



*Burford*

UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

*Party Involvement -  
is this the ELO  
memo which gave  
you concern?*

October 10, 1984

*1. Davis  
2. Mueshardt  
CC: FC*

*July  
John  
3/18  
11:00*

MEMORANDUM FOR: Frank P. Gillespie, Director  
Division of Risk Analysis and Operations  
Office of Nuclear Regulatory Research

FROM: William J. Dimstead  
Director and Chief Counsel, Regulations Division  
Office of the Executive Legal Director

SUBJECT: CHEMICAL TOXICITY OF UF<sub>6</sub> AND EMERGENCY PREPAREDNESS

In your memorandum of August 23, 1984 you requested our opinion on whether NRC has the legal authority to base emergency preparedness regulations for a uranium hexafluoride (UF<sub>6</sub>) release on the chemical toxicity of the compound. It is our conclusion that the chemical toxicity of uranium compounds may be taken into consideration in developing regulations to protect the public health and safety from the radiological effects of UF<sub>6</sub>.

Although the predominant regulatory concern of the NRC for protection of public health and safety has been the radiological hazards associated with source, byproduct, and special nuclear material, under the Atomic Energy Act of 1954, as amended, Commission regulatory authority can be more extensive. The Atomic Energy Act confers broad authority to regulate the use and possession of the defined classes of nuclear materials, i.e., source, byproduct, and special nuclear, in order to protect public health, minimize danger to life or property from the hazards associated with these materials, and to prevent possession and use inimical to the common defense and security. Section 1611.(3) permits the Commission, by rule or order, to regulate any activity authorized by the Act including standards and restrictions governing the operation of facilities used in the activity. Section 161b authorizes the Commission to establish whatever regulations it deems necessary or desirable to protect health and to minimize danger to life or property with respect to the possession and use of source, byproduct, and special nuclear material. In the case of source material Section 63b(1) states that the physical characteristics of source material are to be considered in writing rules for its possession and use. The physical characteristics of source material could include both its chemical and radiological characteristics. Section 63b(1) states the same for special nuclear material. UF<sub>6</sub> can be either source material or special nuclear material depending on whether or not the uranium has been enriched. Under this broad authority the Commission has exercised regulatory authority over all integral parts of an activity for which an NRC license is required by the Atomic Energy Act. See legal opinions printed in the hearing, "Uranium Mill Tailings Control Act of 1978," before the Subcommittee on Energy and Power, Committee on Interstate and Foreign Commerce, 95th Cong. 2d Sess., June 19, 20, and August 2, 1978, at pp. 200-207.

B61014003B B61001  
PDR FOIA  
HIGUCHI86-61 PDR

Enclosure 4

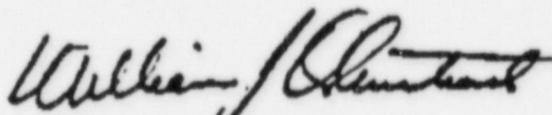
*A-5*

The chemical toxicity of uranium has already been considered in the Commission's regulations. It is our understanding that the values for soluble uranium in air in 10 CFR Part 20, Appendix B are based upon the chemical toxicity of uranium in the human kidney rather than its radiological hazard, even though the concentration limits are expressed in terms of radioactivity. See fn. 4 to Appendix B, 10 CFR Part 20, 39 F.R. 23990 (June 28, 1974). These values would apply to a release of  $UF_6$  that on contact with air hydrolyzes to  $UO_2F_2$ , a compound very soluble in body fluids which would be absorbed into the blood via the lungs.

As a supplement to the Atomic Energy Act, the National Environmental Policy Act of 1969 (NEPA) also supports the establishment of regulations for protection of public health, safety and the environment from other hazardous materials produced in the course of using source, byproduct, or special nuclear material. Calvert Cliff's Coordinating Committee v. AEC, 449 F.2d 1109 (D.C. Cir. 1971) imposed upon the Commission an obligation not only to consider environmental concerns, radiological and nonradiological, but also to take action to mitigate adverse impacts. Ibid p. 1128. See also, Public Service Co v. NRC, 582 F.2d 77 (1st Cir. 1978) (Commission has jurisdiction under Atomic Energy Act to order rerouting of transmission lines to minimize adverse environmental impacts). To implement NEPA objectives in individual licensing actions involving possession and use of  $UF_6$  (both natural and enriched), NRC licenses are already routinely conditioned under Atomic Energy Act authority to require monitoring of emissions of other fluoride compounds such as  $HF$ , and the keeping of monitoring records. However, to avoid dual regulation of such other fluoride compounds, enforcement of violations of Clean Air Act health standards revealed by such monitoring is left to the States, or EPA, as appropriate.

- 1/ Personal communication from Ralph G. Page, Chief, Uranium Fuel Licensing Branch, Division of Fuel Cycle and Material Safety, OMS&S
- 2/ Chemical damage to the kidney sets the basis for bioassay (urinalysis) in uranium mills. See Regulatory Guide 8.22. It is also a factor in the general bioassay program in Regulatory Guide 8.11, in the health physics survey described in Regulatory Guide 8.24, and in the ALARA program for uranium mills in Regulatory Guide 8.31.
- 3/ 40 CFR 190, which was promulgated by EPA under Atomic Energy Act authority, sets the standard for environmental releases of uranium only with respect to radiological consequences. EPA authority under the Atomic Energy Act to establish generally applicable environmental protection standards for uranium does not limit the authority of the NRC to establish specific regulations for emergency preparedness by persons possessing and using  $UF_6$ . The latter is a matter of regulating directly the licensed activities of persons under the Atomic Energy Act.

It is clear from the preceding discussion that licenses are not infrequently conditioned under Atomic Energy Act authority to regulate non-radiological concerns related to the use of source, byproduct, and special nuclear materials. Because the Atomic Energy Act allows regulation by rule on an equal basis to regulation by license condition, it is our opinion that a rule under Atomic Energy Act authority for emergency preparedness for licensees possessing and using UF<sub>6</sub> may be based upon its chemical toxicity as well as its radiological characteristics.



William J. Gilmstead  
Director and Chief Counsel  
Regulations Division  
Office of the Executive  
Legal Director

6 January 1994

MEMORANDUM

SUBJECT: ARAO ASSUMPTIONS ASSOCIATED WITH GORE OF INCIDENT CALCULATIONS.

RELEASE START: 1100CST (1730GMT)  
DURATION: 15 MINUTES

CENTROID OF RELEASE CLOUD AT HGT OF 8 METRES AGL

RELEASE AMOUNT = 24,800 LBS (11257 KG) OF UF<sub>6</sub>  
YIELDING 11,700 KG OF UO<sub>2</sub>F<sub>2</sub> (URANYL FLUORIDE) AND 3040 KG HF. THIS IS BASED ON THE FOLLOWING:

UF<sub>6</sub> + 2(H<sub>2</sub>O) --> (UO<sub>2</sub>F<sub>2</sub>) + 4(HF) + heat

THE RELEASE RATE WAS ASSUMED TO BE CONSTANT OVER THE DURATION OF THE RELEASE.

THE HF WAS MODELED AS VAPOR WITH A 1 CM/S DEPOSITION VELOCITY.

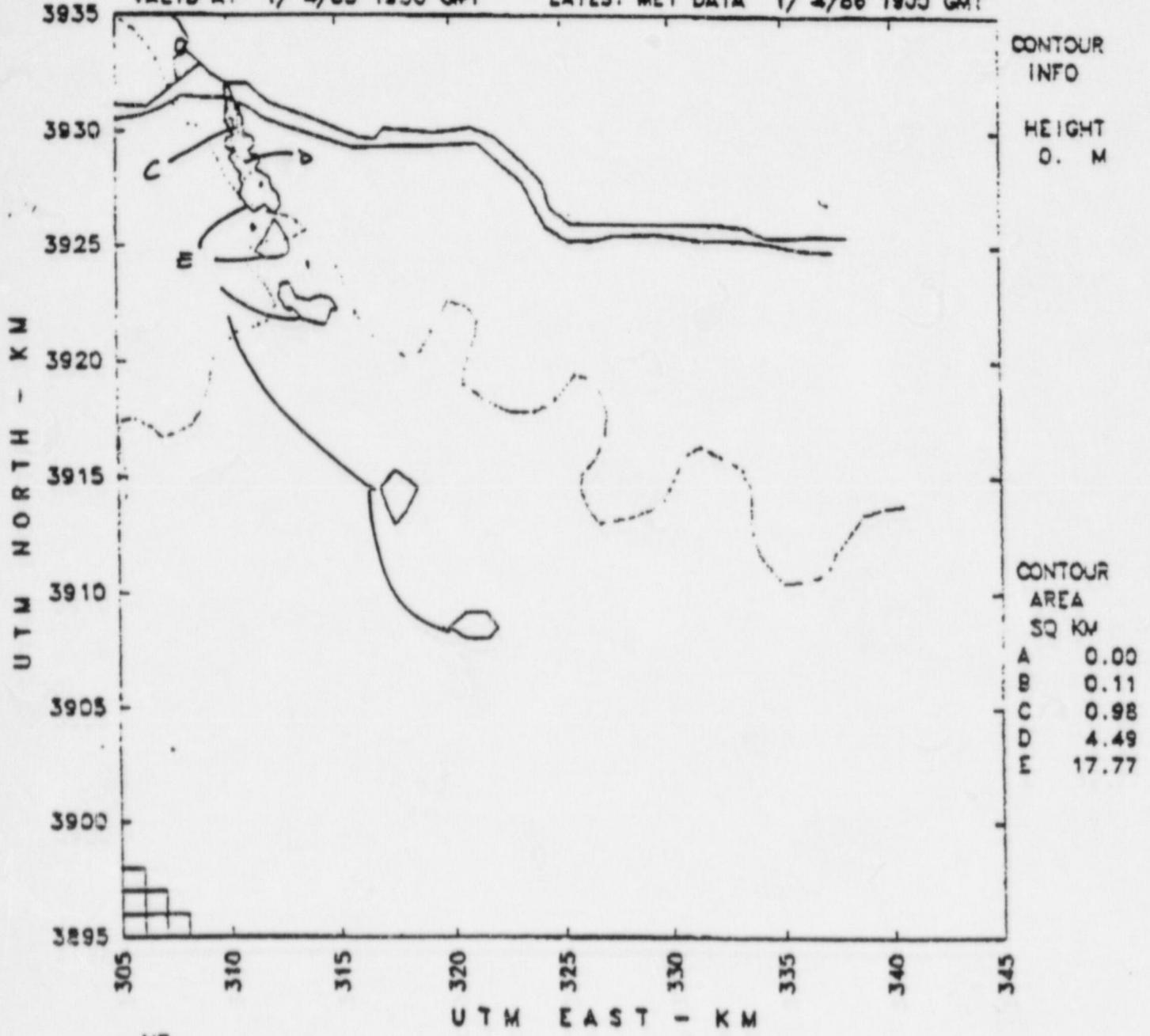
THE UO<sub>2</sub>F<sub>2</sub> WAS MODELED AS PARTICLES WITH A MEDIAN DIAMETER OF ONE MICRON, A STANDARD GEOMETRIC DEVIATION OF 1.5 MICRONS, A MAXIMUM DIAMETER OF 3.0 MICRONS AND A MINIMUM DIAMETER OF 0.31 MICRONS AND A DEPOSITION VELOCITY OF 1 cm/s.

PLEASE NOTE THAT FIGS 3 AND 4 ARE EXPANDED VIEWS OF FIGS 1 AND 2. THE COMPUTATIONAL GRID WAS THE SAME, I.E. 40KM X 40KM WITH A DELTA X AND DELTA Y OF 1KM, AND DELTA Z OF 50 M.

A-6

Rev 1/7/86  
0845

SEQUOYAH FUELS CORP. RELEASE  
VALID AT 1/4/85 1930 GMT LATEST MET DATA 1/4/86 1900 GMT

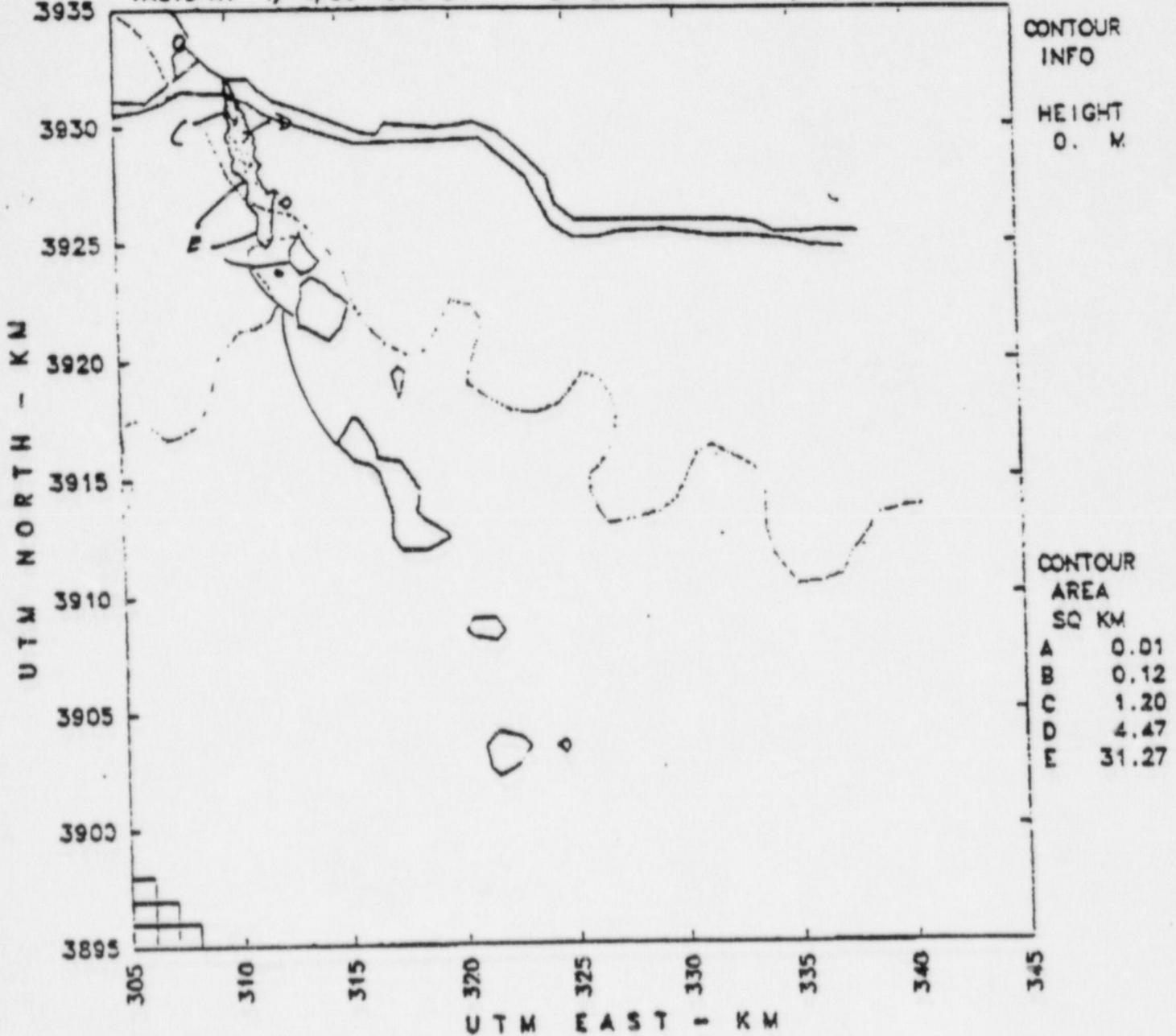


HF  
DEPOSITION FROM 1/4/85 1730 GMT TO 1/4/85 1930 GMT  
CUMULATIVE DEPOSITION  
PROBLEM START 1/4/85 1730 GMT MAXIMUM VALUE 1.08E+01

Fig. 1

1/11/85  
0925

SEQUOYAH FUELS CORP. RELEASE  
VALID AT 1/4/85 1930 GMT      LATEST MET DATA 1/4/86 1900 GMT



UO2F2  
DEPOSITION FROM 1/4/85 1730 GMT TO 1/4/85 1930 GMT  
CUMULATIVE DEPOSITION  
PROBLEM START 1/4/85 1730 GMT      MAXIMUM VALUE 3.97E+01

Fig. 2

7 January 1985

SUBJECT: ARAC NORMALIZED CALCULATION INPUT PARAMETERS

The parameters which are different from the previous ARAC calculations (those which used 29,500 pounds of UF6 as the source) are as follows:

- 1) Initial cloud size determined from building dimensions (250' by 78').
- 2) Used 1 gram of HF and 1 gram of UO2F2 each released over the 15 minute plume duration.
- 3) Computational grid is now 10 by 10 kilometers with 50 meter delta Z. (Delta X and Delta Y equal 250 meters.)
- 4) Source location shifted to the East closer to highway 10.

All other assumptions listed in yesterday's memo were used for this run.

7 January 1986  
22:00 GMT

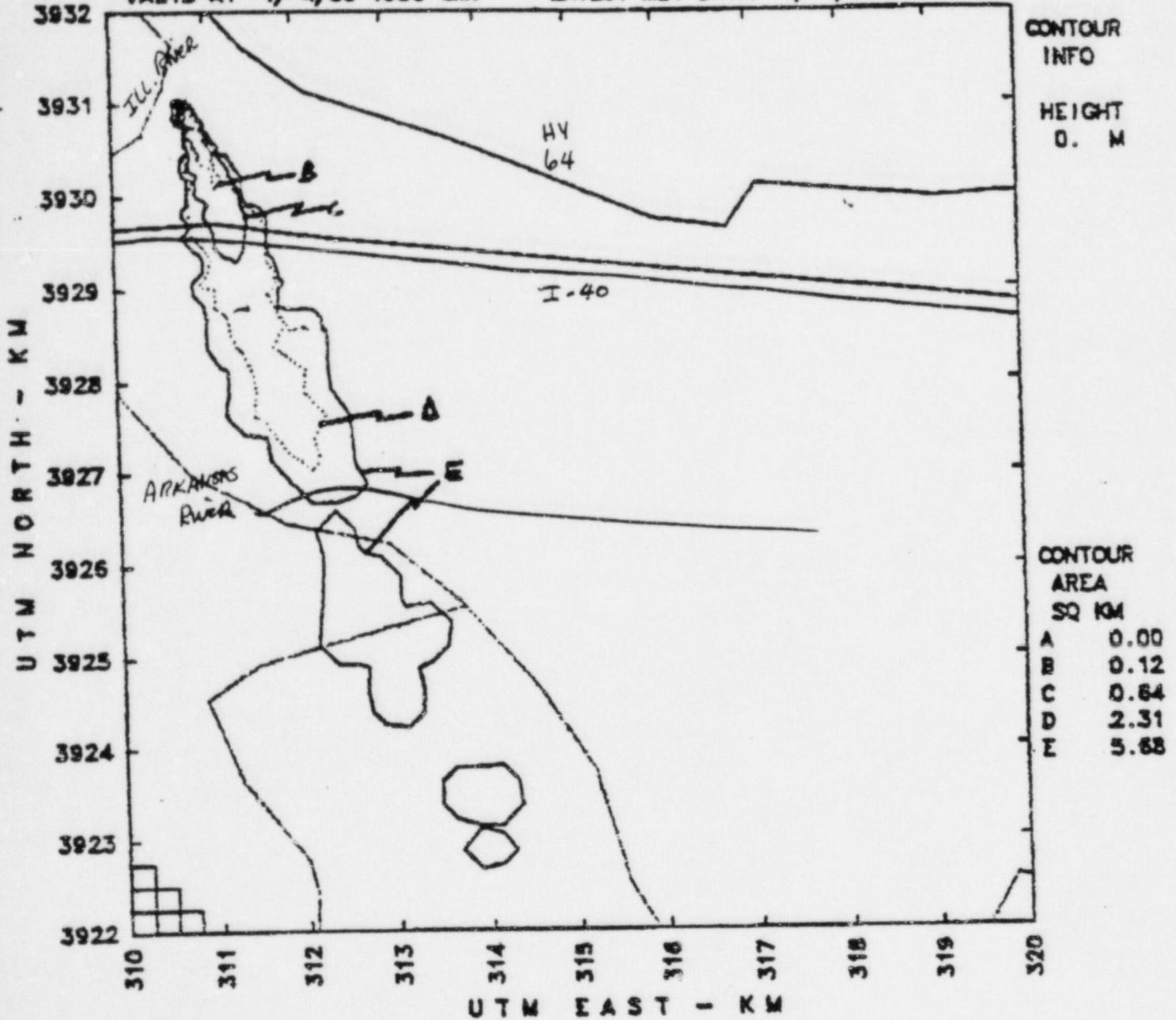
Subject: Additional ARAC Plots

Four additional ARAC plots are being sent:

- 1) Cumulative Deposition contours of UO<sub>2</sub>F<sub>2</sub> assuming maximum source amount (11,788 kg of UO<sub>2</sub>F<sub>2</sub>) on a 10 kilometer by 10 kilometer map.
- 2) Cumulative Deposition contours of HF assuming maximum source amount (3,848 kg of HF) on a 10 kilometer by 10 kilometer map.
- 3) Integrated Normalized Air Concentration contours of UO<sub>2</sub>F<sub>2</sub> on a 40 kilometer by 40 kilometer map.
- 4) Integrated Normalized Air Concentration contours of HF on a 40 kilometer by 40 kilometer map.

To convert normalized contour values of plots 3 and 4 to actual values, multiply the values by the total mass released over the assumed 15 minute release period.

SEQUOYAH FUELS CORP. RELEASE  
 VALID AT 1/ 4/85 1930 GMT LATEST MEY DATA 1/ 4/86 1900 GMT



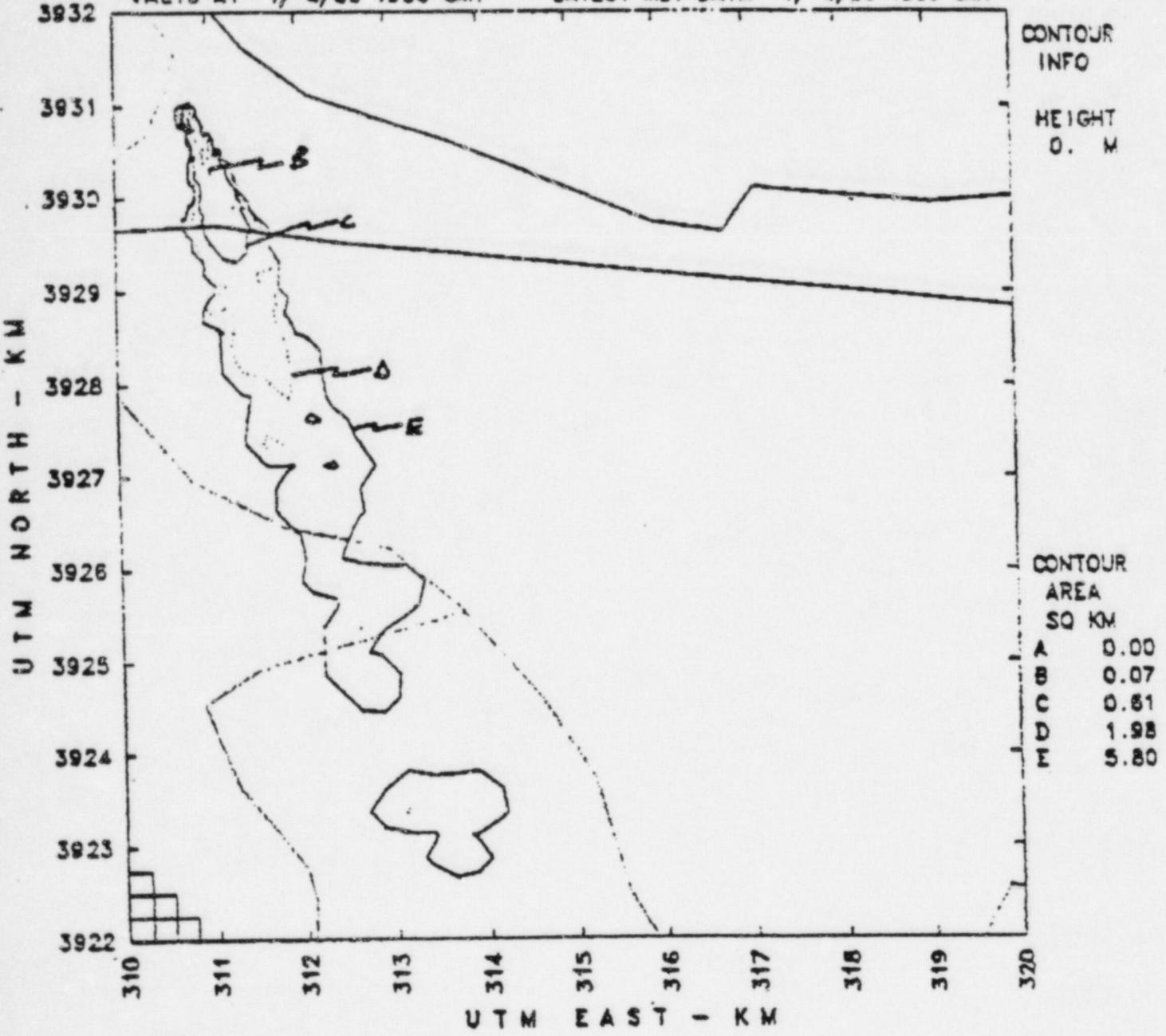
UO2F2  
 DEPOSITION FROM 1/ 4/85 1730 GMT TO 1/ 4/85 1930 GMT  
 MAX SOURCE CUMULATIVE DEPOSITION  
 PROBLEM START 1/ 4/85 1730 GMT

MAXIMUM VALUE 3.76E+01

SEQUOYAH FUELS CORP. RELEASE

VALID AT 1/4/85 1930 GMT

LATEST MET DATA 1/4/86 1900 GMT



HF  
 DEPOSITION FROM 1/4/85 1730 GMT TO 1/4/85 1930 GMT  
 MAX SOURCE CUMULATIVE DEPOSITION  
 PROBLEM START 1/4/85 1730 GMT

MAXIMUM VALUE 1.18E+01

Want  
for  
Samples

1/4/86

0001 1/4/86 0800  
0800 1/4/86 1600

1600  
2400

Reported values are the fraction of the restricted MPC ( $1 \times 10^{-10}$  uCi/ml)

Category	Location	Value	0001 1/4/86 0800	0800 1/4/86 1600	1600	2400
SAMPLING	1 South Wall, 1st	0.09	/	/	/	/
	2 Splitter, 2nd	0.11	/	/	/	/
	3 Splitter, 3rd	0.11	/	/	/	/
	4 Drum Dumper, 4th	0.12	/	/	/	/
	5 Sample Prep Room	0.10	/	/	/	/
DIGEST	6 Center, 1st	0.12	/	/	/	/
	7 East Walkway, 2nd	0.10	/	/	/	/
	8 #3 Digester, -2nd	0.13	/	/	/	/
DECONTAMINATION	10 N. End #1, -1st	0.08	/	/	/	/
	38 Between #3 & #4, 1st	0.11	/	/	/	/
	39 W. #3 Boildown Tank, 1st	0.06	/	/	/	/
	11 W. Side #2, 2nd	0.10	/	/	/	/
	12 E. Side #2, 2nd	0.14	/	/	/	/
REDUCTION-HYDROFLUORINATION	40 Between #3 & #4, 2nd	0.13	/	/	/	/
	13 A-Reactor Blower, 1st	0.09	/	/	/	/
	41 B-Reduction Reactor, 1st	0.11	/	/	/	/
	14 A Backup Filters, 2nd	0.15	/	/	/	/
	42 B-Line, 2nd	0.12	/	/	/	/
	15 A-Line HF CUR, W., 4th	0.12	/	/	/	/
	16 UO2 Seal Bin, E., 4th	0.15	/	/	/	/
	43 B-Line, 3rd	0.17	/	/	/	/
	17 2nd Stage HFR, 3rd	0.15	/	/	/	/
	18 N. of UO3 Pulverizer, 3rd	0.11	/	/	/	/
FLUORINATION	44 B-Line HFR CUR, S., 4th	0.17	/	/	/	/
	19 AHF Furnace, 1st	0.11	/	/	/	/
	20 511 Conveyor, S., 4th	0.15	/	/	/	/
	21 511 Conveyor, NE., 4th	0.12	/	/	/	/
	22 #5 Tower, 1st	0.10	/	/	/	/
	23 #3 Tower, 1st	0.13	/	/	/	/
	24 F2 Heater #1, W., 2nd	0.37	/	/	/	/
	25 F2 Heater #3, NW., 2nd	0.12	/	/	/	/
	26 #5 Tower, S., 2nd	0.10	/	/	/	/
	27 Cold Trap #2, E., 3rd	0.08	/	/	/	/
MISCELLANEOUS	28 Cold Trap #2, W., 3rd	0.11	/	/	/	/
	29 Feed Bin #3, 3rd	0.12	/	/	/	/
	30 Feed Bin Center, 3rd	0.11	/	/	/	/
	36 LF6 Scale Room	0.22	/	/	/	/
	37s Decon Room, South	0.57	/	/	/	/
	37w Decon Room, West	0.40	/	/	/	/
	32 Maint. Shop, SE.	0.15	/	/	/	/
	45 Maint. Shop, West	0.11	/	/	/	/
MISC DIGEST	34 #1 F2 Plant	0.07	/	/	/	/
	35 Cell Reword Area	0.08	/	/	/	/
	46 #2 F2 Plant	0.09	/	/	/	/
ASH REEL	47 N. Side Dumping Station, 3rd		/	/	/	/
	48 S. Side Dumping Station, -3rd		/	/	/	/
	49 Drum Filling Station, 1st		/	/	/	/
	50 Ash Receiver DeSrooke House	0.50	/	/	/	/

Contamination Incident Report required for restricted area concentrations  $> 3 \times 10^{-10}$  uCi/ml

A  
A

JCS

Plant  
Air  
Samples

1/4/86

0800 1/4/86 1600 1/4/86 2000 1/4/86  
 1000 1/4/86 3000 1/4/86 2400 1/4/86

Reported values are the fraction of the restricted MDC ( $1 \times 10^{-10}$  uCi/ml)

Sample No.	Location	0800	1600	2000
1	South Wall, 1st		0.25	0.10
2	Splitter, 2nd		0.20	0.13
3	Splitter, 3rd		0.21	0.14
4	Drum Dumper, 4th		0.25	0.15
5	Sample Prep Room		0.20	0.21
6	Center, 1st		0.12	0.17
7	East Walkway, 2nd		0.11	0.17
8	#3 Digester, -2nd		0.14	0.20
10	N. End #1, -1st		0.07	0.10
88	Between #3 & #4, 1st		0.09	0.11
39	W. #3 Boildown Tank, 1st		0.08	0.16
11	W. Side #2, 2nd		0.09	0.17
12	E. Side #2, 2nd		0.12	0.12
40	Between #3 & #4, 2nd		0.17	0.10
13	A-Reactor Blower, 1st		0.10	0.18
41	B-Reduction Reactor, 1st		0.14	0.14
14	A Backup Filters, 2nd		0.19	0.11
42	B-Line, 2nd		0.08	0.15
15	A-Line HF CUR, W., 4th		0.12	0.06
16	UO2 Seal Bin, E., 4th		0.19	0.17
43	B-Line, 3rd		0.22	0.23
17	2nd Stage HFR, 3rd		0.11	0.08
18	N. of UO3 Pulverizer, 3rd		0.11	0.08
44	B-Line HFR CUR, S., 4th		0.14	0.14
19	AHF Furnace, 1st		0.18	0.12
20	511 Conveyor, S., 4th		2.30	1.60
21	511 Conveyor, NE., 4th		0.86	0.89
22	#5 Tower, 1st		0.17	0.25
23	#3 Tower, 1st		0.41	0.52
24	F2 Heater #1, W., 2nd		0.21	0.13
25	F2 Heater #3, NW., 2nd		0.10	0.11
26	#5 Tower, S., 2nd		0.30	0.48
27	Cold Trap #2, E., 3rd		0.24	0.14
28	Cold Trap #2, W., 3rd		0.19	0.16
29	Feed Bin #3, 3rd		1.20	1.80
30	Feed Bin Center, 3rd		0.68	1.18
36	UF6 Scale Room		0.13	0.29
37s	Decon Room, South		0.10	0.10
37w	Decon Room, West		0.10	0.08
32	Maint. Shop, SE.		0.22	0.20
45	Maint. Shop, West		0.19	0.16
34	#1 F2 Plant		0.11	0.10
35	Cell Keyword Area		0.13	0.19
46	#2 F2 Plant		0.06	0.12
47	N. Side Dumping Station, 3rd			
48	S. Side Dumping Station, 3rd			
49	Drum Filling Station, 1st			
50	Ash Receiver DeSmoke House		0.30	0.34

Contamination Incident Report required for restricted area concentrations  $> 3 \times 10^{10}$  uCi/ml

JCS  
1/4/86

Plant Air Samples	1/5/86	0001 1/5/86	0800 1/5/86	1600 1/5/86	2400 1/5/86
Reported values are the fraction of the restricted MPC ( $1 \times 10^{-10}$ $\mu\text{Ci}/\text{ml}$ )					
1	South Wall, 1st	0.07	0.05		
2	Splitter, 2nd	0.09	0.08		
3	Splitter, 3rd	0.09	0.08		
4	Drum Dumper, 4th	0.08	0.13		
5	Sample Prep Room	0.08	0.11		
6	Center, 1st	0.16	0.12		
7	East Walkway, 2nd	0.07	0.06		
8	#3 Digester, -2nd	0.10	0.08		
10	N. End #1, 1st	0.05	0.04		
38	Between #3 & #4, 1st	0.07	0.03		
39	W. #3 Boil-down Tank, 1st	0.09	0.04		
11	W. Side #2, 2nd	0.08	0.06		
12	E. Side #2, 2nd	0.10	0.06		
40	Between #3 & #4, 2nd	0.10	0.04		
13	A-Reactor Blower, 1st	0.08	0.03		
41	B-Reduction Reactor, 1st	0.13	0.05		
14	A Backup Filters, 2nd	0.09	0.04		
42	B-Line, 2nd	0.10	0.05		
15	A-Line HF CUR, W., 4th	0.06	0.04		
16	UD2 Seal Bin, E., 4th	0.18	0.08		
43	B-Line, 3rd	0.18	0.13		
17	2nd Stage HFR, 3rd	0.10	0.07		
18	N. of UD3 Pulverizer, 3rd	0.04	0.04		
44	B-Line HFR CUR, S., 4th	0.08	0.05		
19	AHF Furnace, 1st	0.09	0.05		
20	511 Conveyor, S., 4th	0.69	0.37		
21	511 Conveyor, NE., 4th	0.13	0.24		
22	#5 Tower, 1st	0.09	0.26		
23	#3 Tower, 1st	0.31	0.12		
24	F2 Heater #1, W., 2nd	0.11	0.06		
25	F2 Heater #3, NW., 2nd	0.12	0.15		
26	#5 Tower, S., 2nd	0.09	0.41		
27	Cold Trap #2, E., 3rd	0.12	0.09		
28	Cold Trap #2, W., 3rd	0.09	0.24		
29	Feed Bin #3, 3rd	0.30	0.40		
30	Feed Bin Center, 3rd	0.24	0.20		
36	UF6 Scale Room	0.09	0.09		
37s	Decon Room, South	0.06	0.03		
37w	Decon Room, West	0.08	0.04		
32	Maint. Shop, SE.	0.11	0.10		
45	Maint. Shop, West	0.11	0.02		
34	#1 F2 Plant	0.10	0.08		
35	Cell Reword Area	0.08	0.03		
46	#2 F2 Plant	0.06	0.09		
47	N. Side Dumping Station, 3rd				
48	S. Side Dumping Station, 3rd				
49	Drum Filling Station, 1st				
50	Ash Receiver DeSmoke House	0.15	0.22		

NRC

Daily Air Monitoring Report

0001 1/16 0800 1/16 1600 1/16-86  
 0800 1/16 1600 1/16 2400 1/16-86

NRC

1	SAMPLING	South Wall, 1st	.06	.07	.06
2		Splitter, 2nd	.08	.08	.05
3		Splitter, 3rd	.08	.12	.07
4		Drum Dumper, 4th	.07	.07	.09
5		Sample Prep Room	.09	.09	.03
6	DIGEST	Center, 1st	.12	.12	.12
7		East Walkway, 2nd	.06	.04	.03
8		#3 Digester, 2nd	.10	.09	.07
10	DETRITATION	N. End #1, 1st	.09	.03	.05
38		Between #3 & #4, 1st	.06	.03	.05
39		W. #3 Boil-down Tank, 1st	.04	.09	.05
11		W. Side #2, 2nd	.03	.05	.04
12		E. Side #2, 2nd	.08	.07	.05
40	Between #3 & #4, 2nd	.05	.05	.03	
13	REDUCTION-HYDROFLUORINATION	A-Reactor Blower, 1st	.07	.04	.03
41		B-Reduction Reactor, 1st	.08	.04	.06
14		A Backup Filters, 2nd	.05	.06	.03
42		B-Line, 2nd	.08	.06	.05
15		A-Line HF CUR, W., 4th	.09	.02	.02
16		UO2 Seal Bin, E., 4th	.10	.07	.09
43		B-Line, 3rd	.15	.13	.11
17		2nd Stage HFR, 3rd	.06	.06	.04
18		N. of UO3 Pulverizer, 3rd	.05	.05	.03
44		B-Line HFR CUR, S., 4th	.08	.04	.03
19	AHF Furnace, 1st	.05	.05	.04	
20	FLUORINATION	511 Conveyor, S., 4th	.27	.22	.13
21		511 Conveyor, NE., 4th	.06	.07	.01
22		#5 Tower, 1st	.05	.05	.04
23		#3 Tower, 1st	① 1.10	1.02	.77
24		F2 Heater #1, W., 2nd	.08	.05	.06
25		F2 Heater #3, NW., 2nd	.07	.07	.03
26		#5 Tower, S., 2nd	.06	.05	.02
27		Cold Trap #2, E., 3rd	.06	.04	.05
28		Cold Trap #2, W., 3rd	.06	.07	.04
29		Feed Bin #3, 3rd	.28	.28	.12
30	Feed Bin Center, 3rd	.27	.25	.23	
36	MISCELLANEOUS	UF6 Scale Room	.06	.07	.04
37s		Decon Room, South	.03	.04	.02
37w		Decon Room, West	.07	.04	.02
32		Maint. Shop, SE.	.10	.06	.06
45		Maint. Shop, West	.08	.05	.07
34		#1 F2 Plant	.06	.04	.03
35		Cell Keyward Area	.07	.05	.04
46		#2 F2 Plant	.10	.18	.01
47	MISC DIGEST	N. Side Dumping Station, 3rd			
48		S. Side Dumping Station, 3rd			
49		Drum-Filling Station, 1st			
50	ASH REL	Ash Receiver DeSmoke House			
			.14	.12	.09

Process  
air  
Samples

1-7-86

0001 117 0800 117 1600 117  
0800 117 1600 117 2400 117

11/8/86  
14.30  
by: *[Signature]*  
To: *[Signature]*  
*[Signature]*  
*[Signature]*

*[Handwritten initials in a circle]*

1	SAMPLING	South Wall, 1st	.06	.17	.06
2		Splitter, 2nd	.05	.10	.07
3		Splitter, 3rd	.08	.15	.08
4		Drum Dumper, 4th	.08	.14	.06
5		Sample Prep Room	.05	.05	.04
6	DIGEST	Center, 1st	.11	.14	.12
7		East Walkway, 2nd	.06	.07	.05
8		#3 Digester, 2nd	.06	.09	.07
10	DECONTAMINATION	N. End #1, 1st	.03	.04	.04
38		Between #3 & #4, 1st	.05	.12	.03
39		W. #3 Boildown Tank, 1st	.04	.07	.05
11		W. Side #2, 2nd	.03	.04	.04
12		E. Side #2, 2nd	.04	.07	.06
40		Between #3 & #4, 2nd	.05	.05	.04
13	REDUCTION-HYDROFLUORINATION	A-Reactor Blower, 1st	.02	.05	.07
41		B-Reduction Reactor, 1st	.03	.04	.06
14		A Backup Filters, 2nd	.05	.05	.05
42		B-Line, 2nd	.07	.08	.06
15		A-Line HF CUR, W., 4th	.02	.03	.02
16		UO2 Seal Bin, E., 4th	.03	.08	.03
43		B-Line, 3rd	.04	.06	.08
17		2nd Stage HFR, 3rd	.04	.03	.05
18		N. of UO3 Pulverizer, 3rd	.04	.03	.03
44		B-Line HFR CUR, S., 4th	.06	.05	.04
19	FLUORINATION	AHF Furnace, 1st	.03	.06	.07
20		511 Conveyor, S., 4th	.05	.06	.08
21		511 Conveyor, NE., 4th	.03	.05	.07
22		#5 Tower, 1st	.02	.03	.04
23		#3 Tower, 1st	.05	.06	.07
24		F2 Heater #1, W., 2nd	.05	.05	.09
25		F2 Heater #3, NW., 2nd	.02	.06	.06
26		#5 Tower, S., 2nd	.05	.08	.07
27		Cold Trap #2, E., 3rd	.04	.07	.07
28		Cold Trap #2, W., 3rd	.04	.05	.04
29	MISCELLANEOUS	Feed Bin #3, 3rd	.03	.08	.06
30		Feed Bin Center, 3rd	.03	.06	.06
36		UF6 Scale Room	.04	.07	.07
37s		Decon Room, South	.02	.05	.04
37w		Decon Room, West	.03	.06	.04
32		Maint. Shop, SE.	.07	.09	.19
45	MISC DIGEST	Maint. Shop, West	.06	.07	.09
34		#1 F2 Plant	.05	.07	.07
35		Cell Rework Area	.03	.04	.06
46		#2 F2 Plant	.05	.06	.08
47	ASH REEL	N. Side Dumping Station, 3rd			
48		S. Side Dumping Station, 3rd			
49		Drum Filling Station, 1st			
50		Ash Receiver DeSmoke House	.14	.17	.14

Contamination Incident Report required for restricted area concentrations > 3 x 10<sup>10</sup> uCi/ml

1/11/86  
1522-  
by: [unclear]  
To: S. Emerson  
B. [unclear]  
J. [unclear]

CA 196  
Served on 1/4/86

HWY - 10 - 1300 - 1315

1/4/86 KHL  
Direct & ym

North of I/40 Bridge	-	200
1/2 to plant	-	200
South Gate lot highway Island	-	200

H-9

I-40 South <sup>EAST BOUND</sup> Direct  $\alpha$  cpm  
 on Ramp to I-40 (1/2 mile)  
 1-4-86  
 1300-1330  
 (Intersect)

1/4	-	< 200
1/2	-	< 200
1 mile	-	< 200
1 1/2 mile	-	< 200
2 mile	-	< 200
2 1/2 mile	-	< 200

I-40 North <sup>WEST BOUND (ON RAMP - WEST)</sup>  
 OFF RAMP  $\alpha$

	-	< 200
1	-	< 200
1 1/2	-	< 200
2	-	< 200
2 1/2 mile	-	< 200

I-40 North - WEST OF (20) - 1/2 mile < 200

I-40 South - WEST OF (40)  
 1/2 mile - < 200

Sequoyah Facility Direct and Smear Survey

Date 1-4-85

KO'S - END

Location	Direct-dpm 59 cm <sup>2</sup>	Smear-dpm 100 cm <sup>2</sup>	Direct-dpm 59 cm <sup>2</sup>	Smear-dpm 100 cm <sup>2</sup>
LOBBY CARPET	400	1200	IVCRETIA OFFICE - FLOOR	600
DESK AT DOOR		200	CONTROL ROOM - WEST CONTROL PANEL	1400
MODEL DESK		200	" FLOOR NORTH	200
COMPUTER ROOM WINDOW		300	" EAST CONTROL PANEL	400
TELEPHONE DESK		500	INSTRUMENT SHOP TABLE	200
BRANCH ROOM FLOOR		600	" FLOOR AT DESK	800
WIMBLES STANGE ROOM ENTRANCE		900	ENGINEER OFFICE - CABOLS DESK	800
HP OFFICE BACK FLOOR	600	1100	STAIRWAY TO FILE ROOM	1800
HP OFFICE SINK		400	FILE ROOM TABLE	600
MENS CHANGE ROOM ENTRANCE	South	500	OUTSIDE FILE ROOM - WEST	700
MENS CHANGE ROOM - TOP OF LOCKER		400		600
" " MILARA		600		
" " FLOOR AT SINK		< 200		
" " GENERAL		1200		
XEROX ROOM - TOP OF FILE CABINET		1300		
FLOOR		200		
TOP OF BULLETIN BOARD		500		
FRONT LAB BENCH		500		
LAB AILE'S DESK		500		
SWANBY'S DESK	1" x 2500	700		
LAB BENCH AT OVEN		700		
ASRAY LAB WEST BENCH	2100	1000		
WEST LAB NORTH BENCH		1100		
COMPUTER ROOM	2900	1300		
STAIRWAY - AT SMALL DOOR	2300	200		
IVCRETIA'S OFFICE - DESK		600		

\* These areas require cleaning.  
\*\* Indicates general area.



~~270-2909~~

~~PROCEDURES~~ PROCEDURES RELATIVE IS UF<sub>6</sub> PROCESS

HP-8 = IN-PLANT AIR SAMPLING (INTERNAL EXPOSURE ESTIMATE)

ACCT-1 = PROCEDURE FOR UF<sub>6</sub> INVENTORY DAILY REPORT

ACCT-7 = RECEIVING UF<sub>6</sub> CYLINDERS

ACCT-8 = PREPARING UF<sub>6</sub> CYLINDERS FOR SHIP

ACCT-9 = SHIPPING UF<sub>6</sub>

EMERGENCY INSTRUCTIONS

E-008 = EMERGENCY PROCEDURE FOR UF<sub>6</sub> RELEASE  
PROCESS INSTA.

N-270-3 = SECONDARY COLD TRAP OPERATION

N-270-4 = PRIMARY COLD TRAP OPERATION

N-270-5 = EMERGENCY DUMP TANK

N-270-7 = CLEAN UP REACTOR

N-270-8 = FLUORINATION TOWER OPERATION

N-270-10 = ASH GRINDING

N-270-11 = MOVING UF<sub>6</sub> SCALE CARTS

N-280-1 = UF<sub>6</sub> PRODUCT HANDLING AND SHIPPING

N-290-3 = UF<sub>6</sub> CYLINDER WASHING, INSPECTING + HYDROSTATIC TESTS

QUALITY ASSURANCE

QA-001 = QUALITY ASSURANCE FOR UF<sub>6</sub> SHIPPING CYLINDERS

QA-002 = INSPECTION - UF<sub>6</sub> CYLINDERS

A-9

Data for Cylinder  
Filled with  $UF_6$

A-1

FIG. 1:  $UF_6$  Solid,  $\rho(T)$  from NUREG/CR-4360, VI, 9/85

$UF_6$  Liquid,  $\rho(T)$  from ORO-651, Rev 4

$\rho$  of HF liq,  $\rho_2(T)$  generated from:

$$\frac{(\rho_s - \rho_v)_1}{(\rho_s - \rho_v)_2} = \left( \frac{T_c - T_2}{T_c - T_1} \right)^{1/3}$$

Perry & Chilton, Chemical Engineers Handbook, 5th Ed., 3-230

and

$T_c = \text{crit. Temp HF} = 188^\circ\text{C} = 370^\circ\text{F}$

condition 1 at b.p. HF

$T_{b.p.} = 19.54^\circ\text{C} = 67.2^\circ\text{F}$  @  $S.G. = 99$

$\therefore \rho_{b.p.} = 61.7 \text{ lb/ft}^3$ ;  $\rho_{v1} = \rho_{v2} = 0$  (assumed)

$$\rho_s = 300 - 0.18 T (^\circ\text{F})$$

: Data from

CRC, Handbook of Chemistry and Physics, 60th Ed.

NUREG/CR-4360, VI § 2.1.3

FIG 2. Volume of mix calculated at Temp. by assigning HF wt. Fract,  $x$ ; therefore  $UF_6$  wt fract =  $1-x$  (2 comp. sys.).

Volume of HF then,  $\tilde{V}_{HF} = W_T x / \rho_{HF}(T)$ ,  $\tilde{V}_{UF_6} = W_T (1-x) / \rho_{UF_6}(T)$

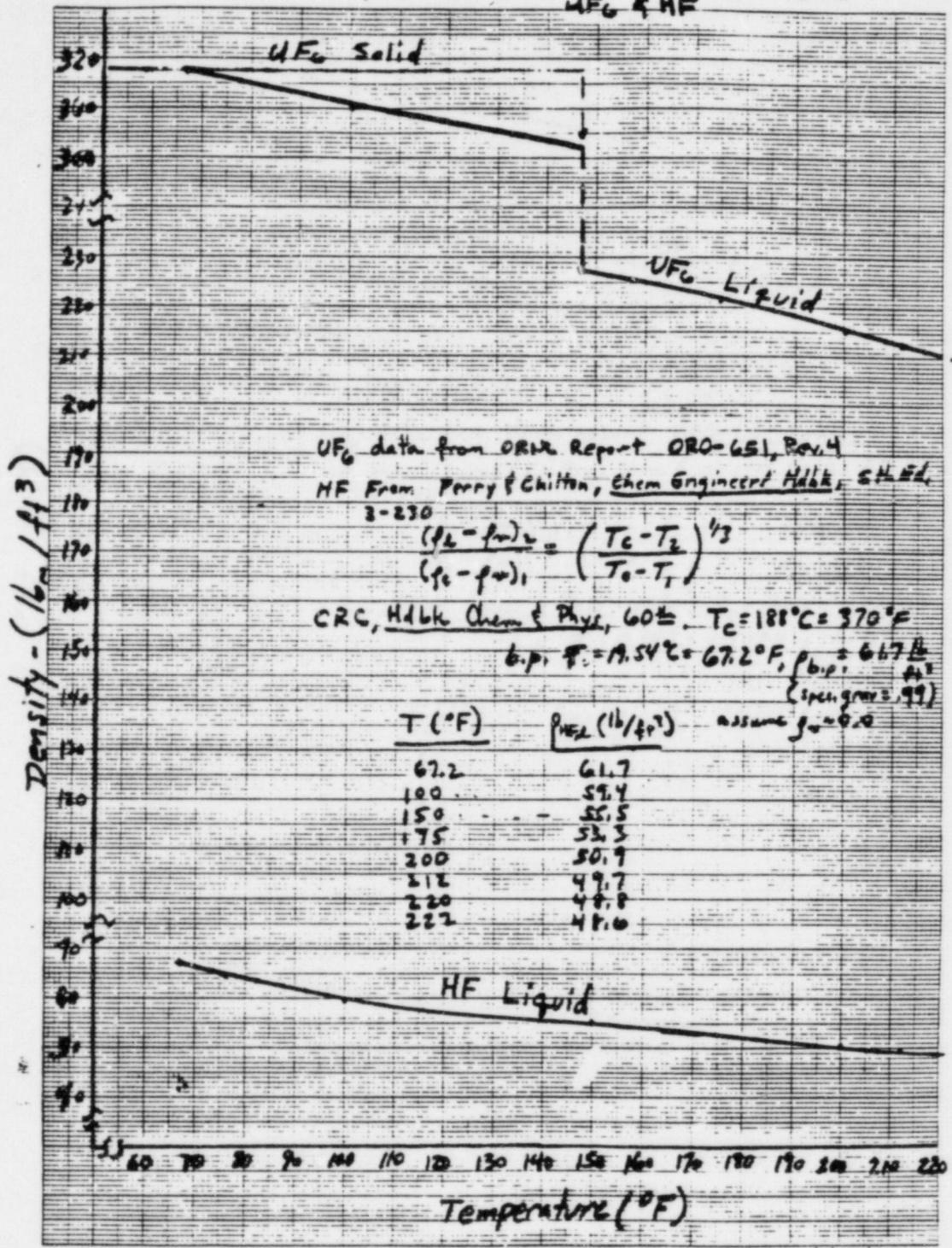
$W_T = \text{Total wt. of mix}$

FIG 3. Solve  $[V_T = W_T (1-x) / \rho_{UF_6} + W_T x / \rho_{HF}]$  for  $x$   
setting  $V_T = \text{Cyl. Vol} = 144.12 \text{ ft}^3$ ,  $W_T = 29500 \text{ lb}$   
 $\rho_{UF_6}, \rho_{HF} = f(T)$ .

FIG. 4 & 5. Fix Volume At  $144 \text{ ft}^3$  and Find Weight of mixture of  $UF_6 + HF$  at given  $T$  that will fill cylinder

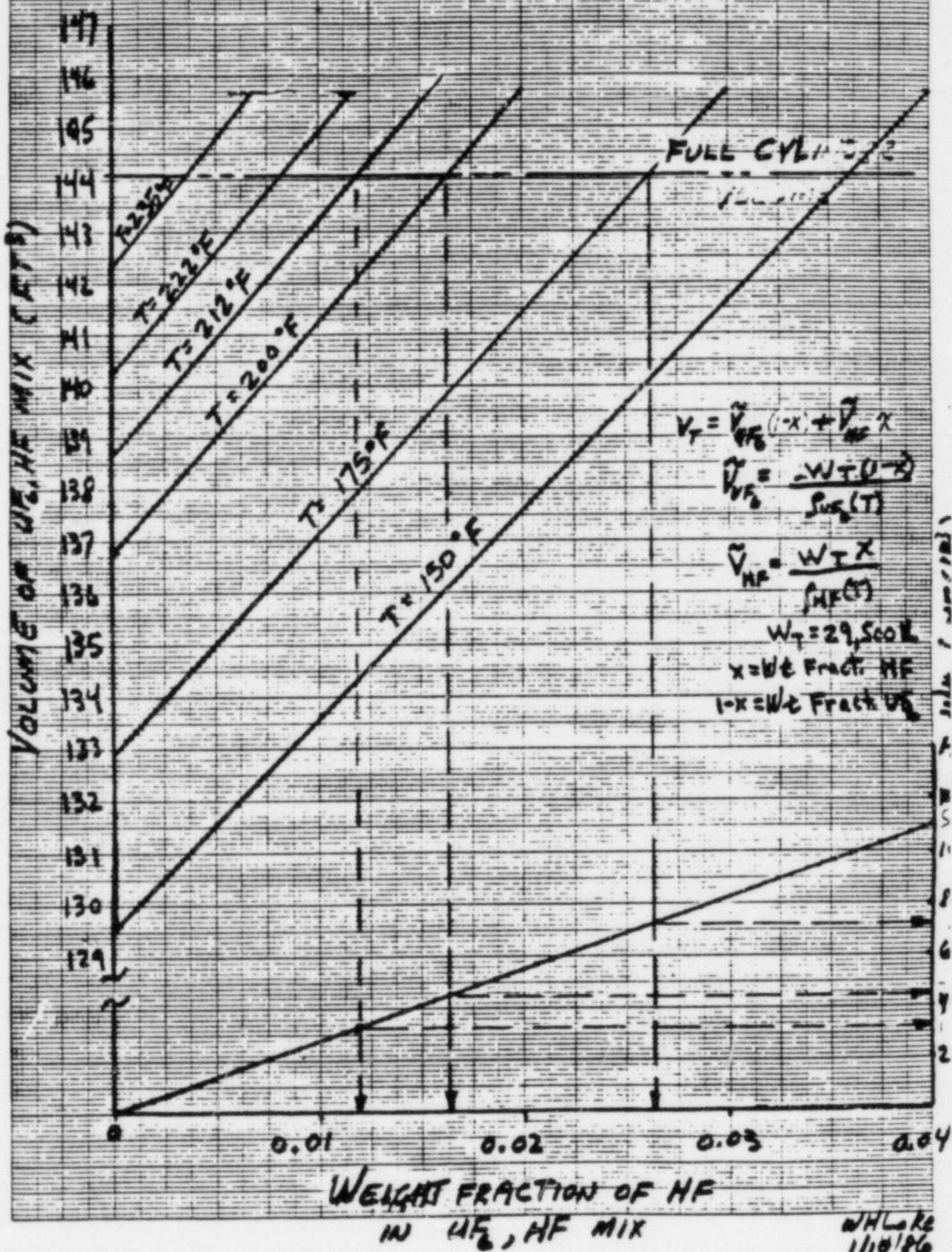
Vol based on 4072 kg water at  $70^\circ\text{F}$  for full cylinder

FIG 1. DENSITY VS TEMPERATURE  
 $UF_6$  &  $HF$



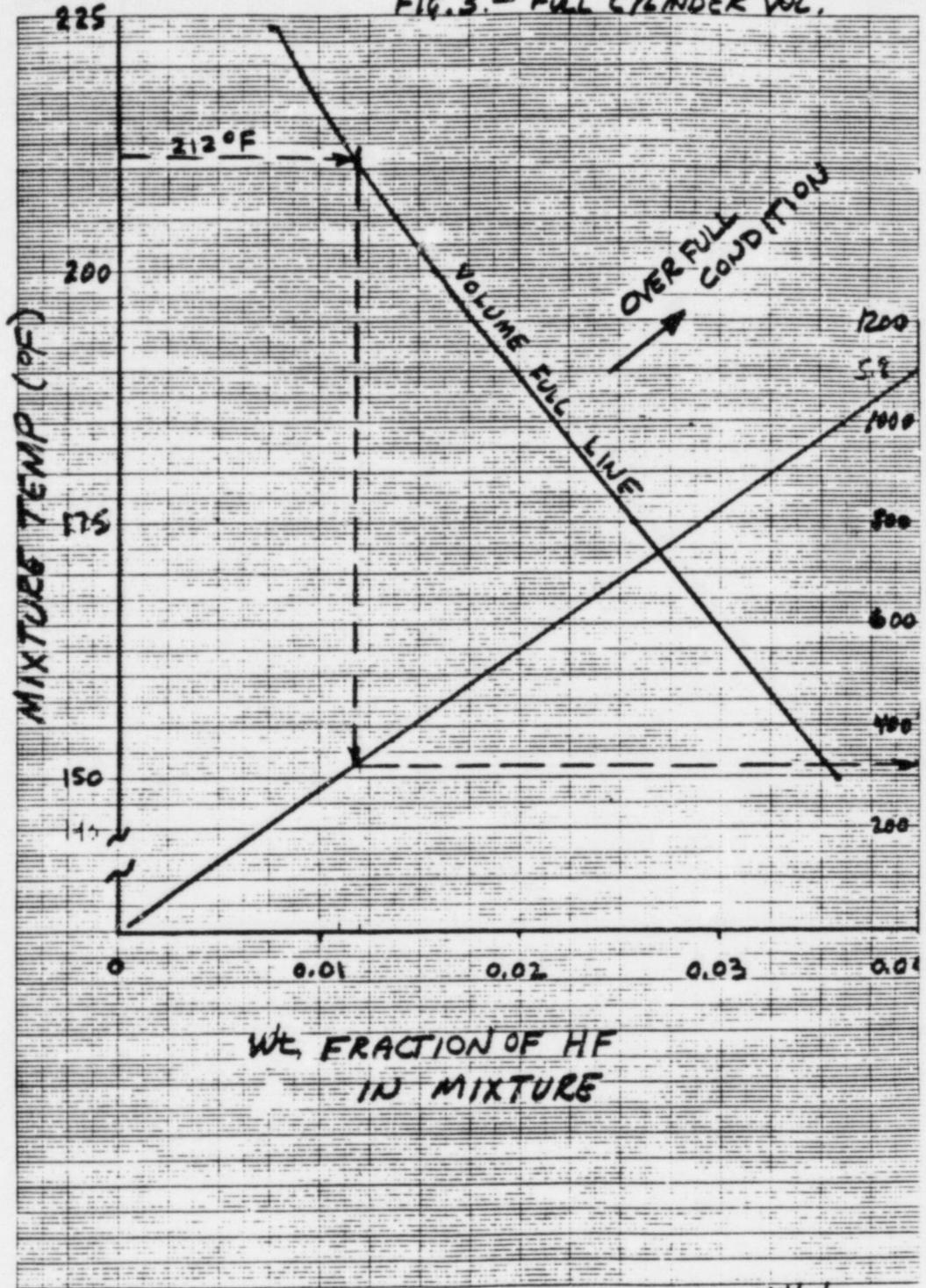
W.H. Lake  
 1/10/66

FIG. 2 - VOLUME OF 29,500 LB MIXTURE OF UF<sub>6</sub> AND HF



WHL:rk  
1/10/86

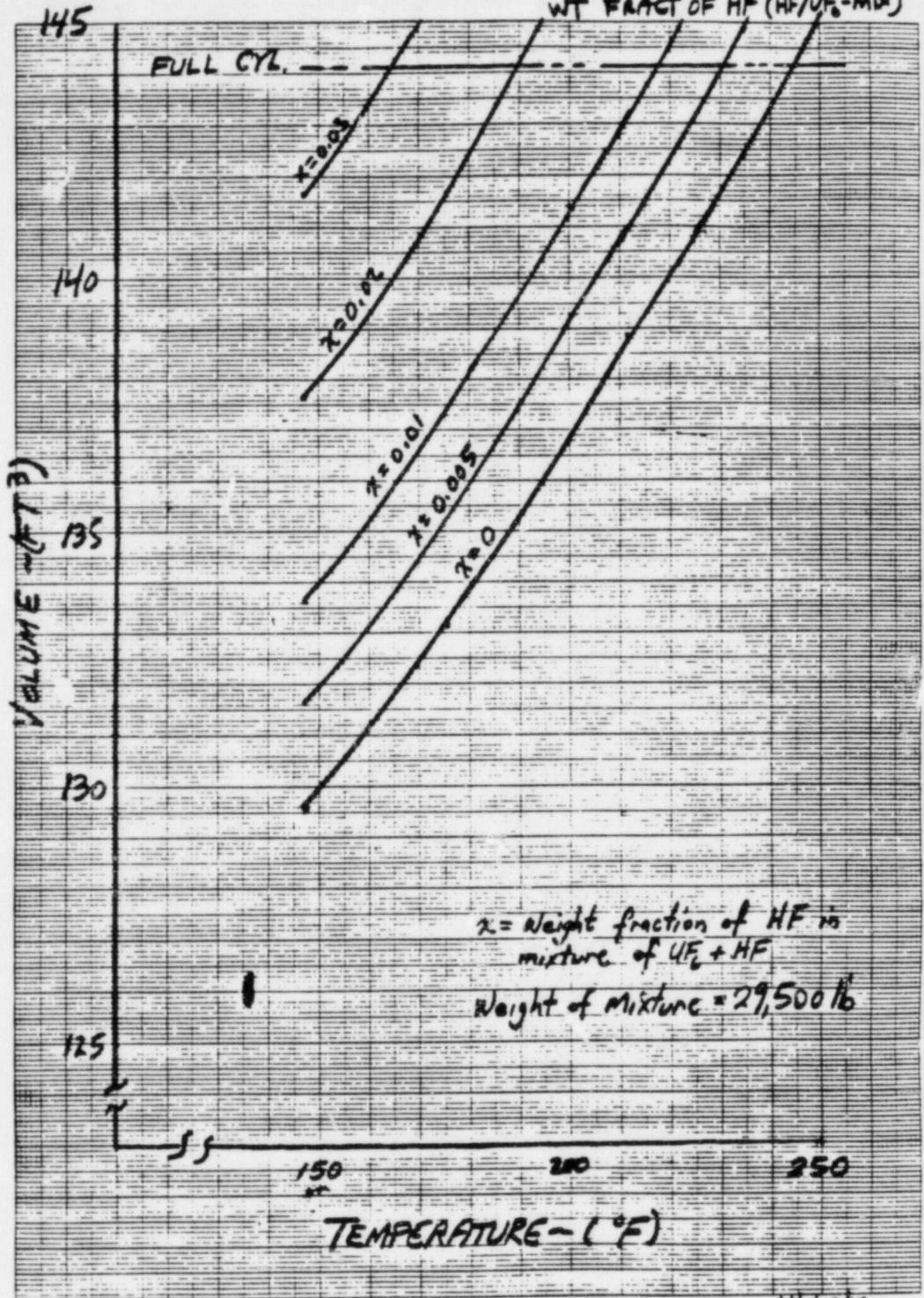
FIG. 3. - FULL CYLINDER VOL.



WHLake  
1/19/86

14-00000-18 3A 1/2000 01010 0000

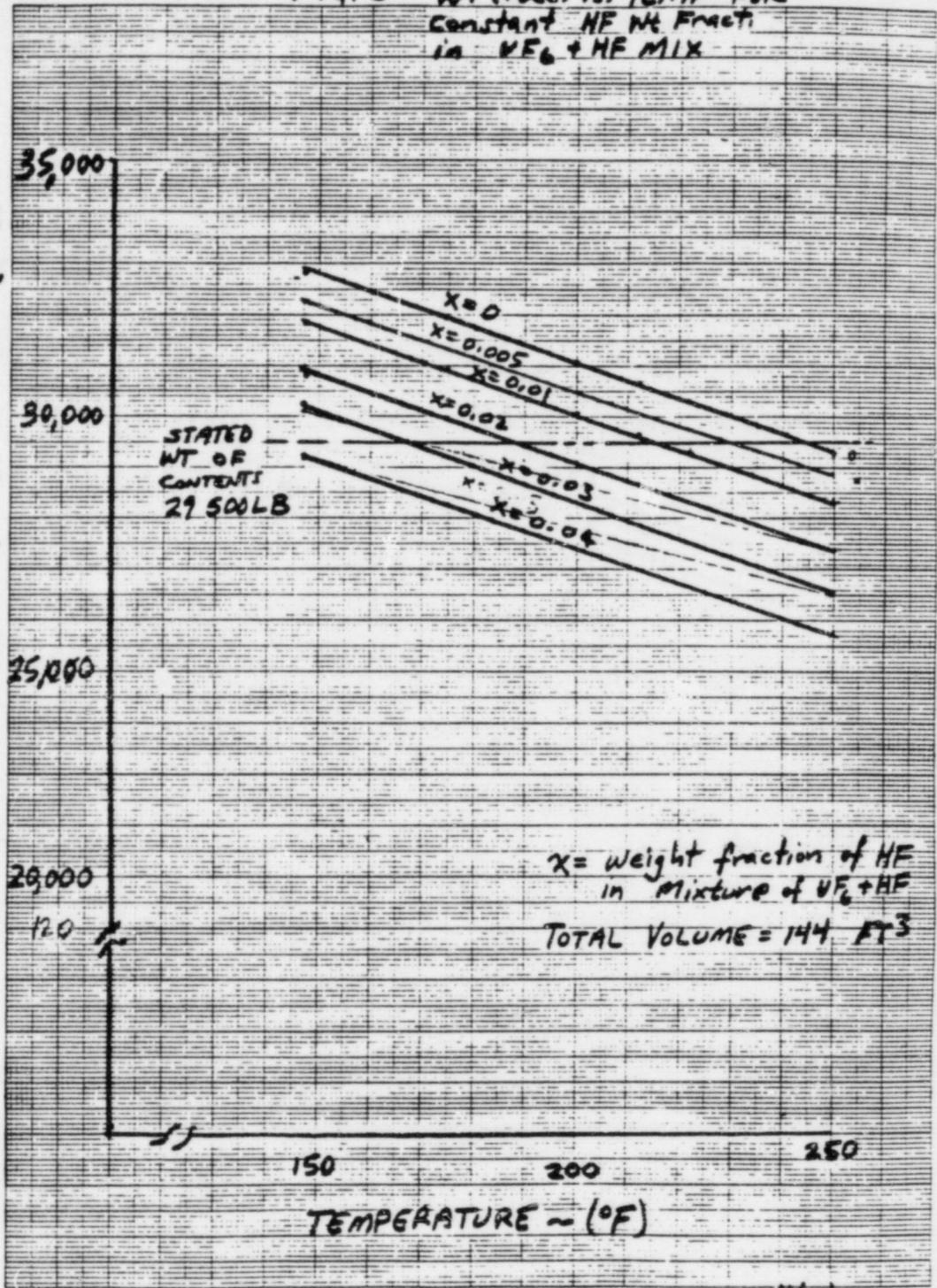
FIG. 4 - VOL. vs TEMP FOR CONSTANT WT FRACT OF HF (HF/UF<sub>6</sub>-MIX)



W.H. Lark  
1/15/86

FIG. 5 - WT (FULL) VS. TEMP FOR  
 constant HF wt fract.  
 in  $UF_6 + HF$  MIX

FULL WEIGHT of  $UF_6 + HF$  MIX ~ (LB)



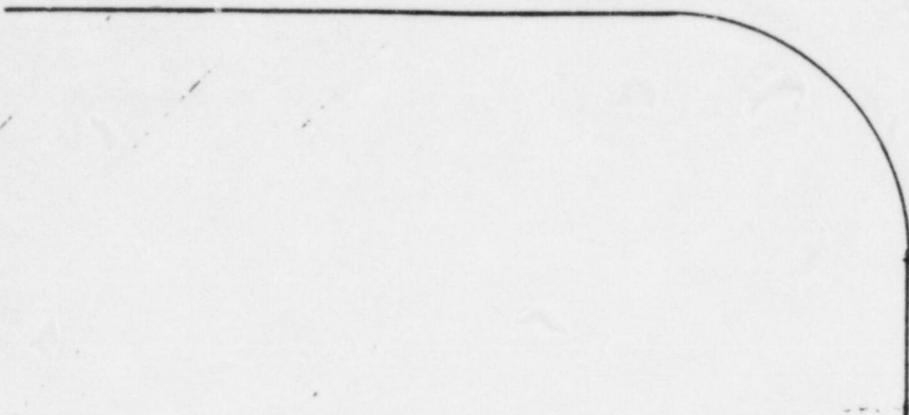
WHLake  
 1/15/86

	67.2	172.5°F	175°F	200°F	212°F	222°F	235°F	250°F	uni
$\rho_{\text{air}}$	0.3178	227.7	221.7	215.6	212.7	210.3	207.1	203.3	lb/ft
$\rho_{\text{H}_2\text{O}}$	61.7	55.5	53.3	50.9	49.2	48.6	47.1	45.3	lb/ft
$\gamma =$									
$\gamma = 29.500 \rho_{\text{air}}$	92.83	129.56	133.06	136.83	138.69	140.28	142.44	145.11	ft <sup>3</sup>
$\gamma = 29.100 \rho_{\text{H}_2\text{O}}$	478.12	531.53	553.47	579.57	593.56	607.00	626.33	651.21	ft <sup>3</sup>
$\gamma = \gamma_{\text{air}}$									ft <sup>3</sup>
$\gamma = \gamma_{\text{H}_2\text{O}}$									ft <sup>3</sup>
$x =$									
$x = .000$	92.8	129.6	133.1	136.8	138.7	140.3	142.4	145.1	
$.005$	94.8	131.6	135.2	139.1	141.0	142.6	144.9	147.6	
$.010$	96.7	133.6	137.3	141.4	143.2	144.9	147.3	150.2	
$.02$	100.5	137.6	141.5	146.0	147.8	149.6	152.1	155.2	
$.03$	104.4	141.6	145.7	150.7	152.3	154.3	157.0	160.3	
$.04$	108.2	145.6	149.9	155.3	156.9	158.9	161.8	165.4	
$W_F = \frac{V_F}{V_A}$									
$\times 29.500$									lb <sub>f</sub>
$x = .000$	45799.2	32815.2	31952.1	31071.7	30655.0	30307.5	29847.9	29298.7	
$.005$	44868.1	32313.9	31455.1	30557.2	30160.4	29811.6	29349.4	28796.6	
$.01$	43974.1	31827.7	30973.4	30059.5	29681.5	29331.6	28867.3	28311.3	
$.02$	42288.8	30898.0	30053.0	29111.2	28767.9	28416.6	27949.0	27388.3	
$.03$	40728.8	30021.0	29185.6	28220.9	27908.9	27557.0	27087.3	26523.6	
$.04$	39278.2	29192.4	28367	27383.4	27099.8	26747.9	26277.2	25711.7	
$x$									
$.000$	45800	32815	31952	31072	30655	30308	29848	29299	lb <sub>f</sub>
$.005$	44868	32314	31455	30557	30160	29812	29349	28797	
$.01$	43974	31828	30973	30060	29682	29332	28867	28311	
$.02$	42289	30898	30053	29111	28768	28417	27949	27388	
$.03$	40729	30021	29186	28221	27909	27557	27087	26524	
$.04$	39278	29192	28367	27383	27100	26748	26277	25712	

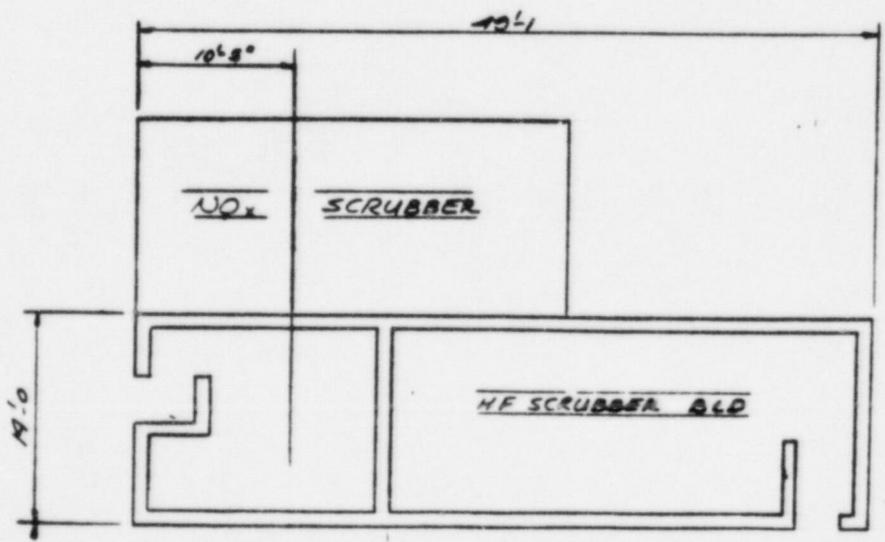
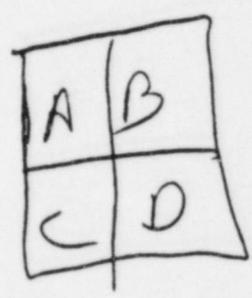
Drawing insert in here

A-2

(A)

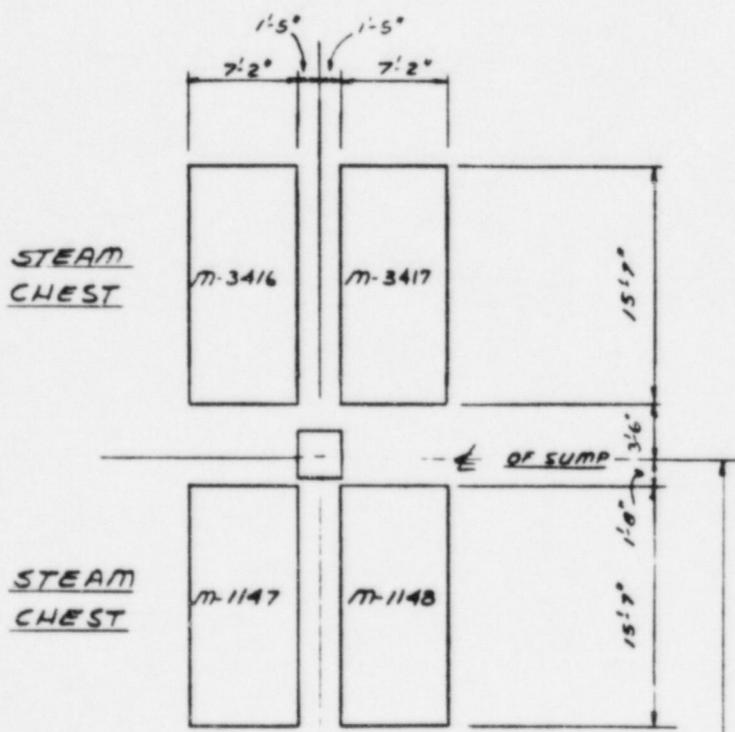


NO 1 TANK FARM



(B)

N  
N

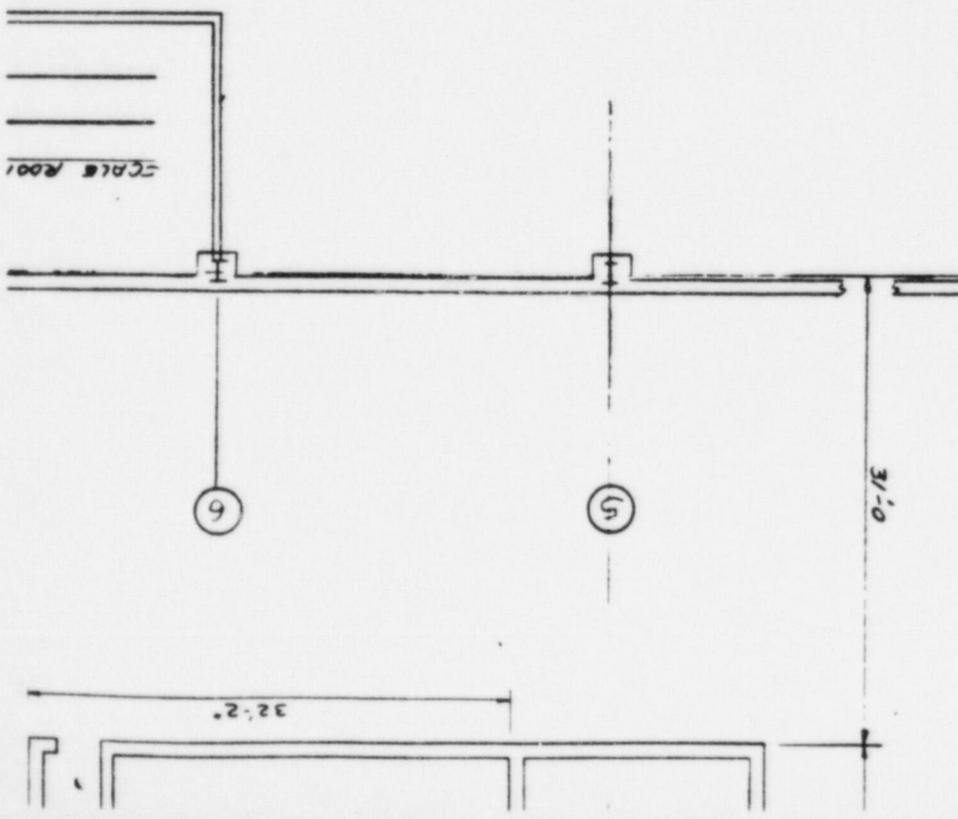




CYL. FILL ST  
SCALE

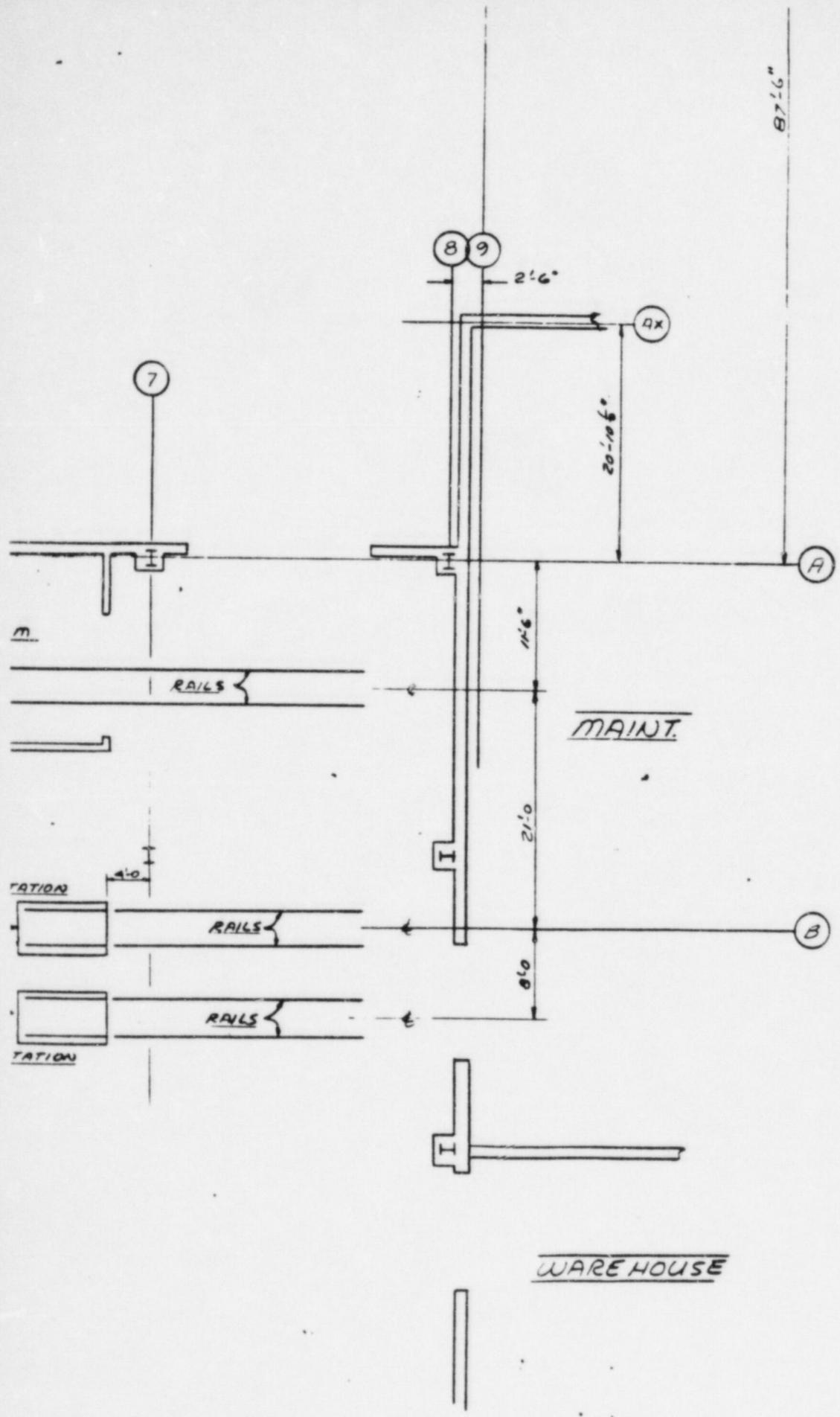
CYL. FILL ST  
SCALE

SCALE ROOM



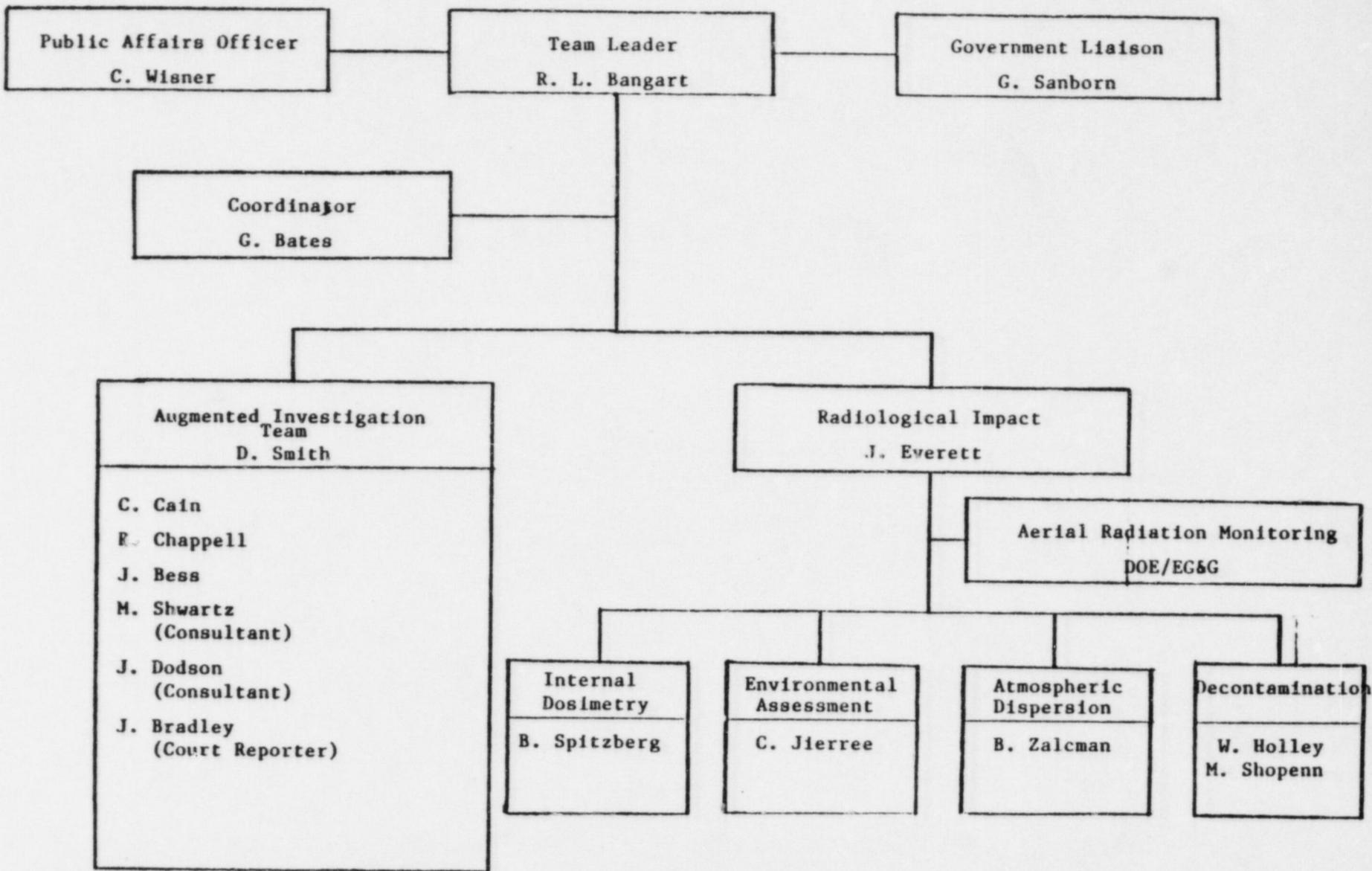
UFG PROCESS PLANT

BY		DATE	APPR	SEQUOYAH FACILITY		SEQUOYAH FUELS CORPORATION		KERRA M-CORP CORPORATION	
REV.		1/18/86	JCS	DORLE DELA.		DALLANOMA CITY, DELA.		DALLANOMA CITY, DELA.	
DESCRIPTION		DATE	APPROVED	DATE	SCALE	DRAWING NUMBER		DRAWING NUMBER	
		7-6-86		8'-1'-0	3333-M-100B		3333-M-100B		
					UFG CYLINDER FILLING, SCALE		ROOM AND STEAM CHEST		
					AREA, PLAN ARRANGEMENT				



D

Organization Chart  
NRC Site Team  
Sequoyah Fuels Facility



A-3



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

MEMORANDUM FOR: Victor Stello, Jr  
Acting Executive Director for Operations

FROM: John G. Davis, Director  
Office of Nuclear Material Safety and Safeguards

SUBJECT: DOCUMENTS REQUESTED BY CHAIRMAN MARKEY IN LETTER  
DATED FEBRUARY 4, 1986

Enclosed are additional documents and a list of the documents in response to Chairman Markey's request dated February 4, 1986.

These documents contain information which is restricted under the Privacy Act in that they contain work experience in the private sector and personal information such as birth date.

John G. Davis, Director  
Office of Nuclear Material  
Safety and Safeguards

Enclosure: Two copies of  
documents and list

A-4