

AMENDMENT TO THE ANNUAL REPORT ON THE OPERATION OF
THE WASHINGTON STATE UNIVERSITY TRIGA REACTOR

Facility License R-76 for the Reporting Period of
July 1, 1988 to June 30, 1989

This amendment to W.S.U. Annual Report contains some corrections and missing data that was not available at the time the Annual Report was prepared. The corrections and completed data are as follows:

Page 1, Section A, Item 2, Narrative Summary of the Year's Operations.

2. There were no changes in the design or operating procedures that related to reactor safety during the reporting period. However, there was a change in the performance characteristics and is as follows;

In April 1989, Bill Wilson re-evaluated the pulsing limit for the W.S.U. reactor for Core 32-A. Based on his re-evaluation, it was determined the Pulsing Limit given in the Technical Specifications, Section 3.3 should be changed from a maximum reactivity limit of \$2.50 to \$2.20. Administratively, the pulsing reactivity limit has been set at \$2.00 since 1976. A complete report of the re-evaluation of the pulsing limit is forth coming.

Page 5, Section G., Table VI, Average Quarterly Reactor and Experimenter Staff Exposure.

June's film badge results were not available from the vendor at the time the Annual Report was prepared. Table VI below now contains the missing film badge results:

TABLE VI
Average Quarterly Reactor and Experimenter Staff Exposure

(in millirem)

Jul-Aug-Sep	Oct-Nov-Dec	Jan-Feb-Mar	Apr-May-Jun
30	57	10	16

Page 6. Section I. Environmental Monitoring Program.

Due to an administrative delay in renewing the contract with the vendor who supplies the TLD dosimeters, new dosimeters have not yet been received. The contract renewal delay has been corrected and new dosimeters are presently being shipped. When they arrive, the dosimeters presently placed about the facility will be changed and processed and the results evaluated.

3.3 Pulse Mode Operation

Applicability: This specification applies to the peak fuel temperature in the reactor as a result of a pulse insertion of reactivity.

Objective: The objective is to ensure that fuel element damage does not occur in any fuel rod during pulsing.

Specification: The maximum reactivity inserted during pulse mode operation shall be such that the peak fuel temperature in any fuel rod in the core does not exceed 830°C . The maximum safe allowable reactivity insertion shall be calculated annually for an existing core and prior to pulsing a new or modified core arrangement.

Basis: TRIGA fuel is fabricated with a nominal hydrogen to zirconium ratio of 1.6 for FLIP fuel and 1.65 for Standard. This yields delta phase zirconium hydride which has a high creep strength and undergoes no phase changes at temperatures over 1000°C . However, after extensive steady state operation at 1 Mw, the hydrogen will redistribute due to migration from the central high temperature regions of the fuel to the cooler outer regions. When the fuel is pulsed, the instantaneous temperature distribution is such that the highest values occur at the surface of the element and the lowest values occur at the center. The higher temperatures in the outer regions occur in fuel with a hydrogen to zirconium ratio that has now substantially increased above the nominal value. This produces hydrogen gas pressures considerably in excess of that expected for $\text{ZrH}_{1.6}$. If the pulse insertion is such that the temperature of the fuel exceeds 874°C , then the pressure will be sufficient to cause expansion of microscopic holes in the fuel that grow larger with each pulse. The expansion of the fuel stresses and distorts the fuel rod material which, in turn, can cause overall swelling and distortion of the cladding and entire fuel rod. The pulsing limit of 830°C is obtained by examining the equilibrium hydrogen pressure of zirconium hydride as a function of temperature. The decrease in temperature from 874°C to 830°C reduces hydrogen pressure by a factor of two, which provides an acceptable safety factor. This phenomenon does not alter the steady state safety limit since the total hydrogen in a fuel element does not change. Thus, the pressure exerted on the clad will not be significantly affected by the distribution of hydrogen within the element.