## SEABROOK Station

# Evaluation and Comparison to BTP APCSB 9.5-1, Appendix A 

Revision 18


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On September 30, 1976, the NRC requested the Public Service Company of New Hampshire to conduct a re-evaluation of the fire protection program proposed for Seabrook Units $1 \& 2$, and to compare in detail the fire protection provisions proposed for Seabrook with the guidelines in Appendix A to Branch Technical Position APCSB 9.5-1. The request also stated that the reevaluation would require the preparation of a fire hazards analysis, with assistance and technical direction from a qualified fire protection engineer.

The above request resulted in a report which included an evaluation and fire hazards analysis originally performed by United Engineers and Constructors under the direction of UE\&C's Mr. Alfred S. Bocchino, P. E. Mr. Bocchino's resume is included in Appendix C of this report. The operational aspects of the re-evaluation were conducted by a Yankee Atomic Electric Company task force under the direction of Mr. E. A. Sawyer, whose resume is also included in Appendix C.

The above evaluation of the fire protection provisions was based on the guidelines contained in Appendix A to BTP APCSB 9.5-1 (plants for which applications for construction permits were docketed prior to July 1, 1976, but have not received a construction permit) and fully addressed the issues, criteria and concerns presented by the NRC.

The major changes incorporated in the above evaluation included:

1. Various changes resulting from the review and evaluation of 10 CFR 50, Appendix R.
2. Incorporation of Safety Evaluation Report (SER) commitments.

In the course of the above evaluation, the concept of "defense-in-depth" was applied and fire protection was treated from this viewpoint. Simply stated, this concept is:

1. Preventing fires from starting;

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2. Detecting fires quickly, suppressing those fires that occur, putting them out quickly, and limiting their damage; and
3. Designing plant safety systems so that a fire that starts in spite of the fire prevention program and burns for a considerable time in spite of fire protection activities will not prevent essential plant safety functions from being performed.

When this report is updated, the philosophy of the methodology remains unchanged. The following discussion describes the philosophy of the above report and any subsequent updates.

Plant design was reviewed and design provisions were included to provide protection of essential plant safety systems by physical barriers or spatial separation. Combustibles were identified and minimized as much as is practicable. Additionally, provisions were included for early detection of possible fires, with primary systems and back-up fire fighting systems available in the safetyrelated plant areas. The plant was designed to be constructed of non-combustible materials, where practical.

The fire protection systems described in this report are those required for protection of structures, systems and components required for safe reactor shutdown and safety-related systems. Other fire protection systems not described in this report are available for protection of non-safety-related structures, systems and components.

For prompt extinguishing of the fires associated with major electrical cables, efficient use of water is made from fixed systems spraying directly on the fires, as well as manual application with fire hoses.

A description of the fire protection system is provided in Section B. Included are pertinent general arrangement and P\&ID system drawings, and a plot plan, as well as a tabulation of suppression and detection means by area and zone.
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A brief discussion on safe shutdown systems and procedures is presented in the Fire Protection of Safe Shutdown Capability (10 CFR, Appendix R) Report.

The criteria used in the evaluation program are presented in Section D of the report, and include the applicable general design criteria as well as criteria for single failure, defense-in-depth, fire suppression systems capacity and capability, and occurrence of fire coincident with other accidents, events or phenomena.

The method of review and analysis is described in Section E of the report.

The basis for the fire hazards analysis is defined and the scope of the evaluation, including assumptions and design basis fire conditions, is provided. Designation of fire areas and zones is also discussed here.

The summary of the results of the evaluation program is set forth in Section F of the report. Subsection F. 1 presents a brief tabular summary indicating compliance, partial compliance or non-compliance with the BTP positions and page number of the partial compliance and noncompliance items. The bulk of the report is contained in Subsection F. 2 which comprises the detailed analyses of the consequences of a fire in each of the designated fire areas/zones, as well as selected general arrangement drawings of the plant areas housing the safety-related equipment and equipment required for safe shutdown of the plant, with the designated fire areas/zones and ingress/egress routes from these areas 5 superimposed. Section F. 3 presents the detailed responses to each of the positions of Branch Technical Position APCSB 9.5-1, Appendix A. This review indicates criteria that are satisfied, partially satisfied and those not satisfied, with an explanation in each instance.

This report is applicable only to Unit 1. The construction to Unit 2 has been halted and the fire protection program evaluation for Unit 2 has been deleted from this report.

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## 1. General

The plant fire protection system is a non-safety-related system designed to detect, control and extinguish potential fires, and to minimize their effect.

The relative location of the various plant buildings is shown on the station layout drawing, UFSAR Figure 1.2-1, sh. 1. The fire protection yard piping system is depicted on UFSAR Figure 9.5-4 and the fire pump house fire protection piping system is depicted on UFSAR Figure 9.5-5.

Fire detection is provided at locations determined by the fire hazard analysis as having significant fire hazards resulting from the presence of combustible liquids, solids or other flammable materials. Detection is also provided in other areas on a case basis.

Fire protection system piping and components in the area of safety-related systems required for safe shutdown of the plant are designed so that neither piping failure, seismic event, nor inadvertent operation of the system components, could result in the loss of safety related systems.

## 2. Design Features

## a. Water Supply and Pumping Arrangements

The water supply for the plant fire protection system is obtained from two (2) 500,000 -gallon water storage tanks. 300,000 gallons of water from each tank is dedicated for fire protection; the remainder is available for other plant use. During the winter months, the fire protection water is heated to prevent freezing. Two (2) diesel-driven and one (1) electric motor-driven fire pumps are provided to guarantee an uninterrupted supply of water.

Two (2) diesel-driven or one (1) diesel-driven and one (1) electric motor-driven fire pumps have the capacity to serve the maximum predicted demand for a safety related area suppression purposes, plus 500 gpm for hose streams through the yard hydrants or standpipe hose reels. (Reference Deviation No. 9, SBN 932, dated January 24, 1986). Deviation No. 9 of SBN-932 indicated that the largest demand safety related area was the Diesel Generator Room. Per EC274103, it has since been determined that the largest demand safety related area is the PAB.

Electric motor-driven jockey pumps normally will maintain system pressure.
A diesel fuel storage tank is provided for each diesel engine to supply fuel for a minimum of eight (8) hours.

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A flow meter is included with the pump installation for the purpose of testing pump performance.

Piping is so arranged that any or all fire pumps can take suction from either water storage tank. The buildings within the protected area are encircled by a 12 " underground cement-lined, welded steel pipe fire loop to supply yard fire hydrants and the various fire protection systems in the plant.

Post indicator isolation valves are provided at strategic locations in the underground loop header to allow for sectionalization during maintenance and repair, and to provide flow from the pumping facilities in either of two different directions in the event of a line break. Post indicator valves are also positioned in the loop header to isolate the loop between the take-offs for primary suppression and secondary systems.

Fire hydrants, spaced approximately 250 feet apart and having individual isolation valves, are provided on branches off the underground loop. Hose houses and associated equipment are located at alternate hydrants.
b. Stand-Pipe System

Wet and dry standpipe systems are installed in the various buildings of the plant, including stair towers and other points of normally accessible areas. Dry standpipes are installed in the containment. Wet standpipes are installed in the control building, primary auxiliary building, fuel storage building, equipment vault, emergency feedwater pump building, diesel generator building and waste processing building. Wet standpipes are also installed in the administration building and turbine building. Hose stations are strategically located throughout the buildings. Hose stations are located in each building or section of building, such that all portions of each elevation of the building are adequately covered.

## c. Sprinkler and Spray Systems

Wet pipe automatic sprinkler systems are installed in the administration and service building, turbine building, guardhouse, chlorination building, fire pump house, Alternate RP Checkpoint and Mechanical Maintenance Storage Facility.

Pre-action sprinkler systems are installed in the electrical tunnels from control building to containment, including penetrations, from the control building to primary auxiliary building (PAB), El. $25^{\prime}-0$ " and the electrical chase of the PAB, the diesel generator fuel oil storage tanks, fuel oil piping in floor trenches in the diesel generator building, diesel generator engine rooms, the PAB (component cooling area), Turbine Generator bearings and oil piping (bearings to guard pipe).

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The following equipment are provided with deluge systems:
Oil - filled Transformers
Lube Oil Storage Tanks
Lube Oil Conditioning Equipment
Hydraulic Oil Pumping Unit
Hydrogen Seal Oil Unit
Oil Day Tanks in the Diesel Generator Building
Cable Spreading Room
Turbine Feedpump Lube Oil Conditioning Equipment
Waste Process Bldg. Equipment (Asphalt Metering Pump; Extr./Evap.; Turn Table Area; Full Drum Conveyor)

An Automatic fixed Halon 1301 fire suppression systems is provided for the main computer room adjacent to the main control room. Fire barrier walls are provided between the main unit, start-up and station service transformers to limit the spread of fire from one transformer to another. The turbine building wall adjacent to the transformers is also a fire barrier wall.

## d. Fire Detection and Alarm

Thermal, ultraviolet, smoke (i.e. photoelectric and ionization) and beam type fire detectors are located throughout the plant, as required by the fire hazard analysis. All fire detectors provide alarm at its local control panel and a visual and an audible alarm in the main control room. Carbon monoxide detectors have been installed at certain charcoal filters. See Table 1 for fire detection and suppression methods employed in the various safety-related fire areas and zones.

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## e. Miscellaneous Fire Protection

Portable hand-held extinguishers, primarily dry chemical, $\mathrm{C}_{2}$, Halon 1211 and water are provided at strategic locations throughout the various buildings to provide protection against small local fire hazards.

Note: The term Halon or Halon 1211 is used to identify any of a family of Halon fire extinguishing gases: Halon 1211 or any of the Halon 1211 replacement gases such as hydrofluorocarbons (HFC's), hydrochlorofluorocarbons (HCFC) or blended agents such as Halotron.

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## TABLE 1

FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE

| FIRE AREA | AREA NAME | FIRE SUPPRESSION SYSTEM |  | DETECTION |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Primary | Secondary |  |


| 1. CONTAINMENT |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| C-F-1-Z | Containment Floor | Port. Exting. | Hose Station | Smoke |
| C-F-2-Z | Containment Floor | Port. Exting. | Hose Station | Smoke |
| C-F-3-Z | Containment Floor CAH-F-8 | Port. Exting. Port. Exting. | Hose Station <br> Hose Station | None <br> Temp Elements \& Carbon Monoxide Detection in Filter |
| 2. EMERGENCY FEEDWATER PUMP BUILDING |  |  |  |  |
| EFP-F-1-A | Feedwater Pump Room | Port. Exting. | Hose Station | Smoke |
| 3. MAIN STEAM AND FEEDWATER PIPE CHASE |  |  |  |  |
| MS-F-1A-Z | Lower Level | Port. Exting. | Yard Hydrant | Smoke |
| MS-F-1B-Z | Lower Level | Port. Exting. | Hose Station | Smoke |
| MS-F-2A-Z | Upper Level | Port. Exting. | Hose Station | Beam |
| MS-F-2B-Z | Upper Level | Port. Exting. | Hose Station | Beam |
| MS-F-3A-Z | Electrical Room | Port. Exting. | Yard Hydrant | Smoke |
| MS-F-3B-Z | Personnel Hatch Area | Port. Exting. | Yard Hydrant | Smoke |
| MS-F-4A-Z | $\mathrm{H}_{2}$ Analyzer Room | Port. Exting. | Yard Hydrant | Smoke |
| MS-F-5A-Z | Cable Tunnel | Port. Exting. | Hose Station | Smoke |


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## TABLE 1

FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE

| FIRE AREA | AREA NAME |  | FIRE SUPPRESSION SYSTEM |  |
| :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |
|  |  | Primary |  | Secondary |
|  |  |  |  |  |
| 4. RHR. S.I. EQUIPMENT VAULT |  |  |  |  |
| RHR-F-1A-Z | Containment Spray 9B | Port. Exting. | Hose Station | Smoke |
| RHR-F-1B-Z | Containment Spray 9A | Port. Exting. | Hose Station | Smoke |
| RHR-F-1C-Z | RHR Pump 8B | Port. Exting. | Hose Station | Smoke |
| RHR-F-1D-Z | RHR Pump 8A | Port. Exting. | Hose Station | Smoke |
| RHR-F-2A-Z | Safety Injection Pump 6B | Port. Exting. | Hose Station | Smoke |
| RHR-F-2B-Z | Safety Injection Pump 6A | Port. Exting. | Hose Station | Smoke |
| RHR-F-3A-Z | RHR Ht. Exch. 9B | Port. Exting. | Hose Station | Smoke |
| RHR-F-3B-Z | RHR Ht. Exch. 9A | Port. Exting. | Hose Station | Smoke |
| RHR-F-4A-Z | Stairway \& Manlift Area - <br> South | Port. Exting. | Hose Station | Smoke |
| RHR-F-4B-Z | Stairway \& Hatch Area - <br> North | Port. Exting. | Hose Station | Smoke |


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| TABLE 1 <br> FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| FIRE AREA | AREA NAME | FIRE SUPPRESSION SYSTEM |  | DETECTION |
|  |  | Primary | Secondary |  |
| 5. CONTROL BUILDING |  |  |  |  |
| CB-F-1A-A | Switchgear Room "A" (Includes MG Set Rod Drive Rooms) | Port. Exting. | Hose Station | Smoke |
| CB-F-1B-A | Switchgear Room "B" | Port. Exting. | Hose Station | Smoke |
| CB-F-1D-A | Battery Room A | Port. Exting. | Hose Station | Smoke |
| CB-F-1E-A | Battery Room C | Port. Exting. | Hose Station | Smoke |
| CB-F-1F-A | Battery Room B | Port. Exting. | Hose Station | Smoke |
| CB-F-1G-A | Battery Room D | Port. Exting. | Hose Station | Smoke |
| CB-F-2A-A | Cable Spreading Room | Auto. Deluge | Port. Exting | Smoke |
| CB-F-2B-A | Mechanical Rm. North | Port. Exting. | Hose Station | Smoke |
| CB-F-2C-A | Mechanical Rm. South | Port. Exting. | Hose Station | Smoke |
| CB-F-3A-A | Control Room | Port. Exting. | Hose Station | Smoke <br> \& Thermal |
| CB-F-3A-A | Computer Engineer's Work Space | Port. Exting. | Hose Station | Smoke |
| CB-F-3B-A | HVAC Eqpt. \& Duct Rm. | Port. Exting. | Hose Station | Smoke |
| CB-F-3B-A | Emerg. Clean-Up Air Unit <br> - CBA-F-38, -8038 | Port. Exting. | Hose Station | Carbon <br> Monoxide <br> Detect <br> Monitored <br> Temp. <br> Indication |
| CB-F-3C-A | Computer Room | Fixed <br> Halon1301 <br> System | Port. Exting. | Smoke |
| CB-F-S1-0 | Stairwell | Port. Exting. | Hose Station | None |
| CB-F-S2-0 | Stairwell | Port. Exting. | Hose Station | None |


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TABLE 1
FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE

| FIRE AREA | AREA NAME | FIRE SUPPRESSION SYSTEM |  | DETECTION |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Primary | Secondary |  |
| 6. ELECTRICAL TUNNELS |  |  |  |  |
| ET-F-1A-A | Upper Electrical Tunnel Train "A" | Pre-Action | Port. Exting. | Smoke |
| ET-F-1B-A | Electrical Tunnel Train "A" | Pre-Action | Port. Exting. | Smoke |
| ET-F-1C-A | Lower Electrical Tunnel Train "B" | Pre-Action | Port. Exting. | Smoke |
| ET-F-1D-A | Electrical Tunnel, Train "B" | Pre-Action | Port. Exting. | Smoke |
| ET-F-S1-0 | Stairwell | Port. Exting. | Hose Station | None |


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## TABLE 1

FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE

| FIRE AREA | AREA NAME | FIRE SUPPRESSION SYSTEM |  | DETECTION |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Primary | Secondary |  |

$\left.\begin{array}{|l|l|l|l|l|}\hline \text { 7. DIESEL GENERATOR BUILDING } & \text { Auto. Preaction } & \text { Port. Exting. } & \begin{array}{l}\text { Smoke \& } \\ \text { Thermal }\end{array} \\ \hline \text { DG-F-1A-A } & \begin{array}{l}\text { Fuel Oil Storage Tank } \\ \text { Area - North }\end{array} & \begin{array}{l}\text { Fuel Oil Storage Tank } \\ \text { Area - South }\end{array} & \text { Auto. Preaction } & \text { Port. Exting. } \\ \hline \text { DG-F-1B-A } & \begin{array}{l}\text { Smoke \& } \\ \text { Thermal }\end{array} \\ \hline \text { DG-F-2A-A } & \text { Engine Room North } & \begin{array}{l}\text { Auto Preaction } \\ \text { (on Oil Piping) } \\ \text { Manual } \\ \text { Preaction (area } \\ \text { wide for room) }\end{array} & \text { Port. Exting. } & \begin{array}{l}\text { Thermal } \\ \text { Smoke } \\ \text { Ultraviolet }\end{array} \\ \hline \text { DG-F-2B-A } & \text { Engine Room South } & \begin{array}{l}\text { Auto } \\ \text { Preaction(on Oil } \\ \text { Piping) Manual } \\ \text { Preaction(area } \\ \text { wide for room) }\end{array} & \text { Port. Exting. } & \begin{array}{l}\text { Thermal } \\ \text { Smoke }\end{array} \\ \text { Ultraviolet }\end{array}\right\}$

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| FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |


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## TABLE 1

FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE

| FIRE AREA | AREA NAME | FIRE SUPPRESSION SYSTEM |  | DETECTION |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Primary | Secondary |  |
| PAB-F-4-Z | Filter Area PAH-F-16 | Port. Exting. Port. Exting. | Hose Station <br> Hose Station | Smoke <br> Temp Elements \& Carbon Monoxide Detection in Filter |
| PAB-F-S1-0 | Stairwell | Port. Exting. | Hose Station | None |
| PAB-F-S2-0 | Stairwell | Port. Exting. | Hose Station | None |

9. FUEL STORAGE BUILDING

| FSB-F-1A-A | $\begin{array}{\|l} \hline \text { Elev. } 7^{\prime}-0^{\prime \prime}, 10^{\prime}-0^{\prime \prime}, 21^{\prime}-6^{\prime \prime}, \\ 25^{\prime}-0^{\prime \prime}, 64^{\prime}-0^{\prime \prime}, 84^{\prime}-0^{\prime \prime}, \\ \text { FAH-F-41,74 } \end{array}$ | Port. Exting. Port. Exting. | Hose Station Hose Station | Smoke <br> Temp Elements \& Carbon Monoxide Detect. in Filters |
| :---: | :---: | :---: | :---: | :---: |
| 10. WASTE PROCESSING BUILDING |  |  |  |  |
| W-F-1A-Z | Truck Bay \& Drum Storage Area | Port. Exting. | Hose Station | Smoke |
| W-F-1B-Z | Decontamination Area | Port. Exting. | Hose Station | Smoke |
| W-F-2A-Z | Extruder/Evap. Area | Deluge System | Hose Station | Smoke <br> \& Thermal |
| W-F-2B-Z | Crystallizer Pump Rm. | Port. Exting. | Hose Station | None |
| W-F-2C-Z | Asphalt Meter Pump Room | Deluge System | Hose Station | Smoke <br> \& Thermal |
| W-F-2D-Z | Turntable \& Drum Conv. Areas | Deluge System | Hose Station | Smoke \& Thermal |
| W-F-2E-Z | Waste Solidification Control Room | Port. Exting. | Hose Station | Smoke |
| TF-F-1-0 | Tank Farm (RWST) | Port. Exting. | Standpipe/ Hose Reel | None |


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## TABLE 1

FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE

| FIRE AREA | AREA NAME | FIRE SUPPRESSION SYSTEM |  | DETECTION |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Primary | Secondary |  |


| 11. SERVICE WATER PUMP HOUSE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| SW-F-1A-Z | Circulating Pump Area | Port. Exting. | Yard Hydrant | None |
| SW-F-1B-A | Electrical Control Room "A" | Port. Exting. | Yard Hydrant | Smoke |
| SW-F-1C-A | Electrical Control Room "B" | Port. Exting. | Yard Hydrant | Smoke |
| SW-F-1D-A | Fan Room | Port. Exting. | Yard Hydrant | Smoke |
| SW-F-1E-Z | Service Water Pump Area | Port. Exting. | Yard Hydrant | Smoke |
| SW-F-2-0 | Service Water Intake \& Discharge Structure | Port. Exting. | Yard Hydrant | None |
| 12. SERVICE WATER COOLING TOWER |  |  |  |  |
| CT-F-1C-A | Switchgear Room \#3 Unit \#1 Train "B" | Port. Exting. | Yard Hydrant | Smoke |
| CT-F-1D-A | Switchgear Room Unit \#1 Train "A" | Port. Exting. | Yard Hydrant | Smoke |
| CT-F-2B-A | Ventilation \& Mech. Room for Unit \#1 | Port. Exting. | Yard Hydrant | Smoke |
| CT-F-3-0 | Top of Cooling Twr. | Port. Exting. | Yard Hydrant | None |
| 13. CONTAINMENT ENCLOSURE VENTILATION AREA AND CONTAINMENT ANNULUS |  |  |  |  |
| CE-F-1-Z | Cont. Encl. Ventil. EAH-F-9, -69 | Port. Exting. <br> Port. Exting. | Hose Station Hose Station | Smoke <br> Temp Elements \& Carbon Monoxide Detect. in Filter |


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| TABLE 1 <br> FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| FIRE AREA | AREA NAME | FIRE SUPPRESSION SYSTEM |  | DETECTION |
|  |  | Primary | Secondary |  |
| 14. FIRE PUMP HOUSE |  |  |  |  |
| FPH-F-1A-A | Diesel Pump Rm.-West | Auto Sprinkler | Port. Exting. | Thermal |
| FPH-F-1B-A | Electric Pump Room | Auto Sprinkler | Port. Exting. | Smoke |
| FPH-F-1C-A | Diesel Pump Rm.-East | Auto Sprinkler | Port. Exting. | Thermal |
| 15. TURBINE BUILDING |  |  |  |  |
| TB-F-1A-Z | Ground Floor | Auto Sprinkler | Hose Station | None |
| TB-F-1B-A | Battery Room | Port. Exting | Hose Station | Smoke |
| TB-F-1C-Z | Relay Room | Port. Exting | Hose Station | Smoke |
| TB-F-2-Z | Mezzanine | Auto Sprinkler | Port. Exting. | None |
| TB-F-3-Z | Start-Up \& Turbine Erector's Office <br> Electronic Work Area SAS Computer Room | Port. Exting <br> Port Exiting | Hose Station <br> Hose Station | Smoke <br> Smoke |
|  |  |  |  |  |
| 16. MECHANICAL PENETRATION AREA |  |  |  |  |
| PP-F-1A-Z | Rad. Piping Area | Port. Exting | Hose Station | Smoke |
| PP-F-2A-Z | Rad. Piping Area | Port. Exting | Hose Station | Smoke |
| PP-F-1B-Z | Rad. Piping Area | Port. Exting | Hose Station | Smoke |
| PP-F-2B-Z | Rad. Piping Area | Port. Exting | Hose Station | Smoke |
| PP-F-3A-Z | Rad. Piping Area | Port. Exting | Hose Station | Smoke |
| PP-F-3B-Z | Rad. Piping Area | Port. Exting | Hose Station | Smoke |
| PP-F-4B-Z | Non-Rad. Piping Area | Port. Exting | Hose Station | Smoke |
| PP-F-5B-Z | Rad. Piping Area | Port. Exting | Hose Station | Smoke |


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## TABLE 1

FIRE DETECTION AND SUPPRESSION METHODS BY FIRE AREA AND ZONE

| FIRE AREA | AREA NAME | FIRE SUPPRESSION SYSTEM |  | DETECTION |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Primary | Secondary |  |
| 17. NON-ESSENTIAL SWITCHGEAR ROOM |  |  |  |  |
| NES-F-1A-Z | Non-Essential Swgr. | Port. Exting | Yard Hydrant | Smoke |
| 18. CONDENSATE STORAGE TANK |  |  |  |  |
| CST-F-1-0 | Cond. Stor. Tank | Port. Exting | Yard Hydrant | None |
| 19. MAKE-UP AIR |  |  |  |  |
| MUA-F-1-0 | Make-Up Air East | Port. Exting | Yard Hydrant | None |
| 20. DUCTBANKS |  |  |  |  |
| DCT-F-1A-0 | Ductbanks | N/A | N/A | N/A |
| DCT-F-1B-0 | Ductbanks | N/A | N/A | N/A |
| DCT-F-2A-0 | Ductbanks | N/A | N/A | N/A |
| DCT-F-2B-0 | Ductbanks | N/A | N/A | N/A |
| DCT-F-3B-0 | Ductbanks | N/A | N/A | N/A |
| DCT-F-4A-0 | Ductbanks | N/A | N/A | N/A |
| DCT-F-4B-0 | Ductbanks | N/A | N/A | N/A |
| DCT-F-5A-0 | Ductbanks | N/A | N/A | N/A |
| DCT-F-5B-0 | Ductbanks | N/A | N/A | N/A |

NOTE: This listing does not include the Administration Building, part of Turbine Building, Chlorination Building, RCA Storage Facility, Mechanical Maintenance Storage Facility, Supplemental Emergency Power System and Guard House which do not contain safety-related equipment.



## See PID-1-FP-B20274

| SEABROOK STATION | Fire Protection Yard Piping |  |
| :--- | :--- | :--- |
| UPDATED FINAL SAFETY |  |  |
| ANALYSIS REPORT |  | Figure 9.5-4 |

See PID-1-FP-B20266
SEABROOK STATION
UpDATED FINAL SAFETY
ANALYSIS REPORT

Fire Protection Fire Pumphouse Detail
Updated Final Safety ANALYSIS REPORT

Figure 9.5-5

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For details relating to safe shutdown systems and safe shutdown capability, refer to the Seabrook Station report, "Fire Protection of Safe Shutdown Capability (10 CFR 50, Appendix R)", latest revision.

Section F.2, Tabs 1 through 17, contain tables labeled "Equipment and Systems in Fire Area/Zone" (Item 12.0.) These tables denote the safety related equipment and systems in each plant Fire Area/Zone.

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The criteria listed below served as the basis for the overall evaluation and comparison of the fire protection system against the guidelines of BTP APCSB 9.5-1, Appendix A:

1. Safe shutdown analyses for the areas listed in this report have been superseded by analyses included in the "Fire Protection of Safe Shutdown Capability, 10 CFR 50, Appendix R" report.

Operation of the Fire Protection system for safe shutdown scenarios, as described in paragraph 3.2.2.3 of the Appendix R report, supersedes the BTP APCSB 9.5-1, Appendix A exclusivity usage requirement.
2. For the purposes of this fire hazard analysis evaluation, a conservative approach was utilized in determining what could be found in any specific fire area or zone. This especially holds true in the electrical design area where the following conservative criteria were applied:
a. Use of cable with low auto-ignition temperature of $750^{\circ} \mathrm{F}$.
b. Use of cable trays $40 \%$ filled for control, instrumentation and low voltage medium power, or a spaced single layer for high voltage power and low voltage power cables.
c. Use of average size cables for cable tray loading and fire loading.
d. Interlocked armored cable will be used for all 15 kV cables and all 5 kV cables, except the condensate and start-up feed pumps, which are routed in duct and conduit runs and the Supplemental Emergency Power System feeders which are routed in dedicated metal raceways.

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3. The fire hazard analysis and evaluation was generally limited to those systems required to place the plant in a cold shutdown condition or to mitigate the consequences of an accident. According to BTP APCSB 9.5-1, safety-related systems and components are systems and components required to shutdown the reactor, mitigate the consequences of postulated accidents or maintain the reactor in a safe shutdown condition.
4. A single failure of an active component in a fire detection or fire support system will not impair both primary and backup plant fire protection capability.
5. Fire barriers between redundant cable separation groups and/or automatic sprinkler systems for cable raceway systems were used as a primary protection means from common mode failure by fire. The cabling raceway design meets the spatial separation requirements of Attachment "C," Physical Independence of Electric Systems, to the AEC letter dated Dec. 14, 1973, a forerunner of Regulatory Guide 1.75 (hereinafter referred to as Attachment "C").

Fire stop locations in vertical cable tray runs were selected on the bases of limiting materially 1) the spread of fire via a vertical cable tray run and 2) the resultant damage due to a fire in a vertical cable tray run.

The following guidelines were employed:
a) Horizontal offsets $>1$ foot were considered to end vertical cable tray runs.
b) Fire stops were not installed where cable tray fire suppression was present regardless of vertical run.

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c) In vertical cable tray runs $>25$ feet, fire stops were placed to limit the spread of fire to not more than 35 feet. In fact more than two thirds of the vertical runs between fire stops are approximately 25 feet or less. The remaining vertical runs between fire stops vary from about 28 feet to about 35 feet. Where practical in vertical cable tray runs greater than 25 feet, fire stop locations were adjusted to floor elevations.
6. The majority of the cable used meet the fire test requirements of IEEE-383-1974 with the exception noted in Section F-3.
7. For each area containing significant fire hazard material, fire protection in the form of appropriate fire detection has been provided.
8. In areas where the fire hazard analysis indicates that a credible fire, should it occur, would adversely affect a safety-related or safe shutdown function, automatic fire suppression capability is provided.
9. Although the fire hazard analysis has indicated that no fire hazard exists, detectors and automatic suppression have been provided in electrical tunnels, chases and the cable spreading room. Also, in other selected electrical areas as shown by Table 1 (Section B), appropriate fire detection has been provided.
10. Fire is not considered to occur simultaneously with other accidents, events or phenomena such as a design-basis accident. Capability is provided to safely shut down the plant in the event of any single fire.

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11. The fires postulated in this fire hazard analysis and evaluation are presented in Subsection F.2, Results of Fire Hazard Analysis. The heat of combustion values used are as follows:

| Combustible | Heat of Combustion |  |
| :--- | :---: | :---: |
| Outo - ignition Temperature |  |  |
| Oil (any type) | $150,000 \mathrm{BTU} / \mathrm{gal}$ | $300^{\circ} \mathrm{F}$ |
| Grease | $18,000 \mathrm{BTU} / \mathrm{lb}$. | $800^{\circ} \mathrm{F}$ |
| Class A (paper, wood) | $8,000 \mathrm{BTU} / \mathrm{lb}$. | $800^{\circ} \mathrm{F}$ |
| Electrical cables | $10,500 \mathrm{BTU} / \mathrm{lb}$. | $750^{\circ} \mathrm{F}$ |


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## 1. Methodology

The organization of the Branch Technical Position APCSB 9.5-1, Appendix A, is broken down into overall fire protection requirements, general guidelines for both building design and specific systems, specific requirements for fire protection and suppression and general guidelines for specific plant areas. For the purpose of review, this fire hazards analysis and evaluation is sub-divided into two major areas in accordance with the above requirements, as follows:
o General fire protection review (fire hazard analysis and evaluation)
o Specific subject review

These two areas of review are detailed in the following paragraphs:
a. General Fire Protection Review

The purpose of this review is to evaluate the fire hazards associated with the plant, the capability to achieve safe reactor plant shutdown and to prevent a single fire from adversely affecting a safety function.

Figure depicts the flow path used for completing this analysis. As can be seen, this was basically accomplished on an area by area and system by system approach.
b. Specific Subject Review

Once the general review was completed, it was further necessary to review the specific requirements for those systems described in the Branch Technical Position, as well as review the guidelines for specific plant areas. Figure also shows the flow path of this review.

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Note that this review is repeated for each individual plant area requirement. In addition, there is an inter-relationship between these flow paths, such that upon completion of the overall plant review, specific and feasible solutions are derived that may or may not completely comply with the guidelines of APCSB 9.5-1, Appendix A. The results of these reviews are contained in this report. A summary of these results are found in Subsection F.1, Evaluation and Comparison Matrix.

The specific subjects under review are enumerated as follows:
o Plant Area Requirements
o Fire Detection
o Fire Suppression (including water supply system)
o Electrical
o Ventilation
o Lighting and Communications
o Construction (fire walls, etc.)

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Figure I


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## 2. Review Assumptions

The assumptions listed below were utilized during this review.
a. Fire areas were established based on plant design and floor levels, and designated as that portion of a building separated from other areas by barriers (walls, floors and ceilings) having designated fire ratings of one, one and one-half, or three-hour, as required by the fire hazard analyses. Fire areas, in some cases, were further subdivided into fire zones for purposes of fire protection evaluation.
b. Credit was taken for spatial separation of combustibles within a given area such that the "maximum credible fire" was established as the postulated fire in each zone. This postulated fire may consist of multiple fires within a given area only if such fires could credibly spread with no suppression.
c. While fire barrier walls may have fire resistance capability in excess of that required for fire protection (because of shielding or structural requirements), the penetrations are designed for the fire resistance rating designated for the fire barrier.
d. For purposes of this report, outside walls and ceilings of the top floors were not considered as requiring a fire rating.
e. It is assumed that a postulated fire cannot exist if only electrical cables are involved. The material selection and construction of the electrical cable insulation meet IEEE 383-1974 (except as noted in Section F-3). In addition, electrical faults will be mitigated by selective tripping of breakers or blowing of fuses.
f. The cable construction and insulation material of the safety related and non-safety related cables meet the requirements of IEEE 383-1974. This will certify the cable's non-propagational and fire resistance capabilities.

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However, it is noted that the cable will burn when subjected to external flame or high temperature (greater than $750^{\circ} \mathrm{F}$ ). Therefore, if a design basis fire is determined to be hot enough and burn long enough, cabling in the immediate vicinity is assumed to burn, incapacitating the system the cabling serves and forming another heat source that is analyzed for additional fire possibilities.
(1) The additional heat source is considered as part of the original postulated fire.
(2) To become an additional heat source, the cable is considered to auto-ignite at an ambient temperature of approximately $750^{\circ} \mathrm{F}$ when heat of the original postulated fire is applied for five (5) minutes or longer.
(3) Once auto-ignition has taken place, the entire stack of cable trays is considered to be involved in the fire.
(4) It is assumed that any cabling system enclosed in conduit, which also passes through a postulated fire area, would not provide additional combustibility to the postulated fire. The cabling is assumed to fail as the heat of the fire destroys the insulation, however, the fire and damage is contained within the conduit. The heat contributed is considered insignificant.
g. Electric motors are not considered as combustibles due to their metal enclosures, and do not add to the intensity of the original postulated fire. They could, however, be damaged by a postulated fire if situated in the cone of fire influence.

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h. It was assumed that electrical equipment such as switchgear, unit substations, motor control centers, etc., do not contribute to a fire due to their metal enclosure. Electrical equipment, however, could be damaged by a fire. Electrical equipment specifications required that organic insulating materials used in the equipment construction be qualified as being self-extinguishing and non-propagating when exposed to fire and flame. It was also assumed that miscellaneous combustible materials mounted on the electrical equipment, such as operating coils, relays, control switches, etc., are of such small quantities that the heat released is insignificant.
i. In many cases small quantities of grease are contained in valves, motors, fans and pumps. Since these small quantities are contained within a packing gland or a bearing, it is not considered as contributing to a fire.
j. Air cleaning units, which contain roughing filters, HEPA filters and charcoal filters, are contained in heavy metal casings and are not considered in the fire hazard analysis for total Fire Loading in the Fire Area and the total combustibles. However, an individual Fire Hazard Analysis was conducted on CAH-F-8, CAP-F-40, EAH-F-9, 69, FAH-F-41, 74 and PAH-F-16, to be used for the Appendix "R" to 10CFR50 Safe Shutdown Study. See Appendix "D" for analysis. All filter units have early Fire Warning Detection Systems, i.e., Carbon Monoxide detectors and temperature elements within the filter units.
k. Pipe and its insulation are not combustible and are not considered in the fire hazard analysis, however, if the pipe is in the cone of fire influence and the temperature of the fire is greater than $2000^{\circ} \mathrm{F}$. for a duration greater than ten (10) minutes, the pipe is considered to rupture, incapacitating the system that it is a part of.

1. Bare structural steel is not combustible but tends to degrade structurally when an ambient temperature of greater than $1100^{\circ} \mathrm{F}$. is maintained for longer than ten (10) minutes. Fireproof-coated steel maintains its integrity for at least three (3) hours.

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m . The fire hazard analysis of each fire area/zone is conducted as follows:

1. The original postulated fire is a fire that starts through the ignition of combustibles and covers a certain floor area. The effects of this fire forms a vertical shaft of fire influence over the fire which extends to the ceiling. For Class "A" fires, the temperature of the vertical shaft is assumed constant throughout its entire height, and is determined with the use of the NFPA heat potential and time/temperature curves or with the use of other published literature on the subject.
2. Effects of the postulated fire on cabling within $3^{\prime}-O^{\prime \prime}$ of the shaft are re-evaluated if the temperature or duration of the fire exceeds the auto-ignition assumptions of the cabling. A time/temperature value is determined by forming a cone of influence over the fire covering an area 20 degrees from the vertical edge of the fire, with the fire acting as a flattened vortex of the cone. The new time/temperature value is determined by dividing the BTU value of the original fire by the area of the cone at the intersection of the combustible and the cone.

If the temperature and duration of the re-evaluated fire exceeds the auto-ignition assumptions of cabling, then the BTU contents of the cabling are added to the original BTU value, and a secondary fire is postulated.

The secondary fire has a time duration equal to that of the postulated fire, and its fire loading is determined by dividing the total BTU value by the area of the entire zone.

If the temperature and duration of this secondary fire exceeds the auto-ignition assumption of cabling, then the remainder of the cabling in the fire area-zone auto-ignites and also burns.

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n. Bulk storage of combustible materials, including spare parts, adjacent to or in safetyrelated buildings during operation, maintenance or refueling periods is controlled by administrative procedures.

## 3. Designation of Fire Area and Zones

As part of the fire hazard analysis effort, applicable plant general arrangement drawings were modified by superimposing on them the perimeters of fire areas and zones. Heavy solid lines were used to denote 3-hour minimum fire-rated walls, thin slanted lines were used to show $1-1 / 2$ hour fire-rated walls, heavy dashed lines were used to identify fire zone boundaries, heavy slanted lines were employed to define outside walls of buildings, and arrows were used to indicate the route to a fire exit.

Designations assigned to the various fire areas and zones denote the name of the building or structure, the floor level and whether the location is an area or zone. As an example, C-F-1-Z = Containment, Fire Analysis, Floor level 1 and Fire Zone. Another example, CB-F-1A-A = Control Building, Fire Analysis, Fire Subdivision A of Floor Level 1 and Fire Area. The Containment was treated as a single fire area comprised of a number of fire zones. Some other designation such as PAB-F-S1-0, Primary Auxiliary Building, Fire Analysis; stairwell has been assigned for convenience. This Suffix "0" designated area may or may not have fire rated boundaries.

A listing of the various fire areas and zones which were subjected to the fire hazards analysis, together with their applicable drawings, is presented in TABLE 2.

Abbreviations for the various buildings, structures and locations used in the fire area and zone designations are tabulated below:

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TABLE 1 - Tab Index

| Tab. | Abbreviation | Name of Building/Structure |
| :--- | :--- | :--- |
| 1 | C | Containment |
| 2 | EFP | Emergency Feedwater Pump Building |
| 3 | MS | Main Steam \& Feedwater Pipe Enclosure |
| 4 | RHR | RHR, S.I., Equipment Vault |
| 5 | CB | Control Building |
| 6 | ET | Electrical Tunnels |
| 7 | DG | Diesel Generator Building |
| 8 | PAB | Primary Auxiliary Building |
| 9 | FSB | Fuel Storage Building |
| 10 | W | Waste Processing Building |
| 10 | TF | Tank Farm |
| 11 | SW | Service Water Pump House |
| 12 | CE | Service Water Cooling Tower |
| 13 | FPH | Containment Enclosure Ventilation Area |
| 14 | TB | Fire Pump House |
| 15 | PP | Turbine Building |
| 16 | NES | Mechanical Penetration Area |
| 17 | CST | Non-Essential Switchgear Room |
| 18 | MUA | Condensate Storage Tank |
| 19 | DCT | Make up Air Intakes - East \& West |
| 20 |  | Ductbanks |
|  |  |  |


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| TABLE 2 <br> Identification of Fire Area and Zones on Drawings |  |  |  |
| :---: | :---: | :---: | :---: |
| TAB | Structure and Applicable Drawings |  | Fire Area or Zone Designation |
| 1 | Containment |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 805051-FP | Containment Structure Plan El. (-) 26'-0" - Gen. Arrg't. | C-F-1-Z |
|  | 805052-FP | Containment Structure Plan El. 0'-0" - Gen. Arrg't. | C-F-2-Z |
|  | 805053-FP | Containment Structure Plan El. 25'-0" - Gen. Arrg't. | C-F-3-Z |
| 2 | Emergency Feedwater Pump Building |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 202065-FP | Emergency Feedwater Pump Building Plan \& Sections, Gen. Arrg't. | EFP-F-1-A |
| 3 | Main Steam and Feedwater Pump Building |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 202063-FP | Main Steam \& Feedwater Pipe Chase - Plan General Arrg't | MS-F-1A-Z, MS-F-1B-Z, MS-F-2A-Z, MS-F-2B-Z, MS-F-3A-Z, MS-F-3B-Z, MS-F-4A-Z, MS-F-5A-Z, EFF-1A-A |
|  | 202064-FP | Main Steam \& Feedwater Pipe Enclosure - Sections General Arrg't | MS-F-1A-Z, MS-F-1B-Z, MS-F-2A-Z, MS-F-2B-Z, MS-F-3A-Z, MS-F-4A-Z |


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| TABLE 2 <br> Identification of Fire Area and Zones on Drawings |  |  |  |
| :---: | :---: | :---: | :---: |
| TAB | Structure and Applicable Drawings |  | Fire Area or Zone Designation |
| 4 | RHR Containment Spray Vault. SI Equipment Vault |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 805060-FP | RHR, Containment Spray, S.I. Equip. Vault - General | RHR-F-1A-Z, RHR-F-1B-Z, RHR-F-1C-Z, RHR-F-1D-Z, RHR-F-2A-Z, RHR-F-2B-Z, RHR-F-3A-Z, RHR-F-3B-Z, RHR-F-4A-Z, RHR-F-4B-Z |
|  | 805078-FP | RHR, Containment Spray, S.I. Equip. Vault - General Arrg't Sections | RHR-F-1A-Z, RHR-F-1B-Z, RHR-F-1C-Z, RHR-F-1D-Z, RHR-F-2A-Z, RHR-F-2B-Z, RHR-F-3A-Z, RHR-F-3B-Z, RHR-F-4A-Z |
| 5 | Control Building |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 310431-FP | Control Building El. 21'-6" Electrical General Arrg't | $\begin{aligned} & \text { CB-F-1A-A, CB-F-1B-A, } \\ & \text { CB-F-S1-0, CB-F-S2-0, } \\ & \text { CB-F-1D-A, CB-F-1E-A, } \\ & \text { CB-F-1F-A,CB-F-1G-A } \end{aligned}$ |
|  | 310452-FP | Control Building El. 50'-0" Cable Tray Layout - Plan | $\begin{aligned} & \text { CB-F-2A-A, CB-F-2B-A, } \\ & \text { CB-F-2C-A, } \end{aligned}$ |
|  | 310455-FP | Control Building El. 21'-6" Cable Tray Layout - Sections Sheet 1 | CB-F-1A-A, |
|  | 310461-FP | Control Building El . 50'-0"' Cable Tray Layout - Sections Sheet 1 | CB-F-2A-A, CB-F-2B-A |
|  | 500090-FP | Control Building Control Room Arrg't Plan at El.75'-0" | $\begin{aligned} & \text { CB-F-3A-A, CB-F-3B-A, } \\ & \text { CB-F-3C-A } \end{aligned}$ |


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| TABLE 2 <br> Identification of Fire Area and Zones on Drawings |  |  |  |
| :---: | :---: | :---: | :---: |
| TAB | Structure and Applicable Drawings |  | Fire Area or Zone Designation |
| 6 | Electrical Tunnels |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 310453-FP | Electrical Tunnel - A Train Cable Tray Layout - Plan | $\begin{aligned} & \text { ET-F-1A-A, ET-F-1B-A, } \\ & \text { ET-F-S1-0 } \end{aligned}$ |
|  | 310454- FP | Electrical Tunnel - B Train Cable Tray Layout - Plan | ET-F-1C-A, ET-F-1D-A |
|  | 310465-FP | Electrical Tunnel - A Train Cable Tray Layout - Sections Sheet 1 | ET-F-1A-A, ET-F-1B-A |
|  | 310466-FP | Electrical Tunnel-A Train Cable Tray Layout - Sections Sheet 2 | ET-F-1A-A, ET-F-1B-A |
|  | 310468-FP | Electrical Tunnel - B Train Cable Tray Layout - Sections Sheet 1 | ET-F-1C-A, ET-F-1D-A |
|  | 310469-FP | Electrical Tunnel - B Train Cable Tray Layout - Sections Sheet 2 | ET-F-1D-A |
| 7 | Diesel Generator Building |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 202068 -FP | Diesel Generator Building -Plan \& Sections - Below Grade General Arrangement | $\begin{aligned} & \text { DC-F-1A-A, DG-F-1B-A, } \\ & \text { DG-F-S1-0, DG-F-S2-0 } \end{aligned}$ |
|  | 202069-FP | Diesel Generator Building -Plan Above Grade - General Arrangement | DC-F-2A-A, DG-F-2B-A, DC-F-3A-Z, DC-F-3B-Z, DC-F-3C-A, DC-F-3D-A, DC-P-3E-A, DG-F-3F-A |


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| TABLE 2 <br> Identification of Fire Area and Zones on Drawings |  |  |  |
| :---: | :---: | :---: | :---: |
| TAB | Structure and Applicable Drawings |  | Fire Area or Zone Designation |
| 8 | Primary Auxiliary Building |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 805061-FP | Primary Auxiliary Building Plans at El. 7'-0" and Below General Arrangement | $\begin{aligned} & \text { PAB-P-1A-Z, PAB-F-1B-Z, } \\ & \text { PAB-F-1C-A, PAB-F-1D-A, } \\ & \text { PAB-F-1E-A, PAB-F-1F-Z, } \\ & \text { PAB-P-1G-A, PAB-F-1J-A, } \\ & \text { PAB-F-1K-Z } \end{aligned}$ |
|  | 805062-FP | Primary Auxiliary Building Plans at El. 25-0" -General Arrangement | $\begin{aligned} & \text { PAB-F-2A-Z, PAB-F-2B-Z, } \\ & \text { PAB-F-2C-Z, PAB-F-1G-A, } \\ & \text { PAB-F-1K-Z } \end{aligned}$ |
|  | 805063-FP | Primary Auxiliary Building Plans at El. 53'-0" \& 81'-0" General Arrangement | $\begin{array}{\|l} \hline \text { PAB-F-3A-Z, PAB-F-3B-Z, } \\ \text { PAB-F-4A-Z, PAB-F-1K-Z, } \\ \text { PAB-F-S1-0, PAB-F-S2-0 } \\ \hline \end{array}$ |
|  | 805060-FP | RHR, Containment Spray, S.I. <br> Equip. Vault - General | PAB-F-1G-A |
| 9 | Fuel Storage Building |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 805058-FP | Fuel Storage Building - Plan at El. 7'- 0" 10'-0" -General Arrangement | FSB-F-1-A |
|  | 805059-FP | Fuel Storage Building - Plan at El. 21'-6" \& 25'-0" -General Arrangement | FSB-F-1-A |
|  | 805084-FP | Fuel Storage Building - Plan at. El. 64'-0" \& 84'-0" -General Arrangement | FSB-F-1-A |


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| TABLE 2 <br> Identification of Fire Area and Zones on Drawings |  |  |  |
| :---: | :---: | :---: | :---: |
| TAB | Structure and Applicable Drawings |  | Fire Area or Zone Designation |
| 10 | Waste Processing Building |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 805661-FP | Waste Processing BuildingPlan at El. 25'-0" -General Arrangement | W-F-1A-Z, W-F-11B-Z, TF-F-1-0 |
|  | 805882-FP | Waste Processing Building Plan \& Sections El. 42'-5" \& 65'-0" - General Arrangement | $\begin{aligned} & \text { W-F-2A-Z, W-F-2B-Z, } \\ & \text { W-F-2C-Z, W-F-2D-Z, } \\ & \text { W-F-2E-Z } \end{aligned}$ |
| 11 | Service Water Pump House |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 202476-FP | Service \& Circ. Water Pump House - Plan \& Section General Arrangement | SW-F-1A-Z, SW-F-1B-A, SW-P-1C-A, SW-F-1D-A, SW-F-1E-Z |
|  | 202478-FP | Service \& Circ. Water Pump <br> House - Sections - General Arrangement | $\begin{aligned} & \text { SW-F-1A-Z, SW-F-1B-A, } \\ & \text { SW-F-1D-A } \end{aligned}$ |
|  | 300245-FP | Underground Duct Plan - Circ. \& Service Water Area | SW-F-2-0 |
| 12 | Service Water Cooling Tower |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 805068- FP | Service Water Cooling Tower General Arrangement | $\begin{aligned} & \text { CT-F-1C-A, CT-F-1D-A, } \\ & \text { CT-F-2B-A, CT-F-3-0 } \end{aligned}$ |


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| TABLE 2 <br> Identification of Fire Area and Zones on Drawings |  |  |  |
| :---: | :---: | :---: | :---: |
| TAB | Structure and Applicable Drawings |  | Fire Area or Zone Designation |
| 13 | Containment Enclosure Ventilation Area |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 805059-FP | Fuel Storage Building - Plan at El. 21'-6" \& 25'-0"' General Arrangement | CE-F-1-Z |
|  | 805053-FP | Containment Structure Plan at Elev. 25'-0" General Arrangement | CE-F-1-Z |
|  | 805052-FP | Containment Structure Plan at Elev. 0'-0" General Arrangement | CE-F-1-Z |
|  | 805051-FP | Containment Structure Plan at Elev. (-)26'-0" General Arrangement | CE-F-1-Z |
|  | 805056-FP | Containment Structure Elev. "D-D", "E-E", "F-F" General Arrangement | CE-F-1-Z |
|  | 805055-FP | Containment Structure Plan at Elev. (-)44'-9" | CE-F-1-Z |
| 14 | Fire Pump House |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 300831-FP | Fire Pump House Tray Plan and Grounding | FPH-F-1A-A, FPH-F-1B-A, FPH-F-1C-A |


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| TABLE 2 <br> Identification of Fire Area and Zones on Drawings |  |  |  |
| :---: | :---: | :---: | :---: |
| TAB | Structure and Applicable Drawings |  | Fire Area or Zone Designation |
| 15 | Turbine Building |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 202052-FP | Turbine Building Plan Ground Floor, Elevation 21'-0", General Arrangement | $\begin{aligned} & \text { TB-F-1A-Z, TB-F-1B-A, } \\ & \text { TB-F-1C-Z } \end{aligned}$ |
|  | 202053-FP | Turbine Bldg Plan, Mezzanine Floor, Elevation 46'-0" and 50' -0 ", General Arrangement | TB-F-2-Z |
|  | 202054-FP | Turbine Building Plan Operating Floor, Elevation 75' 0 ", General Arrangement | TB-F-3-Z |
| 16 | Mechanical Penetration Area |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 311429-FP | Main Steam Tunnel-West Lighting Plan-Lower Levels | $\begin{aligned} & \text { PP-F-1A-Z, PP-F-2A-Z, } \\ & \text { PP-F-1B-Z, PP-F-2B-Z, } \\ & \text { PP-P-3A-Z, PP-F-3B-Z, } \\ & \text { PP-F-4B-Z, PP-F-5B-Z } \end{aligned}$ |
| 17 | Non Essential Switchgear Room |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 310289- FP | Non Essential Swgr. Room Electrical General Arrangement and Grounding | NES-F-1A-Z |
| 18 | Condensate Storage Tank |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 310828-FP | Condensate \& Demineralized Water Stor. Tks. Conduit, Ltg. \& Ground. Plan | CST-F-1-0 |
| 19 | Make-Up Air, East and West |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 310248-FP | Underground Duct Plan - Center | MUA-F-1-0 |


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| TABLE 2 <br> Identification of Fire Area and Zones on Drawings |  |  |  |
| :---: | :---: | :---: | :---: |
| TAB | Structure and Applicable Drawings |  | Fire Area or Zone Designation |
| 20 | Duct Banks |  |  |
|  | Dwg. No. 9763-F- | Title |  |
|  | 320251-FP | Underground Duct Plan - Center | $\begin{aligned} & \text { DCT-F-5A-0 } \\ & \text { DCT-F-5B-0 } \end{aligned}$ |
|  | 310254-FP | Underground Duct \& Grounding, Misc. Area Plans, Details \& Elevations | DCT-F-7-0 |
|  | 310248-FP | Underground Duct Plan - Center | DCT-F-4A-0, <br> DCT-F-1B-0, <br> DCT-F-5A-0, <br> DCT-F-4B-0, <br> DCT-F-7-0, <br> DCT-F-1A-0, <br> DCT-F-3B-0 |
|  | 310249-FP | Underground Duct Plan - South | DCT-F-1A-0, <br> DCT-F-2B-0, <br> DCT-F-lB-0, <br> DCT-F-2A-0 |
|  | 300245- FP | Underground Duct Plan - Circ. \& Service Water Area | DCT-F-6-0 |
|  | 320252-PP | Underground Duct Plan - South | $\begin{aligned} & \text { DCT-F-2A-0 } \\ & \text { DCT-F-2B-0 } \end{aligned}$ |
|  | 310828 -FP | Condensate \& Demineralized Water Storage Tanks Conduit, Lighting \& Grounding Plan | DCT-F-7-0 |

NOTE: Refer to controlled equipment drawings for most up to date equipment locations

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This section summarizes the results of the fire analysis performed on Seabrook Station. The information is presented under the following major headings:
F. $1 \quad$ Evaluation and Comparison Matrix
F. 2 Results of Fire Hazard Analysis
F. 3 Responses to BTP APCSB 9.5-1, Appendix A:
o Overall requirements of Nuclear plant fire protection program
o Administrative procedures, controls and fire brigade
o Quality assurance program
o General guidelines for plant protection
o Fire detection and suppression

- Guidelines for specific plant areas
o Special protection guidelines

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## F. 1 EVALUATION AND COMPARISON MATRIX

The Evaluation and Comparison Matrix, Table 3, correlates the requirements of each position of the BTP with each fire area/zone, and summarizes the areas of compliance, basic compliance and non-compliance with APCSB 9.5-1, Appendix A.

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Table 3
Fire Protection System Evaluation And Comparison Matrix

|  | Appendix A Branch Technical <br> Position <br> APCSB 9.5-1 | Comply <br> With | Partially Comply <br> With | Do Not <br> Comply <br> With | See Following <br> Pages For <br> Discussion |
| :---: | :---: | :---: | :---: | :---: | :---: |

A. Overall Requirements of Nuclear Plant Fire Protection Program

| 1. | Personnel | X |  |  | F.3-15 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2. | Design Bases | X |  |  | F.3-17 |
| 3. | Back-up | X |  |  | F.3-17 |
| 4. | Single Failure Criterion | X |  |  | F.3-18 |
| 5. | Fire Suppression Systems | X |  |  | F.3-20 |
| 6. | Fuel Storage Areas | X |  |  | F.3-21 |
| 7. | Fuel Loading | X |  |  | F.3-21 |
| 8. | Multiple-Reactor Sites | X |  |  | F.3-22 |
| 9. | Simultaneous Fires | X |  |  | F.3-22 |
| B. Administrative Procedures Controls and Fire Brigade |  |  |  |  |  |
| 1. | Fire Protection System and Personnel Administrative Procedures | X |  |  | F.3-23 |
| 2. | Bulk Storage of Combustible Materials | X |  |  | F.3-24 |
| 3. | Normal/Abnormal Conditions Or Other Anticipated Operations | X |  |  | F.3-24 |
| 4. | Public Fire Department Support | X |  |  | F.3-26 |
| 5. | Plant Fire Brigade Guidance | X |  |  | F.3-26 |
| 6. | Coordination With Local Fire Department | X |  |  | F.3-28 |
| 7. | NFPA Standards | X |  |  | F.3-29 |


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Table 3
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|  | Appendix A Branch Technical Position APCSB 9.5-1 | Comply With | Partially Comply With | Do Not Comply With | See Following Pages For Discussion |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C. Quality Assurance Program |  |  |  |  |  |
| 1. | Design Control and Procurement Document Control | X |  |  | F.3-30 |
| 2. | Instructions, Procedures and Drawings | X |  |  | F.3-31 |
| 3. | Control of Purchased Material, Equipment and Services | X |  |  | F.3-31 |
| 4. | Inspection | X |  |  | F.3-32 |
| 5. | Test and Test Control | X |  |  | F.3-32 |
| 6. | Inspection, Test and Operating Status | X |  |  | F.3-33 |
| 7. | Non-Conforming Items | X |  |  | F.3-33 |
| 8. | Corrective Action | X |  |  | F.3-34 |
| 9. | Records | X |  |  | F.3-34 |
| 10. | Audits | X |  |  | F.3-35 |
| D. General Guidelines for Plant Protection |  |  |  |  |  |
| 1. | Building Design |  |  |  |  |
|  | (a) Plant Layouts | X |  |  | F.3-36 |
|  | (b) Detailed Fire Hazard Analysis | X |  |  | F.3-37 |
|  | (c) Cable Spreading Rooms |  | X |  | F.3-37 |
|  | (d) Non-Combustibility Requirements for Interior Construction | X |  |  | F.3-38 |
|  | (e) Metal Deck Roof Construction | X |  |  | F.3-39 |
|  | (f) Suspended Ceilings | X |  |  | F.3-39 |
|  | (g) High Voltage, High Ampere Transformers | X |  |  | F.3-40 |
|  | (h) Oil-Filled Transformers | X |  |  | F.3-40 |
|  | (i) Floor Drains |  | X |  | F.3-41 |
|  | (j) Floors, Walls and Ceilings |  | X |  | F.3-43 |


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Table 3
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|  | Appendix A Branch Technical Position APCSB 9.5-1 | Comply With | Partially Comply With | Do Not Comply With | See Following Pages For Discussion |
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| D. General Guidelines for Plant Protection (Continued) |  |  |  |  |  |
| 2. | Control of Combustibles |  |  |  |  |
|  | (a) Protection of Safety-Related Systems | X |  |  | F.3-44 |
|  | (1) Diesel generator fuel oil day tank | X |  |  | F.3-44 |
|  | (2) Turbine - generator oil and hydraulic control systems | X |  |  | F.3-44 |
|  | (3) Reactor coolant pump lube oil System |  | X |  | F.3-45 |
|  | (b) Bulk Gas Storage | X |  |  | F.3-45 |
|  | (c) Use of Plastic Materials | X |  |  | F.3-48 |
|  | (d) Storage of Flammable Liquids | X |  |  | F.3-49 |
| 3. | Electric Cable Construction, Cable Trays and Cable Penetrations |  |  |  |  |
|  | (a) Cable Tray Construction | X |  |  | F.3-50 |
|  | (b) Cable Spreading Rooms |  | X |  | F.3-50 |
|  | (c) Cable Trays Outside Cable Spreading Rooms |  | X |  | F.3-51 |
|  | (d) Cable and Cable Tray Penetrations of Fire Barriers | X |  |  | F.3-52 |
|  | (e) Fire Breaks | X |  |  | F.3-52 |
|  | (f) Flame Test of Electric Cables | X |  |  | F.3-53 |
|  | (g) Corrosive Gases from Cables | X |  |  | F.3-54 |
|  | (h) Content of Cable Trays, Raceways, Conduit, Trenches and Culverts | X |  |  | F.3-54 |
|  | (i) Smoke Venting of Cable Tunnels, Culverts and Spreading Rooms | X |  |  | F.3-55 |
|  | (j) Control Room Cables |  | X |  | F.3-55 |


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| :--- | :---: | :--- |

Table 3
Fire Protection System Evaluation And Comparison Matrix

|  | Appendix A Branch Technical Position APCSB 9.5-1 | Comply With | Partially Comply With | Do Not Comply With | See Following Pages For Discussion |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D. General Guidelines for Plant Protection (Continued) |  |  |  |  |  |
| 4. | Ventilation |  |  |  |  |
|  | (a) Discharge of Products of Combustion |  | X |  | F.3-56 |
|  | (b) Evaluation of Inadvertent Operation or Single Failures | X |  |  | F.3-57 |
|  | (c) Power Supply and Controls |  | X |  | F.3-58 |
|  | (d) Protection of Charcoal Filters |  | X |  | F.3-59 |
|  | (e) Fresh Air Supply Intakes | X |  |  | F.3-60 |
|  | (f) Stairwells |  | X |  | F.3-60 |
|  | (g) Smoke and Heat Vents |  | X |  | F.3-61 |
|  | (h) Self-Contained Breathing Apparatus | X |  |  | F.3-62 |
|  | (i) $\begin{aligned} & \text { Total Flooding Gas } \\ & \\ & \text { Extinguishing Systems }\end{aligned}$ | X |  |  | F.3-63 |
| 5. | Lighting and Communications |  |  |  |  |
|  | (a) Fixed Emergency Lighting |  | X |  | F.3-63 |
|  | (b) Portable Lights | X |  |  | F.3-63 |
|  | (c) Fixed Emergency Communication | X |  |  | F.3-63 |
|  | (d) Portable Radio Communication | X |  |  | F.3-63 |


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Table 3
Fire Protection System Evaluation And Comparison Matrix

|  | Appendix A Branch Technical Position APCSB 9.5-1 | Comply With | Partially Comply With | Do Not Comply With | See Following Pages For Discussion |
| :---: | :---: | :---: | :---: | :---: | :---: |
| E. Fire Detection \& Suppression |  |  |  |  |  |
| 1. | Fire Detection |  |  |  |  |
|  | (a) Conformance to NFPA 72D | X |  |  | F.3-66 |
|  | (b) Alarm and Annunciation |  | X |  | F.3-66 |
|  | (c) Distinctive and Unique Fire Alarms | X |  |  | F.3-66 |
|  | (d) Connection to Emergency Power Supply | X |  |  | F.3-66 |
| 2. | Fire Protection Water Supply System |  |  |  |  |
|  | (a) Yard Fire Main Loop | X |  |  | F.3-67 |
|  | (b) Multiple Units Fire Protection Water Supply Systems | X |  |  | F.3-68 |
|  | (c) Fire Pump Installation | X |  |  | F.3-69 |
|  | (d) Fire Water Supplies | X |  |  | F.3-70 |
|  | (e) Fire Water Supply Design Bases | X |  |  | F.3-71 |
|  | (f) Lakes or Ponds as Sources | NA |  |  | F.3-72 |
|  | (g) Outside Hose Installations | X |  |  | F.3-73 |
| 3. | Water Sprinklers and Hose Standpipe Systems |  |  |  |  |
|  | (a) Sprinkler and Standpipe Layout | X |  |  | F.3-74 |
|  | (b) Supervision of Valves |  | X |  | F.3-75 |
|  | (c) Automatic Sprinkler Systems | X |  |  | F.3-75 |
|  | (d) Fire Protection Water Supply System |  | X |  | F.3-76 |
|  | (e) Hose Nozzles | X |  |  | F.3-78 |
|  | (f) Foam Suppression | NA |  |  | F.3-78 |
| 4. | Halon Suppression Systems | X |  |  | F.3-79 |
| 5. | Carbon Dioxide Suppression Systems | NA |  |  | F.3-80 |
| 6. | Portable Extinguishers | X |  |  | F.3-81 |


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Table 3
Fire Protection System Evaluation And Comparison Matrix

|  | Appendix A Branch Technical <br> Position <br> APCSB 9.5-1 | Comply <br> With | Partially Comply <br> With | Do Not <br> Comply <br> With | See Following <br> Pages For <br> Discussion |
| :--- | :---: | :---: | :---: | :---: | :---: |


| F. Guidelines for Specific Plant Areas |  |
| :--- | :--- |
| 1. | Primary and Secondary Containment |
|  |  |


|  | (a) Normal Operation |  | X | F.3-82 |
| :---: | :---: | :---: | :---: | :---: |
|  | (b) Refueling and Maintenance | X |  | F.3-84 |
| 2. | Control Room |  | X | F.3-85 |
| 3. | Cable Spreading Room |  | X | F.3-87 |
| 4. | Plant Computer Room | X |  | F.3-89 |
| 5. | Switchgear Rooms |  | X | F.3-90 |
| 6. | Remote Safety-Related Panels |  | X | F.3-91 |
| 7. | Station Battery Rooms | X |  | F.3-92 |
| 8. | Turbine Lubrication and Control Oil Storage and Use Areas | X |  | F.3-93 |
| 9. | Diesel Generator Areas |  | X | F.3-94 |
| 10. | Diesel Fuel Oil Storage Areas |  | X | F.3-96 |
| 11. | Safety-Related Pumps |  | X | F.3-97 |
| 12. | New Fuel Area |  | X | F.3-98 |
| 13. | Spent Fuel Pool Area |  | X | F.3-99 |
| 14. | Radwaste Building |  | X | F.3-100 |
| 15. | Decontamination Areas |  | X | F.3-101 |
| 16. | Safety-Related Water Tanks | X |  | F.3-101 |
| 17. | Cooling Towers | X |  | F.3-102 |
| 18. | Miscellaneous Areas | X |  | F.3-102 |

G. Special Protection Guidelines

| 1. | Welding and Cutting, Acetylene - <br> Oxygen Fuel Gas Systems |  | X | X | $\mathrm{F} .3-103$ |
| :--- | :--- | :---: | :---: | :---: | :---: |
| 2. | Storage Areas for Dry Ion <br> Exchange Resins |  | X |  | $\mathrm{F} .3-104$ |
| 3. | Hazardous Chemicals | X |  |  | $\mathrm{F} .3-104$ |
| 4. | Materials Containing Radioactivity | X |  |  | $\mathrm{F} .3-105$ |


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## Fire Hazard Analysis C-F-1-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Containment Building
C-F-1-Z
Containment Floor
El. (-) 26'-0"
9763-F-805051-FP
3.0 Construction of Area

| 3.1 | Walls |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
|  |  | North | Concrete | 3 Hr . |
|  |  | South | Concrete | 3 Hr . |
|  |  | East | Concrete | 3 Hr . |
|  |  | West | Concrete | 3 Hr . |
| 3.2 | Floor |  | Concrete | 3 Hr . |
| 3.3 | Ceiling |  | Concrete/Grating/Stl Plate | - |
| 3.4 | Doors |  | None | - |
| 3.5 | Others |  | - | - |

4.0 Floor Area $\quad 15,400$ Sq. Ft. Diameter $\underline{140^{\prime}-0^{\prime \prime}}$ Height $\underline{26^{\prime}}$
5.0 Volume $\quad 400,000 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains

Nuclear X Non-Nuclear
7.0 Exhaust Ventilation System
7.1 Percentage of System's Capacity No Exhaust
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area
8.1 Outside Area at Exit Points

$\qquad$
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 This zone will be affected by a fire in the zone above (C-F-2-Z) due to the deck grating at the $0^{\prime}-0^{\prime \prime}$ level, therefore see zone C-F-2-Z for effects of the design basis fire.

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Nuclear Instrumentation \& Cabling | NI | X | X | X |
| Piping, Valves, Equipment \& Cabling | RC | X | X | X |
| Piping, Valves \& Cabling | SI | X | X | X |
| Piping, Valves \& Cabling | CS | X | X | X |
| Cabling | CAP |  | X | X |
| Cabling | CAH |  | X | X |
| Piping, Instrumentation \& Cabling | CBS | X | X | X |
| Piping, Valves, Motors \& Cabling | CC | X | X | X |
| Piping, Valves \& Cabling | COP |  | X | X |
| Penetrations, Equipment \& Cabling | EDE | X | X | X |
| Piping, Valves \& Cabling | NG |  | X | X |
| Piping, Valves \& Cabling | VG |  | X | X |
| Piping Valves \& Cabling | WLD |  | X | X |
| Pressurizer Heaters | RC | X | X |  |
| Cabling | CGC |  | X | X |
| Instrumentation \& Cabling | RM |  | X | X |
| Cabling | ED |  | X |  |
| Cabling | IA |  | X |  |
| Cabling | SA |  | X |  |


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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Incore Instrumentation \& Cabling | IC | X | X | X |
| Instrumentation \& Cabling | FW | X | X | X |
| Instrument Racks | MM | X | X | X |
| Piping, Valves \& Cabling | RH | X | X | X |


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## Fire Hazard Analysis C-F-2-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  | Drawing No |  |
| 3.0 | Construction of Area |  |



### 11.0 Fire Loading in Area

11.1 Refer to page 3 (analysis continued Pg. 2 \& 3)

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Rc Pumps | RC | X |  |  |
| Steam Generators | RC |  |  | X |
| Piping, Valves, Fans \& Cabling | CAH | X | X | X |
| Piping, Valves, <br> Instruments \& Cabling | FW | X | X | X |
| Piping, Valves, <br> Instruments \& Cabling | CC | X | X | X |
| Cabling | CBS | X | X | X |
| Piping, Valves \& Cabling | CAP |  | X | X |
| Penetrations | EDE | X |  | X |
| Cabling | CS | X |  | X |
| Instrument Racks | MM | X | X | X |
| Instruments \& Cabling | RC | X | X | X |
| Radiation Monitors \& Cabling | RM | X | X | X |
| Piping Valves \& Cabling | SI | X | X | X |
| Cabling | NI | X |  |  |
| Distr Pnl \& Cabling | ED | X |  |  |
| Dryer, Contractor \& Cabling | IA | X | X |  |
| Compressor, Control Pnl \& Cabling | SA | X | X |  |
| Cabling | CGC | X |  | X |
| Contm. Coolers | CAH |  | X |  |
| Contm. Coolers | CAH | X |  |  |
| Piping, Valves \& Cabling | SB | X |  | X |
| Incore Instruments \& Cabling | IC | X | X | X |


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| :--- | :---: | :--- |
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13.0 Design Basis Fire


| 13.2 | Total Fire Loading in Area: | 2580 Btu/Sq. Ft. |
| :---: | :---: | :---: |
|  | Total Combustibles: | 39,750,000 Btu |

14.0 Design Basis Fire Description

See Appendix B of this report.


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| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related |
| :--- | :--- | :---: | :---: | :---: |
| Radiation Element. <br> Monitors \& Cabling | RM | X | B | $\frac{\mathrm{X}}{\mathrm{B}}$ |
|  <br> Cabling | RC | X | X | X |
|  <br> Cabling | CAH | X | X | X |
| Piping, Valves, <br> Recombiners \& Cabling <br> Penetrations CGC | X | X | X |  |
|  | MM | X |  | X |


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Fire Hazard Analysis - EFP-F-1-A

| 1.0 | Building |  |  | Emergency Feedwater Pump Building |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | EFP-F-1-A |  |
|  | 2.1 | Area Name |  | Pump Area |  |
|  | 2.2 | Location |  | El. 27'-0" |  |
|  |  | Drawing No |  | 9763-F-20 |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire Rating |
|  | 3.1 | Walls | North | Concrete | Outside |
|  |  |  | South | Concrete | 3 Hr . |
|  |  |  | East | Concrete | $3 \mathrm{Hr} . / O \mathrm{tside}$ |
|  |  |  | West | Concrete | 3 Hr ./Outside |
|  | 3.2 | Floor |  | Concrete | 3 Hr |
|  | 3.3 | Ceiling |  | Concrete | Outside |
|  | 3.4 | Doors |  | Metal | $11 / 2 \mathrm{Hr}$. (Stairwell) |
|  | 3.5 | Others |  | - | - |

4.0 Floor Area 2,400 Sq. Ft. Length $\quad$ 79' Width Varies Height__18'
5.0 Volume $\quad 43,000 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear X_Nonenter None ___
7.0 Exhaust Ventilation System Wall Supply Fan
7.1 Percentage of System's Capacity 100\%

9.0 Operational Radioactivity
9.1 Equipment/Piping $\quad$ Yes $\quad$ No $\frac{\mathrm{X}}{\mathrm{X}}$
9.2 Airborne
10.0 Fire Protection
10.2 Secondary

Yes No X

### 10.1 Primary

Type
Fire Extinguisher(s)
10.3 Detection

Standpipe and Hose Reel
10.4 Other

## Ionization

------------
11.0 Fire Loading in Area
11.1 Refer to page 2. (analysis continued page $2 \& 3$ )

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Emelated |
| :--- | :--- | :--- | :---: | :---: |
| Emergency Feed Pump <br> (M) | FW |  | B | X |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |  |
| :---: | :---: | :---: |
| Oil: | 6 | Gallons |
| Grease: |  | Pounds |
| Class A: |  | Pounds |
| Charcoal: |  | Pounds |
| Chemicals: |  | Pounds |
| Plastics: | 32 | Pounds |
| Resins: |  | Pounds |
| Other: |  |  |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| 375 | Btu/Sq. Ft. |
| :--- | :--- |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 173 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

$$
\begin{aligned}
& \frac{548}{1,316,000} \mathrm{Btu} / \text { Sq. } \mathrm{Ft} . \\
& \text { Btu }
\end{aligned}
$$

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### 14.0 Design-Basis Fire Description

1. Turbine ruptures, oil spills spreading over 78 sq . Ft. Of floor. Oil film is $1 / 8^{\prime \prime}$ thick and burn rate is $5^{\prime \prime}$ per hour.
2. Oil ignites and is consumed.
3. One ventilation supply fan ( $14,000 \mathrm{cfm}$ ) is assumed to fail 30 seconds after fire starts.
4. A fire which considers oil to be sprayed over a large area will have the same total heat release but the heat will not be concentrated to a small area.
5. A fire which considers oil to spill over a small area will be more concentrated.
6. The DBF over the small area as postulated is considered to be the most serious as it will damage electrical cables in the immediate area.
14.1 DBF Fire Loading $\quad 11,500$ Btu/Sq. Ft.
14.2 Duration of Fire $\quad 4 \frac{1}{2}$ Minutes
14.3 Peak Temperature $\quad 601 ~{ }^{\circ} \mathrm{F}$
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Turbine is lost.
15.2 Safe shutdown can be accomplished by use of startup feed pump. For further discussion, refer to the report on "Fire Protection Of Safe Shutdown Capability" (10 CFR 50, Appendix R).
16.0 Consequence of Design Basis Fire with Fire Protection
16.1 Loss of the turbine due to loss of oil.
17.0 Consequence of Inadvertent or Careless Operation or Rupture of the Fire Protection System
17.1 Not applicable (no water fire suppression in area).

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| :--- | :---: | :--- |
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18.0 Containing the Design Basis Fire in the Fire Area/Zone
18.1 A) Short fire duration.
B) Concrete structure.
19.0 How the Redundant Safe Shutdown Equipment in the Same Area is Protected
19.1 Spatial separation between pumps.
19.2 Curb around the turbine base to contain an oil spill.

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| :--- | :---: | :--- |
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Fire Hazard Analysis - MS-F-1A-Z

| 1.0 | Building |  |  | Main Steam \& Feedwater Enclosure (East) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | MS-F-1A-Z |  |
|  | 2.1 | Area Name |  | Lower Level |  |
|  | 2.2 | Location |  | East El. 3'-0" |  |
|  |  | Drawing No |  | 9763-F-202 |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fir |
|  | 3.1 | Walls | North | Concrete | Outside |
|  |  |  | South | Concrete | 3 Hr . |
|  |  |  | East | Concrete | Outside |
|  |  |  | West | Concrete | $3 \mathrm{Hr} . / \mathrm{Ou}$ |
|  | 3.2 | Floor |  | Concrete | 3 Hr |
|  | 3.3 | Ceiling |  | Grating | - |
|  | 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . /-$ |
|  | 3.5 | Others |  | - | - |


5.0 Volume $\quad 20.740 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear __ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System
7.1 Percentage of System's Capacity 100\%
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points

Yes $\qquad$ No

Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection

Yes
Yes
 No

Type
Fire Extinguisher(s)
Yard Hydrant
10.4 Other

Ionization
------
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

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| :--- | :---: | :--- |
| Appendix A | Section F.2 Tab 3 <br> Page 2 of 2 |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Piping, Valves \& Cabling | MS | X | X | X |
| Piping, Valves, Instrumentation \& Cabling | FW | X | X | X |
| Cabling | EAH | X | X | X |
| Terminal Boxes | EDE | X |  | X |
| Piping, Valves \& Cabling | MSD | X |  | X |


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| :--- | :---: | :--- |

Fire Hazard Analysis - MS-F-1B-Z


| 4. | Floor Area | 935 Sq. Ft. Length $74{ }^{\prime}$ | Width | 14' | Height 25' |
| :---: | :---: | :---: | :---: | :---: | :---: |

5.0 Volume $\quad 15,900 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear __ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System
7.1 Percentage of System's Capacity 100\%
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points

Yes $\qquad$ No

Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Yes
Yes
Type
Fire Extinguisher(s)
Hose Station
Ionization
------
11.0 Fire Loading in Area
11.1 Ref. Page 2 of 3

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| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Piping and Valves | SB | X | X | X |
| Instrument Rack -IR-52A, 52B | MM | X | X | X |
| Piping, Valves \& Cabling | MS | X | X | X |
| Cabling | SB | X | X | X |
| Piping, Valves, Instrumentation \& Cabling | FW | X | X | X |
| Terminal Boxes | EDE | X |  | X |
| Piping Valves \& Cabling | MSD | X |  | X |

13.0 Design Base Fire

| 13.1 | Combustible in Area (In Situ) |  |  | Fire Loading in Area |
| :---: | :---: | :---: | :---: | :---: |
|  | Note: | Oil Fire |  |  |
|  | Oil: | 1 | Gallons | $160 \mathrm{Btu} / \mathrm{Sq}$. Ft. |
|  | Grease: |  | Pounds | Btu/Sq. Ft. |
|  | Class A: |  | Pounds | Btu/Sq. Ft. |
|  | Charcoal: |  | Pounds | Btu/Sq. Ft. |
|  | Chemicals: |  | Pounds | Btu/Sq. Ft. |
|  | Plastics: | 11 | Pounds | 153 Btu/Sq. Ft. |
|  | Resins: |  | Pounds | Btu/Sq. Ft. |
|  | Other: |  |  |  |
| 13.2 | Total Fire Loading in Area: Total Combustibles: |  |  | 313 Btu/Sq. Ft. |
|  |  |  |  | 293,000 Btu |

### 14.0 Design-Basis Fire Description

1. One of the four (4) steam recirculating pump ruptures, one quart oil spills on floor covering an area of $3 \mathrm{ft} . \mathrm{x} 4 \mathrm{ft}$. $=12 \mathrm{sq} . \mathrm{Ft}$.
2. To add conservatism, the oil contents of all four (4) pumps is considered to be spilled on floor (total 1.0 gallon) and burn completely.
3. The ventilating supply fan failed.

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| Fire Hazard Analysis - MS-F-1B-Z |  |  |$\quad$| Page 3 of 3 Tab 3 |
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14.1 DBF Fire Loading $\quad 125,000$ Btu/Sq. Ft.
14.2 Peak Zone Temperature Fire $\quad 712{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
$4_{1 / 2}^{2}$ Min.
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of the steam recirculation and layup pumps due to loss of oil.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Not applicable (no water fire suppression in area).
$\begin{array}{ll}17.0 & \text { Consequences of Inadvertent or Careless Operation or Rupture of the Fire Protection } \\ \text { System }\end{array}$
17.1 Not applicable (no water suppression in area).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Short fire duration, less than five minutes.
18.2 Concrete structure.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 The redundant safe shutdown equipment is located in a separate fire area.

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Fire Hazard Analysis - MS-F-2A-Z

| 1.0 | Building |  |  | Main Steam \& Feedwater Enclosure (East) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | MS-F-2A-Z |  |
|  | 2.1 | Area Name |  | Upper Level |  |
|  | 2.2 | Location |  | East El. 27'-6" |  |
|  | Drawing No |  |  | 9763-F-202063-FP, - 20 |  |
| 3.0 | Construction of Area |  |  |  | Min. Fire Rating |
|  |  |  |  | Material |  |
|  | 3.1 | Walls | North | Concrete | Outside |
|  |  |  | South | Concrete | 3 Hr . |
|  |  |  | East | Concrete | Outside |
|  |  |  | West | Concrete | $3 \mathrm{Hr} . / \mathrm{Ou}$ |
|  | 3.2 | Floor |  | Grating | - |
|  | 3.3 | Ceiling |  | Concrete | Outside |
|  | 3.4 | Doors |  | Metal | $3 \mathrm{Hr} /-$ |
|  | 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area $\quad$ 1,220 Sq. Ft. Length 74.75' Width $16.25^{\prime}$ ' Height $40^{\prime}$
5.0 Volume $\quad 48,800 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear X_Non-Nuclear __ None
7.0 Exhaust Ventilation System Supply System Only
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points
$\qquad$ No

Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary

10.3 Detection
10.4 Other

Type
Fire Extinguisher(s)
Hose Station
Beam
-------
11.0 Fire Loading in Area
11.1 Refer to page 2. (analysis continued pages $2 \& 3$ ).

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| :--- | :---: | :--- |
| Fire Hazard Analysis - MS-F-2A-Z |  |  |$\quad$| Section F.2 Tab 3 |
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12.0 Equipment and Systems in Fire Area/Zone

System Train Safety
Equipment
Piping and Valves
Cabling
Piping, Valves \& Cabling

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

| Oil: | Gallons |
| :--- | :--- |
| Grease: | Pounds |
| Class A: | $=$ Pounds |
| Charcoal: | $=$ Pounds |
| Chemicals: | $=$ Pounds |
| Plastics: | Pounds |
| Resins: | $=$ |
| Other: | $=$ |

$\begin{array}{llrl}\text { 13.2 } & \text { Total Fire Loading in Area: } & 320 & \text { Btu/Sq. Ft. } \\ \text { Total Combustibles: } & 390,000 & \text { Btu }\end{array}$

| Fire Load | gin in Area |
| :---: | :---: |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 320 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

Design-Basis Fire Description

1. For conservatism, the ladders are assumed to be in a vertical position. The bottom of both sets of rails are ignited and burn upward.
2. To add conservatism, it is assumed that the fire is self-sustaining, although the fire is not severe and has a low heat release rate.
3. The fire area will be limited to the length of the ladders and about 2 feet from the wall for an area covering $10 \mathrm{ft} . \times 2 \mathrm{ft} .=20 \mathrm{ft}^{2}$.
14.1 DBF Fire Loading

19,500 Btu/Sq. Ft.
14.2 Peak Zone Temperature Fire
14.3 Duration of Fire
$152{ }^{\circ} \mathrm{F}$
$\gg 5$ Minutes

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| :--- | :---: | :--- |
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15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Refer to Seabrook Station fire protection of safe shutdown capability ( 10 CFR 50, App. R).

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 No consequences . . . Fire will be extinguished with manual hose lines or portable extinguishers.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of The Fire Protection System
17.1 Not applicable.
18.0 Containing Design Basis Fire in The Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire would be extinguished using hose lines and/or portable extinguishers.
19.0 How The Redundant Safe Shutdown Equipment in The Same Area is Protected
19.1 Refer to safe shutdown requirements Table 3.2.7.58 of the report Seabrook Station Fire Protection Safe Shutdown Capability (10 CFR 50, Appendix R).

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Fire Hazard Analysis - MS-F-2B-Z

4.0 Floor Area 935 Sq. Ft. Length 66.75' Width $14^{\prime}$ Height $40^{\prime}$
5.0 Volume $\quad 37.400 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear __ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System
7.1 Percentage of System's Capacity $\quad 100 \%$
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points

Yes $\qquad$ No

Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne

10.0 Fire Protection
10.1 Primary
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Hose Station
10.4 Other

Beam
------
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

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| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Piping and Valves | MS | X | X | X | X |
| Cabling | MS | X | X | X | X |
| Cabling | SB | X | X | X | X |


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| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - MS-F-3A-Z |  |

Fire Hazard Analysis - MS-F-3A-Z


5.0 Volume $\quad 5145 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear __ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System EAH
7.1 Percentage of System's Capacity $\quad 100 \%$
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points $\qquad$ No

Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne

10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Type
Fire Extinguisher(s)
Yard Hydrant
Ionization
------
11.0 Fire Loading in Area
11.1 None X_(no further analysis required)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 7 <br> Appendix A <br> Section F.2 Tab 3 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ | $\underline{l}$ System Train | Safety <br> Related |  |
| :--- | :---: | :---: | :---: | :---: |
| MSIV-Logic Cab. <br> CP-182 | MS | X | $\underline{B}$ | X |
| MSIV-Logic Cab. <br> CP-184 | MS |  | X | X |
| Cabling | MS | X | X | X |
|  <br> Cabling | FW | X | X | X |
| Instrument Racks <br> IR-51A, 51B <br>  | HT | X | X | X |
| Cabling |  |  |  |  |


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| :--- | :---: | :--- |
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Fire Hazard Analysis - MS-F-3B-Z

| 1.0 | Building |  |  | Main Steam \& Feedwater Enclosure (West) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | MS-F-3B-Z |  |
|  | 2.1 | Area Name |  | Personnel Hatch Area |  |
|  | 2.2 | Location |  | Northeast of West MS\&FEW - N1 12' $-0^{\prime \prime}$ \& 21' $-0^{\prime \prime}$ |  |
|  |  | Drawin |  | 9761-F-20 |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire |
|  | 3.1 | Walls | North | Concrete | $3 \mathrm{Hr} . / \mathrm{Out}$ |
|  |  |  | South | Concrete | 3 Hr . |
|  |  |  | East | Concrete | 3 Hr . |
|  |  |  | West | Concrete | Outside/- |
|  | 3.2 | Floor |  | Concrete | Outside |
|  | 3.3 | Ceiling |  | Concrete | Outside |
|  | 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . /$ * |
|  | 3.5 | Others |  | - | - |

4.0 Floor Area 1,656 Sq. Ft. Length Varies Width Varies Height Varies
5.0 Volume 40,392 Cu. Ft.
6.0 Floor Drains Nuclear __ Non-Nuclear X None ___
7.0 Exhaust Ventilation System ----
7.1 Percentage of System's Capacity

8.0 8 Hr. Emergency Lighting in Area

Yes $\qquad$ No
8.1 Outside Area at Exit Points

Yes $\qquad$ No

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne

Yes
Yes $\qquad$ No

Type
Fire Extinguisher(s)
Yard Hydrant
Ionization
------
11.0 Fire Loading in Area
11.1 Refer To Page 2. (Analysis continued pages 2 \& 3).

[^1]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 13 <br> Station |
| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{l}$System Train | Safety <br> Related |  |
| :--- | :--- | :--- | :---: | :---: |
| Cabling | MS | X | $\underline{B}$ | $\underline{\mathrm{~A}}$ |
| Cabling | SB | X | X |  |
| Cabling | FW | X | X |  |
| Cabling | AS | X | X |  |
| Cabling | MSD | X | X |  |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Oil: | Gallons |
| :--- | :--- |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | $=$ Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: | $=$ |

13.2 Total Fire Loading in Area:

Total Combustibles:

### 14.0 Design-Basis Fire Description

1. For conservatism, the ladders are assumed to be in a vertical position. The bottom of both sets of rails are ignited and burn upward.
2. To add conservatism, it is assumed that the fire is self-sustaining, although the fire is not severe and has a low heat release rate.
3. The fire area will be limited to the length of the ladders and about 2 feet from the wall for an area covering 40 ft . x $2 \mathrm{ft} .=80 \mathrm{ft}^{2}$.

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Note: Fiberglass ladders previously stored in MS-F-3B-Z were removed per EC 156668, but retained in this fire hazard analysis to support future ladder storage in this fire zone. The plastic components typically contained in the permanent storage area located in this fire zone for a Radiation Protection workstation are not considered to contribute to the design basis fire. Refer to Calc MS-MISC-41 for details and additional discussion.
14.1 DBF Fire Loading 18,038 Btu/Sq. Ft.
14.2 Peak Zone Temperature Fire $219{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire $\quad>5$ Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Refer to Seabrook Station Fire Protection of Safe Shutdown Capability (10 CFR 50, App. R).
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished with manual hose lines or portable extinguishers.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable

### 18.0 Containing Design Basis Fire in The Fire Area/Zone

18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire would be extinguished using hose lines and/or portable extinguishers.
19.0 How The Redundant Safe Shutdown Equipment in The Area is Protected
19.1 Refer to Safe Shutdown Requirements Table 3.2.7.59 of the report Seabrook Station Fire Protection Safe Shutdown Capability (10 CFR 50, Appendix R).

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Fire Hazard Analysis - MS-F-4A-Z

| 1.0 | Building | Mainstream \& Feedwater Pipe Chase (East) |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area or Zone | MS-F-4A-Z |  |
|  | $2.1 \quad$ Area Name | H2 Analyzer Room |  |
|  | $2.2 \quad$ Location | South End of East MS \& FEW - El. 22'-0"' |  |
|  |  | Drawing No | 9763-F-202063-FP \& 202064-FP |

3.0 Construction of Area

| 3.1 | Walls |  | Material | Min. Fire |
| :---: | :---: | :---: | :---: | :---: |
|  |  | North | Concrete | 3 Hr . |
|  |  | South | Concrete | Outside |
|  |  | East | Concrete | Outside |
|  |  | West | Concrete | 3 Hr . |
| 3.2 | Floor |  | Concrete | - |
| 3.3 | Ceiling |  | Concrete | Outside |
| 3.4 | Doors |  | Metal | $11 / 2 \mathrm{Hr}$. |
| 3.5 | Others |  | - | - |

4.0 Floor Area 294 Sq. Ft. Length Varies Width $14^{\prime}-0^{\prime \prime}$ Height $16^{\prime}-0^{\prime \prime}$
5.0 Volume 4,704 Cu. Ft.
6.0 Floor Drains Nuclear __ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System EAH
7.1 Percentage of System's Capacity $\quad 100 \%$
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points $\qquad$ No

Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne

10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Type
Fire Extinguisher(s)
Yard Hydrant
Ionization
------
11.0 Fire Loading in Area
11.1 None X_(no further analysis required)

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ | $\underline{l} \underline{\text { System Train }}$ | Safety <br> Related |  |
| :--- | :--- | :--- | :---: | :---: |
| Fan FN-174A \& B | EAH | X | X | X |
| Cabling | EAH | X | X | X |
|  <br> Cabling | CGC | X | X | X |
| Temperature Sws | EAH | X | X | X |
| Control Panels, Transf. <br> Heaters \& Cabling | HT | X | X | X |


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Fire Hazard Analysis - MS-F-5A-Z

| 1.0 | Building |  |  | Main Steam \& Feedwater Pipe Chase (East) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | MS-F-5A-Z |  |
|  | 2.1 | Area Name |  | Cable Tunnel |  |
|  | 2.2 | Location |  | Northwest of East MS \& FWE - El. 8'-2' |  |
|  |  | Drawin |  | 9763-F-20 |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fir |
|  | 3.1 | Walls | North | Concrete | Outside |
|  |  |  | South | Concrete | 3 Hr . |
|  |  |  | East | Concrete | - |
|  |  |  | West | Concrete | 3 Hr . |
|  | 3.2 | Floor |  | Concrete | Outside |
|  | 3.3 | Ceiling |  | Concrete | Outside/ |
|  | 3.4 | Doors |  | Metal | - /3 Hr. |
|  | 3.5 | Others |  | - | - |

4.0 Floor Area $\quad 485$ Sq. Ft. Length Varies Width Varies Height_12'
5.0 Volume $\quad 5,800 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear __ Non-Nuclear X_None__
7.0 Exhaust Ventilation System
7.1 Percentage of System's Capacity


8 Hr . Emergency Lighting in Area
$\begin{array}{ll}8.0 & 8 \text { Hr. Emergency Lighting in Area } \\ & 8.1 \quad \text { Outside Area at Exit Points }\end{array}$
Yes $\qquad$ No
Yes
Yes $\qquad$ No

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection

Yes
Yes $\qquad$ No $\frac{\mathrm{X}}{\mathrm{X}}$
10.4 Other

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
Ionization
None
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

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12.0 Equipment and Systems in Fire Area/Zone

|  |  |  |  | System Train | Safety <br> Required |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Equipment | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ | $\underline{\text { Shutdown }}$ |
| Cabling | MS | X |  | X | X |
| Cabling | SW | X | X | X |  |
| Cabling | SWA | X | X | X |  |


\(\left.$$
\begin{array}{|l|c|l|}\hline \text { SEABROOK } & \text { Evaluation and Comparison to BTP APCSB 9.5-1, } & \begin{array}{l}\text { Rev 7 } \\
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$$ <br>

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety <br> Related |
| :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |
| Cont. Spray Pump P-9B | CBS |  | X | X |
| Instruments \& Cabling | RH |  | X | X |
| Piping, Valves \& Cabling | CBS |  | X | X |
| Piping, Valves and Cabling | CC |  | X | X |

### 13.0 Design Basis Fire

13.1 Combustible in Area (In Situ)

> Fire Loading in Area

| Note: | Oil Fire |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Oil: | 5.0 | Gallons | 3000 | Btu/Sq. Ft. |
|  | 7.25 | Gallons (other zones) |  |  |
| Grease: |  | Pounds |  | Btu/Sq. Ft. |
| Class A: |  | Pounds |  | Btu/Sq. Ft. |
| Charcoal: |  | Pounds |  | Btu/Sq. Ft. |
| Chemicals: |  | Pounds |  | Btu/Sq. Ft. |
| Plastics: |  | Pounds | 260 | Btu/Sq. Ft. |
| Resins: |  | Pounds |  | Btu/Sq. Ft. |
| Other: |  |  |  |  |
| Total Fire L | ing in Are |  | 3,2 | Btu/Sq. Ft. |
| Total Comb | bles: |  | 815,0 | Btu |


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14.0 Design-Basis Fire Description
(a) Fire zones RHR-F-1AZ, RHR-F-1C-Z, RHR-F-2A-Z, and RHR-F-3A-Z constitute on large fire area as they contain open floor hatches and doors, therefore, heat of fire will be disbursed to all 4 zones.
(b) Containment spray pump ruptures and oil spills on floor covering an area of $5 \mathrm{ft} . \times 13 \mathrm{ft} .=65 \mathrm{sq} . \mathrm{ft}$. .
(c) The entire 5 gallons of oil in this zone will burn. In addition, because of high temperature, remote location and absence of automatic suppression system, entire oil content of RHR-F-1C-Z and RHR-F-2A-Z will burn (total of 12.5 gallons with $1,875,000 \mathrm{Btu}$ as D. B. combustibles).
14.1 DBF Fire Loading

15.0 Consequences of Design Basis Fire without Fire Protection
15.1. Loss of pump and loss of cabling in conduit servicing the motor.
15.2. Possible loss of any or all system "A" Train components located in RHR-F-1A-Z, RHR-F-1C-Z, RHR-F-2A-Z, and RHR-F-3A-Z.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1. Same as above as fire duration is less than five minutes, fire location is remote from control room, no automatic suppression system exists.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1. Not applicable (automatic suppression system does not exist).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1. 3-hr. fire barrier between Train "A" and Train "B" equipment and fire duration is less than five minutes, hence fire will be contained within the zones considered.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1. Safe shutdown can be accomplished with the redundant train equipment located in an area separated by 3-hr. fire barriers.

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Fire Hazard Analysis - RHR-F-1B-Z

| 1.0 | Building | RHR, Containment Spray, SI Equip. Vault |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |  |
|  | $2.1 \quad$ Area Name | RHR-F-1B-Z |  |
|  | $2.2 \quad$ Location | Containment Spray Pump - 9A |  |
|  |  | Drawing No | Northwest El. (-) 61'-0" to 25'-6" |
|  |  | 9763-F-805060-FP, 805078-FP |  |

3.0 Construction of Area

|  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Material | Min. Fire Rating |
| 3.1 | Walls | North | Concrete | Outside/3 Hr. |
|  |  | South | Concrete | 3 Hr . |
|  |  | East | Concrete/Open | - |
|  |  | West | Concrete | Outside |
| 3.2 | Floor |  | Concrete | Outside |
| 3.3 | Ceiling |  | Concrete | - |
| 3.4 | Doors |  | Metal | - |
| 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area 250 Sq. Ft. Length $18^{\prime}$ Width $14^{\prime}$ Height $84^{\prime}$
5.0 Volume $\quad 21,200 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear

X Non-Nuclear $\qquad$ None
7.0 Exhaust Ventilation System
7.1 Percentage of System's Capacity
8.0 8 Hr. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes PAB Exhaust System
100 \% - Recirculated

|  | No |
| :--- | :--- |
|  |  |

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes
9.2 Airborne

Yes $\qquad$ $\frac{\mathrm{X}}{\mathrm{X}}$
10.0 Fire ProtectionType
10.1 Primary

Fire Extinguisher(s)
10.2 Secondary
10.3 Detection
10.4 Other

Standpipe and Hose Reel
Ionization
------
11.0 Fire Loading in Area
11.1 Ref. Page 2 of 3.

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{\text { System Train }}$ | Safety <br> Related |  |
| :--- | :--- | :--- | :---: | :---: |
| Cont. Spray Pump P-9A | CBS | X | $\underline{\mathrm{A}}$ | $\underline{\mathrm{X}}$ |
| Cabling | RH | X | X |  |
|  <br> Cabling | CBS | X | X |  |
| Piping, Valves and <br> Cabling | CC | X | X |  |

### 13.0 Design Basis Fire

13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | ---: |
| Oil: | 5.0 Gallons |
| Grease: | Pounds |
| Class A: | Pounds |

Charcoal: Pounds
Chemicals:
Plastics: $\quad 5$ Pounds
Resins:
Other:
13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| 2,000 | Btu/Sq. Ft. |
| :--- | :--- |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 260 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

3,260 Btu/Sq. Ft. 815,000 Btu

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### 14.0 Design-Basis Fire Description

(A) Fire zones RHR-F-1B-Z, RHR-F-1D-Z, RHR-F-2B-Z and RHR-F-3B-Z constitute one fire area as they contain open floor hatches and doors. Therefore, heat of the fire will be disbursed to all four zones.
(B) Containment spray pump ruptures and oil spills on floor covering an area of $5 \mathrm{ft} . \times 13 \mathrm{ft} .=65 \mathrm{sq} . \mathrm{ft}$.
(C) The entire 5 gallons of oil will burn. In addition, because of high temperature, remote location and absence of automatic suppression system, entire oil content of RHR-F-1D-Z and RHR-F-2B-Z will burn (total of 12.5 gallons with $1,875,000$ Btu as D.B. combustibles).
14.1 DBF Fire Loading

11,719 Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. During Fire
$2,306{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
$41 / 2$ Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1. Loss of pump and loss of cabling in conduit servicing the motor.
15.2. Possible loss of any or all system " B " Train components located in RHR-F-1B-Z, RHR-F-1D-Z, RHR-F-2B-Z, and RHR-F-3B-Z.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1. Same as above as fire duration is less than five minutes, fire location is remote from control room, no automatic suppression system exists.

Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1. Not applicable (automatic suppression system does not exist).

### 18.0 Containing Design Basis Fire in the Fire Area/Zone

18.1. 3-hr. fire barrier between Train " $A$ " and Train " $B$ " equipment and fire duration is less than five minutes, hence fire will be contained within the zones considered.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1. Safe shutdown can be accomplished with the redundant train equipment located in an area separated by 3-hr. fire barriers.

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Fire Hazard Analysis - RHR-F-1C-Z

| 1.0 | Building | RHR, Containment Spray, SI Equip. Vault |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |  |
|  | $2.1 \quad$ Area Name |  |  |
| $2.2 \quad$ Location | RHR-F-1C-Z |  |  |
|  |  | Drawing No | RHR Pump -8B |
|  |  | South Side -El. (-) $61^{\prime}-0 \prime \prime$ |  |

3.0 Construction of Area

|  | 咗 |  | Material |  |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Concrete | 3 Hr . |
|  |  | South | Concrete | Outside |
|  |  | East | Concrete | 3 Hr . |
|  |  | West | Concrete | - |
| 3.2 | Floor |  | Concrete | Outside |
| 3.3 | Ceiling |  | Concrete/Grating | - |
| 3.4 | Doors |  | Metal | $11 / 2 \mathrm{Hr}$. |
| 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area $\quad 360$ Sq. Ft. Length $20^{\prime}$ Width ${ }^{18}$ '_Height 8.5'
5.0 Volume $\quad 3,100 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear X_None_ None_ _ _
7.0 Exhaust Ventilation System PAB Exhaust System
7.1 Percentage of System's Capacity $\quad 100 \%$

| 8.0 | 8 | Hr. Emergency Lighting in Area | Yes |  | No $\quad$ X |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | 8.1 | Outside Area at Exit Points | Yes | X | No |

9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
No
No X
Yes $\qquad$
10.0 Fire Protection
10.1 Primary
10.2 Secondary
$\qquad$
$\qquad$
10.3 Detection

Type
Fire Extinguisher(s)
Standpipe \& Hose Reel
Ionization
10.4 Other
------------
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued pages 2 \& 3)

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{l}$ System Train | Safety <br> Related |  |
| :--- | :--- | :---: | :---: | :---: |
| RHR Pump P-8B | RH |  | $\underline{B}$ | $\underline{X}$ |
| Piping \& Valves | RH |  | X | X |
| Piping \& Valves | CC |  | X | X |
| Piping \& Valves | CBS |  | X | X |
| Cabling | RH |  | X | X |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
|  | 1.75 |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | $=$ |
| Other: |  |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| 729 | Btu/Sq. Ft. |
| :--- | :--- |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 181 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. | _ Btu/Sq. Ft.

[^2]327,500 Btu
\(\left.$$
\begin{array}{|l|c|l|}\hline \text { SEABROOK } & \text { Evaluation and Comparison to BTP APCSB 9.5-1, } & \begin{array}{l}\text { Rev 7 } \\
\text { STATION }\end{array}
$$ <br>
Appendix A <br>

Fage 3 F. 2 Tab 4\end{array}\right]\)| Fire Hazard Analysis - RHR-F-1C-Z |
| :--- |

### 14.0 Design-Basis Fire Description

(A) Zones RHR-F-1C-Z, 2A-Z, 3A-Z and 1A-Z Constitute One Large Fire Area As They Contain Open Floor Hatches and Doors.
(B) RH pump ruptures, lube oil spills on floor, covering area of 24 sq . ft .
(C) 1.75 gallons oil ignites and is consumed. In addition, because of high temp. remote location and absence of automatic spray system, entire oil content of RHR-F-2A-Z AND RHR-F-1A-Z will burn (total of 12.5 gallons with $1,875,000$ Btu as total D.B. combustibles).
14.1 DBF Fire Loading

| $\frac{11,719}{2,306}$ |
| :---: |${ }^{\circ} \mathrm{Ftu} / \mathrm{Sq}. \mathrm{Ft}$.

14.3 Duration of Fire
$41 / 2$ Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of pump and cabling located in conduit servicing the motor.
15.2 Possible loss of any or all system "A" Train components located in RHR-F-1A-Z, RHR-F-1C-Z, RHR-F-2A-Z and RHR-F-3A-Z.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Same as above as fire duration is less than five minutes, fire location is remote from control room, no automatic suppression system exists.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of the Fire Protection System
17.1 Not applicable (automatic suppression system does not exist).

### 18.0 Containing the Design Basis Fire in the Fire Area/Zone

18.1 3-hr. fire barrier between Train "A" and Train "B" equipment and fire duration is less than five minutes, hence fire will be contained within the zones considered.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Safe shutdown can be accomplished with the redundant train equipment located in an area separated by 3-hr. fire barriers.

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Fire Hazard Analysis - RHR-F-1D-Z

| 1.0 | Building | RHR, Containment Spray, SI Equip. Vault |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |  |
|  | $2.1 \quad$ Area Name |  |  |
| $2.2 \quad$ Location | RHR-F-1D-Z |  |  |
|  |  | Drawing No | RHR Pump-8A |
|  |  | North Side - El. $(-) 61^{\prime}-0 \prime \prime$ |  |

3.0 Construction of Area

|  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Material | $\frac{\text { Min. Fire }}{\text { Outside }}$ |
|  |  | South | Concrete | 3 Hr . |
|  |  | East | Concrete | 3 Hr . |
|  |  | West | Concrete | - |
| 3.2 | Floor |  | Concrete | Outside |
| 3.3 | Ceiling |  | Concrete/Grating | - |
| 3.4 | Doors |  | Metal | 11/2 Hr./- |
| 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area 360 Sq. Ft. Length $20^{\prime}$ Width ${ }^{18}$ '_Height 8.5'
5.0 Volume $\quad 3,100 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear X_None_ None_ _ _
7.0 Exhaust Ventilation System PAB Exhaust System
7.1 Percentage of System's Capacity $\quad 100 \%$
$\begin{array}{llllll}8.0 & 8 \mathrm{Hr} \text {. Emergency Lighting in Area } & \text { Yes } & & \text { No } \quad \begin{array}{l}\text { X } \\ \\ 8.1\end{array} & \text { Outside Area at Exit Points } \\ & \text { Yes } & \mathrm{X} & \text { No }\end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
No
No X
Yes
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
$\qquad$

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
Ionization
10.4 Other
------------
11.0 Fire Loading in Area
11.1 Refer to Page 2 (analysis continued pages 2 \& 3)

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{\text { System Train }}$ |  | Safety <br> Related |
| :--- | :--- | :--- | :---: | :---: |
| RHR Pump P-8A | RH | X | $\underline{B}$ | $\underline{\mathrm{~A}}$ |
| Piping \& Valves | RH | X | X |  |
| Piping \& Valves | CC | X | X |  |
| Piping \& Valves | CBS | X | X |  |
| Cabling | RH | X | X |  |

### 13.0 Design Basis Fire

13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |  |
| :---: | :---: | :---: |
| Oil: | 1.75 | Gallons |
| Grease: |  | Pounds |
| Class A: |  | Pounds |
| Charcoal: |  | Pounds |
| Chemicals: |  | Pounds |
| Plastics: | 5 | Pounds |
| Resins: |  | Pounds |
| Other: |  |  |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| 729 | Btu/Sq. Ft. |
| :--- | :--- |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 181 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. | _ Btu/Sq. Ft.

910 Btu/Sq. Ft. 327,500 Btu

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### 14.0 Design-Basis Fire Description

(A) Zones RHR-F-1D-Z, 2B-Z, 3B-Z and 1B-Z constitute one large fire area as they contain open floor hatches and doors.
(B) RH pump ruptures, lube oil spills on floor, covering area of 24 sq . ft .
(C) 1.75 gallons oil ignites and is consumed. In addition, because of high temp. remote location and absence of automatic spray system, entire oil content of RHR-F-2B-Z AND RHR-F-1B-Z will burn (total of 12.5 gallons) with $1,875,000$ Btu as D.B. combustibles.
14.1 DBF Fire Loading

| $\frac{11,719}{2,306}{ }^{\circ}{ }^{\circ} \mathrm{F}$ /u/Sq. Ft. |
| :--- |

14.3 Duration of Fire
$41 / 2$ Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of pump and cabling located in conduit servicing the motor.
15.2 Possible loss of any or all system "a" train components located in RHR-F-1B-Z, RHR-F-1D-Z, RHR-F-2B-Z and RHR-F-3B-Z.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Same as above as fire duration is less than five minutes, fire location is remote from control room, no automatic suppression system exists.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of the Fire Protection System
17.1 Not applicable (automatic suppression system does not exist).

### 18.0 Containing the Design Basis Fire in the Fire Area/Zone

18.1 3-hr. fire barrier between Train " $A$ " and Train " $B$ " equipment and fire duration is less than five minutes, hence fire will be contained within the zones considered.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Safe shutdown can be accomplished with the redundant train equipment located in an area separated by 3-hr. fire barriers.

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Fire Hazard Analysis - RHR-F-2A-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

RHR, Containment Spray, SI Equip. Vault
RHR-F-2A-Z
Safety Injection Pump - 6B
South Side - El. (-) 50'-0" Train B Vault (Vault \#2)
9763-P-805060-FP, 805078-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\frac{\text { Concrete }}{\text { Concrete }}}$ | $\frac{\text { Min. Fire Rating }}{\text { Concrete/Open }}$ <br> 3.2 |
| :--- | :--- | :--- | :--- | :--- |
| Floor |  | $\frac{3 \mathrm{Hr} .}{\text { Concrete }}$ |  |  |
| 3.3 | Ceiling |  | $\frac{\text { Concrete/Grating }}{\text { Concrete/Grating }}$ | $\frac{3 \mathrm{Hr}}{-}$ |
| 3.4 | Doors |  | Metal <br> 3.5 | Others |

4.0 Floor Area 360 Sq. Ft. Length 201' Width $\mathbf{1 8 1}^{\prime}$ Height 15.66’ $^{\prime}$
5.0 Volume $\quad 5,600 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None_ None ___
7.0 Exhaust Ventilation System PAB Exhaust System
7.1 Percentage of System's Capacity $100 \%$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes X

9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
9.2 Airborne
Yes
No
No X
10.0 Fire Protection
10.1 Primary
10.2 Secondary

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
10.3 Detection

Ionization
10.4 Other
------
11.0 Fire Loading in Area
11.1 Refer to Page 2 (analysis continued Pages 2 \& 3)

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| :--- | :---: | :--- |
| Fire Hazard Analysis - RHR-F-2A-Z |  |  |$\quad$| Section F.2 Tab 4 |
| :--- |
| Page 2 of 3 |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |  |
| SI Pump P-6B | SI |  | X | X |  |
| Piping | RC |  | X | X | X |
| Piping \& Valves | CBS |  | X | X | X |
| Piping \& Valves | SI |  | X | X |  |
| Piping \& Valves | CS |  | X | X |  |
| Piping \& Valves | CC |  | X | X | X |
| Piping \& Valves | RH |  | X | X | X |
| Cabling | CBS |  | X | X |  |
| Cabling | RH |  | X | X | X |
| Cabling | SI | X | X | X |  |
| Cabling | CC |  | X | X |  |

### 13.0 Design Base Fire (In Situ)

13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | ---: |
| Oil: | 5.5 Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | $=$ Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | $=$ |
| Other: | $=$ |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area


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14.0 Design-Basis Fire Description
(A) Zones RHR-F-1C-Z, 2A-Z, 3A-Z and 1A-Z constitute one large fire area as they contain open floor hatches and doors.
(B) Safety injection pump ruptures, lube oil spills on floor, covering area of $72 \mathrm{sq} . \mathrm{ft}$.
(C) The entire 5.5 gallons of oil in this zone will burn. In addition, because of high temperature, remote location and absence of automatic spray system, entire oil content of RHR-F-1C-Z and RHR-F-1A-Z will burn (total of 12.5 gallons with 1,875 Btu as D.B. combustibles).
14.1 DBF Fire Loading

| $\frac{11,719}{2,306}$ |  |
| :--- | :--- |
|  |  |
|  |  |
|  |  |

14.3 Duration of Fire
$41 / 2$ Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of pump and cabling located in conduit servicing the motor.
15.2 Possible loss of any or all system "A" Train components located in RHR-F-1A-Z, RHR-F-1C-Z, RHR-F-2A-Z, and RHR-F-3A-Z.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Same as above as fire duration is less than five minutes, fire location is remote from control room, no automatic suppression system exists.

### 17.0 Consequences of Inadvertent or Careless Operation or Rupture of the Fire Protection System

17.1 Not applicable (automatic suppression system does not exist).
18.0 Containing the Design Basis Fire in the Fire Area/Zone
18.1 3-hr. fire barrier between Train "A" and Train "B" equipment and fire duration is less than five minutes, hence fire will be contained within the zones considered.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Safe shutdown can be accomplished with the redundant train equipment located in an area separated by 3-hr. fire barriers.

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Fire Hazard Analysis - RHR-F-2B-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

RHR, Containment Spray, SI Equip. Vault
RHR-F-2B-Z
Safety Injection Pump - 6A
North Side - El. (-) 50'-0" Train A Vault (Vault \#1)
9763-F-805060-FP, 805078-FP
3.0 Construction of Area

4.0 Floor Area 360 Sq. Ft. Length $20^{\prime}$ Width ${ }^{18}$ '_Height $\underline{\text { 15.66’ }}$
5.0 Volume $\quad 5.600 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None_ None_ _ _
7.0 Exhaust Ventilation System PAB Exhaust System
7.1 Percentage of System's Capacity $\quad 100 \%$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes X

9.0 Operational Radioactivity
9.1 Equipment/Piping
 No
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued pages $2 \& 3$ )

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| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| SI Pump P-6A | SI | X |  | X |  |
| Piping | RC | X |  | X | X |
| Piping \& Valves | CBS | X |  | X | X |
| Piping \& Valves | SI | X |  | X |  |
| Piping \& Valves | CS | X |  | X |  |
| Piping \& Valves | CC | X |  | X | X |
| Piping \& Valves | RH | X |  | X | X |
| Cabling | CBS | X |  | X |  |
| Cabling | RH | X |  | X | X |
| Cabling | CS | X | X | X |  |
| Cabling | CC | X |  | X |  |

### 13.0 Design Basis Fire

13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
| Oil: | 5.5 Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | $=$ Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | $\square$ |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| 2.292 | Btu/Sq. Ft. |
| :---: | :---: |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  |  |
| 2,292 | Btu/Sq. Ft. |
| 825,000 | Btu |


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| :--- | :---: | :--- |
| Fire Hazard Analysis - RHR-F-2B-Z |  |  |$\quad$| Section F.2 Tab 4 |
| :--- |
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### 14.0 Design-Basis Fire Description

(A) Zones RHR-F-1D-Z, 2B-Z, 3B-Z and 1B-Z constitute one large fire area as they contain open floor hatches and doors.
(B) Safety injection pump ruptures, lube oil spills on floor, covering area of 72 sq. ft ..
(C) The entire 5.5 gallons of oil in this zone will burn. In addition, because of high temperature, remote location and absence of automatic spray system, entire oil content of RHR-F-1C-Z and RHR-F-1A-Z will burn (total of 12.5 gallons oil with 1,875,000 Btu total D.B. combustibles).
14.1 DBF Fire Loading

| $\frac{11,719}{2,306}{ }^{\circ} \mathrm{Btu} / \mathrm{Fq} . \mathrm{Ft}$. |
| :--- |

14.3 Duration of Fire
$41 / 2$ Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1. Loss of pump and cabling located in conduit servicing the motor.
15.2. Possible loss of any or all system "B" Train components located in RHR-F-1B-Z, RHR-F-1D-Z, RHR-F-2B-Z, and RHR-F-3A-Z.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1. Same as above as fire duration is less than five minutes, fire location is remote from control room, no automatic suppression system exists.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1. Not applicable (automatic suppression system does not exist).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1. 3-hr. fire barrier between Train "A" and Train "B" equipment and fire duration is less than five minutes, hence fire will be contained within the zones considered.
19.0 How is the Redundant Safe Shutdown Equipment in the Area Protected
19.1. Safe shutdown can be accomplished with the redundant train equipment located in an area separated by 3-hr. fire barriers.

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| :--- | :---: | :--- |

Fire Hazard Analysis - RHR-F-3A-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

RHR, Containment Spray, SI Equip. Vault
RHR-F-3A-Z
RHR Heat Exchanger - 9B
South Side El. (-) 31'-10" Train B Vault (Vault \#2)
9763-F-805060, 805078
3.0 Construction of Area

| 3.1 |  |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
|  | Walls | North | Concrete | Outside |
|  |  | South | Concrete | 3 Hr . |
|  |  | East | Concrete | 3 Hr . |
|  |  | West | Concrete/Open | - |
| 3.2 | Floor |  | Concrete/Grating | - |
| 3.3 | Ceiling |  | Concrete/Grating | Outside |
| 3.4 | Doors |  | Metal | $11 / 2 \mathrm{Hr} . /-$ |
| 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area 360 Sq. Ft. Length $20^{\prime}$ Width ${ }^{18}$ '_Height $5^{\prime} 5^{\prime}$
5.0 Volume $\quad 19,800 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None_ None_ ___
7.0 Exhaust Ventilation System PAB Exhaust System
7.1 Percentage of System's Capacity $100 \%$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes X
No X

Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
No
No X
10.0 Fire Protection

Type
10.1 Primary
10.2 Secondary

Fire Extinguisher(s)
Standpipe and Hose Reel
10.3 Detection

Ionization
10.4 Other
-----------
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

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| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Piping and Valves | RH |  | X | X | X |
| Piping and Valves | CC |  | X | X | X |
| RHR Heat Exchanger 9B | RH |  | X | X | X |


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| :--- | :---: | :--- |
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Fire Hazard Analysis - RHR-F-3B-Z

| 1.0 | Building |  |  | RHR, Containment Spray, SI Equip. Vault |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | RHR-F-3B-Z |  |
|  | 2.1 | Area Name |  | RHR Heat Exchanger - 9A |  |
|  | 2.2 | Location |  | North Side El. (-) 31'-10" Train A Vault (Vault \#1) |  |
|  |  | Drawin |  | 9763-F-805060, 805078 |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire |
|  | 3.1 | Walls | North | Concrete | 3 Hr . |
|  |  |  | South | Concrete | 1 Hr . |
|  |  |  | East | Concrete | 3 Hr . |
|  |  |  | West | Concrete/Open | - |
|  | 3.2 | Floor |  | Concrete/Grating | - |
|  | 3.3 | Ceiling |  | Concrete | Outside |
|  | 3.4 | Doors |  | Metal | 11/2 Hr./- |
|  | 3.5 | Others |  | Exposed Ceiling Beams | - |


5.0 Volume $\quad 19,800 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None_ None_ _ _
7.0 Exhaust Ventilation System PAB Exhaust System
7.1 Percentage of System's Capacity $100 \%$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes X
No X

Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
No
No X
10.0 Fire Protection

Type
10.1 Primary
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Standpipe and Hose Reel
10.4 Other

Ionization
-----------
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 8 <br> Station |
| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Piping and Valve | RH | X |  | X | X |
| Piping and Valve | CC | X |  | X | X |
| RHR Heat Exchanger 9A | RH | X |  | X | X |


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| :--- | :---: | :--- |
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Fire Hazard Analysis - RHR-F-4A-Z

| 1.0 | Building |  |  | RHR, Containment Spray, SI Equip. Vault |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | RHR-F-4A-Z |  |
|  | 2.1 | Area Name |  | Stairway \& Manlift Area |  |
|  | 2.2 | Location |  | South, El. (-) 61'-0'' Up to El. 30' -8" |  |
|  |  | Drawing No |  | 9763-F-80 |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. F |
|  | 3.1 | Walls | North | Concrete | 3 Hr . |
|  |  |  | South | Concrete | 3 Hr . |
|  |  |  | East | Concrete | 3 Hr . |
|  |  |  | West | Concrete | 3 Hr . |
|  | 3.2 | Floor |  | Concrete | Outside |
|  | 3.3 | Ceiling |  | Concrete | 3 Hr . |
|  | 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . / 1$ |
|  | 3.5 | Others |  | - | - |


| 4. | Floor Area | 234 Sq. Ft. Length 18' | Width | 13' | Height | 91' |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

5.0 Volume 21,290 Cu. Ft.
6.0 Floor Drains Nuclear X_None_ None ___
7.0 Exhaust Ventilation System PAB Exhaust System
7.1 Percentage of System's Capacity $\quad 100 \%$ - Recirculated
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes

$\qquad$ | No |
| :--- | :--- |
| No |

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ No $\quad \mathrm{X}$
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary

Yes $\qquad$ No X
10.3 Detection

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
10.4 Other

Ionization
-----------
11.0 Fire Loading in Area
11.1 Refer to pages 3 \& 4 (Analysis Continued)

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| :--- | :---: | :--- |
| Section F.2 Tab 4 |  |  |
| Page 2 of 3 |  |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Piping \& Valves | RH |  | X | X | X |
| Piping \& Valves | CBS |  | X | X | X |
| Cabling | CS |  | X | X |  |
| Cabling | RH |  | X | X |  |
| Cabling | CBS |  | X | X |  |
| Local Remote Shutdown Panel | RH |  | X | X | X |

13.0 Design Basis Fire
13.1 Combustibles in Area (In Situ)

| Oil: <br> Grease: <br> Wood | 0.79 gallons |
| :--- | :--- |
| Charcoal: | 142.5 Pounds |
| Pounds |  |
| Chemicals: | Pounds <br> Plastics: <br> Pounds <br> Resins: <br> Other: |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| $\frac{118,800}{}$ | Btu |
| :--- | :--- |
| $1,140,480$ | $"$ |
|  |  |
| 114,796 |  |

### 14.0 Design Basis Fire Description

(a) Oil leaks from both RHR manlift gearboxes onto top of lift cage.
(b) Fire starts and burns wood/oil and subsequently plastic of manlift.
14.1 DBF Fire Loading

5,872 Btu/Sq. Ft.
14.2 Peak Area/ Zone Temp. During Fire $340{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
38.2 Minutes

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| :--- | :---: | :--- |
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15.0 Consequences of Design Basis Fire without Fire Protection
15.1. Refer to Seabrook Station Fire Protection of Safe Shutdown Capability ( 10 CFR 50, App. R).
16.0 Consequences of Design Basis Fire with Fire Protection
16.1. Same as 15.1 , above.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1. Not applicable (No water suppression in area).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1. Early detection from smoke detectors with alarm to control room.
18.2 Fire Brigade hose stream use will reduce fire duration.
18.3 Fire barriers, doors and dampers will limit fire damage to the zone.
19.0 How is Redundant Safe Shutdown Equipment in the Area Protected
19.1. Refer to Seabrook Station Fire Protection of Safe Shutdown Capability (10 CFR 50, App. R).


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| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Piping \& Valves | RH | X |  | X | X |
| Piping \& Valves | CBS | X |  | X | X |
| Cabling | CBS | X |  | X |  |
| Cabling | CC | X |  | X |  |
| Cabling | CS | X |  | X | X |
| Cabling | RH | X |  | X |  |
| Local Remote Shutdown Panel | RH | X |  |  | X |

13.0 Design Basis Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |  |
| :---: | :---: | :---: |
| Oil: | 0.79 | Gallons |
| Grease: |  | Pounds |
| Wood | 142.5 | Pounds |
| Charcoal: |  | Pounds |
| Chemicals: |  | Pounds |
| Plastics: | 7.5 | Pounds |
| Resins: |  | Pounds |
| Other: |  |  |

### 13.2 Total Fire Loading in Area: <br> Total Combustibles:

Fire Loading in Area
118,800 Btu/Sq. Ft. Btu/Sq. Ft.

| $1,140,480$ | Btu/Sq. Ft. |
| :--- | :--- |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 114,796 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

5,872 Btu/Sq. Ft. 1,374,076 Btu

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### 14.0 Design-Basis Fire Description

(a) Oil leaks from both RHR manlift gearboxes onto top of liftcage
(b) Fire starts and burns wood/oil and subsequently plastic of manlift.
14.1 DBF Fire Loading
5,872 Btu/Sq. Ft.
14.2 Peak Area/ Zone Temp. During Fire $340{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire 38.2 Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1. Refer to Seabrook Station Fire Protection of Safe Shutdown Capability (10 CFR 50, App. R).

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1. Same as 15.1 , above.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1. Not applicable (No water suppression in area).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1. Early detection from smoke detectors with alarm to control room.
18.2 Fire Brigade hose stream use will reduce fire duration.
18.3 Fire barriers, doors and dampers will limit fire damage to the zone.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1. Refer to Seabrook Station Fire Protection of Safe Shutdown Capability (10 CFR 50, App. R).

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| :--- | :---: | :--- |

Fire Hazard Analysis - CB-F-1A-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |


3.0 Construction of Area

| 3.1 | Walls |  | Material | Min. F |
| :---: | :---: | :---: | :---: | :---: |
|  |  | North | Concrete | 3 Hr . |
|  |  | South | MCG/Concrete | 3 Hr . |
|  |  | East | Concrete | 3 Hr . |
|  |  | West | MCG/Concrete | 3 Hr . |
| 3.2 | Floor |  | Concrete | 3 Hr . |
| 3.3 | Ceiling |  | Concrete | 3 Hr . |
| 3.4 | Doors |  | Metal | 3 Hr . |
| 3.5 | Others |  | Fireproofed Ce | 3 Hr . |

4.0 Floor Area 2,450 Sq. Ft. Length $58^{\prime}$ Width $42^{\prime}$ Height 27.5'
5.0 Volume $\quad 67,400 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System Switchgear Exhaust
7.1 Percentage of System's Capacity $\quad 100 \%$
8.0 8 Hr. Emergency Lighting in Area Yes X_No No $\qquad$
8.1 Outside Area at Exit Points Yes X No
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Yes
Yes

$$
\begin{aligned}
& \text { No } \frac{X}{\text { No }} \xrightarrow{X} .
\end{aligned}
$$

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
Ionization
Yard Hydrant
11.0 Fire Loading in Area
11.1 Refer to page 4 (analysis continued pages $2-5$ )

* Door C-100 is Not 3 Hr. Fire Rated. Ref. Deviation No. 5, Sbn-904 Dated Dec. 2, 1985.

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| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| 4Kv-SWGR-E5 | EDE | X |  | X |  |
| $\begin{aligned} & \text { 480v-Subst. E51, E52, } \\ & \text { E53 } \end{aligned}$ | EDE | X |  | X |  |
| $\begin{aligned} & \text { 460v-MCC-E512, E515, } \\ & \text { E521, E522, E531, } 231 \end{aligned}$ | EDE | X |  | X |  |
| 120v-AC Distr Pnls | EDE | X |  | X |  |
| $\begin{aligned} & 125 \mathrm{v}-\mathrm{DC} \text { SWGR 11A, } \\ & 11 \mathrm{C} \end{aligned}$ | EDE | X |  | X |  |
| 125v-DC Distr Pnls | EDE | X |  | X |  |
| Battery Chargers BC-1A, $B C-1 C$ | EDE | X |  | X |  |
| Remote Shutdown Panel CP-108A | MM | X |  | X |  |
| Emerg. Pwr. Sequen. CP-79 | DG | X |  | X |  |
| UPS I-1A, I-1C, I-1E | EDE | X |  | X |  |
| Cabling \& Controls | CAH | X |  |  |  |
| Cabling \& Controls | CBA | X |  | X |  |
| Cabling \& Controls | CC | X |  | X |  |
| Cabling \& Controls | CS | X |  | X |  |
| Cabling | DAH | X |  | X | X |
| Cabling | DG | X |  | X | X |


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| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | EAH | X |  | X | X |
| Cabling | EDE | X |  | X | X |
| Cabling | EPA | X |  | X | X |
| Cabling | FW | X |  | X | X |
| Cabling | MS | X |  | X | X |
| Cabling | NI | X |  | X | X |
| Cabling | PAH | X |  | X | X |
| Cabling | RC | X |  | X | X |
| Cabling | RH | X |  | X | X |
| Cabling | SI | X |  | X | X |
| Cabling | SWA | X |  | X | X |
| $125 \mathrm{v}-\mathrm{DC}-$ SWGR 11A | EDE | X |  | X | X |
| Cabling \& Controls | SWA | X |  | X |  |
| Cabling | CAP | X |  | X |  |
| Instruments \& Cabling | CBS | X |  | X |  |
| Cabling \& Controls | CGC | X |  | X |  |
| Cabling | COP | X |  | X |  |
| Cabling | CP | X |  | X |  |
| Cabling | FAH | X |  | X |  |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Appendix A <br> Section F.2 Tab 5 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{\text { System Train }}$ | Safety <br> Related | Required <br> For Safe <br> Shutdown |
| :--- | :--- | :--- | :---: | :---: |
| Cabling | MSD | X | X |  |
| Cabling | NG | X | X |  |
| Cabling | RM | X | X |  |
| Cabling | RMW | X | X |  |
| Cabling | SB | X | X |  |
| Cabling \& Controls | SF | X | X |  |
| Cabling | SS | X | X |  |
| Cabling \& Controls | SW | X | X |  |
| Cabling | VG | X | X |  |
| Cabling | WLD | X | X |  |
| Cabling | SA | X | X |  |
| 460 v-MCC-111, 231 | ED | X | X |  |
| Cabling | CAH | X |  |  |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: |  |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | $=$ Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

Fire Loading in Area

| 62 | Btu/Sq. Ft. |
| :---: | :---: |
|  |  |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 467 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |


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$\begin{array}{llrl}\text { 13.2 } & \text { Total Fire Loading in Area: } & 529 & \text { Btu/Sq. Ft. } \\ \text { Total Combustibles: } & \underline{1,294,000} & \text { Btu }\end{array}$

### 14.0 Design-Basis Fire Description

1. For CB-1-F-1A-A, the entire quantity of oil will be assumed to spill on the floor, as this result in the most limiting fire. In the absence of any curbs or other restrictions, it will spread to a thickness of $1 / 8^{\prime \prime}$ over an area equal to: $1 \mathrm{gal} *\left(\mathrm{ft}^{3} / 7.4805 \mathrm{gal}\right) *(1 / 0.125 \mathrm{in}) *(12 \mathrm{in} / 1 \mathrm{ft})=12.8 \mathrm{ft}^{2}$
2. The ladders are assumed to be not part of the DBF because the plastic will only be assumed to ignite if they meet a temperature of greater than $750^{\circ} \mathrm{F}$.
14.1 DBF Fire Loading
14.2 Peak Zone Temperature Fire
14.3 Duration of Fire
11,719 Btu/Sq. Ft.

Consequences of Design Basis Fire without Fire Protection
15.1 Refer to Seabrook Station Fire Protection Safe Shutdown I Capability (10 CFR 50, Appendix R).
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished with portable extinguishers.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire would be extinguished using hose lines and/or portable extinguishers.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Refer to Seabrook Station Fire Protection Safe Shutdown Capability (10 CFR 50, Appendix R).

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| :--- | :---: | :--- |

Fire Hazard Analysis - CB-F-1B-A

| 1.0 | Building |  |  | Control Building |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | CB-F-1B-A |  |
|  | 2.1 | Area Name |  | Switchgear Room "B" |  |
|  | 2.2 | Location |  | El. 21'-6" |  |
|  |  | Drawing No |  | 9763-F-310431-FP |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire Rating |
|  | 3.1 | Walls | North | MCG/Concrete | 3 Hr . |
|  |  |  | South | Concrete | Outside Wall/3 Hr. |
|  |  |  | East | Concrete | 3 Hr . |
|  |  |  | West | Concrete/MCG | 3 Hr . |
|  | 3.2 | Floor |  | Concrete | 3 Hr . |
|  | 3.3 | Ceiling |  | Concrete | 3 Hr . |
|  | 3.4 | Doors |  | Metal | $3 \mathrm{Hr} / 1^{112} \mathrm{Hr}$.(Stairs) |
|  | 3.5 | Others |  | Fireproofed Ceiling Beams | 3 Hr . |

4.0 Floor Area 2,450 Sq. Ft. Length $58^{\prime}$ Width $42^{\prime} \quad$ Height 27.5'
5.0 Volume $\quad 67,400 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___Non-Nuclear __ None X
7.0 Exhaust Ventilation System Switchgear Exhaust
7.1 Percentage of System's Capacity $\quad 100 \%$
$8.0 \quad 8$ Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points

No $\qquad$
No
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 Refer to page 4

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| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B | Related |  |
| 4kv-Swgr-E6 | EDE |  | X | X |  |
| $\begin{aligned} & 480 \text { v-Subst. E61, E62, } \\ & \text { E63 } \end{aligned}$ | EDE |  | X | X |  |
| $\begin{aligned} & \text { 460v-MCC-E612, E615, } \\ & \text { E621, E622, E631 } \end{aligned}$ | EDE |  | X | X |  |
| 120v-Ac Distr Pnls | EDE |  | X | X |  |
| 125v-DC Swgr 11B, 11D | EDE |  | X | X |  |
| 125v-DC Distr Pnls | EDE |  | X | X |  |
| Battery Chargers BC-1B, $B C-1 D$ | EDE |  | X | X |  |
| Remote Shutdown Panel CP-108b | EDE |  | X | X |  |
| Emerg. Pwr. Sequen. CP-80 | EDE |  | X | X |  |
| UPS I-1B, I-1D, I-1F | EDE |  | X | X |  |
| Cabling \& Controls | CAH |  | X |  |  |
| Cabling \& Controls | CBA |  | X | X |  |
| Cabling \& Controls | CC |  | X | X |  |
| Cabling \& Controls | CS |  | X | X |  |
| 125-DC-SWGR 11B | EDE |  | X | X | X |
| 125v-DC-SWG 11D | EDE |  | X | X | X |
| 120v-AC V Distr. 11F | EDE |  | X | X | X |
| $125 \mathrm{v}-\mathrm{DC}$ Distr. 112B | EDE |  | X | X | X |
| 125v-DC Distr.111D | EDE |  | X | X | X |
| 480-120v Xfmr 31F | EDE |  | X | X | X |
| Aux Relay Panel GN 0 | EDE |  | X | X | X |
| UPS I-1F | EDE |  | X | X | X |


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| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |  |
| Battery Charger BC-1B | EDE |  | X | X | X |
| Battery Charger BC-1D | EDE |  | X | X | X |
| Fuse Box CP-228 | EDE |  | X | X | X |
| Instrumentation \& Cabling | CBS |  | X | X |  |
| Cabling \& Controls | CGC |  | X | X |  |
| Cabling | COP |  | X | X |  |
| Cabling | CP |  | X | X |  |
| Cabling | PAH |  | X | X |  |
| Cabling | MSD |  | X | X |  |
| Cabling | NG |  | X | X |  |
| Cabling | RW |  | X | X |  |
| Cabling | RMW |  | X | X |  |
| Cabling | SB |  | X | X |  |
| Cabling \& Controls | SF |  | X | X |  |
| Cabling | SS |  | X | X |  |
| Cabling \& Controls | SW |  | X | X |  |
| Cabling | VG |  | X | X |  |
| Cabling | WLD |  | X | X |  |
| Cabling | SA |  | X |  |  |
| Msiv, Logic Cabinets CP-183, CP-185 | MS |  | X | X |  |
| Fuse Cabinets | EDE |  | X | X |  |
| Cabling | CAH |  | X | X |  |


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Design-Basis Fire Description

1. For CB-F-1B-A, the combustible content of non IEEE-383 qualified cable (cable dolly) is assumed to burn as this is the most limiting fire. Fire loads in CB-F-1B-A are sufficiently separated that they do not need to be considered in the same design basis fire scenario. As shown on drawing EC285783-C-001, the cable is stored in the east of the CB-F-1B-A, whereas the circuit breaker racking tool is installed in the west side of the room (ref. SKM-07160-1000). The cable burns uniformly across its length (burn area $=\mathrm{dL}=75.8 \mathrm{ft}^{2}$ ). The cable burns over an area of approximately $4 \mathrm{ft}^{2}$, assuming a 2 ft by 2 ft footprint.
2. The ladders are assumed to be not part of the DBF because the plastic will only be assumed to ignite if they meet a temperature of greater than $750^{\circ} \mathrm{F}$.
14.1 DBF Fire Loading
14.2 Peak Zone Temperature Fire
14.3 Duration of Fire
$\xrightarrow{141,750}$ Btu/Sq. Ft.
$678{ }^{\circ} \mathrm{F}$
7.3 Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Refer to Seabrook Station Fire Protection Safe Shutdown I Capability (10 CFR 50, Appendix R).

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| Fire Hazard Analysis - CB-F-1B-A | Page 5 of 5 Tab 5 |  |

16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished with portable extinguishers.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Early warning detectors alarm in the Control Room and alert the Fire Brigade:
18.2 Fire would be limited to cable dolly and the fire extinguished using hose lines and portable extinguishers.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Refer to Seabrook Station Fire Protection Safe Shutdown Capability (10 CFR 50, Appendix R).

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| :--- | :---: | :--- |
| Section F.2 Tab 5 |  |  |
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Fire Hazard Analysis - CB-F-1D-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Control Building

CB-F-1D-A
Battery Room "A"
El. 21'-6"
9763-F-310431-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 330 Sq. Ft. Length $\quad 22^{\prime}$ Width ${ }^{151^{\prime} \quad \text { Height }{ }^{9.5 \prime}}$
5.0 Volume 3,100 Cu. Ft.
6.0 Floor Drains Nuclear___ Non-Nuclear X_None__
7.0 Exhaust Ventilation System Battery Room Exhaust
7.1 Percentage of System's Capacity $\underline{100 \%}$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes No X
8.1 Outside Area at Exit Points

Yes

No X
No
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No X |
| :--- |
| No X |

10.0 Fire Protection

Yes $\qquad$
Type
10.1 Primary

Fire Extinguisher(s)
10.2 Secondary

Standpipe and Hose Reel
10.3 Detection

Ionization
------
11.0 Fire Loading in Area
11.1 Refer to page 3. (analysis continued pages 2 \& 3)

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| :--- | :---: | :--- |

### 12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Battery A | EDE | X |  | X |
| Cabling | EDE | X |  | X |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

Fire Loading in Area

| Oil: | Gallons |
| :--- | :--- |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | $=$ Pounds |
| Chemicals: | $=$ Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: | $=$ |

13.2 Total Fire Loading in Area:

Total Combustibles:
$\begin{array}{ll}46,069 & \text { Btu/Sq. Ft. } \\ 15,202,766 & \text { Btu }\end{array}$

### 14.0 Design-Basis Fire Description

(A) All of the plastic battery jars and covers would be engulfed in a fire.
(b) The electrolyte was not added to the jars as they were dry and subject to being burned.
(c) Fire burns without ventilation air as supply and exhaust air duct fire dampers isolate the subject battery room.
14.1 DBF Fire Loading

1,464 Btu/Sq. Ft.
14.2 Peak Temperature
$690{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
$41 / 2$ Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of battery use due to jar destruction.
15.2 Safe shutdown can be accomplished with use of the redundant battery train.

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| Fire Hazard Analysis - CB-F-1D-A | Page 3 of 3 Tab 5 |  |

16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of battery use due to jar destruction.
16.2 Safe shutdown can be accomplished with use of the redundant battery train.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Duration of the fire is short, therefore the 3 hour partitions will prevent the spread to adjacent areas.
18.2 Fire dampers will prevent the spread of fire from the area.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Not applicable.

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Fire Hazard Analysis - CB-F-1E-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |


| Control Building |
| :--- |
| CB-F-1E-A |
| Battery Room "C" |
| El. 21'-6" |
| $9763-\mathrm{F}-310431-\mathrm{FP}$ |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 330 Sq. Ft. Length $\quad 22^{\prime}$ Width $\underbrace{15^{\prime} \quad \text { Height } 9.5^{\prime}}$
5.0 Volume $\quad 3,100 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X_None__
7.0 Exhaust Ventilation System Battery Room Exhaust
7.1 Percentage of System's Capacity $\underline{100 \%}$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes $\quad$ No $\quad \mathrm{X}$
8.1 Outside Area at Exit Points Yes X
No X
No
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No X |
| :--- |
| No |

10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued pages $2 \& 3$ )

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| :--- | :---: | :--- |
| Fire Hazard Analysis - CB-F-1E-A |  |  |$\quad$| Section F.2 Tab 5 |
| :--- |
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### 12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Battery C | EDE | X |  | X |
| Cabling | EDE | X |  | X |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: |  |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | $=$ Pounds |
| Charcoal: | Pounds |
| Chemicals: | $=$ Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

### 14.0 Design-Basis Fire Description

(A) All of the plastic battery jars and covers would be engulfed in a fire.
(B) The electrolyte was not added to the jars as they were dry and subject to being burned.
(C) Fire burns without ventilation air as supply and exhaust air duct fire dampers isolate the subject battery room.
14.1 DBF Fire Loading
$1,464 \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft}$.
14.2 Peak Zone Temperature Fire
$690{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
$41 / 2$ Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of battery use due to jar destruction.
15.2 Safe shutdown can be accomplished with use of the redundant battery train.

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| Fire Hazard Analysis - CB-F-1E-A |  |  |$\quad$| Page 3 of 3 Tab 5 |
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16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of battery use due to jar destruction.
16.2 Safe shutdown can be accomplished with use of the redundant battery train.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Duration of the fire is short, therefore the 3 hour partitions will prevent the spread to adjacent areas.
18.2 Fire dampers will prevent the spread of fire from the area.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Not applicable.

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Fire Hazard Analysis - CB-F-1F-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |


| Control Building |
| :--- |
| CB-F-1F-A |
| Battery Room "B" |
| El. 21'-6" |
| 9763-F-310431-FP |

3.0 Construction of Area

4.0 Floor Area $\quad 300$ Sq. Ft. Length $\quad 22^{\prime}$ Width $\underbrace{15^{\prime} \quad \text { Height } \quad 9.5^{\prime}}$
5.0 Volume 3,100 Cu. Ft.
6.0 Floor Drains Nuclear__Non-Nuclear X_None__
7.0 Exhaust Ventilation System Battery Room Exhaust
7.1 Percentage of System's Capacity $\underline{100 \%}$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes No X
8.1 Outside Area at Exit Points

Yes

No X
No
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No X |
| :--- |
| No X |

10.0 Fire Protection

Yes $\qquad$
Type
10.1 Primary

Fire Extinguisher(s)
10.2 Secondary

Standpipe and Hose Reel
10.3 Detection

Ionization
------
11.0 Fire Loading in Area
11.1 Refer to page 2. (analysis continued pages 2 \& 3)

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### 12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ | System Train |  | Safety <br> Battery B |
| :--- | :--- | :--- | :--- | :---: |
|  | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |  |
| Cabling | EDE |  | X | X |
|  | EDE |  | X | X |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

Fire Loading in Area

| Oil: | Gallons |
| :--- | :--- |
| Grease: | Pounds |
| Class A: | $=$ Pounds |
| Charcoal: | $=$ Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: | $=$ |


|  | Btu/Sq. Ft. |
| :---: | :---: |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 46,069 | $\mathrm{Btu} / \mathrm{Sq}$. Ft. |
|  | Btu/Sq. Ft. |

13.2 Total Fire Loading in Area:
$\begin{aligned} 46,069 & \text { Btu/Sq. Ft. } \\ 15,202,766 & \text { Btu }\end{aligned}$

### 14.0 Design-Basis Fire Description

(a) All of the plastic battery jars and covers would be engulfed in a fire.
(b) The electrolyte was not added to the jars as they were dry and subject to being burned.
(c) Fire burns without ventilation air as supply and exhaust air duct fire dampers isolate the subject battery room.
14.1 DBF Fire Loading

1,464 Btu/Sq. Ft.
14.2 Peak Zone Temperature Fire
$690{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
$41 / 2$ Minutes

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| :--- | :---: | :--- |

15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of battery use due to jar destruction.
15.2 Safe shutdown can be accomplished with use of the redundant battery train.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of battery use due to jar destruction.
16.2 Safe shutdown can be accomplished with use of the redundant battery train.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Duration of the fire is short, therefore the 3 hour partitions will prevent the spread to adjacent areas.
18.2 Fire dampers will prevent the spread of fire from the area.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Not applicable.

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Fire Hazard Analysis - CB-F-1G-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Control Building
CB-F-1G-A
Battery Room "D"
El. 21'-6"
9763-F-310431-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete }}{\text { Concrete }}$ |
| :--- | :--- | :--- | :--- |
| 3.2 | Floor |  | $\frac{\text { Concrete }}{\text { Concrete }}$ |
| 3.3 | Ceiling |  | $\frac{\text { Concrete }}{\text { Metal }}$ |
| 3.4 | Doors |  |  |
| 3.5 | Others |  |  |


$\frac{\frac{\text { Min. Fire Rating }}{3 \mathrm{Hr} .}}{\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}}$| $\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}$ |
| :--- |
| $\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}$ |

4.0 Floor Area 330 Sq. Ft. Length $22^{\prime}$ Width ${ }^{151^{\prime} \text { Height } 9.5^{\prime}}$
5.0 Volume $\quad 3,100 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear
7.0 Exhaust Ventilation System
7.1 Percentage of System's Capacity $\quad 100 \%$
8.0 8 Hr . Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes X
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Yes $\qquad$
No X

Yes $\qquad$
No X
No

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
Ionization
------
11.0 Fire Loading in Area
11.1 Refer to page 2. (analysis continued pages 2 \& 3)

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| :--- | :---: | :--- |
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### 12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ |  | System Train |  |
| :--- | :--- | :--- | :--- | :---: | | Safety |
| :---: |
| Battery D |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: |  |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | $=$ Pounds |
| Charcoal: | Pounds |
| Chemicals: | $=$ Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

### 14.0 Design-Basis Fire Description

(A) All of the plastic battery jars and covers would be engulfed in a fire.
(B) The electrolyte was not added to the jars as they were dry and subject to being burned.
(C) Fire burns without ventilation air as supply and exhaust air duct fire dampers isolate the subject battery room.
14.1 DBF Fire Loading
$1,464 \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft}$.
14.2 Peak Zone Temperature Fire
$690{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
$41 / 2$ Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of battery use due to jar destruction.
15.2 Safe shutdown can be accomplished with use of the redundant battery train.

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16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of battery use due to jar destruction.
16.2 Safe shutdown can be accomplished with use of the redundant battery train.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Duration of the fire is short, therefore the 3 hour partitions will prevent the spread to adjacent areas.
18.2 Fire dampers will prevent the spread of fire from the area.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Not applicable.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 8 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 5 |  |  |
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Fire Hazard Analysis - CB-F-2A-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Control Building
CB-F-2A-A
Cable Spreading Room
El. 50'-0"
9763-F-310452-FP, 310461-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete }}{\text { Concrete }}$ <br> 3.2 |
| :--- | :--- | :--- | :--- |
| Metal   <br> 3.3 Floor  <br> 3.4 Ceiling  <br> Doors  $\frac{\text { Concrete }}{\text { Concrete }}$ |  |  |  |


| $\frac{\text { Min. Fire Rating }}{3 \mathrm{Hr} . / O u t s i d e ~ W a l l ~}$ |
| :--- |
| $\frac{3 \mathrm{Hr} . / \text { Outside Wall }}{}$ |
| $\frac{\text { Outside Wall }}{3 \mathrm{Hr} .}$ |
| $\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}$ |
| $\frac{11 / 2 \mathrm{Hr} .(\text { Stairs }) /}{3 \mathrm{Hrs} . \text { Others }}$ |
| $\frac{3 \mathrm{Hr} .}{}$ |

4.0 Floor Area 9,200 Sq. Ft. Length $107^{\prime}$ Width $86^{\prime}$ Height $23^{\prime}$
5.0 Volume $\quad 211,600 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X None ___
7.0 Exhaust Ventilation System Cable Spreading Room Exhaust
7.1 Percentage of System's Capacity $100 \%$
$\begin{array}{lllll}8.0 & 8 \mathrm{Hr} \text {. Emergency Lighting in Area } & \text { Yes } & & \text { No } \quad \text { X } \\ & \text { 8.1 } & \text { Outside Area at Exit Points } & \text { Yes } & \mathrm{X}\end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes
9.2 Airborne
Yes $\qquad$
$\stackrel{\text { No }}{\text { No }}$
10.0 Fire Protection
10.1 Primary

Type
Deluge Systems
Fire Extinguisher(s)
Ionization/Thermal
Standpipe and Hose Reel
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 8 <br> Station |
| :--- | :---: | :--- |
| Appendix A |  |  |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | CS | X | X | X |  |
| Cabling | SI | X | X | X |  |
| Cabling | EAH | X | X | X |  |
| Cabling | PAH | X | X | X |  |
| Cabling | RC | X | X | X |  |
| Cabling | SB | X | X | X |  |
| Cabling | SW | X | X | X |  |
| Cabling | RH | X | X | X |  |
| Cabling | DG | X | X | X |  |
| Cabling | EDE | X | X | X |  |
| Cabling | NI | X | X | X |  |
| Cabling | EPA | X | X | X |  |
| Cabling | FW | X | X | X |  |
| Cabling | SWA | X | X | X |  |
| Cabling | CAH | X | X | X |  |
| Cabling | MS | X | X | X |  |
| Cabling | RMW |  | X | X |  |
| Cabling | SB | X | X | X |  |
| Cabling | SF | X | X | X |  |


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12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Related | Required <br> For Safe |
| :--- | :--- | :--- | :--- | :---: | :---: |
| Equipment | $\underline{\text { Shstem }}$ |  |  |  |  |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A |
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| Section F.2 Tab 5 |  |  |
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Fire Hazard Analysis - CB-F-2B-A

| 1.0 | Building |  |  | Control Building |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | CB-F-2B-A |  |
|  | 2.1 | Area Name |  | Mechanical Room - North |  |
|  | 2.2 | Location |  | El. 50'-0' |  |
|  |  | Drawing No |  | 9763-F-310452-FP, 310461-FP |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire Rating |
|  | 3.1 | Walls | North | Concrete | Outside Wall |
|  |  |  | South | Metal | 3 Hr . |
|  |  |  | East | Metal | 3 Hr . |
|  |  |  | West | Concrete | 3 Hr . |
|  | 3.2 | Floor |  | Concrete | 3 Hr . |
|  | 3.3 | Ceiling |  | Concrete | 3 Hr . |
|  | 3.4 | Doors |  | Metal | 3 Hr . |
|  | 3.5 | Others |  | Fireproofed Ceiling Beams | 3 Hr . |

4.0 Floor Area $\quad$ 1,120 Sq. Ft. Length $26^{\prime}$ Width $\quad 43^{\prime}$ Height $23^{\prime}$
5.0 Volume $\quad 25,800 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X_None__
7.0 Exhaust Ventilation System Uses air from diesel generator building
7.1 Percentage of System's Capacity 100\%
8.0 8 Hr . Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes X
No X
No
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No X X |
| :--- |

10.0 Fire Protection
10.1 Primary
10.2 Secondary

Yes $\qquad$
Type
Fire Extinguisher(s)
Standpipe and Hose Reel
10.3 Detection

Ionization
10.4 Other
-----------
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A <br> Section F.2 Tab 5 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{l}$ System Train | Safety <br> Related |  |
| :--- | :--- | :--- | ---: | :---: |
| Fan-FN-19 | CBA | X | $\underline{\mathrm{B}}$ | $\underline{\mathrm{X}}$ |
| Fan-FN-21A | CBA | X | X |  |
| Damper DP-21A | CBA | X | X |  |
| Pressure Switches | CBA | X | X |  |
| Cabling | CBA | X | X |  |
| Fan-FN-20 | CBA | X | X |  |
| Dampers DP-24A, 24B, | CBA | X | X |  |
| 24 C |  | X |  |  |
| Cabling | EDE | X |  |  |


| SEABROOK | Evaluation and Comparison to | Rev .6 |
| :--- | :---: | :--- |
| STATION | BTP APCSB 9.5-1, Appendix A | Table 5 |
|  | Fire Hazard Analysis - CB-F-2C-A | Page 1 of 2 |

Fire Hazard Analysis - CB-F-2C-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Control Building
CB-F-2C-A
Mechanical Room - South
El. 50'-0"
9763-F-310452-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Metal }}$ | $\frac{\text { Min. Fire Rating }}{\text { Metal }}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area $\quad$ 1,120 Sq. Ft. Length $26^{\prime}$ Width $\quad 43^{\prime}$ Height $23^{\prime}$
5.0 Volume $\quad 25,800 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X_None__
7.0 Exhaust Ventilation System Uses air from diesel generator building
7.1 Percentage of System's Capacity $\quad 100 \%$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes X

No X
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection

Yes $\qquad$
No X
No X

Yes
10.4 Other

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
Ionization
-----------
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

| SEABROOK | Evaluation and Comparison to | Rev .6 |
| :--- | :---: | :--- |
| STATION | BTP APCSB 9.5-1, Appendix A | Table 5 |
|  | Fire Hazard Analysis - CB-F-2C-A | Page 2 of 2 |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety <br> Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |  |
| Fan-FN-32 | CBA |  | X | X | X |
| Fan-FN-33 | CBA |  | X | X | X |
| Fan-FN-21B | CBA |  | X | X | X |
| Pressure Switches | CBA |  | X | X | X |
| Dampers DP-21B | CBA |  | X | X | X |
| Cabling | CBA |  | X | X | X |




| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> STATION |
| :--- | :---: | :--- | | Appendix A |
| :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B | Related |  |
| Relay Rack CP-9 | NI | X |  | X |  |
| Relay Rack CP-10 | NI |  | X | X |  |
| Cabinet CP-152A |  | X |  | X |  |
| Cabinet CP-152B |  |  | X | X |  |
| Cabinet CP-12 |  | X |  | X |  |
| Cabinet CP-13 |  |  | X | X |  |
| Instruments And Controls On Main Control Board And Other | SI | X | X | X |  |
|  | RH | X | X | X |  |
| Cabinets And their Associated Cabling | CC | X | X | X |  |
|  | DG | X | X | X |  |
|  | SW | X | X | X |  |
|  | CS | X | X | X |  |
|  | RM | X | X | X |  |
|  | FW | X | X | X |  |
|  | MS | X | X | X |  |
|  | EPA | X | X | X |  |
|  | CAH | X | X | X |  |
|  | SWA | X | X | X |  |
|  | EAH | X | X | X |  |
|  | SB | X | X | X |  |
|  | NI | X | X | X |  |
|  | RC | X | X | X |  |
|  | ED | X | X | X |  |
|  | EDE | X | X | X |  |


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| :--- | :---: | :--- |
| Appendix A | Section F.2 Tab 5 <br> Page 4 of 5 |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Process Prot |  |  |  |  |  |
| CP-L, 2, 3, 4 |  | X | X | X |  |
| Test Cabinets CP-14, 15 |  | X | X | X |  |
| BOP Process Control |  | X | X | X |  |
| Cabinets CP-297A, 297B |  |  |  |  |  |
| Isolation Cabinet CP-470 |  | X | X | X |  |
| BOP Process Control |  | X |  |  |  |
| Cabinet |  |  |  |  |  |
| RVLIS/HELB Cabinet |  | X | X | X |  |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Fire Loading in Area |  |
| :--- | :--- |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 17,711 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| $8,230^{\text {Notel }}$ | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |


| 13.2 | Total Fire Loading in Area: | 25,941 | Btu/Sq. Ft. |
| :--- | :--- | ---: | :--- |
| Total Combustibles: | $181,198,000^{\text {Notel }}$ | Btu |  |

### 14.0 Design-Basis Fire Description

(A) Fire starts in a waste basket in an office
(B) Fire spreads to desk and files within office.

Note 1: Value has been rounded up to the nearest thousands place.

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| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - CB-F-3A-A | Page 5 of 5 Tab 5 |

(C) Fire spreads across glass and metal partitions and consumes one half of the office area.
(D) Hot exhaust air from the affected area is transferred to the return air plenum which in turn will close the R.A. fire damper. In short period of time, the heat transfer thru the supply air ductwork into the return air plenum will close the supply air fire damper at which time ventilation is lost.
14.1 DBF Fire Loading $\quad 7,196$ Btu/Sq. Ft.
14.2 Peak Temperature
$690{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
8.1 Min.

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 The entire control room including the computer area could be rendered uninhabitable due to the smoke.
15.2 Safe shutdown can be accomplished from outside the control room.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 The area contains ionization detectors and in addition is occupied 24 hours per day, therefore the fire will be detected early.
16.2 The use of portable fire extinguishers and hose reels, if necessary, will extinguish the fire before it spreads.
16.3 Damage will be limited to the area where the fire occurs.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable (no water suppression in area).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Early detection due to ionization detection and occupation of space.
18.2 Prompt use of fire extinguishers.
18.3 Three hour fire barrier.
18.4 Major portion of combustibles are contained within steel metal filing cabinets.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Not applicable (See 15.2).

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| :--- | :---: | :--- |
| Fection F.2 Tab 5 |  |  |
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Fire Hazard Analysis - CB-F-3B-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Control Building

CB-F-3B-A
HVAC Equipment \& Duct Area
2.1 Area Name
$\frac{\text { South West El. 75'-0" }}{\text { 9763-F-500090-FP }}$
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East | $\frac{\text { Material }}{\text { MCG }}$ | $\frac{\text { Min. Fire Rating }}{\text { Concrete }}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 1,330 Sq. Ft. Length 26' Width $\int^{51^{\prime} \quad \text { Height } 21^{\prime}}$
5.0 Volume 27,930 Cu. Ft.
6.0 Floor Drains Nuclear ___Non-Nuclear ___ None X
7.0 Exhaust Ventilation System Return air - no exhaust
7.1 Percentage of System's Capacity $\qquad$
8.08 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points

No $\qquad$
No
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No |
| :--- |
| No |

9.2 Airborne

Yes $\qquad$

$$
\text { No } \quad \mathrm{X}
$$

10.0 Fire Protection

Type
10.1 Primary

Fire Extinguisher(s)
10.2 Secondary

Standpipe and Hose Reel
10.3 Detection

Ionization
10.4 Other

Carbon Monoxide Detector in CBA-F-38, -8038
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> STATION |
| :--- | :---: | :--- |
| Appendix A | Section F.2 Tab 5 <br> Page 2 of 2 |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |
| No Equipment Required For Safe Shutdown in This Area |  |  |  |  |
| Air Conditioning AC-3A\&B | CBA | X | X | X |
| Dampers 26A\&B | CBA | X | X | X |
| Dampers 27A\&B | CBA | X | X | X |
| Damper 52 | CBA | X | X | X |
| Cabling | CBA | X | X | X |
| Fans 16A \& B | CBA | X | X | X |
| Fans F-38 | CBA | X |  | X |
| Filter F-8038 | CBA |  | X | X |
| Damper 28 | CBA | X |  | X |
| Damper 1058 | CBA |  | X | X |


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Fire Hazard Analysis - CB-F-3C-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Control Building

CB-F-3C-A
Computer Room
2.1 Area Name

Drawing No

| El. 75'-0" |
| :--- |
| $9763-\mathrm{P}-500090-\mathrm{FP}$ |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\text { MCG }}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area $\quad$ 1,288 Sq. Ft. Length $46^{\prime}$ Width $28^{\prime}$ Height $21^{\prime}$
5.0 Volume 27,050 Cu. Ft.
6.0 Floor Drains Nuclear $\qquad$ Non-Nuclear $\qquad$ None X
7.0 Exhaust Ventilation System Control Room Complex Exhaust
7.1 Percentage of System's Capacity $\quad 100 \%$
8.0 8 Hr . Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points

Yes

No X
No
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne

Yes $\qquad$
Yes $\qquad$
10.0 Fire ProtectionType
10.1 Primary

Halon Fixed Gas Extinguishing System
10.2 Secondary
10.3 Detection
10.4 Outsid Fire Area

Fire Extinguisher(s)
Ionization (Monitored Temp. Indication)
Standpipe and Hose Reel
11.0 Fire Loading in Area
11.1 Refer to Page 2. (analysis continued pages. 2 \& 3)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 14 <br> Station |
| :--- | :---: | :--- |
| Appendix A |  |  |
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### 12.0 Equipment and Systems in Fire Area/Zone

|  |  |  |  | Safety | Required For Safe |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equipment | System | A | B | Related | Shutdown |

No Equipment Required For Safe Shutdown in This Area
Also No Safety Related Equipment in This Area
13.0 Design Base Fire
13.1 Combustible in Area (In Situ) Fire Loading in Area

| Oil: | Gallons |
| :--- | :--- |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | 2,250 |
| Pounds |  |
| Resins: | Pounds |
| Other: |  |


|  | Btu/Sq. Ft. |
| :---: | :---: |
|  | Btu/Sq. Ft. |
| 2,609 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 22,710 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

Total Fire Loading in Area:
Total Combustibles:
$\frac{25,319}{32,6 t u / S q . ~ F t . ~}$
$\overline{32,610,000}$ Btu

### 14.0 Design-Basis Fire Description

(A) Fire starts in a waste basket in an office.
(B) Fire spreads to desk and files within office.
(C) Fire spreads across glass and metal partitions and consumes one half of the office area.
(D) Indoor air conditioning unit shuts off on high ambient temperature. The exhaust air path is normally closed and no supply air is provided from the outside, therefore the ventilation is lost.
14.1 DBF Fire Loading


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| :--- | :---: | :--- |
| Appendix A |  |  |$\quad$| Section F.2 Tab 5 |
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15.0 Consequences of Design Basis Fire without Fire Protection
15.1 The entire computer room could be rendered uninhabitable due to smoke.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 The area is protected by a Halon 1301 Fixed Gas Extinguishing System and early warning ionization detectors, therefore the fire will be detected early.
16.2 The use of portable fire extinguishers and hose reels are available for backup.
16.3 Damage will be limited to the area where fire occurs.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 The area is not required for safe shutdown purpose and can be evacuated with no effect on operation of the control room.
17.2 The expended halon and/or products of combustion can be exhausted from the area by manual switch over to the control room complex exhaust system.

### 18.0 Containing Design Basis Fire in the Fire Area/Zone

18.1 Early detection due to ionization detection.
18.2 Prompt total flooding of the area by the Halon 1301 Fixed Gas Extinguishing System.
18.3 Pressurization of the adjacent control room prevents exfiltration from the area.
18.4 Major portion of combustibles are contained within steel metal filing cabinets.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Not applicable

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Section F.2 Tab 5 <br> Appendix A |
| :--- | :---: | :--- |

Fire Hazard Analysis - CB-F-S1-0

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

> Control Building

CB-F-S1-0
Stairwell

| $\overline{\text { Col. E-4 }}$ |
| :--- |
| $9763-\mathrm{F}-310431-\mathrm{FP}$ |

3.0 Construction of Area

4.0 Floor Area 150 Sq. Ft. Length $18^{\prime}$ Width $8^{\prime}-44^{\prime \prime}$ Height $122^{\prime}$
5.0 Volume $\quad 18,075 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear __ None __
7.0 Exhaust Ventilation System None
7.1 Percentage of System's Capacity N/A
8.0 8 Hr. Emergency Lighting in Area Yes X No
8.1 Outside Area at Exit Points Yes X
$\qquad$
No
$\begin{array}{ll}9.0 & \text { Operational Radioactivity } \\ & 9.1 \quad \text { Equipment/Piping }\end{array}$
$\begin{array}{ll}9.0 & \text { Operational Radioactivity } \\ & 9.1 \quad \text { Equipment/Piping }\end{array}$

Yes $\qquad$ No | X |
| :--- |
| No |${ }^{\mathrm{X}}$

10.0 Fire Protection

Yes $\qquad$
Type
10.1 Primary

Portable Extinguisher(s)
10.2 Secondary

Hose Station
10.3 Detection

None
10.4 Other
------
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Section F.2 Tab 5 <br> Page 2 of 2 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  |  |  | Safety | Required For Safe |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equipment | System | A | B | Related | Shutdown |

No Equipment Required For Safe Shutdown in This Area

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 5 |  |  |
| Page 1 of 2 |  |  |

Fire Hazard Analysis - CB-F-S2-0

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Control Building
CB-F-S2-0
Stairwell

| $\overline{\text { Col. B-1 }}$ |
| :--- |
| $9763-\mathrm{F}-310431-\mathrm{FP}$ |

3.0 Construction of Area

4.0 Floor Area 226 Sq. Ft. Length $22^{\prime}$ Width $10^{\prime}-4{ }^{\prime \prime}$ Height $\int^{50^{\prime}}$
5.0 Volume $\quad 11,330 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear __ None ___
7.0 Exhaust Ventilation System None
7.1 Percentage of System's Capacity N/A

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No |
| :--- |
| No |

10.0 Fire Protection

Yes $\qquad$
Type
10.1 Primary

Portable Extinguisher(s)
Hose Station
None
------
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Section F.2 Tab 5 <br> Page 2 of 2 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  |  |  | Safety | Required <br> For Safe |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equipment | System | A | B | Related | Shutdown |

No Equipment Required For Safe Shutdown in This Area

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 12 <br> Appendix A <br> Section F.2 Tab 6 <br> Page 1 of 3 |
| :--- | :---: | :--- |

Fire Hazard Analysis - ET-F-1A-A
1.0 Building
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location

Drawing No
Electrical Tunnel
ET-F-1A-A
Upper Electrical Tunnel - Train "A" *
El. 0'-0"
9763-F-310453-FP, 310465-FP, 310466-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |


5.0 Volume 53,400 Cu. Ft.
6.0 Floor Drains Nuclear ___ Non-Nuclear X None__
7.0 Exhaust Ventilation System None
7.1 Percentage of System's Capacity _-
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area
8.1 Outside Area at Exit Points
Yes
Yes

$$
\begin{aligned}
& \text { No } \mathrm{X} \\
& \text { No } \\
& \hline
\end{aligned}
$$

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No X |
| :--- |
| No X |

10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection

Yes $\qquad$
Type
Pre-Action System
Fire Extinguisher(s)
Ionization/Photoelectric
10.4 Other
--------
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

[^3]| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 12 <br> Appendix A <br> Section F.2 Tab 6 <br> Page 2 of 3 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | CAH | X |  | X | X |
| Cabling | CC | X |  | X | X |
| Cabling | EDE | X |  | X | X |
| Cabling | EPA | X |  | X | X |
| Cabling | FW | X |  | X | X |
| Cabling | MS | X |  | X | X |
| Cabling | NI | X |  | X | X |
| Cabling | RC | X |  | X | X |
| Cabling | SW | X |  | X | X |
| Cabling | SWA | X |  | X | X |
| Cabling | SI | X |  | X |  |
| Elect. Penetration | EDE | X |  | X | X |
| Dist. Panel PP-6A, C, D, E | RC | X |  | X | X |
| Dist Panel PP-8J | ED | X |  |  | X |
| Cabling | CBS | X |  | X |  |
| Cabling | CAP | X |  | X |  |
| Cabling | RM | X |  | X |  |
| Cabling | SS | X |  | X |  |
| Cabling | NG | X |  | X |  |
| Cabling | SA | X |  |  |  |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 12 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 6 |  |  |
| Page 3 of 3 |  |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{\text { System Train }}$ | Safety <br> Related | Required <br> For Safe |  |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Cabling | IA | X | $\underline{B}$ |  |  |
| Cabling | SB | X | X |  |  |
| Rad Mon | RM | X | X |  |  |
| Cabling | CS | X | X |  |  |
| Fuse Cabinets | EDE | X | X |  |  |
| Cabling | IC | X | X |  |  |
| Transformer ED-X-14J | ED | X |  |  |  |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 12 |
| :--- | :---: | :--- |
| Appendix A |  |  |$\quad$| Section F.2 Tab 6 |
| :--- |
| Page 1 of 2 |

Fire Hazard Analysis - ET-F-1B-A
1.0 Building
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location

Drawing No
Fire Hazard Analysis - ET-F-1B-A

| 2.0 | Fire Name |
| :--- | :--- |
| 2.1 | Area None |
| 2.2 | Location |
|  |  |
|  | Drawing No |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 1,470 Sq. Ft. Length Varies Width Varies Height Varies
5.0 Volume $\quad 33,300 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear ___ Non-Nuclear X None ___
7.0 Exhaust Ventilation System Electric Cable Tunnel Exhaust
7.1 Percentage of System's Capacity $\quad 100 \%$
8.08 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points
Yes
Yes
No X
No $\qquad$
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Yes $\qquad$ | No Xo X |
| :--- |

Type
Pre-Action System
Fire Extinguisher(s)
Ionization/Photoelectric
------
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)
\(\left.$$
\begin{array}{|l|c|l|}\hline \begin{array}{l}\text { SEABROOK } \\
\text { Station }\end{array} & \text { Evaluation and Comparison to BTP APCSB 9.5-1, } \\
\text { Appendix A }\end{array}
$$ \quad \begin{array}{l}Rev. 12 <br>
Section F.2 Tab 6 <br>

Page 2 of 2\end{array}\right]\)| Fire Hazard Analysis -ET-F-1B-A |
| :--- |

12.0 Equipment and Systems in Fire Araa/Zone

| Equipment | System | System Train |  | Safety <br> Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | CAH | X |  | X | X |
| Cabling | CC | X |  | X | X |
| Cabling | EDE | X |  | X | X |
| Cabling | EPA | X |  | x | X |
| Cabling | FW | X |  | X | X |
| Cabling | MS | X |  | X | X |
| Cabling | NI | X |  | X | X |
| Cabling | RC | X |  | X | X |
| Cabling | SW | X |  | X | X |
| Cabling | SB | X |  | X | X |
| Cabling | SWA | X |  | X | X |
| Cabling | SI | X |  | X |  |
| Cabling | CAP | X |  | X |  |
| Cabling | RM | X |  | X |  |
| Cabling | SS | X |  | X |  |
| Cabling | NG | X |  | X |  |
| Cabling | SA | X |  |  |  |
| Cabling | IA | X |  |  |  |
| Cabling | IC | X |  | X |  |

\(\left.$$
\begin{array}{|l|c|l|}\hline \text { SEABROOK } & \text { Evaluation and Comparison to BTP APCSB 9.5-1, } & \begin{array}{l}\text { Rev. 12 } \\
\text { STATION }\end{array}
$$ <br>
Appendix A <br>

Page 1 F. 2 Tab 6\end{array}\right]\)| Fire Hazard Analysis - ET-F-1C-A |
| :--- |

Fire Hazard Analysis - ET-F-1C-A
1.0 Building
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location

Drawing No
Electrical Tunnel
ET-F-1C-A
Lower Electrical Tunnel - Train "B" *
North of Containment El (-) 26' $-0^{\prime \prime}$
9763-F-310454-FP
3.0 Construction of Area

|  |  |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Concrete | Outside |
|  |  | South | Concrete | 3 Hr . |
|  |  | East | Concrete | 3 Hr . |
|  |  | West | Concrete | 3 Hr . |
| 3.2 | Floor |  | Concrete | Outside |
| 3.3 | Ceiling |  | Concrete | 3 Hr . |
| 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . / 1^{1 / 2} \mathrm{Hr}$. (Stairs) |
| 3.5 | Others |  | Concrete |  |


5.0 Volume $\quad 53,400 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X None ___
7.0 Exhaust Ventilation System
7.1 Percentage of System's Capacity
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points

$\qquad$
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 Refer to Page 3.

[^4]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 12 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |$\quad$| Section F.2 Tab 6 |
| :--- |
| Page 2 of 4 |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B | Related |  |
| Cabling | CAH |  | X | X |  |
| Cabling | CC |  | X | X |  |
| Cabling | EDE |  | X | X |  |
| Cabling | EPA |  | X | X |  |
| Cabling | FW |  | X | X |  |
| Cabling | MS |  | X | X |  |
| Cabling | NI |  | X | X |  |
| Cabling \& Instrumentation | RC |  | X | X |  |
| Cabling | SW |  | X | X |  |
| Cabling | SWA |  | X | X |  |
| Cabling | SI |  | X | X |  |
| Elect. Penetration | EDE |  | X | X |  |
| Dist. Pahel PP-6B | RC |  | X | X |  |
| Fuse Cabinets | EDE |  | X | X |  |
| Excore Xmtr | NI |  | X | X |  |
| Rad Mon | RM |  | X | X |  |
| Cabling | CS |  | X | X |  |
| Cabling | CAP |  | X | X |  |
| Cabling | CBS |  | X | X |  |

$\left.\begin{array}{|l|c|l|}\hline \text { SEABROOK } & \text { Evaluation and Comparison to BTP APCSB 9.5-1, } & \begin{array}{l}\text { Rev. 12 } \\ \text { Station }\end{array} \\ \text { Sppendix A }\end{array} \quad \begin{array}{l}\text { Page F.2 Tab 6 } \\ \text { Pare Hazard Analysis - ET-F-1C-A }\end{array}\right]$
12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | COP |  | X | X |  |
| Cabling | NG |  | X | X |  |
| Cabling | VG |  | X | X |  |
| Cabling | WLD |  | X | X |  |
| Cabling | CGC |  | X | X |  |
| Cabling | RM |  | X | X |  |
| Cabling | SA |  | X |  |  |
| Cabling | IA |  | X |  |  |
| Cabling | IC |  | X | X |  |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)
 Other:

### 13.2 Total Fire Loading in Area: <br> Total Combustibles:

Fire Loading in Area


Btu/Sq. Ft. Btu/Sq. Ft. Btu/Sq. Ft. Btu/Sq. Ft. Btu/Sq. Ft. $104.3 \mathrm{Btu} / \mathrm{Sq}$. Ft. $\frac{104.3}{222,864}$ Btu/Sq. Ft.

### 14.0 Design-Basis Fire Description

1. For conservatism all the plastic components of both pumps are assumed to ignite and burn.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 12 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 6 |  |  |
| Page 4 of 4 |  |  |

2. To add conservatism, there are three types of plastic in the components. A series of fire loading calculations using the NRC, NUREG-1805 Fire Dynamics Tools Quantitative Fire Hazard Method for each type of plastic was performed. The bounding maximum burning duration and maximum temperature were determined by taking the maximum duration from all the calculations and the maximum temperature.
3. No credit was given to the CEVA wall that separated the fire location from the remainder of the fire area.
14.1 DBF Fire Loading
104.3 Btu/Sq. Ft.
14.2 Peak Zone Temperature Fire $559.7{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
6.6 Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Cable will not become involved in the fire. Also, redundant cabling is not in this fire area.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished with portable extinguishers.

Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Area is designed with a water spray system; drain paths will remove water.

### 18.0 Containing Design Basis Fire in the Fire Area/Zone

18.1 Fire detectors initiate an alarm in the control room and actuate the pre-action sprinkler system valve, allowing water to fill the piping to the closed head sprinklers. The control room alerts the fire brigade.
18.2 The fire would be extinguished using hose lines and/or portable extinguishers and/or area sprinkler system.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Not applicable as no redundant safe shutdown equipment is located in this fire area.


[^5]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 12 <br> Appendix A |
| :--- | :---: | :--- |
| Station | Fire Hazard Analysis - ET-F-1D-A | Page 2 of 3 Tab 6 <br> Pag |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |  |
| Cabling | CAH |  | X | X | X |
| Cabling | CC |  | X | X | X |
| Cabling | EDE |  | X | X | X |
| Cabling | EPA |  | X | X | X |
| Cabling | FW |  | X | X | X |
| Cabling | MS |  | X | X | X |
| Cabling | NI |  | X | X | X |
| Cabling | RC |  | X | X | X |
| Cabling | PAH |  | X | X | X |
| Cabling | SW |  | X | X | X |
| Cabling | SWA |  | X | X | X |
| Cabling | SI |  | X | X |  |
| Cabling | CBS |  | X | X |  |
| Cabling | COP |  | X | X |  |
| Cabling | NG |  | X | X |  |
| Cabling | VG |  | X | X |  |
| Cabling | WLD |  | X | X |  |
| Cabling | CGC |  | X | X |  |
| Cabling \& Instrumentation | RM |  | X | X |  |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 12 <br> Section F.2 Tab 6 <br> Page 3 of 3 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | SB |  | X | X |  |
| Cabling | SA |  | X |  |  |
| Cabling | IA |  | X |  |  |
| Cabling | IC |  | X |  |  |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 12 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 6 |  |  |
| Page 1 of 2 |  |  |

Fire Hazard Analysis - ET-F-S1-0
1.0 Building
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location

Drawing No
Electrical Tunnel
ET-F-S1-0
Stairwell
El. (-)20 \& (-)26'
9763-F-310453-FP
3.0 Construction of Area

4.0 Floor Area 120 Sq. Ft. Length $\underline{14^{\prime}-6^{\prime \prime}}$ Width $8^{\prime}-44^{\prime \prime}$ Height $64^{\prime}$
5.0 Volume $\quad 7,700 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear __ Non-Nuclear X (Sump pump in stairwell)
7.0 Exhaust Ventilation System None
7.1 Percentage of System's Capacity N/A
8.0 8 Hr. Emergency Lighting in Area
Yes $\qquad$ No

$$
\text { No } \quad \mathrm{X}
$$

8.1 Outside Area at Exit Points
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Yes
Yes


Type
Portable Extinguisher
Hose Station
None
------
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 12 <br> Appendix A <br> Section F.2 Tab 6 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  |  |  |  | Required |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Equipment | $\underline{S y s t e m ~ T r a i n ~}$ | Safety | For Safe |  |  |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ | $\underline{\text { Shutdown }}$ |

No safety related or safe shutdown equipment in this area

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> Appendix A <br> Section F.2 Tab 7 |
| :--- | :---: | :--- |

Fire Hazard Analysis - DG-F-1A-A
$\begin{array}{ll}1.0 & \text { Building } \\ 2.0 & \text { Fire Area or Zone }\end{array}$
2.1 Area Name
2.2 Location

Drawing No

Diesel Generator Building
DG-F-1A-A
Fuel Oil Storage Tank Area
North - El (-) $16^{\prime}-0^{\prime \prime}$
9763-F-202068-FP
3.0 Construction of Area

4.0 Floor Area $\quad$ 1,430 Sq. Ft. Length Varies Width Varies Height 33.5'
5.0 Volume $\quad 47,900 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X None__
7.0 Exhaust Ventilation System Gravity Ventilation
7.1 Percentage of System's Capacity
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points


$$
\begin{aligned}
& \text { No } \mathrm{X} \\
& \text { No }
\end{aligned}
$$

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ No X
No X
Type
Redundant Preaction Systems
Fire Extinguisher(s)
Ionization \& Thermal
Standpipe and Hose Reel

### 11.0 Fire Loading in Area

11.1 Refer to page 2. (Analysis continued page 2)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 7 |  |  |
| Page 2 of 2 |  |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Fuel Oil Storage Tank | DG | X |  | X | * |
| Fuel Oil Transfer Pump P38A | DG | X |  | X | * |
| FLEX Electric Fuel Transfer Pump A | FLEX | X |  | - | - |
| Level Switches | DG | X |  | X | * |
| Cabling | DG | X |  | X | * |
| Piping \& Valves | DG | X |  | X | * |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

| Oil: | 75,000 Gallons |
| :--- | :--- |
| Grease: | Pounds |
| Class A: | $=$ Pounds |
| Charcoal: | Pounds |
| Chemicals: | $=$ Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: | $\square$ |

13.2 Total Fire Loading in Area:

Total Combustibles:

| Fire Loading in Area |  |
| :---: | :---: |
| 7,867,000 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | $\mathrm{Btu} / \mathrm{Sq}$. Ft |
|  | Btu/Sq. F |

$\frac{7,867,000}{1125 \mathrm{X}} \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft}$. $1125 \times 10^{\top} \mathrm{Btu}$

### 14.0 Design-Basis Fire Description

See Appendix "A" of this report.

[^6]| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> Appendix A <br> Pection F.2 Tab 7 |
| :--- | :---: | :--- |

Fire Hazard Analysis - DG-F-1B-A
$\begin{array}{ll}1.0 & \text { Building } \\ 2.0 & \text { Fire Area or Zone }\end{array}$
2.1 Area Name
2.2 Location Drawing No

Diesel Generator Building
DG-F-1B-A
Fuel Oil Storage Tank Area
South - El (-) $16^{\prime}-0$ "
9763-F-202068-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire R }}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 1,430 Sq. Ft. Length Varies Width Varies Height 33.5'
5.0 Volume 47,900 Cu. Ft.
6.0 Floor Drains Nuclear ___ Non-Nuclear $\quad \mathrm{X}$ None___
7.0 Exhaust Ventilation System
Gravity Ventilation
7.1 Percentage of System's Capacity
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points

Yes
$\qquad$

Yes

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Yes
Yes
 Type
Redundant Preaction Systems
Fire Extinguisher(s)
Ionization \& Thermal
Standpipe and Hose Reel
11.0 Fire Loading in Area
11.1 Refer to page 2. (Analysis continued page 2)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> Section F.2 Tab 7 <br> Page 2 of 2 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety <br> Related |
| :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |
| Fuel Oil Storage Tank | DG |  | X | X |
| Fuel Oil Transfer Pump P38B | DG |  | X | X |
| FLEX Electric Fuel Transfer Pump B | FLEX |  | X | - |
| Cabling | DG |  | X | X |
| Piping \& Valves | DG |  | X | X |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: |  |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | $=$ Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

13.2 Total Fire Loading in Area: $\quad \frac{7,867,000}{1125} \mathbf{~ B t u / S q . ~ F t . ~}$

Total Combustibles:

### 14.0 Design-Basis Fire Description

See Appendix "A" of this report.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 7 <br> Page 1 of 5 |  |  |

Fire Hazard Analysis - DG-F-2A-A
1.0 Building
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location

Drawing No
Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |

5.0 Volume $\quad 107,300 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X None ___
7.0 Exhaust Ventilation System Dg Bldg. Exhaust System
7.1 Percentage of System's Capacity
8.0 8 Hr. Emergency Lighting in Area
8.1 Outside Area at Exit Points

No $\qquad$
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes
Yes

No X
9.2 Airborne

Type
10.1 Primary
10.2 Secondary
10.3 Detection

Manual Preaction Providing Area Protection and Auto Preaction in Oil Piping Trench
Fire Extinguisher(s)
Ionization \& Ultraviolet/Thermal in Trench
Standpipe \& Hose Reel
11.0 Fire Loading in Area
11.1 Refer to page 3. (Analysis continued pages 2-4)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 7 <br> Page 2 of 5 |  |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Starting Air Skid 17A | DG | X |  | X |
| Cabling | DG | X |  | X |
| Cabling | DAH | X |  | X |
| Cabling | CBA | X |  | X |
| Diesel Generator Control Cabinet CP-75A | DG | X |  | X |
| Diesel Generator Control Cabinet CP-75B | DG | X |  | X |
| 5 Kv Non-Seg. Bus Duct | EDE | X |  | X |
| Cabling | SW | X |  | X |
| Damper DP-16A | DAH | X |  | X |
| Temp Switches | DAH | X |  | X |
| Diesel Generator Control Panel CP-36 | DG | X |  | X |
| Terminal Box HF7 | DG | X |  |  |
| Diesel Generator 1-A \& Aux | DG | X |  | X |
| Fan-FN-26A | DAH | X |  | X |
| Piping \& Valves | DG | X |  | X |
| 460v MCC-E511 | EDE | X |  | X |
| Cabling \& Controls | RC | X |  | X |
| Disabling Panel MM-CP-450A | MM | X |  | X |
| Backup Control Air Compressor | DG | X |  | X |


| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Appendix A |
| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - DG-F-2A-A | Page 3 of 5 Tab 7 |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ) Fire Loading in Area

| Note: | Oil Fire |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Oil: | 1,627.5 | Gallons | 62,375 | Btu/Sq. Ft. |
| Grease: |  | Pounds |  | Btu/Sq. Ft. |
| Class A: |  | Pounds |  | Btu/Sq. Ft. |
| Charcoal: |  | Pounds |  | Btu/Sq. Ft. |
| Chemicals: |  | Pounds |  | Btu/Sq. Ft. |
| Plastics: | 38 | Pounds | 134 | Btu/Sq. Ft. |
| Resins: |  | Pounds |  | Btu/Sq. Ft. |
| Other: | 55 LF | Cable Trays | 9,964 | Btu/Sq. Ft. |
|  |  | Stacked 3 High |  |  |

### 13.2 Total Fire Loading in Area: <br> Total Combustibles: <br> 72,473 Btu/Sq. Ft. <br> 268,230,000 Btu

### 14.0 Design-Basis Fire Description

1. The diesel engine is located on the $21^{\prime}-6$ " level. The engine is not operating.
2. The fuel oil line connecting the day tank on the 51 ' -6 " level and the diesel engine ruptures.
3. Fuel oil is siphoned from the day tank at a rate of $24 \mathrm{gpm}(30 \mathrm{ft}$. of head in a $1 / 2$ " fuel oil line).
4. Fuel oil is sprayed into the engine room and covers an area of $400 \mathrm{ft}^{2}$ with a film of oil $1 / 16^{\prime \prime}$ thick.
5. The oil flows into the trench around the engine.
6. The oil is ignited at the time of the rupture.
7. The oil burns at a rate of 5 " per hour and consumes 21 gpm , therefore 3 gpm of unburned oil runs into the trench drain and down to the sump in the fuel oil storage tank vault at the (-) $16^{\prime}-0^{\prime \prime}$ level below.
8. The fuel oil transfer pump at the (-) $16^{\prime}-0^{\prime \prime}$ level continues to fill the day tank.
9. The fuel oil in the engine room is heated by the fire ( $4200^{\circ} \mathrm{F}$ flame temperature). The hot oil flowing into the trench will flash upon discharging into the covered sump at the (-)16'-0" level below.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 7 |  |  |
| Page 4 of 5 |  |  |

10. The heat from the fire in the covered sump will activate the sump wet pipe sprinklers and the vaults detection and suppression system and alarm in the control room.
11. It is estimated that a time period of 5 minutes lapses between the oil line rupture and ignition of the oil in the sump.
12. The transfer pump will continue to fill the day tank until either the deluge system deactivates the pump or action is taken by plant personnel in response to the alarm.
13. It is estimated that the detectors in the storage tank vault will alarm in 10 Minutes.
14. It requires 62.5 minutes for the tank to empty after the fuel oil transfer pump shuts down, therefore 1500 gallons of oil drains into the engine room. The engine room fire consumes 1312 gallons while 188 gallons of oil drains into the sump below.
15. Estimated minimum fuel oil consumed by the fire and duration of the fire:

| A) | Line Rupture to Shut Down of Transfer Pump | 15 Min | 315 Gal |
| :--- | :--- | :--- | :--- |
| B) | Complete Discharge of Day Tank Into the | 62.5 Min | 1312 Gal |
|  | Engine Room | 77.5 Min | 1627 Gal |

16. Total combustibles

Plastic
Oil
Cable
Total

494,000 Btu
230,784,000 Btu
36,867,000 Btu
268,150,000 Btu
17. A lube oil fire was postulated but found to be less severe than the fuel oil fire, therefore it has not been considered as the design basis fire for the subject area.
14.1 DBF Fire Loading

72,473 Btu/Sq.Ft.
14.2 Duration of Fire
$>5$ Minutes
14.3 Peak Temperature
$1650{ }^{\circ} \mathrm{F}$

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 7 <br> Page 5 of 5 |  |  |

15.0 Consequences of Design Basis Fire without Fire Protection
15.1 The entire area will be engulfed in flame and all equipment and cable will be lost.
15.2 Possible spalling of concrete.
15.3 Only one diesel generator train will be affected and safe shutdown can be Accomplished By the Redundant Diesel Located in Another Fire Area.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Possible loss of the equipment and cabling.
16.2 No damage to engine due to water deluge system on oil piping.
16.3 Safe shutdown can be accomplished, if necessary, by the redundant diesel train located in another area.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Area floor drains and trenches will prevent buildup of water. Deluge is directed on piping and floor area, therefore it will not affect other equipment.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Early warning ionization detectors alarming in the control room.
18.2 Thermal detectors setting off the deluge system on the oil piping in the event the fire brigade does not respond in time.
18.3 The entire engine room is within a minimum 3 hour fire rated structure.
18.4 Fire dampers in the ductwork will prevent the spread of fire to equipment room above.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Not applicable. (see 15.3)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 16 <br> Section F.2 Tab 7 <br> Page 1 of 5 |
| :--- | :---: | :--- |

Fire Hazard Analysis - DG-F-2B-A
$\begin{array}{ll}1.0 & \text { Building } \\ 2.0 & \text { Fire Area or Zone }\end{array}$
2.1 Area Name
2.2 Location

## Drawing No

Diesel Generator Building
DG-F-2B-A
Engine Room

| South - El. 21'-6" |
| :--- |
| 9763-F-202069-FP |

3.0 Construction of Area

| 3.1 | Walls | North <br> South | $\frac{\text { Material }}{\text { East }}$Concrete <br> Wencrete <br> 3.2 |
| :--- | :--- | :--- | :--- |
| Floor <br> Wencrete |  |  |  |
| 3.3 | Ceiling |  | $\frac{\text { Concrete }}{\text { Doors }}$ |

3.5 Others

Fireproofed Ceiling Beams

| $\frac{\text { Min. Fire Rating }}{3 \mathrm{Hr} .}$ |
| :--- |
| $\frac{\text { Outside }}{3 \mathrm{Hr} .}$ |
| $\frac{\text { Outside }}{3 \mathrm{Hr} .}$ |
| $\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} / \text { Outside/ }}$ |
| $\frac{11 / 2 \mathrm{Hr} .(\text { Stairs })}{3 \mathrm{Hr} .}$ |


6.0 Floor Drains Nuclear

$$
\text { Non-Nuclear } \quad \mathrm{X} \quad \text { None }
$$

7.0 Exhaust Ventilation System
7.1 Percentage of System's Capacity
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area
8.1 Outside Area at Exit Points

$$
\begin{array}{ll}
\text { Yes } & X \\
\cline { 2 - 3 } & \mathrm{Xes} \\
& \mathrm{X}
\end{array}
$$

$\qquad$
7.0 Exhaust Ventilation System
No $\qquad$
9.0 Operational Radioactivity
9.1 Equipment/Piping

10.0 Fire Protection
10.1 Primary

Type
Manual preaction providing area protection and auto preaction in oil piping trench
Fire Extinguisher(s)
Ionization \& Ultraviolet/Thermal in Trench
Standpipe \& Hose Reel
11.0 Fire Loading in Area
11.1 Refer to page 3. (Analysis continued pages 2-4)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 16 <br> Section F.2 Tab 7 <br> Page 2 of 5 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety <br> Related |
| :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |
| Starting Air Skid 17B | DG |  | X | X |
| Cabling | DG |  | X | X |
| Cabling | DAH |  | X | X |
| Cabling | CBA |  | X | X |
| Diesel Generator Control Cabinet CP-76B | DG |  | X | X |
| Diesel Generator Control Cabinet CP-76A | DG |  | X | X |
| 5 Kv Non-Seg. Bus Duct | EDE |  | X | X |
| Damper DP-16B | DAH |  | X | X |
| Temp Switches | DAH |  | X | X |
| Diesel Generator Control Panel CP-37 | DG |  | X | X |
| Diesel Generator 1-B \& Aux | DG |  | X | X |
| Terminal Box HF8 | DG |  | X | X |
| Fan-FN-26B | DAH |  | X | X |
| Cabling | SW |  | X | X |
| Damper DP-16B | DAH |  | X | X |
| Cabling | EDE |  | X | X |
| Piping \& Valves | DG |  | X | X |
| 460v MCC-E611 | EDE |  | X | X |
| Cabling \& Controls | RC |  | X | X |
| Disabling Panel MM-CP-450B | MM |  | X | X |
| Backup Control Air Compressor | DG | X |  | X |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 16 <br> Section F.2 Tab 7 <br> Page 3 of 5 |
| :--- | :---: | :--- |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ) Fire Loading in Area

| Note: | Oil Fire |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Oil: | 1,627.5 | Gallons | 62,375 | Btu/Sq. Ft. |
| Grease: |  | Pounds |  | Btu/Sq. Ft. |
| Class A: |  | Pounds |  | Btu/Sq. Ft. |
| Charcoal: |  | Pounds |  | Btu/Sq. Ft. |
| Chemicals: |  | Pounds |  | Btu/Sq. Ft. |
| Plastics: | 38 | Pounds | 134 | Btu/Sq. Ft. |
| Resins: |  | Pounds |  | Btu/Sq. Ft. |
| Cables: | 268.5 | Pounds |  |  |
| Other: | 55 LF | Cable Trays | 10,726 | Btu/Sq. Ft. |
|  |  | Stacked 3 High |  |  |

13.2 Total Fire Loading in Area:
Total Combustibles:

| $\frac{73,235}{270,963,800}$ | Btu/Sq. Ft. |
| ---: | :--- |

### 14.0 Design-Basis Fire Description

1. The diesel engine is located on the $21^{\prime}-6$ " level. The engine is not operating.
2. The fuel oil line connecting the day tank on the 51 ' -6 " level and the diesel engine ruptures.
3. Fuel oil is siphoned from the day tank at a rate of $24 \mathrm{gpm}(30 \mathrm{ft}$. of head in a $1 / 2$ " fuel oil line).
4. Fuel oil is sprayed into the engine room and covers an area of $400 \mathrm{ft}^{2}$ with a film of oil $1 / 16^{\prime \prime}$ thick.
5. The oil flaws into the trench around the engine.
6. The oil is ignited at the time of the rupture.
7. The oil burns at a rate of 5 " per hour and consumes 21 gpm , therefore 3 gpm of unburned oil runs into the trench drain and down to the sump in the fuel oil storage tank vault at the (-)16'-0" level below.
8. The fuel oil transfer pump at the (-)16'-0" level continues to fill the day tank.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 16 <br> Section F.2 Tab 7 <br> Page 4 of 5 |
| :--- | :---: | :--- |

9. The fuel oil in the engine room is heated by the fire ( $4200^{\circ} \mathrm{F}$ flame temperature). The hot oil flowing into the trench will flash upon discharging into the covered sump at the (-)16'-0" level below.
10. The heat from the fire in the covered sump will activate the sump wet pipe sprinklers and the vaults detection and suppression system and alarm in the control room.
11. It is estimated that a time period of 5 minutes lapses between the oil line rupture and ignition of the oil in the sump.
12. The transfer pump will continue to fill the day tank until either the deluge system deactivates the pump or action is taken by plant personnel in response to the alarm.
13. It is estimated that the detectors in the storage tank vault will alarm in 10 minutes.
14. It requires 62.5 minutes for the tank to empty after the fuel oil transfer pump shuts down, therefore 1500 gallons of oil drains into the engine room. The engine room fire consumes 1312 gallons while 188 gallons of oil drains into the sump below.
15. Estimated minimum fuel oil consumed by the fire and duration of the fire:
A) Line Rupture to Shut Down of Transfer Pump 15 Min 315 Gal
B) Complete Discharge of Day Tank Into the $\quad 62.5 \mathrm{Min} \quad 1312 \mathrm{Gal}$ Engine Room $\quad$ 77.5 Min 1627 Gal
16. Total combustibles

Plastic 494,000 Btu
Oil 230,784,000 Btu
Cable $\quad 39,686,200$ Btu
Total 270,963,800 Btu
17. A lube oil fire was postulated but found to be less severe than the fuel oil fire, therefore it has not been considered as the design basis fire for the subject area.
14.1 DBF Fire Loading

73,235 Btu/Sq.Ft.
14.2 Duration of Fire
$>5$ Minutes
14.3 Peak Temperature
$1650{ }^{\circ} \mathrm{F}$

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 16 <br> Section F.2 Tab 7 <br> Page 5 of 5 |
| :--- | :---: | :--- |

15.0 Consequences of Design Basis Fire without Fire Protection
15.1 The area will be engulfed in flame and all equipment and cable will be lost.
15.2 Possible spalling of concrete.
15.3 Only one diesel generator train will be affected and safe shutdown can be accomplished by the redundant diesel located in another fire area.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Possible loss of the equipment and cabling.
16.2 No damage to engine due to water deluge system on oil piping.
16.3 Safe shutdown can be accomplished, if necessary, by the redundant diesel train located in another area.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Area floor drains and trenches will prevent buildup of water. Deluge is directed on piping and floor area, therefore it will not affect other equipment.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Early warning ionization detectors alarming in the control room.
18.2 Thermal detectors setting off the deluge system on the oil piping in the event the fire brigade does not respond in time.
18.3 The entire engine room is within a minimum 3 hour fire rated structure.
18.4 Fire dampers in the ductwork will prevent the spread of fire to equipment room above.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Not applicable. (See 15.3)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> Appendix A <br> Section F.2 Tab 7 |
| :--- | :---: | :--- |

Fire Hazard Analysis - DG-F-3A-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |


| Diesel Generator Building |
| :--- |
| DG-F-3A-Z |
| HVAC Equipment Area |
| North El. 51'-6" |
| 9763-F-202069-FP |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\text { Open }}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area $\quad$ 1,555 Sq. Ft. Length 42’_ Width $37^{\prime}$ _Height 25’
5.0 Volume $\quad 38,880 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X None ___
7.0 Exhaust Ventilation System None
$\begin{array}{lllll} & 7.1 & \text { Percentage of System's Capacity } & - \\ 8.0 & \begin{array}{l}\text { 8 Hr. Emergency Lighting in Area } \\ 8.1\end{array} & \text { Yes } & \\ & \text { Outside Area at Exit Points } & \text { Yes } & - & \text { No }\end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 Refer to page 3 of 4

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 |
| :--- | :---: | :--- |
| STATION | Appendix A | Section F.2 Tab 7 <br> Page 2 of 4 |

### 12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{l}$ System Train | Safety <br> Related |  |
| :--- | :--- | :--- | :---: | :---: |
| Fan FN-25A | DAH | X |  | X |
| Cabling | DAH | X |  | X |
| Damper DP-15A | DAH | X |  | X |
| Fan FN-27A | CBA | X |  | X |
| Chiller E-230A | CBA | X |  | X |
| Fan FN-211A | CBA | X |  | X |
| Damper DP-53A | CBA |  | X | X |
| Pressure Switches | CBA | X |  | X |
| Cabling | CBA | X | X | X |
| Fan FN-27B | CBA |  | X | X |
| Pumps P-434A/P-435A | CBA | X |  | X |
| Flow Switch | DAH | X |  | X |
| Damper DP-53B | CBA | X |  | X |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)


Other:
13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| 482 | $\begin{aligned} & \text { Btu/Sq. Ft.* } \\ & \text { Btu/Sq. Ft. } \end{aligned}$ |
| :---: | :---: |
|  |  |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. | | 482 | Btu/Sq. Ft.* |
| ---: | :--- |
| $1,500,000$ | Btu |


| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 |
| :--- | :---: | :--- |
| STATION | Appendix A | Section F.2 Tab 7 <br> Page 3 of 4 |

### 14.0 Design-Basis Fire Description

A) Due to a lack of physical boundary both fire zones, DG-1-3A-Z and DG-F-3B-Z constitute a common fire area.
B) The oil content of control building HVAC system compressor/condensing unit spills over floor and catches fire and burn, completely.
14.1 DBF Fire Loading
$11,719 \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft}$.
14.2 Duration of Fire
$41 / 2$ Minutes
14.3 Peak Temperature
$1231{ }^{\circ} \mathrm{F}$
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of both air conditioning trains of control room a/c system because of lack of oil.
15.2 Loss of HVAC system to both diesel generator areas as both ventilating fans are located in the affected area and, both fans take suction of hot air from the same plenum.
*Based on floor area of zones DG-F-3A-Z and DG-F-3B-Z (3100 sq. ft.).
15.3 HVAC system cooling capability for both trains of the emergency switch gear battery room and the cable spreading area will not be lost since the fire dampers in supply air stream from diesel generator building will not reach the fuseable link melting temperature to close as a result of the Design Basis Fire (Ref. Calc. SBC-173).

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Loss of both trains of control room HVAC system because of lack of oil.
16.2 Possible loss of cooling capability of both diesel generator areas as both train ventilating fans are located in the affected area.
16.3 HVAC system cooling capability for both trains of the emergency switch gear battery room and the cable spreading area will not be lost since the fire dampers in supply air stream from diesel generator building will not reach the fuseable link melting temperature to close as a result of the Design Basis Fire (Ref. Calc. SBC-173).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> Appendix A |
| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - DG-F-3A-Z | Section F.2 Tab 7 <br> Page 4 of 4 |

17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable, no automatic water suppression system exists.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 The design base fire will be contained in the fire area bounded by fire rated structures. Both affected zones are contained in the same fire area.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Redundant safe shutdown equipment if any, may be lost. For safe shutdown requirements, refer to Table 3.2.7.41 of the report "Fire Protection of Safe Shutdown Capability" (10 CFR 50, Appendix R).


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 9 <br> Appendix A <br> Pection F.2 Tab 7 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{l}$ System Train | Safety <br> Related |  |
| :--- | :--- | :---: | :---: | :---: |
| Fan-FN-25B | DAH |  | $\underline{B}$ | $\underline{X}$ |
| Cabling | DAH |  | X | X |
| Damper DP-15B | DAH |  | X | X |
| Fan FN-211B | CBA |  | X | X |
| Chiller E-230B | CBA |  | X | X |
| Pressure Switches | CBA |  | X | X |
| Cabling | CBA |  | X | X |
| Pumps P-434B-435B | CBA | X |  | X |
| Flow Switch | DAH |  | X | X |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | $=$ Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

- Based on floor area of zones DG-1-3A-Z and DG-1-3B-Z (3110 Sq. Ft.)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 9 <br> Appendix A <br> Fection F.2 Tab 7 |
| :--- | :---: | :--- |

14.0 Design-Basis Fire Description
A) Due to a lack of physical boundary both fire zones, DG-F-3A-Z and DG-F-3B-Z constitute a common fire area.
B) The oil content of control building HVAC system compressor/condensing unit spills over floor and catches fire and burn completely.
14.1 DBF Fire Loading 11,719 Btu/Sq.Ft.
14.2 Duration of Fire $41 / 2$ Minutes
14.3 Peak Temperature
$1231{ }^{\circ} \mathrm{F}$

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of both air conditioning trains of control room A/C System because of lack of oil.
15.2 Loss of HVAC system to both diesel generator areas as both ventilating fans are located in the affected area and take suction of hot air from the same plenum.
15.3 HVAC system cooling capability for both trains of the emergency switch gear battery room and the cable spreading area will not be lost since the fire dampers in supply air stream from diesel generator building will not reach the fuseable link melting temperature to close as a result of the Design Basis Fire (Ref. Calc. SBC-173).
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of both trains of control room HVAC system because of lack of oil.
16.2 Possible Loss of Cooling Capability of Both Diesel Generator Areas As Both Train Ventilating Fans Are Located in the Affected Area.
16.3 HVAC system cooling capability for both trains of the emergency switch gear battery room and the cable spreading area will not be lost since the fire dampers in supply air stream from diesel generator building will not reach the fuseable link melting temperature to close as a result of the Design Basis Fire (Ref. Calc. SBC-173).
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable, no automatic water suppression system exists.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 9 <br> Section F.2 Tab 7 <br> Page 4 of 4 |
| :--- | :---: | :--- |

18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 The design base fire will be contained in the fire area bounded by fire rated structures. Both affected zones are contained in the same fire area.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 Redundant safe shutdown equipment if any, may be lost. For safe shutdown requirements refer to Table 3.2.7.41 of the report "Fire Protection Safe Shutdown Capability" (10 CFR 50, Appendix R).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 |
| :--- | :---: | :--- |
| STATION | Appendix A | Section F.2 Tab 7 <br> Page 1 of 3 |

Fire Hazard Analysis - DG-F-3C-A
Fire Hazard Analysis - DG-F-3C-A
$\begin{array}{ll}\text { 1.0 } & \text { Building } \\ 2.0 & \text { Fire Area or Zone }\end{array}$
2.1 Area Name
2.2 Location Drawing No
2.0 Fire Area or Zone

Diesel Generator Building
DG-F-3C-A
Fuel Oil Day Tank Area
North - El. 51'-6"
9763-F-202069-FP

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Section F. 2 Tab 7
Page 1 of 3
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete }}{\text { Concrete }}$ <br> 3.2 |
| :--- | :--- | :--- | :--- |
| Concrete |  |  |  |
| 3.3 | Floor |  | $\frac{\text { Coiling }}{\text { Concrete }}$ |
| 3.4 | Doors |  | $\frac{\text { Metal }}{\text { Concrete }}$ |
| 3.5 | Others |  |  |


$\frac{\text { Min. Fire Rating }}{\frac{3 \mathrm{Hr} .}{\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}}}$| $\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}$ |
| :--- |
| $\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}$ |

4.0 Floor Area 200 Sq. Ft. Length 23.5' Width $\underbrace{8.5^{\prime}}$ Height $11.0^{\prime}$
5.0 Volume $\quad 2,200 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X_None_
7.0 Exhaust Ventilation System Gravity
7.1 Percentage of System's Capacity None
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points
Yes
Yes

$$
\begin{array}{ll}
\text { No } & \mathrm{X} \\
\text { No } \\
\hline
\end{array}
$$

9.0 Operational Radioactivity

| 9.1 | Equipment/Piping | Yes | No $\quad$ X |
| :--- | :--- | :--- | :--- |
| 9.2 | Airborne | Yes | No X |

10.0 Fire Protection
10.1 Primary

Type
Deluge Systems
10.2 Secondary
10.3 Detection
10.4 Other

Fire Extinguisher(s)
Ionization \& Thermal
Standpipe and Hose Reel

### 11.0 Fire Loading in Area

11.1 Refer to page 2 (analysis continued Pages 2 \& 3)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 7 |  |  |
| Page 2 of 3 |  |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ | $\underline{\text { System Train }}$ | Safety <br> Related |
| :--- | :---: | :---: | :---: |
| Fuel Oil Day Tank | DG | X | $\underline{\mathrm{B}}$ |
| Instruments | DG | X | X |
| Cabling | DG | X | X |
| Level Switches | DG | X | X |
| Piping \& Valves | DG | X | X |
|  |  |  | X |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: | $\square$ |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| 1,125,000 | Btu/Sq. Ft. |
| :---: | :---: |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

$\begin{array}{ll}1,125,000 & \text { Btu/Sq. Ft. } \\ 225 \times 10^{6} & \text { Btu }\end{array}$ $\underline{225 \times 10^{6}} \mathrm{Btu}$

### 14.0 Design-Basis Fire Description

1. The diesel oil day tank ruptures and oil spills on the enclosure floor. Floor drain will remove some of the oil. It is conservatively assumed that some of the oil will burn in the enclosure.
2. The maximum rate of burn equals 5 " per hour.
3. The oil may burn in excess of 3 hours, at which time the enclosure is assumed to fail. Consequences of failed enclosure is beyond the scope of this appendix A "FHA" report.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 7 |  |  |
| Page 3 of 3 |  |  |

4. During the 3 hours before the failure of the enclosure, 900 gallons of oil is consumed and the remaining oil will be contained within the bottom or stamp section of the enclosure.
14.1 DBF Fire Loading $\quad 675,000$ Btu/Sq.Ft.
14.2 Duration of Fire

3 Hours
14.3 Peak Temperature

$$
\underline{2,650}{ }^{\circ} \mathrm{F}
$$

(Five hours without any means of fire protection)
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of the diesel oil day tank and oil.
15.2 Loss of the instruments, lighting and cable in the tank vault.
15.3 Safe shutdown can be accomplished using the redundant diesel fuel oil day tank which is located outside the 3 hour barrier. (The redundant fuel oil day tank may be lost if fire is not controlled within three hours).
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Possible loss of the day tank, instruments and oil.
16.2 Safe shutdown can be accomplished using the redundant diesel train which is located outside the 3 hour barrier.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Vault contains a floor drain which discharges into the sump in the storage tank vault at the (-) $16^{\prime}-0^{\prime \prime}$ level, therefore damage due to water is of no consequence.

### 18.0 Containing Design Basis Fire in the Fire Area/Zone

18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 In the event the fire brigade cannot extinguish the fire the rate of rise detectors will set off the water deluge fire protection system.
18.3 If deluge system fails then fire will be put out by stand pipe and hose reels.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 There is no redundant safe shutdown equipment in this fire area. (Refer 15.3 above). If in unlikely event both diesel generator day tanks are lost as fire burns beyond three hours, safe shutdown of reactor will be achieved either from control room or RSS panel.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A <br> STATION |
| :--- | :---: | :--- |
| Fire Hazard Analysis - DG-F-3D-A |  |  |$\quad$| Page 1 of 3 Tab 7 |
| :--- |

Fire Hazard Analysis - DG-F-3D-A
Fire Hazard Analysis - DG-F-3D-A
$\begin{array}{ll}1.0 & \text { Building } \\ 2.0 & \text { Fire Area or Zone }\end{array}$
2.1 Area Name
2.2 Location Drawing No
2.0 Fire Area or Zone

Diesel Generator Building
DG-F-3D-A
Fuel Oil Day Tank Area
South El. 51'-6" 9763-F-202069-FP

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Page 1 of 3
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete }}{\text { Concrete }}$ <br> 3.2 |
| :--- | :--- | :--- | :--- |
| Concrete |  |  |  |
| 3.3 | Floor |  | $\frac{\text { Coiling }}{\text { Concrete }}$ |
| 3.4 | Doors |  | $\frac{\text { Metal }}{\text { Concrete }}$ |
| 3.5 | Others |  |  |

$\frac{\text { Min. Fire Rating }}{\frac{3 \mathrm{Hr} .}{\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}}} \frac{\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}}{\frac{3 \mathrm{Hr} .}{3 \mathrm{Hr} .}}$
4.0 Floor Area 200 Sq. Ft. Length 23.5' Width $\underbrace{8.5} \quad$ Height $11.0^{\prime}$
5.0 Volume $\quad 2,200 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear __ Non-Nuclear X_None_
7.0 Exhaust Ventilation System Gravity
7.1 Percentage of System's Capacity None
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes

8.1 Outside Area at Exit Points $\qquad$ | No X |
| :--- |
| No X |

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No X |
| :--- |
| No |

10.0 Fire Protection
10.1 Primary

Yes $\qquad$ No X
Type
10.2 Secondary
10.3 Detectional
10.4 Other

Deluge Systems
Fire Extinguisher(s)
Ionization \& Thermal
Standpipe and Hose Reel

### 11.0 Fire Loading in Area

11.1 Refer to page 2 (analysis continued pages 2 \& 3)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A <br> Pection F.2 Tab 7 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{S y s t e m}$ | $\underline{l}$ System Train | Safety <br> Fuel Oil Day Tank | DG |
| :--- | :---: | :---: | :---: | :---: |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |  |
| :---: | :---: | :---: |
| Oil: | 1,500 | Gallons |
| Grease: |  | Pounds |
| Class A: |  | Pounds |
| Charcoal: |  | Pounds |
| Chemicals: |  | Pounds |
| Plastics: |  | Pounds |
| Resins: |  | Pounds |
| Other: |  |  |

$\begin{array}{llll}\text { 13.2 } & \text { Total Fire Loading in Area: } & \underline{1,125,000} & \text { Btu/Sq. Ft. } \\ \text { Total Combustibles: } & \underline{225 \times 10^{6}} & \text { Btu }\end{array}$

### 14.0 Design-Basis Fire Description

1. The diesel oil day tank ruptures and oil spills on the enclosure floor. Floor drain will remove some of the oil. It is conservatively assumed that some of the oil will burn in the enclosure.
2. The maximum rate of burn equals 5 " per hour.
3. The oil may burn in excess of 3 hours, at which time the enclosure is assumed to fail. Consequences of failed enclosure is beyond the scope of this Appendix A "FHA" report.
4. During the 3 hours before the failure of the enclosure, 900 gallons of oil is consumed. The remaining oil will be contained within the bottom part or sump section of the enclosure.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A <br> Section F.2 Tab 7 |
| :--- | :---: | :--- |

14.1 DBF Fire Loading $\quad 675,000$ Btu/Sq.Ft.
14.2 Duration of Fire

3 Hours
$2,650{ }^{\circ} \mathrm{F}$
(Five hours without any means of fire protection)

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of the diesel oil day tank and oil.
15.2 Loss of the instruments, lighting and cable in the tank vault.
15.3 Safe shutdown can be accomplished using the redundant diesel fuel oil day tank which is located outside the 3 hour barrier. (The redundant fuel oil day tank may be lost if fire is not controlled within three hours).
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Possible loss of the day tank, instruments and oil.
16.2 Safe shutdown can be accomplished using the redundant diesel train which is located outside the 3 hour barrier.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Vault contains a floor drain which discharges into the sump in the storage tank vault at the (-) 16'-0" level, therefore damage due to water is of no consequence.

### 18.0 Containing Design Basis Fire in the Fire Area/Zone

18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 In the event the fire brigade cannot extinguish the fire the rate of rise detectors will set off the water deluge fire protection system.
18.3 If deluge system fails then fire will be put out by stand pipe and hose reels.
19.0 How the Redundant Safe Shutdown Equipment in the Area is Protected
19.1 There is no redundant safe shutdown equipment in this fire area. (Refer 15.3 above). If in unlikely event both diesel generator day tanks are lost as fire burns beyond three hours, safe shutdown of reactor will be achieved either from control room or RSS panel.


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 6 <br> Section F.2 Tab 7 <br> Page 2 of 2 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ | $\underline{\text { System Train }}$ | Safety <br> Related |  |
| :--- | :---: | :---: | :---: | :---: |
| Air Intake Filter F-36Z | DG | X | $\underline{B}$ | $\underline{\mathrm{X}}$ |
| Exhaust Silencer DG | X |  | X |  |
| MM-8A |  |  |  |  |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 7 |  |  |
| Page 1 of 2 |  |  |

Fire Hazard Analysis - DG-F-3F-A
1.0 Building
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location

Drawing No
Fire Hazard Analysis - DG-F-3F-A

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Page 1 of 2
3.0 Construction of Area

| 3.1 | Walls |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
|  |  | North | Concrete/MCG | 3 Hr . |
|  |  | South | Concrete | Outside |
|  |  | East | Concrete/MCG | 3 Hr . |
|  |  | West | Concrete/MCG | Outside/3 Hr. |
| 3.2 | Floor |  | Concrete | 3 Hr . |
| 3.3 | Ceiling |  | Concrete | Outside |
| 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . / 1^{11 / 2} \mathrm{Hr}$. (Stairs) |
| 3.5 | Others |  | - | - |

4.0 Floor Area 2,050 Sq. Ft. Length Varies Width Varies Height 25'
5.0 Volume $\quad 51,250 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear __ Non-Nuclear X_None __
7.0 Exhaust Ventilation System None
7.1 Percentage of System's Capacity _-
8.0 8 Hr . Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points


$$
\begin{aligned}
& \text { No } \mathrm{X} \\
& \text { No }
\end{aligned}
$$

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ No $\frac{\mathrm{X}}{\text { No }} \mathrm{X}$
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

### 11.0 Fire Loading in Area

11.1 None X (No Further Analysis Required)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A <br> STATION |
| :--- | :---: | :--- |
| Fection F.2 Tab 7 |  |  |
| Page 2 of 2 |  |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ | $\underline{l}$ System Train | Safety <br> Related |  |
| :--- | :--- | :--- | :---: | :---: |
| Air Intake Filter F-36B | DG |  | $\underline{B}$ | $\underline{X}$ |
| Exhaust Silencer DG |  | X | X |  |
| MM-8B |  |  |  |  |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Aection F.2 Tab 7 <br> Page 1 of 2 |
| :--- | :---: | :--- |

Fire Hazard Analysis - DG-F-S1-0
1.0 Building
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location Drawing No

Diesel Generator Building
DG-F-S1-0
Stairwell
Col. A-9
9763-F-202068-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\frac{\text { Outside }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |
| 3.2 | Floor |  | $\frac{\text { Concrete }}{\text { CHr. }}$ |  |
| 3.3 | Ceiling |  | $\frac{\text { Concrete }}{\text { Metal }}$ | $\frac{\frac{\text { Outside }}{\text { Outside }}}{3.4}$ |
| Doors |  |  |  |  |
| 3.5 | Others |  | - | $\frac{\frac{\text { Outside }}{11 / 2 H r .}}{\square}$ |

4.0 Floor Area 137 Sq. Ft. Length 16'-4" Width 8'-4" Height 43'
5.0 Volume $\quad 5,890 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear __ Non-Nuclear X_None_
7.0 Exhaust Ventilation System None
7.1 Percentage of System's Capacity N/A
8.0 8 Hr . Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points
$\begin{array}{ll}\text { Yes } \\ \text { Yes } & \\ \end{array}$

$$
\begin{aligned}
& \text { No } \mathrm{X} \\
& \text { No }
\end{aligned}
$$

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ No X
9.2 Airborne

Yes $\qquad$ No X
10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary
10.3 Detection

Portable Extinguisher(s)
Hose Station
10.4 Other

None
------

### 11.0 Fire Loading in Area

11.1 None X (no further analysis required)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 6 <br> Section F.2 Tab 7 <br> Page 2 of 2 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No Safety Related or Safe Shutdown Equipment in This Area

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 7 <br> Page 1 of 2 |  |  |

Fire Hazard Analysis - DG-F-S2-0

| 1.0 |  |  |
| :--- | :--- | :--- |
| Building |  |  |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Diesel Generator Building
DG-F-S2-0
Stairwell
Col. E-9
9763-F-202068-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\frac{\text { Material }}{\text { Concrete }}}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- |
| 3.2 | Floor |  | $\frac{\text { Concrete }}{\text { Concrete }}$ |
| 3.3 | Ceiling |  |  |
| 3.4 | Doors |  | $\frac{\text { Concrete }}{\text { Metal }}$ |
| 3.5 | Others |  |  |

4.0 Floor Area 137 Sq. Ft. Length $16^{\prime}-6^{\prime \prime}$ Width $8^{\prime}-4{ }^{\prime \prime}$ Height $\underline{11^{\prime}-6 " \prime}$
5.0 Volume $\quad 9,795 \mathrm{Cu} . \mathrm{Ft}$.

| 6.0 | Floor Drains | Nuclear | Non-Nuclear |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 7.0 | Exhaust Ventilation System |  |  | None | X None |
|  | 7.1 Perce | of System's Cap |  | N/A |  |
| 8.0 | 8 Hr . Emerge | ighting in Area | Yes | X | No |
|  | 8.1 Outsid | a at Exit Points | Yes | X | No |

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne

Yes
Yes $\qquad$
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Type
Portable Extinguisher(s)
Hose Station
None
------
11.0 Fire Loading in Area
11.1 None X_ (no further analysis required)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |$\quad$| Section F.2 Tab 7 |
| :--- |
| Page 2 of 2 |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

[^7]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 |
| :--- | :---: | :--- |
| STATION | Appendix A | Section F.2 Tab 8 <br> Page 1 of 3 |

PAB-F-1A-Z


### 11.0 Fire Loading in Area

11.1 Refer to pages 2 and 3.

[^8]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 |
| :--- | :---: | :--- |
| STATION | Appendix A | Section F.2 Tab 8 <br> Page 2 of 3 |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Cabling | SW | X | X | X |
| Cabling | CC | X | X | X |
| Cabling | CS | X | X | X |
| Cabling | SWA | X | X | X |
| Cabling | EDE | X | X | X |
| Cabling | EAH |  | X | X |
| Cabling | PAH |  | X | X |
| Piping, Valves \& Instrumentation | CC | X | X | X |
| Piping, Valves \& Instrumentation | CS | X | X | X |
| Instrument Rack IR-L7 | MM | X | X | X |
| Cabling | RC |  | X | X |
| Cabling | SI |  | X | X |
| Terminal Boxes | EDE | X | X | X |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
|  |  |
| Oil: | 6.0 |
|  |  |

Grease: Pounds
Class A: Pounds
Charcoal: Pounds
Chemicals: Pounds
Plastics: 28 Pounds
Resins:
Other:
13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| 176.5 | Btu/Sq. Ft. |
| ---: | :--- |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 71.4 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |


| 248 | Btu/Sq. Ft. |
| :--- | :--- |
| $1,264,000$ | Btu |


| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
| Fire Hazard Analysis - PAB-F-1A-Z |  |  |$\quad$| Page 3 of 3 Tab 8 |
| :--- |

### 14.0 Design-Basis Fire Description

(A) Conservatively assume both chiller pumps, chiller, both makeup water pumps and chromated water connection tank pump skid rupture simultaneously and spill over an area of 77 sq . ft . and burn.
(B) To add additional conservatism consider ventilation supply/exhaust air has been isolated.
14.1 DBF Fire Loading

11,688 Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. During Fire $585{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire $4 \frac{1}{2}$ Min.

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 The chiller, chiller pumps, chromated water pump, and the reactor makeup water pumps will be lost upon loss of oil.
15.2 Possible loss of some instruments and control devices.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 The chiller pumps, chromated water pump, and the reactor makeup water pumps may be lost.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable as no automatic water suppression system is provided in the zone.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Total combustibles will burn in less than five minutes. all surrounding zones/area are separated by concrete structures (many walls are fire rated), and hence the oil fire on 77 sq. ft . of the total 5100 sq . ft . area will be contained in the affected zone.
19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable as no redundant safe shutdown equipment is located in the same fire zone.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A <br> StATION |
| :--- | :---: | :--- |
| Fire Hazard Analysis - PAB-F-1B-Z |  |  |$\quad$| Page 1 of 2 Tab 8 |
| :--- |

PAB-F-1B-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building
PAB-F-1B-Z
Demin. Filter and Valve Maint. Area
West Side - El. (-) 6'0" To 7'0'"
9763-F-805061-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete }}{\text { Concrete }}$ <br> 3.2 |
| :--- | :--- | :--- | :--- |
| 3.3 | Floor |  | $\frac{\text { Concrete }}{\text { Concrete }}$ |
| 3.4 | Doors |  | $\frac{\text { Concrete }}{\text { Metal }}$ |
| 3.5 | Others |  | $\frac{\text { Exposed Ceiling }}{}$ |


4.0 Floor Area 2,900 Sq. Ft. Length 82' Width 35.5' Height Varies
5.0 Volume $\quad 61,000 \mathrm{Cu} . \mathrm{Ft}$.
7.0 Exhaust Ventilation System PAB
7.1 Percentage of System's Capacity $\underline{100 \%}$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes $\quad$ No $\quad \mathrm{X}$
8.1 Outside Area at Exit Points Yes X No
9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
Yes $\qquad$
No $\qquad$
9.2 Airborne
10.0 Fire Protection
10.1 Primary

Type
Fire Extinguisher(s)
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (No further analysis required)

Standpipe and Hose Reel
None
------

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev 6 <br> Section F.2 Tab 8 <br> Page 2 of 2 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety |
| :--- | :--- | :--- | :--- | :--- |
| Equipment | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No equipment required for safe shutdown in this zone also, no safety related equipment here.


| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 8 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
| Section F.2 Tab 8 |  |  |
| Fage 2 of 3 |  |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Charging Pump P-2A | CS | X |  | X | X |
| Piping \& Valves | CBS | X |  | X | X |
| Piping \& Valves | CS | X |  | X | X |
| Piping \& Valves | CC | X |  | X | X |
| Cabling | CS | X |  | X | X |
| Pressure Switches | CS | X |  | X |  |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area


28,744 Btu/Sq. Ft. $\xlongequal{9,150,000}$ Btu

### 14.0 Design-Basis Fire Description

1. Oil reservoir rupture, oil spreads over the entire floor area of the room ( 318 sq . ft .). The thickness of the oil film is $1 / 4$ " over the entire floor area.
2. The oil is ignited, burns and is consumed.
3. The space temperature is assumed to be sufficiently high that all the cable in the space will fail. Cable will not contribute to the fire because it is contained within conduit.
14.1 DBF Fire Loading

1,524 Btu/Sq. Ft.
14.2 Fire Duration
14.3 Peak Temperature

Less than one minute.
$5959{ }^{\circ} \mathrm{F}$ (High temp. spike in short duration).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 8 <br> Appendix A |
| :--- | :---: | :--- |
| StATION | Fire Hazard Analysis - PAB-F-1C-A | Sage 3 of 3 Tab 8 |

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of the pump due to rupture and loss of oil.
15.2 Loss of the cabling due to fire.
15.3 The adjacent fire area containing a redundant unit is separated by a 3-hour barrier; therefore safe shutdown can be accomplished.
15.4 The structural steel beams and metal partition are covered with a fire protective coating, therefore no damage.
15.5 There will be possible spalling of the concrete.
15.6 The fire will be contained within the area due to its short duration.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Loss of the pump due to rupture and loss of oil.
16.2 Possible loss of cabling to pump.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable (no water suppression in area).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire brigade will extinguish the fire using portable fire extinguishers or fire hoses if necessary.
18.3 Concrete walls and fire proofing on metal partition and exposed steel will limit the fire to the subject area.
18.4 Fire dampers in the ductwork will prevent the spread of fire to adjacent areas.
19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable (see 15.3).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 8 |
| :--- | :---: | :--- |
| Appendix A |  |  |
| STATION | Fire Hazard Analysis - PAB-F-1D-A | Sage 1 of 3 Tab 8 |

PAB-F-1D-A

11.0 Fire Loading in Area
11.1 Refer to page 2. (analysis continued pg. 2-4)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 8 <br> Appendix A |
| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - PAB-F-1D-A F.2 Tab 8 | Page 2 of 3 |

### 12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Charging Pump P-2b | CS |  | X | X | X |
| Piping \& Valves | CBS |  | X | X | X |
| Piping \& Valves | CS |  | X | X | X |
| Piping \& Valves | CC |  | X | X | X |
| Cabling | CS |  | X | X | X |
| Press Switches | CS |  | X | X |  |

### 13.0 Design Base Fire (In Situ)

13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

Fire Loading in Area

| 28,774 |
| :---: |
|  |
|  |
|  |
|  |
|  |
|  |

28,774 Btu/Sq. Ft. $9,150,000$ Btu

### 14.0 Design-Basis Fire Description

1. Oil reservoir rupture, oil spreads over the entire floor area of the room ( 318 sq . ft.). The thickness of the oil film is $1 / 4$ " over the entire floor area.
2. The oil is ignited, burns and is consumed.
3. The space temperature is assumed to be sufficiently high that all the cable in the space will fail. Cable will not contribute to the fire because it is contained within conduit.
14.1 DBF Fire Loading ${ }^{1,524}$ Btu/Sq. Ft. (3.23 gallons oil consumed in 318 sq. ft.)
14.2 Fire Duration Less than one minute.
14.3 Peak Temperature $\quad 5959{ }^{\circ} \mathrm{F}$ (High temp. spike in short duration).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 8 |
| :--- | :---: | :--- |
| Aptation | Fire Hazard Analysis - PAB-F-1D-A | Section F.2 Tab 8 <br> Page 3 of 3 |

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of the pump due to rupture and loss of oil.
15.2 Loss of the cabling due to fire.
15.3 The adjacent fire area containing a redundant unit is separated by a 3-hour barrier; therefore, safe shutdown can be accomplished.
15.4 The structural steel beams and metal partition are covered with a fire protective coating, therefore no damage.
15.5 There will be possible spalling of the concrete.
15.6 The fire will be contained within the area due to its short duration.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of the pump due to rupture and loss of oil.
16.2 Possible loss of cabling to pump.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable (no water suppression in area).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The Control room alerts the fire brigade.
18.2 The fire brigade will extinguish the fire using portable fire extinguishers or fire hoses if necessary.
18.3 Concrete walls and fire proofing on metal partition and exposed steel will limit the fire to the subject area.
18.4 Fire dampers in the ductwork will prevent the spread of fire to adjacent areas.
19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable (see 15.3).

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev 6 <br> Section F.2 Tab 8 <br> Page 1 of 3 |
| :--- | :---: | :--- |

PAB-F-1E-A
$\begin{array}{ll}1.0 & \text { Building } \\ 2.0 & \text { Fire Area or Zone }\end{array}$
2.1 Area Name
2.2 Location Drawing No

Primary Auxiliary Building
PAB-F-1E-A
Reciprocating Charging Pump Area

| East Side - El. 7'0" |
| :--- |
| 9763-F-805061-FP |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire }}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 272 Sq. Ft. Length 26.5' Width $\underline{10.25^{\prime}}$ Height $\underline{15.25^{\prime}}$
5.0 Volume $\quad 4,100 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None_ None ___
7.0 Exhaust Ventilation System PAB
7.1 Percentage of System's Capacity $\underline{100 \%}$
8.0 8 Hr . Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes

| No X |
| :--- |
| No X |

9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
9.2 Airborne
Yes
No $\qquad$
10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary
10.3 Detection
10.4 Other

Fire Extinguisher(s)
Standpipe and Hose Reel Ionization
------
11.0 Fire Loading in Area
11.1 Refer to page 2. (analysis continued pg. 2-4)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1,, | Rev 6 <br> Appendix A <br> Pection F.2 Tab 8 |
| :--- | :---: | :--- |

### 12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |  |
| No Equipment Required For Safe Shutdown in This Area |  |  |  |  |  |
| Piping Valves | CBS | X |  | X |  |
| Piping Valves | CC | X |  | X |  |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
| Oil: | 14.0 Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |

Other:
13.2 Total Fire Loading in Area:

Total Combustibles:
Fire Loading in Area
$\qquad$

| $\frac{7721}{}$ | Btu/Sq. Ft. |
| ---: | :--- |
| $2,200,000$ | Btu |

### 14.0 Design-Basis Fire Description

1. Pump ruptures, oil spread over floor covering 605 sq . Ft. Of area ( $1 / 8^{\prime \prime}$ thick).
2. Oil is ignited and is consumed.
3. The space temperature in the area is assumed to be sufficiently high that all the cable in the space is assumed to fail. Cable will not contribute to the fire because it is contained within conduit.
14.1 DBF Fire Loading $\quad 2,275$ Btu/Sq. Ft. (2.73 gallons oil consumed in 318 sq. ft.)
14.2 Fire Duration Less than one minute.
14.3 Peak Temperature $\quad 5958{ }^{\circ} \mathrm{F}$ (High temp. spike in short duration).

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1,, | Rev 6 <br> Appendix A <br> Section F.2 Tab 8 |
| :--- | :---: | :--- |

15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of the pump due to rupture and loss of oil.
15.2 Loss of cabling due to fire.
15.3 The adjacent fire area containing safe shutdown equipment will not be affected.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of the pump due to rupture and loss of oil.
16.2 Possible loss of cabling to pump.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable (no water suppression in area).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Duration of the fire is short, therefore the fire barrier walls will prevent the spread to adjacent pump areas.
18.2 Fire dampers will prevent the spread of fire from the area.
19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable (see 15.3).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 7 <br> Appendix A |
| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - PAB-F-1F-Z | Section F.2 Tab 8 <br> Page 1 of 3 |

## PAB-F-1F-Z

$\begin{array}{ll}1.0 & \text { Building } \\ 2.0 & \text { Fire Area or Zone }\end{array}$
2.1 Area Name
2.2 Location Drawing No

Primary Auxiliary Building
PAB-F-1F-Z
Letdown Degasifier Area

| East Side El. 7'0"' |
| :--- |
| 9763-F-805061-FP |

3.0 Construction of Area

|  |  |  | Material | Min. Fire |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Concrete | $11 / 2 \mathrm{Hr}$. |
|  |  | South | Concrete | - |
|  |  | East | Concrete | Outside |
|  |  | West | Concrete | - |
| 3.2 | Floor |  | Concrete | - |
| 3.3 | Ceiling |  | Concrete/Grating | - |
| 3.4 | Doors |  | Metal | - |
| 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area $\quad 9,400$ Sq. Ft. Length 23.5' Width $13.33^{\prime}$ Height $30^{\prime}$
5.0 Volume $\quad 9,400 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_Nonent None_
7.0 Exhaust Ventilation System PAB
7.1 Percentage of System's Capacity $\underline{100 \%}$
8.0 8 Hr . Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes -

| No X |
| :--- |
| No X |

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes
9.2 Airborne

Yes (Minimal)
No X
No
10.0 Fire Protection
10.1 Primary

Type
Fire Extinguisher(s)
10.2 Secondary
10.3 Detection
10.4 Other

Standpipe and Hose Reel Ionization
------
11.0 Fire Loading in Area
11.1 Refer to page 2. (analysis continued pg. 2 \& 3)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1,, | Rev 7 <br> Appendix A <br> Pection F.2 Tab 8 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No equipment required for safe shutdown in this zone also, no safety related equipment here.
13.1 Combustible in Area (In Situ) Fire Loading in Area

| Note: | Oil Fire |
| :--- | :--- |
| Oil: | 1.0 |
| Gallons |  |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |


| 13.2 | Total Fire Loading in Area: | 478 | $\mathrm{Btu} / \mathrm{Sq}. \mathrm{Ft}$. |
| :--- | :--- | ---: | :--- |
| Total Combustibles: | $-150,000$ | Btu |  |


| Fire Loading in Area |  |
| ---: | ---: |
| 478 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

$\begin{array}{rl}478 & \mathrm{Btu} / \mathrm{Sq} . \text { Ft. } \\ 150,000 & \mathrm{Btu}\end{array}$

### 14.0 Design-Basis Fire Description

(A) The letdown degasifier reciprocating pump will rupture, the entire contents of oil spills on the floor covering approximately a 13 sq . ft. area and burns completely.
14.1 DBF fire loading

$$
11,538 \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft} .
$$

14.2 Peak area/zone temperature during fire

$$
505{ }^{\circ} \mathrm{F}
$$

14.3 Duration of fire

$$
41 / 2 \text { Minutes }
$$

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of degasifier pump due to loss of oil.
15.2 Possible loss of the cabling and instrumentation/controls in the area.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 The consequences are the same as 15.1 and 15.2.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable as no automatic water suppression system is provided.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev 7 <br> Section F.2 Tab 8 <br> Page 3 of 3 |
| :--- | :---: | :--- |

18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire brigade will extinguish the fire using portable fire extinguishers or fire hoses if necessary.
18.3 Because the subject fire zone is bounded by a concrete structure and the duration of the fire is less than 5 minutes, the design base fire will be contained in the area. However, with the lack of fire dampers in the supply or exhaust air system, the hot air and smoke will travel through PAB normal exhaust filter unit to the outside. (The air has not been transferred from this zone to any other zones in PAB).
19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable. No safe shutdown equipment in the area.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 |
| :--- | :---: | :--- |
| STATION | Appendix A | Section F.2 Tab 8 <br> Page 1 of 2 |

PAB-F-1G-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building
PAB-F- 1G-A
Electrical Chase \& Elec. Tunnel Between Control Bldg \& PAB ${ }^{*}$
El. (-) 26'-0" To El. 35'-3" \& 30'08"
9763-F-805061-FP. 805062-FP \& 805060-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete/MCG }}{\text { Concrete }}$ |
| :--- | :--- | :--- | :--- |
| 3.2 | Floor |  | $\frac{\text { Concrete/MCG }}{\text { Concrete }}$ |
| 3.3 | Ceiling |  | $\frac{\text { Concrete }}{\text { Metal }}$ |
| 3.4 | Doors |  |  |
| 3.5 | Others |  | $\frac{-}{-}$ |

4.0 Floor Area 1,120 Sq. Ft. Length $80^{\prime}-0^{\prime \prime}$ Width $14^{\prime}-0^{\prime \prime}$ Height $20^{\prime}-0^{\prime \prime}$
5.0 Volume 22,400; 31,400; 9000 Cu . Ft.
6.0 Floor Drains Nuclear __ Non-Nuclear X None ___
7.0 Exhaust Ventilation System None
7.1 Percentage of System's Capacity N/A
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes $\qquad$ No X
No X
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No |
| :--- |
| No |

10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary
10.3 Detection

Pre-Action Systems
10.4 Other

Fire Extinguisher(s)
Ionization \& Photoelectric
------
11.0 Fire Loading in Area
11.1 None X_ (no further analysis required)

* Safety Related Cable Requires Fire Protection.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1,, | Rev 6 <br> Appendix A <br> Section F.2 Tab 8 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | CC | X | X | X | X |
| Cabling | CS | X | X | X | X |
| Cabling | EAH | X | X | X | X |
| Cabling | SI | X | X | X |  |
| Cabling | PAH | X | X | X | X |
| Cabling | SW | X | X | X | X |
| Cabling | SWA | X | X | X |  |
| Cabling | RH | X | X | X |  |
| Cabling | RC | X | X | X |  |
| Cabling | CBS | X | X | X |  |
| Cabling | FAH | X | X | X |  |
| Cabling | WLD | X |  | X |  |
| Cabling | SF | X | X | X |  |
| Cabling | VG | X |  | X |  |
| Cabling | SS |  | X | X |  |
| Cabling | NG | X |  | X |  |
| Cabling | RMW |  | X | X |  |
| Cabling | CAH | X | X | X |  |


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| :--- | :---: | :--- |

PAB-F-1J-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building
PAB-F-1J-Z
Aux. Steam Condensate Tank Area

| North End PAB El. (-) 6'-0: \& (-) 26'-0"' |
| :--- |
| $9763-$ F-805061-FP |

3.0 Construction of Area

|  |  |  | Material | Min. Fire Ratin |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Concrete | $3 \mathrm{Hr} . / \mathrm{Outside}$ |
|  |  | South | Concrete | - /Outside |
|  |  | East | Concrete | - $/ 3 \mathrm{Hr}$. |
|  |  | West | Concrete | $3 \mathrm{Hr} . / \mathrm{Outside}$ |
| 3.2 | Floor |  | Concrete/Grating | - |
| 3.3 | Ceiling |  | Concrete | - |
| 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . /-$ |
| 3.5 | Others |  | - | - |

4.0 Floor Area 1,980 Sq. Ft. Length Varies Width Varies Height $11^{\prime} \& 18^{\prime}$
5.0 Volume $\quad 23,782 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_Non-Nuclear ___ None __
7.0 Exhaust Ventilation System PAH
7.1 Percentage of System's Capacity $\quad 100 \%$
$8.0-8 \mathrm{Hr}$. Emergency Lighting in Area
8.1 Outside Area at Exit Points Yes
No
No X
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 Refer to page 2 of 4

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev 7 <br> Section F.2 Tab 8 <br> Page 2 of 3 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Piping \& Valves | CS | X | X | X |
| Cabling | CS | X | X | X |
| Piping \& Valves | SI | X | X | X |
| Cabling | SI | X | X | X |
| Cabling | RC | X | X | X |
| Cabling | CC | X | X | X |
| Cabling | CAH | X | X | X |
| Cabling | VG | X |  | X |
| Cabling | CBS | X |  | X |
| Cabling | NG | X |  | X |
| Cabling | RMW |  | X | X |
| Cabling | WLD |  | X | X |
| Temperature Elements \& Cabling | MM | X | X | X |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |  |
| :---: | :---: | :---: |
| Oil: | 1.0 | Gallons |
| Grease: |  | Pounds |
| Class A: |  | Pounds |
| Charcoal: |  | Pounds |
| Chemicals: |  | Pounds |
| Plastics: | 5 | Pounds |
| Resins: |  | Pounds |

Other:
13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area


| 109 |
| :--- |
| 215,000 |
| Btu/Sq. Ft. |


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| :--- | :---: | :--- |

14.0 Design-Basis Fire Description
(A) The condensate pump oil reservoir will rupture and oil spills on an area of 13 sq . Ft., ignites and burns completely.
14.1 DBF Fire Loading $\quad 11,538$ Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. During Fire $309{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire $4 \frac{1}{2}$ Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of condensate pump as a result of the loss of oil content.
15.2 Because of the non-ducted exhaust air from the area and the lack of fire dampers, smoke and fire will spread into the upper zones of PAB, via PAB-F-1A-Z, PAB-F-2C-Z, PAB-3B-Z.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of the condensate pump as a result of the loss of oil content.
16.2 Area detection system will alarm in control room and early response of the fire brigade will minimize the spread of smoke and fire to the upper zones.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable as no automatic water suppression system exists.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 The subject pumps are located in a pit at elevation of $26^{\prime}-0^{\prime \prime}$. The localized zone is bounded by a concrete structure and most of the fire will be contained. However, because of the lack of isolation of ventilation air and non-ducted exhaust air, fire and particularly smoke will spread to the other parts of the building, including the component cooling heat exchanger and pump area.

### 19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected

1. Not applicable. The separation of the safe shutdown equipment is discussed in the report "Fire Protection of Safe Shutdown Capability" (10 CFR 50 Appendix R).

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev 6 <br> Section F.2 Tab 8 <br> Page 1 of 2 |
| :--- | :---: | :--- |

## PAB-F-1K-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building
PAB-F-1K-Z
Non-Radioactive Pipe Tunnels \& Pine Chase
Northwest Corner - El. (-)6'-O" Up Thru 53'-O"
9763-F-805061-FP, 809062-FP \& 805063-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete }}{\text { Concrete }}$ |
| :--- | :--- | :--- | :--- |
| 3.2 | Floor |  | $\frac{\text { Concrete }}{\text { Concrete }}$ |
| 3.3 | Ceiling |  |  |
| 3.4 | Doors |  | $\frac{\text { Concrete }}{\text { Metal }}$ |
| 3.5 | Others |  | - |

4.0 Floor Area 4,620 Sq. Ft. Length 68'-0" Width $9^{\prime}-0^{\prime \prime} \& 15 '_{\prime}^{\prime \prime}$ Height Varies
5.0 Volume $\quad 75,350 \mathrm{Cu} . \mathrm{Ft}$.
(El (-)6',5'
6.0 Floor Drains Nuclear X_\& 53') Non-Nuclear ___
7.0 Exhaust Ventilation System PAH-FN-L47
7.1 Percentage of System's Capacity $100 \%$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes $\qquad$

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection

Yes $\qquad$ | No |
| :--- |
| No |

10.4 Other

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
None - SBN-439, Dated $1 / 21 / 85$
-----------

[^9]| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev 6 <br> Section F.2 Tab 8 <br> Page 2 of 2 |
| :--- | :---: | :--- |

11.0 Fire Loading in Area
11.1 None X (no further analysis required)
12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ |  | System Train |  |
| :--- | :--- | :--- | :--- | :---: | | Safety |
| :---: |
| Piping \& Valves |


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| :--- | :---: | :--- |

PAB-F-2A-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building

| PAB-F-2A-Z |
| :--- |
| Resin Fill Tank Area |
| South-East El. 25'-0" |
| $9763-F-805062-F P$ |

3.0 Construction of Area

4.0 Floor Area 1,550 Sq. Ft. Length 43.5' Width 38.5' Height 26'
5.0 Volume $\quad 40,400 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_Nonent None_
7.0 Exhaust Ventilation System PAB
7.1 Percentage of System's Capacity $100 \%$
8.0 8 Hr. Emergency Lighting in Area Yes X No $\qquad$
8.1 Outside Area at Exit Points Yes X

No
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\quad \mathrm{X}$
No
9.2 Airborne

Yes
No X
10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary
10.3 Detection
10.4 Other

Fire Extinguisher(s)
Standpipe and Hose Reel Ionization
-----
11.0 Fire Loading in Area
11.1 Refer to page 2. (analysis continued page 2 \& 3).

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 16 <br> Appendix A <br> Section F.2 Tab 8 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{\text { System Train }}$ |  | Safety <br> Related |
| :--- | :--- | :--- | :---: | :---: |
| Cabling | SW | X | X | X |
| Cabling | SWA | X | X | X |
| Cabling | EDE | X | X | X |
| Cabling | EAH |  | X | X |
| Cabling | PAH | X | X | X |
| Damper DP-35A | PAH | X |  | X |
| Cabling | CS | X | X | X |
| Cabling | FAH |  | X | X |
| Cabling | CC |  | X | X |
| Cabling | SF |  | X | X |
| Sample Panel CP-482 | SS |  | X | X |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

| Note: |  |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | $=$ Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: | $=$ |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area


| 889 | Btu/Sq. Ft. |
| ---: | :--- |
| $1,378,000$ <br> Btu |  |


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| :--- | :---: | :--- |

### 14.0 Design-Basis Fire Description

1. For conservatism the ladders are assumed to be in a vertical position. The bottom of both sets of rails are ignited and burn upward.
2. To add conservatism, it is assumed that the fire is self sustaining although the fire is not severe and has a low heat release rate.
3. The fire area will be limited to the length of the ladder and about 2 feet from the wall for an area covering $30 \mathrm{ft} . \mathrm{x} 2 \mathrm{ft} .=60 \mathrm{sq} . \mathrm{ft}$.
14.1 DBF fire loading $\quad 22,967$ Btu/Sq. Ft.
14.2 Peak area/zone temperature during fire $\quad 147{ }^{\circ} \mathrm{F}$
14.3 Duration of fire $>5$ Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Refer to Seabrook Station Fire Protection of Safe Shutdown Capability ( 10 CFR 50, App. R).

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 No consequences. Fire will be extinguished with portable extinguishers.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire would be extinguished using portable extinguishers and/or hose lines.
19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Refer To Seabrook Station Fire Protection of Safe Shutdown Capability (10 CFR 50, App. R).

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| STATION | Fire Hazard Analysis - PAB-F-2B-Z | Rection F.2 Tab 8 <br> Page 1 of 2 |

PAB-F-2B-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building
PAB-F-2B-Z
Boric Acid Tank Area

| South-West El. 25'-O" |
| :--- |
| $9763-F-805062$-FP |

3.0 Construction of Area

3.1 \begin{tabular}{llll}

Walls \& \begin{tabular}{l}
North <br>
South <br>
East <br>
West

 \& 

$\frac{\text { Material }}{\text { Concrete/Metal }}$ <br>

| Concrete |
| :--- | :--- | :--- | <br>

3.2

 \& 

Floor <br>
3.3
\end{tabular} <br>

Cencrete/Metal <br>
3.4 \& Doors <br>
3.5 \& Others \& \& $\frac{\text { Concrete }}{\text { Concrete }}$ <br>
Oetal <br>
Exposed Ceiling Beams
\end{tabular}

Min. Fire Rating | Outside |
| :--- |
| $\frac{-}{3 \mathrm{Hr} .}$ |
| $\frac{-}{3 \mathrm{Hr} . /-}$ |
| - |

4.0 Floor Area $\quad 1,300$ Sq. Ft. Length Varies Width Varies Height 26'
5.0 Volume $\quad 33,800 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None_ None_ _ _
7.0 Exhaust Ventilation System PAB
7.1 Percentage of System's Capacity $\quad 100 \%$
8.0 8 Hr. Emergency Lighting in Area Yes X No $\qquad$
8.1 Outside Area at Exit Points

Yes
X
No $\qquad$
9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
No $\qquad$
9.2 Airborne
Yes
No X
10.0 Fire Protection
10.1 Primary

Type
Fire Extinguisher(s)
10.2 Secondary
10.3 Detection
10.4 Other

Standpipe and Hose Reel Ionization
-----
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
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| STATION | Fire Hazard Analysis - PAB-F-2B-Z | Rection F.2 Tab 8 <br> Page 2 of 2 |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Piping \& Valves | CS | X | X | X | X |
| Cabling | CS | X | X | X |  |
| Boric Acid Tanks | CS | X | X | X |  |


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| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - PAB-F-2C-Z | Sage 1 of 4 <br> Pab 8 |

PAB-F-2C-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building
PAB-F-2C-Z
Primary Component Cooling Pump Area
North - El 25'-0"
9763-F-805062-FP
3.0 Construction of Area

4.0 Floor Area 7,200 Sq. Ft. Length Varies Width Varies Height 26'
$5.0 \quad$ Volume $\quad 187,000 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_Non None_ ___
7.0 Exhaust Ventilation System PAB
7.1 Percentage of System's Capacity $100 \%$
8.0 8 Hr. Emergency Lighting in Area Yes X No $\qquad$
8.1 Outside Area at Exit Points Yes X

No
9.0 Operational Radioactivity

| 9.1 | Equipment/Piping | Yes | X | No |
| :--- | :--- | :--- | :--- | :--- |
| 9.2 | Airborne | Yes |  | No_ $\quad \mathrm{X}$ |

10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary
10.3 Detection

Pre-Action System
10.4 Other

Fire Extinguisher(s)
Ionization \& Photoelectric
-----
11.0 Fire Loading in Area
11.1 Refer to page $\qquad$ (analysis continued pg. 2-4)

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| Section F.2 Tab 8 |  |  |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Pump P-11A, P-11C | CC | X |  | X |
| Cabling | CC | X | X | X |
| Pump P-11B, P-11D | CC |  | X | X |
| Piping \& Valves | CC | X | X | X |
| Piping \& Valves | SW | X | X | X |
| Instrument Rack IR-93 | MM | X | X | X |
| Cabling | CS | X | X | X |
| Cabling | SW | X | X | X |
| Cabling | SWA | X | X | X |
| Cabling | EAH | X | X | X |
| Cabling | SI | X | X | X |
| Cabling | PAH | X | X | X |
| Cabling | RM | X | X | X |
| Terminal Boxes \& Cabling | EDE | X | X | X |
| Piping \& Valves | CS | X | X | X |
| Fan-FN-42A | PAH | X |  | X |
| Fan-FN-42B | PAH |  | X | X |
| Dampers | PAH | X | X | X |
| Instruments | PAH | X | X | X |
| Instruments | PAH | X | X | X |


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| :--- | :---: | :--- |
| Fire Hazard Analysis - PAB-F-2C-Z |  |  |$\quad$| Page 3 of 4 |
| :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Radiation Monitors | RM | X | X | X |
| Cabling | CBS | X | X | X |
| Cabling | CAP | X | X | X |
| $\begin{aligned} & \text { PCCW HX-CC-E-17A } \\ & \& ~ B \end{aligned}$ | CC | X | X | X |
| Boron Injection TK-SI-TK-6 | SI | X | X | X |
| Piping \& Valves | SI | X | X | X |
| Cabling | COP | X | X | X |
| Control Panel CP-443A, B | CC | X | X | X |
| Temperature Elements \& Cabling | MM | X | X | X |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
| Oil: | 1.75 Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | $=$ |
| Other: |  |

13.2 Total Fire Loading in Area:

Total Combustibles:
Fire Loading in Area

| 36.5 | Btu/Sq. Ft. |
| :---: | :---: |
|  |  |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

[^10]| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 16 <br> Section F.2 Tab 8 <br> Page 4 of 4 |
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### 14.0 Design-Basis Fire Description

1. Oil reservoir ruptures, oil spreads over 16.0 sq. ft. of floor ( $1 / 8^{\prime \prime}$ thick).
2. Oil ignites, burns and is consumed.
14.1 DBF Fire Loading
11,688 Btu/Sq. Ft.
14.2 Peak Temperature
$146{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
$41 / 2$ Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of pump due to rupture.
15.2 Possible loss of pump cable.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of pump due to rupture.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 A double failure would be required to inadvertently spray water in area.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Duration of the fire is short.
18.2 Total fire loading in zone is light (36.5 Btu/Sq. Ft).
19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Spatial separation and metal shield wall.
19.2 The design base fire has neither the duration or intensity to ignite cable or damage equipment.
19.3 Water shields are installed over PCCW pump motors.

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| STATION | Fire Hazard Analysis - PAB-F-3A-Z | Section F.2 Tab 8 <br> Page 1 of 3 |

PAB-F-3A-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building
PAB-F-3A-Z
Water Cooler Heat Exchanger Area
North El. 53'-0"
9763-F-805063-FP
3.0 Construction of Area

4.0 Floor Area 4,000 Sq. Ft. Length $\quad$ 53' Width $\quad 75^{\prime} \quad$ Height $26^{\prime}$
5.0 Volume $\quad 103,400 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_Non None__
7.0 Exhaust Ventilation System PAB
7.1 Percentage of System's Capacity $\quad 100 \%$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes $\quad$ No $\quad$ X
8.1 Outside Area at Exit Points Yes X

$$
\begin{aligned}
& \text { No } \mathrm{No}^{\mathrm{X}} \\
& \hline
\end{aligned}
$$

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\quad \mathrm{X}$
No
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection

Yes $\qquad$ No X
10.4 Other

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
Ionization
Carbon Monoxide Detector in CAP-F-40
11.0 Fire Loading in Area
11.1 Refer to page 3 of 4

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| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - PAB-F-3A-Z | Section F.2 Tab 8 <br> Page 2 of 3 |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System |  | System Train |  |
| :--- | :--- | :--- | :---: | :---: | \(\left.\begin{array}{c}Safety <br>

Related\end{array}\right]\) Cabling
13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |  |
| :---: | :---: | :---: |
| Oil: | 2.25 | Gallons |
| Grease: |  | Pounds |
| Class A: |  | Pounds |
| Charcoal: | 6,600 | Pounds |
| Chemicals: |  | Pounds |
| Plastics: |  | Pounds |
| Resins: |  | Pounds |
| Other: |  |  |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

$84 \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft}$. 37,500 Btu

Charcoal Fire Loading Was Not Considered in Total Area. See Appendix D.

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14.0 Design-Basis Fire Description
(A) The flash tank distillate pump oil reservoir fails and the entire 2.25 gallon of oil spreads over $29 \mathrm{sq} . \mathrm{ft}$. and will ignite and is assumed to burn completely.
14.1 DBF Fire Loading $\quad 11,638$ Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. During Fire $240{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire $4 \frac{1}{2}$ Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of the flash tank distillate pumps as a result of the loss of oil.
15.2 Failure of instruments, controls and cabling within the area of immediate vicinity of the fire.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Loss of the flash tank distillate pumps as a result of the loss of oil.
16.2 The possible loss of instruments, controls and cabling within the area of immediate vicinity of the fire.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable as no automatic water suppression system exists.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 The fire duration is less than five minutes. The fire location is in the north east corner of the zone and is surrounded by outside fire rated concrete structures. Hence, the bulk of the fire will be contained within the zone. However, due to the lack of ventilation exhaust system isolation, the smoke will spread to fire zone PAB-F-3B-Z.
19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable. For the separation requirements refer to report "Fire Protection Of Safe Shutdown Capability (10 CFR 50, Appendix R)".

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PAB-F-3B-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building

PAB-F-3B-Z
PAB Supply and Exhaust Fan Area

| South Side El. 53'-0" |
| :--- |
| $9763-\mathrm{F}-805063-\mathrm{FP}$ |

3.0 Construction of Area

|  |  |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Metal/Open | - |
|  |  | South | Concrete | $\overline{\text { Outside/3 Hr. }}$ |
|  |  | East | Concrete | Outside/3 Hr. ${ }^{\text {r }}$ |
|  |  | West | Concrete | Outside/ - |
| 3.2 | Floor |  | Concrete | - |
| 3.3 | Ceiling |  | Concrete | -/Outside |
| 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . /-$ |
| 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area 6,600 Sq. Ft. Length $88^{\prime}$ Width ${ }^{75}$ Height ${ }^{26^{\prime}}$
5.0 Volume $\quad 171,600 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None_ None ___
7.0 Exhaust Ventilation System PAB
7.1 Percentage of System's Capacity $\underline{100 \%}$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes $\quad$ No $\quad \mathrm{X}$
8.1 Outside Area at Exit Points Yes X
No
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\quad \mathrm{X}$
No
No X
9.2 Airborne

Yes
10.0 Fire Protection
10.1 Primary

Type
Fire Extinguisher(s)
10.2 Secondary
10.3 Detection

Standpipe and Hose Reel
Ionization \& Photoelectric
10.4 Other
-----
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued pg. 2 \& 3)

[^11]| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Appendix A |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{l}$ System Train | Safety <br> Related |  |
| :--- | :--- | :--- | :---: | :---: |
| Piping \& Valves | CS | X | $\underline{\mathrm{B}}$ | $\underline{\mathrm{X}}$ |
| Cabling | CS | X | X | X |
| Instruments \& Cabling | CAP | X |  | X |
| Instruments \& Cabling | COP | X | X | X |
| Instruments \& Cabling | PAH | X |  | X |
| Temperature Elements \& | MM | X | X | X |
| Cabling |  |  |  | X |
| Instruments \& Cabling | CC | X | X | X |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area


| $\frac{1,633}{}$ | Btu/Sq. Ft. |
| :--- | :--- |
| $1,611,422$ | Btu |


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| :--- | :---: | :--- |

### 14.0 Design-Basis Fire Description

1. Oil reservoir in the monorail crane hoist ruptures and $1 / 2$ gallon of oil spills covering 6.4 sq. Ft. of the boric acid storage area floor. The oil runs under two stacked wood pallets, which has a burning area of 24 sq . Ft
2. The oil is ignited and burns along with the pallets.
3. Design basis fire is separated from the fan area by metal partitions.
14.1 DBF Fire Loading

28,386 Btu/Sq. Ft.
14.2 Peak Temperature
$1,560{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
4.8 Minutes.
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of monorail crane.
15.2 Loss of the boric acid storage area.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of monorail crane due to loss of oil.
16.2 Possible loss of boric acid storage area.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire brigade will extinguish the fire using portable fire extinguishers or fire hoses if necessary.
18.3 The fire rating of the structure exceeds the duration of the fire.
19.0 How is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable (equipment is not required for safe shutdown).

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| :--- | :---: | :--- |

PAB-F-4-Z

| 1.0 | Building |  |  | Primary Auxiliary Building |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | PAB-F-4-Z |  |
|  | 2.1 | Area Name |  | Filter Area |  |
|  | 2.2 | Location |  | El. 81'-0" |  |
|  |  | Drawing No |  | 9763-P-805063-FP |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire |
|  | 3.1 | Walls | North | Concrete | Outside |
|  |  |  | South | Concrete | Outside |
|  |  |  | East | Concrete | Outside |
|  |  |  | West | Concrete | Outside |
|  | 3.2 | Floor |  | Concrete | - |
|  | 3.3 | Ceiling |  | Concrete | Outside |
|  | 3.4 | Doors |  | Metal | - |
|  | 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area 2,650 Sq. Ft. Length $54^{\prime}$ Width ${\text { 49'_Height } 25^{\prime}}^{( }$
5.0 Volume $\quad 66,000 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None_ None_ ___
7.0 Exhaust Ventilation System Mechanical Room

| 8.0 | 8 Hr . Emergency Lighting in Area | Yes |  | No | X |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8.1 Outside Area at Exit Points | Yes | X | No |  |

9.0 Operational Radioactivity

| 9.1 | Equipment/Piping | Yes | No X |  |
| :--- | :--- | :--- | :--- | :--- |
| 9.2 | Airborne | Yes | $\square$ | No X |

10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary
10.3 Detection
10.4 Other

Fire Extinguisher(s)
Standpipe \& Hose Reel Ionization
Temperature Elements in Filters/ Carbon Monoxide Detection in PAH-F-16
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

[^12]| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
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12.0 Equipment and Systems in Fire Area/Zone *

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No safety related or safe shutdown equipment in this zone

[^13]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 |
| :--- | :---: | :--- |
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PAB-F-S1-0

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building
PAB-F-S1-0
Stairwell

| $\frac{\text { Col. C-1 }}{9763-F-805063-F P ~}$ |
| :--- |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\frac{\text { Material }}{\text { Concrete }}}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- |
| 3.2 | Floor |  | $\frac{\text { Concrete }}{\text { Concrete }}$ |
| 3.3 | Ceiling |  |  |
| 3.4 | Doors |  | $\frac{\text { Concrete }}{\text { Metal }}$ |
| 3.5 | Others |  |  |

4.0 Floor Area 127 Sq. Ft. Length $15^{\prime}-4{ }^{\prime \prime}$ Width $8^{\prime \prime-4 \prime \prime}$ Height $37^{\prime}$
5.0 Volume 4,700 Cu. Ft.
6.0 Floor Drains Nuclear _ Non-Nuclear _ _
7.0 Exhaust Ventilation System None
7.1 Percentage of System's Capacity N/A
8.0 8 Hr. Emergency Lighting in Area Yes X No
8.1 Outside Area at Exit Points Yes X

No
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
$\begin{array}{ll}\text { Yes } & \mathrm{X} \\ & \\ & \end{array}$
No $\qquad$
0.0 Fire Protection
10.1 Primary

Type
Portable Extinguisher
10.2 Secondary

Hose Station
10.3 Detection
10.4 Other

None
------
11.0 Fire Loading in Area
11.1 None X_ (no further analysis required)

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12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No safety related or safe shutdown equipment in this zone

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| :--- | :---: | :--- |
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PAB-F-S2-0

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Primary Auxiliary Building
PAB-F-S2-0
Stairwell
Col. D-6
9763-F-805063-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete }}{\text { Concrete }}$ <br> 3.2 |
| :--- | :--- | :--- | :--- |
| Concrete |  |  |  |
| 3.3 | Floor |  | $\frac{\text { Coiling }}{\text { Concrete }}$ |
| 3.4 | Doors |  | $\frac{\text { Concrete }}{\text { Metal }}$ |


$\frac{\text { Min. Fire Rating }}{\frac{3 \text { Hrs. }}{\frac{\text { Outside }}{}}}$| $\frac{3 \text { Hrs. }}{3 \text { Hrs. }}$ |
| :--- |
| $\frac{\text { Outside }}{\text { Outside }}$ |
| $\frac{11 / 2 \mathrm{Hr} .}{-}$ |


5.0 Volume 8,600 Cu. Ft.
6.0 Floor Drains Nuclear _ Non-Nuclear _ _
7.0 Exhaust Ventilation System None
7.1 Percentage of System's Capacity N/A
8.0 8 Hr. Emergency Lighting in Area Yes X No
8.1 Outside Area at Exit Points Yes X $\qquad$
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$
9.2 Airborne

Yes $\qquad$ | No X X |
| :--- |

10.0 Fire Protection
10.1 Primary

Type
Portable Extinguisher
10.2 Secondary
10.3 Detection

Hose Station
10.4 Other

None
-----
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

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12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No safety related or safe shutdown equipment in this zone

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Fire Hazard Analysis - FSB-F-1-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Fuel Storage Building
FSB-F-1-A
-----
El 7'-0", $10^{\prime \prime}-0$ ", 21'-6", 25"-0", 64"-0" \& 84'-0" 9763-F-805058-FP, 805059-FP \& 805084-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East | $\frac{\text { Material }}{\text { Concrete }}$ <br> West | $\frac{\text { Concrete }}{\text { Concrete }}$ |
| :--- | :--- | :--- | :--- | :--- |
| 3.2 | Floor |  | $\frac{\text { Min. Fire Rating }}{\text { MCG/Concrete }}$ |  |
| 3.3 | Ceiling |  | $\frac{\text { Concrete }}{\text { Concrete }}$ | $\frac{\frac{\text { Outside }}{\text { Outside }}}{3.4}$ |
| Doors |  |  |  |  |
| 3.5 | Others |  | $\frac{3 \text { Mr./Outside** }}{-}$ | $\frac{\frac{\text { Outside }}{\text { Outside }}}{3+}$ |

4.0 Floor Area 5,350 Sq. Ft. Length 93' Width Varies Height Varies
5.0 Volume 579,100 Cu . Ft.

| 6.0 | Floor Drains | Nuclear | X |  | Nuclear | , |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7.0 | Exhaust Ventilation System |  |  |  | FSB Normal Exhaust |  |  |
|  | 7.1 Percentage of System's Capacity |  |  |  | 100\% |  |  |
| 8.0 | 8 Hr . Emerge | Lighting in |  | Yes |  | No | X |
|  | 8.1 Outsid | a at Exit |  | Yes | X | No |  |

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
$\begin{array}{ll}\text { Yes } & \mathrm{X} \\ & \end{array}$
No $\qquad$

Type
Fire Extinguisher(s)
Standpipe \& Hose Reel Ionization
Carbon Monoxide Detector in FAH-F-41, 74

### 11.0 Fire Loading in Area

11.1 Refer to page 3 (analysis continued on pages 2, 3, 4).

* Walkway and piping tunnel between column A of FSB and column D of PAB has 3 hr . fire rated ceiling.
** 3 hr . fire rated fire damper has not been provided in exhaust duct to the point of connection at plant vent. Ref. To Deviation No. 1 SBN-904 Dated 12/2/85

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety |
| :---: | :---: | :---: | :---: | :---: |
|  | System | A | B | Related |
| Spent Fuel Pool P-10A | SF | X |  | X |
| Spent Fuel Pool P-10B | SF |  | X | X |
| Piping \& Valves | CC | X | X | X |
| Controls \& Instruments | FAH | X | X | X |
| FAH-FN-11A \& 124 | FAH | X |  | X |
| FAH - FN - 11B | FAH |  | X | X |
| Heaters | FAH | X | X | X |
| Filters 41, 71 | FAH | X | X | X |
| Dampers | FAH | X | X | X |
| Cabling | FAH | X | X | X |
| Cabling | CC | X | X | X |
| Spent Fuel Pool P-10C | SF | $\mathrm{X}^{\text {Note } 1}$ | $\mathrm{X}^{\text {Note } 1}$ | X |

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13.0 Total Fire Loading in Area
13.1 Combustible in Area (In Situ)

| Oil: | 323.7 | Gallons | 9,076 | Btu/Sq. Ft. |
| :---: | :---: | :---: | :---: | :---: |
| Grease: | 79.5 | Pounds | 268 | Btu/Sq. Ft. |
| Class A: | 10,078 | Pounds | 15,070 | Btu/Sq. Ft. |
| Charcoal: | 21,750 | Pounds | * | Btu/Sq. Ft. |
| Chemicals: | 0 | Pounds | 0 | Btu/Sq. Ft. |
| Plastics: | 138 | Pounds | 335 | Btu/Sq. Ft. |
| Resins: |  | Pounds |  | Btu/Sq. Ft. |
| Cables: | 22,803 | Pounds | 44,754 | Btu/Sq. Ft. |
| ML-2 |  | Pounds |  | Btu/Sq. Ft. |
| Hydraulic |  |  |  |  |
| Fluid | 17.5 | Gallons | 491 | Btu/Sq. Ft. |
| Total Fire L | ding in Ar |  | 69,502 | Btu/Sq. Ft. |
| Total Comb | ibles: |  | 369,835,500 | Btu |

### 14.0 Design-Basis Fire Description

1. One of the four (4) Spent Fuel Pool pumps ruptures, lubrication oil spills on floor. For conservatism, the lubrication oil from the other three (3) adjacent pumps are also considered as combustible; therefore, all four (4) gallons of lubrication oil are assumed spilled on floor covering an area of 40 sq . ft . The entire four (4) gallons of lubrication oil ignite and are consumed. The normal exhaust system fails. Oil thickness is $1 / 6$ inch.
2. Maximum peak temperature throughout the entire fire area will reach $160.6^{\circ} \mathrm{F}$ based on ( $\Delta \mathrm{T} 60.6^{\circ} \mathrm{F}+100^{\circ} \mathrm{F}$ ambient temperature).
Note 1: Fiberglass ladders not included since ladders will not ignite at the DBF peak temperature.

Note 2: Reactor Coolant Pump (RCP) motor lubrication oil not included since the lubrication oil is contained in a metal reservoir and the RCP motor is not in-service or available for service.

Note 3: Cask crane lubrication oil and hydraulic fluid not included since crane not normally energized and location of lubrication oil reservoir and hydraulic fluid.

[^15]| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 18 <br> Section F.2 Tab 9 <br> Page 4 of 4 |
| :--- | :---: | :--- |

14.1 DBF Fire Loading
14.2 Peak Temperature
14.3 Duration of Fire

15,000 Btu/Sq. Ft.
$161{ }^{\circ} \mathrm{F}$
5.775 Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of spent fuel pool pump due to loss of oil.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Fire duration will be short with peak temperature of $160^{\circ} \mathrm{F}$; hence, spent fuel pool pump might be lost.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable as no automatic suppression system exists in the area.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire duration is short and will be contained in the subject fire area of concrete structure.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable as pump is not required for safe shutdown.

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| :--- | :---: | :--- |

W-F-1A-Z

| 1.0 | Building |  |  | Waste Proce |
| :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | W-F-1A-Z |
|  | $\begin{aligned} & 2.1 \\ & 2.2 \end{aligned}$ | Area Name |  | Truck Bay |
|  |  | Location |  | South Side El |
|  |  | Drawing No |  | 9763-F-805 |
| 3.0 | Construction of Area |  |  |  |
|  |  |  |  | Material |
|  | 3.1 | Walls | North | Concrete |
|  |  |  | South | Concrete |
|  |  |  | East | Concrete |
|  |  |  | West | Concrete |
|  | 3.2 | Floor |  | Concrete |
|  | 3.3 | Ceiling |  | Concrete |
|  | 3.4 | Doors |  | Metal |
|  | 3.5 | Others |  | - |


4.0 Floor Area 2,050 Sq. Ft. Length 81.5' Width $\underbrace{25} \quad$ Height Varies
5.0 Volume $\quad 87,400 \mathrm{Cu}$. Ft.

| 6.0 | Floor Drains | Nuclear | X |  | uclear | ne |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7.0 | Exhaust Ventilation System |  |  |  | WPB Exhaust System |  |  |
|  | 7.1 Percentage of System's Capacity |  |  |  | 100\% |  |  |
| 8.0 | 8 Hr . Emergency Lighting in Area |  |  | Ye |  | No | X |
|  | 8.1 Outsid | a at Exit P |  | Yes |  | No | X |

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
$\begin{array}{ll}\text { Yes } & \mathrm{X} \\ & \\ & \end{array}$
No $\qquad$
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
Ionization
-----
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued pg. 2 \& 3)

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12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No Safety Related or Safe Shutdown Equipment in ThisArea
$13.0 \quad$ Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Class A Fire |
| :--- | ---: |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | 1,400 Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

$\frac{10,056}{20,614,076}$ Bu/Sq. Ft. $\overline{20,614,076}$ Btu

### 14.0 Design-Basis Fire Description

(A) This fire zone is not separated from adjacent fire zones (W-F-1A-Z, W-F-2A-Z, W-F-2B-Z, W-F-2C-Z and W-F-2D-Z) by fire rated walls and hence it is assumed that all combustibles in all these zones will ignite and burn simultaneously. Total combustibles are $28,744,076$ Btu spread over 1598 sq.ft. (fire loading 17,988 Btu/ft. ${ }^{2}$ ).
(B) These zones are non-safety related and hence additional combustibles due to cable loading will have no significance.
14.1 DBF Fire Loading
$\xrightarrow{17,988}$ Btu/Sq. Ft.
14.2 Peak Fire Temperature
$2,104{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire

28 Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 No safe shutdown or safety related equipment in the area.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 None

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Aptation |
| :--- | :---: | :--- |
| Apendix A |  |  |
| Section F.2 Tab 10 |  |  |
| Page 3 of 3 |  |  |

17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable. There is no water fire suppression in the subject area.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Spatial separation and the PAB's 3 hour barrier prevents loss of any safe shutdown, or safety-related function.
18.2 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.3 The fire brigade will extinguish the fire using portable fire extinguishers or hose reel, as necessary.
19.0 How the Redundant Safe Shutdown Equipment in the Area Is Protected
19.1 Not applicable (see 15.2).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
| Fire Hazard Analysis - W-F-1B-Z |  |  |$\quad$| Sage 1 of 2 Tab 10 |
| :--- |

W-F-1B-Z

| 1.0 | Building |  |  | Waste Processing Building |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | W-F-1B-Z |  |
|  | 2.1 | Area Name |  | Decontamination Area |  |
|  | 2.2 | Location |  | South Side El. 25'-0" |  |
|  | Drawing No |  |  | 9763-F-80 |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire Rating |
|  | 3.1 | Walls | North | Concrete | - |
|  |  |  | South | Concrete | Outside |
|  |  |  | East | Concrete | Outside |
|  |  |  | West | Concrete | - |
|  | 3.2 | Floor |  | Concrete | - |
|  | 3.3 | Ceiling |  | Concrete | - |
|  | 3.4 | Doors |  | Metal | - |
|  | 3.5 | Others |  | - | - |

4.0 Floor Area 500 Sq. Ft. Length $\underline{25 '}^{\prime}-6^{\prime \prime}$ Width $\underline{19 '}^{\prime}-6^{\prime \prime}$ Height $\underline{26 ' 0 \prime}^{\prime \prime}$
5.0 Volume $\quad 13,000 \mathrm{Cu} . \mathrm{Ft}$.

| 6.0 | Floor Drains | Nuclear | X |  | clear | ne |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7.0 | Exhaust Ventilation System |  |  |  | WPB Exhaust System |  |  |
|  | 7.1 Percentage of System's Capacity |  |  |  | . $01 \%$ |  |  |
| 8.0 | 8 Hr . Emergency Lighting in Area |  |  | Yes |  | No | X |
|  | 8.1 Outsid | a at Exit P |  | Yes |  | No | X |

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
$\begin{array}{ll}\text { Yes } & \mathrm{X} \\ & \\ & \end{array}$
No $\qquad$
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection

Type
Fire Extinguisher(s)
Standpipe and Hose Reel
10.4 Other

## Ionization

-----
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, |  |
| :--- | :---: | :--- |
| STATION | Appendix A | Rev. 6 <br> Section F.2 Tab 10 <br> Page 2 of 2 |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No Safety Related or Safe Shutdown Equipment in ThisArea

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 10 |  |  |
| Page 1 of 3 |  |  |

W-F-2A-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Waste Processing Building
W-F-2A-Z
Extruder/Evaporator Area
42'-5" Elev. Cols. "A" To "B" - "2" To " 3 " + 9763-F-805882-FP
3.0 Construction of Area

|  |  |  | Material | Min. Fire |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | 3'-0" Concrete | 3 Hrs. |
|  |  | South | 1'-6" \& 2'-6" Concrete | None |
|  |  | East | 2'-6" Concrete | None |
|  |  | West | 1'-6" Concrete | None |
| 3.2 | Floor |  | 2'-6" Concrete \& Open | None |
| 3.3 | Ceiling |  | 2'-6" Concrete | None |
| 3.4 | Doors |  | Open Access | None |
| 3.5 | Others |  | Ladder | None |

4.0 Floor Area 491 Sq. Ft. Length $\underline{27 \prime} / 14^{\prime}$ Width $\underline{18^{\prime} / 10^{\prime}}$ Height $\underline{10^{\prime}-6^{\prime \prime}}$
5.0 Volume 5,156 Cu. Ft.
6.0 Floor Drains Nuclear X Non-Nuclear $\qquad$ None $\qquad$
7.0 Exhaust Ventilation System Waste Solidification Exhaust System
7.1 Percentage of System's Capacity $\qquad$ 3\%
8.0 8 Hr. Emergency Lighting in Area Yes

8.1 Outside Area at Exit Points Yes $\qquad$ | No X |
| :--- |
| No X |

9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
No
No X
10.0 Fire Protection

Type
Water Deluge System
10.1 Primary
10.2 Secondary

Standpipe and Hose Reel Station
Ionization and Thermal
10.3 Detection
10.4 Other
----
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued pg. 2, 3 \& 4)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 7 <br> Section F.2 Tab 10 <br> Page 2 of 3 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety |
| :--- | :--- | :--- | :--- | :--- |
| Equipment | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No Safety Related or Safe Shutdown Equipment in ThisArea
13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Class A Fire |
| :---: | :---: |
| Oil: | 2.2 Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

$672 \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft}$.

### 14.0 Design-Basis Fire Description

(A) This fire zone is not separated from adjacent fire zones (W-F-1A-Z, W-F-1B-Z, W-F-2A-Z, W-F-2B-Z, W-F-2C-Z \& W-F-2D-Z) by fire rated walls and hence it is assumed that all combustibles in all these zones will ignite and burn simultaneously. Total combustibles are $32,155,000$ Btu spread over 1598 sq.ft. (fire loading 20,122 Btu/ $\mathrm{ft}{ }^{2}$ ).
(B) These zones are non-safety related and hence additional combustibles due to cable loading will have no significance.
14.1 DBF Fire Loading

20,122 Btu/Sq. Ft.
14.2 Peak Fire Temperature
14.3 Fire Duration
$3,112{ }^{\circ} \mathrm{F}$
10 Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of extruder/evaporator function.
15.2 No safe shutdown or safety related equipment in the area.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 7 <br> Section F.2 Tab 10 <br> Page 3 of 3 |
| :--- | :---: | :--- |

17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 No consequences.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire brigade will put out the fire with hose reels and/or portable extinguishers.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable (see 15.2).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
| Section F.2 Tab 10 |  |  |
| Page 1 of 3 |  |  |

W-F-2B-Z

| 1.0 | Building |  |  | Waste Processin |
| :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | W-F-2B-Z |
|  | $2.1$ | Area Name |  | Crystallizer Pum |
|  | $2.2$ | Location |  | 4.2'-5" Elev. Co |
|  |  | Drawing No |  | 9763-F-805882- |
| 3.0 | Construction of Area |  |  |  |
|  |  |  |  | Material |
|  | 3.1 | Walls | North | 1'-6" Concrete |
|  |  |  | South | 2'-6" Concrete |
|  |  |  | East | 1'-6" Concrete |
|  |  |  | West | 2'-6" Concrete |
|  | 3.2 | Floor |  | 2'-3" Concrete |
|  | 3.3 | Ceiling |  | 2'-0" Concrete |
|  | 3.4 | Doors |  | - |
|  | 3.5 | Others |  | - |


| Min. Fire Rating |
| :--- |
| 3 Hrs. <br> None <br> None <br> None <br> None <br> None <br> - |

4.0 Floor Area 187 Sq. Ft. Length $17^{\prime}$ Width $11^{\prime}$ Height $10^{\prime \prime-6 \prime \prime}$
5.0 Volume $\quad 1,964 \mathrm{Cu} . \mathrm{Ft}$.

| 6.0 | Floor Drains $\quad$ Nuclear | X | Non-Nuclear |
| :--- | :--- | :--- | :--- |
| 7.0 | Exhaust Ventilation System |  | None |
|  | 7.1 | Percentage of System's Capacity |  |
|  | $\underline{3.3 \%}$ |  |  |


| 8.0 | 8 |  |  |  | Nr. Emergency Lighting in Area |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | 8.1 | Yes |  |  |  |
|  | Outside Area at Exit Points | Yes | X | No |  |

9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
No
No X
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Type
Portable Extinguishers
Stand Pipe System Hose Station
None
-----
11.0 Fire Loading in Area
11.1 Refer to page 2.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> Appendix A |
| :--- | :---: | :--- |
| STATION |  |  |$\quad$| Fire Hazard Analysis - W-F-2B-Z |
| :--- |$\quad$| Page 2 of 3 Tab 10 |
| :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety |
| :--- | :--- | :--- | :--- | :--- |
| Equipment | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No Safety Related or Safe Shutdown Equipment in ThisArea

### 13.0 Design Base Fire

Note: Oil Fire
13.1 Combustible in Area (In Situ) Fire Loading in Area

| Note: | Oil Fire |  |  |
| :---: | :---: | :---: | :---: |
| Oil: | 1.5 Gallons | 1,203 | Btu/Sq. Ft. |
| Grease: | Pounds |  | Btu/Sq. Ft. |
| Class A: | Pounds |  | Btu/Sq. Ft. |
| Charcoal: | Pounds |  | Btu/Sq. Ft. |
| Chemicals: | Pounds |  | Btu/Sq. Ft. |
| Plastics: | Pounds |  | Btu/Sq. Ft. |
| Resins: | Pounds |  | Btu/Sq. Ft. |
| Other: |  |  |  |
| Total Fire L | ing in Area: | 1203 | Btu/Sq. Ft. |
| Total Comb | bles: | 225,000 | Btu |

### 14.0 Design-Basis Fire Description

(A) This fire zone is not separated from adjacent fire zones (W-F-1A-Z, W-F-1B-Z, W-F-2A-Z, W-F-2B-Z, W-F-2C-Z and W-F-2D-Z) by fire rated walls and hence it is assumed that all combustibles in all these zones will ignite and burn simultaneously. Total combustibles are $32,155,000$ Btu spread over 1598 sq.ft. (fire loading 20,122 Btu/ $\mathrm{ft} .^{2}$ ).
(B) These zones are non-safety related and hence additional combustibles due to cable loading will have no significance.
14.1 DBF Fire Loading

20,122 Btu/Sq. Ft.
14.2 Peak Fire Temperature

$$
\frac{3,112}{10}{ }^{\circ} \mathrm{F} \text { Minutes }
$$

14.3 Duration of Fire
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of crystal recirculation pumps.
15.2 No safe shutdown or safety related equipment in the area.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Possible loss of cryst. Pumps.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
| Fire Hazard Analysis - W-F-2B-Z |  |  |$\quad$| Page 3 of 3 Tab 10 |
| :--- |

17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable. There is no water fire suppression in the subject area.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire brigade will put out the fire with hose reels and/or portable extinguishers.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable (see 15.2).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
| Section F.2 Tab 10 |  |  |
| Page 1 of 3 |  |  |

W-F-2C-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Waste Processing Building
W-F-2C-Z
Asphalt Meter Pump Area
42'-5" Elev. Cols. A-3
9763-F-805882-FP
3.0 Construction of Area

| Tatal |  |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | 3'-0" Concrete | 3 Hrs. |
|  |  | South | 1'-6" Concrete | None |
|  |  | East | 1'-6" Concrete | None |
|  |  | West | 2'-6" Concrete | Outside Wall |
| 3.2 | Floor |  | 2'-6" Concrete | None |
| 3.3 | Ceiling |  | 2'-6" Concrete | None |
| 3.4 | Doors |  | One (1) | 3 Hrs. |
| 3.5 | Others |  | One (1) Locked Mesh Door | None |

4.0 Floor Area 150 Sq. Ft. Length $10^{\prime}-0^{\prime \prime}$ Width $15^{\prime}-0^{\prime \prime}$ Height $10^{\prime}-6^{\prime \prime}$
5.0 Volume $\quad 1,575 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear

Non-Nuclear $\qquad$ None $\quad$ X

| 7.0 | Exhaust Ventilation System | Waste Solidification Exhaust System |  |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  | 7.1 | Percentage of System's Capacity | $8.5 \%$ |

$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area Yes 8.1 Outside Area at Exit Points Yes $\qquad$ No X
No
9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
No
Yes
$\square$

$$
\text { No } \mathrm{X}
$$

10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Type
Water Deluge System
Standpipe and Hose Reel Station
Ionization and Thermal
-----
11.0 Fire Loading in Area
11.1 Refer to page 2.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> Appendix A |
| :--- | :---: | :--- |
| STATION |  |  |$\quad$| Section F.2 Tab 10 |
| :--- |
| Page 2 of 3 |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
| $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |  |

No Safety Related or Safe Shutdown Equipment in ThisArea
13.0 Design Base Fire

| 13.1 | Combustible in Area (In Situ) |  |  | Fire Loading in Area |
| :---: | :---: | :---: | :---: | :---: |
|  | Note: | Oil Fire |  |  |
|  | Oil: | 4.25 | Gallons | 4250 Btu/Sq. Ft. |
|  | Grease: |  | Pounds | Btu/Sq. Ft. |
|  | Class A: |  | Pounds | Btu/Sq. Ft. |
|  | Charcoal: |  | Pounds | Btu/Sq. Ft. |
|  | Chemicals: |  | Pounds | Btu/Sq. Ft. |
|  | Plastics: |  | Pounds | Btu/Sq. Ft. |
|  | Resins: |  | Pounds | Btu/Sq. Ft. |
|  | Other: | Asphalt -5 | Gallons | 5,000 Btu/Sq. Ft. |
| 13.2 | Total Fire L | ding in Area |  | 9,250 Btu/Sq. Ft. |
|  | Total Comb | tibles: |  | 1,387,500 Btu |

### 14.0 Design-Basis Fire Description

(A) This fire zone is not separated from adjacent fire zones (W-F-1A-Z, W-F-1B-Z, W-F-2A-Z, W-F-2B-Z, W-F-2C-Z \& W-F-2D-Z) by fire rated walls and hence it is assumed that all combustibles in all these zones will ignite and burn simultaneously. Total combustibles are $32,155,000$ Btu spread over 1598 sq.ft. (fire loading $20,122 \mathrm{Btu} / \mathrm{ft}^{2}$ ).
(B) These zones are non-safety related and hence additional combustibles due to cable loading will have no significance.
14.1 DBF Fire Loading

20,122 Btu/Sq. Ft.
14.2 Peak Fire Temperature
14.3 Duration of Fire

$$
3,112{ }^{\circ} \mathrm{F}
$$

10 Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of metering function.
15.2 No safe shutdown or safety related equipment in the area.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> STATION |
| :--- | :---: | :--- |
| Fire Hazard Analysis A - W-F-2C-Z |  |  |$\quad$| Section F.2 Tab 10 |
| :--- |
| Page 3 of 3 |

17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 No consequences.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire brigade will put out the fire with hose reels and/or portable extinguishers.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable (see 15.2).

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 7 <br> Section F.2 Tab 10 <br> Page 1 of 3 |
| :--- | :---: | :--- |

W-F-2D-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Waste Processing Building
W-F-2D-Z
Turntable and Drum Conveyor Area 25'-0" Elev, Cols. "A" - "B" \& " 2 " - " $4 "$
F-805661-FP
3.0 Construction of Area

4.0 Floor Area 507 Sq. Ft. Length $39^{\prime}-0^{\prime \prime}$ Width $13^{\prime}-0^{\prime \prime}$ Height $17^{\prime}-0^{\prime \prime}$
5.0 Volume $\quad 8,619 \mathrm{Cu}$. Ft.

| 6.0 | Floor Drains $\quad$ Nuclear | X | Non-Nuclear | None |
| :--- | :--- | :--- | :--- | :--- |
| 7.0 | Exhaust Ventilation System |  | Waste Solidification Exhaust System |  |
|  | $7.1 \quad$ Percentage of System's Capacity | $\underline{70 \%}$ |  |  |


9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\quad \mathrm{X}$
No
No X
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection

Type
Water Deluge System
Standpipe and Hose Reel Station
Ionization and Thermal
10.4 Other
-----
11.0 Fire Loading in Area
11.1 Refer to page 2.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 7 <br> Section F.2 Tab 10 <br> Page 2 of 3 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety |
| :--- | :--- | :--- | :--- | :--- |
| Equipment | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No Safety Related or Safe Shutdown Equipment in ThisArea
13.0 Design Base Fire

| 13.1 | Combustible in Area (In Situ) |  |  | Fire Loading in Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Note: | Oil Fire |  |  |  |
|  | Oil: | 41.25 | Gallons | 12,204 | Btu/Sq. Ft. |
|  | Grease: |  | Pounds |  | Btu/Sq. Ft. |
|  | Class A: |  | Pounds |  | Btu/Sq. Ft. |
|  | Charcoal: |  | Pounds |  | Btu/Sq. Ft. |
|  | Chemicals: |  | Pounds |  | Btu/Sq. Ft. |
|  | Plastics: |  | Pounds |  | Btu/Sq. Ft. |
|  | Resins: |  | Pounds |  | Btu/Sq. Ft. |
|  | Other: |  |  |  |  |
| 13.2 | Total Fire L | ing in Area |  | 12,204 | Btu/Sq. Ft. |
|  | Total Comb | bles: |  | 6,187,500 | Btu |

14.0 Design-Basis Fire Description
(A) This fire zone is not separated from adjacent fire zones (W-F-1A-Z, W-F-LB-Z, W-F-2A-Z, W-F-2B-Z, W-F-2C-Z \& W-F-2D-Z) by fire rated walls and hence it is assumed that all combustibles in all these zones will ignite and burn simultaneously. Total combustibles are $32,155,000$ Btu spread over 1598 sq.ft. (fire loading 20,122 Btu/ $\mathrm{ft} .^{2}$ ).
(B) These zones are non-safety related and hence additional combustibles due to cable loading will have no significance.
14.1 DBF Fire Loading

20,122 Btu/Sq. Ft.
14.2 Peak Fire Temperature
3,112
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of drum conveyor.
15.2 No safe shutdown or safety-related equipment in the area.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 No consequences -- fire will be extinguished.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 7 <br> STATION |
| :--- | :---: | :--- |
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17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 No consequences.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire brigade will put out the fire with hose reels and/or portable extinguishers.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Space Protected

1. Not applicable (see 15.2).

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Section F.2 Tab 10 <br> Page 1 of 2 |
| :--- | :---: | :--- |

W-F-2E-Z

| 1.0 | Building |  |  | Waste Processing Building |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | W-F-2E-Z |  |
|  | 2.1 | Area Name |  | Waste Solidification Control Room |  |
|  | 2.2 | Location |  | 25'-0" Elev. Cols. "A-B" \& "3"-"4" |  |
|  | Drawing No |  |  | 9763-F-80566 |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire |
|  | 3.1 | Walls | North | 3'-0" Concrete | 3 Hrs . |
|  |  |  | South | 3'-0" Concrete | None |
|  |  |  | East | 2'-0" Concrete | None |
|  |  |  | West | 2'-6" Concrete | Outside |
|  | 3.2 | Floor |  | 2'-0" Concrete | None |
|  | 3.3 | Ceiling |  | 2'-0" Concrete | None |
|  | 3.4 | Doors |  | One (1) | 3 Hrs. |
|  | 3.5 | Others |  | None | - |

4.0 Floor Area 477 Sq. Ft. Length 26'-6" Width $18^{\prime \prime}-0^{\prime \prime}$ Height $14^{\prime}-6^{\prime \prime}$
$5.0 \quad$ Volume $\quad 6,917 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None_ None ___
7.0 Exhaust Ventilation System WAH-AC-76 Air Conditioning Unit
7.1 Percentage of System's Capacity $100 \%$
$\begin{array}{llllll}8.0 & 8 & & & \text { Hr. Emergency Lighting in Area } & \text { Yes } \\ & \text { 8.1 } & \text { Outside Area at Exit Points } & \text { Yes } & \text { X } & \text { No } \\ & & & \text { No }\end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes
9.2 Airborne
10.0 Fire Protection

Yes

| No X |
| :--- |
| No |

10.1 Primary

Type
10.2 Secondary

Portable Extinguisher
10.3 Detection

Standpipe and Hose Reel Station
10.4 Other

Ionization
-----
11.0 Fire Loading in Area
11.1 None X_ (No Further Analysis Required)

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| :--- | :---: | :--- |
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| :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  | System Train |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No Safety Related or Safe Shutdown Equipment in ThisArea

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A |
| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - TF-F-1-0 |  |$\quad$| Page 1 of 2 Tab 10 |
| :--- |

TF-F-1-0
1.0 Building
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location

Drawing No

Tank Farm (RWST)
TF-F-1-0
Refueling Water Storage Tank (RWST) Area
Between PAB \& Waste Processing Building 805661-FP
3.0 Construction of Area

|  |  |  | Material | Min. Fire Ratin |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | $22^{\prime}-0{ }^{\prime \prime} \mathrm{H} \times 2{ }^{\prime}-0{ }^{\prime \prime}$ Conc. |  |
|  |  |  | W/Siding to Roof | 3 Hr . |
|  |  | South | $22^{\prime}-0$ " H x 2'-0" Conc. Dike | - |
|  |  | East | $2^{\prime}-0^{\prime \prime}$ Concrete | 3 Hr ( (PAB) |
|  |  | West | 2'-0" Concrete | - |
| 3.2 | Floor |  | Concrete | - |
| 3.3 | Ceiling |  | Buildup Roof | - |
| 3.4 | Doors |  | None | - |
| 3.5 | Others |  | - | - |

4.0 Floor Area 3,120 Sq. Ft. Length 65'-0" Width $48^{\prime}-0^{\prime \prime}$ Height $60^{\prime}-0^{\prime \prime}$
5.0 Volume $\quad 187,200 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None
7.0 Exhaust Ventilation System WAH-FN-59A\&B
7.1 Percentage of System's Capacity $\quad 100 \%$
$\begin{array}{lllll}8.0 & 8 \mathrm{Hr} \text {. Emergency Lighting in Area } & \text { Yes } & & \text { No } \quad \text { X } \\ & 8.1 & \text { Outside Area at Exit Points } & \text { Yes } & \square\end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Yes
Yes Type
$\qquad$

Ref. Deviation No. 2
SBN-904 Dated 12/2/85
Fire Extinguisher(s)
Standpipe and Hose Reel
None
-----

### 11.0 Fire Loading in Area

11.1 None X (no further analysis required)

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| :--- | :---: | :--- |
| Fire Hazard Analysis - TF-F-1-0 |  |  |$\quad$| Sage 2 of 2 Tab 10 |
| :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ | $\underline{l} \underline{\text { System Train }}$ | Safety <br> Related |  |
| :--- | :--- | :--- | :---: | :---: |
|  <br> Instruments | CBS | X | X | X |
| Cabling | CBS | X | X | X |
| Piping \& Valves | CS | X | X | X |
| Cabling | CS | X | X | X |


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| :--- | :---: | :--- |
|  | Appendix A |  |
| Fire Hazard Analysis - SW-F-1A-Z | Page 1 of 3 Tab 11 |  |

SW-F-1A-Z

| 1.0 | Building |  |  | Service Water Pump House |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | SW-F-1A-Z |  |
|  | 2.1 | Area Name |  | Circulating Water Pump |  |
|  | 2.2 | Location |  | North Side El 21' - ${ }^{\prime \prime}$ |  |
|  |  | Drawin |  | 9763-F-202476-FP, 2024i |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire |
|  | 3.1 | Walls | North | Metal | Outside |
|  |  |  | South | Concrete | $11 / 2 \mathrm{Hr}$. ${ }^{\text {² }}$ |
|  |  |  | East | Metal | Outside |
|  |  |  | West | Metal | Outside |
|  | 3.2 | Floor |  | Grating/Concrete | - |
|  | 3.3 | Ceiling |  | Concrete/Fiberboard | Outside |
|  | 3.4 | Doors |  | Metal | - |
|  | 3.5 | Others |  | Exposed Steel Beams | - |

4.0 Floor Area 14,800 Sq. Ft. Length $125^{\prime}$ Width $\underline{118.67 ' ~}^{\prime}$ Height 29.83'
5.0 Volume $\quad 442,500 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear __ Non-Nuclear X (Grating)
7.0 Exhaust Ventilation System Wall Exhaust
7.1 Percentage of System's Capacity $\quad 100 \%$
$\begin{array}{lllll}8.0 & 8 & & & \\ & \text { 8r. Emergency Lighting in Area } & \text { Yes } & & \text { No } \quad \mathrm{X} \\ & \text { Outside Area at Exit Points } & \text { Yes } & \text { X } & \text { No }\end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Yes
Yes
Type
Fire Extinguisher(s)
Yard Hydrant
None
----
11.0 Fire Loading in Area
11.1 Refer to page 2.

[^16]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> AtATION |
| :--- | :---: | :--- |
| Fire Hazard Analysis - SW-F-1A-Z |  |  |$\quad$| Section F.2 Tab 11 |
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12.0 Equipment and Systems in Fire Area/Zone

|  |  | $\underline{\text { System Train }}$ |  | Safety <br> Equipment |
| :--- | :--- | :--- | :--- | :--- |
|  | $\underline{\text { System }}$ | $\underline{A}$ | $\underline{B}$ | $\underline{\text { Related }}$ |

No Safety Related or Safe Shutdown Equipment in This Area

### 13.0 Design Base Fire

| 13.1 | Combustible in Area (In Situ) |  |  | Fire Loading in Area |
| :---: | :---: | :---: | :---: | :---: |
|  | Note: | Oil Fire |  |  |
|  | Oil: | 145.5 | Gallons | 1,475 Btu/Sq. Ft. |
|  | Grease: |  | Pounds | Btu/Sq. Ft. |
|  | Class A: |  | Pounds | Btu/Sq. Ft. |
|  | Charcoal: |  | Pounds | Btu/Sq. Ft. |
|  | Chemicals: |  | Pounds | Btu/Sq. Ft. |
|  | Plastics: | 3,542 | Pounds | 3,111 Btu/Sq. Ft. |
|  | Resins: |  | Pounds | Btu/Sq. Ft. |
|  | Other: |  |  |  |
| 13.2 | Total Fire L | ing in Are |  | 4,586 Btu/Sq. Ft. |
|  | Total Comb | bles: |  | $\overline{67,880,000}$ Btu |

### 14.0 Design-Basis Fire Description

(A) One of the three (3) circulating water pumps ruptures and the entire contents ( 32.5 gallon/unit x $1=32.5$ gallons) of oil will spill down and be contained in the cubicle at pit floor at elevation $4^{\prime}-0^{\prime \prime}$. This will cover an area of approximately $16^{\prime}-0^{\prime \prime} \times 26^{\prime}-0^{\prime \prime}=416 \mathrm{sq}$. Ft. The entire contents will ignite and burn.
(B) The oil from one of the three circulating water pump traveling screens spills on the floor and the total of 70.5 gallons of oil will ignite and burn covering an area of $15^{\prime}-0^{\prime \prime} \times 60^{\prime}-0^{\prime \prime}=900 \mathrm{sq} . \mathrm{ft}$.
14.1 DBF Fire Loading

$$
\begin{aligned}
\frac{11,719}{476} & \\
& \text { Btu/Sq. Ft. } \\
4^{1 / 2} & \text { Minutes }
\end{aligned}
$$

14.2 Peak Area/Zone Temp. During Fire $\quad 476{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of affected service water pump due to loss of oil. Fire duration is less than 5 minutes and affected pit is separated from adjoining pit by a concrete structure.

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| :--- | :---: | :--- |
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### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Not applicable (neither automatic suppression system nor fire detection system is present). Effect will be the loss of affected pump.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable (automatic suppression system does not exist).
18.0 Containing the Design Basis Fire in the Fire Area/Zone
18.1 The pit of each pump is surrounded by a concrete structure. The fire duration is less than 5 minutes and the pit is 16.0 feet deep.

A fire involving a traveling screen will not spread to other fire zones. The subject fire zone is separated from other zones by a concrete structure. The exception is an opening in the trench loading to SW-F-1E-Z. Exhaust air moment, however, is away from SW-F-1E-Z and therefore the fire will not spread to this fire zone.

### 19.0 How Is Redundant Safe Shutdown Equipment in Same Area Protected

19.1 There is no safe shutdown equipment in the affected area.

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| :--- | :---: | :--- |
| Fire Hazard Analysis - SW-F-1B-A |  |  |$\quad$| Section F.2 Tab 11 |
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SW-F-1B-A

4.0 Floor Area $\quad 725$ Sq. Ft. Length $31^{\prime}$ Width $23.3^{\prime}$ Height 17.5'
5.0 Volume $\quad 12,700 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear __ Non-Nuclear __ None $\quad \mathrm{X}$
7.0 Exhaust Ventilation System Pressurized Supply
7.1 Percentage of System's Capacity $\quad 100 \%$
$\begin{array}{llllll}8.0 & 8 & & & & \text { Nr. Emergency Lighting in Area } \\ & \text { 8.1 } & \text { Yes } & & \text { Nutside Area at Exit Points } & \text { Yes } \\ & \text { X } & & \text { No } & \end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes $\qquad$ $\underset{\text { No }}{\text { No }}$
10.0 Fire Protection

Type
10.1 Primary

Fire Extinguisher(s)
10.2 Secondary

Yard Hydrant
10.3 Detection Ionization
10.4 Other
-----

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| :--- | :---: | :--- |
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11.0 Fire Loading in Area
11.1 Total Combustibles:
182,000 Btu
11.2 Design Basis Fire: No Design Basis Fire postulated
12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| 460 Motor | EDE | X |  | X |

Control Centers E514

| Cabling | EDE | X |  | X |
| :--- | :--- | :--- | :--- | :--- |
| Cabling | SW | X |  | X |
| Cabling | SWA | X | X | X |
| Temp. Switches | SWA | X | X | X |
| Cabling | CW | X |  |  |


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| :--- | :---: | :--- |
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SW-F-1C-A

| 1.0 | Building | Service Water Pump House |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area or Zone | SW-F-1C-A |  |
|  | $2.1 \quad$ Area Name |  |  |
|  | $2.2 \quad$ Location | Electrical Control Room "B" |  |
|  |  | Drawing No | Southwest El 22'-0" |
|  |  | 9763-F-202476-FP |  |

3.0 Construction of Area

|  |  |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Concrete | 3 Hr . |
|  |  | South | Concrete | Outside |
|  |  | East | Concrete | $11 / 2 \mathrm{Hr}$. |
|  |  | West | Concrete | Outside/1 $1^{1 / 2} \mathrm{Hr}$. |
| 3.2 | Floor |  | Concrete | Outside |
| 3.3 | Ceiling |  | Concrete | Outside |
| 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . / 1^{1 / 2} \mathrm{Hr}$. |
| 3.5 | Others |  | Exposed Steel Beams | - |

4.0 Floor Area 375 Sq. Ft. Length 23.3' Width $\mathbf{1 6 '}^{\prime}$ Height $17.5^{\prime}$
5.0 Volume 6,530 Cu. Ft.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System Pressurized Supply
7.1 Percentage of System's Capacity $\quad 100 \%$
$\begin{array}{llllll}8.0 & 8 & & & & \text { Nr. Emergency Lighting in Area } \\ & \text { 8.1 } & \text { Yes } & & \text { Nutside Area at Exit Points } & \text { Yes } \\ & \text { X } & & \text { No } & \end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No |
| :--- |
| No |

10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary

Fire Extinguisher (s)
10.3 Detection

Yard Hydrant
Ionization
10.4 Other
-----
11.0 Fire Loading in Area
11.1 None X_ (no further analysis required)

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| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Temp. Switches | SWA | X | X | X |  |
| Cabling | SWA | X | X | X | X |
| $460 \mathrm{v}-$ Motor Control Centers E614 | EDE |  | X | X | X |
| Cabling | SW |  | X | X | X |
| Cabling | SWA |  | X | X | X |


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| Station | Fire Hazard Analysis - SW-F-1D-A | Page 1 of 2 Tab 11 |

SW-F-1D-A

4.0 Floor Area $\quad 110$ Sq. Ft. Length $16.5^{\prime}$ Width ${ }^{6.6^{\prime} \quad \text { Height } 17.5^{\prime}}$
5.0 Volume $\quad 1,925 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System Electrical Room Vent System
7.1 Percentage of System's Capacity $\underline{100 \%}$

| 8.0 | 8 Hr . Emergency Lighting in Area | Yes |  |  |
| :--- | :--- | :--- | :--- | :--- |
|  | 8.1 | Outside Area at Exit Points | Yes | $\square$ |$\quad$| No $\quad$ X |
| :--- |

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No X |
| :--- |
| No X |

10.0 Fire Protection
10.1 Primary

Fire Extinguisher (s)
10.2 Secondary

Yard Hydrant
10.3 Detection

Ionization
10.4 Other
-----
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

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| :--- | :---: | :--- |
| Fire Hazard Analysis - SW-F-1D-A |  |  |$\quad$| Section F.2 Tab 11 |
| :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |
| Fan-FN-40A | SWA | X |  | X |
| Cabling | SWA | X | X | X |
| Fan FN-40B | SWA |  | X | X |


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SW-F-1E-Z

| 1.0 | Building |  |  | Service Water Pump House |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | SW-F-1E-Z |  |
|  | 2.1 | Area Name |  | Service Water Pump Area |  |
|  | 2.2 | Location |  | South Side El 21'-0" |  |
|  |  | Drawing |  | 9763-F-202476-FP \& 202478 - FP |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire Rating |
|  | 3.1 | Walls | North | Concrete | $1_{*}^{1 / 2} \mathrm{Hr}$. |
|  |  |  | South | Concrete | Outside |
|  |  |  | East | Concrete | Outside |
|  |  |  | West | Concrete | $11 / 2 \mathrm{Hr}$. |
|  | 3.2 | Floor |  | Grating/Concrete | - |
|  | 3.3 | Ceiling |  | Concrete | Outside |
|  | 3.4 | Doors |  | Metal | $11 / 2 \mathrm{Hr}$. |
|  | 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area 8,500 Sq. Ft. Length 114.6' Width $\mathbf{7 4}^{\prime}$ Height 27.25'
5.0 Volume $\quad 231,250 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear__ Non-Nuclear X_(Grating)

| 7.0 | Exhaust Ventilation System |  | Wall Exhaust |  |
| :--- | :--- | :--- | :--- | :--- |
|  | 7.1 | Percentage of System's Capacity | $\underline{100 \%}$ |  |
| 8.0 | 8 Hr. Emergency Lighting in Area | Yes |  | No $\quad \mathrm{X}$ |
|  | 8.1 | Outside Area at Exit Points | Yes | X |

9.0 Operational Radioactivity

| 9.1 | Equipment/Piping | Yes | No $\quad$ X |
| :--- | :--- | :--- | :--- |
| 9.2 | Airborne | Yes | $\square$ |

10.0 Fire Protection
10.1 Primary

Type
Fire Extinguisher (s)
10.2 Secondary

Yard Hydrant
10.3 Detection

Ionization
10.4 Other
-----

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11.0 Fire Loading in Area
11.1 Refer to page 2 of 3.
12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related |
| :--- | :--- | :--- | :---: | :---: |
| Pump P-41A | SW | X | $\underline{B}$ | $\frac{\mathrm{X}}{\mathrm{A}}$ |
| Cabling | SW | X | X | X |
| Pump P-41C | SW | X |  | X |
| Piping, Valves \& | SW | X | X | X |
| Instruments |  |  |  |  |
| Pump P-41B | SW |  | X | X |
| Pump P-41D | SW |  | X | X |
| Instrument Rack IR - 73 | MM | X | X | X |
| Fans FN - 38A \& 38B | SWA | X | X | X |
| Dampers DP - 39A \& | SWA | X | X | X |
| 39B |  |  |  |  |
| Temp. Switches | SWA | X | X | X |
| Cabling | SWA | X | X | X |
| FLEX Equipment | FLEX |  |  |  |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |  |
| :---: | :---: | :---: |
| Oil: | 357.9 | Gallons |
| Grease: |  | Pounds |
| Class A: | 5,889.8 | Pounds |
| Charcoal: |  | Pounds |
| Chemicals: |  | Pounds |
| Plastics: | 15,528.6 | Pounds |
| Resins: |  | Pounds |
| Cables: | 919.6 | Pounds |

Other:
13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area
6,316.1 Btu/Sq. Ft.
$\longrightarrow$ Btu/Sq. Ft.

5,543.3 Btu/Sq. Ft. Btu/Sq. Ft. Btu/Sq. Ft.
23,749.5 Btu/Sq. Ft. Btu/Sq. Ft.
$1,136 \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft}$.

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### 14.0 Design-Basis Fire Description

(A) Two out of a total of four service water pumps rupture. Total oil content of 26.5 gallons spills to the pit floor at elevation $4^{\prime}-0^{\prime \prime}$ and burns completely, covering an area of 342 square feet.
14.1 DBF Fire Loading

11,623 Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. During Fire
$804{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
4.5 Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 The affected circulating water pumps are lost due to loss of oil.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Because of the remote location from the control room, the short duration of fire (less than five minutes and manual fire protection systems consisting of fire hydrant and fire extinguishers, only the affected circulating water pumps may be lost.

### 17.0 Consequences of in Advertent or Careless Operation or Rupture of Fire Protection System

17.1 Not applicable (automatic suppression system does not exist).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 The subject zone is surrounded by a concrete structure which separates adjoining fire zones with the exception of the opening however, is away from SW-F-1A-Z, and therefore, the fire will not spread to other fire zone.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 There is no safe shutdown equipment in the subject fire zone.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> ATATION |
| :--- | :---: | :--- |
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SW-F-2-0

| 1.0 | Building |  |  | Service Water Intake \& Discharge Structure |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | SW-F-2-0 |  |
|  | 2.1 2.2 | Area Name |  | Service Water Intake \& Discharge Structure |  |
|  | 2.2 | Location |  | E-6500, N-10,000 \& N-9,990 |  |
|  |  | Drawin |  | $9763-\mathrm{F}-3002$ |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire |
|  | 3.1 | Walls | North | Concrete | Outside |
|  |  |  | South | Concrete | Outside |
|  |  |  | East | Concrete | Outside |
|  |  |  | West | Concrete | Outside |
|  | 3.2 | Floor |  | Grating | Outside |
|  | 3.3 | Ceiling |  | Concrete | Outside |
|  | 3.4 | Doors |  | Tornado/Missil | - |
|  | 3.5 | Others |  | - | - |

4.0 Floor Area 2,086/1,876 Sq. Ft. Length $75^{\prime} / 67^{\prime}$ Width $\quad$ 74'/67' Height $101^{\prime} / 101^{\prime}$
$5.0 \quad$ Volume $\quad 210,686 / 189,476 \mathrm{Cu} . \mathrm{Ft}$.


9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes
9.2 Airborne

Yes $\qquad$ | No |
| :--- |
| No |

10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Type
Portable Extinguishers
Yard Hydrant
None
-----
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

[^18]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> StATION |
| :--- | :---: | :--- |
| Appendix A <br> Section F.2 Tab 11 |  |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System |  | System Train |  |
| :--- | :--- | :--- | :---: | :---: | | Safety |
| :---: |
| SW-V-44 |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Appendix A <br> Pection F.2 Tab 12 |
| :--- | :---: | :--- |

## CT-F-1C-A

| 1.0 | Building |  |  | Cooling Tower |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | CT-F-1C-A |  |
|  | 2.1 | Area Name |  | Switchgear Room Unit \#1 Train "B" |  |
|  | 2.2 | Location |  | East Side El 22 ' -0" |  |
|  |  | Drawing No |  | 9763-F -805068-FP |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire Rating |
|  | 3.1 | Walls | North | Concrete | Outside |
|  |  |  | South | Concrete | 3 Hr . |
|  |  |  | East | Concrete | Outside |
|  |  |  | West | Concrete | $11 / 2 \mathrm{Hr}$. |
|  | 3.2 | Floor |  | Concrete | Outside |
|  | 3.3 | Ceiling |  | Concrete | $11 / 2 \mathrm{Hr}$. |
|  | 3.4 | Doors |  | Metal | $3 \mathrm{Hr} / 1^{1 / 2} \mathrm{Hr}$. |
|  | 3.5 | Others |  | Exposed Ceiling Beams | - |

4.0 Floor Area $\quad 615$ Sq. Ft. Length $25^{\prime}$ Width $24.5^{\prime}$ Height $22^{\prime}$
5.0 Volume $\quad 13,500 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System Pressurized Supply
7.1 Percentage of System's Capacity $\quad 100 \%$

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne

Yes

| No X |
| :--- |
| No X |

10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Yes
Type
Fire Extinguisher(s)
Yard Hydrant
Ionization
------
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued page 2)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> StATION |
| :--- | :---: | :--- |
| Appendix A |  |  |$\quad$| Section F.2 Tab 12 |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B | Related |  |
| Temp. Switches | SWA |  | X | X |  |
| 480v Subst. E64 | EDE |  | X | X |  |
| Cabling | EDE |  | X | X |  |
| 460v - Motor Control <br> Centers MCC-E-641 | EDE |  | X | X | X |
| Cabling | SW |  | X | X | X |
| Cabling | SWA |  | X | X |  |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: |  |  |
| :---: | :---: | :---: |
| Oil: |  | Gallons |
| Grease: |  | Pounds |
| Class A: |  | Pounds |
| Charcoal: |  | Pounds |
| Chemicals: |  | Pounds |
| Plastics: | 30 | Pounds |
| Resins: |  | Pounds |
| Other: |  |  |

### 13.2 Total Fire Loading in Area: <br> Total Combustibles:

Fire Loading in Area

|  | Btu/Sq. Ft. |
| :---: | :---: |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 634 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. | Btu/Sq. Ft. Btu/Sq. Ft. Btu/Sq. Ft. Btu/Sq. Ft. Btu/Sq. Ft. Btu/Sq. Ft. | 634 | Btu/Sq. Ft. |
| ---: | :--- |
| 390,000 | Btu |

### 14.0 Design-Basis Fire Description

1. The combustible portions of the racking tool ignite and burn over an area covering $2 \mathrm{ft} . \mathrm{x} 2.2 \mathrm{ft}=4.4 \mathrm{ft}^{2}$. This is the approximate size of breaker racking tool.
2. The entire combustible content of the tool burns.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |$\quad$| Section F.2 Tab 12 |
| :--- |
| Page 3 of 3 |

14.1 DBF Fire Loading
14.2 Peak Area/Zone Temp. Fire
14.3 Duration of Fire

Consequences of Design Basis Fire without Fire Protection
15.1 Train B service water may not be available due to smoke damage. Thermal damage is expected to be minimal.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished with manual hose lines.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable. There is no fire suppression in the subject area.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire would be extinguished using portable extinguishers and/or hose lines.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 The redundant Train A equipment and cables are located in a separate fire area.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 8 <br> Appendix A |
| :--- | :---: | :--- |
| STATION |  |  |$\quad$| Section F.2 Tab 12 |
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CT-F-1D-A

11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued page 2)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 8 |
| :--- | :---: | :--- |
| STATION | Appendix A | Section F.2 Tab 12 <br> Page 2 of 3 |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{\text { System Train }}$ | Safety <br> Related | Required <br> For Safe |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Shutdown |  |  |  |  |
| Centers E-513 | EDE | X | X |  |
| Cabling | EDE | X | X |  |
| Cabling | SW | X | X | X |
| Cabling | SWA | X | X |  |
| Temp. Switches | SWA | X | X |  |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

| Note: | $=$ |
| :--- | :--- |
| Oil: | $=$ |
| Greallons |  |
| Pounds |  |
| Class A: | $=$ Pounds |
| Charcoal: | $=$ Pounds |
| Chemicals: | $=$Pounds <br> Plastics: <br> Pesins: <br> Pounds |
| Other: | $=$ |

### 13.2 Total Fire Loading in Area: <br> Total Combustibles:

Fire Loading in Area

 | 571 | $\mathrm{Btu} / \mathrm{Sq}. \mathrm{Ft}$. |
| ---: | :--- |
| 351,000 | Btu |

### 14.0 Design-Basis Fire Description

3. For conservatism the ladders are assumed to be in a vertical position. The bottom of both sets of rails are ignited and burn upward.
4. To add conservatism, it is assumed that the fire is self sustaining although the fire is not severe and has a low heat release rate.
5. The fire area will be limited to the length of the ladder and about 2 feet from the wall for an area covering 20 ft . $\mathrm{X} 2 \mathrm{ft} .=40 \mathrm{sq} . \mathrm{ft}$.
14.1 DBF Fire Loading

| $\frac{8775}{}{ }^{165}{ }^{\circ} \mathrm{Ftu} / \mathrm{Fq}. \mathrm{Ft}$. |
| :--- |

14.3 Duration of Fire

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 8 <br> Appendix A |
| :--- | :---: | :--- |
| Station | Fire Hazard Analysis - CT-F-1D-A | Section F.2 Tab 12 <br> Page 3 of 3 |

15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Train a service water may not be available due to smoke damage. Thermal damage is expected to be minimal.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished with manual hose lines.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.3 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.4 The fire would be extinguished using portable extinguishers and/or hose lines.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 The redundant Train B equipment and cables are located in a separate fire area.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 8 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 12 |  |  |
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CT-F-2B-A

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Cooling Tower
CT-F-2B-A

Ventilation \& Mech. Rooms For Unit \#1
$\frac{\text { East Side El 46' - 0"' }}{\text { 9763-F -805068-FP }}$
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 3,575 Sq. Ft. Length 71.5' Width ${ }^{50} \quad$ Height 29.5'
5.0 Volume $\quad 105,460 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X_None_
7.0 Exhaust Ventilation System Roof Ventilators
7.1 Percentage of System's Capacity $\quad 100 \%$
$\begin{array}{llllll}8.0 & 8 & & & & \text { Nr. Emergency Lighting in Area } \\ & \text { 8.1 } & \text { Yes } & & \text { Nutside Area at Exit Points } & \text { Yes } \\ & \text { X } & & \text { No } & \end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes $\qquad$ | No |
| :--- |
| No |

10.0 Fire Protection
10.1 Primary

Type
Fire Extinguisher(s)
10.2 Secondary

Yard Hydrant
10.3 Detection

Ionization
10.4 Other
------
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued page $2 \& 3$ ).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 8 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |$\quad$| Section F.2 Tab 12 |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Pump - P - 110A | SW | X |  | X |  |
| Cabling | SW | X |  | X | X |
| Pump - P -110B | SW |  | X | X |  |
| Piping \& Valves | SW | X | X | X | X |
| Fan FN-64 | SWA | X |  | X |  |
| Cabling | SWA | X |  | X |  |
| Fan FN-63 | SWA |  | X | X |  |
| Damper Dp-65, 66 | SWA |  | X | X |  |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: |  |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area

| 1,112 | Btu/Sq. Ft. |
| :---: | :---: |
|  |  |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 156 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |


| 1,268 | Btu/Sq. Ft. |
| ---: | :--- |
| $3,975,000$ | Btu |


| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 8 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |$\quad$| Section F.2 Tab 12 |
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### 14.0 Design-Basis Fire Description

1. One of the two (2) Service Water Pumps rupture, oil spills on the floor. For conservatism, the oil from the other pump is added to the spill, therefore a total of 26.5 gallons of oil is assumed spilled.
2. This oil is assumed to cover an area of approximately 350 square feet. It ignites and burns completely.
14.1 DBF Fire Loading $\quad 1,112$ Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. During Fire $1658{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire
$<5$ Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Refer to Seabrook Station Fire Protection of Safe Shutdown Capability (10 CFR 50, App. R).
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished with portable extinguishers.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire would be extinguished using portable extinguishers and/or fire hoses.

### 19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected

19.1 Refer to Seabrook Station Fire Protection of Safe Shutdown Capability (10 CFR 50, App. R).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> Appendix A |
| :--- | :---: | :--- |
| Station | Fire Hazard Analysis - CT-F-3-0 |  |$\quad$| Page 1 of 2 Tab 12 |
| :--- |

CT-F-3-0

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Cooling Tower

CT-F-3-0 Top of Cooling Tower | Outside - Top of Cooling Tower El. 77' $-0 \prime \prime$ |
| :--- |
| 9763-F-805068-FP |

3.0 Construction of Area

|  | 咗 |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | N/A | N/A |
|  |  | South | N/A | N/A |
|  |  | East | N/A | N/A |
|  |  | West | N/A | N/A |
| 3.2 | Floor |  | N/A | N/A |
| 3.3 | Ceiling |  | N/A | N/A |
| 3.4 | Doors |  | - | - |
| 3.5 | Others |  | - | - |

4.0 Floor Area N/A Sq. Ft. Length N/A Width N/A Height N/A
5.0 Volume N/A Cu. Ft.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None X_
7.0 Exhaust Ventilation System N/A
7.1 Percentage of System's Capacity N/A
$\begin{array}{llllll}8.0 & 8 & & & & \text { Nr. Emergency Lighting in Area } \\ & \text { 8.1 } & \text { Yes } & & \text { Outside Area at Exit Points } & \text { Yes } \\ & \text { X } & & \text { No } & \end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes

| No X |
| :--- |
| No X |

10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Yard Hydrant
None
------
11.0 Fire Loading in Area
11.1 Approximately 70 gallons of oil in each Train A fan gear reducer and approximately 30 gallons of oil in each Train B fan gear reducer. Outside location no further analysis required.

$\left.$| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 6 <br> STATION |
| :--- | :---: | :--- | | Appendix A |
| :--- |
| Section F.2 Tab 12 | \right\rvert\, | Fage 2 of 2 |
| :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety |
| :---: | :---: | :---: | :---: | :---: |
|  | System | A | B | Related |
| No Equipment Required For Safe Shutdown in This Area |  |  |  |  |
| Fan-FN-1-51A | SW | X |  | X |
| Fan-1-FN-51B | SW |  | X | X |
| Fan-2-FN-51B | SW |  | X | X |
| Fan-2-FN-51A | SW |  | X | X |
| Cabling | SW | X | X | X |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 15 <br> Section F.2 Tab 13 <br> Page 1 of 4 |
| :--- | :---: | :--- |

CE-F-1-Z


### 11.0 Fire Loading in Area

11.1 Refer to page $3^{* * *}$ (analysis continued pages 2-4)

[^19]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> STATION |
| :--- | :---: | :--- | | Appendix A |
| :--- |
| Section F.2 Tab 13 |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety Related |
| :---: | :---: | :---: | :---: | :---: |
|  | System | A | B |  |
| Cooling Unit AC-2A | EAH | X |  | X |
| Cabling | EAH | X | X | X |
| Cooling Unit AC-2B | EAH |  | X | X |
| Damper DP - 3A | EAH | X |  | X |
| Damper DP - 3B | EAH |  | X | X |
| Fan FN-31A | EAH | X |  | X |
| Fan FN-31B | EAH |  | X | X |
| Damper DP - 25A | EAH | X |  |  |
| Damper DP - 25B | EAH |  | X |  |
| Cabling | PAH |  | X | X |
| Damper DP - 35B, 36b | PAH |  | X | X |
| Filters F-9, 69 | EAH | X | X | X |
| Fan FN-4A, B | EAH | X | X | X |
| Dampers DP - 30A, B | EAH | X | X | X |
| Dampers DP - 29A, B | EAH | X | X | X |
| Cabling | SF | X | X | X |
| Cabling | FAH | X | X | X |
| Cabling | CC | X | X | X |
| FN FN - 5A, B | EAH | X | X | X |
| Damper DP-37A, B | EAH | X | X | X |
| Instruments | EAH | X | X | X |
| Piping, Valves, Instruments \& Cabling | CAP | X | X | X |
| Damper DP - 13A, B | FAH | X | X | X |

$13.0^{*} \quad$ No 3 hr . Rated fire damper provided in exhaust duct at the point of connection to the unit plant vent.
No Automatic Detection in Containment Annulus Area.
Ref: Deviation No. 1
SBN - 904 Dated 12/2/85
Ref: Deviation No. 2
SBN - 904 Dated 12/2/85

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 <br> STATION |
| :--- | :---: | :--- |
| Fire Hazard Analysis - CE-F-1-Z |  |  |$\quad$| Section F.2 Tab 13 |
| :--- |
| Page 3 of 4 |

### 13.0 Design Base Fire

13.1 Combustible in Area (In Situ)

| Note: |  |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | 2,100 Pounds |
| Chemicals: | 35 Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

### 13.2 Total Fire Loading in Area: <br> Total Combustibles:

Fire Loading in Area

|  | Btu/Sq. Ft. |
| :---: | :---: |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| * | Btu/Sq. Ft. |
| 97 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

97 Btu/Sq. Ft. 455.000 Btu

### 14.0 Design-Basis Fire Description

1. For conservatism the ladders are assumed to be in a vertical position. The bottom of both sets of rails are ignited and burn upward.
2. To add conservatism, it is assumed that the fire is self sustaining although the fire is not severe and has a low heat release rate.
3. The fire area will be limited to the length of the ladders and about 2 feet from the wall for an area covering 24 ft . $\mathrm{X} 2 \mathrm{ft} .=48 \mathrm{ft}^{2}$.
14.1 DBF Fire Loading


### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Refer to Seabrook Station Fire Protection of Safe Shutdown Capability (10 CFR 50, App. R).

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 No consequences. Fire will be extinguished with portable extinguishers.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System

### 17.1 Not applicable

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 15 |
| :--- | :---: | :--- |
| STATION | Appendix A | Section F.2 Tab 13 |
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18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire would be extinguished using hose lines and/or portable extinguishers.
19.0 How the Redundant Safe Shutdown Equipment in the Area Is Protected
19.1 Refer to Seabrook Station Fire Protection of Safe Shutdown Capability (10 CFR 50, App. R).

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |$\quad$| Section F.2 Tab 14 |
| :--- |
| Page 1 of 3 |

FPH-F-1A-A

| 1.0 | Building |  |  | Fire Pump House |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | FPH-F-1A-A |  |
|  | 2.1 | Area Name |  | Diesel Pump Room - West |  |
|  | 2.2 | Location |  | $\frac{\text { EL 21'-0" }}{9763-F-300831-F P}$ |  |
|  |  | Drawin |  |  |  |
| 3.0 | Construction of Area |  |  |  | Min. Fire Rating |
|  |  |  |  | Material |  |
|  | 3.1 | Walls | North | Metal | Outside |
|  |  |  | South | Metal | Outside |
|  |  |  | East | Concrete | 3 Hr . |
|  |  |  | West | Metal | Outside |
|  | 3.2 | Floor |  | Concrete | Outside |
|  | 3.3 | Ceiling |  | Concrete | - |
|  | 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . /-$ |
|  | 3.5 | Others |  | Exposed Steel Beams | - |

4.0 Floor Area $\quad 825$ Sq. Ft. Length $30^{\prime}$ Width $\xrightarrow{27.5^{\prime} \text { Height } \quad 17{ }^{\prime}}$
5.0 Volume $14,025 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X None ___
7.0 Exhaust Ventilation System Pump Room Exhaust System
7.1 Percentage of System's Capacity $\underline{100 \%}$
$\begin{array}{llllll}8.0 & 8 & & & \text { Hr. Emergency Lighting in Area } & \text { Yes } \\ & \text { 8.1 } & \text { Outside Area at Exit Points } & \text { Yes } & \text { X } & \text { No } \\ & & & \text { No__ }\end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
$\begin{array}{cll}\text { Yes } & \left.\text { No } \begin{array}{l}\text { X } \\ \text { Yes }\end{array} \quad \begin{array}{ll}\text { No X }\end{array}\right]\end{array}$
10.0 Fire Protection

Type
10.1 Primary

Wet Pipe Sprinkler System
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Thermal
10.4 Other
---------
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued pg. 2 \& 3)

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A <br> Section F.2 Tab 14 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  |  |  | Safety | Required For Safe |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B | Related | Shutdown |

13.0 Design Basis Fire

| 13.1 | Combustible in Area (In Situ) |  |  |
| :---: | :--- | :--- | :---: |
|  | Note: | Oil Fire |  |
|  | Oil: | $\frac{7}{\text { Gallons }}$ |  |


| Grease: | Pounds |
| :--- | :--- |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | $=732$ Pounds |
| Plastics: | Pounds |
| Resins: |  |

Other:
13.2 Total Fire Loading in Area:

Total Combustibles:

### 14.0 Design-Basis Fire Description

1. The engine lube oil system ruptures and the entire contents (7 gallons of oil) are sprayed over the pump room covering an area of 91 square feet. Oil film thickness is $1 / 8^{\prime \prime}$.
2. Oil is ignited, burned and consumed.
14.1 DBF Fire Loading
$11,538 \mathrm{Btu} / \mathrm{Sq}$. Ft.
14.2 Fire Area Peak Temperature $2,164{ }^{\circ} \mathrm{F}$
14.3 Fire Duration
$41 / 2$ Minutes
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of diesel fire pump engine.
15.2 Loss of controls to pump engine.
15.3 Redundant pump, located in separate fire area.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 |
| :--- | :---: | :--- |
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### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Loss of diesel fire pump engine due to lose of oil.
16.2 Possible loss of engine controls.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Possible loss of engine controls.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 The fire duration is short, therefore, the structure will contain the fire. The consequences of fire are mitigated further by operation of the sprinkler system.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable. (see 15.1) fire pumps are not required for safe shutdown nor are they safety related.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A | Section F.2 Tab 14 <br> Page 1 of 2 |  |

FPH-F-1B-A
1.0 Building

Fire Pump House
2.0 Fire Area or Zone
2.1 Area Name

FPH-F-1B-A
Electric Pump Room
El 21' - 0"
9763-F-300831-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East | $\frac{\text { Material }}{\text { Metal }}$ | $\frac{\text { Min. Fire Rating }}{\text { Concrete }}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 480 Sq. Ft. Length $16^{\prime}$ Width $\quad 30^{\prime} \quad$ Height ${ }^{17}$
5.0 Volume $\quad 8,160 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X_None__
7.0 Exhaust Ventilation System Pump Room Exhaust System
7.1 Percentage of System's Capacity $\underline{100 \%}$
8.0 8 Hr. Emergency Lighting in Area Yes No X
8.1 Outside Area at Exit Points Yes X

No
9.0 Operational Radioactivity

| 9.1 | Equipment/Piping | Yes | No $\quad$ X |
| :--- | :--- | :--- | :--- |
| 9.2 | Airborne | Yes | $\square$ |

10.0 Fire Protection
10.1 Primary

Type
Wet Pipe Sprinkler System
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Ionization
10.4 Other
------
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A | Section F.2 Tab 14 <br> Page 2 of 2 |  |

12.0 Equipment and Systems in Fire Area/Zone

|  |  |  |  | Sequired <br> Equipment | $\underline{\text { System Train }}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |$\quad \underline{\text { Safety }}$| For Safe |
| :---: |

No Equipment Required For Safe Shutdown in This Area

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
| :--- | :---: | :--- |
| STATION |  |  |$\quad$| Section F.2. Tab 14 |
| :--- |
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FPH-F-1C-A
1.0 Building

Fire Pump House
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location

Drawing No
FPH-F-1C-A
Diesel Pump Room East
El 21'-0"
9763-F-300831-FP
3.0 Construction of Area

|  |  |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Metal | Outside |
|  |  | South | Metal | Outside |
|  |  | East | Metal | Outside |
|  |  | West | Concrete | 3 Hr . |
| 3.2 | Floor |  | Concrete | Outside |
| 3.3 | Ceiling |  | Concrete | - |
| 3.4 | Doors |  | Metal | $3 \mathrm{Hr} . /-$ |
| 3.5 | Others |  | Exposed Steel Beams | - |

4.0 Floor Area $\quad 825$ Sq. Ft. Length $\quad 30^{\prime} \quad$ Width $\quad 27.5^{\prime}$ Height $\quad 17^{\prime}$
$5.0 \quad$ Volume $\quad 14,025 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X_None__
7.0 Exhaust Ventilation System Pump Room Exhaust System
7.1 Percentage of System's Capacity $\underline{100 \%}$
8.0 8 Hr. Emergency Lighting in Area Yes $\quad$ No_ X
8.1 Outside Area at Exit Points Yes X $\qquad$
9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes


| No X X |
| :--- |

Yes $\qquad$
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection

Type
Wet Pipe Sprinkler System
Fire Extinguisher(s)
Thermal
10.4 Other
------
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued pg. 2 \& 3)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
| Section F.2. Tab 14 |  |  |
| Page 2 of 3 |  |  |

12.0

Equipment

Equipment and Systems in Fire Area/Zone

| Equipment |  |  |  | Safety | Required For Safe |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | System | A | B | Related | Shutdown |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Oil Fire |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | $=33$ Pounds |
| Plastics: | Pounds |
| Resins: | $=$ |
| Other: |  |

13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area
1,273 Btu/Sq. Ft
$\square$ Btu/Sq. Ft. Btu/Sq. Ft.
$\ldots$ Btu/Sq. Ft.
520 Btu/Sq. Ft. Btu/Sq. Ft.

| $\frac{1,793}{1,479,000} \mathrm{Btu} / \mathrm{Sq}. \mathrm{Ft}$. |
| :--- |

### 14.0 Design-Basis Fire Description

1. the Engine Lube Oil System Ruptures and the Entire Contents (7 Gallons of Oil) Are Sprayed Over the Pump Room Covering An Area of 91 Square Feet. Oil Film Thickness Is $1 / 8^{\prime \prime}$.
2. Oil Is Ignited, Burned and Consumed.
3. Duration of Fire Is $1 \frac{1}{2}$ Minutes.
14.1 DBF Fire Loading
14.2 Fire Area Peak Temperature

| $\frac{11,538}{2,105}$ |
| :--- |
|  |
| ${ }^{\circ} \mathrm{Btu} / \mathrm{Fq}$ |
|  |

15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of diesel fire pump engine.
15.2 Loss of controls to pump engine.
15.3 Redundant pump, located elsewhere, is unaffected.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
| Section F.2. Tab 14 |  |  |
| Page 3 of 3 |  |  |

16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of diesel fire pump engine due to loss of oil.
16.2 Possible loss of engine controls.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable (no water suppression in area).
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 The fire duration is short therefore the structure will contain the fire.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable (see 15.3). Fire pumps are not required for safe shutdown nor are they safety related.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 18 <br> Section F.2 Tab 15 <br> Page 1 of 3 |
| :--- | :---: | :--- |

TB-F-1A-Z

| 1.0 | Building | Turbine Building |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area or Zone | TB-F-1A-Z |  |
|  | $2.1 \quad$ Area Name |  |  |
|  | $2.2 \quad$ Location | Ground Floor |  |
|  |  | Drawing No |  |
|  |  | El 21'-0" Southwest |  |

3.0 Construction of Area

|  |  |  | Material | Min. Fire Rating |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Concrete/Block | - |
|  |  | South | Concrete/Metal | $3 \mathrm{Hr} . / \mathrm{Outside}$ |
|  |  | East | - | - |
|  |  | West | Concrete/Block | 3 Hr . |
| 3.2 | Floor |  | Concrete | Outside |
| 3.3 | Ceiling |  | Grating | - |
| 3.4 | Doors |  | Metal | 3 Hr . |
| 3.5 | Others |  | - | - |


11.0 Fire Loading in Area
11.1 Refer to page 3.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 18 <br> Appendix A |
| :--- | :---: | :--- |
| Pection F.2 Tab 15 |  |  |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B | Related |
| Cabling | EDE | X | X |  |

Non Seg Bus Feeder For EDE X 4160v Swgr E5

| Non Seg Bus Feeder For <br> 4160v Swgr E6 | EDE |  | X |
| :--- | :--- | :--- | :--- |
| Air Compressor | SA | X | X |
| SA-SKD-137A, |  |  |  |
| SA-SKD-137B, |  |  |  |
| SA-SKD-137C |  |  |  |


| Instruments | SA | X | X |  |
| :--- | :--- | :--- | :--- | :--- |
| Piping \& Valves | SA | X | X |  |
| Dryer SKD-18A, 18B | IA | X | X |  |
| Cabling | SA | X | X |  |
| Cabling | IA | X | X |  |
| Cabling | FW | X | X | X |
| Cabling | MS | X | X | X |

125 V Dc Switch Gear EDE X
12A, 12B
Pump P-113 FW X
Cabling $\quad \mathrm{CO} \quad \mathrm{X}$
PAA Skid SKD-900 CAS
Security Enclosure, SFD
1-SFD-MM-2009

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 18 <br> STATION |
| :--- | :---: | :--- |
| Fire Hazard Analysis A TB-F-1A-Z |  |  |$\quad$| Section F.2 Tab 15 |
| :--- |
| Page 3 of 3 |

### 13.0 Design Base Fire

| 13.1 | Combustible in Area (In Situ) |  |  | Fire Loading in Area |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Note: | Oil Fire |  |  |  |
|  | Oil: | 961 | Gallons | 3,372 | Btu/Sq. Ft. |
|  | Grease: |  | Pounds |  | Btu/Sq. Ft. |
|  | Class A: |  | Pounds |  | $\mathrm{Btu} / \mathrm{Sq}$. Ft. |
|  | Charcoal: |  | Pounds |  | $\mathrm{Btu} / \mathrm{Sq}$. Ft. |
|  | Chemicals: | 1,677.3 (PAA) | Pounds | 420.2 | Btu/Sq. Ft. |
|  | Plastics: | 109 | Pounds | 33.1 | Btu/Sq. Ft. |
|  | Resins: |  | Pounds |  | Btu/Sq. Ft. |
|  | Other: |  | Pounds |  | Btu/Sq. Ft. |
|  | Hydrogen | 2,860 | Cubic Feet | 22 | Btu/Sq. Ft. |
| 13.2 | Total Fire Loading in Area: |  |  | 3,847.3 | Btu/Sq. Ft. |
|  | Total Comb | tibles: |  | 164,472,075 | Btu |

### 14.0 Design-Basis Fire Description

(a) The single largest quantity of oil, 680 gallons, which is associated with hydrogen seal unit, is spilled over a curbed area of 320 square feet and burned completely.
(b) Ventilation supply air thru open louvers and exhaust air thru roof ventilators is passing over the fire area providing oxygen for burning.
(c) Oil fire causes spill and ignition of PAA, contributing to DBF.

| 14.1 | DBF Fire Loading | 639,536 |
| :---: | :---: | :---: |
| 14.2 | Peak Area/Zone Temp. During Fire | 222 |
| 14.3 | Duration of Fire | 130 |

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Hydrogen seal unit is lost because of loss of oil leading to eventual trip.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Hydrogen seal unit may be lost because of loss of oil possibly leading to reactor trip.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Inadvertent actuation of deluge sprinkler system will cause minor flooding. Hydrogen seal unit is unaffected. Floor is sloped for drainage.
18.0 Containing the Design Basis Fire in the Fire Area/Zone
18.1 The entire spill of oil is isolated by a curbed area from surroundings. The fire will be contained locally.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable as no redundant safe shutdown equipment in the vicinity of the affected zone.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
| :--- | :---: | :--- |
| STATION |  |  |$\quad$| Fire Hazard Analysis - TB-F-1B-A |
| :--- |$\quad$| Page 1 of 3 Tab 15 |
| :--- |

TB-F-1B-A

| 1.0 | Building | Turbine Building |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area or Zone | TB-F-1B-A |  |
|  | $2.1 \quad$ Area Name |  |  |
|  | $2.2 \quad$ Location |  |  |
|  |  | Drawing No | Battery Room |
|  |  | El 21'-0" SW Corner |  |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete/Block }}$ | $\frac{\text { Min. Fire }}{\frac{\text { Concrete/Block }}{\text { Concrete/Block }}}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 450 Sq. Ft. Length $28^{\prime}-0{ }^{\prime \prime}$ Width $16^{\prime}-0^{\prime \prime}$ Height $14^{\prime}-4{ }^{\prime \prime}$
5.0 Volume $\quad 6,422 \mathrm{Cu}$. Ft.

| 6.0 | Floor Drains | Nuclear | Non-Nuclear |  | None | X |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7.0 | Exhaust Ventilation System |  |  | Wall Exhaust Fan |  |  |
|  | 7.1 Percen | f System's |  | 100\% |  |  |
| 8.0 | 8 Hr . Emergency Lighting in Area Ye |  |  |  | No | X |
|  | 8.1 Outsid | a at Exit P | Ye |  | No | X |

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
Yes
Yes
$\qquad$ No
No
$X$
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other

Type
Fire Extinguisher(s)
Standpipe \& Hose Reel
Ionization
Yard Hydrant
11.0 Fire Loading in Area
11.1 Refer to page 2 of 3

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Station |
| :--- | :---: | :--- |
| Fippendix A |  |  |
| Sage Hazard Analysis - TB-F-1B-A 2 of 3 |  |  |$\quad$| Pab 15 |
| :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety |
| :---: | :---: | :---: | :---: | :---: |
|  |  | A | B | Related |
| Battery B-2A, B | ED | X |  |  |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

Fire Loading in Area

| Note: | Class A Material Fire |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | 1,888 Pounds |
| Resins: | Pounds |
| Other: |  |


|  | Btu/Sq. Ft. |
| :---: | :---: |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |
| 67,568 | Btu/Sq. Ft. |
|  | Btu/Sq. Ft. |

$\begin{array}{llrl}13.2 & \text { Total Fire Loading in Area: } & \frac{67,568}{} & \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft} . \\ \text { Total Combustibles: } & 30,405,532 & \mathrm{Btu}\end{array}$

### 14.0 Design-Basis Fire Description

(A) Fire Starts Involving the Battery Cells.
(B) the Fire Spreads To Involve All Battery Cells.
(C) This Area Is Cut-Off From the Main Turbine Ground Floor By Fire Rated Construction. A Fire Is Not Expected To Propagate Beyond This Area.
14.1 DBF Fire Loading $\quad 67.568$ Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. During Fire $\quad>750{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire $\quad>5$ Minutes

### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of batteries.
15.2 Refer to Seabrook Station Safe Shutdown Capability "Appendix R" analysis.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of one of two batteries.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable. No water suppression in area.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
| :--- | :---: | :--- |
| STATION | Fire Hazard Analysis - TB-F-1B-A | Sage 3 of 3 Tab 15 <br> Page |

18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Area is separated from the main turbine building ground floor by fire rated barriers.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 See 15.0 above.

| SEABROOK | Evaluation and Comparison to | Rev 6 |
| :--- | :---: | :--- |
| STATION | BTP APCSB 9.5-1, Appendix A | Section F.2 Tab 15 <br> Page 1 of 3 |

TB-F-1C-Z

| 1.0 | Building |  | Turbine Building |
| :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  | TB-F-1C-Z |
|  | 2.1 | Area Name | Relay Room |
|  | 2.2 | Location | Northwest El. 21' ${ }^{\prime \prime \prime}$ |
|  |  | Drawing No | 9763-F -202052 |

3.0 Construction of Area

|  |  |  | Material | Min. Fire |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Concrete/Block | - |
|  |  | South | Concrete/Block | - |
|  |  | East | Concrete/Block | - |
|  |  | West | Concrete/Block | 3 Hr . |
| 3.2 | Floor |  | Concrete | Outside |
| 3.3 | Ceiling |  | Concrete Plank | - |
| 3.4 | Doors |  | Metal | 3 Hr . |
| 3.5 | Others |  | - | - |


5.0 Volume $\quad 36,400 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear X None __
7.0 Exhaust Ventilation System TAH-FN-127 \& TAH-FN-67
7.1 Percentage of System's Capacity 7.6\%
$\begin{array}{llll}8.0 & 8 \mathrm{Hr} \text {. Emergency Lighting in Area } & \text { Yes } \\ & 8.1 & \text { Outside Area at Exit Points } & \text { Yes }\end{array} \quad \begin{aligned} & \text { — }\end{aligned} \quad \begin{aligned} & \text { No } \quad \text { X } \\ & \end{aligned}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 Refer to page 2 of 3.

| SEABROOK | Evaluation and Comparison to | Rev 6 |
| :--- | :---: | :--- |
| STATION | BTP APCSB 9.5-1, Appendix A | Section F.2 Tab 15 <br> Page 2 of 3 |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Control Panel CP-84 | SY | X | X |  | X |
| Cabling | EDE | X | X |  | X |
| Control Panel CP-85 | SY | X | X |  | X |
| Control Panel CP-86 | SY | X | X |  | X |
| Control Panel CP-87 | SY | X | X |  | X |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)

| Note: | Class A Material Fire |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

13.2 Total Fire Loading in Area:

Total Combustibles:
14.0 Design-Basis Fire Description
A. Fire starts in one of the two battery rooms.
B. The fire spreads to involve all the battery cells within the room.
14.1 DBF Fire Loading 36,300 Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. During Fire $\quad 1,040{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire

41 Minutes

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| :--- | :---: | :--- |
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### 15.0 Consequences of Design Basis Fire without Fire Protection

15.1 Loss of battery function.
15.2 Refer to Seabrook Station Safe Shutdown Capability "Appendix R" analysis.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 Loss of one of two batteries.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable. No water suppression in zone.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Batteries are not separated from relay room by fire-rated construction. Effects from battery fire may propagate to relay room. See 15.0 above.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 See 15.0 above.

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TB-F-2-Z


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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\underline{l}$ System Train | Safety <br> Related |  |
| :--- | :--- | :--- | :--- | :--- |
| Control Panel CP-414 <br> Control Panel CP-558 | FP | X | $\underline{B}$ |  |
| Cabling | CBA | X |  |  |
| Cabling | EDE | X |  |  |
| Cabling | SA | X |  |  |
| Cabling | MS | X | X | X |


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| STATION | Fire Hazard Analysis - TB-F-3-Z | Section F.2 Tab 15 <br> Page 1 of 3 |

TB-F-3-Z

| 1.0 | Building |  |  | Turbine Building |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  |  | TB-F-3-Z |  |
|  |  |  |  | SAS \& Computer Rooms, Start-Up \& Turbine Erector's Office - Electronic Work Area |  |
|  |  | Area Name |  |  |  |
|  |  | Location |  | El 75' - 0 " SW Corner |  |
|  |  | Drawing No |  | 9763-F-202054-FP |  |
| 3.0 | Construction of Area |  |  |  |  |
|  |  |  |  | Material | Min. Fire |
|  | 3.1 | Walls | North | Concrete | - |
|  |  |  | South | Concrete | - |
|  |  |  | East | Concrete | - |
|  |  |  | West | Metal | Outside/3 |
|  | 3.2 | Floor |  | Concrete | - |
|  |  |  |  | Class I Interior Floor Finish |  |
|  | 3.3 | Ceiling |  | Concrete | - |
|  | 3.4 | Doors |  | Metal | - |
|  | 3.5 | Others |  | - | - |

4.0 Floor Area 4,030 Sq. Ft. Length $62^{\prime}$ Width $6^{6 \prime}$ Height ${ }^{25^{\prime}}$
$5.0 \quad$ Volume $\quad 100,750 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System Office Air Conditioning System
7.1 Percentage of System's Capacity

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes
Yes $\qquad$

| No |
| :--- | :--- |
| No |

10.0 Fire Protection

Type
(Sprinkler system above rooms)
10.1 Primary

Fire Extinguisher(s)
Standpipe \& Hose Reel
Ionization \& Photoelectric
10.3 Detection
------
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued pg. 2 \& 3)

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### 12.0 Equipment and Systems in Fire Area/Zone

|  |  |  |  |  | Required |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Equipment | $\underline{\text { System Train }}$ | Safety | For Safe <br> Fhatem | $\underline{A}$ | $\underline{B}$ |

No Safety Related Equipment Required For Safe Shutdown in This Zone
13.0 Design Base Fire
13.1 Combustible in Area (In Situ) Fire Loading in Area

| Note: | Class A Material Fire |
| :--- | :--- |
| Oil: | Gallons |
| Grease: | Pounds |
| Class A: | 4,500 Pounds |
| Charcoal: | Pounds |
| Chemicals: | Pounds |
| Plastics: | Pounds |
| Resins: | Pounds |
| Other: |  |

13.2 Total Fire Loading in Area: $\quad \frac{12,630}{36,000,000} \frac{\mathrm{Btu} / \mathrm{Sq} . \text { Ft. }}{\mathrm{Btu}}$

Total Combustibles:
36,000,000 Btu
14.0 Design-Basis Fire Description
A. Fire starts in an office waste paper basket.
B. Fire spreads throughout the entire fire zone consuming all combustibles (class a material).
C. The affected zone is isolated from ventilation air by the fire damper, allowing only partial combustibles to burn.
14.1 DBF Fire Loading $\quad 12,630$ Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. During Fire
690
${ }^{\circ} \mathrm{Eight}(8)$
15.0 Consequences of Design Basis Fire without Fire Protection
15.1 Loss of occupancy of the offices and electronic work room.
15.2 There is no safe shutdown nor safety related equipment in the zone. Therefore, the consequences of a design basis fire will not be serious.

### 16.0 Consequences of Design Basis Fire with Fire Protection

16.1 Possible loss of occupancy of the subject area.

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17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable. No water suppression in area.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Separation from the control room by a three-hour-rated fire barrier prevents loss of any safety-related function..
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable (see 15.2)

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| :--- | :---: | :--- |
| Fire Hazard Analysis - PP-F-1A-Z |  |  |$\quad$| Page 1 of 2 |
| :--- |

PP-F-1A-Z

| 1.0 | Building | Mechanical Penetration Area |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |  |
|  | $2.1 \quad$ Area Name |  |  |
|  | $2.2 \quad$ Location | Radioactive Piping Area |  |
|  |  | Drawing No | $\underline{\text { Northeast Corner - El. }(-) 34^{\prime}-6^{\prime \prime},(-) 20^{\prime}-0 \prime \prime}$ |

3.0 Construction of Area

4.0 Floor Area $\quad 450$ Sq. Ft. Length $36^{\prime}$ Width Varies Height $22^{\prime}$
5.0 Volume $\quad 9,900 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System EAH (Non-Ducted)
7.1 Percentage of System's Capacity 33\%
8.0 8 Hr. Emergency Lighting in Area Yes

8.1 Outside Area at Exit Points Yes $\qquad$ | No X |
| :--- |
| No X |

9.0 Operational Radioactivity
9.1 Equipment/Piping
$\begin{array}{ll}\text { Yes } & \mathrm{X} \\ & \\ & \end{array}$ $\qquad$
10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Standpipe and Hose Reel
10.4 Other

Ionization
----
11.0 Fire Loading in Area
11.1 None X_(no further analysis required)

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| :--- | :---: | :--- |
| Fire Hazard Analysis - PP-F-1A-Z |  |  |$\quad$| Page 2 of 2 Tab 16 |
| :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Piping \& Valves | CS | X | X | X | X |
| Piping \& Valves | RC | X | X | X |  |
| Piping \& Valves | RH | X | X | X |  |
| Piping \& Valves | CBS | X |  | X |  |
| Cabling | RH | X | X | X |  |
| Cabling | CBS | X |  | X |  |
| Cabling | CS | X | X | X | X |
| Cabling | RC | X | X | X |  |
| Instrumentation | SI | X |  | X |  |


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PP-F-1B-Z

| 1.0 | Building | Mechanical Penetration Area |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | $2.1 \quad$ Area Name |  |
|  | $2.2 \quad$ Location | PP-F-1B-Z |
|  |  | Drawing No |

3.0 Construction of Area

4.0 Floor Area 441 Sq. Ft. Length Varies Width Varies Height $16^{\prime} \& 22^{\prime}$
5.0 Volume $\quad 7,704 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear X_None None ___ None
7.0 Exhaust Ventilation System EAH (Non-Ducted)
7.1 Percentage of System's Capacity 33\%
$\begin{array}{lllll}8.0 & 8 \mathrm{Hr} \text {. Emergency Lighting in Area } & \text { Yes } \\ & 8.1 & \text { Outside Area at Exit Points } & \text { Yes } & \square\end{array} \quad \begin{aligned} & \text { No } \quad \text { X } \\ & \end{aligned}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary

| Yes | X | No |
| :--- | :--- | :--- |
|  | X | No |
|  |  |  |

10.3 Detection

Type
Fire Extinguisher(s)
10.4 Other

Standpipe and Hose Reel
Ionization
---
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Piping \& Valves | RH |  | X | X | X |
| Cabling | SI | X | X | X |  |
| Cabling | CS | X | X | X |  |
| Piping \& Valves | CBS | X | X | X |  |
| Piping \& Valves | RC | X |  | X |  |
| Piping \& Valves | SI | X | X | X |  |
| Cabling | RH |  | X | X |  |
| Cabling | RC | X |  | X |  |
| Instruments | SI | X |  | X |  |
| Piping \& Valves | VG | X |  | X |  |
| Cabling | VG | X |  | X |  |
| Piping \& Valves | WLD | X |  | X |  |
| Instrument Rack IR-13A | MM | X |  | X |  |
| Temperature Elements \& Cabling | MM | X | X | X |  |


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PP-F-2A-Z

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | $2.1 \quad$ Area Name |  |
| $2.2 \quad$ Location | Mechanical Penetration Area |  |
|  |  | Drawing No |

3.0 Construction of Area

4.0 Floor Area 252 Sq. Ft. Length $18^{\prime}$ Width $14^{\prime}$ Height $35^{\prime}-6^{\prime \prime}$
5.0 Volume $\quad 8,946 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None ___
7.0 Exhaust Ventilation System EAH (Non-Ducted)
7.1 Percentage of System's Capacity 33\%
8.0 8 Hr . Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes $\qquad$
No X
9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne

| Yes | X |
| :--- | :--- |
|  |  |
|  |  |

No $\qquad$
0.0 Fire Protection
10.1 Primary

Type
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Standpipe \& Hose Reel Ionization
10.4 Other
----
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

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| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  |  |  | Required <br> Equipment | $\underline{\text { System Train }}$ |
| :--- | :--- | :--- | :---: | :---: | :---: |


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PP-F-2B-Z

| 1.0 | Building | Mechanical Penetration Area |
| :--- | :--- | :--- |
| 2.0 | Fire Area or Zone |  |
|  | $2.1 \quad$ Area Name |  |
|  | $2.2 \quad$ Location | PP-F-2B-Z |
|  |  | Drawing No |

3.0 Construction of Area

|  |  |  | Material | Min. Fire |
| :---: | :---: | :---: | :---: | :---: |
| 3.1 | Walls | North | Concrete/Open | - |
|  |  | South | Concrete | - |
|  |  | East | Concrete/Open | - |
|  |  | West | MCG | 3 Hr . |
| 3.2 | Floor |  | Concrete | Outside |
| 3.3 | Ceiling |  | Concrete | - |
| 3.4 | Doors |  | Metal | 3 Hr . |
| 3.5 | Others |  | - | - |


5.0 Volume $\quad 2,512 \mathrm{Cu}$. Ft.
6.0 Floor Drains Nuclear X_None_ None ___
7.0 Exhaust Ventilation System EAH (Non-Ducted)
7.1 Percentage of System's Capacity 33\%
8.0 8 Hr . Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes $\qquad$
No X

Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
$\begin{array}{ll}\text { Yes } & \mathrm{X} \\ & \end{array}$
No $\qquad$
No $\qquad$
10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Standpipe \& Hose Reel Ionization
10.4 Other
----
11.0 Fire Loading in Area
11.1 None X (no further analysis required)

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety <br> Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | CC |  | X | X | X |
| Cabling | CS | X | X | X |  |
| Cabling | RH |  | X | X |  |
| Cabling | CBS | X | X | X |  |
| Cabling | RC | X |  | X |  |
| Cabling | SI | X | X | X |  |


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PP-F-3A-Z

| 1.0 | Building | Mechanical Penetration Area |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area or Zone | PP-F-3A-Z |  |
|  | $2.1 \quad$ Area Name | Radioactive Piping Area |  |
|  | $2.2 \quad$ Location |  | Northeast Corner, El. $(-) 11$ |
|  |  | Drawing No $-21 / 2 "$ |  |
|  |  | 9763-F-311429-FP |  |

3.0 Construction of Area

4.0 Floor Area 450 Sq. Ft. Length $36^{\prime}$ Width Varies Height $\mathbf{1 2}^{\prime}$
5.0 Volume $\quad 5,400 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None _X
7.0 Exhaust Ventilation System EAH (Non-Ducted)
7.1 Percentage of System's Capacity

33\%
8.0 8 Hr. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes $\qquad$
No X

Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne

| Yes | X |
| :--- | :--- |
|  |  |
|  |  | $\qquad$

10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Standpipe and Hose Reel
10.4 Other Ionization
----
11.0 Fire Loading in Area
11.1 None $\qquad$ (no further analysis required)

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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | CS | X | X | X | X |
| Instrumentation | SI |  | X | X |  |
| Piping \& Valves | SI | X | X | X |  |
| Piping \& Valves | CBS |  | X | X |  |
| Cabling | SI | X | X | X |  |
| Cabling | CBS |  | X | X |  |


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PP-F-3B-Z

| 1.0 | Building <br> Fire Area or Zone | Mechanical Penetration Area |
| :---: | :---: | :---: |
| 2.0 |  | PP-F-3B-Z |
|  | 2.1 Area Name | Radioactive Piping Area |
|  | 2.2 Location | West Central - El. (-) 34' -6" To (-) 11' $-211 / 2$ ", (-) 26' $-0^{\prime \prime}$ |
|  | Drawing No | 9763-F-311429- FP |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete/Open }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\frac{\text { Concrete }}{-}}$ |
| :--- | :--- | :--- | :--- | :--- |
| 3.2 | Floor |  | $\frac{\text { Concrete }}{\text { Concrete }}$ | $\frac{-}{-}$ |
| 3.3 | Ceiling |  | $\frac{-}{3 \text { Hr. }}$ |  |
| 3.4 | Doors | Others |  | - |

4.0 Floor Area 199 Sq. Ft. Length 26'-6" Width ${ }^{\text {7'-6" }}$ Height 35'-6"
5.0 Volume 7,065 Cu. Ft.
6.0 Floor Drains Nuclear __ Non-Nuclear __ None $\quad \mathrm{X}$
7.0 Exhaust Ventilation System EAH (Non-Ducted)
7.1 Percentage of System's Capacity

33\%
8.0 8 Hr. Emergency Lighting in Area Yes
8.1 Outside Area at Exit Points Yes
$\square$
No X
$\begin{array}{llr}9.0 & \text { Operational Radioactivity } \\ & 9.1 \quad \text { Equipment/Piping }\end{array}$
$\begin{array}{ll}9.0 & \text { Operational Radioactivity } \\ & 9.1 \quad \text { Equipment/Piping }\end{array}$
9.2 Airborne

| Yes | X |
| :--- | :--- |
|  |  |

No $\qquad$
10.0 Fire Protection
10.1 Primary

Type
10.2 Secondary

Fire Extinguisher(s)
10.3 Detection

Standpipe and Hose Reel Ionization
10.4 Other
------
11.0 Fire Loading in Area
11.1 None $\quad \mathrm{X}$ (no further analysis required)

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| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required For Safe Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Cabling | CS |  | X | X | X |
| Cabling | RH |  | X | X |  |
| Cabling | CBS |  | X | X |  |


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## PP-F-4B-Z

| 1.0 | Building |  | Mechanical Penetration Area |
| :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  | PP-F-4B-Z |
|  | 2.1 | Area Name | Non-Radioactive Piping Area |
|  | 2.2 | Location | El. (-) 8' $-0^{\prime \prime}$ \& (-) 11' $-21 / 2{ }^{\prime \prime}$ |
|  |  | Drawing No | 9763-F-311429-FP |

3.0 Construction of Area

4.0 Floor Area 555 Sq. Ft. Length Varies Width Varies Height Varies
5.0 Volume $\quad 5,307 \mathrm{Cu} . \mathrm{Ft}$.
6.0 Floor Drains Nuclear __ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System EAH (Non-Ducted)
7.1 Percentage of System's Capacity 33\%
$\begin{array}{lllll}8.0 & 8 & \text { Hr. Emergency Lighting in Area } & \text { Yes } & \mathrm{X} \\ & \text { 8.1 } & \text { Outside Area at Exit Points } & \text { Yes } & -\end{array}$
9.0 Operational Radioactivity
9.1 Equipment/Piping
Yes

$\qquad$
10.0 Fire Protection

Type
Fire Extinguisher(s)
10.1 Primary

Standpipe and Hose Reel
10.2 Secondary

Ionization
10.3 Detection
------
11.0 Fire Loading in Area
11.1 None X_ (no further analysis required)

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| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | System Train |  | Safety Related | Required <br> For Safe <br> Shutdown |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B |  |  |
| Piping \& Valves | CC | X | X | X | X |
| Cabling | CC | X | X | X | X |
| Piping \& Valves | CBS |  | X | X |  |
| Cabling | CBS |  | X | X |  |
| Cabling | CS |  | X | X | X |


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### 12.0 Equipment and Systems in Fire Area/Zone

| Equipment |  | System Train |  | Safety |
| :---: | :---: | :---: | :---: | :---: |
|  | System | A | B | Related |
| No Equipment Required For Safe Shutdown in This Zone |  |  |  |  |
| Piping \& Valves | CS | X |  | X |
| Instrumentation | SI | X |  | X |
| Cabling | CS | X |  | X |
| Cabling | SI | X |  | X |


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| :--- | :---: | :--- |

NES-F-1A-Z
1.0 Building
2.0 Fire Area or Zone
2.1 Area Name
2.2 Location

Drawing No

Non-Essential Switchgear Room
NES-F-1A-Z
Non-Essential Switchgear Area
North of Control Building, El. 21' $-6^{\prime \prime}$ \& 37' $-6^{\prime \prime}$ 9763-F -310289-FP
3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | Material |
| :---: | :---: | :---: | :---: |
|  |  |  | Concrete/Block |
|  |  |  | Concrete |
|  |  |  | Concrete/Block |
|  |  |  | Concrete/Block |
| 3.2 | Floor |  | Concrete |
| 3.3 | Ceiling |  | Concrete/Plank |
| 3.4 | Doors |  | Metal |
| 3.5 | Others |  | - |


| Min. Fire Rating |
| :---: |
| 3 Hr . |
| $3 \mathrm{Hr} . *$ |
| 3 Hr . |
| Outside |
| Outside |
| Outside |
| $3 \mathrm{Hr} /$ /Outside |
| - |

4.0 Floor Area 3,552 Sq. Ft. Length $\quad 96$ ' Width $\quad 37^{\prime}$ Height $\quad 27^{\prime}$
5.0 Volume $\quad 95,904 \mathrm{Cu} . \mathrm{Ft}$.

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection
10.1 Primary
10.2 Secondary
10.3 Detection
10.4 Other
11.0 Fire Loading in Area
11.1 Refer to page 2 (analysis continued page 2)

[^21]Ref. Deviation No. 5, SBN-904, Dated Dec. 2, 1985.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev. 16 <br> Section F.2 Tab 17 <br> Page 2 of 3 |
| :--- | :---: | :--- |

12.0 Equipment and Systems in Fire Area/Zone

|  |  |  |  |  |  |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Equipment | $\underline{\text { System Train }}$ | $\underline{\mathrm{A}}$ | $\underline{\mathrm{B}}$ | Safety <br> Related | Required <br> For Safe <br> Shutdown |
| Cabling | EDE | X |  | X |  |
| Cabling | ED | X |  | X |  |
| Cabling | RC | X | X |  |  |

13.0 Design Base Fire
13.1 Combustible in Area (In Situ)


Grease: $\quad$ Pounds
Class A: Pounds
Charcoal: Pounds
Chemicals: Pounds
Plastics: $\quad 30$ Pounds
Resins:
Other:
13.2 Total Fire Loading in Area:

Total Combustibles:

Fire Loading in Area
$\qquad$ Btu/Sq. Ft.
$110 \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft}$. 390,000 Btu

### 14.0 Design-Basis Fire Description

1. The combustible portions of the racking tool ignite and burn over an area covering 2 ft . $\mathrm{x} 2.2 \mathrm{ft}=4.4 \mathrm{ft}^{2}$. This is the approximate size of breaker racking tool.
2. The entire combustible content of the tool burns.
14.1 DBF Fire Loading

88,636 Btu/Sq. Ft.
14.2 Peak Area/Zone Temp. Fire
$144{ }^{\circ} \mathrm{F}$
14.3 Duration of Fire

93 Minutes

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev. 16 <br> Appendix A |
| :--- | :---: | :--- |
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15.0 Consequences of Design Basis Fire without Fire Protection
15.1 A fire could result in loss of CST level instrumentation due to loss of ED-I-4, ED-PP-5, ED-CP-532, MM-CP-153; loss of RC pump switchgear control power (ED-SWG-1 and ED-SWG-2); loss of Pressurizer heaters C, D and control group power (ED-US-11 and ED-US-23) and loss of offsite power from EDE-SWG-5.
16.0 Consequences of Design Basis Fire with Fire Protection
16.1 No consequences. Fire will be extinguished with manual hose lines.
17.0 Consequences of Inadvertent or Careless Operation or Rupture of Fire Protection System
17.1 Not applicable. There is no fire suppression in the subject area.
18.0 Containing Design Basis Fire in the Fire Area/Zone
18.1 Fire detectors initiate an alarm in the control room. The control room alerts the fire brigade.
18.2 The fire would be extinguished using portable extinguishers and/or hose lines.
19.0 How Is Redundant Safe Shutdown Equipment in the Same Area Protected
19.1 Not applicable - Only Train A cables are located in NES-F-1-A-Z.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
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CST-F-1-0

| 1.0 | Building |  |
| :--- | :--- | :--- |
| 2.0 | Fire Area Or Zone |  |
|  | 2.1 | Area Name |
|  | 2.2 | Location |
|  |  | Drawing No |

Condensate Storage Tank
CST-F-1-0
Condensate Storage Tank

| $\mathrm{E}-6,100 \mathrm{~N}-10,200$ |
| :--- |
| $9763-\mathrm{F}-310248-\mathrm{FP}$ |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East <br> West | $\frac{\text { Material }}{\text { Concrete }}$ <br> $\frac{\text { Concrete }}{\text { Concrete }}$ | $\frac{\text { Min. Fire Rating }}{\frac{\text { Outside }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |
| 3.2 | Floor |  | $\frac{\frac{\text { Outside }}{\text { Concrete }}}{\text { Outside }}$ |  |
| 3.3 | Ceiling |  | $\frac{\text { Concrete }}{\text { Metal }}$ | $\frac{\frac{\text { Outside }}{\text { Outside }}}{3.4}$ |
| Doors | Others |  | $\frac{\text { Outside }}{-}$ | - |

4.0 Floor Area $468 / 150$ Sq. Ft. Length $\underline{48}^{\prime} / 30^{\prime}$ Width $\xrightarrow{8^{\prime} / 3^{\prime} \text { Height } 13^{\prime} / 7^{\prime}}$
5.0 Volume $\quad 6,084 / 1,050 \mathrm{Cu}$. Ft.

| 6.0 | Floor Drains Nuclear |  | Nuclear | None | X |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 7.0 | Exhaust Ventilation System |  | None |  |  |
|  | 7.1 Percentage of System's Cap |  | N/A\% |  |  |
| 8.0 | 8 Hr. Emergency Lighting in Area | Yes | X | No |  |
|  | 8.1 Outside Area at Exit Points | Yes | XA | No |  |
| 9.0 | Operational Radioactivity |  |  |  |  |
|  | 9.1 Equipment/Piping | Yes | X | No |  |
|  | 9.2 Airborne | Yes | X | No |  |
| 10.0 | Fire Protection | Typ |  |  |  |
|  | 10.1 Primary | Fire | tinguish |  |  |
|  | 10.2 Secondary | Yard | ydrant |  |  |
|  | 10.3 Detection | Non |  |  |  |
|  | 10.4 Other |  |  |  |  |

11.0 Fire Loading In Area
11.1 None $\qquad$ X (no further analysis required)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Station |
| :--- | :---: | :--- |
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12.0 Equipment and Systems in Fire Area/Zone

| Equipment | $\underline{\text { System }}$ |  | System Train |  |
| :--- | :--- | :--- | :--- | :---: |$\quad$| Safety |
| :---: |
| CO-LT-4096 A |

Instrumentaion \& $\quad \mathrm{CO}$
Cabling
Condensate Storage $\quad$ CO $\quad$ X $\quad$ X
Tank TK-25
$\begin{array}{lllll}\text { Piping \& Valves } & \text { CO } & \text { X }\end{array}$

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
| :--- | :---: | :--- |
| Section F.2 Tab 19 |  |  |
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MUA-F-1-0

| 1.0 | Building | Make Up Air - East |  |
| :--- | :--- | :--- | :--- |
| 2.0 | Fire Area Or Zone |  |  |
|  | $2.1 \quad$ Area Name |  |  |
|  | $2.2 \quad$ Location | MUA-F-1-0 | Make Up Air East <br>  |

3.0 Construction of Area

| 3.1 | Walls | North <br> South <br> East | $\frac{\text { Material }}{\text { Concrete }}$ <br> West | $\frac{\text { Min. Fire Rating }}{\frac{\text { Concrete }}{\text { Concrete }}}$ |
| :--- | :--- | :--- | :--- | :--- |

4.0 Floor Area 205 Sq. Ft. Length 14'-4" Width $14^{\prime}-4{ }^{\prime \prime}$ Height $8^{\prime \prime}-9{ }^{\prime \prime}$
5.0 Volume 1,790 Cu. Ft.
6.0 Floor Drains Nuclear ___ Non-Nuclear ___ None X
7.0 Exhaust Ventilation System Control Building Make Up Air
7.1 Percentage of System's Capacity $\quad 100 \%$
$8.0 \quad 8 \mathrm{Hr}$. Emergency Lighting in Area
8.1 Outside Area at Exit Points

9.0 Operational Radioactivity
9.1 Equipment/Piping
9.2 Airborne
10.0 Fire Protection

Type
10.1 Primary
10.2 Secondary
10.3 Detection

Yes


| No X |
| :--- |
| No X |

10.4 Other

Portable Extinguishers
Yard Hydrant
None ${ }^{-}$
$\qquad$
11.0 Fire Loading In Area
11.1 None X_ (no further analysis required)

[^22]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A |  |  |
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| Page 2 of 2 |  |  |

12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\frac{\text { System Train }}{\text { A }}$ |  | $\underline{B}$ |
| :--- | :--- | :--- | :---: | :---: | | Safety |
| :---: |
| Related |


| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, <br> Appendix A | Rev 6 <br> Section F.2 Tab 20 <br> Page 1 of 2 |
| :--- | :---: | :--- |

DCT-F-*

| 1.0 | Building |  | Ductbanks |
| :---: | :---: | :---: | :---: |
| 2.0 | Fire Area or Zone |  | DCT-F-1A-0, 1B-0, 2A-0, 2B-0, 3B-0, |
|  |  |  | 4A-0, 4B-0, 5A-0 5B-0, 6-0, 7-0 |
|  | $\begin{aligned} & 2.1 \\ & 2.2 \end{aligned}$ | Area Name | Ductbanks |
|  |  | Location | Site |
|  |  | Drawing No | 9763-F-310828-FP; 320251-FP; 300245-FP; |
|  |  |  | 310254-FP; 310248-FP; 310249-FP; 320252-FP |

3.0 Construction of Area

4.0 Floor Area N/A Sq. Ft. Length $\qquad$ Width $\qquad$ Height $\qquad$
5.0 Volume $\qquad$ Cu. Ft.

| 6.0 | Floor Drains | $\mathrm{N} / \mathrm{A}$ |  |
| :--- | :--- | :--- | :--- | :--- |
| 7.0 | Exhaust Ventilation System |  | N/A |
|  | 7.1 | Percentage of System's Capacity | N/A |


| 8.0 | 8 Hr . Emergency Lighting in Area | Yes |  |  |
| :--- | :--- | :--- | :--- | :--- |
|  | 8.1 | Outside Area at Exit Points | Yes | $\square$ |

9.0 Operational Radioactivity
9.1 Equipment/Piping

Yes
Yes
No $\qquad$
10.0 Fire Protection

Type
Ref: Deviation No. 2
SBN-904 Dated 12/2/85
10.1 Primary

N/A
10.2 Secondary

N/A
10.3 Detection

N/A
10.4 Other

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
| :--- | :---: | :--- |
| Appendix A | Section F.2 Tab 20 <br> Page 2 of 2 |  |

11.0 Fire Loading In Area
11.1 None X (no further analysis required)
12.0 Equipment and Systems in Fire Area/Zone

| Equipment | System | $\frac{\text { System Train }}{\mathrm{A}}$ |  | $\underline{B}$ |
| :--- | :--- | :--- | :--- | :---: | | Safety |
| :---: |
| Related |


| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
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## F. 2 RESULTS OF FIRE HAZARD ANALYSIS

This section presents the detailed results of an analysis of the consequences of a fire in each designated fire area and zone. These details are presented on standardized "Fire Hazard Analysis" forms which consolidate all desired information for each designated area and zone. Information provided includes, as applicable to a particular fire area or zone, the type of construction, combustibles, fire protection/detection, safety-related systems ${ }^{*}$ and description of equipment within the area, radioactivity within the area, consequences of a fire with and without suppression, consequences of inadvertent operation or rupture of fire protection equipment, means for containing and inhibiting fires, and protection of redundant equipment within the fire area. The fire load within the total fire area or zone can be found on line 13.2 of the form; the worst fire load within the floor area covered by the combustibles is found on line 14.1.

For-areas which do not include any safety-related system components, analyses were still made to determine if the effects of a fire within such areas could jeopardize adjacent areas containing safety-related systems.

Table 4 identifies by tab the various fire areas and zones located in each building.
Abbreviations of equipment and system used in the fire hazard analysis are as follows:

| Abbreviation | $\frac{\text { System }}{\text { Auxiliary Steam Heating }}$ |
| :--- | :--- |
| ASH | Containment Air Handling |
| CAH | Containment Air Purge |
| CAP | Control Building Air Handling |
| CBA | Containment Building Spray |
| CBS | Component Cooling Water - Primary |
| CC | Chlorination |
| CL | Containment on-line Purge |
| COP | Rod Control and Position |
| CP | Chemical and Volume Control |
| CS | Diesel Generator Air Handling |
| DAH | Drains - Floor |
| DF | Diesel Generator System |
| DG |  |

[^23]| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> STATION |
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| Abbreviation | System |
| :--- | :--- |
| DM | Demineralized Water |
| EAH | Containment Enclosure Air Handling |
| ED | Electrical Distribution |
| EDE | Electrical Distribution - Emergency |
| FO | Fuel Oil |
| FP | Fire Protection |
| FPA | Fire Pumphouse Air Handling |
| FW | Feed Water or Emergency Feedwater |
| HWS | Heating Water System |
| IA | Instrument Air |
| MS | Main Steam |
| NG | Nitrogen Gas |
| NI | Nuclear Instrumentation |
| PAH | PAB Air Handling |
| PW | Potable Water |
| RC | Reactor Coolant |
| RH | Residual Heat Removal |
| RM. | Radiation Monitor |
| RPI | Rod Position Indicator |
| SB | Steam Generator Blowdown |
| SI | Safety Injection |
| SS | Sampling System |
| SW | Service Water |
| WLD | Nuclear Equipment/Floor Drains |
|  |  |


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| :--- | :---: | :--- |

The details on the specific areas and zones analyzed are found behind the tabs listed below:

## Table 4



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| :--- | :---: | :--- |

## Table 4

## Buildings

6. Electrical Tunnels
7. Diesel Generator Building
8. Primary Auxiliary Building
9. Fuel Storage Building

Fire Are
CB-F-S1-0
CB-F-S2-0
ET-F-1A-A
ET-F-1B-A
ET-F-1C-A
ET-F-1D-A
ET-F-S1-0
DG-F-1A-A
DG-F-1B-A
DG-F-2A-A
DG-F-2B-A
DG-F-3C-A
DG-F-3D-A
DG-F-3E-A
DG-F-3F-A
DG-F-S1-0
DG-F-S2-0
PAB-F-1C-A
PAB-F-1D-A PAB-F-1B-Z
PAB-F-1E-A PAB-F-1F-Z
PAB-F-1G-A PAB-F-2A-Z
PAB-F-S1-0 PAB-F-2B-Z
PAB-F-S2-0 PAB-F-2C-Z
PAB-F-3A-Z
PAB-F-3B-Z
PAB-F-4-Z
PAB-F-1J-Z
PAB-F-1K-Z

Tab
6.
7.
8.
9.

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| :--- | :---: | :--- |

## Table 4

## Buildings

10. Waste Processing Building
11. Service Water Pump House
12. Service Water Cooling Tower
13. Containment Enclosure Ventilation Area
14. Fire Pump House
15. Turbine Building
16. Mechanical Penetration Area
17. Non-Essential Switch-Gear Room
18. Condensate Storage Tank
19. Make-Up Air, East

Fire Area

SW-F-1B-A
SW-F-1C-A SW-F-1D-A
SW-F-2-0
CT-F-1C-A
CT-F-1D-A
CT-F-2B-A
CT-F-3-0

FPH-F-1A-A FPH-F-1B-A FPH-F-1C-A
TB-F-1B-A

CST-F-1-0
MUA-F-1-0

CE-F-1-Z
13.
14.
15.

TB-F-1C-Z
TB-F-2-Z
TB-F-E-Z
PP-F-1A-Z
16.

PP-F-2A-Z
PP-F-1B-Z
PP-F-2B-Z
PP-F-3A-Z
PP-F-3B-Z
PP-F-4B-Z
PP-F-5B-Z
NES-F-1A-Z
17.

Fire Zones
W-F-1A-Z
Tab

W-F-1B-Z
TF-F-1-0
W-F-2A-Z
W-F-2B-Z
W-F-2C-Z
W-F-2D-Z
W-F-2E-Z
SW-F-1A-Z
SW-F-1E-Z
18.
19.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A <br> Rection F.2 |
| :--- | :---: | :--- |

## Table 4

## Buildings

20. Ductbanks

Fire Area Fire Zones Tab
DCT-F-1A-0 20. DCT-F-1B-0
DCT-F-2A-0
DCT-F-2B-0
DCT-F-3B-0
DCT-F-4A-0
DCT-F-4B-0
DCT-F-5A-0
DCT-F-5B-0
DCT-F-6-0
DCT-F-7-0

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
| :--- | :---: | :--- |
| Appendix A |  |  |
| Page 1 |  |  |

## Design Basis Fire

1. Diesel oil spills onto the floor of the storage room and is ignited.
2. The flame spreads in all directions (unless obstructed) from the point of ignition at a rate of $3 \mathrm{in} . / \mathrm{sec}$. (1).
3. The burning rate is 8.3 inches of depth per hour (2).
4. The fire burns at the rate until $50 \%$ of the initial oxygen supply is gone (3).
5. The burning rate decreases linearly from the $50 \%$ moment to zero when $100 \%$ of the initial oxygen supply in exhausted.

## Assumptions

1. The heat value of the oil is taken a $19,000 \mathrm{Btu} / \mathrm{lb}$. (4).
2. The specific heat of all gases is taken as that of air at standard conditions.
3. The products of combustion are taken to be carbon monoxide and water. This is a very conservative assumption in that it uses oxygen at a slower rate than would an assumption of carbon dioxide product. The heat value in such a case would be much lower in this case than $19,000 \mathrm{Btu} / \mathrm{lb}$., which assumes complete combustion.
4. Heat transfer to passive heat sinks has been considered. Heat transfer coefficients were calculated on the basis of blackbody radiation for the bare concrete walls and ceiling and steel fuel oil tank directly exposed to the flame, turbulent convection for the remainder of the tank, $1 \mathrm{Btu} / \mathrm{hr} \mathrm{Ft} .^{2}-{ }^{\circ} \mathrm{F}$ outside the room.

## Dimensional Parameters

1. Room size is $40.5 \mathrm{ft} . \mathrm{x} 40 \mathrm{ft}$. and 33.5 ft height.
2. Diameter of the tank is 20 ft . and the length of the straight part is 28 ft .
3. Area of the vent is 4 sq. ft .
4. Heat transfer surfaces exposed to direct radiation are $1,429 \mathrm{sq}$. ft . concrete ceiling ( 4 ft . thick), 1,393 sq. ft , concrete walls ( 3.5 ft . thick) and $909 \mathrm{sq} . \mathrm{ft}$. steel ( $1 / 2$ inch thick), convective heat transfer being considered for the rest of the tank surface.

| SEABROOK <br> STATION | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
| :--- | :---: | :--- |
| Pagendix A |  |  |

## Method Of Analysis

1. Flow to and from the room is calculated based on room pressure by the computer code CONTEMPT, which also calculates the room temperature and pressure transients, as well as the temperature profiles in the concrete.
2. Credit is taken for the depletion of oxygen due to venting during the early, maximum burn, stage of fire in the following manner:
(a) Based on assumptions listed above, the rate of heat addition to the room is $39.17 \mathrm{t}^{2}$ $\mathrm{Btu} / \mathrm{sec}$. ( t in seconds), and at $19,000 \mathrm{Btu} / \mathrm{lb}$, the mass addition rate is $2.06 \times 10^{-3}$ $\mathrm{t}^{2} \mathrm{lb} / \mathrm{sec}$.
(b) Conservatively using standard conditions, there are $3,058 \mathrm{lbs}$. air initially of which 710 lb . is oxygen.
(c) The mass and energy addition rates in (a), above are inputted to CONTEMPT which is run 100 or so seconds of fire at maximum burn. From the output of this run $R(t)$ the venting rate from the room, and $M(t)$ the total lbs. of air in the room are ascertained as tabular functions of time.
(d) Based on the oil consumption rate, $2.06 \times 10^{-3} \mathrm{t}^{2} \mathrm{lb} / \mathrm{sec}$., a typical diesel fuel oil composition (5) and combustion products consisting Of CO and $\mathrm{H}_{2} \mathrm{O}$, the oxygen consumption rate due to combustion is found to be $3.96 \times 10^{-3} \mathrm{t}^{2} \mathrm{lb} / \mathrm{sec}$.
(e) The equation:
$\frac{d 0(t)}{d t}=-3.96 \times 10^{-3} t^{2}-\frac{R(t)}{M(t)} 0(t)$
which determines $0(t)$, the time-dependent mass of oxygen in the room, is numerically integrated to find the time at which $50 \%$ of the initial amount of oxygen is exhausted.
(f) The period of maximum burn rate is thus obtained as the time of $50 \%$ oxygen remaining in the room.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
| :--- | :---: | :--- |
| STATION | Diesel Fuel Storage Room Fire Analysis A | Page 3 |

3. After the maximum burning time, although the venting rate is considerable at that time, no credit is taken for further loss of oxygen through this means. The fire burns at a linearly decreasing rate until the remaining oxygen is consumed. It is recognized that during the late stages of the fire, as the room cools, air will actually be drawn into the room through the vent sustaining some combustion. It should be noted, however, that the mechanism is self-defeating and that air can enter only when the temperature of the room is dropping, thus the peak temperatures will never be approached again. A slow, smoldering condition will result.

## RESULTS

## Case I: Without Spray Actuation

In the case when the spray fails to actuate, the room pressure reaches a maximum of 4.2 psig at 29 seconds when $50 \%$ of the oxygen is exhausted, and the room temperature peaks at $1,582^{\circ} \mathrm{F}$ at 41 seconds. Figure 1 shows the transient pressure/temperature responses. The ceiling concrete temperature reaches a maximum of $774^{\circ} \mathrm{F}$ at 135 seconds. The fire continues to burn till 237 seconds. Figure 2 shows the temperature profiles through ceiling concrete.

## Case II: With Spray Actuation

In the case when the spray with a flow rate of 625 gpm at $90^{\circ} \mathrm{F}$ temperature actuates automatically when the room temperature reaches $200^{\circ} \mathrm{F}$, the situation greatly improves. The spray starts at approximately 18 seconds when the rate of rise of pressure/temperature is significantly reduced resulting in much less severe transients. No credits have been considered for removal of heat due to vaporization of spray water which is expected to reduce the consequences further.

The room pressure reaches a maximum of 0.9 psig at 37 seconds when $50 \%$ of the oxygen is exhausted, and the room temperature peaks at $611^{\circ} \mathrm{F}$ at 41 seconds. Figure 3 shows the transient pressure/temperature responses. The fire continues for 157 seconds. The ceiling concrete temperature reaches a maximum of $316^{\circ} \mathrm{F}$ at 70 seconds and the temperature profiles are presented in Figure 4.

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix A |
| :--- | :---: | :--- |
| STATION | Diesel Fuel Storage Room Fire Analysis | Appendix <br> Page 4 |

## References

1. Mackinven, R., Hansel, J.G., and Glassman, I., "Influence of Laboratory Parameters on Flame Spread Across Liquid Fuels". Combustion Science \& Technology, Volume 1 - pp. 293-306, 1970
2. Blinor, V.1., and Khidiakor, G.N., "Certain Laws Governing Diffusive Burning of Liquids", Fire Research Abstract and Review, Volume - 1 pp. 41-44, 1958
3. Zabetokis, G.M., "Flammability Characteristics of Combustible Gases and Vapors", Bulletin 627, Bureaus of Mines, U.S. Dept. of Interior, 1965
4. Perry, J.H., et al.; Chemical Engineering Handbook, 4th Edition, pp.142-143, McGrawHill 1963
5. Marks' Handbook of Mechanical Engineering, p. 7-22, California Fuel Oil (other oils with higher carbon and hydrogen fractions consume oxygen more rapidly). (The corresponding heat rate for this oil was not used.)

| SEABROOK | Evaluation and Comparison to BTP APCSB 9.5-1, | Rev 6 <br> Appendix B |
| :--- | :---: | :--- |
| STATION | Reactor Coolant Pump Fire Analysis | Appendix B <br> Page 1 |

## Design Basis Fire

1. RCP lube oil leaks from the pump, is heated close to its flash point while traveling over piping, falls to the floor of the containment and is ignited.
2. The oil spill is limited to an area of $150 \mathrm{ft}^{2}$.
3. The entire 265 gallons of lubricating oil in the pump burns.

## Assumptions

1. The heat value of the oil is $150,000 \mathrm{Btu} / \mathrm{gal}$.
2. The burning rate is equivalent to 5.0 inches of depth per hour.
3. Heat transfer to passive heat sinks has been considered. A heat transfer coefficient of 2 $\mathrm{Btu} / \mathrm{ft}^{2}-\mathrm{hr}-{ }^{0} \mathrm{~F}$, characteristic of laminar convection, was conservatively used for transfer to the steel and concrete within the containment and to the containment walls. No radiative heat transfer has been accounted for.
4. Heat removal by active heat sinks (Fan coolers) was also considered. The five fan coolers just balance the containment sensible heat generation rate $\left(5.85 \times 10^{6} \mathrm{Btu} / \mathrm{hr}\right)$ at $120^{\circ} \mathrm{F}$ containment atmosphere temperature. At a temperature of $300^{\circ} \mathrm{F}$, the total capacity of the fan coolers is $25 \times 10^{6} \mathrm{Btu} / \mathrm{hr}$ (or $19.15 \times 10^{6} \mathrm{Btu} / \mathrm{hr}$ in excess of containment sensible heat generation rate). In actuality, the capacity is somewhat higher, thus that used is conservative.
5. The burning of the oil would add approximately 1900 lbs . to the containment atmosphere mass. This is neglected. Doing so yields a slightly higher peak temperature and an insignificantly lower peak pressure. The temperature transient is more severe and therefore the omission is conservative.
6. The initial temperature and pressure of the containment atmosphere are $120^{\circ} \mathrm{F}$ and 15.2 psia, respectively.

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7. Each Seabrook Station reactor coolant pump contains approximately 240 gallons of oil. Each collection tank has a capacity of 320 gallons. The tanks were sized to hold the entire inventory of one pump plus $25 \%$. However, if the lube oil systems for two pumps were to fail simultaneously, there would be an excess of 160 gallons of oil per tank. In order to contain this excess oil, a seismically designed dike will be built around the tank. The tanks and their dikes are located such that the excess oil does not present a fire hazard to any safety-related equipment. Additionally, there is no ignition source near the diked area. (Ref.: SBN-762, dated February 8, 1985.)

## Method of Analysis

1. Based on the assumptions above, the duration of the fire is calculated to be 34 minutes with a constant heat addition rate of $1.169 \times 10^{6} \mathrm{Btu} / \mathrm{hr}$.
2. The computer code CONTRAST-S was used to calculate the temperature and pressure transients due to the fire.

## Results

The maximum temperature obtaining in the containment is $253^{\circ} \mathrm{F}$ and the maximum pressure is 4 psig . Both peaks occur at 34 minutes, at which time the fire burns itself out. The temperature transient is shown in Figure 1 and the pressure transient is shown in Figure 2. Both temperature and pressure decay rapidly as soon as burning stops.

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## RESUME

## ALFRED S. BOCCHINO

United Engineers \& Constructors Inc.
EDUCATION B.S.M.E., 1939, University of Alabama
PROFESSIONAL Delaware New Jersey
ENGINEERING Missouri Pennsylvania
REGISTRATION New Hampshire
MEMBERSHIPS American Society of Mechanical Engineers
New Jersey Society of Professional Engineers
National Society of Professional Engineers
Society of Fire Protection Engineers
SUMMARY Over thirty-three years of experience in the engineering and design of power plants, manufacturing facilities, chemical plants and oil refineries. Developed the scope of various projects, specified equipment and supervised the engineering and design of fire protection systems and mechanical facilities, both process and service. Especially competent in plant fire protection including water supply, fire pumps, yard mains, automatic sprinkler system, etc. and the plant service area consisting of plumbing and drainage, waste treatment facilities, dust collection, central vacuum cleaning systems, heating, ventilating, air conditioning and special nuclear related air cleaning systems. Responsible for the coordination of the engineering and design for complete service and fire protection facilities of several power plants, both fossil and nuclear, and manufacturing plants. Responsibility in the nuclear field included preparation of preliminary safety analysis reports, final safety analysis reports, environmental reports, fire protection system design, and other licensing activities for pressurized water reactors (PWR) and High Temperature Gas-Cooled Reactors (HTGR) power plants.

EXPERIENCE United Engineers \& Constructors Inc.
Philadelphia. Pennsylvania 19101

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present

May 1972 to
October 1975

January 1971 to
November 1974

July 1970 to
January 1974

October 1975 to Consultant - Mechanical Services Engineer
Responsible for the review, comment and approval of Mechanical Services related work, including plant fire protection, on fossil and nuclear power plants designed by UE\&C. The Branch Technical Position APCSB 9.5-1 and Regulatory Guide 1.120 are used as guides in the review of fire protection for safety-related systems and equipment.

Supervising Discipline Engineer
Project - Delmarva Power \& Light Company, Summit Power Station, Summit Bridge, Delaware, two 770 Mw HTGR Units No. 1 and Unit No.
Responsible for engineering the heating, ventilating and air conditioning systems; plant fire protection system, including yard hydrant system complete with water storage and pumping facilities, building standpipe systems, sprinkler systems, pre-action sprinkler systems, deluge systems, specified use of $\mathrm{CO}_{2}$ and Halon extinguishers. This project was not completed.

## Supervising Discipline Engineer

Project - Philadelphia Electric Company, Eddystone Generating Station, two 400 Mw crude oil-fired peaking generating units Nos. 3 and 4. Responsibilities same as for period May 1972 to October 1975. In addition, engineered automatic foam fire protection system for crude oil spill areas resulting from possible oil pipe rupture.

Supervising Discipline Engineer
Project - Atlantic City Electric Company, B. L. England Station. Conversion of Low existing coal-burning units to burn crude oil.
Design of new 150 Mw crude oil-fired plant. Units Nos. 1, 2 and 3. Responsibilities same as for period May 1972 to October 1975. In addition engineered (1) foam fire protection system for crude oil storage tanks; (2) a combustible gas detection system for continuously detecting and indicating the presence of combustible gas fumes in selected plant areas; (3) special ventilating systems for removal of gas fumes from burner areas.

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December 1970 to
July 1973

March 1971 to
February 1973

April 1969 to June 1972

August 1967 to
September 1969

September 1966 to
February 1971

November 1965 to
December 1973

Supervising Discipline Engineer
Project - Public Service Electric \& Gas Company, Sewaren Generating Station; two 400 Mw oil-fired peaking units, Unit Nos. 7 and 8. Responsibilities same as for period May 1972 to October 1975. This project was not completed.

Supervising Discipline Engineer
Project - Puerto Rico Water Resources Authority, Aguirre Nuclear
Plant, Unit No. 1, P.W.R. units.
Provide consulting engineering services on plant service facilities. This project was not completed.

Supervising Discipline Engineer
Project - Delmarva Power \& Light Company, Vienna Power Station; 150 Mw oil-fired generating unit, Unit No. 8.
Responsibilities same as for period May 1972 to October 1975, except no Halon extinguishing equipment.

Supervising Discipline Engineer
Project - Delmarva Power \& Light Company, Indian River Power Station; 150 Mw coal-fired Unit No. 3.
Responsibilities same as for period May 1972 to October 1975, except no pre-action systems, Halon extinguishing equipment water supply or pumping equipment.

Mechanical Supervising Engineer
Project - Alleghony Power System, Hatfield Power Station, three 500 Mw coal-fired units, Units Nos. 1, 2 and 3.
Responsibilities same as for period May 1972 to October 1975, except no Halon extinguishing equipment.

Mechanical Supervising Engineer
Project - Consolidated Edison Company of New York, Indian Point Generating Station, Units Nos. 2 and 3, P.W.R. units.
Responsibilities same as for period May 1972 to October 1975, except no Halon extinguishing equipment. Fixed foam systems used on turbine oil storage tanks and associated equipment.

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April 1965 to
July 1966

April 1964 to
March 1968

June 1964
to
February 1965

March 1961 to
November 1962

May 1961
to
March 1962

September 1960 to
May 1961

Mechanical Supervising Engineer
Project - Pickands Mather \& Company, Taconite Harbor Power Station, Unit No. 3, coal-fired.
Extended yard fire protection and building standpipe system. Specified deluge spray system for transformers.

Mechanical Supervising Engineer
Project - Union Electric Company, Sioux Power Plant, Units Nos. 1 and $2,500,000 \mathrm{kw}$ capacity coal-fired units.
Responsibilities same as for period May 1972 to October 1975, except no Halon extinguishing equipment.

Mechanical Supervising Engineer
Project - United States Steel Corporation, Clairton Works. Addition to Boiler House No. 3.
Extended yard fire protection system, added transformer deluge water spray systems.

Mechanical Supervising Engineer
Project - Connecticut Light \& Power Company, Norwalk Harbor Station; 165,000 kw capacity, Unit No. 2, coal-fired.
Responsibilities same as for period JuLy 1972 to October 1975, except no pre-action sprinkler systems, Halon extinguishing equipment or water supply and pumping equipment.

Mechanical Supervising Engineer
Project - Texas Electric Company, Handley Station; 35,000 kw capacity, gas-fired outdoor plant.
Responsibilities same as for period May 1972 to October 1975, except no pre-action sprinkler systems, standpipe systems or Halon extinguishing equipment.

Mechanical Supervising Engineer
Project - National Aniline Division, Allied Chemical Corporation, Polyamide Fiber Plant, Hopewell, Virginia.
Responsibilities same as for period May 1972 to October 1975, except no pre-action sprinkler systems or Halon extinguishing equipment.

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February 1960 to
September 1960

October 1957 to
February 1960

June 1957 to
October 1957

May 1955
to
June 1957

August 1939 to
May 1955

Mechanical Supervising Engineer
Project - Western Electric, Kansas City, Missouri, Electronic Facilities covering $11 / 2$ million square feet of building area.
Responsibilities same as for period May 1972 to October 1975, except no pre-action sprinkler systems or Halon extinguishing equipment.

Mechanical Supervising Engineer
Project - Connecticut Light \& Power Company, Norfolk Harbor Station, 150,000 kw capacity, Unit No. 1, coal-fired.
Responsibilities same as for period May 1972 to October 1975, except no pre-action sprinkler systems or Halon extinguishing equipment.

Mechanical Supervising Engineer
Project - Connecticut Light \& Power Company, Devon Generating Station; $112,000 \mathrm{Kw}$ capacity, Unit No. 8, coal-fired.
Responsibilities same as for period May 1972 to October 1975, except no pre-action sprinkler systems or Halon extinguishing equipment.

Mechanical Supervising Engineer
Project - Delaware Power \& Light Company, Indian River Power Station; two 85,000 Kw units, Units Nos. 1 and 2, coal-fired. Responsibilities same as for period May 1972 to October 1975, except no pre-action sprinkler systems or Halon extinguishing equipment.

This time period is no longer relevant to the matter at hand and is not included in this resume.

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## RESUME

EDWARD A. SAWYER

Fire Protection Coordinator
Yankee Atomic Electric Co.

EDUCATION 1977 - Series of short intensive courses on Fire Protection for Nuclear Power Plants, Fire Protection for Nuclear Power Plant Operating Personnel, and Fire Hazard Analysis for Nuclear Power Plant. All given by NATLSCo and Professional Loss Control, Inc.

September 1976 - December 1976 - Worcester Polytechnical Institute. Engineering Methodology for Building Fire Safety Evaluation.

August 1976 - University of Wisconsin-Extension. Fire Safety Design for Buildings.

1965 - Northeastern University - BS in Electrical Engineering.
MEMBERSHIPS Society of Fire Protection Engineers
National Fire Protection Association

## EXPERIENCE Yankee Atomic Electric Company

July 1976 to Present

Fire Protection Coordinator directly responsible for the overall preparation and implementation of the fire prevention and protection programs for three operating nuclear power plants - Yankee Rowe, Vermont Yankee, and Maine Yankee. Specifically responsible for the performance of the fire hazard analysis at the plants, and the development and implementation of recommendations concerning the updating and backfitting of the plants to the applicable requirements contained in Appendix A to the Branch Technical Position on Fire Protection, APCSB 9. 5-1, Regulatory Guide 1. 120, and any further NRC requirements in the area of fire protection. Responsible for insuring, the development of fire prevention and protection procedures, including programs for the training of the plant staff and plant fire brigade. Responsible for ultimate review and approval of the design of Seabrook Station and NEP 1 and 2 with respect to coordination of design with fire protection requirements.

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Responsible for the ultimate review and approval of the fire hazard analysis and the Fire Protection Reevaluation Report. Responsible for dealing with the insurers for the operating plants in matters relating to fire protection.

November 1971 Assistant to the Project Engineer for Vermont Yankee Nuclear Power

August 1974 to July 1976

January 1972 to
August 1974
to January 1972

September 1970
to
November 1971

Project Manager on the Central Maine Power Company Nuclear Project directly responsible for coordinating the development of project design and engineering schedules with the principal contractors, administration of the Project Engineers under my direction, developing, monitoring and controlling project costs: including dealing with insurers of the project; generally responsible for the licensing of the project and for engineering, design, and quality assurance activities related to the work of the principal contractor organizations associated with the project.

Electrical Project Engineer on the Seabrook Nuclear Power Station. Duties consisted of supervision of the Electrical Engineering effort of the A/E and Yankee in PSAR submittal and in plant design, and responsibility to the Project Manager for licensing activities, engineering coordination, notification of any cost or schedular problems, including dealing with NELPIA in areas of fire protection design.

Project Engineer on the engineering, construction and testing of an Advanced Off-Gas Control System for the Vermont Yankee Nuclear Power Plant. Duties consisted of supervising the engineering, scheduling and cost control efforts of the $\mathrm{A} / \mathrm{E}$ and Yankee personnel; and following of the construction effort and test effort for the system. Plant. Duties consisted of aiding in plant licensing, plant licensing, writing of plant Environmental Report.

Vermont Yankee Nuclear Power Plant
Technical Assistant to the Plant Maintenance Supervisor. Duties consisted of aiding Maintenance Department personnel in preparing the $\mathrm{p}-\mathrm{l}$-ant for commission, ranging from work on Microwave Communications, Metering, and Relaying to work on large motors, switchgear, and power transformers.

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January 1968 to
September 1970

Yankee Atomic Electric Company
Engineer in the Project group for the Vermont Yankee Nuclear Power Plant. The Project group coordinated the work done on the plant by the Architect Engineer, Nuclear Steam Supplier, and the various other vendors and suppliers. Work was mainly in the Electrical and Instrumentation coordination and design, with some excursions into Nuclear and Mechanical areas, including working with NELPIA in developing fire protection systems.

April 1963 to June 1965

New England Electric System

Brayton Point Generating Station, Somerset, Massachusetts. Co-op employment as Assistant to the Electrical Department Foreign of a 500 M Thermal Generating Plant - Maintenance planning, job planning, parts ordering, responsibility for maintenance of fire protection systems.

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HAZARDS ANALYSES OF SEABROOK STATION
CHARCOAL FILTER UNITS
Seabrook Station
Public Service Company of New Hampshire
New Hampshire Yankee Division

Revision 1
November 1991


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Yankee Atomic Electric Company Nuclear Services Division
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\section*{INTRODUCTION}

This report describes a Hazards Analysis conducted on Seabrook Station's filter units, which contain charcoal beds/cells. Table 1 identifies Seabrook's nine (9) filter units and theix location.

\section*{BACKGROUND}

Seabrook's approach to a charcoal fire within the filter units is fire prevention and detection as outlined within the guidelines of Item II.B(3) of 10CFR50, Appendix R, which states, "specify measures for fire prevention, fire detection, fire suppression, and fire containment, and alternative shutdown capability as required for each fire area containing structures, systems, and components important to safety in accordance with NRC guidelines and regulations."

To address internal charcoal fires, an analysis was conducted on all Seabrook filter units, which contain charcoal beds/cells, to determine the maximum temperatures of the charcoal adsorber sections, due to decay beat from iodine and its daughter product decay without air flow. This analysis showed that the overall maximun temperature would be 1 imited to \(170^{\circ} \mathrm{F}\). Additional analyses indicate that the maximum temperature for the HEPA filters (due to decay heat from the particulate iodines accumulated in these filters) will be limited to \(187^{\circ} \mathrm{F}\). These temperatures are well below the maximum limit of \(300^{\circ} \mathrm{F}\) recommended in ANSI-NSO9-1980. Thus, there is no possibility of an internal charcoal fire due to decay heat.

Seabrook's charcoal adsorber filters are also protected from external fires since they are contained in a combination of heavy metal casing, wire debris screens, and fire retardant HEPA filters as recommended in Regulatory Guide 1.52, Design, Testing, and Maintenance Criteria for Post-Accident Engineered - Safety Feature Atmosphere Cleanup System Air Filtration and Adsorption Units of Light-Water-Cooled \(]\) Nuclear Power Plants, Revision 2, March 1978.

Further, transient combustibles are limited administratively. Any welding or open flame sources will be controlled and limited. A fire watch will be maintained per plant administrative procedures during these activities. These precautions will prevent external sources from causing internal combustion to the charcoal beds/cells.

However, a fire bazard analysis is developed in this report to address the effects of a postulated charcoal fire in the filter units and its impact on equipment needed for safe shutdown. A realistic, but conservative approach was used to model the charcoal fires since charcoal is a slow burning medium.

DIScussion
The following assumptions were used in this hazard analysis.
1. Fire will be detected by reliable and early warning system.
2. From detection, which is alarmed in Control Room, Operations per Operating Procedures will shutdown air flow to the filter units. Assume five minutes time from alarm conditions to shutdown of ait flow. Charcoal is assumed to be ignited in this time frame.
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3. The Fire Brigade will respond to the charcoal filter within 20 minutes from notification by the Control Room for all protected plant areas except Containment. This notification is per Operating Procedures. For a fire within Containment, the Fire Brigade will respond within 90 minutes. (See Engineering Evaluation EE-05-033, Revision 00.)
4. Ignition of the charcoal starts at the top of the charcoal bed/cell. This is assumed conservative since a fire located lower in the bed/cell would burn the retaining mesh and drop the charcoal from the air flow path precluding rapid fire propagation.
5. Since a fire cannot be started due to internal decay heat, the fire must be started from an external source. Assume an outside source is carried into the filter unit. All the units have HEPA filters on the inlet before the charcoal bed. Each HEPA filter section assembly is made up of a grouping of HEPA filter elements 24 " x 24 " x 11-1/2". Each element is a throwaway, extended medium, dry-type filter, which are open face, rectangular, fire-resistance type design for radioactive service. Assume the source carried internal by air flow totally ignites one HEPA filter element, \(2^{\prime} \times 2^{\prime}\). This \(2^{\prime} \times 2^{\prime}\) filter element is assumed to ignite a \(4 \mathrm{ft}^{2}{ }^{2}\) area of the charcoal bed/cell.
6. Air flow through the charcoal bed/cell is assumed to be from the start of ignition. \(4 \mathrm{ft}{ }^{2}\) area of charcoal will burn under air flow condition for a period of 5 minutes time. At this point forced air flow has stopped and the resulting fire will be analyzed under natural draft air flow.
7. Air flow velocity through the charcoal during forced ventilation is 40 feet per minute which is Seabrook's charcoal bed/cell design velocity.
8. Further assumptions are used in Appendix I, "Evaluation of Charcoal Filter Unit Fires at Seabrook Station," 9-29-86 by Professional Loss Control, Inc. and are noted in that Appendix.

The Hazard Analysis consist of 3 parts, (1) Determination of charcoal bed burning rates, (2) a heat transfer model of the charcoal beds/cells and (3) effects of the heat transfer on safe shutdown equipment.

\section*{(1) Determination of Charcoal Bed Burning Rates}

A charcoal fire test was conducted by NUCON in their ASTM D3466 Test Rig. Data from this test was used by Professional Loss Control, Inc. (PLC) in their unsteady state heat transfer model of each of Seabrook's filter units, which contain charcoal beds/cells, excluding CBA-F-38 and CBA-F-8038. Each Seabrook filter was reviewed separately. NUCON's ASTM D3466 Test conducted for Seabrook used the same type of charcoal used in Seabrook's charcoal beds/cells. The test normally is performed at 100 feet per minute air velocity, however, 40 FPM velocity was used which is Seabrook's filter design velocity. The bed depth is normally 1.0 inch deep.

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For Seabrook's test a 2.0 inches deep bed was used which is the limit of the ASIM D3466 apparatus. Seabrook's bed depth is 4.0 inches. Use of the test data by PLC is conservative since the test was conducted under forced air flow over a one hour period. Seabrook's filter unit heat transfer model assumes five minutes time from charcoal ignition to shutdown of air flow; where-as air flow will be shutdown five minutes after detection of a potential fire, which most likely occurs before sufficient temperature is available to ignite the charcoal.

A fire wind tunnel (FWT) test was conducted by NUCON on a 24 inch \(x 24\) inch face area carbon adsorber specimen. The depth of the bed tested was 4.0 inches. Again, the charcoal used was the same type used at Seabrook, \(2 \%\) KI and \(2 \%\) TEDA impregated carbon.

The charcoal was ignited by preheating inlet air to the charcoal specimen. The specimen started burning approximately 6 minutes after CO production levels of 50 ppm were measured. Air flow was then continued for an additional 5 minutes, then stopped. Inlet and outlet temperatures were then monitored for one hour. Seabrook's anticipated alarm setpoint for \(C O\) is 50 ppm and the normal background level is 2 ppro.

The purpose of the FWT test was to look at the actual test size modeled by PLC under fire conditions.

Air flow conditions under forced ventilation were the same for the FWT test versus Seabrook's filter unit design velocity. Once the ventilation was stopped and natural drafting began, the FWT test was no longer similar to Seabrook because of duct configuration differences. Seabrook's filter units have outlet dampers, long HVAC duct rums, and in some cases inlet dampers which are isolated once the filter fans are shutdown. Thus, natural drafting through Seabrook's filters would be small. The FWT test with natural drafting indicates the charcoal fire will contain itself to a limited fire with decreasing temperature after stopping forced ventilation.

Results of the FWT test show, under conditions used in the PLC model, carbon loss for a test duration of one hour was 4.53 lbs which is approximately \(10 \%\) of the test dry carbon weight. Also that co levels increase well above normal environment levels long before a fire starts.

\section*{(2) Heat Transfer Model}

The PLC unsteady heat conduction analysis looked at each charcoal filter unit, except CBA-F-38 and CBA-F-8038, to determine the net heat trancfer to the filter housing surface based on charcoal temperature data supplied by NUCON. Radiation and convection heat transfer was also considered in PLC's analysis.

Radiation Heat Transfer from the fire was considered, taking into account the geometry of each of the filter units. The HEPA filters have a nominal \(24^{\prime \prime} \times 24^{\prime \prime}\) outside dimensions with a \(22^{\prime \prime} \times 22^{\prime \prime}\) steel mounting frame opening, which limits the burning material to one HEPA filter size. The burning charcoal surface area was conservatively assumed to be a 24 -inch square. The larger burning surface area accounts for any fire propagation under the five minute forced ventilation period. The temperatures used in the analysis were measured within the charcoal bed on the outlet side. The highest of any of the temperatures measured was also used. Radiation Heat Loss from the steel housing to its surroundings was also considered.

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For convective heat transfer, forced convection within the filter housing was neglected. If accounted for, the forced air stream would be beated and enhance th heat removal from the housing. Therefore, this assumption is conservative. Free convection heat transfer was considered on the outside of the filter housing.

Attachment II gives the detailed methodology and results of the analysis.
The following conclusions are drawn from a fire involving the charcoal beds/cells in the filter units.
1. The worst case maximum localized steel plate housing temperature was calculated to be \(704^{\circ} \mathrm{F}\). This temperature is substantially below that required for structural failure of the steel housing.
2. Structural failure of any steel beam or column in the vicinity of these filter units cannot be caused by heat transfer from the filter housing.
3. The maximum radiant heat emissive flux from the housing at \(704^{\circ} \mathrm{F}\), calculated to be less than \(10 \mathrm{KW} / \mathrm{m}^{2}\), is less than half the critical radiant flux necessary to ignite the worst case cable jacket materials as determined by EPRI sponsored tests at Factory Mutual Research Corporation (EPRI NP-1200, Part 1).

\section*{(3) Safe Shutdown Equipment Review}

From the conclusions of the heat transfer model there would be no structural steel failures in the vicinity of Seabrook's charcoal filters. Thus no safe shutdown equipment would be effected due to steel failures. Equipment further than three feet from the filter units also would not be effected based on the maximum heat flux from the housing.
An evaluation of safe shutdown equipment was conducted looking at the equipment within and including three feet from each of the filter units.

CBA-F-38, 8038 - No charcoal fire modeling was done on these filters. It is assumed that a charcoal fire will cause loss of all equipment within its fire area (i.e., CB-F-3B-A). Seabrook's present Appendix R Safe Shutdown Study shows this to be acceptable. Also there is no concern of damage to structural steel since all this steel in this fire area is fire proofed.

CAP-F-40 - There is no safe shutdow equipment used during a fire in this fire area, PAB-F-3A-2, within and including three feet, of CAP-F-40.

CAB-F-4Q - There is no safe shutdown equipment used during a fire in this fire area, \(\mathrm{C}-\mathrm{F}-3-\mathrm{Z}\), within and including three feet of CAB-F-40.

EAF-F-9. 69 - There is no safe shutdown equipment used during a fire in this fire area, CE-F-1-Z, within and including three feet of EAB-F-9,69.

EAB-F-4he 74 - There is no safe shutdown equipment used during a fire in this fire area, FSB-F1-A.
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\(\mathrm{PAB}-\mathrm{F}-16\) - There is no safe shutdown equipment used during a fire in this fire area PAB-F-4-Z, within and including three feet of PAB-F-16.
conclusion
The hazards posed by the heating of the steel housing from a charcoal bed/cell filter fire, under the operational guidelines to shutdown forced ventilation of the filter in question, will not jeopardize the safe shutdown of Seabrook Station.
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\end{tabular}
TABLE 1
\begin{tabular}{|c|c|c|c|c|}
\hline Filter ID & Safety/Non & Meets RG_1.52 & Area Detection & Fire Area \\
\hline EAR-F-9 & Safety & Yes & Yes & \begin{tabular}{l}
CE-F-1-Z Containment Enclosure \\
EL 21' \(6^{\prime \prime}\)
\end{tabular} \\
\hline EAR-F-69 & Safety & Yes & Yes & CE-F-1-Z Containment Enclosure EL \(21^{\prime} 6^{\prime \prime}\) \\
\hline FAH-F-41 & Safety & Yes & Yes & FSB-F1-A Fuel Building EL \(84^{\prime} 0^{\prime \prime}\) \\
\hline FAH-F-74 & Safety & Yes & Yes & FSB-F1-A Fuel Building EL \(84^{*} 0^{\prime \prime}\) \\
\hline CAH-F-8 & Non & No & Yes & C-F-3-2 Containment \\
\hline PAB-F-16 & Non & No & Yes & PAB-F-4-Z Primary Auxiliary Building EL 81' \(\mathbf{0 '}^{\prime \prime}\) \\
\hline CAP-F-40 & Non & No & Yes & PAB-F-3A-2 Primary Auxiliary Building EL 53' \(0^{\prime \prime}\) \\
\hline CBA-F-38 & Safety & Yes & Yes & CB-F-3B-A Control Room HVAC Equipront Room EL 75' \\
\hline CBA-F-8038 & Safety & Yes & Yes & CB-F-3B-A Control Room HVAC Equipment Room EL 75' \\
\hline
\end{tabular}

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\begin{abstract}
INTRODUCTION
This report describes an engineering analysis conducted to characterize the hazard of a fire involving the charcoal filter unfts at the seabrook station. An unsteady-state heat conduction analysis has been performed to predict the local temperature rise in the plate steel tousing exposed to a charcoal filter fire for each of seven air handing units.

\section*{BACKGROUND}

Charcoal filter beds are installed in the seven (7) air handifing unfts identified in Table 1. Inside the housing are numerous charcoal filter bed cells. The number of cells within a housing enclosure ranges fram 4 to 28. The charcoal ignition source is assumed to be external to the unit. The configuration of aif cleaning systems is such that the charcoal absorbers are preceded by HEPA filters. The HEPA filter mounting frame is a steel structure with 22 inch \(\times 22\) inch openings. Therefore, no larger burning material than one \(H E P A\) filter size could enter the carbon bed. Anything larger would be stopped by the KEPA mounting frame structure even If it would penetrate the preceding components. This was the reason for the selection of a 24 inch \(\times 24\) inch exposure to a single carbon cell for both the FST test and subsequent engineering analysis.

An unsteady-state heat conduction andiysis was performed on the steel housing. Since the heat conduction within the steel plate occurs very rapidly, a lumped heat capacity approach could be applied to simplify the mathematics involved. The steel housing was considered to receive radiant heat from the buming charcoal bed. Radiative and convective heat losses from the steel housing to the surfoundings were included. A detailed description and the equations for the analysis are included in Appendix \(A\).
\end{abstract}
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\end{tabular}

TABLE 1
DIMENSIONS OF CHARCOAL SECTION OF UNITS
\begin{tabular}{|c|c|c|c|}
\hline Unit & A & B & C \\
\hline PAH-F-16 & 5'1" & 12'2" & \(26^{\prime \prime} 7^{\prime \prime}\) \\
\hline \[
\begin{aligned}
& \text { EAK-F-9 } \\
& \text { EAH-F-69 }
\end{aligned}
\] & 5'1" & 5'6" & 3'6" \\
\hline \[
\begin{aligned}
& \text { FAH-F-41 } \\
& \text { FAH-F-74 }
\end{aligned}
\] & 5'1" & 10'3" & 14'8" \\
\hline CAP \(-5-40\) & 5'1" & 10'0' & 9'11" \\
\hline CAH-F-8 & 2'6" & 54" & 8'0" \\
\hline
\end{tabular}

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\section*{TABLE 2}
(Table 1 from September 15, 1986 , "Iodine Adsorber Fire Test" by Nuclear Consulting Services, Inc.)
```

08Pi942 - 3 Sept 1986
Test Date

```

Carbon ignition followed by rasidual heating (1.e. air flow continued but best off).

Hethod: ASTM D3466 except: 40 FPM, 2 inch bed depth and raat beat up
Material: Dry air and wuSorb EITBC II Lot 45/10
Starting condition: \(25^{\circ} \mathrm{C}\)
Ignition oceurrod at an upper bed (outlot) temperature of approximately \(400^{\circ} \mathrm{C}\), lower bed (inlat) temperature of \(285^{\circ} \mathrm{C}\), air inlet temp. \(285^{\circ} \mathrm{C}\).

Temperatures arter ignition:

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FIGURE 1


Temperature History in Charcool Bed
\begin{tabular}{|l|c|l|}
\hline \begin{tabular}{l} 
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\section*{DISCUSSION}

The temperature rise of the steel housing on the seven charcoal fititer units of concem is presented in Tables 3 through 7. As noted in the tables, the naximum localized housing temperature for Unfts PAH-F-16 (see Table 3), CAP-F-40 (see Table 5), FNH-F-42 and FAH-F-74 (see Table 6), are within \(50^{\circ} \mathrm{F}\) of one another (between 411 and \(461^{\circ} \mathrm{F}\) ). The surface temperatures present a minimal hazard to fixed equipment or cabling unless mounted directly on the housing, as well as to personnel, unless they came into contact with the enclosure itself.

The maximum localized temperature predicted for Units EAH-F-9 and EAH-F-69 is \(704^{\circ} \mathrm{F}\) (see Table 4). The increased temperature is due to the reduced size of the housing, which includes less stetl through which the heat can be diffused. Still, this temperature would not appear to be at a level or exist for a sufficiently long duration to pose a serious exposure condition, unless the materials of concem are in direct contact with the housfing.

Finally, because of the different air flow arrangement, the naximus temperature to the top of the enclosure for CAH-F-8 is \(638^{\circ} \mathrm{F}\) (see Table 7). This temperature is due to the relatively small size of the enclosure unit as well as the location of the exposed side being the top of the enclosure. Being located on the top, the convective heat losses are substantially reduced from that of a side.

As noted in the tables, the analysis was terminated at 60 minutes. Extending the duration beyond 60 minutes is not necessary since the steel temperature is deciining 15 to 20 minutes into the incident with no action other than shutting dow the related fan within 5 minutes of the fire initiation.
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\section*{TABLE 3}

LOCAL HOUSING TEMPERATURE VS. TIME IN UNIT PAK-F-16

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TABLE 4
LOCAL HOUSING TEMPERATURE VS. TIME IN UNITS EAH-F-9 and EAK-F-69
\begin{tabular}{|c|c|c|c|}
\hline UNITS
\[
\begin{gathered}
\text { EAK-F-9, EAH-F-69 } \\
\text { TIME } \\
\text { (MIN) } \\
\hline
\end{gathered}
\] & \begin{tabular}{l}
\(\qquad\) \\
LOCAL HOUSING TEMP. (DEG F)
\end{tabular} &  & \begin{tabular}{l} 
MXIMUM \\
LOCAL \\
HOUSING TEMP. \\
(DEG F) \\
\hline
\end{tabular} \\
\hline - 1 & 121 & 31 & 544 \\
\hline 2 & 152 & 32 & 532 \\
\hline 3 & 186 & 33 & 520 \\
\hline 4 & 222 & 34 & 508 \\
\hline 5 & 261 & 35 & 497 \\
\hline 6 & 303 & 36 & 486 \\
\hline 7 & 349 & 37 & 475 \\
\hline 8 & 398 & 38 & 464 \\
\hline 9 & 449 & 39 & 454 \\
\hline 10 & 503 & 40 & 444 \\
\hline 11 & 559 & 41 & 434 \\
\hline 12 & 617 & 42 & 424 \\
\hline 13 & 657 & 43 & 415 \\
\hline 14 & 684 & 44 & 406 \\
\hline 15 & 698 & 45 & 398 \\
\hline \(-16\) & 704 & 46 & 390 \\
\hline \(-17\) & 704 & 47 & 382 \\
\hline 18 & 699 & 48 & 374 \\
\hline 19 & 691 & 49 & 367 \\
\hline 20 & 682 & 50 & 360 \\
\hline 21 & 670 & 51 & 353 \\
\hline 22 & 659 & 52 & 347 \\
\hline 23 & 646 & 53 & 341 \\
\hline 24 & 633 & 54 & 335 \\
\hline 25 & 620 & 55 & 329 \\
\hline 26 & 608 & 56 & 324 \\
\hline 27 & 595 & 57 & 319 \\
\hline 28 & 582 & 58 & 315 \\
\hline 29 & 569 & 59 ' & 310 \\
\hline 30 & 556 & 60 & 306 \\
\hline
\end{tabular}
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\hline
\end{tabular}

TABLE 5
LOCAL HOUSING TEMPERATURE YS TIME IN UNITS FAK-F-41 and FAH-F-74
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{c} 
UNIT \\
FAH-F-41, FAH-F-74 \\
TiME \\
(MIN) \\
\hline
\end{tabular} &  & \begin{tabular}{c}
\(\substack{\text { UNIT } \\
\text { FAH-F-4 } \\
\text { FNH-F-74 } \\
\text { TIME } \\
\text { (MIN) } \\
\hline}\)
\end{tabular} &  \\
\hline 1 & 96 & 31 & 369 \\
\hline 2 & 106 & 32 & 359 \\
\hline 3 & 318 & 33 & 350 \\
\hline 4 & 132 & 34 & 340 \\
\hline 5 & 148 & 35 & 331 \\
\hline 6 & 167 & 36 & 321 \\
\hline 7 & 188 & 37 & 312 \\
\hline 8 & 212 & 38 & 303 \\
\hline 9 & 239 & 39 & 294 \\
\hline 10 & 269 & 40 & 285 \\
\hline 11 & 302 & 41 & 276 \\
\hline 12 & 339 & 42 & 267 \\
\hline 13 & 369 & 43 & 259 \\
\hline 14 & 394 & 44 & 251 \\
\hline 15 & 412 & 45 & 243 \\
\hline 16 & 426 & 46 & 235 \\
\hline 17 & 436 & 47 & 227 \\
\hline 18 & 442 & 48 & 220 \\
\hline 19 & 445 & 49 & 213 \\
\hline 20 & 445 & 50 & 206 \\
\hline 21 & 443 & 51 & 199 \\
\hline 22 & 440 & 52 & 192 \\
\hline 23 & 435 & 53 & 186 \\
\hline -24 & 428 - & 54 & 180 \\
\hline 25 & 421 & 55 & 174 \\
\hline 26 & 414 & 56 & 169 \\
\hline 27 & 405 & 57 & 163 \\
\hline 28 & 397 & 58 & 158 \\
\hline 29 & 388 & 59 & 153 \\
\hline 30 & 378 & 60 & 148 \\
\hline
\end{tabular}
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TABLE 6
LOCAL HOUSING TEMPERATURE VS. TIME IK UNIT CAP-F-40
\begin{tabular}{|c|c|c|c|}
\hline \[
\begin{aligned}
& \text { UNIT } \\
& \text { CAP-F-40 } \\
& \text { TIME } \\
& \text { (MIN) } \\
& \hline
\end{aligned}
\] & MAXIMUM
LOCAL
HOUSING TEMP.
(DEG F) & \[
\begin{gathered}
\text { UNIT } \\
\text { CAP-F-40 } \\
\text { TIME } \\
\text { (MIN) } \\
\hline
\end{gathered}
\] &  \\
\hline \(\frac{1}{1}\) & 97 & 31 & 382 \\
\hline 2 & 109 & 32 & 372 \\
\hline 3 & 122 & 33 & 363 \\
\hline 4 & 137 & 34 & 353 \\
\hline 5 & 155 & 35 & 343 \\
\hline 6 & 175 & 36 & 334 \\
\hline 7 & 197 & 37 & 325 \\
\hline 8 & 222 & 38 & 316 \\
\hline 9 & 251 & 39 & 306 \\
\hline 10 & 282 & 40 & 298 \\
\hline 11 & 316 & 41 & 289 \\
\hline 12 & 354 & 42 & 280 \\
\hline 13 & 385 & 43 & 272 \\
\hline 14 & 410 & 44 & 264 \\
\hline 14 & & 45 & 256 \\
\hline 15 & 429 & 46 & 248 \\
\hline 16 & 443 & 46 & 241 \\
\hline 17 & 452 & 47 & 234 \\
\hline 18 & 458 & 48 & 234 \\
\hline \(-19\) & 461 - & 49 & 227 \\
\hline 20 & 460 & 50 & 220 \\
\hline 21 & 458 & 51 & 213 \\
\hline 22 & 454 & 52 & 207 \\
\hline 23 & 449 & 53 & 201 \\
\hline 24 & 443 & 54 & 195 \\
\hline 25 & 435 & 55 & 189 \\
\hline 26 & 427 & 56 & 184 \\
\hline 27 & 419 & 57 & 178 \\
\hline 28 & 410 & 58 & 173 \\
\hline 29 & 401 & 59 & 169 \\
\hline 30 & 391 & 60 & 164 \\
\hline
\end{tabular}
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TABLE 7
LOCAL ROUSING TEMPERATURE VS. TIME IN CAH-F-8 UNIT
\begin{tabular}{|c|c|c|c|c|}
\hline \[
\begin{gathered}
\text { UNIT } \\
\text { CAH-F-8 } \\
\text { TIME } \\
\text { (MIN) } \\
\hline
\end{gathered}
\] & \(\qquad\) & \[
\begin{gathered}
\text { UNIT } \\
\text { CAH-F-8 } \\
\text { TIME } \\
\text { (MIN) } \\
\hline
\end{gathered}
\] & & \begin{tabular}{l} 
MAXIMUM \\
LOCAL \\
HOUSING TEMP. \\
(DEG F) \\
\hline
\end{tabular} \\
\hline 1 & 106 & 31 & & 486 \\
\hline 2 & 124 & 32 & & 472 \\
\hline 3 & 144 & 33 & & 459 \\
\hline 4 & 168 & 34 & & 445 \\
\hline 5 & 197 & 35 & & 432 \\
\hline 6 & 229 & 36 & & 419 \\
\hline 7 & 266 & 37 & & 406 \\
\hline 8 & 307 & 38 & & 393 \\
\hline 9 & 354 & 39 & & 380 \\
\hline 10 & 405 & 40 & & 368 \\
\hline 11 & 460 & 41 & & 356 \\
\hline 12 & 519 & 42 & & 344 \\
\hline 13 & 565 & 43 & & 332 \\
\hline 14 & 597 & 44 & & 321 \\
\hline 15 & 619 & 45 & & 310 \\
\hline 16 & 632 & 46 & & 299 \\
\hline 17 & 637 & 47 & & 288 \\
\hline - 18 & 637 - & 48 & & 278 \\
\hline 19 & 633 & 49 & & 268 \\
\hline 20 & 626 & 50 & & 258 \\
\hline 21 & 617 & 51 & & 248 \\
\hline 22 & 606 & 52 & & 239 \\
\hline 23 & 594 & 53 & & 230 \\
\hline 24 & 582 & 54 & & 221 \\
\hline 25 & 569 & 55 & . & 213 \\
\hline 26 & 555 & 56 & & 204 \\
\hline 27 & 542 & 57 & & 196 \\
\hline 28 & 428 & \(58{ }^{\prime}\) & & 189 \\
\hline 29 & 514 & 59 & & 181 \\
\hline 30 & 500 & 60 & & 174 \\
\hline
\end{tabular}
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CONCLUSIONS
Based upion conservative, worst case calculations, the following conclusions are drawn from fire involving the charcoal cells in the air handing units:
1. The worst case maximum iocalized-steel plate tousing temperature was calculated to be \(704^{\circ} \mathrm{F}\). This temperature is substantially below that required for structural fallure of the steel mousing.
2. Structural failure of any steel beam or colum in the vicinity of these filiter units cannot be caused by heat transfer from the filter housing.
3. The maximum radiant heat emissive flux from the housing at \(704^{\circ} \mathrm{F}\), calculated to be less than \(10 \mathrm{~kW} / \mathrm{m}^{2}\), is less than half the critical radiant flux necessary to ignite the worst case cable jacket materials as determined by EPRI sponsored tests at Factory Mutual Research Corporation (EPRI NP-1200 part 1).

Therefore, the hazards posed by the heating of the steel housing from a charcoal bed filter cell fire will not jeopardize the safe shutdom of the plant.
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\section*{APPENDIX A}

\section*{ANALYSIS METHODOLOGY}

The unsteady heat conduction analysis used for this study is described in detail in this appendix. A lumped heat eapacity approach was utilized, valid as long as the heat conduction is sufficiently fast, as compared to the rate of heat transfer to the object (the appropriateness of the lumped heat capacity approach is reviewed later in this appendix).

Figure \(A-1\) depicts the heat transfer to the steel housing. The net heat transfer to the steel acts to increase the internal energy of the steel, resulting in a temperature rise. This can be described in equation [1] as:
\[
\rho c_{p} V \frac{d T_{5}}{d t}=Q_{N}-Q_{R L}-Q_{c}
\]
where:
\(Q_{e f}=\) Radiative heat transfer fram fire (W)
\(Q_{R_{L}}=\) Radiative heat loss from steel to surroundings (W)
\(Q_{c}\) - Convective heat loss fram steel to surroundings ( \(K\) )
\(T_{s}=\) Steel temperature ( \({ }^{\circ} \mathrm{C}\) )
\(t\) - Time (sec.)
e = Steel density ( \(7700 \mathrm{~kg} / \mathrm{m}^{3}\) )
\(C_{r}\). Steel speciffic heat ( \(520 \mathrm{~J} / \mathrm{kg}{ }^{\circ} \mathrm{C}\) )
\(v=\) Steel volume ( \(\mathrm{m}^{3}\) )

It should be noted that conductive losses through the steel to the remainder of the housing have been neglected. This assumption is conservative by ignoring heat which diffuses throughout the assembly.
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\end{tabular}

Figure A - 1
Heat Transfer Process

\(Q_{c}=\) convection heat loss
\(Q_{R L}\) - radiation heat loss
\(Q_{R F}=\) radiation from fire
\[
A-2
\]
\begin{tabular}{|l|c|l|}
\hline \begin{tabular}{l} 
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The three terms involving radiation or convection heat transfer will now be described.

Radiation Heat Transfer fro Fire

In general, radiation heat transfer between two finite, non-black bodies is given by:
\[
Q_{R F}=\frac{\sigma\left(T_{c}^{4}-T_{s}^{4}\right)}{\frac{1-e_{s}}{e_{c} \lambda_{C}}+\frac{1}{T_{c} T_{c s}}+\frac{1-e_{s}}{e_{s} A_{s}}}
\]
where:
\(\sigma\). Stefan-Boltzmann Constant ( \(5.67 \times 10^{-8} \mathrm{~W} / \mathrm{m}^{2} \mathrm{~K}\) )
\(T_{c}=\) Charcoal temperature ( \({ }^{\circ} \mathrm{K}\) )
\(T_{s}=\) Steel temperature ( \({ }^{\circ} \mathrm{K}\) )
\(e_{c}=\) Charcoal enissivity (assume .75)
\(A_{c}=\) Area of burning charcoal ( \(\mathrm{m}^{2}\) )
\(F_{C S}=\) View factor (assume 1.0)
\(e_{s}\) - Steel emissivity conservatively approximated as 0.8 (1)
\(A_{5}=\) Area of steel ( \(\mathrm{m}^{2}\) )

The surface area of steel directly exposed to the radiant heat from the charcoal filter bed cell fire varied for the five distinct Unit types. For each unit, the area can be calculated as the product of dimensions "A" and " 8 " from Table 1, except for Unit CAH-F-8 where the area is the product of dimensions " \(A\) " and " \(C\) ".

The view factor can be determined using graphs and view factor algebra. Because of the steel area being appreciably greater than the exposing charcoal bed area, the view factor was approximated as 1.0 . It should be noted that since the steel and charcoal are finite in size, the view factor is actually slightly less than \(\mathbf{1 . 0}\). Estimation of the view factor of 1.0 is conservative, f.e., this will lead to a greater steel temperature.
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The charcoal enissivity is assumed to be 0.75 , as suggested by Evans and Emmons (2). The burning charcoal surface area ( \(A_{C}\) ) was conservatively assumed to be \(0.465 \mathrm{~m}^{2}\) ( 26 inches square) which is larger than the maximum possible fire exposure ( 22 inches square) to the charcoal bed. The charcoal temperature is a function of time, as provided in the test report summarized in Table 2 of this report (3). The temperatures used in this analysis were measured within the charcoal bed on the outlet side. This set of temperatures was the highest of any of the temperatures measured, thereby yielding a conservative prediction of the steel temperature. This is also conservative since the temperature used is an interior temperature as opposed to surface temperature (which the radiation is dependent on) which would be cooler.

\section*{Radiative Heat Loss}

Since the temperature of the surroundings of the steel housing, other than the burning charcoal filter bed cell, is assumed to be unaffected by the fire, the surroundings will remain cool in comparison to the steel plate. As a result, radiation heat transfer will occur from the steel to the surroundings, resulting in net heat loss from the steel. Since the surroundings are infinite in size as compared to the housing, the radiative heat loss is given by:
\[
Q_{R L}=e_{S} A_{5} \sigma\left(T_{5}^{4}-T_{R}{ }^{4}\right)
\]
where:
\(\mathrm{T}_{\mathrm{R}}=\) Room temperature ( \({ }^{\circ} \mathrm{K}\) )
\(T_{s}, e_{s}\) and \(\sigma\) were defined previousiy for equation [2]. A room temperature of \(27^{\circ} \mathrm{C}\left(B 1^{\circ} \mathrm{F}\right)\) was arbitrarily selected for use in the calculations.

The radiative heat loss is assumed to occur on both sides of the steel housing.
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\section*{Convective Heat Loss}

\section*{\%}

As long as the surrounding air temperature is less than the steel temperature, free convection heat transfer will occur. Due to the forced air flow of \(40 \mathrm{ft} / \mathrm{min}\). through the charcoal filter bed and within the housing during the first five minutes after ignition, forced convection heat transfer also can be expected. The addition of forced convection will lead to an enhanced convective heat loss from the steel. For the purpose of this analysis. the forced convection was neglected, since the forced air stream can be expected to be heated, as documented in the test report. It should be noted that the heated air temperature is expected to be less than the steel temperature. Thus, neglecting the forced convection heat transfer is conservative.

The free convection heat transfer will occur due to the heating of the air adjacent to the steel plate, resulting in air movement due to a buoyancy change. Equation [4] describes the free convection heat loss.
\[
Q_{c}=h A_{s}(\Delta T) \quad[4]
\]
where:
\(h\) = Convection heat transfer coefficient ( \(\mathrm{H} / \mathrm{m}^{2}{ }^{\circ} \mathrm{K}\) )
\(\Delta T=\) Temperature difference between steel and ambient air ( \({ }^{\circ} \mathrm{K}\) ).

The convection coefficient can be approximated as \(4.5 \mathrm{~W} / \mathrm{m}^{2}{ }^{\circ} \mathrm{K}(1)\). This value can be checked use enpirically derived values for the coefficient, where the convecting fluid is air (1).
\[
h=\left\{\begin{array}{l}
0.95(\Delta T)^{1 / 3} \text { for vertical plate } \\
1.43(\Delta T)^{1 / 3} \text { for horizontal plate }
\end{array}\right.
\]

The condition of horizontal plate is present for unit CAH-f-8. The value of the convection coefficient will be reviewed after the steel temperature is estimated, so that the, temperature difference can be evaluated.
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In the case of the units where the exposed housing surface is vertical (PAK-F-16, EAK-F-9, EAK-F-69, FAK-F-41, FAH-F-74 and CAP-F-40), the free convection heat transfer is assumed to occur on both sides of the housing. Unit CAK-F-8, with the exposed horizontal surface, the free convection is assumed to occur only from the top surface. Free convection will also exist from the lower surface, but at a much reduced rate due to the convecting air moving in opposition to smoke produced by the burning charcoal. In all cases, the ambient air temperature is arbitrarily assumed to be \(27^{\circ} \mathrm{C}\left(81^{\circ} \mathrm{F}\right)\).

\section*{Solution for Steel Temperature}

The steel temperature can be determined by substituting equations [2]. [3] and [4] into equation [1]. The derivative, \(\frac{d T s}{d t}\), can be replaced by \(\frac{\Delta T_{s}}{\Delta t}\). An fierative solution techaque can be applied to determine \(T_{s}\) after a time duration of interest. For this study, a total time of 60 minutes was considered. In general, the equation for \(T_{s}\) is given as:
\(\Delta T_{s}=\frac{\Delta t}{\rho_{C} V}\left[\frac{\sigma\left(T_{c}{ }^{4}-T_{s}^{4}\right)}{\frac{1-e_{c}}{e_{c} A_{c}}+\frac{1}{A_{c}}+\frac{1-e_{s}}{e_{s} A_{s}}}+e_{s} A_{s} \sigma\left(T_{s}^{4}-T_{R}^{4}\right)-4.5 A_{s}\left(T_{s}-T_{R}\right)\right][6]\)

Since estimates for the steel temperature are now available, the validity of two key assumptions can be checked. One assumption considered the rate of conduction heat transfer within the steel to be much greater than the radiation and convection heat transfer on the steel boundary. The second assumption stated that the convection heat transfer coefficient was 4.5 \(\mathrm{W} / \mathrm{m}^{2} \mathrm{*} \mathrm{K}\). The second assumption will be addressed first, since the examination of the first assumption requires the convection coefficient to be known.

The convection heat transfer coefficient can be determined from equation [5]. Considering the temperature difference to be \(200^{\circ} \mathrm{C}\) (an approximate
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average temperature difference during the 60 -minute exposure), the convection coefficient is actually \(5.5 \mathrm{M} / \mathrm{m}^{2}\) * K for the vertical plate and 8.43 \(W / m^{2}{ }^{*} K\) for the torizontal plate. Thus, use of the value of \(4.5 \mathrm{~W} / \mathrm{m}^{2}{ }^{\circ} \mathrm{K}\) for the convection coefficient underestimated the convective heat loss. yielding greater steel temperatures. Since the assumption of \(4.5 \mathrm{~W} / \mathrm{m}^{2}{ }^{\circ} \mathrm{X}\) is \(s\) hom to be conservative, without grossly underestimating the convective heat loss, the assumption is considered valit.

The validity of the first and more important assumption can now be assessed. The comparison of rates of conduction to convection and radiation teat transfer can be performed by evaluating the parameter, H/k as noted in equation [7]:
\[
\begin{equation*}
\frac{\mathrm{KL}}{\mathrm{~K}}<0.1 \tag{7}
\end{equation*}
\]
where:
H = Combined radiation and convection heat transfer coefficient ( \(\mathrm{W} / \mathrm{n}^{2}{ }^{\circ} \mathrm{K}\) )
\(L \quad\) - Characteristic dimension of steel (m)
\(k\) - Steel themal conductivity ( \(W / m{ }^{*} \mathrm{~K}\) )
The combined radiation and convection heat transfer coefficient is given as:
\(H^{-}=h_{c}+h_{2 L}+h_{2 r}\)
where:
\(h_{c}=4.5 \mathrm{~N} / \mathrm{m}^{2}{ }^{\circ} \mathrm{K}\)
\(n_{R L}=\frac{D_{26}}{T_{5}-T_{2}}\)
\(n_{E F}=\frac{Q_{N F}}{T_{C}-T_{S}}\)
\(h_{R_{1}}\) can be re-expressed as:
\(h_{R L}=\frac{Q_{R L}}{T_{S}-T_{R}}=\frac{e_{S} A_{S}-\left(T_{S}{ }^{4}-T_{R}{ }^{4}\right)}{T_{S}-T_{R}}\)
Sinilarly, \(h_{s}\) is:
\(n_{* F}=\frac{\sigma\left(T_{C}^{4}-T_{s}{ }^{4}\right)}{\left(\frac{1-e_{C}}{E_{C} A_{C}}+\frac{1}{A_{C}}+\frac{1-C_{s}}{E_{s} A_{s}}\right)\left(T_{C}-T_{s}\right)}\)
\[
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\]
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Assuming an average steel temperature of \(500{ }^{\circ} \mathrm{K}\), average charcoal temperature of \(1000{ }^{\circ} \mathrm{K}\), and roan temperature of \(300^{\circ} \mathrm{K} h_{\text {RL }}\) and \(h_{\text {gf }}\) can be evaluated, using the values for all other parameters which were previously presented.
\[
\begin{aligned}
& h_{R L}=56.8 \mathrm{~m} / \mathrm{m}^{2} \mathrm{~K} \\
& h_{R F}=36.4 \mathrm{~W} / \mathrm{m}^{2} \mathrm{~K}
\end{aligned}
\]

Thus, the sum of the heat transfer coefficients is \(97.7 \mathrm{~m} / \mathrm{m}^{2}{ }^{\circ} \mathrm{K}\).

The characteristic dimension of the steel (L) is the ratio of the volume to the surface area. In this case the characteristic dimension is the plate thickness, f.e., 0.001 m ( \(1 / 4\) inch).

Assuming the steel conductivity is estimated as \(25 \mathrm{~W} / \mathrm{mK}\),
\[
\frac{H L}{K}=\frac{97.7 \times .001}{25}=0.004<0.1
\]

Thus, the assumption of the rate of heat conduction being substantially greater than that of the convection and radiation heat transfer is appropriate.

The convective and radiative losses can also be compared to assess the sensitivity of the analysis to the selected room temperature. For illustration purposes if the assumed room temperature is increased from \(81{ }^{\circ} \mathrm{F}\) to \(120^{\circ} \mathrm{F}\) ( \(27{ }^{\circ} \mathrm{C}\) to \(49{ }^{\circ} \mathrm{C}\) ), the maximum localized housing temperature increases by only approximately \(20^{\circ} \mathrm{F}\).
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\section*{Selected References}
1. Holman, J.P., Heat Transfer, 6th Edition, New York, McGraw Hill, 1986.
2. Evans, D.D. and Emmons, "Combustion of Mood Charcoal," Fire Research. 1, (1977). p. 57-66. (see Appendix B)
3. Nuclear Consulting Services, Inc.. "Iodine Adsorber Fire Test," September 15, 1986 (unpublished).

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Combustion of Wood Charcoal
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(Recetved Juse 21, 2876)

\section*{SUMOARY}

The dynamics of burning of wood charcoal in an air stream is examined both experimentally and theoretically. To simplify the theory, an experimental arrangement approximating a one dimensional phenomenon was adopted. The theory includes conduction in the solid, chemical reactions and heat relesse at the surface, and heat and mass transfer in the gas boundary layer above the surface. The molar \(\mathrm{CO} / \mathrm{CO}_{2}\) ratio is measured. The theory predicts surface temperature, solid temperature distribution and burning rate within experimental error. An effective reaction rate formula is developed.

\section*{DNTRODUCTION}

This study is a step toward understanding the details of the extinguishment of wood fires by water. To avoid the complications in chemistry during the pyrolysis that wood undergoes as it burns, the initial study reported here is for the burning of wood charcoal. The burning of wood charcoal offers a simplified chemistry while maintaining a physical struc. ture closely related to the original wood, and is an important process in a wood fire as well.

The wood charcoal used in this experiment was commercially available and produced from basswood (Tilia americana). When wood charcoal is burned, the burning surface becornes complicated by a system of eracks generated in the combustion process, and by a fiberous array of residual ash (see Fig. 1). Considering these complications, it is not surprising that little quantitative work on the

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combustion of wood charcoal has been done in the past. Most basic studies of carbon combustion utilize graphite which is easily obtained more chemically pure and physically uniform. Notable arnong the studies of graphite combustion is the extensive work performed by Nagle and Strickland-Constable [1] in which an expression for the chemical rate of reaction of pyro graphite with oxygen was developed. One might consider initially burning graphite to avoid the ash and cracking problems. However the low porosity (relative to charcoal) and the consequent large changes of properties makes such tests of little value for the present problem. In fact, sraphite will not burn in the present apparatur.

The primary goal of this investigation is to predict the burning charncteristics of wood charcoal from basic physical principles. Hopefully this same model will prove adequate to describe more complex cases and in particular will be heipful in the study of extinguishment. Thus it is advantageous to set up an experiment that is easlly modeled. One finds that If an isolated piece of wood charcoal is ignited, it will not continue to burn unless one blows an oxidizer, Le. air, on to it. A particularly useful way to blow air on it and at the same time to produce a nearly one dimensionas phenomenon, is to locate the burning surface in a stagnation point flow fieid. In the laminar case, the stagnation point flow field develops a uniform boundary layer thickness over the impingerment plane and thus uniform transport phenomenon can be expected. Unfortunately, in order to maintain combustion, air must be blown at the charcoal burping surface at high mainstream velocities; velocities that are high enough to make the Now turbulent. The degree to which the boundary layer thickness for a turbulent stagnation point flow field remains uniform, is in the
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Fie. 1. Burning surfect of a charcoal cyiadar thowing encha and mome wh cover. The girtular crow-wellion of the aurface appears alliptical because the eamert was held at an angle to the axie of the rylinder to heep it out of the air thow field.
case of the laminar @ow was not investigated, but the experimental results were found to be well approximated by a one dimensional theory.

The model of the buming process used here assumes that an overall reaction between earbon and oxysen takes place on the projected surface area (i.e. not counting the additional ares within cracks or pores; the cracks cover about \(0.5 \%\) of the projected area while the pores are very small complex and constitute about \(80 \%\) of the volume) to produce carbon dioxide and carbon monoxide. The energy and mass balances at the surface require a knowledge of the convective heat and mass transfer rates, the radiative heat exchange, and the conduction into the solid.

Heat transfer coefficients were measured by the cooling of a copper slug in the place of the charcoal sample. The results are presented In dimensionless form.

Mass transfer coefficients were measured by the evaporation of waler from a wet porous slug in the place of the charcoal sample. The results are presented in dimensionless form
and are compared with the heat trassfer results.

The radiation is eomputed by assuming a surfacetmmissivily for charcoal of 0.75 . This value Tals within the range of Literature values for "rough carbon" as for example ref. 2.

The heat conduction into the churcoal is the heat required to heat the charcoal from the ambleat iemperature to the surface temperature.

Finally the ratio of carbon monoxide to carbon dioxide produced during charcoal combustion was measured by a mass spectrometer analysis of grab samples. The result are compared with lilerature values.

BURNINC RATE AND SURFACE TEMPERATURE: EXPERIMENTAL APPARATUS AND RESULTS

The wood charcoal obtained from basp wood used in this experiment is that commercially sold by William Dixon Co. of Carlsiadt, New Jersey, in solid blocks with
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Fig. 2 Schematic diagram of apparatus.
pproximate dimensions \(17 \times 10 \times 3.5 \mathrm{~cm}\). Bulk densities ranged from 0.26 to 0.34 \(\mathrm{s} / \mathrm{cm}^{2}\) and ash content from 0.5 to \(1.5 \%\) by weight. No correlation of ash concentration with the charcoal density was observed. The densities of the test charcoal fall in the same range as the densities which result from a fire, although the latter are usually riddled with cracks-large and small-while the experimental samples were free of cracks before the test and during the test only small surface cracks appeared.

To make the measurements of burning rate, surface temperature, and internal temperature distribution of a wood charcoal cylinder burn. ing in a stagnation point flow, the apparatus schematically represented in Fig. 2 was assem bled. A charcoal cylinder approximately 2.7 \(\mathbf{c m}\) in diameter and initially 11.4 cm in height is shown burning surrounded by insulating material. This insulation is essential if the phenomenon is to be one dimensional. The charcoal cylinder is cut from a larger block of charcoal such that the grain direction is perpendicular to the exis of the cylinder. As the burning surface regresses towards the bottom of the cylinder, the motor driven platform assembly with manually operated speed control pushes the core up at the same rate as the surface is regressing. The burning surface is thus maintained at the same level as the top surface of the insulation on which the air flow


Fig. 3. Charcoal burning rale us mainatream air velocity: \(x\), experimenial data; -, predicied burning rocity; for varioum hinetic parameter values.
impinges setting up the stagnation point fow field. Mainstream air velocities measured at the exit of the nozzle up to \(45 \mathrm{~m} / \mathrm{sec}\) were available. The insulation plate was held a fixed distance of two nozzle dimmeters from the exit of the nozzle by a larger aluminum plate with a circular opening centered on the axis of the flow.

The internal temperature distribution in the burning charcoal sample was measured by thermocouples implanted near the bottom end of the cylinder. As the burning surface regressed, the thermocouples would come closer to the burning surface eventually passing through it. From measurements of the surface positions, internal lemperature information from the thermocouples could be related to their distance from the burning surface. To measure the surface position with respect to the platform, the pin on the end of a scale was lowered periodically to the surface. Contact of the pin was determined visually by observing the pin through the magnifying optics system of the pyrometer. When the pin was not in use, it was swung out of the flow field since its wake in the flow when located more than a few pin diameters above the burning surface was an unacceptably large disturbance. Aside from being used es a telescope, a disappearing filament type pyrometer was one of the pyrometers used to measure the temperature of the burning sur-
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Fig. 4. Surfece lemperature in, mainatreama air veloehy: 0 , filament pyrometer; \(O\), infrared pyrometer; \(\bullet\), thermocouple: - predie
kinetic parsmeter valuen.
face independent of the readings obtalned from the thermocouples.

Figure 3 shows the experimental results for the steady state buming nate of the charcoal as a function of the mainstream air velocity. The burning rate of the charcoal is calculated as the product of the rate of regression of the burning surface and bulk density of the charcoal cylinder measured in room air. The carbon content of the charcoal was determined to be approximately \(93 \pi\) by weight. The remainder included residual hydrogen and oxygen in the charcoal structure, moisture, adsorbed gases, and ash. Thus the charconal burning rate measured differs slightly from a carbon burning rate.

The lowest recorded mainstream air velocity at which the charcoal would self-sustain its own combustion was \(7.7 \mathrm{~m} / \mathrm{sec}\). Repeated tries to bum cylinders at a mainstrean velocity of \(4.6 \mathrm{~m} / \mathrm{sec}\) failed. After ignition on each of these trials, extinguishment began at the circumference of the burning surface near the insulation and progressed inward towards the center. This sequence of events reveals the iofluence of some heat loss to the incilation ring. For the purpose of analysis of these dats,
a self extinction velocity of \(5.5 \mathrm{~m} / \mathrm{sec}\) will a ceifex

The corresponding measurements of the burning surface temperature measured with the thermocouples and two pyrometers as a function of the mainstream air valocity are thown in Fig. 4. Pyrometer measurements are based on a surface emissivity of 0.75 , which is representative of carbon surfaces at temperatures around \(900^{\circ} \mathrm{C}\). The maximum temperature measured by an implanted thermocouple was genenally below the measurements made by the pyrometers. This is not unex. pected as near the surface it was common for pected as near the surface it was common for
the leads of the 0.025 cm diameter chromelthe leads of the 0.025 cm diameter chrome
alumel wire threaded radially through the cylinder to be exposed by Eurface irregular. jties to the cooling effects of the air flow.

The disappearing filament type optical pyrometer manufactured by Pyrometer Instrument Company was used to measure the temperature of specific small aress of the burning surface where ash cover was a minimum. The area chosen to be measured and balancing of the instrument was left to the judgement of the operator.

The in!rared pyrometer was a Barnes Ingineering Co., Infrascope Mark 1. This instrument was set up to give a continual reading of the average temperature in a \(1 / \mathrm{cm}^{2}\) irea in the center of the buming surface. Its record provided an indication of an effective surface semperature including the influence of the ash layer. Because of fuxuations caused by pieces of ash cover being swept away in the air flow and chanping surface crack patterns, some judgement was exercised in assigning one value of temperature characterixing the output. Generally the uncertainity associated with these measurements is \(115^{\circ} \mathrm{C}\).

Close examination of the pyrometer data reveals that the measurements made with the infrared pyrometer, influenced by the ash layer, are approximately \(25{ }^{\circ} \mathrm{C}\) lower than those made with the filament pyrometer, measuring temperatures in areas of minimum ash concentration, for low air velocities. With increasing air velocity, the two sets of data blend together. This trend indicater the decreasing influence of the ash layer at higher alr velocities, as it is swept from the surfsee more easily than at lower velocities. At the highest air velocity, \(43 \mathrm{~m} / \mathrm{sec}\), the measurements with the infrared pyrometer are re-

\section*{SEABROOK Evaluation and Comparison to BTP APCSB 9.5-1, STATION Appendix A}
corded as higher than thove with the fllament pyrometer. This could indicate that the chogen emissivity for the burning surface is too low. Assuming that the infuence of the ash in nedligible at this high sir velocity, the value of the surface emissivity that brings both pyrometer mesurements into agreement at \(48 \mathrm{~m} / \mathrm{sec}\) and \(1055^{\circ} \mathrm{C}\) is 0.85 . It if also likely that the differences in temperature recorded are simply the result of uncertainties in the measurements as they approach the limits of securacy for the measurements.

GURNING RATE AND SURFACE TEMPERATURE: THEORETICAL MODEL

As mentioned in the introduction, \(s\) one dimensional model is adequate for these experimental results. It is desirable to know the detailed chemical kinetic mechanism involving reactions at the carbon surface, in cracks and pores, and in the gas phase. Unfortunately suf. Diciently detailed chemical data was not found. The graphite reaction kinetic formula of Nagle and Strickland-Constable [1] was tried but as expected was wholly inadequate (low by a factor of about 50). A messurement of the local density near the charcoal surface suggests some burning in the pores and cracks (up to 10\%). With charcoal there is no significant burning out in the boundary layer or else the fire could be "blown out" as is the case with burning polymethylmethacrylate. The absence of such major boundary layer burning does not preclude minor reactions in the boundary layer nor major reactions in the gas phase very close to the charcoal surface.

In the absence of applicable chemical data, we will assume an overall reaction and reaction kinetics formula applicable to the charcoal projected surface area. Thus we assume an effective surface resction:
\(\mathrm{C}+\mathrm{xO}_{2} \rightarrow \mathrm{aCO}+\mathrm{bCO}_{2}\)
where
\(a+b=1\)
\(x=\frac{k}{2}+b\)
As discussed later the CO to \(\mathrm{CO}_{2}\) molar ratio is given by
\(\mathrm{a} / \mathrm{b}=4.3 \exp (-3390 / T)\)
and the reaction rate is assumed in the form of a first order Arrhenius resction.
\(\rightarrow m_{c}^{\prime \prime}=A p_{\rho_{2}, ~}=\exp (-E / R T)=X P_{O_{2}}=\)
Prediction of the burning rate and surface temperature of the charcoal in ateady state combustion is done by solving simultaneously two independent equations relating the buming rate and surface tempenture. The first equation involves an eneray balance at the buming surface equating the energy generated in the above chemical reaction to that lost through heat trasfer. The burning nite of the charcoal based on the surface energy belance is given by:
- \(\dot{m}_{c}^{\prime \prime}=\left[h_{i}\left(T_{\sigma}-T_{s}\right)+e o\left(T_{s}^{4}-T_{s}^{6}\right)\right] /\)
\(\left[-\Delta H_{\mathrm{Co}}^{*}-b \Delta H_{\mathrm{CO}_{2}}\right.\) +
\(+\left\langle c_{c}+x \frac{M_{O_{2}}}{M_{c}} c_{O_{2}}-d \frac{M_{c o}}{M_{c}} c_{c o}\right.\)
\(\left.-b \frac{M_{\mathrm{cO}_{2}}}{M_{\mathrm{c}}} \mathrm{c}_{\mathrm{cO}}\right) \times\)
\(\left.\times\left(T_{*}-T^{*}\right)-c_{c}\left(T_{*}-T_{*}\right)\right]\)
In eqn. (6), the value of \(h\) is given as shown later by:
\(\mathrm{Nu}=h \mathrm{~d} / \mathrm{k}=3.3\) (ReP.J \({ }^{0.3 \mathrm{~s}}\)
The recond equation relating the buming rate and surface temperature is eqn. (5) which however requires the oxygen partial pressure at the burning surfice. The oxygen partial pressure at the surface \(\mathrm{P}_{\mathrm{O}_{2}}\). v is determined from the conservation of species equations at the burning surface. For oxygen this takes the form:
\(h_{m}\left(Y_{O_{2,4}}-Y_{O_{2}, ~}\right)+\dot{m}_{c}^{\prime \prime} Y_{0_{2},}=-\dot{m}_{c}^{\prime \prime} \frac{M_{O_{2}}}{M_{c}} x\)

Similay balancés for all the other species are needed to determine the composition of the mixture of gases at the buming surface in order to find the oxygen partisi pressure. For this calculation the transport rate per unit concentration difference of each speeies is considered equal to that for oxygen. As deucribed laler, the mass transfer coefficient is given by
\(\mathrm{Sh}=h_{\mathrm{m}} \mathrm{d} / \mathrm{P}_{\mathrm{ca}} \mathrm{D}=2.7(\mathrm{ReSc})^{0.4}\) (9)
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The oxygen partial pressure at the surface is thus found to be

Substitution of this expression into eqn. (b) yields the second equation relating the buming rate and the aurface temperature after come manipulation as:
\[
\begin{align*}
\dot{m_{c}} \ddot{c}= & \frac{M_{c}}{M_{O_{2}}(x-2)}\left[\left(X x \frac{M_{O_{2}}}{M_{c}} p+h_{m} Y_{O_{2}, 4}+\frac{M_{O_{2}}}{M_{N_{2}}} h_{2} Y_{M_{2}, 4}\right)\right. \\
& \left.-\left\{\left(X x \frac{M_{O_{3}}}{M_{c}} p+h_{m} Y_{O_{3}, 4}+\frac{M_{O_{2}}}{M_{N_{2}}} h_{m} Y_{N_{2}, 4}\right)^{2}-4 h_{m} Y_{O_{2}, 4} X \frac{M_{O_{2}}}{M_{c}}(x-1) p\right\}^{3 / 2}\right] \tag{11}
\end{align*}
\]

Solutions for the steady burning rate and surface vemperature catisfying eqns. (6) and (11) were found as a function of the mainstream air velocity and values for all the parameters in the reaction rate expreasion eqn. (5). In all the predictions, a pressure of 1 atm and an ambient temperature of \(20.4^{\circ} \mathrm{C}\) representing the average value during all the tests gielding the data recorded in Figs. 3 and 4 was used.
The most powerful piece of information obtained from the data in terms of predicting values of the rate parametern \(A\) and \(E / R\) was the delermination of the self-extinction velocity. From experiments, the minimum air velocity at which the charcoal will sustain its own combustion can only be axid to be between 4.4 and \(7.7 \mathrm{~m} / \mathrm{sec}\). For determining appropriate values of the parameters \(A\) and \(\Sigma / R\), assumed to be constant, the value of the air velocity set as the self-extinction velocity was \(5.5 \mathrm{ni} / \mathrm{sec}\). Choosing a value for \(E / R\), a corresponding value for \(A\) can be found such that no solution to eqns. (6) and (11) representing steady burning exists at sir velocilies below \(5.5 \mathrm{~m} / \mathrm{sec}\). Following this procedure, the lines on Figs. 3 and 4 show the colculated results for burning rale and surface temperature for three values of \(E / R-8000,9000\) and 10,000 -assuming an emissivity for the buming surface of 0.75 . The corresponding value of \(A\) is given in each case. Comparing the calculation to the experimentad data, one can see that in all cases the general agreement is good. The combination of \(E / R=9000\left({ }^{\circ} \mathrm{K}\right)\)
and \(A=25.42\left(\mathrm{~g} / \mathrm{cm}^{2} \sec \mathrm{~atm}\right)\) results in the best agreement considering both sets of experimental date.
Because the extinction velocity is important in the determination of the constants \(A\) and \(E / R\), some analysis was performed to determine the effect of the uncertainty in this value on the results. Varying the extinction velocity above and below \(5.5 \mathrm{~m} / \mathrm{sec}\) by 1.5 \(\mathrm{m} / \mathrm{sec}\) for a value of \(E / R\) equal to 9000 , changed the value of \(A\) to 24.19 and 27.31 respectively. In terms of an overall first order reaction oceurring on the surface, the form of the expression for the effective chemical kinetic rate of reaction applicable to wood charcon oxidized in air.is:
\(-\dot{m}_{c}=(25.4) p_{0_{3}} . e^{-(0000 / T)}\left(\mathrm{g} \mathrm{cm}^{-2} \mathrm{~s}^{-3}\right)(12)\)
The value of \(E / R\) of 9000 found applicable to wood churcoal compares favorably with a value of 8160 found useful for Austrian brown coal char in a work by Hamor, Smith and Tyler [3]. Both of these vilues do not agree well with the 15,100 value of \(E / R\) found applicable to the oxidization of pyro graphite in the work of Nagle and Strickland-Constable [1]. A possible explanation for the difference between the results for graphile and thove for coal char and charcoal could be the infuence of a substantial amount of burning occurring in pores opening onto the surface. Under certain conditions, combustion in pores as opposed to that on an exposed surface can lower the observed activation energy by a factor of two from the actual value associated

\section*{SEABROOK Evaluation and Comparison to BTP APCSB 9.5-1, Station Appendix A}

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with the reaction occurring at the buming surface. A detailed discussion of this effect is given by Wheeler [4].

THE TBAPERATURE DISTRIBUTION WITHIN THE UNBURNED SOLID
To model the temperature distribution in the charcoal below the burning murface, a steady state solution to the one-dimensional heat conduction equation in a semi-infinite solid was sought. The burning murface was asumed to have constant temperature \(T_{\sigma}\) and to travel at a constant velocity \(V\), (with respect to a coordinate sysiem fixed to the base of the charconl cylinder) into the unburned solid, initially at uniform temperature \(T_{0}\).

No steady state solution exists in a frame of reference in which the surface moves; but with respect to a system in which the buming surface remains fixed in spice, the steady state solution is:
\[
\begin{equation*}
\left(T-T_{0}\right)=\left(T_{v}-T_{0}\right) \exp (-V X / a) \tag{13}
\end{equation*}
\]

To obtain eqn. (13) all the properties of the charcoal forming the thermal diffusivity \(a\), \((\alpha=k / p c)\), were assumed constant, and heat flux only in the axial direction was allowed.

The exponential form of the anticipated temperature profile suggests that a useful way to plot the experimental results would be in the form of \(\ln \left(T-T_{0}\right)\) vo. \(X\). From eqn. (13) It would be expected that a straight-line with slope -V/a would result.

Figure 5 shows the experimental results for a charcoal cylinder with density \(0.329 \mathrm{~g} / \mathrm{cm}^{3}\) and initial temperature of \(19.7^{\circ} \mathrm{C}\) bumed in mainstream air velocity of \(21 \mathrm{~m} / \mathrm{sec}\). The temperature outputs from two thermocouples jocated on the axis of the cylinder and initially 99.2 mm and 104.3 mm from the end of the cylinder to be burned, ( 1 and 2 respectively in Fig. 2), are shown as functions of the distance from the burning surface. The plot yields a rough straight-line with mark deviations at large distances from the burning surface and in the range of temperature difference equal to \(100^{\circ} \mathrm{C}\). At large distances from the burning surface, the deviation is caused by termination of the insulation around the cylinder at 56 cm . The deviation in the region of a tempernture difference of \(100^{\circ} \mathrm{C}\) is believed due to


Fig. 5. Experimental data for the ateady stave iaternal temperature distribution in a eharcoal eyliader with density \(0.329 \mathrm{~g} / \mathrm{cm}^{2}\), and initial temperntare \(\left\{T_{0}\right.\) ) of \(19.7^{\circ} \mathrm{C}\) burned in a mainatreann air velocity of 21 mo/vec. Dala shown from the thermoeouplas ( + ) and (0) initially 99.2 mm and 104.3 mm from the burning surface respectively. Line: straighs line fit of dath sear buming surface.
desorption of adsorbed geses from the charcol structure.

From a knowledge of the surface velocity, \(V\) (for this test \(0.138 \mathrm{~cm} / \mathrm{min}\) ) and the slope of the data near the burning surface, a value of the thermal diffusivity of wood charconl appropriate to that temperature range can be found as indicated by the results of the simple conduction model. The straight-line fit of the data shown in Fig. 5, yjelds a value for the thermal diffusivity, \(\alpha\), of \(0.0026 \mathrm{~cm}^{2} / \mathrm{s}\). Use of the slope of the data at lower temperatures to predict the thermal diffusivity using the result of the simple conduction model, eqn. (13) would be inappropriate because of the influence of the desorption region, the termination of the insulation, and consequent radial hest loss.

A modest attempt was made to calculate the thermal diffusivity from measurements of the basic properties of thermal conductivity, density and specific heat. The thermal conductivity of wood charcoal was measured and is given by
\(h=0.0016 \rho-0.00017\left(\mathrm{cal} \mathrm{cm}^{-1} \mathrm{~s}^{-1} \mathrm{C}^{-1}\right)\)
(14)
applicable at room temperature, and the specific heat was measured as room temperature and was found to be 0.24 ( \(\mathrm{cel} \mathrm{g}^{-1}{ }^{\circ} \mathrm{C}^{-1}\) ).

The resultant thermal diffusivity was \(0.0045 \mathrm{~cm}^{2} / \mathrm{sec}\) to be compared with 0.0026 \(\mathrm{cm}^{2} / \mathrm{sec}\) found from the burning experiment.
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4
The exact reason for the discrepancy was not sought but is probably associated with the fact that the burning test value is in a higher temperature range where the adsorbed gases hrve been expelled from the charcoal.

HEAT AND MASS TRANSEER COEFTICIENTS
To measure the convective heat transfer mite as a function of the mainstream air velocIty, a copper cylinder the same diameter as the chatcoal cylinders being used was ret into the insulation so that it occupied the came position the charcoal would normally. The rate of energy lost as it cooled from 350 to \(250^{\circ} \mathrm{C}\) was determined. This measurement was corrected for heat lost to the insulation to find the convective heat loss rate from the exposed surface. The mass transfer characteristics of the now field were determined from measurements of the rate of evaporation of water from a sintered disk of the same diameter and located in the same position in the air flow as a charcoal cylinder.

The non-dimensionalized results of the experiment are shown in Figure 6. The results for the heat and mass transfer rates are fit by eqns. (7) and (9) respectively. All of the . properties used in the non-dimensionalization are evaluated at the film temperature, the average between the surface and ambient temperatures. The binary diffusion coefficient for water into air, \(D_{\mathrm{H}_{2} \mathrm{O} \rightarrow \text { w, }}\) was calculated from an expression developed from kinetic theory by Chapman and Enskog [5]. Good agreement among the two sets of measurements in terms of the analogy between convective heat transfer and mass transfer rates is revealed.

Also shown in Fig. 6 are the results for heat transfer in a turbulent stagnation point flow taken from Garden and Cobonpue [6] and Jakob [7]. In selecting results from these cources an effort was made to preserve the ratios of the distance of the stagnation plane from the nozzle exit to the nozzle diameter ( \(1 / d\) ) and diameler of the nozzle to the diameter of the circular heat transfer surface ( \(d / s\) ).

CARBON MONOXIDE FORMATION DURDN
BURNING
To determine the energy released in the combustion of the charcoal, it is necessary to


Fig. 6. Hest tranafer and mens tranafer dals. + Present beat transfer memnurement, \(L / d=2, d / 8=1.94\). I Pres ont mans transfer mesemurement \(V / d \cdot 2, d / a=1.94\). - Dita from Cardon and Coboapue (5) 81 , 0.72 ) \(V d=2, d / s=2.51,-\cdots-N u=3.5(\) ReP \()\) ) ni of \(\mathrm{D}:-\mathrm{N}\) of : \(\mathrm{Nu}=0.533\left(\mathrm{ReF}_{z}\right)^{0.5 \%}\); from dakob fs) \((\operatorname{Pr}=72) ; / / d=1.43, d / s=1.75\).
determine the ratio of carbon monoxide to carbon dioxide formed in the reaction. Samples of gas extracted from a region fust above the level of the surface and at the circumfer. ence of the burning surface, were analyzed for the \(\mathrm{CO} / \mathrm{CO}_{2}\) ratio with a mass spectrometer. Figure 7 shows the results plotted as a function of the surface temperature. OriginalIy the data were collected as a function of the mainstream air velocity of the flow indicated at the iop of Fig. 7. Characteristic surface temperatures as a function of the air velocity shown in Fig. 4 from the infrared pyrometer were used to convert the data from an air velocity dependence to aurface temperature dependence.

Also indicated in Fig. 7 is the result of Arthur [8] for the \(\mathrm{CO} / \mathrm{CO}_{2}\) ratio produced in the combustion of graphite and cosi char granules in a quartz reacting vessel. The relation \(X_{\mathrm{co}} \mid X_{\mathrm{CO}_{7}}=10^{2.4} \exp (-12,400 / T)\) he determined from analysis of the products of the carbon reaction with a flow of oxygen nitrogen, and a small amount of phosphoryl chloride ( \(\mathrm{POCl}_{3}\) ) vapor. The \(\mathrm{POCl}_{3}\) was added to inhibit the gas phase reaction of carbon monoxide to carbon dioxide. In a previous study [9], the effect of this inhibitor on the ratio of carbon monoxide to carbon dioxide formed during the oxidation of graphite was examined. It was found that a concentration of \(\mathrm{POCl}_{3}\) of less than \(1 \%\) in the air flow raised the \(\mathrm{CO} / \mathrm{CO}_{2}\) ratio in the products of combur tion to 8.4 from a value of 0.05 (shown in
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Fig. 7. Molar ratio of \(\mathrm{CO} / \mathrm{CO}_{2}\) whe inverse aurface semperature.

Fig. 7 with no inhibitor present). Also shown in Fig. 7 is one value for the \(\mathrm{CO} / \mathrm{CO}_{2}\) ratio measured in the combustion of charcoal by Parker and Hottel [10]. Comparing the results of the measurements reported here to those of Arthur would suggest that some gas phase reaction is involved in our combustion of wood charcoal. Because of the high sir velocities used in this experiment, if a gas phase reaction does exist it must be confined to a region very close to the burning surface.

\section*{CONCLUSIONS}

The simple surface combustion model presented in this work can be used to predict the burning rate and surface ternperature of wood charcoal bumed in a stagnation point flow of air.

An expression for the effective chemical rate of reaction of wood charcoal oxidized in air has been developed. Since this result is empirical and not based upon detailed chemical mechanisms, further work is required to determine the extent of its applicability.

Predictions of the internal temperature . distribution in the burning sample can be made based on a simple one-dimensional conduction
model in a semi-infinite solid, if a value for the thermal diffusivity appropriate to wood charcoal at elevated temperatures can be obtained and adequate insulation is used around the bufning sample.

Besults of this study imply that both a gas phase reaction and substantial combustion in pores may be involved in the oxidation of wood charcoal in air. These detailed mechsnisms atill need elucidation.

\section*{ACKNOWLEDGEAENTS}

This work is a result of the thesis study of Evans and was supported in part by the National Science Foundation under Grant NSF G134734, and by the Division of Engineering and Applied Physics, Hazvard University.

\section*{LIST OF SYMBOLS}
a Moles of CO produced per mole C burned
A pre-exponential factor, \(\mathrm{B} / \mathrm{cm}^{2}\) sec atm b moles of \(\mathrm{CO}_{2}\) produced per mole C burned
burned specific heat, cal \(/ \mathrm{g}^{\circ} \mathrm{C}\)
c - specific heat, cal/g \({ }^{\circ} \mathrm{C}\)
D binary diffusion coefficient, specie j into air, assumed all equal to oxygen in calculation, \(\mathrm{cm}^{2} / \mathrm{sec}\)
\(E\) activation energy, cal/g-mole
\(h \quad\) heat transfer coefficient, \(\mathrm{cal} / \mathrm{cm}^{2} \mathrm{sec}\)

negative of the heat of combustion of charcoal to product \(i\), cal/g carbon \(h_{\text {m }} \quad\) mass transfer coefficient, \(\mathrm{g} / \mathrm{cm}^{2} \mathrm{sec}\) \(k\) thermal conductivity, cal/ \(\mathrm{cm} \sec { }^{\circ} \mathrm{C}\)
\(\boldsymbol{X} \quad A \exp (-E / R T)\)
1 distance from nozzle exit to impingement plane, cm
\(\dot{m}^{\prime \prime} \quad\) rate of increase of mass per unit time per unit area, g/cm \({ }^{2} \mathrm{sec}\)
\(M\) per unit area, g/cm
\(\begin{array}{ll}M & \text { molecular weight } \\ \mathrm{Nu} & \text { Nusselt number, } h \mathrm{~d} / \mathrm{k}\end{array}\)
P pressure, atm
A partial pressure of specie i, atm
\(\boldsymbol{R}\) ideal gas constant, cal \(/ \mathrm{g}\)-mole \({ }^{\circ} \mathrm{K}\)
RePr product of Reynolds and Prandt product of Rey
numbers, vd/a
ReSc product of Reynolds and Schmidt numbers, ud/D
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\begin{tabular}{|c|c|}
\hline \(t\) & diameter of heat flux sensor, cm \\
\hline Sh & Sherwood number, \(h_{\text {g }} d / p_{\text {sp }} D\) \\
\hline \(\nu\) & mainstream air velocity, rm/sec \\
\hline \(V\) & surface velocity, cm/sec \\
\hline \(x\) & ( \(a / 2\) ) + b [see eqns. (1), (2), (3)] \\
\hline \(\boldsymbol{X}\) & distance from the burning surface \\
\hline & the solid, cm \\
\hline \(\boldsymbol{X}_{1}\) & mole fraction of species ! \\
\hline \(\boldsymbol{Y}\) & mass fraction of species \({ }^{\text {a }}\) \\
\hline Gree & \\
\hline * & thermal diffusivity, \(k / \rho c, \mathrm{~cm}^{2} / \mathrm{sec}\) \\
\hline 1 & surace emissivity \\
\hline - & density, \(/ \mathrm{cm}^{2}\) \\
\hline - & Stefan-Bolizmann constant, cal \(/ \mathrm{cm}^{2}\) \\
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Subscripts
air ambien
\(c\) earbon
CO carbon monoxide
\(\mathrm{CO}_{2}\) curbon dioxide
\(\mathrm{m}_{2}\) property of the mixture
\(\mathrm{N}_{2}\) nitrogen
\(\mathrm{O}_{2}\) axygen
0 burning surface
initial value
Superseript
at the reference temperature for the
heats of formation \(-18^{\circ} \mathrm{C}\)

\section*{REPERENCES}

1 d. Nagle and R. F. 8 trickiand-Conatsble, Oxidation gearbon briwera 2000 and 2000 C, Froc. Fifih Carbon Cont., 1 (1961) 154 -164.
2 G. G. Ouboreff, J. E Laumen and R. H. Torborg. Tiwermal Radiation Properies §urvey, Haneywell Research Canter, Minseapolin, Minn, 2nd edn. (1960)

2 R. 1. Memor, 1. W. Amith and R. I. Tyier, Kinetie of combution of pulverised browa coal char betweon 830 and 2200 K , Combution asd Flame. 21 (1973) 183 -162.
4 A. Wheoler, Resetion rotes and seiectivity in catalyat porss, Adv. Cutalyais and Related Subjoets, Vol. 3, Aesdemic Preec, New York, 1951. pp. 275 -282.
3 R. Bird, w. Sleward and E. Lightoot, Transport Thrnomens, Wiley, New York, 1960, pp. 510512.
- R. Cardoa and 2. Cobonpue, Heat Lanafer between a fiet plate and jeis of air lanpinging un in, Intern. Heat Tranafar Coaf., University of Colorsio, 1961. 7 M . Jakob, Some invesigations in the seld of heat transfer, Proc. Phys Soc. London, 59 (1947) 736 -755.
1 J. R. Arthur, Renctions between carbon and oxyeve, Trans. Faraday Soc., 47 (1951) 164-178.
1. R. Arthur, D. H. Bapgham and J. R. Bowring. Kinetic aspects of the combustion of solid fuels, Third Symp. on Combustion, Fisme, and Expiosion Phenomens, Williams and Wilkias Co., Belimore. Maryland, 1949, pp. \(456-476\).
10 A. \&. Parker and H. C. Hotiel, Combustion rave of carben study of gen-fims atrueture by mierosampling. Ind. Eng. Chern., 28 (1936) 1334 . 1341.
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Attachment II to
Hazards Analyses of
Seabrook Station
Charcoal Filter Units,
YAEC 1571

Iodine Adsorber Fira Iest

\section*{performed for}

\section*{Tankee Atomic Electrio Co.} New Hamphire Iankee
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Introduction
The impregnated carbon used in the various alr cleaning systems is typically protected froz fire by water deluge ayatems. The initiation of the water deluge normily takes place by temperature rise aignal. Inis type or fire control has eeveral inherent problems:

b) water distribution in pleated carbon beds is non uniform
c) very large amounts of potentially contaminated witer ars generated.

To avoid these problems a aystem test was performed to evaluate the detection of earbon oxidation by \(c 0\) monttoring and to throttle carbon fires by stopping forced airflow through the carbon bed. Tests vere perfromed in both the iSTM ignition test rig and in the Fire Wind Tunnel ( \(F\) KT) to evaluate \(C O\) penetration and temperature seneration.

Description or the Equipment a Procedures
1) The ASTM D3466 Test Rig which consists of beated air flow through a earbon bed with inlet alr, inlet carbon bed and outlet carbon bed temperature measurement. The test is normally performed at 100 FPM relocity, hovever, for these tests the alrfiow was reduced to 40 FPM which is the design velocity of the Seabrook air cleaning systems. The bed depth normally is 1.0 inch deep for these tests. Two inch deep beds of \(50 \mathrm{ml}(-25 \mathrm{~g})\) of carbon was used.
2) The NUCON fire wind tunnel (FWT) consists of an adjustible flow blower followed by an indirect fired natural gas furnace to heat the air, and an adjustable plenum to hold a \(2 k\) inch \(X 24\) inch race area adsorber apeciven, and the commenaurate reduction for outlet ducting.

For these tests a 4.0 inch deep carbon bed was used filled with 25 XI and 25 IEDA impregnated carbon. The inlet temperature to the carbon bed was monitored at a single point in the center area four inches from inlet face of the adsorber. The outhet face of the adsorber was instruvented at 4.0 inches avay from the adsorber with five thermocouples. The CO monitor (an infrared sensor type) was taking samples 2 feet down stream from the filter outlet face in the 10 inch reduced duct section.
\begin{tabular}{|c|c|c|}
\hline er & full weight before fire was empty weight & \[
\begin{array}{ll}
65.8 & \mathrm{lbg} \\
18.4 \mathrm{bbe}
\end{array}
\] \\
\hline & as is carbon weight & 47.41 lbs \\
\hline & dry carbon weight (less \(\mathrm{H}_{2} \mathrm{O}\) ) & 43.6 Lbs \\
\hline
\end{tabular}

When the test was performed, the gas heater was turned on maximum heat to accomplish as fast heat-up as possible. Air flow mas maintained for five minutes after fire was detected, then airfiow was stopped and the carbon bed inlet and outlet temperatures monitored for 1 hour. The carbon bed was removed from the FWT and weighed.
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Test Result
The test (result of the oarbon burning test) in the ASTM rig was oonducted until all. of the carbon was consumed at 40 FPM velocity. The temperatures of the inlet and outlet carbon bed are shown on Table 1.

The results of the fire wind tunnel (FYT) test are shown on Table 2 and on Figure No. 1.

The pertinent values are as follows:
co of 50 ppmat 11 ninutes
Co off scale \((200+\mathrm{ppm})\) at 19 minutes
Fire in carbon bed at 19:15-19:45 minutes
Airfiow atopped at 24 minutea
Maximum Femperature \(\mathbf{~} 4.0\) inches from \(\quad 375^{\circ} \mathrm{C}\)
outlet face
Temperature at 1.0 hour after ignition with no alr flow 4.0 Inches from outhet face

Carbon loss, total test duration (excluding moisture and \(2 \$\) IEDA which would evaporate in test)
4.53 1bs

Carbon monoxide aignal aharply Increasing at inlet temperature of \(175^{\circ} \mathrm{C}\)
Filter frame (304 SS) bright red at 24 ainutes
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\section*{Evaluation of the Fest Resulta}

The configuration of air cleaning syatems is such that the iodine adsorbers are preceded by HEPA filters. The HEPA filter mounting frase is a seel atructure with 22 inch X 22 inch openings, therefore, mo iarger burning material than one HEPA filter size could onter from the carbon bed, anything larger would be stopped by the EEPA mounting frame structure even if it would penttrate the preceding-components. Thia was the reason for the selection of a 24 inch \(I 24\) Inch aarbon eection for the FWI test.

The Seabrook procedure is based on bhut down of the airifiow 5 tinutes after a co alarm. However, to maintain conservatism in the test, the airflow was shut down HOT 5 minutes arter CO alars, but 5 ainutes after actual burning of the carbon in the test section. Even under these conditions the maximum temperature at 4.0 Inches from the outlet face of the adsorber was only \(375^{\circ} \mathrm{C}\), and the temperature started to drop as soon as the blover was bhut off. It is important to note that no isolation dampers were closed in tbe inlet and outlet of the FNT, thus natural air convection wis maintained during the test even with the blower ahut orf, which is another conservatism because most air cleaning aystems are equipped with outlet dampers and several are isolatable on both inlet and outlet Eide.

The ASTM test rig data indicates (from Table 1) that even with airfiow maintained, approximately one hour is needed to burn 2.0 inch depth of carbon. While the results frow the FWT test indicate that ir airflow is atopped five minutes after carbon burning only approximately \(10 \%\) of the carbon is burned in one hour. While if the carbon monoxide signal is used for system isolation, the fire itself will probably be prevented.

The sharp increase in \(C O\) concentration at \(175^{\circ} \mathrm{C}\) inlet air temperature was also deterinined in the \(1 S T M\) test rig at 40 FPM and it indicated sharp riat at \(175^{\circ} \mathrm{C}\) Inlet air teaperature while autoignition did not take place until in excess of \(250^{\circ} \mathrm{C}\) indet air temperature.

Conclusions and Recommendations
Carbon monoxide monitoring is a very good detection method of carbon oxidation PRIOR TO ACTUAL aelrsustained burning of the carbon. Isolation of the aystem indicating fire within five anutes of \(C 0\) aignal will probably prevent development of selfsustaining carbon flre. Iaciation of the system can, after the fire develops during air flow, result in sharp temperature drop upon isolation or the air flow. The maximum temperature finches downstream of the burning carbon bed with air fiow at 40 FPM was \(375^{\circ} \mathrm{C}\).

Based on these results it is recomended that \(C 0\) monitors be instailed in the housing at outlet of the housing and another preferably in the inlet area (Just upstream from carbon beds at the top of housing, aince co is iighter than air)

The system should be isolated within five minutes of a CO signal of 50 ppm naximum.
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Table 1
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Carbon ignition followed by residual heating (1.e. air flow continued but heat orf).

Method: ASTM D3466 except: 40 FPM, 2 inch bed depth and fast beat up
Material: Dry alr and NUSORB KITEG II Lot 45/10
Starting condition: \(25^{\circ} \mathrm{C}\)
Ignition occurred at an upper bed (outlet) temperature or approximately \(400^{\circ} \mathrm{C}\), lower bed (inlet) temperature of \(285^{\circ} \mathrm{C}\), air inlet temp. \(285^{\circ} \mathrm{C}\).

Temperatures after ignition:

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Table 2
FII Test Data


Both inlet and outlet temperatures at 4.0 inches from filter face in the flow direction.
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\section*{F. 3 RESPONSES TO BTP APCSB 9.5-1, APPENDIX A}

This section presents a detailed comparison of the Branch Technical Position APCSB 9.5-1, Appendix A, on a position by position basis, with the approach taken in the design of Seabrook Station. Positions found in the left-hand column of each page of Appendix A are restated followed by a discussion as to how closely the plant design complies with the particular Appendix position. Each position and its corresponding response have been presented on a separate page(s).

It should be noted that Appendix A to Branch Technical Position APCSB 9.5-1 requires that plants for which applications for construction were docketed prior to July 1, 1976, but have not received a construction permit, address the positions presented in the left hand side of each page of Appendix A, whereas those plants for which construction permits were issued discuss the positions on the right hand side of the pages. Since the Licensing Board's Initial Decision awarding the Seabrook construction permits is dated June 29, 1976, whereas the permits themselves are dated July 7, 1976, it was debated whether the responses should be to the positions in the right-hand side of the pages. The decision reached was to address the left-hand side and, thereby, provide, in many cases, a more conservative response.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 15 \\
\hline
\end{tabular}

\section*{A. Overall Requirements of Nuclear Plant Fire Protection Program}

APCSB 9.5-1, App. A
Page Paragraph
1 A. 1

\section*{Personnel}

Responsibility for the overall fire protection program should be assigned to a designated person in the upper level of management. This person should retain ultimate responsibility even though formulation and assurance of program implementation is delegated. Such delegation of authority should be to staff personnel prepared by training and experience in fire protection and nuclear plant safety to provide a balanced approach in directing the fire protection programs for nuclear power plants. The qualification requirements for the fire protection engineer or consultant who will assist in the design and selection of equipment, inspect and test the completed physical aspects of the system, develop the fire protection program, and assist in the fire-fighting training for the operating plant should be stated. Subsequently, the FSAR should discuss the training and the updating provisions such as fire drills provided for maintaining the competence of the station fire-fighting and operating crew, including personnel responsible for maintaining and inspecting the fire protection equipment.

The fire protection staff should be responsible for:
(a) Coordination of building layout and systems design with fire area requirements, including consideration of potential hazards associated with postulated design basis fire,
(b) Design and maintenance of fire detection, suppression and extinguishing systems,
(c) Fire prevention activities,
(d) Training and manual fire fighting activities of plant personnel and the fire brigade.
(NOTE: NFPA 6 - Recommendations for Organization of Industrial Fire Loss Prevention, contains useful guidance for organization and operation of the entire fire loss prevention program).

The ultimate responsibility for the overall fire protection program for Seabrook Station rests with the Site Vice President.

The responsibility for various parts of the program has been delegated to other staff personnel and organizations prepared by training and experience in fire protection and in nuclear plant safety in order to provide a balanced approach in direction of the program.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 16 \\
\hline
\end{tabular}

The initial design, construction and basic engineering responsibility for building layout and systems design of Seabrook Station relative to fire area requirements, including consideration of potential hazards associated with postulated fires, fire detection, suppression and extinguishing systems, was assigned to the architect-engineer, United Engineers \& Constructors Inc. This included responsibility for design of fire detection, suppression, and extinguishing systems. Coordination of this effort at UE\&C was handled by a representative of UE\&C's fire protection group which was responsible for ensuring that all applicable fire protection and prevention codes and NRC regulatory requirements were complied with. The representative directed the conduct of the fire hazards analysis to verify that the effects of postulated fires were correctly evaluated and protected against. Final review and approval at UE\&C of the fire hazard analysis and the Fire Protection Reevaluation Report was performed by a staff-level fire protection engineer, an individual with an extensive background in fire protection design and evaluation. A copy of his resume has been included in this report.

During the initial design, construction and basic engineering, final review and approval of the layout and design came under the cognizance of Yankee Atomic Electric Company, Nuclear Services Division, who represented the owner. The responsibility for final review and approval of this effort with respect to fire area requirements was assigned to the Fire Protection Coordinator, who was also assigned the responsibility for the ultimate review and approval of the Seabrook fire hazard analysis and the Fire Protection Re-evaluation Report. A copy of the Yankee Atomic Electric Company Fire Protection Coordinator's resume has been included in this report. The responsibility for the fire prevention program during construction of Seabrook Station was assigned to the Resident Construction Manager. He and his staff were assisted in these activities by the YAEC Fire Protection Coordinator. Subsequent to construction completion and core load the corporate fire protection program responsibility has been assigned to the Director of Engineering. The Director of Engineering has assigned this responsibility to the Manager of Design Engineering to coordinate all fire protection activities and to perform technical reviews and evaluations of modifications and program implementation. Lead responsibility for fire protection engineering is assigned to corporate Design Engineering.

The responsibility for the maintenance of fire detection, suppression, and extinguishing systems has been assigned to the Seabrook Station Director. In addition, he has been assigned the responsibility for fire prevention activities at the plant, including training and manual fire fighting activities of plant personnel, including the fire brigade. He is assisted in these activities by his plant staff. The development of the in-plant program, plan and procedures is more fully addressed in responses to Paragraph B. 1 through B.7.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 17 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{2 A. 2}

\section*{Design Bases}

The overall fire protection program should be based upon evaluation of potential fire hazards throughout the plant and the effect of postulated design basis fires relative to maintaining ability to perform safety shutdown functions and minimize radioactive releases to the environment.

\section*{Response}

The overall fire protection systems for the Seabrook plant are based upon evaluation of potential fire hazards throughout the plant and the effect of postulated fires relative to maintaining ability to perform safe shutdown functions and minimize radioactive releases to the environment.

APCSB 9.5-1, App. A
Page Paragraph
2 A. 3

\section*{Back-up}

Total reliance should not be placed on a single automatic fire suppression system. Appropriate back-up fire suppression capability should be provided.

\section*{Response}

Total reliance has not been placed on a single automatic fire suppression system. In all instances, there is at least one back-up system available to suppress a fire. Additional back-up capability is provided by the fire brigade as well as response by an outside fire department. Portable fire extinguishers are provided throughout the plant for use on small fires.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 18 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 2 A. 4 \\ Single Failure Criterion}

A single failure in the fire suppression system should not impair both the primary and backup fire suppression capability. For example, redundant fire water pumps with independent power supplies and controls should be provided.

Postulated fires or fire protection system failures need not be considered concurrent with other plant accidents or the most severe natural phenomena. However, in the event of the most severe earthquake, i.e. the safe shutdown earthquake (SSE), the fire suppression systems should be capable of delivering water to manual hose stations located within hose reach of areas containing equipment required for safe plant shutdown. The fire protection system should, however, retain their original design capability for:
(1) natural phenomena of less severity and greater frequency (approximately once in 10 years) such as tornadoes, hurricanes, floods, ice storms or small intensity earthquakes which are characteristic of the site geographic region and
(2) for potential man-created site related events such as oil barge collisions, aircraft crashes which have a reasonable probability of occurring at a specific plant site. The effects of lightning strikes should be included in the overall plant fire protection program.

\section*{Response}

The fire suppression system includes three redundant fire water pumps; each pump designed to handle \(50 \%\) of capacity. One of the fire pumps is electrically driven while the other two are individually diesel engine driven. The electric power for the motor-driven pump is provided with two independent power supplies. Each diesel engine-driven pump has its own controller. Each controller has two independent batteries. Upon loss of power from one battery, the other battery is available to supply the required power for starting the diesel engine-driven pump. Each controller is furnished with a battery charger for charging both batteries simultaneously.

The yard fire water main piping is supplied from the three independent discharge lines from the fire pumps. These lines feed the fire main piping in two directions.

The fire tanks are grounded; the fire pumps are housed within a grounded building; the fire lines are run underground and are free from the effects of lightning. Adequate grounding in plant buildings provides assurance that the effects of lightning strikes will not degrade the performance of fire detection systems.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 19 \\
\hline
\end{tabular}

Those portions of the fire suppression system which are underground or contained in seismic Category I buildings are protected against tornadoes and tornado driven missiles. The potential for damage of other portions of the fire suppression system by tornadoes is low because of the low incidence of tornadoes in the Seabrook area.

The entire fire suppression system including the fire pump house structure and fire protection storage tanks is designed to withstand the effects of the 100 year hurricane- 110 mph . (See FSAR, Section 3.3). This wind could possibly cause the removal of some of the steel siding of the fire pump house, but would not otherwise cause the building structure to fail.

Since the elevation of the fire pump house floor slab is \(21^{\prime}-0\) ', the 100 year flood which results in a still water elevation of 20.6' would cause no damage to the fire suppression system components here. Seabrook FSAR Section 3.4.1 describes the flood protection provided for Category I structures and their contents.

All buildings containing fire suppression systems are designed to withstand the 100 year snow and/or ice storm, which is equivalent to a roof loading of 75 psf (see FSAR Section 2.3).

In general, the fire suppression system is not designed as a seismic Category I system. However, those portions of this system within seismic Category I structures necessary to deliver water to manual hose stations located within hose reach of areas containing equipment required for safe plant shutdown are designed to withstand the effects of the SSE. Three exceptions are certain hose stations serving the Control Building, "A" Train Electrical Tunnel, and "B" Train Electrical Tunnel. These hose stations were added so that the served areas could be reached with an effective water stream using a maximum hose length of 100 feet. For physical reasons, they are connected to the non-seismic part of the fire protection system. During a fire, however, the fire brigade can add additional hose to other seismic hose stations serving these areas to provide satisfactory coverage if the non-seismic stations are unavailable. The fire pump house, as with all non-seismic Category I buildings, is designed to the requirements of the Uniform Building Code. Thus, the pump house structure will not fail as a result of an earthquake with a ground acceleration up to approximately 0.12 g . In the Seabrook area, the 10 year earthquake is estimated to have a ground acceleration of approximately 0.05 g .

In the event of the most severe earthquake, the SSE, the fire suppression system is capable of delivering water to manual hose stations located within hose reach of areas containing equipment required for safe plant shutdown in the following manner:
All such areas (except as noted above) are provided with standpipes (Category I design) which are connected through an administratively controlled valve to plant service water system, also seismic Category I designed.

The potential for man-created, site related events such as oil barge collisions, aircraft crashes and explosions which could adversely affect the fire suppression system is of a very low probability. The details pertaining to these events are given in the FSAR Section 2.2 and in the NRC staff Safety Evaluation Report for the Seabrook station.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 20 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{3 A. 5}

\section*{Fire Suppression System}

Failure or inadvertent operation of the fire suppression system should not incapacitate safety related systems or components. Fire suppression systems that are pressurized during normal plant operation should meet the guideline specified in APCSB Branch Technical Position 3-1, "Protection Against Postulated Piping Failures in Fluid Systems Outside Containment".

\section*{Response}

The failure or inadvertent operation of the fire suppression systems will not incapacitate safety related systems or components.

The fixed fire suppression system for safety-related areas consists of standpipes and hose reels and automatic water spray systems. All standpipes are pressurized except those in the containment building which are dry. The automatic pre-action sprinkler systems are pressurized with air but are not wet until actuated by the Fire Detection System. The automatic water spray deluge systems are not pressurized. The standpipes in the containment building are not pressurized until the water supply valves are opened.

Standpipes and automatic water spray deluge piping systems in safety-related areas are designed and supported as required for a Category I system to prevent pipe failure and subsequent pipe whip.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 21 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{3 A. 6}

\section*{Fuel Storage Areas}

The fire protection program (plans, personnel and equipment) for buildings storing new reactor fuel and for adjacent fire zones which could affect the fuel storage zone should be fully operational before fuel is received at the site. Schedule for implementation of modifications, if any, will be established on a case-by-case basis.

\section*{Response}

The fire protection system for the fuel area and the adjacent fire areas was operational prior to receiving fuel on site. The portion of the fire protection program required to protect the new fuel storage building, including implementing procedures and personnel training, was in effect prior to receiving fuel on site.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{\(4 \quad\) A. 7}

\section*{Fuel Loading}

The fire protection program for an entire reactor unit should be fully operational prior to initial fuel loading in that reactor unit. Schedule for implementation of modifications, if any, will be established on a case-by-case basis.

\section*{Response}

The fire protection program was operational prior to initial fuel loading.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 22 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{4 A. 8}

\section*{Multiple-Reactor Sites}

On multiple-reactor sites where there are operating reactors and construction of remaining units is being completed, the fire protection program should provide continuing evaluation and include additional fire barriers, fire protection capability, and administrative controls necessary to protect the operating units from construction fire hazards. The superintendent of the operating plant should have the lead responsibility for site fire protection.

\section*{Response}

Seabrook 2 construction activities have been stopped. The fire protection program developed for Seabrook 1 provides for a continuing evaluation and the administrative controls necessary to protect the operating unit from fire hazards. The provision of additional fire protection capability is based upon the results of this continuing evaluation. The response to Paragraph A. 1 provides the responsibilities applicable to the post-construction operational phase.

APCSB 9.5-1, App. A

\section*{Page Paragraph}

4 A. 9
Simultaneous Fires
Simultaneous fires in more than one reactor need not be postulated where separation requirements are met. A fire involving more than one reactor unit need not be postulated except for facilities shared between units.

\section*{Response}

A fire involving more than one reactor has not been postulated. Construction on Seabrook 2 has been stopped.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
Page 23 \\
\hline
\end{tabular}

\section*{B. Administrative Procedures, Controls and Fire Brigade}

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{4 B. 1}

\section*{Fire Protection System and Personnel Administrative Procedures}

Administrative procedures consistent with the need for maintaining the performance of the fire protection system and personnel in nuclear power plants should be provided.

Guidance is contained in the following publications:
NFPA 4 - Organization for Fire Services
NFPA 4A - Organization for Fire Department
NFPA 6 - Industrial Fire Loss Prevention
NFPA 7 - Management of Fire Emergencies
NFPA 8 - Management Responsibility for Effects of Fire on Operations
NFPA 27 - Private Fire Brigades

\section*{Response}

Administrative procedures consistent with the need for maintaining the performance of the fire protection system and personnel in nuclear power plants is provided using the guidance contained in the appropriate NFPA publications. These procedures are described in the Station Fire Protection Manual.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
Page 24 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 5 B. 2 \\ Bulk Storage of Combustible Materials}

Effective administrative measures should be implemented to prohibit bulk storage of combustible materials inside or adjacent to safety related buildings or systems during operation or maintenance periods. Regulatory Guide 1.39, "Housekeeping Requirements for Water-Cooled Nuclear Power Plants", provides guidance on housekeeping, including the disposal of combustible materials.

\section*{Response}

Effective administrative measures are implemented to govern the storage of materials and the housekeeping of the plant. The plant "Station Maintenance Manual" shall be the governing administrative document for housekeeping. The "Station Fire Protection Manual" is the administrative manual to control combustible materials.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

5 B. 3

\section*{Normal/Abnormal Conditions Or Other Anticipated Operations}

Normal and abnormal conditions or other anticipated operations such as modifications (e.g., breaking fire stops, impairment of fire detection and suppression systems) and refueling activities should be reviewed by appropriate levels of management and appropriate special actions and procedures such as fire watches or temporary fire barriers implemented to assure adequate fire protection and reactor safety. In particular:
(a) Work involving ignition sources such as welding and flame cutting should be done under closely controlled conditions. Procedures governing such work should be reviewed and approved by persons trained and experienced in fire protection. Persons performing and directly assisting in such work should be trained and equipped to prevent and combat fires. If this is not possible, a person qualified in fire protection should directly monitor the work and function as a fire watch.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 25 \\
\hline
\end{tabular}
(b) Leak testing, and similar procedures such as air flow determination, should use one of the commercially available aerosol techniques. Open flames or combustion generated smoke should not be permitted.
(c) Use of combustible material, e.g., HEPA and charcoal filters, dry ion exchange resins or other combustible supplies, in safety related areas should be controlled. Use of wood inside buildings containing safety related systems or equipment should be permitted only when suitable non-combustible substitutes are not available. If wood must be used, only fire-retardant treated wood (scaffolding, lay down blocks) should be permitted. Such materials should be allowed into safety related areas only when they are to be used immediately. Their possible and probable use should be considered in the fire hazard analysis to determine the adequacy of the installed fire protection systems.

\section*{Response}

Any plant modifications, engineering design change requests, and plant design change requests are reviewed for fire protection concerns. Plant procedures are reviewed by plant management. Maintenance procedures, except for routine jobs in non-controlled areas, are reviewed by plant management.
(a) Work involving welding, cutting and brazing is controlled and covered in the Station Fire Protection Manual.
(b) Open flames or combustion generated smoke will not be used for leak testing or air flow determinations.
(c) Storage of combustible supplies are controlled in plant areas. Use of wood is controlled by the Station Fire Protection Manual. In-situ combustibles are considered in the fire hazards analysis. Transient combustibles used during maintenance or refueling are controlled by the Station Fire Protection Manual.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 26 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 6 B. 4 \\ Public Fire Department Support}

Nuclear power plants are frequently located in remote areas, at some distance from public fire departments. Also, first response fire departments are often volunteer. Public fire department response should be considered in the overall fire protection program. However, the plant should be designed to be self-sufficient with respect to fire fighting activities and rely on the public response only for supplemental or backup capability.

\section*{Response}

The plant fire protection systems plus the fire brigade allow the plant to be self-sufficient with respect to fire fighting. Reliance on the local fire department is for backup capability.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{\(7 \quad\) B. 5}

\section*{Plant Fire Brigade Guidance}

The need for good organization, training and equipping of fire brigades at nuclear power plant sites requires effective measures be implemented to assure proper discharge of these functions. The guidance in Regulatory Guide 1.101, "Emergency Planning for Nuclear Power Plants", should be followed as applicable.
(a) Successful fire fighting requires testing and maintenance of the fire protection equipment, emergency lighting and communication, as well as practice as brigades for the people who must utilize the equipment. A test plan that lists the individuals and their responsibilities in connection with routine tests and inspections of the fire detection and protection systems should be developed. The test plan should contain the types, frequency and detailed procedures for testing. Procedures should also contain instructions on maintaining fire protection during those periods when the fire protection system is impaired or during periods of plant maintenance, e.g., fire watches or temporary hose connections to water systems.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
Page 27
\end{tabular} \\
\hline
\end{tabular}
(b) Basic training is a necessary element in effective fire fighting operation. In order for a fire brigade to operate effectively, it must operate as a team. All members must know what their individual duties are. They must be familiar with the layout of the plant and equipment location and operation in order to permit effective fire fighting operations during times when a particular area is filled with smoke or is insufficiently lighted. Such training can only be accomplished by conducting drills several times a year (at least quarterly) so that all members of the fire brigade have had the opportunity to train as a team, testing itself in the major areas of the plant. The drills should include the simulated use of equipment in each area and should be pre planned and post-critiques to establish the training objective of the drills and determine how well these objectives have been met. These drills should periodically (at least annually) include local fire department participation where possible. Such drills also permit supervising personnel to evaluate the effectiveness of communications within the fire brigade and with the on scene fire team leader, the reactor operator in the control room, and the offsite command post.

\section*{Response}
(a) Effective measures for training and equipping fire brigades, testing and maintaining fire protection equipment, emergency lighting and communication have been implemented to cover the above subjects.

Testing and inspections of fire detection and protection systems have been covered by established procedures.
(b) Fire brigade training is accomplished in a manner to include all of the above concerns.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 28 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
8 B. 6

\section*{Coordination With Local Fire Department}

To have proper coverage during all phases of operation, members of each shift crew should be trained in fire protection. Training of the plant fire brigade should be coordinated with the local fire department so that responsibilities and duties are delineated in advance. This coordination should be part of the training course and implemented into the training of the local fire department staff. Local fire departments should be educated in the operational precautions when fighting fires on nuclear power plant sites. Local fire departments should be made aware of the need for radioactive protection of personnel and the special hazards associated with a nuclear power plant site.

\section*{Response}

Selected shift crew personnel are trained in fire protection. Shift crew fire protection training is by job classification which is directed towards those individuals who are at liberty to leave the control room during various phases of plant operation.

The plant fire protection training program is offered annually to local fire departments where practicable. Local fire department training curriculum includes the pertinent aspects of:
a. Station layout
b. Operational precautions
c. Radiological and other hazards
d. Types and locations of probable fires
e. Responsibilities and limitations of authority
f. Other topics, as necessary
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 29 \\
\hline
\end{tabular}

APCSB 9.5-1, App. A
Page Paragraph

\section*{\(9 \quad\) B. 7}

\section*{NFPA Standards}

NFPA 27, "Private Fire Brigade" should be followed in organization, training, and fire drills. This standard also is applicable for the inspection and maintenance of fire fighting equipment. Among the standards referenced in this document, the following should be utilized: NFPA 194, "Standard for Screw Threads and Gaskets for Fire Hose Couplings", NFPA 196, "Standard for Fire Hose", NFPA 197, "Training Standard on Initial Fire Attacks", NFPA 601, "Recommended Manual of Instructions and Duties for the Plant Watchman on Guard". NFPA booklets and pamphlets listed on page 27-11 of Volume 8, 1971-72 are also applicable for good training references. In addition, courses in fire prevention and fire suppression which are recognized and/or sponsored by the fire protection industry should be utilized.

\section*{Response}

Fire brigade training is formulated around the recommendations in NFPA 27. Other NFPA manuals are used as they apply to the plant fire protection program.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 30 \\
\hline
\end{tabular}

\section*{C. Quality Assurance Program}

Quality Assurance (QA) programs of applicants and contractors should be developed and implemented to assure that the requirements for design, procurement, installation, and testing and administrative controls for the fire protection program for safety-related areas as defined in this Branch Position are satisfied. The program should be under the management control of the Oversight organization. The QA program criteria that apply to the fire protection program should include the following:

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

10 C. 1

\section*{Design Control and Procurement Document Control}

Measures should be established to assure that all design related guidelines of the Branch Technical Position are included in design and procurement documents and that deviations therefrom are controlled.

\section*{Response}

During initial design and construction UE\&C engineering organization prepared fire protection design engineering and procurement documents which met the guidelines of the Branch Technical Positions. The Yankee Atomic Electric Company (YAEC) reviewed design and procurement documents to ensure compliance. The above functions are currently the responsibility of Engineering.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 31 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{10 C. 2}

\section*{Instructions, Procedures and Drawings}

Inspections, tests, administrative controls, fire drills and training that govern the fire protection program should be prescribed by documented instructions, procedures or drawings and should be accomplished in accordance with these documents.

\section*{Response}

Detailed, written operational test, inspection, fire drill, training and administrative control procedures for the fire protection program have been prepared by the plant staff. These activities are audited by the Oversight Organization.

APCSB 9.5-1, App. A

\section*{Page Paragraph}

10 C. 3
Control of Purchased Material, Equipment and Services
Measures should be established to assure that purchased material, equipment and services conform to the procurement documents.

\section*{Response}

The Operational Quality Assurance Program (OQAP) defines and establishes the application of the OQAP to Fire Protection Program.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 32 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{11 C. 4}

\section*{Inspection}

A program for independent inspection of activities affecting fire protection should be established and executed by, or for, the organization performing the activity to verify conformance with documented installation drawings and test procedures for accomplishing the activities.

\section*{Response}

The Oversight organization performs audits to verify implementation of the fire protection program.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{11 C. 5}

\section*{Test and Test Control}

A test program should be established and implemented to assure that testing is performed and verified by inspection and audit to demonstrate conformance with design and system readiness requirements. The tests should be performed in accordance with written test procedures; test results should be properly evaluated and acted on.

\section*{Response}

A fire protection test program has been established and implemented to assure that the fire protection systems are in conformance with the design requirements. Current station procedures provide for tests and inspections to assure readiness of the systems and its components. The fire protection surveillance program is audited by the Oversight organization.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 33 \\
\hline
\end{tabular}

APCSB 9.5-1, App. A
Page Paragraph
11 C. 6

\section*{Inspection, Test and Operating Status}

Measures should be established to provide for the identification of items that have satisfactorily passed required tests and inspections.

\section*{Response}

Procedure documentation is provided for the identification of items that have satisfactorily passed required tests and inspections. The Oversight organization performs audits to verify documentation.

APCSB 9.5-1, App. A
Page Paragraph
11 C. 7
Non- Conforming Items
Measures should be established to control items that do not conform to specified requirements to prevent inadvertent use or installation.

\section*{Response}

The OQAP provides measures to control the use of items and to prevent inadvertent use or installation of non-conforming items.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 34 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{11 C. 8}

\section*{Corrective Action}

Measures should be established to assure that conditions adverse to fire protection, such as failures, malfunctions, deficiencies, deviations, defective components, uncontrolled combustible material and non-conformances are promptly identified, reported and corrected.

\section*{Response}

Measures have been established and implemented via the Fire Protection Program per the responsibilities discussed in the response to Paragraph A.1.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

12 C. 9
Records
Records should be prepared and maintained to furnish evidence that the criteria enumerated above are being met for activities affecting the fire protection program.

Response
Records for fire protection activities are prepared and maintained per Administrative Procedures.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 35 \\
\hline
\end{tabular}

APCSB 9.5-1, App. A
Page Paragraph
12 C. 10
Audits
Audits should be conducted and documented to verify compliance with the fire protection program including design and procurement documents; instructions; procedures and drawings; and inspection and test activities.

\section*{Response}

The Oversight organization provides audits to verify the above activities.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 36 \\
\hline
\end{tabular}

\section*{D. General Guidelines for Plant Protection}

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{12 D. 1 (a)}

\section*{Building Design - Plant Layouts}

Plant layouts should be arranged to:
(1) Isolate safety-related systems from unacceptable hazards, and
(2) Separate redundant safety-related systems from each other so that both are not subject to damage from a single fire hazard.

\section*{Response}

The above stated design requirements of "isolation and separation" have been adhered to in the layout of the plant, to the maximum extent practical. Where safety-related systems cannot be isolated from potential fire hazards, additional detection, barriers and/or automatic fire suppression methods with appropriate backup are provided.

Those safety-related systems which are required to safely shut down the plant consist of separate and independent flow trains. No portions of these systems are located near or in any area which could potentially become a significant fire hazard. In those cases where redundant safety-related equipment (e.g. the primary component cooling water heat exchangers) are not separated from each other by a physical barrier, no combustible materials of any significant quantity are present within the immediate vicinity of the equipment, precluding the possibility of damage to redundant equipment due to a potential fire. Where necessary, an adequate barrier is provided to prevent the propagation of a postulated fire caused by combustible material contained in one safety-related component (e.g. component cooling pump) from jeopardizing the operation of a redundant component.

Electrical and instrument layouts are arranged to isolate safety-related systems from unacceptable fire hazards by eliminating the use of combustible materials to the greatest extent possible. Redundant safety-related electrical equipment are separated from each other by physical barriers or distance to prevent both systems from damage due to a single fire hazard. Each diesel generator has been structurally segregated from its redundant adjacent unit. The wall which separates the units on the main level and below is constructed of two-foot thick reinforced concrete with a fire rating in excess of three hours. Upper floor walls, which are one-foot thick reinforced concrete, have a three hour fire rating.

The circulating and service water areas are separated by a two-foot thick reinforced concrete wall whose fire rating is in excess of one and one-half hours. (Reference Deviation \#3, SBN-904).
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 37 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 3 D. 1 (b) \\ Building Design - Detailed Fire Hazard Analysis}

In order to accomplish l.(a) above, safety related systems and fire hazards should be identified throughout the plant. Therefore, a detailed fire hazard analysis should be made. The fire hazards analysis should be reviewed and updated as necessary.

\section*{Response}

A detailed fire hazards analysis of all areas which include safe shutdown systems has been provided in this report. The need for additional hazard analyses will be determined based on the type and extent of proposed plant modifications.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{13 D. 1 (c)}

\section*{Building Design - Cable Spreading Room}

For multiple reactor sites, cable spreading rooms should not be shared between reactors. Each cable spreading room should be separated from other areas of the plant by barriers (walls and floors) having a minimum fire resistance of three hours. Cabling for redundant safety divisions should be separated by walls having three hour fire barriers.

\section*{Response}

The cable spreading room is designated a "fire area" and is separated from other areas of the plant by fire barriers having a fire resistance of three hours. Three hour fire barrier walls are not provided between redundant safety-related cable trays in the cable spreading room because the space allocation of the station design makes it physically impossible. However, the redundant safety-related cables are located in the cable trays which are separated by distance, and this distance meets or exceeds that required by "Attachment C, Physical Independence of Electric Systems" of AEC letter dated \(12 / 14 / 73\), which is generally in agreement with Regulatory Guide 1.75.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 38 \\
\hline
\end{tabular}

In addition, the cable spreading room does not contain high energy equipment such as switchgear, transformers or potential sources of missile or pipe whip, and is not used for storage of flammable materials. Circuits in trays are limited to control and instrument functions. Those power supply circuits serving the control room are routed in embedded conduits. All cables are self-extinguishing and non-propagating and, as a minimum, pass the IEEE-383 1974 flame test. See response to D.3(c) for justification of design.

APCSB 9.5-1, App. A

\section*{Page Paragraph}

13 D. 1 (d)

\section*{Building Design - Non-Combustibility Requirements for Interior Construction}

Interior wall and structural components, thermal insulation materials and radiation shielding materials and sound-proofing should be non-combustible. Interior finishes should be non-combustible or listed by a nationally recognized testing laboratory, such as Factory Mutual or Underwriters' Laboratory, Inc. for flame spread, smoke and fuel contribution of 25 or less in its configuration (ASTM E-84 Test, "Surface Burning Characteristics of Building Materials").

\section*{Response}

Thermal insulating materials meet the non-combustible definition in Branch Technical Position CMEB 9.5-1, "Guidelines for Fire Protection for Nuclear Power Plants." They have flame spread/smoke developed/fuel contributed rating of \(25 / 50 / 50\), as tested by Underwriters' Laboratories Inc. in its use configuration, ASTM E-84 test "Surface Burning Characteristics of Building Materials."

Interior walls and structural components, radiation shielding materials and sound-proofing and interior finishes are non-combustible or listed by a nationally recognized testing laboratory, such as Factory Mutual or Underwriters' Laboratory, Inc. for flame spread, smoke and fuel contribution of 25 or less in its use configuration, ASTM E-84 Test, "Surface Burning Characteristics Building Materials"

Prior to 1978 the ASTM E-84 Test reported flame spread, smoke developed and fuel contribution. However, fuel contribution is no longer reported. Therefore, materials tested prior to 1978 must report flame spread, smoke developed and fuel contribution. Materials tested in 1978 and after must only report flame spread and smoke developed.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 39 \\
\hline
\end{tabular}

APCSB 9.5-1, App. A
Page Paragraph
13 D. 1 (e)

\section*{Building Design - Metal Deck Roof Construction}

Metal deck roof construction should be non-combustible (see the building materials directory of the Underwriters' Laboratory, Inc.) or listed as Class I by Factory Mutual System Guide.

\section*{Response}

Metal deck roof construction is non-combustible or listed as Class I by Factory Mutual System Approval Guide.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

14 D. 1 (f)

\section*{Building Design - Suspended Ceilings}

Suspended ceilings and their supports should be of non-combustible construction. Concealed spaces should be devoid of combustibles.

\section*{Response}

Suspended ceilings and their supports are non-combustible construction.
Concealed spaces in safety-related areas are devoid of combustibles. Such spaces, however, may contain metal-sheathed lighting cable type "ALS", which is not considered combustible.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 40 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
14 D. 1 (g)

\section*{Building Design - High Voltage. High Ampere Transformers}

High voltage - high ampere transformers installed inside buildings containing safety related systems should be of the dry type or insulated and cooled with non-combustible liquid.

\section*{Response}

The only high voltage - high ampere transformers installed inside buildings containing safety related systems are 480 volt unit substations which utilize dry type transformers.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

14 D. 1 (h)

\section*{Building Design - Oil Filled Transformers}

Buildings containing safety related systems should be protected from exposure or spill fires involving oil filled transformers by:
locating such transformers at least 50 feet distant; or
ensuring that such building walls within 50 feet of oil filled transformers are without openings and have a fire resistance rating of at least three hours.

\section*{Response}

The generator step-up transformers, unit auxiliary transformers and reserve auxiliary transformers are the only oil-filled transformers, and are located outside along the north wall of the turbine building. The north wall has a three hour fire resistance rating. Refer to Tab 15. All oil-filled transformers are protected by automatic water spray systems, and are located at least 50 feet from any safety related systems.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 41 \\
\hline
\end{tabular}

APCSB 9.5-1, App. A
Page Paragraph

\section*{15 D. 1 (i)}

\section*{Building Design - Floor Drains}

Floor drains, sized to remove expected fire fighting water flow should be provided in those areas where fixed water fire suppression systems are installed. Drains should also be provided in other areas where hand hose lines may be used if such fire fighting water could cause unacceptable damage to equipment in the area. Equipment should be installed on pedestals, or curbs should be provided as required to contain water and direct it to floor drains (see NFPA 92M "Waterproofing and Drainage of Floors"). Drains in areas containing combustible liquids should have provisions for preventing the spread of the fire throughout the drain system. Water drainage from areas which may contain radioactivity should be sampled and analyzed before discharge to the environment.

\section*{Response}

Floor drains are located in those areas where automatic sprinkler and spray systems are installed. These drains are sized to pass the expected flows resulting from automatic system actuation, as well as that produced by manual hose application if employed.

In areas where hand hose lines are the only water sources utilized to combat a fire, drains are provided if accumulation of fire fighting water could result in unacceptable damage to safety-related equipment in the area. In such areas, the operator can use the hose to control the quantity of drain water to avoid unacceptable damage to equipment.

Water drainage from buildings with potential for radioactive contamination will be routed to the waste processing building, where it is sampled and analyzed for radioactivity.

Drainage within the diesel generator building is designed to prevent the spread of fire from one area to another. Other areas with combustible liquids have normally closed shut-off valves in the drain lines or drain directly to the oil/water separation vault.

A fire in the primary auxiliary building, should it occur, may require large amounts of fire fighting water, which could result in the PAB floor drain sump overflowing and spilling over into the pipe tunnel between the vault area and the containment building. The combined pipe tunnel area and the PAB sump can hold up to 14,000 gallons of fire fighting water. Water in excess of this would overflow into the vault No. 2 floor drain sump. This contained water would not jeopardize the operability of safety-related equipment and equipment required for a safe plant shutdown. Contaminated drainage is processed through the liquid waste system. Sump pumps located in the affected areas pump water at a nominal rate of 25 gpm per pump to the floor drain tanks in the waste processing building. Provisions for sample analysis are available at the waste test tank prior to discharge to the environment.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 42 \\
\hline
\end{tabular}

In the event of a fire in either the waste processing building or the fuel storage building, the fire fighting water could drain to the lowest elevation of the building, where it would be contained. Any resulting flooding in either building would thus not jeopardize the operability of safety-related equipment or equipment required for the safe shutdown of the plant. Sump pumps located in the affected areas pump water at a nominal rate of 25 gpm per pump to the floor drain tanks in the waste processing building.

If a fire requiring large amounts of water should occur in the containment building, there exists a possibility of flooding the reactor instrument cavity. However, the cavity can hold more than 47,000 gallons of water without jeopardizing the operability of safety-related equipment or equipment required for safe shutdown of the plant. Sump pumps located in the affected areas pump water at a nominal rate of 25 gpm per pump to the floor drain tanks in the waste processing building.

All safety-related equipment, except draw-out switchgear and local control panels are mounted on pedestals to avoid water damage, or provided with curbs or other barriers, as required, to contain the water and direct it to floor drains. The draw-out switchgear and local control panels are capable of withstanding a minimal degree of floor flooding without damage.

The electrical tunnels contain no sources of flood water other than the fire protection system piping. The fire protection system piping are zoned pre-action dry pipe systems with the zone valves located external to the tunnel areas. The individual fire protection system zones will be actuated by ionization fire detectors. Fire detectors are provided in the areas zoned to provide for local indication and for an audible and visual alarm in the control room and the guardhouse. Water from the fire protection system will be drained from the tunnel zones to a sump external to the electrical tunnel areas.

Redundant pumps have been installed in the sump to pump the water collected from the tunnel fire water drains to the storm drain system.

The electrical tunnel areas are zoned for fire protection. It is highly improbable that a fire will occur in more than one zone at any time; therefore the capacity of each pump is based on the flow of the largest tunnel zone. Each pump is connected to a redundant emergency bus. The installed pump capacity is capable of handling the flow requirements from two zones at all times except in the event of loss of power on one emergency bus.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
Page 43
\end{tabular} \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 15 D. 1 (j) \\ Building Design - Floors, Walls and Ceilings}

Floors, walls and ceilings enclosing separate fire areas should have minimum fire rating of three hours. Penetrations in these fire barriers, including conduits and piping, should be sealed or closed to provide a fire resistance rating at least equal to that of the fire barrier itself. Door openings should be protected with equivalent rated doors, frames and hardware that have been tested and approved by a nationally recognized laboratory. Such doors should be normally closed and locked or alarmed with alarm and annunciation in the control room. Penetrations for ventilation system should be protected by a standard "fire door damper" where required. (Refer to NFPA 80, "Fire Doors and Windows".)

\section*{Response}

Except for exterior walls and ceilings, floors, walls and ceilings enclosing separate fire areas have a minimum \(11 / 2\) hour or three hour fire rating. Stairwells have three hour rated walls and \(11 / 2\) hour rated doors.

Penetrations in fire barriers having a fire resistance of three hours, including conduits, piping and sleeves, are sealed or closed with materials providing a fire resistance rating at least equal to that designated for the fire barrier itself, with the exception of bus duct penetrations in the east wall of the non essential switchgear room and bus duct penetration in the north wall of turbine building. Refer to Deviation 14, SBN 970, dated March 18, 1986.

Door openings, except where noted above, are protected with equivalent rated doors, frames and hardware that have been tested and approved by a nationally recognized laboratory. Only doors providing access to the buildings from outside or doors providing access to vital areas are locked and alarmed.

Penetrations for ventilation ducts are protected by a standard "fire door damper", where required, with a fire rating equal to fire barrier itself.

For compliance of 3-hour rated double leaf pressure doors in fire zones GB-FI 2B-A, CB-F-2B-A, CB-F-2C-A and PAB-F-2B-Z, refer to Deviation No. 11, SBN 932, dated March 18, 1986. Refer to the following letters for additional deviations: Deviation 5, SBN-904; Deviation 6, SBN-904; Deviation 7, SBN-904; Deviation 8, SBN-904.

The sub units of multi-section type rated fire dampers, CBA-DP-131 (CB-F-4A-A); DAH-DP-163 \& 164 (DG-F-3A-Z \& 3B-Z) have been independently tested and UL certified. Refer to Deviation No. 12, SBN 932, dated January 24, 1986; and Deviation 8, SBN-970.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 44 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 16 D. 2 (a) \\ Control of Combustibles \\ Protection of Safety-Related Systems}

Safety related systems should be isolated or separated from combustible materials. When this is not possible because of the nature of the safety system or the combustible material, special protection should be provided to prevent a fire from defeating the safety system function. Such protection may involve a combination of automatic fire suppression and construction capable of withstanding and containing a fire that consumes all combustibles present. Examples of such combustible materials that may not be separable from the remainder of its system are:
(1) emergency diesel generator fuel oil day tanks
(2) turbine generator oil and hydraulic control fluid systems
(3) reactor coolant pump lube oil system

\section*{Response}

All safety related systems are isolated or separated from combustible material wherever feasible. Where isolation is not feasible, as noted below, the fire protection system supplies suppression, based on the fire hazard analysis, to insure that a fire does not defeat the safety system function.
(1) The redundant emergency diesel generator fuel oil day tank and associated piping are separated from each other by three hour fire rated barriers. No combustible materials other than the fuel oil in the day tank and piping is stored in the area. Each system is protected by an automatic deluge water spray system which is actuated by a detection system.
(2) The turbine-generator lube oil tank and reservoir, even though a non safety-related system, is separated and protected as described above.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 45 \\
\hline
\end{tabular}
(3) The reactor coolant pump oil systems are provided with an oil collection system and are isolated by virtue of spatial separation and would, should a fire occur, only involve one reactor coolant pump area. The fire hazard analysis presented in Appendix B of this report demonstrates that during a design basis fire, except for the vertical shaft of fire influence, the operation of the containment fan coolers and the heat sink of the steel and concrete would limit the temperature of the general containment area to \(253^{\circ} \mathrm{F}\). The associated pressure at this time in the containment would be 4.0 psig . This temperature and pressure throughout the containment would not prevent the safe shutdown of the reactor. The vertical shaft of fire influence, while being much hotter than the general area (flame temperature of \(4000^{\circ} \mathrm{F}\) ), does not impinge on, nor would it damage, any system or components required for safe shutdown of the reactor.

Based on the results of the fire hazard analysis, no fire suppression system is provided in these areas.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{16 D. 2 (b)}

\section*{Bulk Gas Storage}

Bulk gas storage (either compressed or cryogenic), should not be permitted inside structures housing safety-related equipment. Storage of flammable gas such as hydrogen, should be located outdoors or in separate detached buildings so that a fire or explosion will not adversely affect any safety-related systems or equipment. (Refer to NFPA 50A, "Gaseous Hydrogen Systems".)
Care should be taken to locate high pressure gas storage containers with the long axis parallel to building walls. This will minimize the possibility of wall penetration in the event of a container failure. Use of compressed gases (especially flammable and fuel gases) inside buildings should be controlled. (Refer to NFPA 6, "Industrial Fire Loss Prevention".)

\section*{Response}

There are no large bulk containers (non-DOT cylinders) of flammable gas inside structures near safety-related equipment. Bulk Hydrogen storage is located outdoors and remote from any safety related equipment. The bulk gas storage located within the Turbine Building is the non-flammable, low pressure \(2-3 / 4\) ton, carbon dioxide storage tank for the generator purge system. Also stored in the Administration Building are DOT approved cyrogenic containers of Argon and Nitrogen. The containers are equipped with DOT required and approved pressure relief valves. The containers are installed per Station requirements. The gases are non-flammable and are used by Chemistry and Health Physics.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 46 \\
\hline
\end{tabular}

Many of the different gases being utilized within the administration and service building are stored outdoors located within a roofed over storage area south of the administration and service building (See Table 1 for the gases being used).
Seabrook Station requires the installation of several DOT approved compressed gas cylinders inside structure housing safety-related equipment. These DOT cylinders are seismically mounted and/or restrained in seismic buildings and restrained in bottle racks in non-seismic buildings. The DOT cylinders are fitted with an approved safety device to allow gas to escape, preventing an explosion, of the normally charged cylinders if they are exposed to a fire.

The following is a description of the general location and purpose of the DOT cylinder installations:
(A) West Feedwater Pipe Chase - nitrogen cylinder(s) are installed at elevation \(3^{\prime}-0\) ', to provide a backup safety-grade supply of control "air" for the atmospheric steam dump valves (MS-PV-3001 and MS-PV-3004).
(B) Personnel Hatch Area - nitrogen cylinder(s) are installed at elevation \(21^{\prime}-0\) ", to provide a refill supply of control "air" for the West Chase Feedwater and Main Steam Isolation valves.
(C) East Feedwater Pipe Chase - nitrogen cylinder(s) are installed at elevation \(3^{\prime}-0\) ", to provide a backup safety-grade supply of control "air" for the atmospheric steam dump valves (MS-PV-3002 and MS-PV-3003).
(D) Primary Auxiliary Building - nitrogen cylinder(s) are installed at elevation \(25^{\prime}-0\) ', to provide a safety-grade backup "air" supply for each Train of primary component cooling water temperature control valves (CC-TV-2171-1,2 and CC-TV-2271-1).
(E) Diesel Generator Building - nitrogen cylinder(s) are installed in each stairwell, elevation \(21^{\prime}-6\) ", to provide an "air" supply for the preaction sprinkler system, installed over the diesel generators.
(F) Primary Auxiliary Building Sample Room - Argon cylinder(s) are installed in the Sample Room for an inert gas supply for the Flush Tank (SS-TK-197). Nitrogen Cylinders are installed for purging the hydrogen sensor.
(G) Hydrogen Analyzer Room - Oxygen cylinder(s) are installed in the room to provide reagent gas for the analyzers.
(H) Turbine Building - Carbon dioxide and hydrogen cylinders are installed at the generator pedestal, elevation \(21^{\prime}-6\) ", to provide a backup supply of gases for the generator hydrogen and purge systems.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 47 \\
\hline
\end{tabular}
(I) Turbine Building - Air cylinder(s) are installed in the vicinity of the generator pedestal, elevation \(21^{\prime}-6\) ", to provide a backup supply of air, during maintenance to the generator breaker air receivers.
(J) Turbine Building - Nitrogen cylinder(s) are located on the northwest side of the Generator Stator (GSC) Coolant Tank, elevation \(21^{\prime}-0^{\prime \prime}\) to provide a supply of purge gas for calibration of the coolant tank vent hydrogen monitor.
(K) Turbine Building - Oxygen cylinder(s) are located on the northeast side of the Generator Stator (GSC) Coolant Tank, elevation \(21^{\prime}-0\) " to provide a supply of oxygen for maintaining an oxygen saturated environment within the GSC cooling water.
(L) Fuel Storage Building - Nitrogen cylinder(s) are located on the south side of the spent fuel pool near the spent fuel pool heat exchangers, to provide a supply of Nitrogen for tools and accessories used on the Spent Fuel Bridge Crane.
(M) 345 kV Switchyard Equipment Enclosure and Overhead Crane Structure - \(\mathrm{SF}_{6}\) Gas Cylinders are located in the southwest corner of the enclosure at elevation 55' - \(11 / 4\) " to provide a supply of gas for the Gas Insulated Substation equipment located in the 345 kV Switchyard.

\section*{Table 1}
\begin{tabular}{lccc}
\multicolumn{1}{c}{ Gas } & \begin{tabular}{c} 
Cylinder \\
Volume \(\left(\mathrm{Ft}^{3}\right)^{*}\)
\end{tabular} & \begin{tabular}{c} 
Storage \\
Condition \((\mathrm{psi})\)
\end{tabular} & \begin{tabular}{c} 
Number of \\
Cylinders
\end{tabular} \\
Acetylene & 300 & 250 & 2 \\
Argon & 331 & 2400 & 9 \\
Argon/Methane & 240 & 2200 & 10 \\
Helium & 291 & 2400 & 6 \\
Nitrogen & 301 & 2400 & 12 \\
Propane & \(172^{* *}\) & 516 & 3
\end{tabular}
* At \(70{ }^{\circ} \mathrm{F}, 14.7 \mathrm{psi}\)
** 20-pound cylinders
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
Page 48 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 17 D. 2 (c) \\ Use of Plastic Materials}

The use of plastic materials should be minimized. In particular, halogenated plastics such as polyvinyl chloride (PVC) and neoprene should be used only when substitute non-combustible materials are not available. All plastic materials, including flame and fire retardant materials, will burn with an intensity and BTU production in a range similar to that of ordinary hydrocarbons. When burning, they produce heavy smoke that obscures visibility and can plug air filters, especially charcoal and HEPA. The halogenated plastics also release free chlorine and hydrogen chloride when burning which are toxic to humans and corrosive to equipment.

\section*{Response}

Usage of plastic materials (except that employed as insulating materials on electric cabling, see Section D.3.(g)) is as follows:

The use of plastic materials, especially PVC and neoprene, has been minimized. In electrical specifications, all materials are required to be self-extinguishing and non-propagating when exposed to fire and flames, to the extent practical.

Fiberglass-reinforced plastic (FRP) floating covers are used in the boric acid, recovery test and reactor makeup water tanks. The FRP skin on the polyurethane foam core has a flame spread rating of 100 which is equivalent to that of redwood. In normal operation the tanks will be at least partially filled with water and the covers will be in full contact with water. The probability of initiating combustion in the cover under this condition and having the combustion spread is extremely low.

Fiberglass-reinforced plastic is used for the chemical drain, chemical drain treatment, and seal water supply tanks. Each tank is located in a separate cubicle. In the highly unlikely event of combustion igniting the tank, the flame would be extinguished at the tank water level.
Plastic spent fuel pool and reactor cavity skimmers are partially immersed in water and, therefore, not a fire hazard.

Batteries in the four battery rooms of the Control Building, one battery room in the Turbine Building and two battery rooms in the Relay Room are fabricated with plastic. The containers will contain the electrolyte solution.

Fibercast Factory Manual (FM) approved pipe and fittings are being used in the fire protection underground piping system. This use of Fiberglass-reinforced pipe does not create an unacceptable fire hazard.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 49 \\
\hline
\end{tabular}

PVC piping and polyethylene containers are used in the Fire Pump House as part of the chlorine addition system for the Fire Protection Water Storage Tanks. These materials are used because the Sodium Hypochlorite is not compatible with carbon steel equipment. This material is being installed in a sprinkler area. Therefore, it does not create an unacceptable fire hazard.
Fiberglass-reinforced plastic (FRP) piping is used in the Air Removal System from the Waterbox Priming Drop Out Tank to the Priming pumps to eliminate the corrosion experienced with carbon steel equipment. This piping is only installed in sprinkler areas of the Turbine Building. Therefore, it does not create a unacceptable fire hazard.

Polyethylene (plastic) high integrity containers (HIC) in steel overpacks are used to hold spent resins in the drum storage area of the Waster Processing building. Because the HICs are contained in the steel overpacks, the HICs are not a fire hazard and will not add to the combustible loading of the building.

Vendor-supplied Leased Makeup Water Treatment System piping and conduit is plastic. The room has sprinklers and is cut off from the Administration Building by CMU block walls. The installation is therefore acceptable.

The Waste Processing Building air filters 1-WAH-F-11 and 1-WAH-F-170 contain filter cores that are three-inch, schedule 40, PVC. The PVC cores may be installed on the filter supply and take-up reels if metal filter cores are not available. A filter fire would not adversely affect the ability to achieve and maintain shutdown in the event of a fire. It is preferable to install non-PVC roll filter cores in these filters.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

17 D. 2 (d)

\section*{Storage of Flammable Liquids}

Storage of flammable liquids should as a minimum, comply with the requirements of NFPA 30, "Flammable and Combustible Liquids Code".

\section*{Response}

Storage of flammable liquids complies with the requirements of NFPA 30, "Flammable and Combustible Liquids Code" in the design and venting of tanks.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 50 \\
\hline
\end{tabular}

APCSB 9.5-1, App. A
Page Paragraph
18 D. 3 (a)

\section*{Electric Cable Construction, Cable Trays and Cable Penetrations}

\section*{Cable Tray Construction}

Only non-combustible materials should be used for cable tray construction.

\section*{Response}

All cable trays are of unpainted galvanized steel construction except for cable trays used in the 345 kV switchyard enclosure area which are of unpainted aluminum construction.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

18 D.3(b)

\section*{Cable Spreading Rooms}

See Section F. 3 for fire protection guidelines for cable spreading rooms.
Response
See response to APCSB 9.5-1, Appendix A, Section F. 3 on cable spreading room.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 51 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1; App. A \\ Page Paragraph \\ 18 D. 3 (c) \\ Cable Trays Outside Cable Spreading Rooms}

Automatic water sprinkler systems should be provided for cable trays outside the cable spreading room. Cables should be designed to allow wetting down with deluge water without electrical faulting. Manual hose stations and portable hand extinguishers should be provided as backup. Safety related equipment in the vicinity of such cable trays, that does not itself require water fire protection, but is subject to unacceptable damage from sprinkler water discharge, should be protected from sprinkler system operation or malfunction.

\section*{Response}

Water based fire protection systems are provided for cable trays except for trays containing only instrumentation cables, in the cable spreading room, cable chases, electrical tunnels, penetration areas outside of containment and elevation \(25^{\prime}-0^{\prime \prime}\) of the primary auxiliary building. Manual hose stations and portable extinguishers are provided as backup in these areas and all other areas. However, automatic water sprinkler systems are not provided in other areas for the reasons stated below.

The cables to be used will be self extinguishing, non-propagating and, as a minimum, will pass the IEEE-383-1974 flame test. Control and instrumentation cables cannot ignite from overloading or grounds since the maximum fault is insufficient to heat the insulation to the flash point. Power cables can carry sufficient fault current to reach the flash point of the cable insulation; however, protective relaying on the switchgear circuits will respond to fault currents and open the circuit before enough heating has occurred to damage the cable insulation and start a fire. For additional protection, interlocked armored cable will be used for all 15 kV cables and those 5 kV cables which are routed in trays except cables for the Supplemental Emergency Power System (SEPS). Cables for the SEPS are triplex cables routed in solid bottom trays with solid covers. The redundant safety divisions are separated in accordance with Attachment "C" of AEC letter dated 12/14/73 "Physical Independence of Electric Systems and the fire hazard analysis has assured that both divisions can not be incapacitated by a single fire.

Cables are designed for wet and dry locations without electrical faulting.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 18 D. 3 (d)}

\section*{Cable and Cable Tray Penetration of Fire Barriers}

Cable and cable tray penetration of fire barriers (vertical and horizontal) should be sealed to give protection at least equivalent to that fire barrier. The design of fire barriers for horizontal and vertical cable trays should, minimum meet the requirements of ASTM E-119, "Fire Test of Building Construction and Materials", including the hose stream test.

\section*{Response}

Penetrations of fire barriers by cable and cable trays are sealed with materials providing a fire resistance rating at least equal to that designated for the fire barrier. The fire seals, as a minimum, meet the requirements of ASTM E-119, "Fire Test of Building Construction and Materials".

\section*{APCSB 9.5-1, App. A}

Page Paragraph
18 D. 3 (e)

\section*{Fire Breaks}

Fire breaks should be provided as deemed necessary by the fire hazards analysis. Flame or flame retardant coatings may be used as a fire break for grouped electrical cables to limit spread of fire in cable ventings. (Possible cable derating owing to use of such coating materials must be considered during design.)

\section*{Response}

Fire breaks are not provided in horizontal tray runs between the fire barriers, based on fire hazard analysis.

Fire stop locations in vertical cable tray runs were selected on the bases of limiting materially 1) the spread of fire via a vertical cable tray and 2) the resultant damage due to a fire in a vertical cable tray run.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
Page 53
\end{tabular} \\
\hline
\end{tabular}

The following guidelines were employed:
a) Horizontal offsets \(>1\) foot were considered to end vertical cable tray runs.
b) Fire stops were not installed where cable tray fire suppression was present regardless of length of vertical run.
c) In vertical cable tray runs \(>25\) feet, fire stops were placed to limit the spread of fire to not more than 35 feet. In fact more than two thirds of the vertical runs between fire stops are approximately 25 feet or less. The remaining vertical runs between fire stops vary from about 28 feet to about 35 feet. Where practical in vertical cable tray runs greater than 25 feet, fire stop locations were adjusted to floor elevations.

\section*{APCSB 9.5-1, App. A}

Page Paragraph
19 D. 3 (f)

\section*{Flame Test of Electric Cables}

Electric cable constructions should as a minimum pass the current IEEE No. 383 flame test. (This does not imply that cables passing this test will not require additional fire protection.)

\section*{Response}

The majority of the control cable construction used is at a minimum qualified to the IEEE-383 (1974) flame test. Non-IEEE 383 control cable and wiring is used in some locations and is considered to be insignificant. Examples of non-IEEE 383 cable and wiring uses include vendor supplied wiring under the computer room floor; detector cable for Lubricating Oil and Turbine Bearing running above elevation 75' of the Turbine Building; Excore Neutron Monitoring Cable Assemblies; various telephone wiring; and wiring within some pre-wired cabinets, such as the Main Plant Computer System Cabinets in the Computer Room.

Power cable is qualified to the IEEE-383 (1974) flame test.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 54 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 19 D. 3 (g) \\ Corrosive Gases from Cables}

To the extent practical, cable construction that does not give off corrosive gases while burning should be used.

\section*{Response}

There is no objective standard corrosion test available. From the presently available tests, results are subject to individual judgement and are not repeatable. Available copper mirror test date was reviewed prior to award of the cable order.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

19 D. 3 (h)

\section*{Content of Cable Trays, Raceways, Conduit, Trenches and Culverts}

Cable trays, raceways, conduit, trenches, or culverts should be used only for cables. Miscellaneous storage should not be permitted, nor should piping for flammable or combustible liquids or gases be installed in these areas.

\section*{Response}

Electrical cable trays, raceways, conduit, or trenches are normally used exclusively for cables. No piping for flammable or combustible liquids or gases are installed in these areas. The introduction of combustible materials into these areas are reviewed by Engineering and administratively controlled to ensure that safety related systems will not be impacted. The use of combustible materials has been minimized to the extent practical. The use of combustible materials in these areas is as follows:

Nylon 11 tubing (Imperial Eastman Nylo-Seal) has been installed in conduits and junction boxes with cables which service non-safety related plant equipment. This tubing supports the Chemical Analysis System Hydrogen detection sensors which monitor the Excess Letdown Hx and Letdown Hx compartments, and the Valve Room in containment for Hydrogen concentrations below \(50 \%\) of the lowest explosive limit. Since the tubing is routed in conduit which does not service equipment required for accident mitigation or post accident monitoring, the probability of initiating combustion and having the combustion impact a safety system is extremely low.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

19 D. 3 (i)

\section*{Smoke Venting of Cable Tunnels, Culverts and Spreading Rooms}

The design of cable tunnels, culverts and spreading rooms should provide for automatic or manual smoke venting as required to facilitate manual fire fighting capability.

\section*{Response}

Manual smoke venting is provided in the cable spreading rooms and cable tunnels, but not for the containment electrical penetration area. The present ventilation system in this penetration area consists of recirculation air cooling units which have no exhaust capability. Portable fans will be used by the fire brigade for smoke removal if necessary.

The design of cable tunnels and spreading room provides for manual smoke venting, as required to facilitate manual fire fighting capability.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

19 D. 3 (j)

\section*{Control Room Cables}

Cables in the control room should be kept to the minimum necessary for operation of the control room. All cables entering the control room should terminate there. Cable should not be installed in floor trenches or culverts in the control room.

\section*{Response}

The control room is not used as a raceway for cables between other rooms or buildings. Cables entering the control room are terminated there. Cables routed to the control room are the minimum necessary for operation of the units.

A floor trench, less than one square foot in cross section, connects the computer room to the control room and leads to a trench under the main control board. It accommodates low voltage signal cables.

A second floor trench, less than one square foot in cross section, connects the computer room to the control room and leads to auxiliary control consoles in the control room. It accommodates low voltage signal cables. Both of the above trenches between the computer room and the control room total less than one square foot in cross sectional area.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 56 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
20 D. 4 (a)

\section*{Ventilation}

\section*{Discharge of Products of Combustion}

The products of combustion that need to be removed from a specific fire area should be evaluated to determine how they will be controlled. Smoke and corrosive gases should generally be automatically discharged directly outside to a safe location. Smoke and gases containing radioactive materials should be monitored in the fire area to determine if release to the environment is within the permissible limits of the plant technical specifications.

\section*{Response}

The products of combustion that need to be removed from a specific fire area have been evaluated as part of our fire hazard analysis.

All fire areas are exhausted through the normal plant ventilation system, if available and practical, in the event of a fire. Portable exhausters are available to remove smoke and corrosive gases from fire areas in case of closure of ventilation fire dampers. The exhausts from the radioactive areas are monitored by permanently installed radiation instrumentation. High radiation is alarmed in the control room. Additionally, portable radiation instrumentation can be used if necessary. Should the products of combustion contain radioactivity above the permissible limits of the plant technical specifications, the exhaust of the products of combustion will be terminated until adequate cleanup can be conducted.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 57 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
20 D. 4 (b)

\section*{Evaluation of Inadvertent Operation or Single Failures}

Any ventilation system designed to exhaust smoke or corrosive gases should be evaluated to ensure that inadvertent operation or single failures will not violate the controlled areas of the plant design. This requirement includes containment functions for protection of the public and maintaining habitability of operations personnel.

\section*{Response}

There is no ventilation system designed specifically to exhaust smoke or corrosive gases; normal ventilation is designed so there is no possibility for an inadvertent operation or single failure to violate the plant controlled areas.

The plant ventilation system is designed to ensure containment capability during a single failure or inadvertent operation without violating the controlled areas or endangering the public or operating personnel.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 58 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 20 D. 4 (c)}

\section*{Power Supply and Controls}

The power supply and controls for mechanical ventilation systems should be run outside the fire area served by the system.

\section*{Response}

All mechanical ventilation equipment is located in mechanical equipment rooms. The power supply and controls for the mechanical ventilation systems are generally run outside the fire area served by the system, with the following exceptions:

The power supply and controls of the ventilation system for the A Train switchgear room is supplied from a motor control center in that room. A similar system fed from a B Train motor control center ventilates the B Train switchgear room. The control cables are routed in separated paths through the cable spreading room.

Ventilation of the cable spreading room is controlled by cables passing through the cable spreading room, but its power feed is routed outside the spreading room. The control cables for the cable spreading room ventilation fans are run through the cable spreading room since it is not feasible to bring the control cables into the main control room except via the cable spreading room.

It is necessary to locate the power supply to each 4 kV switchgear room ventilation fan in its switchgear area because it is not feasible to do otherwise. In addition, fire detection and manual fire protection are provided in the areas.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
20 D. 4 (d)

\section*{Protection of Charcoal Filters}

Fire suppression systems should be installed to protect charcoal filters in accordance with Regulatory Guide 1.52, "Design Testing and Maintenance Criteria for Atmospheric Clean-Up Air Filtration".

\section*{Response}

Charcoal filters provided for this project are not equipped with fire suppression systems. Ref.: SBN-1208, dated October 9, 1986 and SBN-97O, dated March 18, 1986.

Revision Regulatory Guide 1.52, dated July 1976, states that a single failure-proof low flow air bleed system or other cooling mechanisms is acceptable to prevent excessive temperature rise in the charcoal filter bed.

A low flow air bleed system, which meets the requirements of R.G. 1.52, is provided for the following safety-related charcoal filters:
\begin{tabular}{lll} 
Filter No. & \multicolumn{1}{c}{ System } & Low Flow Air Source \\
EAH-F-9 \& & Containment Enclosure Emergency & By-Pass Air from Redundant \\
EAH-E-69 & Exhaust (Redundant Filter and Fans) & Fan \\
FAH-F-41 \& & \begin{tabular}{l} 
Fuel Storage Building Exhaust Unit \\
(Redundant Filter and Fans)
\end{tabular} & \begin{tabular}{l} 
By-Pass Air from Redundant \\
FAH-F-74
\end{tabular} \\
CBA-F-38 \& & Control Room Emergency Clean Up Unit & By-Pass Air from Redundant \\
CBA-F-8038 & (Redundant Filter and Fans) & Fan
\end{tabular}

The following non-safety-related charcoal filters do not meet the guidelines of R.G. 1.52. However, per Reference SBN-970, Deviation No. 13 and SBN-1208, no fire would result from loss of air flow across these charcoal filters.
\begin{tabular}{ll} 
Filter No. & \multicolumn{1}{c}{\(\underline{\text { System }}\)} \\
CAH-F-8 & Containment Recirculation Unit \\
PAH-F-16 & PAB Nominal Exhaust Unit \\
CAP-F-40 & Containment On-Line Purge Unit
\end{tabular}

All the charcoal filters, both safety and non-safety, are provided with temperature alarms and carbon monoxide alarms in the Control Room.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 60 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 20 D. 4 (e)}

\section*{Fresh Air Supply Intakes}

The fresh air supply intakes to areas containing safety related equipment or systems should be located remote from the exhaust air outlets and smoke vents of other fire areas to minimize the possibility of contaminating the intake air with the products of combustion.

\section*{Response}

All buildings satisfy the above requirements. In addition, the fresh air intakes for the control room which provide air for ventilation and pressurization are obtained from two locations remote from exhaust air outlets and smoke vents of other fire areas. These are the only sources of supply air to the control room.

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{21 \\ D. 4 (f)}

\section*{Stairwells}

Stairwells should be designed to minimize smoke infiltration during a fire. Staircases should serve as escape routes and access routes for fire fighting. Fire exit routes should be clearly marked. Stairwells, elevators and chutes should be enclosed in masonry towers with minimum fire rating of three hours and automatic fire doors at least equal to the enclosure construction, at each opening into the building. Elevators should not be used during fire emergencies.

\section*{Response}

Stairwells are designed to minimize smoke infiltration during a fire, and to serve as escape and access routes in the event of a fire. Fire exits are clearly marked and established by pre-fire plan. Stairways, designated as fire access or egress routes, except in the primary containment structure, are enclosed with fire barriers having a designated fire resistance rating of at least three hours ( 2 hours for the Administration Building), and have approved automatic fire door assemblies rated at a minimum of one and one-half hours.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 61 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
21 D.4(g)

\section*{Smoke and Heat Vents}

Smoke and heat vents may be useful in specific areas such as cable spreading rooms and diesel fuel oil storage areas and switchgear rooms. When natural-convection ventilation is used, a minimum ratio of 1 square foot of venting area per 200 square feet of floor area should be provided. If forced-convection ventilation is used, 300 CFM should be provided for every 200 square feet of floor area. See NFPA No. 204 for additional guidance on smoke control.

\section*{Response}

Smoke and heat vents have generally not been used since the normal ventilation system for potentially affected area can be manually controlled and can be used for smoke and heat venting, unless the fire damper in the fire wall closes due to excessive heat. Portable exhausters are available to remove smoke and heat upon closure of the ventilation fire dampers.

The normal ventilation exhaust system for the cable spreading room and switchgear rooms can be utilized for smoke and heat relief. The cable spreading room and each switchgear room is supplied air from its own supply fan, and air is exhausted from each area by its own exhaust fan. Ventilation air can be drawn into the cable spreading room or switchgear rooms by opening doors. Air would be exhausted through the affected room exhaust system.

The supply air system will be manually shut down if smoke or radiation is detected in the supply plenum of the PAB.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 62 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 21 D. 4 (h) \\ Self-Contained Breathing Apparatus}

Self-contained breathing apparatus, using full face positive pressure masks, approved by NIOSH (National Institute for Occupational Safety and Health -approval formerly given by the U.S. Bureau of Mines) should be provided for fire brigade, damage control and control room personnel. Control room personnel may be furnished breathing air by a manifold system piped from a storage reservoir if practical. Service or operating life should be a minimum of one half hour for the self-contained units.

At least two extra air bottles should be located on-site for each self-contained breathing unit. In addition, an on-site six hour supply of reserve air should be provided and arranged to permit quick and complete replenishment of exhausted supply air bottles as they are returned. If compressors are used as a source of breathing air, only units approved for breathing air should be used. Special care must be taken to locate the compressor in areas free of dust and containments.

\section*{Response}

Self-contained breathing apparatus using full face positive pressure masks and approved by NIOSH have been provided for fire fighting, damage control and control room personnel. These units have a minimum operating life of one-half hour and have been distributed in the control room and the fire brigade lockers. At least two extra air bottles for these units, each with a minimum operating life of one-half hour, are located on-site. The plant also has a respiratory air compressor for recharging the air bottles on-site. The air compressor is located in an area free of dust and contaminants.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
Page 63
\end{tabular} \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
22 D.4(i)

\section*{Total Flooding Gas Extinguishing Systems}

Where total flooding gas extinguishing systems are used, area intake and exhaust ventilation dampers should close upon initiation of gas flow to maintain necessary gas concentration. (See NFPA 12, "Carbon Dioxide System" and 12A, Halon 1301 Systems).

\section*{Response}

Areas having Halon 1301 gas extinguishing systems are provided with automatic damper closures in the supply and exhaust ducts, initiated from the Halon control panel upon actuation of the system in conformance to NFPA-12A.

APCSB 9.5-1, App. A

\section*{Page Paragraph}

22 D. 5

\section*{Lighting and Communication}

Lighting and two way voice communication are vital to safe shutdown and emergency response in the event of fire. Suitable fixed and portable emergency lighting and communication devices should be provided to satisfy the following requirements:
(a) Fixed emergency lighting should consist of sealed beam units with individual 8-hour minimum battery power supplies.
(b) Suitable sealed beam battery powered portable hand lights should be provided for emergency use.
(c) Fixed emergency communication should use voice powered head sets at pre-selected stations.
(d) Fixed repeaters installed to permit use of portable radio communication units should be protected from exposure fire damage.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & \\
\hline
\end{tabular}

\section*{Response}
(a) The following tabulation identifies lighting systems available at each area required to be manned for safe shutdown of the reactor.
\begin{tabular}{|c|c|c|c|}
\hline Area & Normal Lighting & \(\underline{\underline{\text { Essential }}}\) & Emergency Lighting \\
\hline 1. Control Room & Yes & Train A \& B & Diesel Generator powered fluorescent fixtures (Train A \& B) per deviation request transmittal by letter SBN-932 Battery Packs (8 hour) \\
\hline 2. Train A Switchgear Room & Yes & Train A \& B & Diesel Generator powered fluorescent fixtures (Train B) per deviation request transmitted by letter SBN-932 Battery Packs (8 hour) \\
\hline 3. Train B Switchgear Room & Yes & Train A \& B & Diesel Generator powered fluorescent fixtures (Train B) per deviation request transmitted by letter SBN-932 Battery Packs (8 hour) \\
\hline 4. Diesel Generator Room A & Yes & Train A \& B & Battery Packs (8 hours) \\
\hline 5. Diesel Generator Room B & Yes & Train A \& B & Battery Packs (8 hours) \\
\hline 6. PAB Boric Acid Tank Room & Yes & Train B & Battery Packs (8 hours) \\
\hline 7. PAB Charging Pump Rm. CS-P-2A & Yes & Train B & Battery Packs (8 hours) \\
\hline 8. PAB Charging Pump Rm. CS-P-2B & Yes & Train B & Battery Packs (8 hours) \\
\hline 9. PAB DG Heat Exchanger Area - Valve SW-V-17 & Yes & Train B & Battery Packs (8 hours) \\
\hline 10. Mechanical & Yes & Train B & Battery Packs (8 hours) \\
\hline 11. Turbine Bldg. Main Fl. Valves SCC-V138 and SCC-V139 & Yes & Train A & Battery Packs (8 hours) \\
\hline 12. Condensate Storage Tank NW Valve Room & Yes & None & Battery Packs (8 hours) \\
\hline 13. Non-Essential & Yes & Train A & Battery Packs (8 hours) \\
\hline 14. Control Rm. HVAC Equip. Rm. & Yes & None & Battery Packs (8 hours) \\
\hline
\end{tabular}
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
Page 65
\end{tabular} \\
\hline
\end{tabular}

In compliance with 10CFR Part 50, Appendix R, Section III-J, all the above areas are also provided with eight-hour-rated self-contained battery packs with sealed beam units for access and egress lighting. All other plant areas are provided with \(11 / 2\) hour rated self-contained battery packs with sealed beam units for egress lighting.

The extent of the compliance to above requirements refer to Deviation No. 10, SBN-932, dated March 18, 1986.
(b) Fire brigade and operation personnel required to achieve safe plant shutdown have been provided with suitable battery-powered, portable hand lights.
(c) For those events which require Control Room evacuation, we have identified the following areas as requiring manning to achieve and maintain cold shutdown.

\section*{Switchgear Rooms A and B \\ Diesel Generator Control Panels A and B}

In addition, there are other areas (e.g., Boric Acid Tank Room) where one time actions (e.g., valve operation) may be necessary.

The remote shutdown locations identified above share a dedicated sound powered telephone channel (headphones are provided as necessary to assure effective communications). Each location also has access to a dedicated paging station. There is also an extension from the station telephone system near each location.
(d) The station trunked radio system is designed to provide communications between all areas of the station via hand-held portable radios. The radio system would provide communication to those areas noted in (c) as requiring one time actions.

The trunked radio system equipment (trunking controller, repeaters, and RF mixing rack) is powered from Unit 1 non-safety power system. Back-up power is provided by the Train A emergency diesel generator and a dedicated battery rated for 2-hour use.

Portable units are powered by rechargeable batteries.
The trunked radio system equipment (trunking controller, repeaters, and RF mixing rack) is protected from exposure to possible fire damage.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 66 \\
\hline
\end{tabular}

\section*{E. Fire Detection and Suppression}

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{23 E. 1}

\section*{Fire Detection}
(a) Fire detection systems should as a minimum comply with NFPA 72D, "Standard for the Installation, Maintenance and Use of Proprietary Protective Signaling Systems."
(b) Fire detection systems should give audible and visual alarm and annunciation in the control room. Local audible alarms should also sound at the location of the fire.
(c) Fire alarms should be distinctive and unique. They should not be capable of being confused with any other plant system alarms.
(d) Fire detection and actuation systems should be connected to the plant emergency power supply.

\section*{Response}
(a) The fire detection system will comply with NFPA 72D as follows:

The fire detection system provides in the main control room distinctive displays of either fire or trouble for each fire control panel. Each change in status is recorded on hard copy for record purposes. The record identifies time, date, and occurrence.
Inspection and tests of automatic fire detectors is conducted in accordance with Chapter 8 of NFPA 72E (1987). Due to the lack of combustibles, detectors have not been provided above the suspended ceiling in the control room. Reference Deviation 16, SBN-970, dated March 18, 1986.

The electronic fire detection and alarm system employs a multiplexed reporting system using a multi-conductor data bus to interconnect different fire zones. Circuits have been arranged such that a single break or a single ground fault in the wiring will not result in a false alarm signal.

An open circuit will not prevent transmission on either side of the fault. The system is checked against open circuit by means of periodic maintenance tests.

A ground or a short circuit will be alarmed automatically as a system trouble alarm.
Fire detecting equipment is installed in accordance with Paragraph 2-6 of NFPA 72E, Automatic Fire Detectors.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 67 \\
\hline
\end{tabular}

The circuit arrangement, system equipment and trunk capacities of the multiplexed fire detection system complies with the requirements of Table A of Article 430.
(b) The fire detection system gives an alarm locally at its control panel and an audible and a visual alarm in the main control room. Furthermore, the plant PA system will be utilized to warn personnel for a fire in an area. The trouble signals are similarly annunciated at the same locations.
(c) Fire alarms are distinctive and unique. They are not capable of being confused with any other plant system alarms.
(d) The fire detection alarm panels on Main Control Board are fed by the 120 V A-C uninterruptible power bus. Alarm data loop is powered by the emergency diesel. Power to local detectors and local panels is provided by the 120 V A-C emergency diesel bus where available. Each local panel has built-in battery backup.

APCSB 9.5-1, App. A

\section*{Page Paragraph}

23 E. 2 (a)
Fire Protection Water Supply Systems

\section*{Yard Fire Main Loop}

An underground yard fire main loop should be installed to furnish anticipated fire water requirements. NFPA 24, "Standard for Outside Protection", gives necessary guidance for such installation. It references other design codes and standards developed by such organizations as the American National Standards Institute (ANSI) and the American Water Works Association (AWA). Lined steel or cast iron pipe should be used to reduce internal tuberculation. Such tuberculation deposits in an unlined pipe over a period of years can significantly reduce water flow through the combination of increased friction and reduced pipe diameter. Means for treating and flushing the systems should be provided. Approved visually indicating sectional control valves, such as post indicator valves, should be provided to isolate portions of the main for maintenance or repair without shutting off the entire system.

The fire main system piping should be separate from service or sanitary water system piping.

\section*{Response}

The underground fire main loop was designed to furnish the anticipated fire water requirements using published codes and standards for guidance as enumerated above.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 68 \\
\hline
\end{tabular}

The pipe material is cement-lined welded steel pipe, (except the feed to the General Office Building outside the Protected Area which is plastic pipe and the underground feed to the Mechanical Maintenance Storage Facility, and the RCA Storage Facility which is Fibercast, Factory Mutual (FM) approved, Class 1614 , pipe.) to reduce internal tuberculation, coated and wrapped on the outside with bituminous coal tar paint and paper wrapping.

Water from the town of Seabrook water system is used to fill the fire water tanks. A metering pump automatically injects sodium hypochlorite into the fire water tank fill line as required. Flushing of the entire system will be accomplished by discharging water through selected hydrants.

Sections of the main can be isolated, during periods of maintenance and repair, by closing, approved visually-indicating, sectional post indicator valves. The fire main system piping serves the fire protection system exclusively.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

24 E. 2 (b)

\section*{Multiple Units Fire Protection Water Supply Systems}

A common yard fire main loop may serve multi-unit nuclear power plant sites, if cross-connected between units. Sectional control valves should permit maintaining independence of the individual loop around each unit. For such installations, common water supplies may also be utilized. The water supply should be sized for the largest single expected flow. For multiple reactor sites with widely separated plants (approaching 1 mile or so), separate yard fire main loops should be used.

\section*{Response}

The yard fire main system consists of a single loop with cross-connection between units. Unit 2 construction has been stopped, however some Unit 2 buildings have active water suppression systems installed for property loss conservation. Post indicating valves are provided to allow maintenance of a portion of the loop, if required. The water supply is sized for the largest single expected flow including 500 gpm for manual hose streams. The fire water piping main is supplied from three independent discharge lines, one from each fire pump. These lines feed in two directions to supply water to each half of the looped plant fire main piping.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 69 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 25 E. 2 (c)}

\section*{Fire Pump Installation}

If pumps are required to meet system pressure or flow requirements, a sufficient number of pumps should be provided so that \(100 \%\) capacity will be available with one pump inactive (e.g. three \(50 \%\) pumps or two \(100 \%\) pumps). The connection to the yard fire main loop from each fire pump should be widely separated, preferably located on opposite sides of the plant. Each pump should have its own driver with independent power supplies and control. At least one pump (if not powered from the emergency diesels) should be driven by non-electrical means, preferably diesel engine. Pump and drivers should be located in rooms separated from the remaining pumps and equipment by a minimum three-hour fire wall. Alarms indicating pump running, driver availability, or failure to start should be provided in the control room.

Details of the fire pump installation should as a minimum conform to NFPA 20 "Standard for the Installation of Centrifugal Fire Pumps".

\section*{Response}

The fire protection system has three \(50 \%\) pumps. During a fire, water is supplied by operation of one (1) motor driven pump and one (1) diesel engine-driven pump with the second diesel engine-driven pump functioning as a spare. At all times \(100 \%\) capacity is available with one \(50 \%\) pump inactive.

Fire pump discharge connections to the yard fire main loop are not located on opposite sides of the plant. Each fire pump discharges to an outside manifold with independent sectional valves. The yard fire main loop is supplied in two directions from the outside manifold arranged to discharge to either half of the loop.

Each pump has its own driver with independent power supplies and control. There are 3 hour rated fire barrier walls between each of the three fire pumps. Each of the fire pumps with its controller is in a separate fire area.

Remote indication and alarm is provided in the control room for engine failure to start, low lube oil pressure, high engine jacket water temperature, engine overspeed, A-C power failure and battery failure.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 70 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
25 E. 2 (d)

\section*{Fire Water Supplies}

Two separate reliable water supplies should be provided. If tanks are used, two \(100 \%\) (minimum of 300,000 gallons each) system capacity tanks should be installed. They should be so interconnected that pumps can take suction from either or both. However, a leak in one tank or its piping should not cause both tanks to drain. The main plant fire water supply capacity should be capable of refilling either tank in a minimum of eight hours.

Common tanks are permitted for fire and sanitary or service water storage. When this is done, however, minimum fire water storage requirements should be dedicated by means of a vertical standpipe for other water sources.

\section*{Response}

The water supply for the fire protection system is stored in two 500,000 gallon tanks. 300,000 gallons in each tank is reserved exclusively for fire protection by means of vertical standpipes for other water sources. This standpipe extends up to the 300,000 gallon level in each tank and provides a source of water for non-fire protection service. The Technical Requirement minimum volume of water in each tank is 215,000 gallons.

The suction piping to the three fire pumps is arranged to permit suction from either or both of the two fire water storage tanks.

The manual valves in the suction piping to the fire pumps and in the relief valve header permit isolation of either storage tank.

The plant's fire water supply system is capable of refilling either tank in eight hours to the 300,000 gallon level.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 71 \\
\hline
\end{tabular}

APCSB 9.5-1, App. A
Page Paragraph

\section*{26 E. 2 (e)}

\section*{Fire Water Supply Design Bases}

The fire water supply (total capacity and flow rate) should be calculated on the basis of the largest expected flow rate for a period of two hours, but not less than 300,000 gallons. This flow rate should be based (conservatively) on 1,000 GPM for manual hose streams plus the greater of:
(1) all sprinkler heads opened and flowing in the largest designed fire area; or
(2) the largest open head deluge system(s) operating.

\section*{Response}

The two (2) 500,000 gallon tanks, with 300,000 gallons per tank dedicated for fire protection supply capacity meet the above requirements for hose streams plus the largest demand on a safety related area. Reference Deviation No. 9, SBN 932, dated January 24, 1986. Deviation No. 9 of SBN-932 indicated that the largest demand safety related area was the Diesel Generator Room. Per EC274103, it has since been determined that the largest demand safety related area is the PAB. This does not alter the conclusion of this paragraph or the commitment of this response.

The flow from two fire pumps, each sized to deliver 1,500 GPM at a discharge head of 125 PSI, exceeds the above requirements.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 72 \\
\hline
\end{tabular}

APCSB 9.5-1, App. A
Page Paragraph
26 E. 2 (f)

\section*{Lakes or Ponds as Sources}

Lakes or fresh water ponds of sufficient size may qualify as sole source of water for fire protection, but require at least two intakes to the pump supply. When a common water supply is permitted for fire protection and the ultimate heat sink, the following conditions should also be satisfied.
(1) the additional fire protection water requirements are designed into the total storage capacity; and
(2) failure of the fire protection system should not degrade the function of the ultimate heat sink.

Response
Lakes or fresh water ponds are not utilized as a source of fire protection.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
Page 73 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 27 \\ E. \(2(\mathrm{~g})\)}

\section*{Outside Hose Installations}

Outside manual hose installation should be sufficient to reach any location with an effective hose stream. To accomplish this hydrants should be installed approximately every 250 feet on the yard main system. The lateral to each hydrant from the yard main should be controlled by a visually indicating or key operated (curb) valve. A hose house, equipped with hose and combination nozzle, and other auxiliary equipment recommended in NFPA 24, "Outside Protection," should be provided as needed but at least every 1000 feet.

Threads compatible with those used by local fire departments should be provided on all hydrants, hose couplings and standpipe risers.

\section*{Response}

Factory mutual approved, or UL listed fire hydrants equipped with 6 " inlet and two (2) \(2^{1} / 2\) " hose connections are located throughout the plant site. These hydrants are supplied from the main fire loop through a 6 " branch line with shut-off valve and valve box to grade. The hydrants are so located that no structure is jeopardized by hydrant spacing, due to plant layout, in excess of 250 feet, since they are within 50 feet of any structure. Hose houses are provided at designated hydrant locations.

Each hose house is equipped with 250 feet of \(21 / 2^{\prime \prime}\) woven jacket lined fire hose and other auxiliary equipment recommended in NFPA No. 24, "Outside Protection."

All \(2^{1} / 2\) " and larger threads used on standpipe risers, hose couplings and hydrants are American Standard (National) threads and all \(1 \frac{1}{2 \prime \prime}\) threads are Iron Pipe Thread (IPT). The threads are compatible with equipment used by the local fire department.

There is a wall hydrant with two \(21 / 2\) " hose connections located on the west side of the Mechanical Maintenance Storage Facility.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
Page 74 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 27 \\ E. 3 (a) \\ Water Sprinklers and Hose Standpipe Systems \\ Sprinkler and Standpipe Layout}

Each automatic sprinkler system and manual hose station standpipe should have independent connection to the plant underground water main. Headers fed from each end are permitted inside buildings to supply multiple sprinkler and standpipe systems. When provided, such headers are considered an extension of the yard main system. The header arrangement should be such that no single failure can impair both the primary and backup fire protection systems.

Each sprinkler and standpipe system should be equipped with OS\&Y (outside screw and yoke) gate valve, or other approved shutoff valve, and water flow alarm. Safety related equipment that does not itself require sprinkler water fire protection, but is subject to unacceptable damage if wetted by sprinkler water discharge should be protected by water shields or baffles.

\section*{Response}

All automatic sprinkler systems and manual hose station standpipes located throughout the plant are connected to the plant underground water main. Sufficient isolation valves are provided in the distribution piping to insure flow to both the primary and backup systems. Each of the above systems is equipped with an OS\&Y gate valve.

The sprinkler and hose reels in the Mechanical Maintenance Storage Facility are controlled by a common OS\&Y gate valve. The wall hydrant could provide a supply for backup protection.

The Administration building has a combined sprinkler manual hose station system.
Automatic sprinkler systems and automatic water spray deluge systems alarm and annunciate in the main control room where location of a fire is readily identified. Water flow alarms are not provided in standpipe systems since hose stations must be manned by fire fighting personnel before water flow could signal an alarm. Since fire fighting personnel are already at the site of the fire, an alarm serves no useful purpose.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
Page 75 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
28 E. 3 (b)

\section*{Supervision of Valves}

All valves in the fire water systems should be electrically supervised. The electrical supervision signal should indicate in the control room and other appropriate command locations in the plant (See NFPA 26, "Supervision of Valves").

\section*{Response}

Valves for automatic sprinkler systems and hose standpipe systems are either electrically or administratively supervised.

Post indicator valves in the yard loop show "open" or "shut" and are supervised by the administrative control.

With valves supervised as described above, and with the administrative control supervised by the plant operators, adequate control is provided for fire protection.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

28 E. 3 (c)

\section*{Automatic Sprinkler Systems}

Automatic sprinkler systems should as a minimum conform to requirements of appropriate standards such as NFPA 13, "Standard for the Installation of Sprinkler Systems" and NFPA 15, "Standard for Water Spray Fixed Systems".

\section*{Response}

The automatic sprinkler systems conform to the requirements of NFPA 13, "Standard for the Installation of Sprinkler System" and NFPA 15, "Standard for Water Spray Fixed System".

An exception is face bushings that were installed in the piping. A limited number of face bushings were permitted on condition that they were installed without screwed automatic sprinkler heads. See also Deviations 1 and 6, SBN- 970.

An additional exception is the Administration Building which has a combined sprinkler/manual hose station system.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
Page 76 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 28 E. 3 (d)}

\section*{Fire Protection Water Supply System}

Interior manual hose installation should be able to reach any location with at least one effective hose stream. To accomplish this, standpipes with hose connections, equipped with a maximum 100 feet of \(11 / 2\) inch woven jacket lined fire hose and suitable nozzles should be provided in all buildings, including containment, on all floors and should be spaced at not more than 100 foot intervals. Individual standpipes should be of at least 4 inch diameter for multiple hose connections and \(2 \frac{1}{4}\) inch diameter for single hose connections. These systems should follow the requirements of NFPA 14, "Standpipe and Hose Systems" for sizing, spacing and pipe support requirements.

Hose stations should be located outside entrances to normally unoccupied areas and inside normally occupied areas. Standpipes serving hose stations in areas housing safety related equipment should have shut off valves and pressure reducing devices (if applicable) outside the area.

Provisions should be made to supply water at least to standpipes and hose connections for manual fire fighting in areas within hose reach of equipment required for safe plant shutdown in the event of a safe shutdown earthquake (SSE). The standpipe system serving such hose stations should be analyzed for SSE loading and should be provided with supports to assure system pressure integrity. The piping and valves for the portion of hose standpipe system affected by this functional requirements should at least satisfy ANSI Standard B31.1, "Power Piping". The water supply for this condition may be obtained by manual operator actuation of valve(s) in a connection to the hose standpipe header from a normal Seismic Category I water system such as essential service water system. The cross connection should be:
(a) capable of providing flow to at least two hose stations (approximately 75 GPM/hose station) and,
(b) designed to the same standards as the Seismic Category I water system. It should not degrade the performance of the Seismic Category I water system.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 77 \\
\hline
\end{tabular}

\section*{Response}

Interior manual hose stations are spaced at approximately 100 foot intervals, and will reach any location with an effective hose stream.

Each hose station consists of a \(21 / 2\) " hose connection with \(2 \frac{1}{2 \prime}\) " valve, \(2^{1 / 2 "} \times 1^{1} / 2\) " reducer, 100 feet of \(11 / 2^{\prime \prime}\) (minimum) woven jacket lined fire hose and nozzle. In some cases \(13 / 4^{\prime \prime}\) fire hose with \(1^{1 / 2 "}\) couplings may be used in lieu of \(1^{1 / 2 "}\) hose.

The hose stations are supplied by standpipes with a minimum diameter of 4" (except for those hose stations, in non-safety related buildings, connected to sprinkler systems). Also, a \(2.5{ }^{\prime \prime}\) bypass line with a restricting orifice is included in the 6 " Fire Protection header supplying the Control Building and Diesel Generator Building hose stations to limit flooding in the event of a pipe rupture. The bypass line pipes flow around a normally closed \(6^{\prime \prime}\) butterfly valve. The restricting orifice and bypass line have an inner diameter of less than \(4^{\prime \prime}\), but have been sized to allow the required flow and pressure to the downstream hose stations. If additional flow or pressure is desired, the \(6 "\) valve may be opened.

With the ability to open the 6 " valve and provide a large diameter flow path, the system complies with NFPA 14, "Standpipe and Hose Systems."

Hose stations for normally unoccupied areas are located at the outside entrances and for normally occupied areas at the inside of the entrance, except containment and control room. Hose stations in the containment are located to provide complete coverage of the areas.

The basic fire protection system is designated as an NNS system, and is designed so that failure of the system will not induce failure of any safety-related system or equipment.

Standpipes located in buildings containing safety-related equipment though not safety related are supported in the same manner as a Seismic Category I system, except as noted in the response to paragraph A. 4 of Appendix "A" to BTP 9.5-1. These standpipes are connected through an administratively controlled valve to a safety-related service water system having the capacity to supply 150 gpm flow, which will be available for use following an SSE. The required amount of water flow and pressure in the Seismic Category I standpipe system is assured by a seismically qualified booster pump which is powered from a diesel backed seismically qualified motor control center. If this backup fire protection water supply is placed in service, the 6 " butterfly valve described above is opened to ensure full flow capability to the downstream hose stations.

The safety-related equipment, structure and/or components in the Cooling Tower East Main Steam and Feedwater Pipe Chases, Service Water Pumphouse, Intake and Discharge Structures are protected by hose houses provided at yard fire hydrants located near these structures. Reference Deviation No. 15, SBN 970, dated March 18, 1986.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 78 \\
\hline
\end{tabular}

Hose reels in the Mechanical Maintenance Storage Facility are supplied by the building's sprinkler system. Each hose station consists of a \(1 \frac{1}{2 \prime \prime}\) hose connection and a one hundred foot length of \(11 / 2^{\prime \prime}\) hose.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

30 E. 3 (e)

\section*{Hose Nozzles}

The proper type of hose nozzles to be supplied to each area should be based on the fire hazard analysis. The usual combination spray/straight-stream nozzle may cause unacceptable mechanical damage (for example, the delicate electronic equipment in the control room) and be unsuitable. Electrically safe nozzles should be provided at locations where electrical equipment or cabling is located.

\section*{Response}

Standpipe hose racks or reels are equipped with adjustable spray (fog) nozzles that are Factory Mutual approved and/or Underwriters Laboratory, Inc. listed. Only spray type nozzles have been provided for use on energized electrical equipment and on energized cabling. Solid stream nozzles are not provided for use on energized electrical equipment or cabling.

\section*{APCSB 9.5-1, App. A}

Page Paragraph
30 E. 3 (f)

\section*{Foam Suppression}

Certain fires such as those involving flammable liquids respond well to foam suppression. Consideration should be given to use of any of the available foams for such specialized protection application. These include the more common chemical and mechanical low expansion foams, high expansion foam and the relatively new aqueous film forming foam (AFFF).

\section*{Response}

The design of the fire protection system does not include the use of foam suppression. Tanks and transformers containing flammable liquids that are within or near buildings are protected by automatic deluge systems actuated by thermal detection. Detectors alarm in the main control room.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 79 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

31 E. 4

\section*{Halon Suppression Systems}

The use of Halon fire extinguishing agents should as a minimum comply with the requirements of NFPA 12A and 12B, "Halogenated Fire Extinguishing Agent Systems", Halon 1301 and Halon 1211. Only UL or FM approved agents should be used.

In addition to the guidelines of NFPA 12A and 12B, preventative maintenance and testing of the systems, including check weighing of the Halon cylinders should be done at least quarterly.

Particular consideration should also be given to:
(a) minimum required Halon concentration and soak time
(b) toxicity of Halon
(c) toxicity and corrosive characteristics of thermal decomposition products of Halon.

\section*{Response}

Halon 1301 fixed gas extinguishing systems used in the plant facilities meet the requirements of NFPA 12A and are UL listed or FM approved.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 80 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{31 E. 5}

\section*{Carbon Dioxide Suppression Systems}

The use of carbon dioxide extinguishing systems should as a minimum comply with the requirements of NFPA 12, "Carbon Dioxide Extinguishing Systems".

Particular consideration should also be given to:
(1) minimum required \(\mathrm{CO}_{2}\) concentration and soak time;
(2) toxicity of \(\mathrm{CO}_{2}\)
(3) possibility of secondary thermal shock (cooling) damage;
(4) offsetting requirements for venting during \(\mathrm{CO}_{2}\) injection to prevent over pressurization versus sealing to prevent loss of agent;
(5) design requirements from over pressurization; and
(6) possibility and probability of \(\mathrm{CO}_{2}\) systems being out-of-service because of personnel safety consideration. \(\mathrm{CO}_{2}\) systems are disarmed whenever people are present in an area so protected. Areas entered frequently (even though duration time for any visit is short) have often been found with \(\mathrm{CO}_{2}\) systems shut off.

\section*{Response}

No carbon dioxide suppression systems, except for portable extinguishers, are used in the plant fire protection system.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 81 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
32 E. 6

\section*{Portable Extinguishers}

Fire extinguishers should be provided in accordance with guidelines of NFPA 10 and 10A, "Portable Fire Extinguishers, Maintenance and Use". Dry chemical extinguishers should be installed with due consideration given to clean-up problems after use and possible adverse effects on equipment installed in the area.

\section*{Response}

Portable fire extinguishers are provided in accordance with guidelines of NFPA 10 and 10A, "Portable Fire Extinguishers, Maintenance and Use".

Extinguishers (Halon, \(\mathrm{CO}_{2}\), dry chemical or pressurized water) are selected and installed with consideration given to 1) combustibles in the area, such as paper and wood, liquid fuel and electrical equipment and 2) the avoidance of detrimental effects on equipment installed in the area of possible usage.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 82 \\
\hline
\end{tabular}

\section*{F. Guidelines for Specific Plant Areas}

APCSB 9.5-1, App. A
Page Paragraph
32 F. 1 (a)

\section*{Primary and Secondary Containment - Normal Operation}

Fire protection requirements for the primary and secondary containment areas should be provided on the basis of specific identified hazards. For example:
- Lubricating oil or hydraulic fluid system for the primary coolant pumps.
- Cable tray arrangements and cable penetrations.
- Charcoal filters.

Because of the general inaccessibility of these areas during normal plant operations, protection should be provided by automatic fixed systems. Automatic sprinklers should be installed for those hazards identified as requiring fixed suppression.

Operation of the fire protection systems should not compromise integrity of the containment or the other safety-related systems. Fire protection activities in the containment areas should function in conjunction with total containment requirements such as control of contaminated liquid and gaseous release and ventilation.

Fire detection systems should alarm and annunciate in the control room. The type of detection used and the location of the detectors should be most suitable to the particular type of fire that could be expected from the identified hazard. A primary containment general area fire detection capability should be provided as backup for the above described hazard detection. To accomplish this, suitable smoke detection (e.g., visual obscuration, light scattering and particle counting) should be installed in the air recirculation system ahead of any filters.

Automatic fire suppression capability need not be provided in the primary containment atmospheres that are inserted during normal operation. However, special fire protection requirements during refueling and maintenance operations should be satisfied as provided below.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
Page 83
\end{tabular} \\
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\end{tabular}

\section*{Response}

An automatic water spray deluge system is not provided for the reactor coolant pumps lube oil systems located in the primary containment, since the fire hazard analysis presented in Appendix B of this report demonstrates that a suppression system is not necessary to prevent damage to safety-related systems or components. An automatic pre-action system is provided for the electrical penetration areas of the secondary containment.

The cable tray arrangement inside the primary containment is not provided with fixed suppression or detection systems, since there are no combustibles stored in this area. The cable used is a fire retardant, non-propagating type, meeting the fire test requirements of IEEE-383. Cabling for redundant safety divisions is separated by distance or barrier, as described in response D.1. (c). Fire hose stations and portable fire extinguishers are readily available for use in the unlikely event of a fire.

Each of the reactor coolant pump areas in the containment is provided with high voltage ionization fire detectors.

The primary containment is accessible for manual fire fighting during normal operation.
Control of contaminated liquid and gaseous release is ensured by the primary containment ventilation purge system.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
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\end{tabular} \\
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\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 34 F. 1 (b)}

\section*{Primary and Secondary Containment - Refueling and Maintenance}

Refueling and maintenance operations in containment may introduce additional hazards such as contamination control materials, decontamination supplies, wood planking, temporary wiring, welding and flame cutting (with portable compressed fuel gas supply). Possible fires would not necessarily be in the vicinity of fixed detection and suppression systems.

Management procedures and controls necessary to assure adequate fire protection are discussed in Section 3a.

In addition, manual fire fighting capability should be permanently installed in containment. Standpipes with hose stations, and portable fire extinguishers, should be installed at strategic locations throughout containment for any required manual fire fighting operations.

Adequate self-contained breathing apparatus should be provided near the containment entrances for fire fighting and damage control personnel. These units should be independent of any breathing apparatus or air supply systems provided for general plant activities.

\section*{Response}

The permanent fire detection and suppression systems in the containment are discussed in the response to Section F. 1 (a).

It is realized that refueling and maintenance operations in the containment could introduce additional transient loads, such as decontamination control materials, decontamination supplies and temporary wood staging, as well as introducing additional hazards such as welding and cutting and temporary wiring. Procedures and controls necessary to assure adequate fire protection during this time period have been developed. These are more fully discussed in the response to Section B.3.

Standpipes with hose stations have been permanently installed in the containment for use as required in any fire fighting operations during a refueling or maintenance outage. In addition, portable fire extinguishers are available at strategic locations in the containment.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
Page 85
\end{tabular} \\
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\end{tabular}

\section*{APCSB 9.5-b. App. A \\ Page Paragraph \\ 35 F. 2 \\ Control Room}

The control room is essential to safe reactor operation. It must be protected against disabling fire damage and should be separated from other areas of the plant by floors, walls and roofs having minimum fire resistance ratings of three hours.

Control room cabinets and consoles are subject to damage from two distinct fire hazards:
(a) Fire originating within a cabinet or console; and
(b) Exposure fire involving combustibles in the general room area.

Manual fire fighting capability should be provided for both hazards. Hose stations and portable water and Halon extinguishers should be located in the control room to eliminate the need for operators to leave the control room. An additional hose piping shutoff valve and pressure reducing device should be installed outside the control room. Hose stations adjacent to the control room with portable extinguishers in the control room are acceptable.

Nozzles that are compatible with the hazards and equipment in the control room should be provided for the manual hose station. The nozzles chosen should satisfy actual fire fighting needs, satisfy electrical safety and minimize physical damage to electrical equipment from hose stream impingement.

Fire detection in the control room cabinets and consoles should be provided by smoke and heat detectors in each fire area. Alarm and annunciation should be provided in the control room. Fire alarms in other parts of the plant should also be alarmed and annunciated in the control room.

Breathing apparatus for control room operators should be readily available. Control room floors, ceiling, supporting structures, and walls, including penetrations and doors, should be designed to a minimum fire rating of three hours. All penetration seals should be air tight.

The control room ventilation intake should be provided with smoke detection capability to automatically alarm locally and isolate the control room ventilation system to protect operation by preventing smoke from entering the control room. Manually operated venting of the control room should be available so that operators have the option of venting for visibility. Cables should not be located in concealed floor and ceiling spaces. All cables that enter the control room should terminate in the control room. That is, no cabling should be simply routed through the control room from one area to another.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 86 \\
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\end{tabular}

Safety related equipment should be mounted on pedestals or the control room should have curbs and drains to direct water away from such equipment. Such drains should be provided with means for closing to maintain integrity of the control room in the event of other accidents requiring control room isolation.

\section*{Response}

The control room complex is separated from other areas of the plant by floors and walls having a minimum fire resistance rating of three hours. All penetration seals have a minimum fire resistance rating equal to that designated for the wall and floor they penetrate.

Manual hose stations are located outside the control room. Nozzles were chosen for the hose stations to satisfy actual fire fighting needs, satisfy electrical safety and minimize physical damage to the electrical equipment from hose stream impingement. Portable fire extinguishers are located in the control room. Breathing apparatus is provided for the control room operators.

Fire detection in the control room complex is provided by ionization detectors. Alarm and annunciation is provided in the main control room. Fire detection from other parts of the plant is also alarmed and annunciated at the same location.

The control room ventilation intake is provided with smoke detection capability to automatically alarm and permit isolation of the control room ventilation so as to protect operators by preventing smoke from entering the control room. A recirculation system with charcoal filters has been provided. This system can be started manually by the control room operator from the Main Control Board to remove smoke. Additional venting of the control room could be accomplished by opening the doors.

All cables that enter the control room terminate in the control room. There is no cabling routed through the control room from one area to another.

Metal jacketed lighting cable (Type ALS) is used in the control room ceiling spaces. This cable has an aluminum sheath which is not a combustible material. No other cables are located in ceiling spaces.

Control room electrical equipment is not provided with pedestals, and floor drains are not provided. These features are not required, as hose stations and standpipes are located outside the room and up to 4 inches of flooding can be tolerated without damage to any safety-related equipment. Drainage can be maintained through the open door to the turbine building or the stairwell to the outdoors.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 87 \\
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\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 37 F. 3 \\ Cable Spreading Room}

The primary fire suppression in the cable spreading room should be an automatic water system such as closed head sprinklers, open head deluge, or open directional spray nozzles. Deluge and open spray systems should have provisions for manual operation at a remote station; however, there should be provisions to preclude inadvertent operation. Location of sprinkler heads or spray nozzles should consider cable tray sizing and arrangements to assure adequate water coverage. Cables should be designed to allow wetting down with deluge water without electrical faulting.

Open head deluge and open directional spray systems should be zoned so that a single failure will not deprive the entire area of automatic fire suppression capability.

The use of foam is acceptable, provided it is of a type capable of being delivered by a sprinkler or deluge system, such as an Aqueous Film Forming Foam (AFFF).

An automatic water suppression system with manual hoses and portable extinguisher backup is acceptable, provided:
(a) At least two remote and separate entrances are provided to the room for access by fire brigade personnel; and
(b) Aisle separation provided between tray stacks should be at least three feet wide and eight feet high.

Alternately, gas systems (Halon or \(\mathrm{C}_{2}\) ) may be used for primary fire suppression if they are backed up by an installed water spray system and hose stations and portable extinguishers immediately outside the room and if the access requirements stated above are met.

Electric cable construction should, as a minimum, pass the flame test in IEEE Std 383, "IEEE Standard for Type Test of Class 1E Electric Cables, Field Splices and Connections for Nuclear Power Generating Stations."

Drains to remove fire fighting water should be provided with adequate seals when gas extinguishing systems are also installed.

Redundant safety related cable division should be separated by walls with a three-hour fire rating.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 88 \\
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\end{tabular}

For multiple-reactor unit sites, cable spreading rooms should not be shared between reactors. Each cable spreading room of each unit should have divisional cable separation as stated above and be separated from the other and the rest of the plant by a wall with a minimum fire rating of three hours. (See NFPA 251, "Fire Tests, Building Construction and Materials", or ASTM E-119, "Fire Test of Building Construction and Materials", for fire test resistance rating.)

The ventilation system to the cable spreading room should be designed to isolate the area upon actuation of any gas extinguishing system in the area. In addition, smoke venting of the cable spreading room may be desirable. Such smoke venting systems should be controlled automatically by the fire detection or suppression system as appropriate. Capability for remote manual control should also be provided.

\section*{Response}

The primary fire suppression in the cable spreading room consists of several automatic fixed spray dry pipe deluge systems. Automatic water sprinkler systems are provided for cable trays except for trays containing only instrumentation cables. Instrumentation cables would not ignite from over loading since the maximum fault current is insufficient to heat the insulation to the flash point. Provisions are made to preclude inadvertent operation by having two or more fire detection heads actuate the automatic spray systems. Location of spray nozzles considers cable tray sizing and arrangement to assure adequate water coverage. Cables are specified to allow wetting down with deluge water without electrical faulting.

Spray systems are zoned so that a single failure will not deprive the entire area of automatic fire suppression capability. Manual hoses and portable extinguishers are provided in adjacent areas for back-up use in the cable spreading room. Access to the cable spreading room is provided through two remote and separated entrances. Aisle separation between stacked cable trays meets the three feet wide by eight feet high, except in limited cross-over locations which do not limit personnel access. Electric cable construction, as a minimum, pass the flame test in IEEE Standard 383.

Cabling for redundant safety divisions is separated by distance or barrier as described in Attachment "C" Physical Independence of Electric Systems of AEC letter dated 12/14/73, which is generally in agreement with Regulatory Guide 1.75.

Cable spreading rooms are not shared between reactors. Construction on Unit 2 has been stopped. Unit 1 cable spreading room is designated a "fire area" and is separated from other areas of the plant by a fire barrier having a fire resistance of three hours.

The cable spreading room does not contain high energy equipment such as switchgear, transformer or potential sources of missiles or pipe whip, and is not used for storing flammable materials. Circuits in trays are limited to control and instrument functions. Those power supply circuits serving the control room are routed in embedded conduits. There are no combustible materials other than cable in the cable spreading room and all cables are self-extinguishing and non-propagating; therefore, the fire hazard evaluation shows that a postulated fire will not occur in the cable spreading room.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & \\
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\end{tabular}

Smoke venting of the cable spreading room is available by use of the normal Ventilation system. This system is not controlled automatically by the fire detection or suppression system but by remote manual control. Portable fans can be used for smoke removal upon closure of ventilation fire dampers. Automatic fire detectors provide an alarm at its local control panel and a visual and an audible alarm in the main control room.

Drains are provided to remove fire water from actuation of the deluge system.
See D.3(c) for justification of adequacy of separation without the use of three hour fire rated walls.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{\(39 \quad\) F. 4}

\section*{Plant Computer Room}

Safety related computers should be separated from other areas of the plant by barriers having a minimum three-hour fire resistant rating. Automatic fire detection should be provided to alarm and annunciate in the control room and alarm locally. Manual hose stations and portable water and Halon fire extinguishers should be provided.

\section*{Response}

The plant computer does not perform any safety function, and the total failure of the computer will not prevent the safe and orderly shutdown of the plant. The plant computer room is a portion of the control room complex but is separated from the main control room by three hour fire rated walls. Automatic fire detectors with fixed Halon 1301 system are provided in the computer room to provide an alarm at its local control panel and a visual and an audible alarm in the main control room. Manual hose stations are located outside the control room. Halon hand-held extinguishers are located in the computer room. Portable water extinguishers are not provided.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 90 \\
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\end{tabular}

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

\section*{40 F. 5}

\section*{Switchgear Rooms}

Switchgear rooms should be separated from the remainder of the plant by minimum three-hour rated fire barriers, if practicable. Automatic fire detection should alarm and annunciate in the control room and alarm locally. Fire hose stations and portable extinguishers should be readily available.

Acceptable protection for cables that pass through the switchgear room is automatic water or gas agent suppression. Such automatic suppression must consider preventing unacceptable damage to electrical equipment and possible necessary containment of agent following discharge.

\section*{Response}

Switchgear rooms are separated from the remainder of the plant by minimum three-hour rated fire barriers. Automatic fire detection is alarmed and annunciated in the main control room. Even though switchgear rooms are unoccupied, alarms are provided. Alarm and indication in the main control room readily identify the fire control panel in alarm. Portable extinguishers are provided in the area with hose stations located outside in an adjacent area and yard fire hydrants readily available for use if and when required.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 91 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ \(40 \quad\) F. 6 \\ Remote Safety-Related Panels}

The general area housing remote safety related panels should be provided with automatic fire detectors that alarm locally and alarm and annunciate in the control room. Combustible materials should be controlled and limited to those required for operation. Portable extinguishers and manual hose stations should be provided.

\section*{Response}

The remote safety-related shutdown panels are housed in the control building at floor elevation \(21^{\prime}-6\) ' and in the diesel generator building at floor elevation 2l'-6". (See drawings F-310431 and F-202069.)

Automatic fire detectors are provided in the control building at floor elevation \(21^{\prime}-6\) " and in the diesel generator building at floor elevation \(21^{\prime}-6\) '". These automatic fire detectors provide local indication plus alarm and indication in the main control room. In addition, the diesel generator building at elevation \(21^{\prime}-6^{\prime \prime}\) is protected by a manual preaction sprinkler system.

Combustible materials are minimized in all of the above areas. Portable extinguishers are provided inside these areas, and manual hose stations are provided outside these areas.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 92 \\
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\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{41 \\ F. 7}

\section*{Station Battery Rooms}

Battery rooms should be protected against fire explosions. Battery rooms should be separated from each other and other areas of the plant by barriers having a minimum fire rating of three-hours inclusive of all penetrations and openings. (See NFPA 69, "Standard on Explosion Prevention Systems.") Ventilation systems in the battery rooms should be capable of maintaining the hydrogen concentration well below \(2 \mathrm{vol} . \%\) hydrogen concentration. Standpipe and hose and portable extinguishers should be provided.

Alternatives:
(a) Provide a total fire rated barrier enclosure of the battery room complex that exceeds the fire load contained in the room.
(b) Reduce the fire load to be within the fire barrier capability of \(1 \frac{1}{2}\) hours.
(c) Provide a remote manual actuated sprinkler system in each room and provide the \(1 \frac{1}{2}\) hour fire barrier separation.

\section*{Response}

Battery rooms are separated from each other and other areas of the plant by barriers having a fire rating of 3 hours. The exhaust ventilation system for the battery rooms is capable of maintaining a hydrogen concentration well below \(2 \%\) by volume. The exhaust system is redundant, and powered from independent safety related electrical trains. Each exhaust fan is provided with a flow switch which indicates loss of flow in the control room.

Portable fire extinguishers are located nearby, and a hose station is available within hose reach of the battery rooms.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
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APCSB 9.5-1, App. A
Page Paragraph
41 F. 8

\section*{Turbine Lubrication and Control Oil Storage and Use Areas}

A blank fire wall having a minimum resistance rating of three hours should separate all areas containing safety related systems and equipment from the turbine oil system.

\section*{Response}

The turbine lube oil tank is located adjacent to the exterior wall of the turbine building inside a one (1) foot thick concrete wall enclosure whose fire rating is in excess of three (3) hours. This enclosure is capable of containing the contents of the tank. Although there are no safety related systems located in the vicinity, the fire protection system in this area consists of an automatic deluge suppression system and back-up protection with local hose stations.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
Page 94 \\
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\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 42 F. 9 \\ Diesel Generator Areas}

Diesel generators should be separated from each other and other areas of the plant by fire barriers having a minimum fire resistance rating of three hours.

Automatic fire suppression such as AFFF foam, or sprinklers should be installed to combat any diesel generator or lubricating oil fires. Automatic fire detection should be provided to alarm and annunciate in the control room and alarm locally. Drainage for fire fighting water and means for local manual venting of smoke should be provided. Day tanks with total capacity up to 1,100 gallons are permitted in the diesel generator area under the following conditions:
a. The day tank is located in a separate enclosure, with a minimum fire resistance rating of three hours, including doors or penetrations. These enclosures should be capable of containing the entire contents of the day tanks. The enclosure should be ventilated to avoid accumulation of oil fumes.
b. The enclosure should-be protected by automatic fire suppression systems such as AFFF or sprinklers.

\section*{Response}

Each diesel generator, along with its associated auxiliary equipment, is separated from the adjacent redundant unit by a wall having a fire rating in excess of the designated rating of three hours. Doors in these walls are Class A with a three hour fire rating.

Each fuel oil day tank ( 1500 gallons) is installed in a separate enclosure which is located on the floor above the diesel generator served. This enclosure is designed with walls, floor and ceiling having a fire rating in excess of the designated rating of three hours, and sized to contain the contents of the tank. Doors servicing these enclosures are Class A.

Redundant automatic preaction water systems are provided in each of the two Fuel Oil Storage Tanks areas. Automatic deluge water systems are provided in each of the two fuel oil day tank areas. Automatic preaction water system in fuel oil piping trenches is provided in each of the two engine rooms. Manual preaction water system for area wide coverage is provided in each of the two engine rooms. Drainage is provided to remove fire protection water.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 95 \\
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\end{tabular}

Automatic fire detection has been provided in the fuel oil storage areas and trenches and in the diesel generator area, with an alarm at its local control panel and a visual and an audible alarm in the main control room. Sufficient detection devices are available to detect that a fire exists in the area and alarm. Local fire hydrants are available to extinguish a fire outside the range of the fixed water spray system.

The normal ventilation systems have the capacity to exhaust the area during and after a fire, unless heat from the fire closes the fire damper in the system. A gravity vent system is provided for the diesel fuel oil vapor, but will not provide sufficient air for sustaining combustion should a fire start. This restriction of combustion air is more important than smoke and heat removal from this area.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 96 \\
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\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ \(42 \quad\) F. 10 \\ Diesel Fuel Oil Storage Areas}

Diesel fuel oil tanks with a capacity greater than 1,100 gallons should not be located inside the buildings containing safety related equipment. They should be located at least 50 feet from any building containing safety related equipment, or if located within 50 feet, they should be housed in a separate building with construction having a minimum fire resistance rating of three hours. Buried tanks are considered as meeting the three-hours fire resistance requirements. See NFPA 30, Flammable and Combustible Liquids Code, for additional guidance.

When located in a separate building the tank should be protected by an automatic fire suppression system such as AFFF or sprinklers.

Tanks, unless buried, should not be located directly above or below safety related systems or equipment regardless of the fire rating of separating floors or ceilings.

\section*{Response}

Although the design of the fuel oil storage areas differs from the design Specified above, the results of the fire hazard analysis presented in Appendix A of this report demonstrates the adequacy of the provided construction, even under the most extreme condition of failure of the water spray system. The design provides fire protection comparable to that recommended in the above guidelines.

Each of the SEPS diesel fuel tanks is in excess of 6,000 gallons. The SEPS diesel generators with their fuel tanks are located less than 50 feet from the Cooling Tower that contains safety related equipment. The generator enclosures are not fire rated. However, the south wall of the Cooling Tower, adjacent to the SEPS installation is three-hour fire rated. The construction of this wall would prevent a fire in the non-safety related SEPS diesel generators from adversely affecting the operation of the safety related equipment in the Cooling Tower. This design meets the intent of these guidelines.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & \begin{tabular}{l} 
Section F.3 \\
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\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ \(44 \quad\) F. 11 \\ Safety-Related Pumps}

Pump houses and rooms housing safety-related pumps should be protected by automatic sprinkler protection unless a fire hazards analysis can demonstrate that a fire will not endanger other safety-related equipment required for safe plant shutdown. Early warning fire detection should be installed with alarm and annunciation locally and in the control room. Local hose stations and portable extinguishers should also be provided.

Equipment pedestals or curbs and drains should be provided to remove and direct water away from safety-related equipment.

Provisions should be made for manual control of the ventilation system to facilitate smoke removal if required for manual fire fighting operation.

\section*{Response}

The equipment vault areas and the charging pump areas which house safety related pumps and heat exchangers are each divided into fire areas separated by fire barriers having at least \(1 \frac{1}{2}\) or 3 hour ratings. Each fire area contains only one of two redundant components in a safety related system. The fire hazard analysis demonstrates that any postulated fire in one fire area will not affect safety related equipment in an adjacent fire area. These areas are equipped with portable fire extinguishers and have standpipe hose stations available.

Both of the redundant primary component cooling water pumps are located in one fire area. A metal barrier partition has been placed between the two pumps and a preaction sprinkler system has been provided above the pumps.

Both the motor driven and turbine driven emergency feedwater pumps are located in one fire area. Our fire hazard analysis indicates there are minimal combustibles, other than pump lubricating oil and fiberglass ladders, located in this area. The pumps are separated by 15 feet. Ionization detectors have been provided for early warning of a fire and portable extinguishers and hose station for manual firefighting.

The service water pump and the circulating water pump areas are separated by a \(11 / 2\) hour fire wall. Our fire hazard analysis indicates that combustibles located in these areas consist of pump lubricating oil and fiberglass ladders. Ionization detectors have been provided in the service water pump area and portable extinguishers supplemental by yard hydrants for manual firefighting.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page \\
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\end{tabular}

Normal ventilation equipment can be used to facilitate smoke removal, as it can be manually controlled from the main control room until the fire dampers close.

All safety-related pumps and equipment are supported on curbs or pedestals. Floor drains in these areas will direct all water to either the radioactive liquid waste or non-radioactive liquid waste system, as required.

APCSB 9.5-1, App. A
Page Paragraph
\(44 \quad\) F. 12

\section*{New Fuel Area}

Hand portable extinguishers should be located within this area. Also, local hose stations should be located outside but within hose reach of this area. Automatic fire detection should alarm and annunciate in the control room and alarm locally. Combustibles should be limited to a minimum in the new fuel area. The storage area should be provided with a drainage system to preclude accumulation of water.

The storage configuration of new fuel should always be so maintained as to preclude criticality for any water density that might occur during fire water application.

\section*{Response}

Portable extinguishers are located in the fuel storage building. A local hose station is located outside the area but within hose reach.

There are minimal combustibles in the fuel storage building. A fire detection system has been provided.

Sumps and sump pumps are provided to prevent accumulation of water. New fuel is stored to preclude criticality should unborated water accumulate in this area.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 99 \\
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\end{tabular}

APCSB 9.5-1, App. A
Page Paragraph
\(45 \quad\) F. 13

\section*{Spent Fuel Pool Area}

Protection for the spent fuel pool area should be provided by local hose stations and portable extinguishers. Automatic fire detection should be provided to alarm and annunciate in the control room and to alarm locally.

\section*{Response}

Portable fire extinguishers are provided, and a local hose station is within hose reach of the spent fuel storage area.

There are minimal combustibles in the spent fuel area. A fire detection system has been provided.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 100 \\
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\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ \(45 \quad\) F. 14 \\ Radwaste Building}

The Radwaste Building should be separated from other areas of the plant by fire barriers having at least three-hour ratings. Automatic sprinklers should be used in all areas where combustible materials are located. Automatic fire detection should be provided to annunciate and alarm in the control room and alarm locally. During a fire, the ventilation systems in these areas should be capable of being isolated. Water should drain to liquid radwaste building sumps.

Acceptable alternate fire protection is automatic fire detection to alarm and annunciate in the control room, in addition to manual hose stations and portable extinguishers consisting of hand held and large wheeled units.

\section*{Response}

The radwaste building is separated from other areas of the plant by fire barrier having 3 hour rating. Automatic deluge systems are provided in the extruder/evaporator area, asphalt meter pump room and turn table/drum conveyor area. Ionization type fire detectors are provided in the waste compactor area, decontamination area, extruder/evaporator area (thermal detection also), asphalt meter pump room (thermal detection also), turntable/drum conveyor area (thermal detection also) and waste solidification control room to indicate locally at the control panel and to initiate visual and audible alarm in the main control room. Manual hose stations and portable fire extinguishers are available for use. The ventilation system is capable of being isolated during a fire. All water from the fire suppression systems will drain to the waste processing building sumps.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 101 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph \\ 46 F. 15}

\section*{Decontamination Areas}

The decontamination areas should be protected by automatic sprinklers if flammable liquids are stored. Automatic fire detection should be provided to annunciate and alarm in the control room and alarm locally. The ventilation system should be capable of being isolated. Local hose stations and hand portable extinguishers should be provided as back-up to the sprinkler system.

\section*{Response}

No flammable liquids are stored in the decontamination area nor are other combustibles stored in the decontamination area, therefore no automatic sprinklers are provided. However, smoke detectors have been installed and portable fire extinguishers and hose stations are available. With the aid of early detection, the operator has the capability for shutting down the ventilation system and manually fight an unlikely fire.

\section*{APCSB 9.5-1, App. A}

\section*{Page Paragraph}

46 F. 16

\section*{Safety-Related Water Tanks}

Storage tanks that supply water for safe shutdown should be protected from the effects of fire. Local hose stations and portable extinguishers should be provided. Portable extinguishers should be located in nearby hose houses. Combustible materials should not be stored next to outdoor tanks. A minimum of 50 feet of separation should be provided between outdoor tank and combustible materials where feasible.

\section*{Response}

Combustible materials should not be stored near safe shutdown water storage tanks in such a manner that the operability of the tanks could be compromised by the effects of a fire. Hose reels and/or hydrants and portable extinguishers are provided as fire protection.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 102 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{\(46 \quad\) F. 17}

\section*{Cooling Towers}

Cooling towers should be of non-combustible construction or so located that a fire wall not adversely affect any safety-related systems or equipment. Cooling towers should be of non-combustible construction when the basins are used for the ultimate heat sink or for the fire protection water supply.

\section*{Response}

The service water cooling tower is constructed of non-combustible material. Concrete is used for the superstructure. The fill material is a hard burned clay which is chemically inert, and the mist eliminators are fiberglass.

\section*{APCSB 9.5-1, App. A}

Page Paragraph

\section*{\(47 \quad\) F. 18}

Miscellaneous Areas
Miscellaneous areas such as records storage areas, shops, warehouses, and auxiliary boiler rooms should be so located that a fire or effects of a fire, including smoke, will not adversely affect any safety related systems or equipment. Fuel oil tanks for auxiliary boilers should be buried or provided with dikes to contain the entire tank contents.

\section*{Response}

The record storage, shops, storage room, and auxiliary boiler room within the Administration and Service Building are separated from other buildings by barriers having a three (3) hour fire rating. Due to their remote location relative to safety related systems and equipment, a fire in these areas could not adversely affect any safety related systems or equipment. The fuel oil tank for the auxiliary boilers is provided with a dike to contain its entire contents.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 103 \\
\hline
\end{tabular}

\section*{G. Special Protection Guidelines}

APCSB 9.5-1, App. A
Page Paragraph
47 G. 1

\section*{Welding and Cutting Acetylene - Oxygen Fuel Gas Systems}

This equipment is used in various areas throughout the plant. Storage areas should be chosen to permit fire protection by automatic sprinkler systems. Local hose stations and portable equipment should be provided as backup. The requirements of NFPA 51 and 51B are applicable to these hazards. A permit system should be required to utilize this equipment (also refer to 2 f herein).

\section*{Response}

Flammable welding gas equipment is generally stored in the Administrative Building - Machine Shops, Chlorination - Machine Shop, Circulating Water Pumphouse. Portable extinguishers, hose stations, and/or hydrants with hose houses are provided in these areas. Administrative procedures have been generated for the use of this equipment; hot work permits are required for utilization of this equipment.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 104 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A \\ Page Paragraph}

\section*{47 \\ G. 2}

\section*{Storage Areas for Dry Ion Exchange Resins}

Dry ion exchange resins should not be stored near essential safety related systems. Dry unused resins should be protected by automatic wet pipe sprinkler installations. Detection by smoke and heat detectors should alarm and annunciate in the control room and alarm locally. Local hose stations and portable extinguishers should provide backup for these areas. Storage areas of dry resin should have curbs and drains. (Refer to NFPA 92M, "Waterproofing and Draining of Floors.")

\section*{Response}

Dry ion exchange resin is not stored near essential safety related systems. Long term storage of dry ion exchange resin will be in the service building and/or warehouses. The storeroom in the service building and warehouses are protected by sprinkler systems. Local hose stations and hydrants are provided as backup fire protection. Fire protection flow alarms would indicate fire conditions in the warehouses. Curbs are not provided for these storage areas. Drains are provided.

\section*{APCSB 9.5-1, App. A}

Page Paragraph
\[
48
\]
G. 3

\section*{Hazardous Chemicals}

Hazardous chemicals should be stored and protected in accordance with the recommendations of NFPA 49 "Hazardous Chemicals Data". Chemical storage areas should be well ventilated and protected against flooding conditions since some chemicals may react with water to produce ignition.

\section*{Response}

Chemicals are stored in the chemical storage room and storeroom of the service building and in the warehouses. These areas are well ventilated and protected against flooding conditions. Small quantities of chemicals are also stored for use in the chemical laboratories which are well ventilated and protected against flooding.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 105 \\
\hline
\end{tabular}

\section*{APCSB 9.5-1, App. A}

Page Paragraph
48 G. 4

\section*{Materials Containing Radioactivity}

Materials that collect and contain radioactivity such as spent ion exchange resins, charcoal filters, and HEPA filters should be stored in closed metal tanks or containers that are located in areas free from ignition sources or combustibles. These materials should be protected from exposure to fires in adjacent areas as well. Consideration should be given to requirements for removal of isotopic decay heat from entrained radioactive material.

\section*{Response}

Materials that have collected and contain radioactivity are stored in metal tanks or containers which are located in the waste processing building. The storage area is free from ignition sources and combustibles and is separated from fires in adjacent buildings by a three hour rated fire wall. Decay heat emanating from the containers is removed by the building ventilation system.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 106 \\
\hline
\end{tabular}

\section*{H. Deviations from National Fire Protection Association (NFPA) Code/Underwriter's Laboratory (UL) Listing}

Ref.: -SBN- 970, dated 3/18/86
Section 9.5.1.1 from Seabrook's FSAR states:
The Fire Protection Systems have been designed using the general guidelines of the following codes and standards:
(a) American Nuclear Insurers (ANI) - Specifications for Fire Protection of New Plants.
(b) National Fire Protection Association (NFPA) and ABS Codes as Listed in Table 9S-I.
(c) Uniform Building Code (UBC).

The following are deviations from NFPA:
1. Low Point Drain Valves in Sprinkler Systems:

Most of the low point drain valves, used throughout the sprinkler systems, do not meet NFPA 13, Section 3-14 since they are not UL listed. These drain valves, United Brass Series 125 S Globe Valves, have all the same characteristics as United Brass UL listed valves, except for the flow characteristics. Since these valves are only used as low point drains, the flow characteristics are not of a concern. The use of non-UL listed valves in this application is acceptable.
2. The test flow meter for Fire Pumps 1-FP-P-20A, 20B, and 20C does not meet NFPA 20:

NFPA 20 states that the test flow meter must be capable of up to \(175 \%\) of rated pump capacity. The pumps have a rated capacity of \(1,500 \mathrm{gpm}\). One hundred seventy-five percent ( \(175 \%\) ) of this is \(2,625 \mathrm{gpm}\), but the flow meter is only capable up to \(2,600 \mathrm{gpm}\).

These pumps will only be tested to a maximum \(150 \%\) of their rated capacity which is well within the range of the flow meter. The capacity of the flow meter is also only \(1 \%\) lower than what is required by code.

Because of the above stated reasons, the test flow meter is acceptable.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 107 \\
\hline
\end{tabular}
3. Audible evacuation alarms do not meet NFPA 72A:

NFPA 72A, Section 2-5.4, "Distribution of Evacuation Signals," states that fire alarm systems provided for evacuation of occupants shall have one or more audible alarms on each floor divided by a fire wall. Areas of the plant which are protected by preaction sprinkler systems do not have audible alarms throughout the area for the evacuation of occupants. However, if there is a fire problem, the Control Room will receive an alarm from the area detection and/or the water flow alarm valves on the sprinkler systems. Plant operating personnel and the fire brigade will be immediately dispatched to the area in question.

Because of this reason, lack of the audible alarms within the fire area is acceptable.
The areas which do not have audible alarms throughout the area include the Fuel Oil Day Tank Rooms, the Mechanical Room on El. 51'-6", the Diesel Generator Rooms, and the Fuel Oil Storage Rooms in the Diesel Generator Building, the Turbine Building. El. 25' in the PAB, the electrical tunnels Trains A and B, the cable spreading area in the Control Building, and the extruder/evaporator area, the metering pump area, and the turntable/conveyor belt area in the Waste Process Building.
4. Fire tanks were not built to AWWA Standards as required by NFPA 22, but instead, to API 650:

The requirements for a tank built to American Petroleum Institute Standard 650, for storage of petroleum, are more stringent than the requirements in AWWA Standards for water tanks. The tanks are, therefore, acceptable.
5. HVAC fans do not shut down upon detection of smoke as required by NFPA 90A:

For safety-related ventilation systems, there is a conflict between the nuclear safety-related HVAC System and NFPA 90A. It is necessary to keep the ventilation system operational (depending on area heat loads). This is especially true for a ventilation system serving multiple areas. If a damper in a branch duct for one fire area closes due to fire in its respective fire area, it is necessary to continue operating fans to provide cooling air to other areas served. This design philosophy is also applied to nonsafety-related HVAC Systems at Seabrook.

Seabrook Station relies on area detection for early warning of fire problems. These detectors alarm in the Control Room. Plant operating personnel will take immediate action to determine the magnitude of the fire problem and will, at that time, decide if it is necessary to shut down fans.

For these reasons, not shutting down the fans is an acceptable deviation.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 108 \\
\hline
\end{tabular}
6. Sprinklers for area coverage over the PCCW pumps in the PAB El. 25', do not strictly meet NFPA 13:

Due to severe congestion at the ceiling and the thickness of the beams at the ceiling, several sprinklers over the PCCW pumps could not be located in strict accordance with NFPA 13, Section 4.3.

The ceiling beams, extending down to 42 inches from the ceiling, do not physically allow sprinkler location to meet Table 4-2.4.b in NFPA 13. The sprinklers are, however, placed in the beam pockets to compensate for the obstruction of the spray patterns due to the beams. There are also areas in the PAB in which the ceiling is heavily congested with supplementary steel, supports, and conduits not allowing the sprinklers to meet the maximum distance from the ceiling criteria in NFPA 13. In these cases, the sprinklers were placed in the best location possible to allow for complete coverage of the floor. For the above reasons, the locations of the sprinklers are an acceptable deviation.
7. Fire protection booster pump does not meet NFPA 20:

Per Branch Technical Position APCSB 9.5-1, Appendix A, Position C3(d) - A backup to the normal Fire Protection System was provided for the standpipes servicing safety equipment in the event of a Safe Shutdown Earthquake (SSE). A permanent connection between one train of service water and the Fire Protection System (safety-related area standpipe) is provided with a booster pump to supply the required pressure.

The fire protection booster pump is an Aurora Series 350, stainless steel pump that is not UL listed, nor FM approved. The pump controller is a non-automatic (manual) controller which includes a local on-off push button with status lights. There is a gate valve and a pressure gauge in both the suction and discharge lines to the pump. A relief valve is located at the pump discharge. An orifice plate is located in a test line connecting the suction and discharge of the pump so that pump flow may be tested. A permanent flow meter is not being provided, but there are connections for a portable flow meter.

One requirement in NFPA 20 is that fire pumps shall be listed for fire protection. Even though the FP booster pump is not UL/FM, it has similar characteristics to a UL/FM pump. UL/FM pumps, however, are made from cast iron which cannot be seismically qualified. The FP booster pump is made from stainless steel and, therefore, can be seismically qualified.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 109 \\
\hline
\end{tabular}

NFPA 20 also requires that fire pumps shall have an automatic controller which would start the pump upon a low pressure reading. The pump is also required by NFPA 20 to have remote reading. The pump is also required by NFPA 20 to have remote alarm and signal devices at a point of constant, attendance to indicate such items as that the controller has operated into a motor running condition and loss of line power on the line side of the motor starter. NFPA 20 also requires to galvanize or paint the suction pipe to prevent tuberculation.

The FP booster pump is not, however, the main fire pump. It is a small ( 150 gpm ) backup fire pump which only supplies the standpipe (hose reel) systems in certain areas of the plant in the unlikely event that SSE damages the normal fire protection supply. The plant operating personnel will be immediately dispatched to the FP booster pump to open the isolation valve between the Service Water System and the Fire Protection System, and to start the pump. Due to these circumstances, an automatic controller is not necessary. The alarms required by NFPA 20 are also not needed since plant operating personnel will be at the pump if there is a problem with it. Since tuberculation is also not seen as being a problem due to the limited use of the pump, lining of the suction piping is not required.

For these reasons, the deviations stated above are acceptable.
Equipment in the Fire Protection Systems, except as noted in the FSAR, conforms to the standards of the NFPA, and is Underwriter's Laboratory (UL) listed and/or Factory Mutual (FM) approved. The following is a deviation from UL listed:
1. Teflon used to enhance closure of UL listed fire damper:

A Teflon coating has been applied to the blade guide flange of the fire dampers to improve their closure characteristics under flow. Although the dampers are not tested with the Teflon coating, this coating will not prevent the dampers from meeting the test requirements of UL 555. In the damper closure part of the test, the dampers were tested under no flow conditions. The untested, per UL, Teflon modification allows the damper to close under a flow condition.

UL 555 under "Corrosion Protection," allows after a damper is tested the use of epoxy or alkyd-resin type or other outdoor paint in the surface of the damper. Since the Teflon coating is, in essence, the same as a paint coating, it will not affect the rating of the damper. The use of Teflon on fire dampers is acceptable.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5-1, & Rev. 15 \\
STATION & Appendix A & Section F.3 \\
& Responses To BTP APCSB 9.5-1 & Page 110 \\
\hline
\end{tabular}

The following is a deviation from the FM approval requirements:
1. Fibercast fittings used in the underground sprinkler supply line to the Alternate RP Checkpoint:

During installation of the underground sprinkler supply line to the Alternate RP Checkpoint, it was discovered that FM approved Fibercast pipe and fittings were no longer available from the manufacturer. There was sufficient inventory of FM approved Fibercast pipe in stock to complete the installation. However, fittings (tee, flanges and elbows) were not in stock. Fibercast fittings made from the same material, with the same dimensions and the same engagement as the FM approved Fibercast fittings were available without the FM stamp. Engineering reviewed the form, fit and function of the substitute Fibercast fittings and allowed their installation in this application only.

\section*{I. Fire Proofing for Structural Steel}
(Ref.: Letter to NRC SBN-1O17, dated April 24, 1986)
Professional Loss Control, Inc. (PLC) conducted a Seabrook Structural Steel Survivability Analysis for those areas noted in Table 1. Wherever PLC indicated structural steel needed to be fire proofed, a structural integrity review was conducted on the fire areas as indicated by PLC temperatures. In most cases, the structure can withstand the potential loss of structural steel. No fireproofing will be done on these beams and/or columns. A few limited cases, some steel was fireproofed in a fire area but only steel indicated by PLC and needed to maintain the fire areas structure.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5, \\
STATION & Appendix A & \begin{tabular}{l} 
Rev. 15 \\
Section F. 3 \\
Page 111
\end{tabular} \\
\hline
\end{tabular}

TABLE 1
STRUCTURAL STEEL FIRE PROOFING ANALYSIS CHART
\begin{tabular}{cc} 
& \\
& PLC Analysis of \\
Area Shows no \\
Fire & Structural Steel \\
Area/Zone & Fireproof Required
\end{tabular}
EFP-F-1-A X
MS-F-1A-Z X
MS-F-1B-Z X

MS-F-2A-Z
MS-F-2B-Z
MS-F-3A-Z
MS-F-3B-Z

MS-F-4A-Z
X

MS-F-5A-Z

PLC Analysis of Area Shows Only Limited Fireproofing of Structural Steel is

Needed

PLC Analysis of Area Shows
Only Limited Fireproofing of Structural Steel is Needed UE\&C Has Determined Structure Can Accept Steel \(\underline{\text { Losses }}\)

RHR-F-1A-Z X
RHR-F-1B-Z X
RHR-F-1C-Z X
RHR-F-1D-Z X
RHR-F-2A-Z X
RHR-F-2B-Z

Does not contain exposed combustibles. Low Loading.

Does not contain exposed combustibles. Low Loading.

Exposed steel used for cable tray supports. Concrete slab is self-supporting.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5, \\
STATION & Appendix A & \begin{tabular}{l} 
Rev. 15 \\
Section F.3 \\
Page 112
\end{tabular} \\
\hline
\end{tabular}

TABLE 1
STRUCTURAL STEEL FIRE PROOFING ANALYSIS CHART
\begin{tabular}{|c|c|c|c|c|}
\hline Fire Area/Zone & PLC Analysis of Area Shows no Structural Steel Fireproof Required & PLC Analysis of Area Shows Only Limited Fireproofing of Structural Steel is Needed & PLC Analysis of Area Shows Only Limited Fireproofing of Structural Steel is Needed UE\&C Has Determined Structure Can Accept Steel Losses & Miscellaneous Notes \\
\hline RHR-F-3A-Z & X & & & \\
\hline RHR-F-3B-Z & X & & & \\
\hline CB-F-3B-A & X & & & \\
\hline \[
\begin{aligned}
& \text { CB-F-S1-0 } \\
& \text { CB-F-S2-0 }
\end{aligned}
\] & & & & Does not contain exposed combustibles. Low Loading. \\
\hline \begin{tabular}{l}
ET-F-1A-A \\
ET-F-1B-A \\
ET-F-1C-A \\
ET-F-1D-A \\
ET-F-S1-0
\end{tabular} & & & & Slab is self-supporting. Do not need structure steel. \\
\hline DG-F-3A-Z & X & & & \\
\hline DG-F-3B-Z & X & & & \\
\hline DG-F-3E-A & X & & & \\
\hline DG-F-3F-A & X & & & \\
\hline PAB-F-1A-Z & & & X & \\
\hline PAB-F-1B-Z & X & & & \\
\hline PAB-F-1F-Z & X & & & \\
\hline PAB-F-1G-A & X & & & \\
\hline
\end{tabular}
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5, \\
ATATION & Appendix A & \begin{tabular}{l} 
Rev. 15 \\
Section F.3 \\
Page 113
\end{tabular} \\
\hline
\end{tabular}

TABLE 1
STRUCTURAL STEEL FIRE PROOFING ANALYSIS CHART
\begin{tabular}{cc} 
& PLC Analysis of \\
& Area Shows no \\
Fire & Structural Steel \\
Area/Zone & Fireproof Required \\
\hline
\end{tabular}

PAB-F-S1-0
PAB-F-S2-0
PAB-F-2A-Z X
PAB-F-2B-Z
PAB-F-2C-Z
PAB-F-3A-Z X
PAB-F-3B-Z X
PAB-F-4-Z X
PAB-F-1J-Z X
PAB-F-1K-Z

FSB-F-1A
X
SW-F-1A-Z

PLC Analysis of Area Shows
PLC Analysis of Area Shows Only Limited Fireproofing of Structural Steel is

Needed

Only Limited Fireproofing of Structural Steel is Needed UE\&C Has Determined Structure Can Accept Steel Losses

Does not contain exposed PAB combustibles. Low loading.

Does not contain exposed combustibles. Low loading.

Structure is separated from fire area used for safe shutdown by seismic gap. Can accept loss of structure.
\begin{tabular}{|l|c|l|}
\hline SEABROOK & Evaluation and Comparison to BTP APCSB 9.5, \\
STATION & Appendix A & \begin{tabular}{l} 
Rev. 15 \\
Section F.3 \\
Page 114
\end{tabular} \\
\hline
\end{tabular}
\begin{tabular}{cc} 
\\
& \\
PLC Analysis of \\
Area Shows no \\
Firea/Zone & \begin{tabular}{c} 
Structural Steel \\
Fireproof Required
\end{tabular} \\
\hline
\end{tabular}

SW-F-1B-A
SW-F-1C-A
SW-F-1D-A
SW-F-1E-Z
SW-F-2-0
CT-F-1C-A
CT-F-1D-A
CT-F-2B-A
CT-F-3-0
CE-F-1-A
FPH-F-1A-A
FPH-F-1B-A
FPH-F-1C-A
TB-F-1B-A
TB-F-1A-Z
TB-F-1C-Z
TB-F-2-Z
TB-F-3-Z
NES-F-1A-A
TABLE 1
STRUCTURAL STEEL FIRE PROOFING ANALYSIS CHART

\section*{PLC Analysis of Area Shows Only Limited Fireproofing of Structural Steel is \\ Needed}

PLC Analysis of Area Shows
Only Limited Fireproofing of Structural Steel is Needed UE\&C Has Determined Structure Can Accept Steel
\(\underline{\text { Losses }}\)

\section*{Miscellaneous Notes}

Loss of this structure does not affect safe shutdown. Structure is isolated from remaining fire areas.

Loss of this structure does not affect safe shutdown. Structure is isolated from remaining fire areas.

Loss of this structure does not affect safe shutdown. Structure is isolated from remaining fire areas

Loss of this structure does not affect safe shutdown. Structure is isolated from fire areas used during safe shutdown by seismic gap.

Loss of this structure does not affect safe shutdown. Structure is isolated from fire areas used during safe shutdown by seismic gap.```


[^0]:    * Ref. Deviation No. 2, SBN-904, Dated Dec. 2, 1985.

[^1]:    * Personnel Hatch

[^2]:    910 Btu/Sq. Ft.

[^3]:    * Safe Shutdown Cable Requires Fire Protection.

[^4]:    * Safe Shutdown Cable Requires Fire Protection

[^5]:    * Safe shutdown cable requires fire protection

[^6]:    * Required for safe shutdown only on loss of offsite power.

[^7]:    No Safety Related or Safe Shutdown Equipment in This Area

[^8]:    * The ceiling of piping tunnel and walkway between Fuel Storage Building and $\mathrm{PAB} 7^{\prime}$, elevation which is also a floor of fire zone CE-F-1-Z (Tab 13) is 3 hr . fire rated.

[^9]:    * Door No. W-400 Leading Into Waste Process Building is Not 3 Hr. Fire Rated Door. Ref. Deviation No. 7, SBN-9o4, Dated Dec. 2, 1985.

[^10]:    $36.5 \mathrm{Btu} / \mathrm{Sq} . \mathrm{Ft}$. 262,500 Btu

[^11]:    * 3 Hr. Fire Damper Has Not Been Provided in Exhaust Duct at the Point of Connection To Unit Plant Vent. Ref: Deviation No. 1 SBN-904 Dated 12/2/85

[^12]:    * Charcoal Loading For PAH-F-L6 is 25750 Lbs. of Charcoal. CharcoalFire Loading Was Not Considered in Total Area. See Appendix "D'.

[^13]:    * 3 Hr. Fire Damper Has Not Been Provided in Exhaust Duct, 81'-0" Elev. at the Point of Connection To Unit Plant Vent.
    * Ref: Deviation No. 1

    SBN- 904
    Dated 12/02/85

[^14]:    Note 1: Capable of being powered from either Train A or Train B

[^15]:    * Charcoal fire loading was not considered in total area. See App. "D".

[^16]:    * 2' $-0^{\prime \prime} \mathrm{X} 1$ ' $-8^{\prime \prime}$ Trash Through Penetration Is Not Fire Rated. Ref. Deviation No. 3 SBN-904 Dated 12/2/85

[^17]:    ${ }^{*} 2^{\prime}-0$ " X 1 ' -8 " Trash Through Penetration Is Not Fire Rated. Ref: Deviation No. 3 SBN-904 Dated 12/2/85

[^18]:    * Ref.: Deviation No. 2, SBN-904, Dated Dec. 2, 1985

[^19]:    ** Cont. Encl. Vent Eq. Area and Cont. Annulus Are in Communication with Each Other Thru Structural Openings.

    * Cont. Annulus Portion Has No Detection.

    Ref. Deviation No. 2, SBN-904, Dated 12/02/85
    *** Charcoal Loading For Both EAH-F-9, 69 Total Is 2100 Lbs. Charcoal. Charcoal Fire Loading Was Not Considered in Total Area. See Appendix D.

[^20]:    * Entries for Hallway in parenthesis and italicized for differentiation

[^21]:    * Door C-100 Is Not 3 Hr. Fire Rated. (no further analysis required)

[^22]:    * Ref. Deviation No. 2, SBN-904, Dated Dec. 2, 1985.

[^23]:    * See page C-1 for the criterion used for "safe shutdown."

