TENNESSEE VALLEY AUTHORITY

CHATTANOOGA, TENNESSEE 37401 5N 157B Lookout Place

AUG 1 1 1987

U.S. Nuclear Regulatory Commission Office of Nuclear Regulatory Research Attention: Document Control Desk Washington, DC 20555

Gentlemen:

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SEQUOYAH NUCLEAR PLANT, UNITS 1 AND 2 - NUREG-1150 (REACTOR RISK REFERENCE DOCUMENT)

Please refer to my letter dated July 31, 1987.

Enclosed is TVA's response to the request for additional technical information on Sequoyah submitted by James G. Keppler's letter to S. A. White dated July 23, 1987. If you have any questions, please telephone D. L. Williams at (615) 632-7170.

Very truly yours,

TENNESSEE VALLEY AUTHORITY

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R. L. Gridley, Director Nuclear Safety and Licensing

Enclosures cc (Enclosures):

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ENCLOSURE

Response to Request for Additional Information Letter from James G. Keppler to S. A. White Dated July 23, 1987

Comments

- Please provide the probability data and the calculational basis to justify a frequency for loss of offsite power of less than 7E-2 per year.
- 8. We are currently using Cluster 7 from NUREG-1032 for probabilities for failure to restore offsite ac power. Please provide any justification or data you have to support a lower (i.e., better) curve for recovery of ac power at Sequoyah.

Response

Questions 1 and 8 related to the frequency and duration of loss of offsite power. NUREG-1032, "Evaluation of Station Blackout Accidents at Nuclear Power Plants (Draft)," is cited as the reference for this information in the NUREG-1150 analysis. However, TVA's analysis based on the criteria outlined in NUREG-1032 indicates that Sequoyah should be considered a cluster group 2 plant for loss of offsite power initiating event frequency instead of cluster group 7 as assumed in the NUREG-1150 analysis. Therefore, we believe using the cluster group 2 data is appropriate for SQN. Attachment A provides information previously supplied to EI Services (NRC subcontractor on this program).

Comment

 Please provide your estimate of battery depletion time during station blackout sequences and the basis.

Response

The Sequoyah design basis for battery depletion time under station blackout conditions is two hours (reference FSAR section 8.3.2). The 125V dc batteries at Sequoyah are tested at least once every 18 months in accordance with SI-105 (Attachment B) to ensure a minimum discharge time of two hours. Also, the manufacturer specification on the batteries specifies a minimum of two hours to discharge.

A separate TVA analysis supporting the four-hour battery depletion time used by NRC in the NUREG-1150 analysis does not exist. However, additional information is available to support this assumption. A successful test simulating loss of ac power was performed by TVA as a part of the special low power testing program at Sequoyah. Also, as part of a station blackout risk study for TVA's Browns Ferry Nuclear Plant performed by Oak Ridge National Laboratory (NUREG/CR-2182), TVA determined that the four hour battery depletion time initially assumed in the study could be extended to seven hours. We expect that a similar analysis for the Sequoyah batteries would provide comparable results. TVA plars to pursue this matter as part of the current industry initiatives to address NRC's unresolved safety issue A-44. Given this data and our experience with risk-based evaluations, it is our judgment that the battery depletion time used in NUREG-1150 is reasonable.

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- 3. A primary sequence of interest is the reactor coolant pump (RCP) seal loss of coolant accident (LOCA) after loss of all seal cooling due to total loss of plant service water or component cooling water. Please provide any test results or engineering analyses to establish:
 - a. the time to failure of RCP seals after loss of seal cooling (and leak rate); and
 - b. the ability of the centrifugal charging pumps to operate after a failure of the component cooling system.

Response

- a. The time of failure of RCP seals after loss of seal cooling (and the leak rate) is available in Westinghouse WCAP-10541, "Reactor Coolant Pump Seal Performance Following a Loss of All AC Power," Revision 2. A copy of this WCAP has previously been submitted to NRC by the Westinghouse Owners' Group (reference Westinghouse letter OG-206 dated December 10, 1986, from L. D. Butterfield to J. Lyons). This information applies to SQN.
- b. Testing has been conducted to show the centrifugal charging pump (CCP) operation is not degraded by the loss of component cooling (CCS) for a period of at least 24 hours. This testing is discussed in an April 7, 1987 letter from M. J. Hitchler (Westinghouse) to W. Mims (TVA), a copy of which is provided as Attachment C.

Comment

 Please provide thermal/hydraulic analysis results showing containment pressure time histories for small (2" and 1/2") LOCAs after actuation of the containment sprays.

Response

Containment pressure time histories for small break LOCAs (2-inch) are covered by IDCOR Task 23.1S; "Sequoyah Nuclear Plant: Integrated Containment Analysis," a copy of which is provided as Attachment D. Similar information on 1/2-inch LOCAs is not available; however, it is our understanding that the submittal of this IDCOR report is responsive to the staff's request.

Comment

5. Please provide the results of analyses which show rates of temperature rise in the switchgear rooms upon loss of heating, ventilation or air conditioning (HVAC) to the rooms.

Response

Engineering calculation TI-ECS-61, Revision 1 (Attachment E) provides "Electric Board Room Temperature Profiles Versus Time Upon Loss Of Cooling." This calculation assumes loss of all HVAC and considers operator actions. In addition, engineering calculation TI-ECS-69 (Attachment F) provides a similar analysis assuming availability of an air handling unit to circulate air within the affected spaces.

Comment

6. Please provide plant-specific data for diesel generator failure to start and diesel generator test/maintenance outages.

Response

Attachment G provides information concerning diesel generator availability at Sequoyah. TVA agrees that the diesel generator failure rates used in NUREG-1150 are reasonable.

Comment

7. Please send latest revision of all emergency procedures, functional restoration procedures, emergency contingency actions, and operating procedures for loss of component cooling water, essential raw cooling water, instrument air, and a vital bus.

Response

Attachment H identifies the procedures requested by NRC. Copies of these procedures are enclosed in this transmittal.





NUREG-1032

Clu	ster	Group	0 1	Clu	ster	Group	2 (Cont'd)	Ciu	ister	Gro	up 3 (Cont'd)
GR	I	SR	SS	GR	I	SR	SS	GR	I	SR	SS
1	1	1	1	2	1	3	1	1	3	5	1
1	1	2	2	2	1	4	1	1	3	5	2
1	2	1	1	2	1	4	2	2	1	3	2
1	2	2	1	2	2	1	2	2	1	5	1
2	1	1	1	2	2	2	2	2	1	5	2
2	1	2	1	2	2	3	1	2	2	3	2
2	2	1	1	2	2	4	1	2	2	5	1
2	2	2	1	2	2	4	2	2	2	5	2
				2	3	1	1	2	3	1	2
Clus	ter	Group	2	2	3	2	1	2	3	2	2
								2	3	3	1
äR	I	SR	SS	Clus	ster	Group	3	2	3	3	2
		~						2	3	4	1
	1	1	2	GR	I	SR	SS	2	3	4	2
	1	2	2					2	3	5	1
	1	3	1	1	1	3	2	2	3	5	2
	1	4	1	1	1	5	1				
	1	4	2	1	1	5	2	Clus	ster	Grou	p 4
	2	1	2	1	2	3	2	a na			
	2	2	2	1	2	5	1	GR	I	SR	SS
	2	3	1	1	2	5	2				
	2	4	1	1	3	1	2	1	1	1	4
	2	4	2	1	3	2	2	1	1	2	4
	3	1	1)	1	3	3	1	1	1	3	4
	3	2	1	1	3	3	2	1	1	4	4
	1	1	2	1	3	4	1	1	1	5	4
	1	2	2	1	3	4	2	1	1	6	3

Table A.11 Identification of grid (GR), offsite power system design (I), severe weather (SR), and extremely severe weather (SS) factors included in nine cluster groups

	Grid reliability(G))	
Grid reliability group (G)		Frequency of grid loss	
G1		Less that (0.01/si	n <u>l per 60 site-year:</u> te-year)
G2		<pre>> 1 per { < 1 per { (0.03/sit)</pre>	60 site-years and 30 site-years te-year)
G3		> 1 per 2 < 1 per 6 (0.1/site	20 site-years and 5 site-years e-year)
G4		Greater t per 6 sit (0.3/site	than or equal to 1 te-years e-year)
	Recovery (R)		
Recovery from grid blackout group (R)		Recovery	capability
R1		Plant has procedure (non-emer the site following	capability and s to recover offsite gency) AC power to within 1/2 hour a grid blackout.
R2		All other	plants not in R1.
G	rid reliability/recovery	(GR [*])	
Grid reliability/ recovery group (GR)	Grid reliabilit group (G)	ty ·	Recovery from grid blackout group (R)
GR1 GR2 GR3 GR4 GR5 GR6 GR7	G1 G2 G3 G4 G1 G2 G3		R1 R1 R1 R2 R2 R2 R2

NUREG-1032

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A-20

Group designation	Desig featu	n res*	Mean time to restore offsite power (hrs)
Il	A3 an	d (B3, B4 or B2b)	0.13
12	A3 an	d (B1 or B2a)	0.21
13	(A1 (B3) of	A2) and B4, or B2b)	0.50
I.	(A1 o (B1 o	r A2) and r B2a)	0.97
	Sta	atistical Test Valu	ies
Test	Design factor	F value	Pr F
Test for interaction	A B A*B	7.01 1.67 0.85	0.0132 0.2062 0.3637
Test for main effects	A B	6.92 2.68	0.0135 0.1125

Table A.3	Mean time	to restore offsite	power	and statistical	test values
	for plant	design groupings	C		

*A1, A2, A3, B1, B2, B3, and B4 are defined in Table A.2.

Note: Frequency of plant-centered loss-of-offsite-power events was 0.056 per site-year.

Table A.2 Definitions of offsite power system design factors

r design factor	Desi	Design features		
Independence of offsite power sources to the nuclear power plant	1.	All offsite power sources are connected to the plant through one switchyard.		
	2.)	All offsite power sources are connected to the plant through two or more switchyards, and the switchyards are electricall connected.		
	3.	All offsite power sources are connected to the plant through two or more switchyards or separate incoming transmission lines, but at least one of the AC sources is electrically independent of the others.		
Automatic and manual transfer schemes for the Class 1E buses when the normal source of AC power fails and when the backup sources of offsite power fail	1.	If the normal source of AC powe fails, there are no automatic transfers and one or more manua transfers to preferred or alter nate offsite power sources.		
	2.	If the normal source of AC powe fails, there is one automatic transfer but no manual transfer to prefer-red or alternate off- site power sources.		
		a. All of the Class 1E buses in a unit are connected to the same preferred power source after the automatic transfer of power sources.		
		b. The Class 1E buses in a unit are connected to separate offsite power sources after the auto- matic transfer of power sources.		
	3.	After loss of the normal AC power source, there is one auto matic transfer. If this source fails, there may be one or more manual transfers of power sources to preferred or alter- nate offsite power sources.		
	r design factor Independence of offsite power sources to the nuclear power plant Automatic and manual transfer schemes for the Class 1E buses when the normal source of AC power fails and when the backup sources of offsite power fail	r design factor Desi Independence of offsite power plant 1. (2.) Automatic and manual transfer schemes for the Class 1E buses when the normal source of AC power fails and when the backup sources of offsite power fail 2. (3.)		

NUREG-1032

A-6

Major design factor	Design features
	a. All of the Class 1E buses in a unit are connected to one preferred power source after the first automatic transfer.
	b. The Class 1E buses in a unit are connected to separate offsite power sources after the first automatic transfer.
	 4. If the normal source of AC power fails, there is an automatic transfer to a preferred source of power. If this preferred source of power fails, there is an automatic transfer to another source of offsite power.
	a. All of the Class 1E buses in a unit are connected to the same preferred power source after the first automatic transfer.
	b. The Class 1E buses in a unit are connected to sepa rate offsite power sources after the first automatic transfer of power sources.

Table A.2 (continued)

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Severe-weather-induced	loss-	of-offsite-power fr	equency (S)	
Frequency group (S)	Frequency of severe weather-induced loss of offsite power			
S1)	Less than 1 per 350 site-years (0.002/site-year)			
S2	<pre>> 1 per 350 site-years and < 1 per 120 site-years (0.005/site-year)</pre>			
\$3	Greater than or equal to 1 per 120 site-years (0.015/site-years)			
	Recov	ery (R)		
Recovery from severe-weather-indu loss-of-offsite-power groups (R)	ced	Recovery capabili	ty	
RI		Plant has capabil recover offsite (power to the site following a sever loss of offsite p	ity and procedures to non-emergency) AC within 2 hours e-weather-induced ower.	
R2		All other plants not in R1		
Severe-weather-induced loss-	of-of	fsite-power frequen	cy/recovery (SR)	
Severe-weather-induced loss-of- offsite-power frequency/recovery group (SR)	Frei	qwency group (S)	Recovery group (R)	
SR1 SR2 SR3 SR4 SR5 SR6	S1 S2 S3 S1 S2 S3		R1 R1 R1 R2 R2 R2 R2	

Table A.8 Severe-weather-induced loss-of-offsite-power frequency/recovery

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Frequency groups(SS)	Extremely severe-weather-induced loss-of-offsite-power frequency		
551	Less than 1 per 3500 site-years (0.0002/site-year)		
SS2	<pre>> 1 per 3500 site-years and < 1 per 1200 site-years (0.0005/site-year)</pre>		
SS3	<pre>> 1 per 1200 site-years and < 1 per 350 site-years (0.0015/site-year)</pre>		
SS4	<pre>> 1 per 350 site-years and < 1 per 120 site-years (0.005/site-year)</pre>		
\$\$5	Greater than or equal to 1 per 120 site-years (0.015/site-year)		

Table A.9 Extremely severe-weather induced loss-of-offsite-power frequency

12