#### SEP 0 5 1989

MEMORANDUM FOR: Charles E. Rossi, Director Division of Operational Events Assessment

Charles J. Haughney, Chief FROM: Events Assessment Branch Division of Operational Events Assessment

THE OPERATING REACTORS EVENTS MEETING SUBJECT: August 30, 1989 - MEETING 89-31

On August 30, 1989, we conducted an Operating Reactors Events meeting (89-31) to brief senior managers from NRR, AEOD, ACRS, RES, Commission Staff, and regional offices on selected events that occurred since our last meeting on August 23, 1989. Enclosure 1 lists the attendees.

Enclosure 2 presents the significant elements of the discussed events. Enclosure 3 contains a summary of reactor scrams for the week ending 08/27/89 and a comparison of weekly statistics with industry averages. We identified one significant event for input into the NRC performance indicator program.

> Charles J. Haughney, Chief Events Assessment Branch Division of Operational Events Assessment

(Republic)

Enclosures: As stated

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| IAME :MLReardon  | :CJHaughney :   |   |  |  |   |
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cc: T. Murley, NRR F. Miraglia, NRR J. Sniezek, NRR E. Jordan, AEOD J. Taylor, EDO E. Beckjord, RES W. Russell, RI S. Ebneter, RII B. Davis, RIII R. D. Martin, RIV J. B. Martin, RV W. Kane, RI L. Reyes, RII E. Greenman, RIII L. Callan, RIV R. Zimmerman, RV S. Varga, NRR B. Boger, NRR G. Lainas, NRR L. Shao, NRR B. Grimes, NRR F. Congel, NRR E. Weiss, AEOD T. Martin, EDO J. Lieberman, OE J. Guttmann, SECY A. Thadani, NRR S. Rubin, AEOD J. Forsyth, INPO R. Barrett, NRR M. Harper, AEOD R. Newlin, GPA H. Alderman, ACRS

D. Hood, NRR D. Matthews, NRR J. Hayes, NRR E. Adensam, NRR P. Shemanski, NRR M. Slosson, NRR R. Capra, NRR



September 5, 1989

- MEMORANDUM FOR: Charles E. Rossi, Director Division of Operational Events Assessment
- FROM: Charles J. Haughney, Chief Events Assessment Branch Division of Operational Events Assessment
- SUBJECT: THE OPERATING REACTORS EVENTS MEETING , August 3C, 1989 - MEETING 89-31

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Charles J. Haughpey, Chief Events Assessment Branch Division of Operational Events Assessment

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cc w/Encl.: See Next Page

#### ENCLOSURE 1

## LIST OF ATTENDEES

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## OPERATING REACTORS EVENTS BRIEFING (89-31)

# August 30, 1989

| NAME ORGANIZATION  |   | NAME   | ORGANIZATIO  |  |
|--|---|--|--|--|
| E. Adensam<br>J. Hayes<br>R. Borchardt<br>W. Troskoski<br>M. Reardon<br>L. Norrholm<br>G. Hammer<br>J. Carter<br>R. Karsch               | NRR/DRP<br>NRP/DRP<br>OEDO<br>OE<br>NRR/DOEA<br>OCM/KC<br>NRR/DET<br>NRR/DOEA<br>NRR/DOEA<br>NRR/DOEA           | NAME<br>J. Roe<br>C. Rossi<br>J. Partlow<br>W. Minners<br>T. Greene<br>J. Raleigh<br>S. Stein<br>D. Hood<br>A. Gilbert           | NRR/DLPQ<br>NRR/DOEA<br>NRR/ADP<br>RES/DSIR<br>NRR/DOEA<br>NRR/DOEA<br>NRR/DRIS<br>NRR/DD2-3<br>NRR/DOEA |  |
| P. Schemanski<br>H. Ornstein<br>L. Kintner<br>A. Gibson<br>P. Cortland<br>S. Varga<br>D. Trimble<br>M. Slosson<br>D. Matthews<br>P. Bobe | NRR/PD3-2<br>AEOD<br>NRR/PD4<br>Region II<br>NRR/TVA<br>NRR/DRP<br>OCM/JC<br>NRR/PD1-1<br>NRR/PD1-3<br>AEOD/DSP | C. Daily<br>S. Long<br>S. Newberry<br>H. Li<br>R. Lobel<br>T. Gody, Jr.<br>G. Lainas<br>P. Baranowsky<br>R. Benedict<br>R. Capra | ACRS<br>ACRS<br>NRR/SICB<br>NRR/DOEA<br>NRR/DOEA<br>NRR/DOEA<br>NRR/DOEA<br>NRR/DOEA<br>NRR/PD1-1        |  |

ENCLOSURE 2

# OPERATING REACTORS EVENTS BRIEFING 89-31 EVENTS ASSESSMENT BRANCH LOCATION: 15B-11, WHITE FLINT WEDNESDAY, AUGUST 30, 1989, 11:00 A.M.

MCGUIRE UNIT 2

STEEL CONTAINMENT VESSEL CORROSION

SUMMER UNIT 1

REPEAT EVENT SPURIOUS PRESSURIZER SAFETY VALVE OPENING

LASALLE UNIT 2

SCRAM WITH POSSIBLE RPS MALFUNCTION

NINE MILE POINT UNIT 1 CONTAMINATION OF SUB-BASEMENT BY LEAKING DRUMS (AIT UPDATE)

GENERIC ISSUE

SOLENCID VALVE FAILURES

## MCGUIRE UNIT 2 STEEL CONTAINMENT VESSEL CORROSION AUGUST 24, 1989

## PROELEM

CORROSION OF STEEL CONTAINMENT VESSEL.

## CAUSE

COLLECTION OF WATER ON FLOOR OF ANNULUS BETWEEN CONTAINMENT VESSEL AND CONCRETE SHIELD BUILDING.

SAFETY SIGNIFICANCE POTENTIAL WEAK SPCT IN CONTAINMENT VESSEL.

### DISCUSSION

- O PROTECTIVE COATING DEGRADED, PERMITTING CORROSION OF STEEL.
- O AREA ABOUT 1-1/2 INCHES HIGH BY ABOUT 30 FEET LONG, DIRECTLY ABOVE ANNULUS FLOOR.
- c 1/16 INCH GENERAL CORROSION, PITTING TO 1/10 INCH.
- o STEEL IS 1 INCH THICK.
- U ADEQUATE REMAINING WALL THICKNESS.
- O INSPECTION ACCESS IS LIMITED DUE TO AIR DUCTS.
- C SOURCE OF WATER IS UNKNOWN, BUT LICENSEE IS LOOKING FOR IT. MAY BE LEAKING VALVES OR FLOOR SUMP OVERFLOW.
- O WEEKLY SURVEILLANCE.
- O REPAIR AT NEXT REFUELING CLEAN, WELD DEPOSIT, DIFFERENT COATING.
- O UNIT 1 CHECKED 8/29/89.

#### FOLLOWUP

REGION MAY PERFORM ITS OWN INSPECTION OR PARTICIPATE IN LICENSEE'S INSPECTION.

CONTACT: R. BENEDICT REFERENCE: 10 CFR 50.72 #16392 SIGEVENT NO

## SUMMER UNIT 1 REPEAT EVENT SPURIOUS PRESSURIZER SAFETY VALVE OPENING AUGUST 25, 1989

### PROBLEM

A PRESSURIZER CODE SAFETY VALVE OPENED SPURIOUSLY DURING POWER OPERATION.

#### CAUSE

LOSS OF LOOP SEAL (ROOT CAUSE UNKNOWN).

### SAFETY SIGNIFICANCE

LOSS OF REACTOR COOLANT AND POTENTIAL CHALLENGE TO PLANT SAFETY SYSTEMS.

### BACKGROUND

- MAY 28, 1989, SUMMER UNIT 1 HAD A SPURIOUS OPENING OF "C" PRESSURIZER CODE SAFETY VALVE DURING 100% POWER OPERATION (2250 PSIA).
- c "C" AND "E" WERE REPLACED. ("B" WAS REPLACED DUE TO SEAT LEAKAGE.)
- O TESTS ON FAULTY VALVES AT A M TEST FACILITY IN CALIFORNIA WERE INCONCLUSIVE--THE LICENSEE FOUND NO DEFECTS IN THE VALVE.
- C LICENSEE HAS BEEN CONTINUALLY MONITORING ALL PRESSURIZER CODE SAFETY VALVES FOR VALVE BODY TEMPERATURE (LOOP SEAL LEAKAGE RAISES THE TEMPERATURE) SINCE THE JUNE STARTUP.

## DISCUSSION

- O SAFETY VALVE "A" HAS BEEN LEAKING SINCE SHORTLY AFTER THE JUNE STARTUP.
- C CN AUGUST 25, 1989, SUMMER UNIT 1 HAD SPURIOUS OPENING OF "A" PZR CODE SAFETY VALVE DURING 100% POWER OPERATION.

CONTACT: A. GILBERT. REFERENCE: 10 CFR 50.72 #16404 SIGEVENT YES

#### SUMMER UNIT 1

- REACTOR COOLANT SYSTEM PRESSURE DECREASED GUICKLY.
- MANUAL REACTOR TRIP AT ABOUT 2000 PSI, NO SAFETY INJECTION. SETPOINT IS 1875 PSI.

- 2 -

- SAFETY VALVE "A" RESEATED; PRESSURE LEVELED AT ABOUT 1950 PSI.
- LICENSEE BROUGHT PLANT TO COLD SHUTDOWN.
- O VALVE "A" HAS BEEN REPLACED AND IS EXPECTED TO BE TESTED.
- C REPLACEMENT VALVE IS A REFURBISHED VALVE FROM THE SAME WESTINGHOUSE FACILITY IN CALIFORNIA. (THE SAME TYPE OF REPLACEMENT AS WAS USED FOR "E" AND "C" VALVES IN MAY.)
- O LICENSEE PLANS TO STARTUP THIS WEEKEND.

FOLLOWUP

REGION II IS FOLLOWING THIS EVENT. MECHANICAL ENGINEERING BRANCH AND AEOD ARE LOOKING AT THE GENERIC ASPECTS OF THIS PROBLEM.



## CASALLE UNIT 2 SCRAM WITH POSSIBLE RPS MALFUNCTION AUGUST 26, 1389

#### PROBLEM

AFTER RECEIPT OF A SCRAM SIGNAL 2 OF 8 INDICATING LIGHTS FOR RPS SUBCHANNELS REMAINED LIT INDICATING POSSIBLE STICKING OF A SCRAM CONTACTOR.

#### CAUSE

UNKNOWN AT THIS TIME.

#### SAFETY SIGNIFICANCE

FAILURE OF TWO CONTACTORS IN CERTAIN CHANNELS COULD LEAD TO AN ATWS. ONLY ONE CONTACTOR IS SUSPECTED TO HAVE MOMENTARILY STUCK.

#### DISCUSSION

- C LASALLE UNIT 2 WAS AT 10% POWER TESTING TURBINE STOP VALVE CLOSURE WHEN THE REACTOR AUTO SCRAMMED.
- O TWO OF EIGHT RPS SCRAM LIGHTS STAYED ON, INDICATING THAT THE SCRAM VALVES DID NOT OPEN.
- MANY PIECES OF EQUIPMENT WHICH COULD HAVE PREVENTED THIS EVENT OR PROVIDED INFORMATION TO UNDERSTAND WHAT HAPPENED EITHER FAILED OR WERE INOPERATIVE, E.G.,
  - MSSV POSITION INDICATION FOR THE #3 VALVE SHOWED FULL OPEN,
  - TURBINE FIRST STAGE PRESSURE CHART RECORDER HAD RUN OUT OF INK,
  - ALARM TYPER DATA RECORDER FAILED BECAUSE THE INPUT WAS OVERLOADED DUE TO NUISANCE ALARMS.
  - STARTREK WAS NOT WORKING BECAUSE IT HAD NO INPUT SIGNAL.
- O THE SCRAM CONTACTOR "K14E" MAY HAVE BEEN SLOW TO OPEN, CAUSING SCRAM LIGHTS "A2" AND "A3" TO REMAIN LIT.
- C THE OPERATOR OBSERVED THAT SCRAM LIGHTS "A2 AND "A3" WERE STILL LIT AFTER SCRAM ACTUATION.

CONTACT: RUDY KARSCH REFERENCE: 10 CFR 50.72 #16411 SIGEVENT TBD

#### LASALLE UNIT 2

C THE OPERATOR MANUALLY SCRAMMED THE REACTOR 13 SECONDS AFTER THE AUTO SCRAM.

#### FOLLOWUF

- O THE LICENSEE WILL CONDUCT THE FOLLOWING INVESTIGATIONS:
  - TRACE THE PREVENTIVE MAINTENANCE HISTORY OF THE SCRAM CONTACTORS,
  - CONFUCT A FAULT TREE ANALYSIS TO DISCOVER IF THERE ARE ANY OTHER WAYS TO PRODUCE THE OBSERVED SYMPTOMS,
  - DC & REVERSE CALIERATION STUDY TO DETERMINE IF INSTRUMENTATION MALADJUSTMENT ALONE COULD CAUSE THIS EVENT.
- O IN ADDITION THE LICENSEE WILL PROVIDE DETAILS RECARDING ALL THE OBSERVED EQUIPMENT MALFUNCTIONS AND PROVIDE AN EXPLANATION THAT TIES UP ALL THE LOOSE ENDS.
- O REGION 111 SENT AN ELECTRICAL SPECIALIST TO THE SITE.
- O NRR/ICSB WILL EE THE FOCAL POINT FOR ONGOING FOLLOWUP.



### 89-31

# NINE MILE POINT UNIT 1 CONTAMINATION OF SUB-BASEMENT BY LEAKING DRUMS (AIT UPDATE) AUGUST 21, 1989

### PROBLEM

RESIN STORAGE DRUMS SPILL RADIOACTIVE MATERIAL DUE TO THEIR BEING LEFT UNCOVERED.

AIT FINDINGS

- O SUB-BASEMENT WAS USED FOR OVERFLOW FROM DRAINING OPERATIONS SINCE PLANT WAS LICENSED. (NOT UNCOMMON FOR PLANTS OF THAT VINTAGE DUE TO UNDER DESIGN OF RAD WASTE SYSTEM).
- O IN 1981 SIGNIFICANTLY MORE WATER WAS DUMPED INTO THE ROOM, FOUR FEET OF WATER INSTEAD OF ONE FOOT.
- O AT THAT TIME THE ROOM HELD DRUMS FULL OF SPENT RESIN. THE DRUMS WERE OPEN WAITING FOR THE RESINS TO DRY OUT.
- o THE WATER DISLODGED THE DRUMS SPILLING THE CONTENTS ONTO THE FLOOR.
- G AIT DETERMINED THAT THERE IS NO RELEASE PATHWAY FOR LIQUID OR SOLID RAD WASTE. AIRBORNE RELEASE IS MONITORED VIA THE PLANT STACK.
- O POSSIBLE ENFORCEMENT ACTION BECAUSE THE LICENSEE DID NOT FILE A 50.59 ANALYSIS AND FSAR UPDATE.

CONTACT: R. KARSCH REFERENCE: 10 CFR 50.72 #16374 AIT YES SIGEVENT NO

### GENERIC ISSUE

## POTENTIAL COMMON MODE FAILURE OF MSIVS DUE TO ASCO VALVES EXCEEDING GUALIFIED OPERATING LIFE

#### PROBLEM

ALL SOLENOID VALVES USED AT GRAND GULF TO ACHIEVE MSIV CLOSURE HAD DEGRADED ELASTOMER SEAT MATERIAL.

### CAUSE

SOLENOID VALVES APPEAR TO HAVE HAD AN IMPROPERLY CALCULATED GUALIFIED LIFE DECAUSE IMPROPER TEMPERATURES IN THE REGION OF THE ELASTOMER WERE USED.

#### SAFETY SIGNIFICANCE

POTENTIAL FOR COMMON MODE FAILURE OF MSIVS EXISTS DUE TO OPERATION EEYOND THE ACTUAL LIFE EXPECTANCY OF THE SOLENOID VALVES.

#### DISCUSSION

- O SOLENOID VALVES WIDELY USED IN MANY SAFETY-RELATED SYSTEMS.
- O COMMON MODE FAILURE MECHANISMS IDENTIFIED FOR ASCO MODEL NP 8323
  - NP 0212
  - ELASTOMER DEGRADATION
  - STICKING INTERNALS
- O CRAND GULF CALCULATED GUALIFICATION LIFE IN 1985 USING SINGLE COIL HEATUP DATA: LIFE WAS 8.6 - 5.9 YEARS.
- O DUAL COIL HEATUP DATA BECAME AVAILABLE IN 1987
  - SEAT TEMPERATURE ABOUT 100 F ABOVE AMBIENT.
- G RECALCULATED GUALIFICATION LIFE AS 2.9 YRS.; ACTUAL WAS 4.5 YRS.
- O BOTH BWRS AND PWRS HAVE ASCO DUAL COIL SOLENOID VALVES.
- O MANY GENERIC COMMUNICATIONS ISSUED.
  - MOST RECENTLY INFORMATION NOTICES 88-43 AND GE SIL 481.

#### FOLLOWUP

- O ASCO IS PREPARING A SERVICE BULLETIN TO DESCRIBE THE CHANGES IN TEMPERATURE INFORMATION AND WHAT TO DO TO ASSURE A VALID GUALIFICATION LIFE FOR ACTUAL OPERATING CONDITIONS.
- O AN IN IS BEING DRAFTED TO ALERT THE NUCLEAR INDUSTRY.
- C AEOD COMPLETING CASE STUDY ON SOLENOID VALVE FAILURES.

CONTACT: J. CARTER REFERENCES: 10 CFR 50.72 #16355

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|   |  |   | OLENOID'B'   |  |
| 131°C   | 219°C  | 227.0   | OLENOID'B'   | 170°C  |
| 131°C<br>66°C   | 219°C  | 227 °C  | OLENOID'B'   | 170°C  |
| 131°C<br>66°C<br>49°C   | 219°C<br>163°C<br>147°C  | 227°C<br>175°C<br>160°C   | <u>OLENOID'B</u><br><u>176°C</u><br>121°C<br>108°C   | 170°C<br>113°C<br>99°C   |
| 131°C<br>66°C<br>49°C<br>25°C   | 219°C<br>163°C<br>147°C<br>126°C   | 227 °C<br>175 °C<br>160 °C<br>141 °C  | <u>OLENOID'B'</u><br>176°C<br>121°C<br>108°C<br>88°C   | 170°C<br>113°C<br>99°C<br>77°C   |
| 131°C<br>66°C<br>49°C<br>25°C<br>AMBIENT  | 219°C<br>163°C<br>147°C<br>126°C<br>COIL-SOL.'A'   | 227 °C<br>175 °C<br>160 °C<br>141 °C<br>COIL-SOL 'B'  | OLENOID'B'<br>176°C<br>121°C<br>108°C<br>88°C<br>CORE DISC   | 170 °C<br>113 °C<br>99 °C<br>77 °C<br>LOWER DISC   |
| 131°C<br>66°C<br>49°C<br>25°C<br>AMBIENT<br>TEMP  | 219°C<br>163°C<br>147°C<br>126°C<br>COIL°SOL.'A'   | 227 °C<br>175 °C<br>160 °C<br>141 °C<br>COIL-SOL. 'B'<br>MAXIMUM TEMP   | DLENDID'B'<br>176°C<br>121°C<br>108°C<br>88°C<br>CORE DISC<br>PERATURE   | 170 °C<br>113 °C<br>99 °C<br>77 °C<br>LOWER DISC   |
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| 131°C<br>66°C<br>49°C<br>25°C<br>AMBIENT<br>TEMP<br>ITEM  | 219°C<br>I 63°C<br>I 47°C<br>I 26°C<br>COIL·SOL.'A'  | 227 °C<br>175 °C<br>160 °C<br>141 °C<br>COIL-SOL 'B'<br>MAXIMUM TEMP<br>RES OF COIL AND<br>E ENERGIZED AN   | OLENOID'B'   | 170 °C<br>113 °C<br>99 °C<br>77 °C<br>LOWER DISC<br>LOWER DISC<br>NO. BY DATE APP DATE   |
| IBI°C<br>66°C<br>49°C<br>25°C<br>AMBIENT<br>TEMP<br>ITEM<br>MAXIMU<br>ELASTON<br>BY<br>ORAWN BWE  | 219°C<br>163°C<br>147°C<br>126°C<br>COIL·SOL.'A'<br>M TEMPERATUR<br>MERS WITH VALV<br>DATE<br>MANUFACTUR<br>BE IN ACCOL<br>PROCES  | 227 °C<br>175 °C<br>160 °C<br>141 °C<br>COIL-SOL 'B'<br>MAXIMUM TEMP<br>RES OF COIL AND<br>E ENERGIZED AN<br>NON<br>DURE MP 3003<br>E CAN   | OLENOID'B'   | 170 °C<br>113 °C<br>99 °C<br>77 °C<br>LOWER DISC<br>   |
| I 31 °C<br>66°C<br>49°C<br>25°C<br>AMBIENT<br>TEM<br>ITEM<br>MAXIMU<br>ELASTON<br>BY<br>DRAWN BWE<br>PROJ AFF. I<br>CHECRED [G.V.<br>DFT. AFF.] | 219°C<br>163°C<br>147°C<br>126°C<br>COIL·SOL.'A'<br>JM TEMPERATUR<br>MERS WITH VALV<br>DATE<br>JMANUFACTUR<br>BE IN ACCOU<br>PROCESS<br>7-7-87<br>PROPERTY DF AUTH<br>WORE DRLY. ALL | 227 °C<br>175 °C<br>160 °C<br>141 °C<br>COIL-SOL 'B'<br>MAXIMUM TEMP<br>RES OF COIL AND<br>E ENERGIZED AN<br>AND TEMPSODS<br>RES OF COIL AND<br>E ENERGIZED AN<br>AND TOLERANCES TO<br>RDANCE WITH ASCO<br>DURE MP 3:003<br>BCAI<br>DUATIC SMITCH COMPARY, USE PERMI<br>BIGHTS OF DESIGN OR INVERTION A | OLENOID'B'<br>176°C<br>121°C<br>121°C<br>108°C<br>88°C<br>CORE DISC<br>DERATURE<br>DERATURE<br>DERATURE<br>DERATURE<br>AB<br>DERATURE<br>DERATURE<br>AB<br>DERATURE<br>AB<br>CAR<br>AB<br>AB<br>AB<br>AB<br>AB<br>AB<br>AB<br>AB<br>AB<br>AB | 170°C<br>113°C<br>99°C<br>77°C<br>LOWER DISC<br>LOWER DISC<br>NO. BY DATE APP DATE<br>AN OAL OAN OA<br>AV OAR OAA OR<br>AV OAR OAA<br>AN OAL |

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#### REACTOR SCRAM SUMMARY WEEK ENDING 08/27/89

#### 1. PLANT SPECIFIC DATA

| DATE     | SITE           | UMIT | POWER | *\$16KAL | CAUSE     | COMPLI-<br>CATIONS | YTD<br>ABOVE<br>152 | YTD<br>BELOW<br>157 | TTD<br>TOTAL |
|----------|----------------|------|-------|----------|-----------|--------------------|---------------------|---------------------|--------------|
| 08/22/89 | BIG ROCK POINT | 1    | 96    |          | EQUIPMENT | MO                 | 1                   | 0                   | 1            |
| 08/23/89 | SOUTH TELAS    | 2    | 100   |          | EQUIPMENT | NO                 | 4                   | 1                   | 5            |
| 08/24/89 | CATAWBA        | 1    | 98    | Ħ        | EQUIPMENT | NO                 | 3                   | 0                   | 3            |
| 08/25/89 | SUMMER         | 1    | 97    | Ħ        | EDUIPMENT | NO                 | 4                   | 0                   | 4            |
| 08/26/89 | LASALLE        | 2    | 10    |          | EQUIPMENT | NO                 | 0                   | 1                   | 1            |
| 08/26/89 | MCBUIRE        | 1    | 100   | 4        | EQUIPMENT | MO                 | 2                   | 0                   | 2            |
| 08/26/89 | DUANE ARNOLD   | 1    | 98    | A        | EQUIPHENT | NO                 | 5                   | 0                   | 5            |

Fage No." 1 .8/25/89

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# PERFORMANCE INDICATORS SIGNIFICANT EVENTS

ENCLOSURE 3

PLANT NAME EVENT EVENT DESCRIPTION . OTR SIGNIFICANCE

POBINSON 2

08 16/89 INADEDUATE NPSH FOR AUX FEEDWATER PUMPS.

0 POTENTIAL FOR OR ACTUAL DEGRADATION DF SAFETY-RELATED EQUIPMENT 11. COMPARISON OF WEEKLY STATISTICS WITH INDUSTRY AVERAGES

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SCRAMS FOR WEEK ENDING

| SCRAM CAUSE      | POWER | NUMPER<br>OF<br>SCRAMS(5) | 1989<br>WEEKLY<br>AVERAGE<br>YTD | 1988<br>WEEKLY<br>AVERAGE | 1987<br>WEEKLY<br>AVERAGE | 1986<br>WEEKLY<br>AVERAGE<br>(3)(4) | 1985<br>WEEKLY<br>AVERAGE<br>(8)(9) |
|------------------|-------|---------------------------|----------------------------------|---------------------------|---------------------------|-------------------------------------|-------------------------------------|
| ** POWER >15%    | 154   |                           | 3.0                              | 3.1                       | 3.9                       | 4.3                                 | 5.4                                 |
| EQUIP. RELATED   | >184  | 0                         | 1.2                              | 1.0                       | 1.3                       | 1.3                                 | 2.0                                 |
| PERS. RELATED(0) | >15%  | 0                         | 0.1                              | 0.5                       | 1.2                       | 0.4                                 | 0.6                                 |
| UTHER(7)         | 12210 | v                         | V                                |                           |                           |                                     |                                     |
| ** Subtotal **   |       | 6                         | 4.3                              | 4.6                       | 6.4                       | 6.5                                 | 8.0                                 |
| ** POWER <15%    |       |                           |                                  |                           |                           |                                     |                                     |
| EQUIP. RELATED   | <15%  | 1                         | 0.4                              | 0.5                       | 1.2                       | 1.4                                 | 1.3                                 |
| PERS. RELATED    | <15%  | 0                         | 0.3                              | 0.3                       | 0.6                       | 0.8                                 | 0.9                                 |
| OTHER            | <15%  | 0                         | 0.0                              | 0.1                       | 0.3                       | 0.2                                 | 0.2                                 |
| ** Subtotal **   |       | 1                         | 0.7                              | 0.9                       | 2.1                       | 2.4                                 | 2.4                                 |
| *** Total ***    |       | 7                         | 5.0                              | 5.5                       | 8.5                       | 8.9                                 | 10.4                                |

#### MANUAL VS AUTO SCRAMS

| TYPE          | NUMBER<br>OF<br>SCRAMS | 1989<br>WEEKLY<br>AVERAGE<br>YTD | 1988<br>WEEKLY<br>AVERAGE | 1987<br>WEEKLY<br>AVERAGE | 1986<br>WEEKLY<br>AVERAGE | 1985<br>WEEKLY<br>AVERAGE |
|---------------|------------------------|----------------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| •             |                        |                                  |                           |                           |                           |                           |
| MANUAL SCRAMS | 2 5                    | 0.9                              | 1.0                       | 1.4                       | 1.0                       | 1.0<br>9.4                |

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- PLANT SPECIFIC DATA BASED ON INITIAL REVIEW OF 50.72 REPORTS FOR THE WEEK OF INTEREST. PERIOD IS MIDNIGHT SUNDAY THROUGH MIDNIGHT SUNDAY. SCRAMS ARE DEFINED AS REACTOR PROTECTIVE ACTUATIONS WHICH RESULT IN ROD MOTION, AND EXCLUDE PLANNED TESTS OR SCRAMS AS PART OF PLANNED SHUTDOWN IN ACCORDANCE WITH A PLANT PROCEDURE. THERE ARE 111 REACTORS HOLDING AN OPERATING LICENSE.
- COMPLICATIONS: RECOVERY COMPLICATED BY EQUIPMENT FAILURES OR PERSONNEL ERRORS UNRELATED TO CAUSE OF SCRAM.
- PERSONNEL RELATED PROBLEMS INCLUDE HUMAN ERROR, PROCEDURAL DEFICIENCIES, AND MANUAL STEAM GENERATOR LEVEL CONTROL PROBLEMS.
- "OTHER" INCLUDES AUTOMATIC SCRAMS ATTRIBUTED TO ENVIRONMENTAL CAUSES (LIGHTNING), SYSTEM DESIGN, OR UNKNOWN CAUSE.