Carolina Power & Light Company

Raleigh, North Carolina 27602

March 25, 1970



Dr. Peter A. Morris, Director Division of Reactor Licensing United States Atomic Energy Commission Washington, D. C. 20545

Regulatory

File Cy.

Re: Docket Nos. 50-324 and 50-325.

Dear Dr. Morris:

The Company transmits herewith additional information in support of its proposed reduction in the design pressure of the containment dry well and torus of the Brunswick units from 62 psig to 53 psig. This submittal is in response to a Staff request for specific data used in the calculation of the Brunswick containment design pressure.

In order that the engineering and construction of the Brunswick units may proceed on schedule, the Company desires to discuss this submission with the Staff at the earliest possible date.

Very truly yours,

J. A. Jones

Vice President - Power Supply

JAJ:ej



8709240386 870921 PDR FGIA MENZ87-111 PDR

In the Matter of)

CAROLINA POWER & LIGHT COMPANY)

(Brunswick Steam Electric Plant)

Units 1 and 2)

Docket Nos. 50-324 50-325

Regulatory

File Cy.

AFFIDAVIT OF J. A. JONES

Received w/Ltr Dated 3-25-70

I, J. A. Jones, being duly sworn, depose and state that I reside in Raleigh, North Carolina; that I am Vice President, Power Supply, Carolina Power & Light Company; that I am fully cognizant of the contents of the foregoing document entitled "Brunswick Containment Analysis Data", and that the contents of the same are true and correct to the best of my knowledge.

J. A. Jones

Subscribed and sworn to before me this 35 day of March, 1970, at Raleigh, North Carolina.

Marjacet M. Cox

My commission expires: July 4,1970

904

In the Matter of)

CAROLINA POWER & LIGHT COMPANY)

(Brunswick Steam Electric Plant)

Units 1 and 2)

Docket Nos. 50-324

50-325

AFFIDAVIT OF J. A. JONES

I, J. A. Jones, being duly sworn, depose and state that I reside in Raleigh, North Carolina; that I am Vice President, Power Supply, Carolina Power & Light Company; that I am fully cognizant of the contents of the foregoing document entitled "Brunswick Containment Analysis Data", and that the contents of the same are true and correct to the best of my knowledge.

J. A. Jones

Subscribed and sworn to before me this 25 day of March, 1970, at Raleigh, North Carolina.

Notary Public

BSEP 1 & 2

DOCKET NOS. 50-324 & 50-325

BRUNSWICK CONTAINMENT ANALYSIS DATA

Group 1 Data

Initial Pool Temperature	· oF	90
Initial Wetwell Air Temperature	°F	90
Initial Drywell Temperature	\circ_{F}	130
Initial Wetwell Pressure	PSIG	1.3
Initial Drywell Pressure	PSIG	1.3
Initial Wetwell Relative Humidity	%	100
Initial Drywell Relative Humidity	%	30
Downcomer Submergence	Ft.	4
Wetwell Pool Volume	Cu.Ft.	87300
Initial Reactor Power	MWT	2550
Initial Mass of Water in Reactor	Lb.	464,500
Initial Mass of Steam in Reactor	Lb.	18,200
Assume Enthalpy of Water	Btu/Lb.	545
Assumed Enthalpy of Steam	Btu/Lb.	1191

Group 2 Data

- (1) Reactor pressure versus time supplied in Table 1.
- (2) No feedwater flow assumed during blowdown. Feedwater enthalpy is less than saturated and would tend to depressurize vessel if flow included. Assuming no flow maximizes reactor pressure thereby maximizing loading on containment (effect small in any event).
- (3) Steam flow versus time provided in Table 1. This flow is handled merely as an outflow from vessel. Energy assumed dumped to main condenser.

Group 3 Data

- (1) Flow out of break provided in Table 1.
- (2) Energy rate out of break also provided in Table 1.

BSEP 1 & 2 DOCKET NOS. 50-324 & 50-325

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TABLE 1
REACTOR CHARACTERISTICS DURING BLOWDOWN

0 2513 1020 38890 545 0 1191 .944 2513 1011 38770 543 0 1191.3 1.88 2390 1002 38630 542 0 1191.6 2.82 1570 993 38480 540 0 1192 3.44 150 993 38580 542 0 1191.7 5.32 0 1008 38720 543 0 1191.4 6.57 0 1013 38790 543 0 1191.2 8.82 0 1015 38810 544 0 1191 9.88 0 1005 16660 542 6261 1191.5 11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 <	Time Sec.	Steamline Flow Lb/Sec.	Reactor Pressure PSIA	Liquid Flow Break Lb/Sec.	Liquid Enthalpy Btu/lb.	Steam Flow Break Lb/Sec.	Steam Enthalpy Btu/lb.
1.88 2390 1002 38630 542 0 1191.6 2.82 1570 993 38480 540 0 1192 3.44 150 993 38490 540 0 1192 4.07 0 999 38580 542 0 1191.7 5.32 0 1008 38720 543 0 1191.4 6.57 0 1013 38790 543 0 1191.2 8.82 0 1015 38810 544 0 1191 9.88 0 1005 16660 542 6261 1191.5 11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5 <td>0</td> <td>2513</td> <td>1020</td> <td>38890</td> <td>545</td> <td>0</td> <td>1191</td>	0	2513	1020	38890	545	0	1191
2.82 1570 993 38480 540 0 1192 3.44 150 993 38490 540 0 1192 4.07 0 999 38580 542 0 1191.7 5.32 0 1008 38720 543 0 1191.4 6.57 0 1013 38790 543 0 1191.2 8.82 0 1015 38810 544 0 1191 9.88 0 1005 16660 542 6261 1191.5 11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	.944	2513	1011	38770	543	0	1191.3
3.44 150 993 38490 540 0 1192 4.07 0 999 38580 542 0 1191.7 5.32 0 1008 38720 543 0 1191.4 6.57 0 1013 38790 543 0 1191.2 8.82 0 1015 38810 544 0 1191 9.88 0 1005 16660 542 6261 1191.5 11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	1.88	2390	1002	38630	542	0	1191.6
4.07 0 999 38580 542 0 1191.7 5.32 0 1008 38720 543 0 1191.4 6.57 0 1013 38790 543 0 1191.2 8.82 0 1015 38810 544 0 1191 9.88 0 1005 16660 542 6261 1191.5 11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	2.82	1570	993	38480	540	0	1192
5.32 0 1008 38720 543 0 1191.4 6.57 0 1013 38790 543 0 1191.2 8.82 0 1015 38810 544 0 1191 9.88 0 1005 16660 542 6261 1191.5 11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	3.44	150	993	38490	540	0	1192
6.57 0 1013 38790 543 0 1191.2 8.82 0 1015 38810 544 0 1191 9.88 0 1005 16660 542 6261 1191.5 11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	4.07	0	999	38580	542	0	1191.7
8.82 0 1015 38810 544 0 1191 9.88 0 1005 16660 542 6261 1191.5 11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	5.32	0	1008	38720	543	0	1191.4
9.88 0 1005 16660 542 6261 1191.5 11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	6.57	0	1013	38790	543	0	1191.2
11.07 0 876 13260 522 5843 1196.2 12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	8.82	0	1015	38810	544	0	1191
12.32 0 750 10460 502 5388 1200 12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	9.88	0	1005	16660	542	6261	1191.5
12.94 0 689 9221 490 5131 1201.4 15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	11.07	0	876	13260	522	5843	1196.2
15.44 0 470 5203 442 3955 1204.6 19.19 0 237 1749 372 2291 1200.5	12.32	0	750	10460	502	5388	1200
19.19 0 237 1749 372 2291 1200.5	12.94	0	689	9221	490	5131	1201.4
	15.44	0	. 470	5203	442	3955	1204.6
26.19 0 57 39 259 561 1176.6	19.19	0	237	1749	372	2291	1200.5
	26.19	0	57	39	259	561	1176.6