



LONG ISLAND LIGHTING COMPANY

SHOREHAM NUCLEAR POWER STATION

P.O. BOX 618, NORTH COUNTRY ROAD • WADING RIVER, N.Y. 11792

JOHN D. LEONARD, JR.
VICE PRESIDENT - NUCLEAR OPERATIONS

SEP 24 1987

SNRC-1351

U. S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, D.C. 20555

I.E. Bulletin 85-03
Motor Operated Valve Common Mode Failures During
Plant Transients Due to Improper Switch Settings
Shoreham Nuclear Power Station - Unit 1
Docket No. 50-322

1987 SEP 28 A 9 55
USNRC-DS

Reference: LILCO (J. D. Leonard, Jr.) letter SNRC-1233, dated
October 8, 1986, to NRC (T. Murley)

Gentlemen:

The purpose of this letter is to update previously transmitted motor operated valve (MOV) data thereby fulfilling our commitment in the referenced letter. The attached Table 1A replaces Table 1 transmitted via the referenced letter. The original table contained data which indicated that thirteen (13) MOVs had a higher maximum expected differential pressure than those utilized in Shoreham's design basis. This data was computed using the generic Boiling Water Reactor Owner's Group (BWROG) Methodology. The attached, revised table shows that there are nine (9) MOVs with higher maximum expected differential pressures. This revised table was developed by applying plant specific criteria to the same generic BWROG methodology. An operability analysis has been performed for these nine (9) valves, and we have determined that seven (7) valves are capable of operating against the revised differential pressures after minor adjustments to torque switch settings are made. The remaining two (2) valves are presently under engineering review to determine appropriate torque switch settings.

In the referenced letter, LILCO provided a schedule to comply with the testing requirements of I.E. Bulletin 85-03. This schedule was based upon a combination of the requirements of the bulletin and the belief that Shoreham would have received its full power license on or about June 1987. Since motor operated

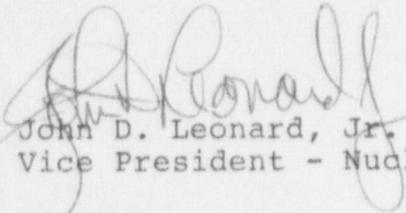
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valve dynamic testing is an integral part of the Shoreham Power Ascension Test Program (PATP), LILCO's plan was to comply with the bulletin's testing requirements through the test program. In fact, some limited motor operated valve dynamic testing has occurred (see Sections 2.4 and 4.0 of NRC Region I inspection report 50-322/87-13). However, the completion of this testing through the PATP is not going to be possible to achieve by the end of the third quarter in 1987 without a full power license. Further, LILCO presently does not expect to conduct additional low power testing before September 30, 1987. Thus, LILCO now proposes to complete the dynamic testing requirements of I.E. Bulletin on a schedule consistent with the power ascension test program.

If there are any questions or should you need additional clarification, please contact this office.

Very truly yours,



John D. Leonard, Jr.
Vice President - Nuclear Operations

TD:ck

Attachment

cc: W. Russell
C. Warren
R. Lo

Attachment to SNRC-1351
 I. E. Bulletin 85-03
 Table 1A

VALVE ID	Limitorque Valve Operator	Valve Functions	Design Differential Pressure	MAXIMUM DIFFERENTIAL PRESSURE OPENING(3)	BWROG ABNORMAL EVENTS	NOTES
1E41*MOV035 14"-900# Gate	SMB-3-100	HPCI PP DISCH	1140	1161	1164	2
1E41*MOV036 4"-900# Globe	SMB-00-10	Min Flow Bypass To Supp Pool	1200	1400	1385	2
1E41*MOV031 16"-150# Gate	SMB-0-25	HPCI Pump Suct Cond TK	35	-----	28	
1E41*MOV032 16"-150# Gate	SMB-0-25	HPCI Pump Suct Supp Pool	35	98	35	2
1E41*MOV037 8"-900# Globe	SMB-1-25	HPCI Pump Disch Cond TK	1475	-----	1385	4
1E41*MOV038 10"-900# Gate	SMB-1-40	HPCI Disch Cond TK	1475	-----	1385	4
1E41*MOV034 14"-900# Gate	SMB-2-60	HPCI Pump Disch	1140	1090	-----	
1E41*MOV039 2"-1500# Globe	SMB-000-5	HPCI Lubz Oil Cooler	250	42	43	
1E41*MOV043 10"-900# Gate	SMB-1-60	HPCI Steam To Turb	1135	1115	1115	
1E41*MOV041 10"-900 Gate	SMB-3-80	HPCI Steam To Turb	1135	1115	1115	1

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 Table 1A

VALVE ID	Limitorque Valve Operator	Valve Functions	Design Differential Pressure	ABNORMAL EVENTS		NOTES
				MAXIMUM DIFFERENTIAL PRESSURE OPENING(3)	CLOSING	
1E41*MOV042 10"-900# Gate	SMB-1-60	HPCI Steam To Turb	1135	1115	1115	1
1E41*MOV047 1"-1500# Globe	SMB-000-2	1E41*MOV041 Bypass	1050	----	1115	2, 5
1E41*MOV048 1"-1500# Globe	SMB-000-2	1E41*MOV042 Bypass	1140	----	1115	
1E41*MOV044 18"-150# Gate	SMB-0-15	Turb Exh to Supp Pool	52	----	0	
1E41*MOV049 2"-600# Globe	SMB-000-2	HPCI Turb Exh Vac Break	52	----	50	
1E51*MOV035 6"-900# Gate	SMB-00-25	RCIC Pump Disch	1300	1211	1225	
1E51*MOV036 2"-1500# Globe	SMB-000-5	Min Flow Bypass To Supp Pool	1280	1314	1314	2
1E51*MOV031 6"-150# Gate	SMB-00-5	RCIC Pump Suct Cond TK	130	----	28	
1E51*MOV032 6"-150# Gate	SMB-00-5	RCIC Pump Suct Supp Pool	130	145	35	2
1E51*MOV037 4"-900# Gate	SMB-00-10	RCIC Pump Disch To Cond Tk	1215	----	1290	2
1E51*MOV034 4"-900# Gate	SMB-00-10	RCIC Pump Disch	1300	1288	----	

Attachment to SNRC-1351
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 Table IA

VALVE ID	Limitorque Valve Operator	Valve Functions	Design Differential Pressure	MAXIMUM DIFFERENTIAL PRESSURE OPENING(3)	ABNORMAL EVENTS	NOTES
					BWROG CLOSING	
1E51*MOV038 2"-1500# Globe	SMB-000-5	RCIC Lube Oil Cooler	1300	1319	39	2
1E51*MOV046 2"-600# Globe	SMB-000-2	Vac Pump Disch To Supp Pool	60	----	35	
1E51*MOV043 3"-900# Gate	SMB-00-7.5	RCIC Steam To Turb	1135	1115	1115	
1E51*MOV041 3"-900 # Gate	SMB-00-10	RCIC Steam to Turb	1135	1115	1115	1
1E51*MOV042 3"-900# Gate	SMB-00-7.5	RCIC Steam to Turb	1135	1115	1115	1
1E51*MOV047 1"-1500# Globe	SMB-000-2	1E51*MOV041 Bypass	1050	----	1115	2, 5
1E51*MOV048 1"-1500# Globe	SMB-000-2	1E51*MOV042 Bypass	1140	----	1115	

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VALVE ID	Limitorque Valve Operator	Valve Functions	Design Differential Pressure	BWR0G ABNORMAL EVENTS		NOTES
				MAXIMUM DIFFERENTIAL PRESSURE OPENING(3)	CLOSING	
1E51*MOV045 8"-150# Gate	SMB-000-5	RCIC Turb Exh	10	-----	0	
1E51*MOV049 1.5"-600# Globe	SMB-000-2	RCIC Turb Exh Vac Break	60	-----	50	

- (1) Documentation was submitted via SNRC-1185 dated 6/28/85 to Mr. H.R. Denton to demonstrate valve would perform isolation function due to line break.
- (2) Calculated maximum differential pressure using BWR0G methodology results in a higher differential pressure than that utilized in the Shoreham design bases.
- (3) The torque switch is nonfunctional in the opening direction as it is permanently shorted out of the circuit.
- (4) Consistent with the BWR0G methodology, these valves have no active safety function because they are normally closed and open only during pump testing. These valves are presently under engineering review to resolve concerns identified during pump testing.
- (5) This 1" inboard containment isolation valve is presently under engineering review to determine appropriate torque switch settings.