibration error and reallocate errors to the individual loop components. The
24 requirement to perform error allocation in this manner is captured as ASAI 2 in Section 4.0 of this
25 SE.

26
27 3.13. Establishing Appropriate Criteria for Flagging Potential Excessive Drift Performance

28
29 The NRC staff notes that the licensing basis for most operating plants includes the development
30 of design basis instrument setpoint calculations. These calculations address applicable criteria
31 and guidance for establishing performance monitoring acceptance limits for "As-Found" and "As-
32 Left" Tolerance Limits. The "As-Found" tolerance limits serve as the basis for determining
33 whether a transmitter is performing appropriately (i.e., as predicted or expected) when tested
34 during instrument calibration surveillance test intervals under normal calibration conditions.
35 These setpoint calculation documents establish the design and licensing basis for maintaining
36 acceptable performance of safety related instrument channels serving as SSCs to accomplish
37 LSSSs.

38
39 As described in Section 3.12 above, OLM methods require an evaluation of the uncertainties of
40 the portion of the instrument loop equipment that are used to transmit the output signal from the
41 transmitter to the OLM process data monitoring system. Applicants and licensees proposing to
42 adopt OLM methods for determining whether a transmitter needs a calibration check should
43 carefully evaluate the results of these design basis setpoint calculation documents to determine
44 an OLM drift acceptance criteria that is more conservative than the design basis As-Found
45 Tolerance limits for the plant, while not being too restrictive so as to flag an acceptably-
46 performing transmitter unnecessarily.

47
48 The AMS OLM TR describes a method for establishing this flagging criterion, however licensees
49 may choose to use a more conservative or less conservative flagging limit, provided it is
50 compatible with the design basis As-Found Tolerance limits established in the plant setpoint

1 calculations. If the licensee or applicant does not adopt the method for establishing this flagging
2 limit using the process described in the AMS OLM TR, it should describe its proposed
3 methodology for establishing this limit in its application for a license application or amendment to
4 adopt the OLM method for identifying transmitters that need calibration checks as an alternative
5 to incorporating a fixed calibration surveillance interval in the plant TS. This is captured as
6 ASAI 5 in Section 4.0 of this SE.

7
8 3.14. Regulatory Compliance

9
10 The OLM methodology provided in the AMS OLM TR provides an alternate means of determining
11 when pressure, level, and flow instrument calibration checks and follow-up calibrations are
12 required to provide adequate assurance that the necessary quality of systems and components is
13 maintained, that facility operation will be within safety limits, and that the limiting conditions for
14 operation will be met.

15
16 The NRC staff finds this methodology can be applied as an acceptable means of determining
17 whether protection systems are functioning as required, by flagging when calibration of these
18 instruments is needed. A licensee applying these methods shall perform a plant specific
19 assessment of the transmitters being included in the OLM program to ensure that requirements
20 of 10 CFR 36(c) can be met upon implementation of these OLM methods.

21
22 The NRC staff finds the AMS OLM TR methods for performing OLM to measure pressure, level,
23 and flow sensor calibration performance during plant operation to be consistent with regulatory
24 requirements of GDC 21 and 10 CFR 50.55a(h) applicable to reliability and testability of plant
25 protection and safety systems. Therefore, the NRC staff finds that the OLM methods outlined in
26 Section 11, "OLM Implementation Methodology," of the AMS OLM TR can be used to verify the
27 safety systems' capability to perform its safety functions. These OLM techniques may therefore
28 be credited in lieu of manual periodic calibration SR tests provided ASAI 5 in Section 4.0 of this
29 SE are performed.

30
31 4.0 APPLICATION SPECIFIC ACTION ITEMS

32
33 ASAI 1 - **Evaluation and Proposed Mark-up of Existing Plant Technical**
34 **Specifications** – When preparing a license amendment request to adopt OLM
35 methods for establishing calibration frequency, licensees should consider
36 markups that provide clear requirements for accomplishing plant operations,
37 engineering data analysis, and instrument channel maintenance. Such TS
38 changes would need to include appropriate markups of the TS tables
39 describing limiting conditions for operation and surveillance requirements, the
40 technical basis for the changes, and the administrative programs section.

41
42 ASAI 2 - **Identification of Calibration Error Source** – When determining whether an
43 instrument can be included in the plant OLM program, the licensee shall
44 evaluate calibration error source in order to account for the uncertainty due to
45 multiple instruments used to support the transfer of transmitter signal data to
46 the data collection system. Calibration errors identified through OLM should be
47 attributed to the transmitter until testing can be performed on other support
48 devices to correctly determine the source of calibration error and reallocate
49 errors to these other loop components.

1 ASAI 3 - **Response Time Test Elimination Basis** – If the plant has eliminated
2 requirements for performing periodic RT testing of transmitters to be included in
3 the OLM program, then the licensee shall perform an assessment of the basis
4 for RT test elimination to determine if this basis will remain valid upon
5 implementation of the OLM program and to determine if the RT test elimination
6 will need to be changed to credit the OLM program rather than the periodic
7 calibration test program.

8
9 ASAI 4 - **Use of Calibration Surveillance Interval Backstop** – In its application for a
10 license or license amendment to incorporate OLM methods for establishing
11 calibration surveillance intervals, applicants or licensees should describe how
12 they intend to apply backstop intervals as a means for mitigating the potential
13 that a process groups could be experiencing undetected common mode drift
14 characteristics.

15
16 ASAI 5 - **Use of Criteria other than in AMS OLM TR for Establishing Transmitter**
17 **Drift Flagging Limit** – In its application for a license or license amendment to
18 incorporate OLM methods for establishing calibration surveillance intervals,
19 applicants or licensees should describe whether they intend to adopt the
20 criteria within the AMS OLM TR for flagging transmitter drift or whether they
21 plan to use a different methodology for determining this limit.

22
23 5.0 CONCLUSION

24
25 The NRC staff determined that the methodology outlined in the AMS OLM TR for applying OLM
26 techniques to pressure, level, and flow transmitters can be used to provide reasonable assurance
27 that required TS instrument calibration requirements for transmitters will be maintained. This
28 determination is based on the NRC staff finding that OLM techniques: a) are effective at
29 identifying instrument calibration drift during plant operation, b) provide an acceptable means of
30 identifying when manual transmitter calibration using traditional calibration methods are needed,
31 and c) will maintain an acceptable level of performance that is traceable to calibration prime
32 standards. The NRC staff determined that reliance on a carefully developed OLM program to
33 determine appropriate calibration surveillance intervals, within the conditions and limitations
34 described in the AMS OLM TR, supports meeting the calibration surveillance requirements for
35 safety related pressure, level, and flow transmitters is acceptable under 10 CFR 50.36(c)(1)(ii)(A)
36 and 10 CFR 50.36(c)(3).

37
38 The NRC staff notes that the OLM methods described in the AMS OLM TR are not applicable for
39 meeting the instrument channel functional test surveillance requirements in the plant TS.
40 Therefore, the NRC staff finds that implementation of an OLM program in accordance with the
41 approved AMS OLM TR provides an acceptable alternative to periodic manual calibration
42 surveillance requirements upon implementation of the application specific action items in
43 Section 4.0 of this SE.
44

6.0 REFERENCES

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