



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555  
**FEB 19 1986**

Docket Nos.: 50-440/441

MEMORANDUM FOR: B. D. Liaw, Chief  
Engineering Branch  
Division of BWR Licensing

THROUGH: *RCG* Robert LaGrange, Section Leader  
Engineering Branch  
Division of BWR Licensing

FROM: Phyllis Sobel, Geophysicist  
Engineering Branch  
Division of BWR Licensing

SUBJECT: JANUARY 31, 1986 EARTHQUAKE NEAR PERRY NUCLEAR POWER PLANT

At 16:46:41.7 GMT (11:46 EDT) on January 31, 1986 a magnitude 4.9 to 5.0 ( $m_b$ ) earthquake occurred about 10 miles south of the Perry plant in northeastern Ohio. The USGS-NEIS report the epicenter was at 41.65°N and 81.10°W. The earthquake was felt as far away as Washington, D.C., about 300 miles from the epicenter and there were reports of damage such as cracked walls, falling roof tiles and shattered windows near the epicenter. There have been five small aftershocks; the largest was about a magnitude 2 to 2.3 on February 7. The aftershocks were 2 to 9 km deep and some were felt, although not at the Perry site.

A site area emergency was declared at the Perry site and plant personnel surveyed for any damage. The NRC project manager, John Stefano, a DSRD seismologist, Leon Reiter and a DSRD mechanical engineer, Tsung-Yung Chang inspected the plant on February 1, 1986. The initial reports indicated no significant damage. Another NRC team (including Arnold Lee of NRR and Jag Singh from EG&G) inspected the plant on February 6 and 7 and found no damage. The utility is continuing the survey for damage.

The January 31 earthquake triggered the in-plant seismic monitoring instruments. Preliminary acceleration data indicate that some of the recorded ground motions exceeded the Operating Basis and Safe Shutdown Earthquake design spectra at high frequencies (above 15 hertz). The earthquake motion recorded at the reactor building foundation was of short duration (about one second) and predominantly high frequencies. The utility met with the staff on February 11 and submitted their report on the earthquake data on February 12.

Contact: P. Sobel  
X-27592

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3 PP.

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The size and proximity of the January 31 earthquake are consistent with observations of historical seismicity in the Central Stable Region. In the SER the staff compared the Perry SSE design spectrum to a larger event (magnitude 5.3) at this distance. The location of the earthquake, its aftershocks and focal mechanisms will have to be examined with respect to known geological features and statements in the SER to determine if significant new findings can be made. The significance of the high frequency peak accelerations observed in the plant is being assessed by the utility and the staff with respect to plant structures and components. The staff has contracted with Jim Johnson of NTS/Structural Mechanics Associates to inspect the Perry facility for structural damage and equipment failure or malfunction and to evaluate the seismic instrumentation recordings and the utility's findings.

I will notify you of any additional information we receive.

| p |

Phyllis Sobel, Geophysicist  
Engineering Branch  
Division of BWR Licensing

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-----:  
W\*\*\* :PSobel.cdd :R.LaGrange : : : :  
-----:  
DATE :2/19/86 :2/ 19/86 : : : :

From The Desk of:  
J. A. Grobe

DICK,

THESE ARE COPIES OF ALL OF  
THE SEISMIC INSTRUMENT CALIBRATION  
DATA SHEETS. I THINK THAT THE  
DATA SHEETS ARE SELF EXPLANATORY.  
IF YOU NEED THE SPECIFIC PROCEDURES  
LET ME KNOW. HARRISON/MUFFET SHOULD  
BE INTERESTED IN THIS INFO. ANY Q's  
CALL ME

JAK

FEB 24 1988

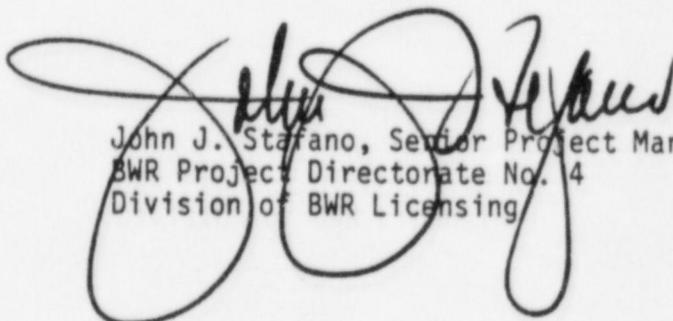
A/60



completed. In view of these conclusions, CEI maintained that the SSE design basis for the Perry plant remains valid. These conclusions appear to be borne out by the fact that little or no damage had been observed during an intense walkdown of the plant conducted by the CEI staff.

The NRC staff advised CEI that it still needed to conduct its own independent evaluation of the earthquake and that this effort would consider CEI's findings (a detailed report was filed by CEI with the Commission on February 12, 1986). The NRC staff also informed CEI that the issue would be discussed with the ACRS, and that meetings with the ACRS Subcommittee and the ACRS Full Committee were scheduled for February 12 and 13, 1986, respectively. (NRC and CEI briefed the ACRS on those dates). Lastly, the NRC staff advised CEI that its independent evaluation would not be completed before March 1, 1986, and that completion of its evaluation by that date assumed receipt of all outstanding data promised by CEI before February 17, 1986.

The morning session of the February 11, 1986 meeting was completed at 11:30 am after which time the NRC staff answered questions posed by the press and public representatives in attendance. The NRC staff also met with its respective CEI technical counterparts to go over in more detail the information presented by CEI during the formal meeting.

  
John J. Stafano, Senior Project Manager  
BWR Project Directorate No. 4  
Division of BWR Licensing

Enclosure: As stated

cc w/enclosure: See next page

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Perry Nuclear Power Plant  
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Enclosure 1

CEI/NRC MEETING  
AT PERRY SITE

FEBRUARY 11, 1986  
(MORNING SESSION ONLY)

EARTHQUAKE EVENT

CEI

M. R. Edelman  
A. Kaplan  
E. Buzzelli  
F. Stead  
M. Lister  
R. Stratman  
Others

NRC

R. M. Bernero, NRR/DBL  
J. G. Keppler, RIII  
C. J. Paperiello, RIII  
R. C. Knop, RIII  
J. A. Grobe, RIII  
J. J. Stefano, NRR/DBL  
W. R. Butler, NRR/DBL  
R. Hernon, NRR/DBL  
H. Polk, NRR/DBL  
J. Johnson, Consultant (SMA)  
J. Singh, Consultant (EG&G)  
D. Guzy, RES  
G. Cumming, Consultant

Gilbert Associates

C. Chen  
R. Ailey

CEI Consultants

R. Holt

USGS

L. Langer



THE CLEVELAND ELECTRIC ILLUMINATING COMPANY  
SEISMIC EVENT EVALUATION  
TECHNICAL PRESENTATION  
AGENDA

FEBRUARY 11, 1986

INTRODUCTION & OVERVIEW	M. R. EDELMAN
PLANT STATUS AND RESPONSE	R. A. STRATMAN
EARTHQUAKE ANALYSIS AND SEISMICITY	R. HOLT WESTON GEOPHYSICAL
PLANT SEISMIC DESIGN EVALUATION	DR. C. CHEN GILBERT COMMONWEALTH
SUMMARY AND CONCLUSIONS	M. R. EDELMAN

PLANT STATUS PRIOR  
TO SEISMIC EVENT

- o ONGOING TESTING, CALIBRATION, WORK ACTIVITIES
- o PREPARATION FOR DIVISION II DIESEL GENERATOR TESTING
- o STARTUP SOURCES NOT YET MOVED
- o SYSTEMS ENERGIZED (IN OPERATION AND STANDBY MODE)
  - SAFETY SYSTEMS
  - NON-SAFETY SYSTEMS

SYSTEMPLANT STATUS

G33 REACTOR WATER CLEANUP	A & B PUMPS WITH FLOW TO THE MAIN COND. AT 55 GPM NO FILTER/DEMINERALIZERS IN SERVICE
G41 FUEL POOL COOLING AND CLEANUP	A PUMP RUNNING B FILTER/DEMINERALIZER TRAIN IN SERVICE
M35 TURBINE BUILDING COOLING AND VENTILATION	B FAN RUNNING
M41 HEATER BAY VENTILATION	B FAN RUNNING
M45 CIRCWATER PUMP HOUSE VENTILATION	A AND B FANS RUNNING
N21 CONDENSATE	A HOTWELL PUMP IN SHORTCYCLE CLEANUP A, B, C CONDENSATE BOOSTER PUMP LUBE OIL PUMPS
N23 CONDENSATE FILTRATION	FILTERS B, C, E
N24 CONDENSATE DEMINERALIZERS	DEMINERALIZERS A, B
N32 TURBINE CONTROL (EHC)	RECIRCULATION PUMP RUNNING
N71 CIRCULATING WATER	A & B PUMPS RUNNING B, C, D LOOPS IN OPERATION COOLING TOWER IN BYPASS
P11 CONDENSATE TRANSFER	NORMAL PUMP RUNNING B PUMP IN STANDBY
P20 WATER TREATMENT	A AND B COAGULATORS IN SERVICE
P21/22 TWO-BED/MIXED-BED DEMINERALIZERS	B STREAM IN SERVICE B SULFITE PUMP RUNNING B AND C CLEARWELL PUMPS RUNNING
P41 SERVICE WATER	B AND C PUMPS RUNNING
P43 NUCLEAR CLOSED COOLING	B AND C PUMPS RUNNING A HEAT EXCHANGER IN SERVICE
P44 TURBINE BUILDING CLOSED COOLING	B AND C PUMPS RUNNING A HEAT EXCHANGER IN SERVICE

<u>SYSTEM</u>	<u>PLANT STATUS</u>
P52 INSTRUMENT AIR	UNIT 1 COMPRESSOR RUNNING
P55 BUILDING HEATING	A PUMP RUNNING
P61 AUXILIARY STEAM	B BOILER C BOILER FEED PUMP
P62 AUXILIARY BOILER FUEL OIL	B FUEL OIL PUMP
P72 PLANT UNDERDRAIN	PUMPS IN AUTOMATIC
C11 CONTROL ROD DRIVE	A PUMP A FLOW CONTROL VALVE
C41 STANDBY LIQUID CONTROL	TANK HEATERS ENERGIZED
C71 REACTOR PROTECTION SYSTEM	ENERGIZED
D17 PLANT RADIATION MONITORS	ENERGIZED
E12 RESIDUAL HEAT REMOVAL	KEEP FILL PUMP FOR LOOPS B & C
E21 LOW PRESSURE CORE SPRAY	KEEP FILL PUMP FOR LPCS AND RHR LOOP A
E22 HIGH PRESSURE CORE SPRAY	KEEP FILL PUMP FOR HPCS
F42 FUEL TRANSFER EQUIPMENT	ENERGIZED
M11 CONTAINMENT VESSEL COOLING	B, C, E, F FANS RUNNING
M13 DRYWELL COOLING	1A, 2A, 3B FANS RUNNING B COOLING COIL
M15 ANNULUS EXHAUST GAS TREATMENT	A TRAIN RUNNING B TRAIN IN STANDBY
M21 CONTROLLED ACCESS VENTILATION	A TRAIN RUNNING B TRAIN STANDBY
M23/24 MCC SWITCHGEAR & MISC. AREA VENTILATION/BATTERY ROOM EXHAUST	A TRAIN RUNNING B TRAIN STANDBY
M25/26 CONTROL ROOM VENTILATION/ EMERGENCY RECIRCULATION MODE	A TRAIN RUNNING IN NORMAL MODE B TRAIN STANDBY
M27 COMPUTER ROOM VENTILATION	A FAN RUNNING

SYSTEM

M32 ESW Pumphouse VENTILATION

M40 FUEL HANDLING BUILDING  
VENTILATIONM43 DIESEL GENERATOR BUILDING  
VENTILATION

P45 EMERGENCY SERVICE WATER

P47 CONTROL COMPLEX CHILLED  
WATERP49 EMERGENCY SERVICE WATER  
SCREEN WASH

P54 FIRE PROTECTION

PLANT SYSTEM

A AND B FANS RUNNING

B AND C EXHAUST FANS

2B FAN RUNNING

A AND B PUMPS RUNNING WITH ALL  
LOADS VALVED INA CHILLER RUNNING WITH NORMAL LOADS  
A CIRCWATER PUMP RUNNING

BOTH SCREENS OPERATING

RECIRC PUMP (CONSTRUCTION) RUNNING  
NO INITIATION OF CO<sub>2</sub>, HALON, OR  
SPRINKLER SUPPRESSION SYSTEMS

## INSPECTIONS AND FINDINGS FOLLOWING SEISMIC EVENT

- o OPERATOR SURVEY (NO STRUCTURAL DAMAGE)
- o WALKDOWNS BY PLANT MAINTENANCE PERSONNEL (NO STRUCTURAL DAMAGE)
- o SYSTEMATIC PLANT WALKDOWNS BY 65 ENGINEERS AND TECHNICIANS  
(No Structural/Equipment Damage)
  - IDENTIFY AND DOCUMENT ALL DISCREPANT CONDITIONS
  - 480 OBSERVATIONS DOCUMENTED (MINOR ITEMS)
  - REVIEW FOR RELATIONSHIP TO EARTHQUAKE
  - REVIEW OF OBSERVATIONS BY CEI AND NRC
- o ADDITIONAL INSPECTIONS/SURVEYS
  - SITE SURVEY
  - PLANT SETTLEMENT SURVEY
  - COOLING TOWER WALKDOWN
- o SEISMIC CLEARANCE INSPECTION
- o ENERGIZED ELECTRICAL EQUIPMENT STUDY
- o ONGOING SURVEILLANCE (SVI's)
- o NEW PROCEDURE
  - ASSURES CEI/NRC REVIEW OF ALL POTENTIAL EARTHQUAKE-RELATED ITEMS
  - REVIEW ALL WORK REQUESTS FOR RELATIONSHIP TO EARTHQUAKE
  - NO WORK ON EARTHQUAKE-RELATED OR INDETERMINATE CONDITIONS WITHOUT CEI/NRC REVIEW

## **MAIN SHOCK**

**January 31, 1986**

origin time :  $16^{\text{hr}}\ 46^{\text{m}}\ 47^{\text{s}}_{\text{on}}$  U.T.

latitude : **41.649° N**

longitude : **81.105° W**

focal depth : **10 Km**

based on : **64 stations (worldwide)**

$M_b = 4.9$

$M_{blg} = 4.96 \leftarrow$

location : **Geauga County**

Near intersection of  
Highway 86 and 166

est. distance

to plant : **11 miles**

**17.7 km**

based on : **NEIS solution**

**EARTHQUAKE MAGNITUDE & INTENSITY**

**4.96 M BLG - USGS (EQUIVALENT RICHTER SCALE)**

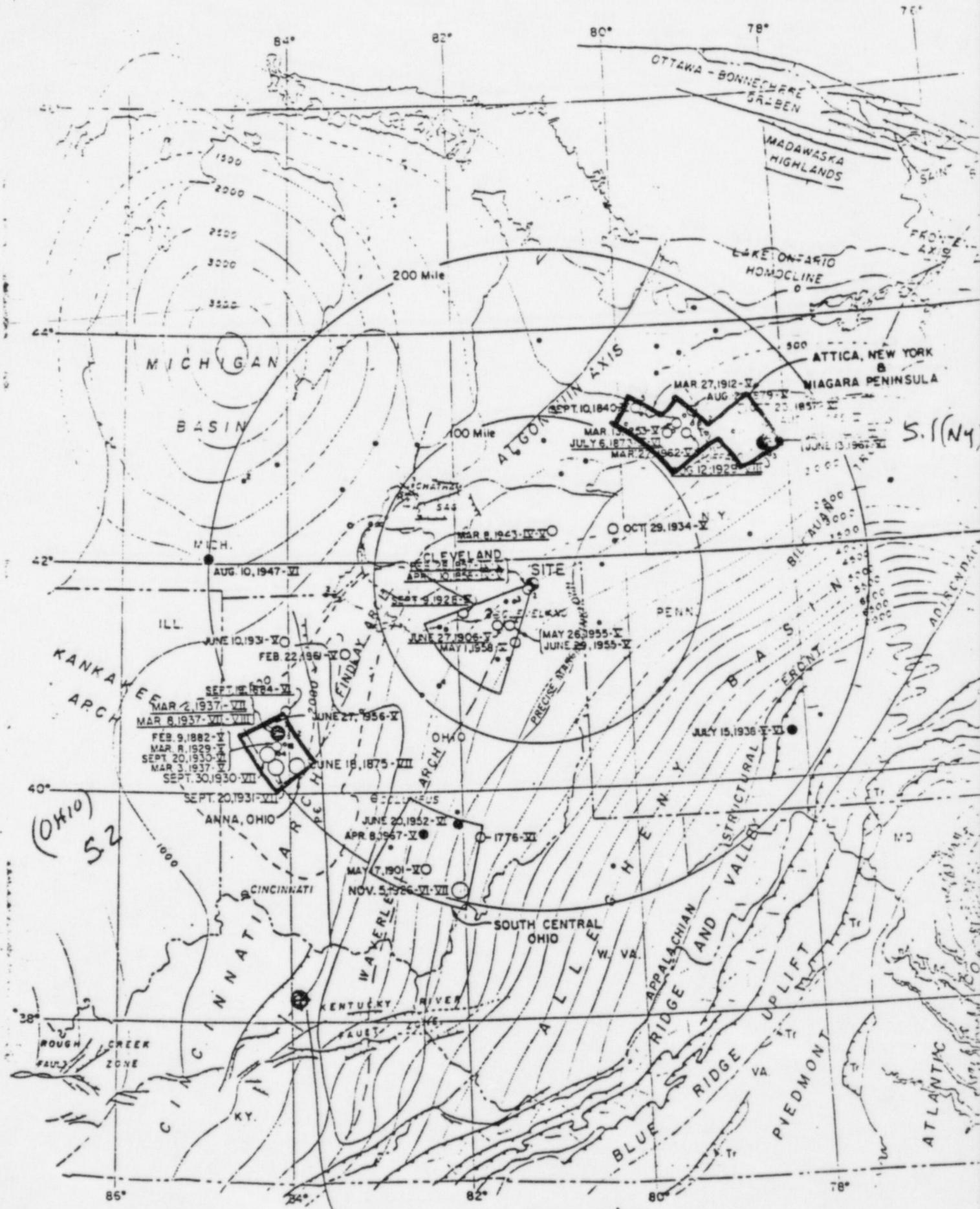
**MODIFIED MERCALLI INTENSITY VI - PRELIMINARY -**

**WESTON GEOPHYSICAL**

**● QUESTIONNAIRE**

**● REPORTED EFFECTS**

**FEW DAMAGED CHIMNEYS  
CRACKS IN WALLS  
CRACKED/FALLEN PLASTER  
BROKEN WINDOWS  
WELL-WATER EFFECTS**



↑ 1980 S.2 (Kentucky)  
 PBO 7/27 18:52 38.19 83.69 DEPTH=16KM 5.1mb 5.2mbLg

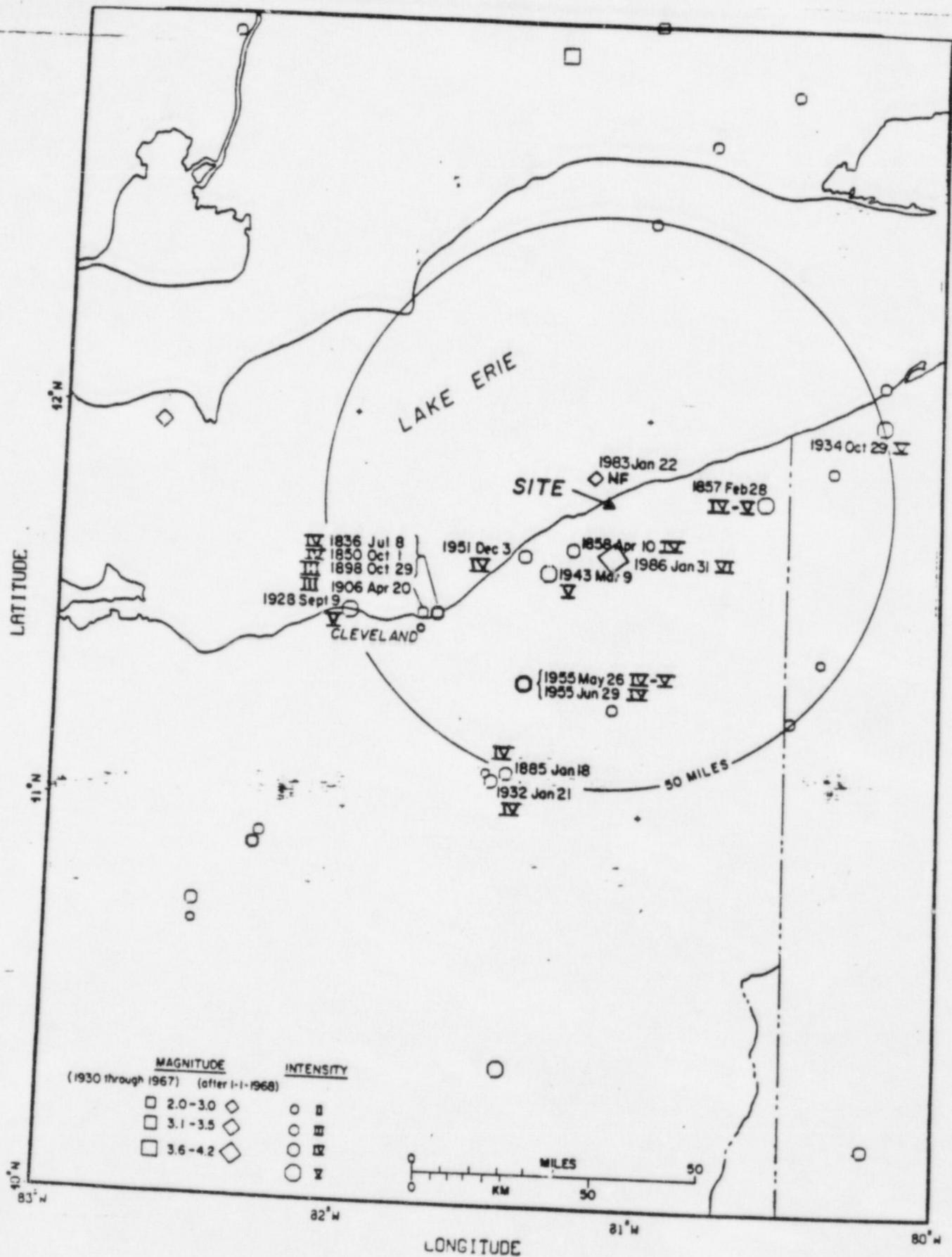
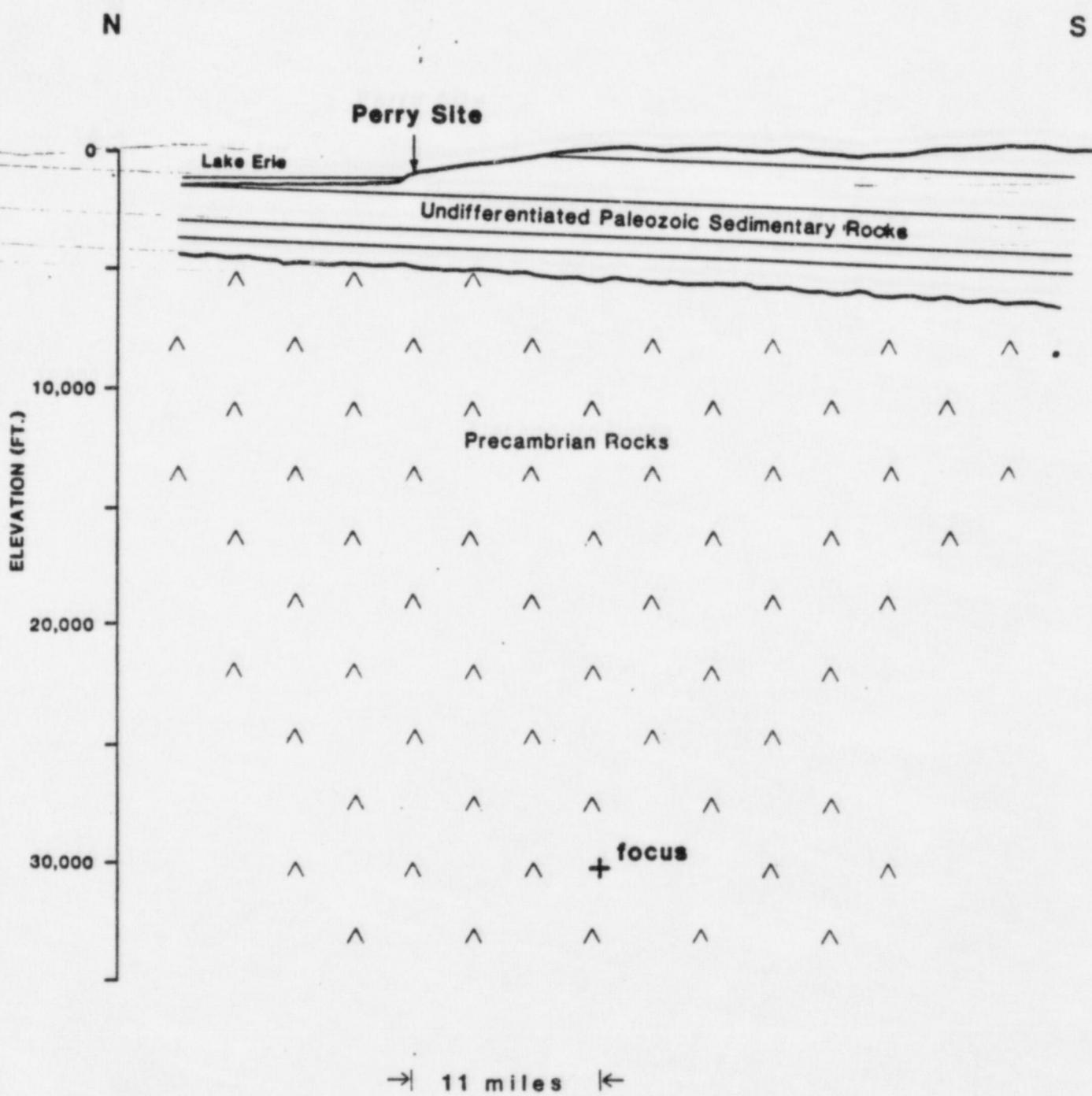


Figure 4 Seismicity Map





SAFE SHUTDOWN EARTHQUAKE

MODIFIED MERCALLI INTENSITY = VII

PEAK GROUND ACCELERATION - 0.15 g

REGULATORY GUIDE 1.60 SPECTRA

SITE SPECIFIC SPECTRA

- $M_{BLG} \pm .5$
- $M_{BLG} \pm .3$

FIFTY-MILE SEISMICITY

RELATIVELY LOW SEISMICITY

NO CAPABLE FAULTS

HIGHEST INTENSITY - MODIFIED  
MERCALLI VI

INTENSITY (6) EST

HIGHEST MAGNITUDE - 4.96 M BLG

## CONCLUSIONS

TECTONIC PROVINCE APPROACH STILL VALID

- NO CAPABLE FAULT
- NO TECTONIC STRUCTURE

SAFE SHUTDOWN EARTHQUAKE INTENSITY

- MODIFIED MERCALLI VII vs. VI

SITE SPECIFIC

- $5.5 \pm .3$  vs. 4.96
- $5.3 \pm .5$  vs. 4.96

EXCEEDANCE OF SAFE SHUDOWN EARTHQUAKE

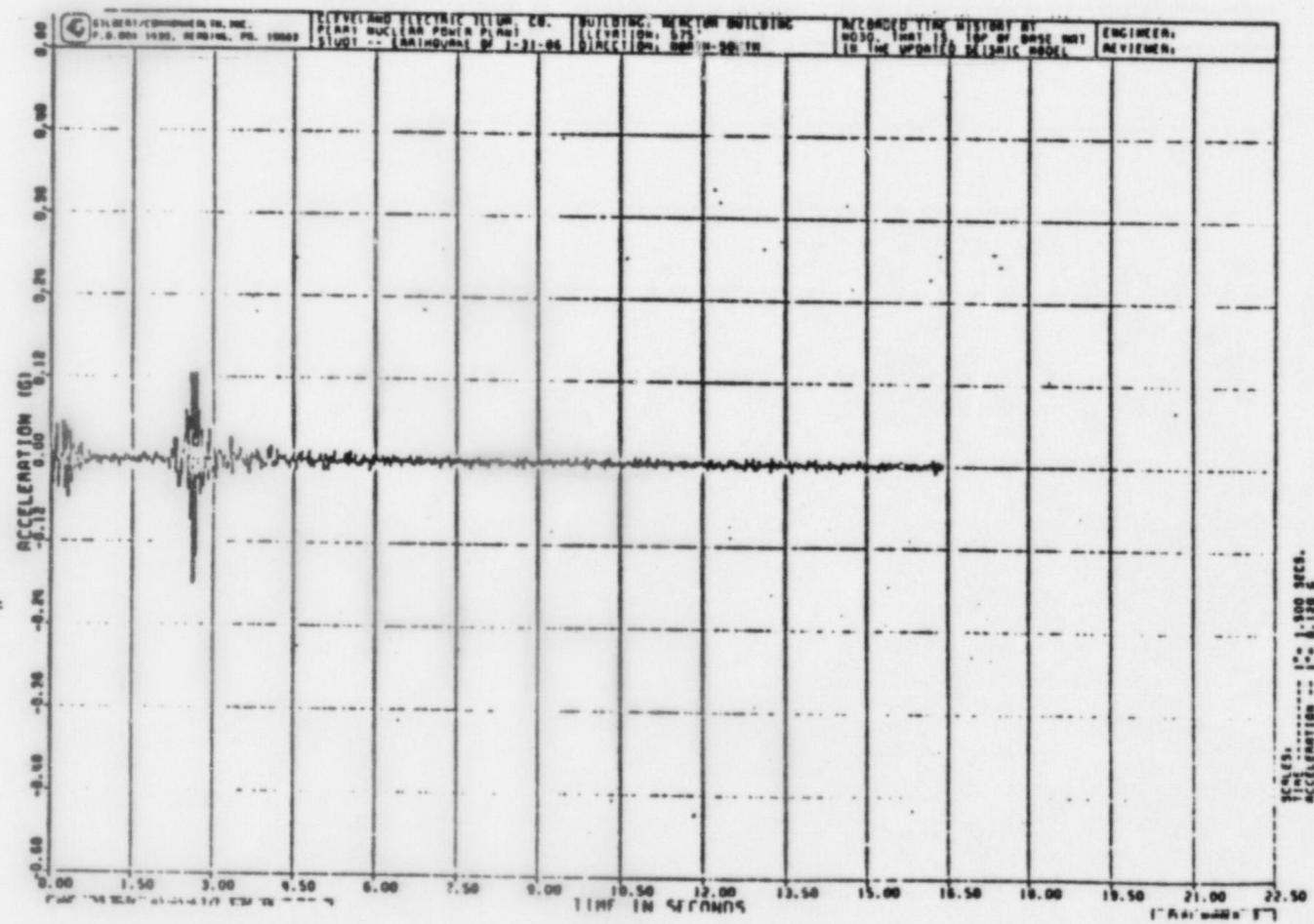
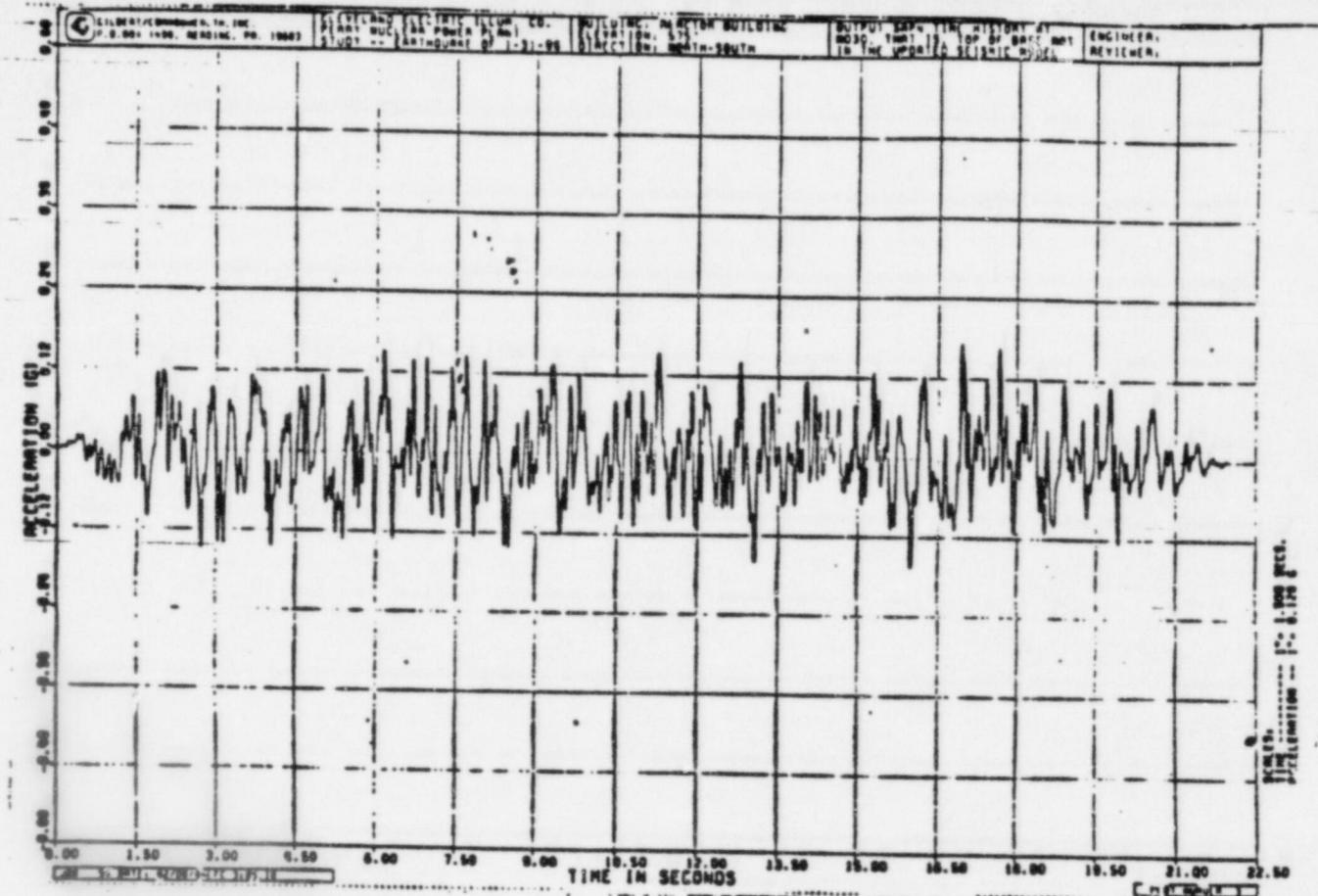
- SHORT DURATION (< 0.5 sec.)
- HIGH FREQUENCY (20 Hz)
- EXCEEDANCE ABOVE 84% EXPECTED

## CHARACTERISTICS OF THE 1986 OHIO EARTHQUAKE

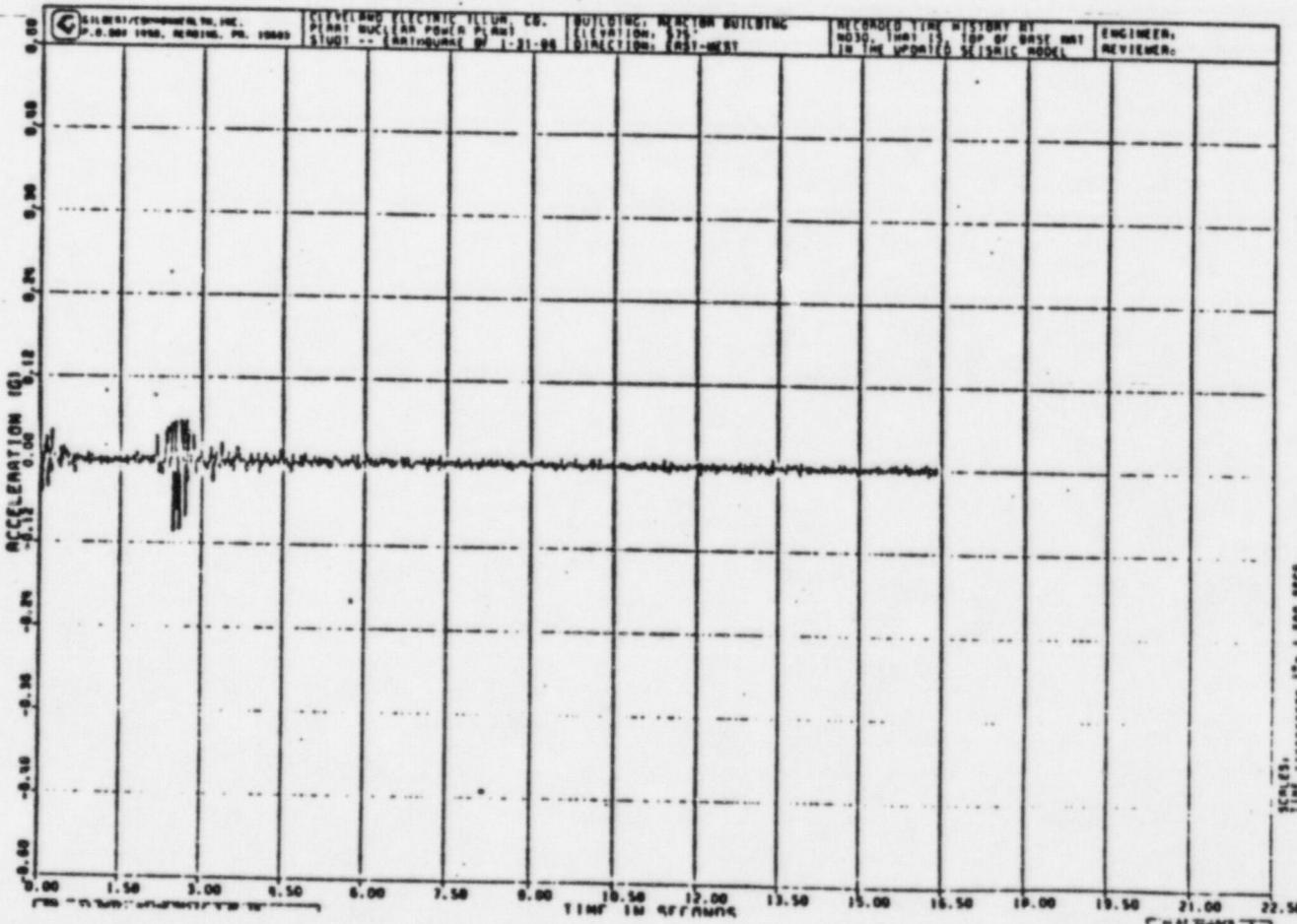
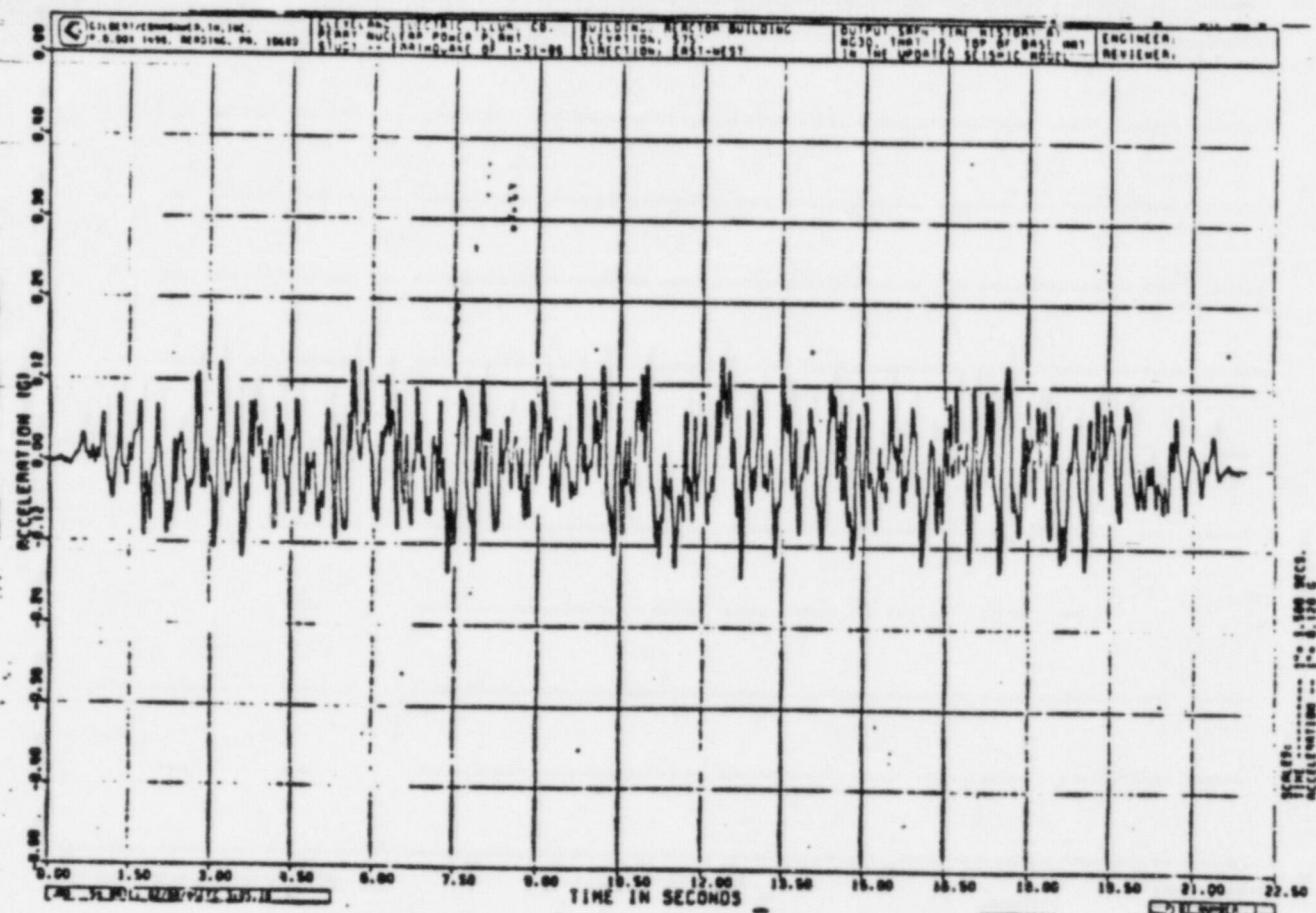
- HIGH FREQUENCIES
- SHORT DURATION
- LOW ENERGY
- LOW VELOCITY
- SMALL DISPLACEMENT

## CHARACTERISTICS OF THE PERRY DESIGN BASIS EARTHQUAKE (SSE)

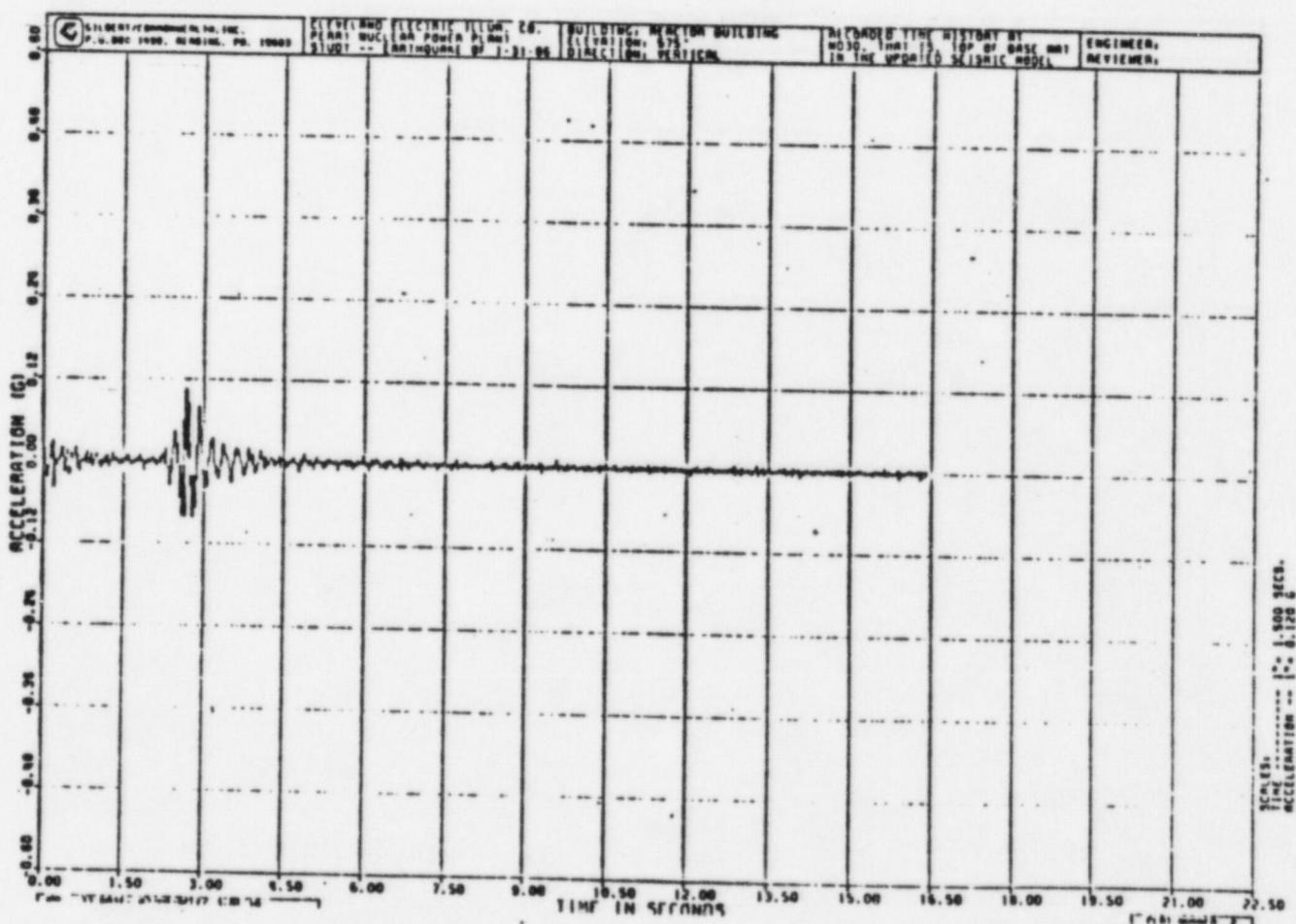
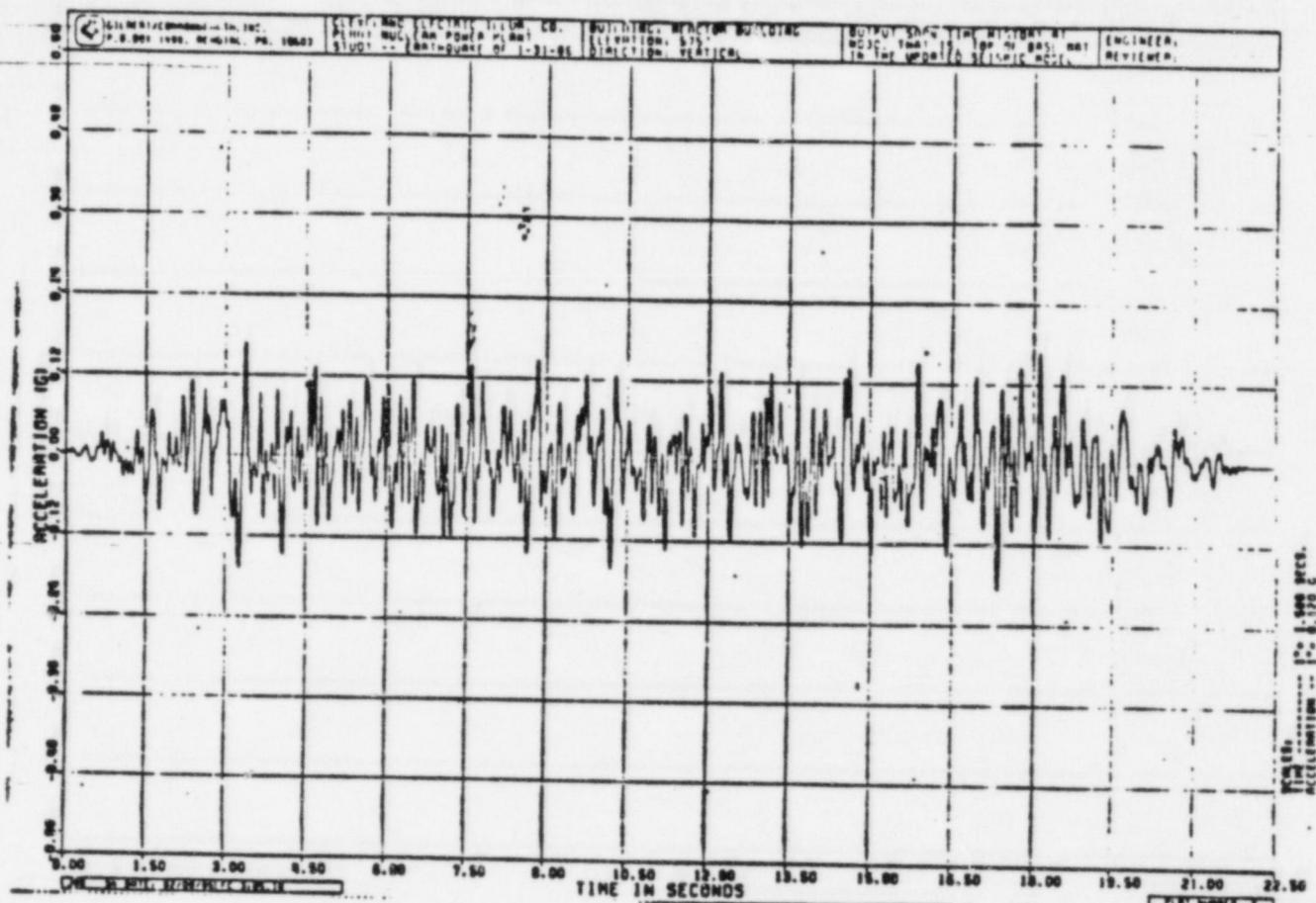
- BROAD BAND FREQUENCIES
- LONG DURATION
- HIGH VELOCITY
- LARGE DISPLACEMENT
- HIGH ENERGY



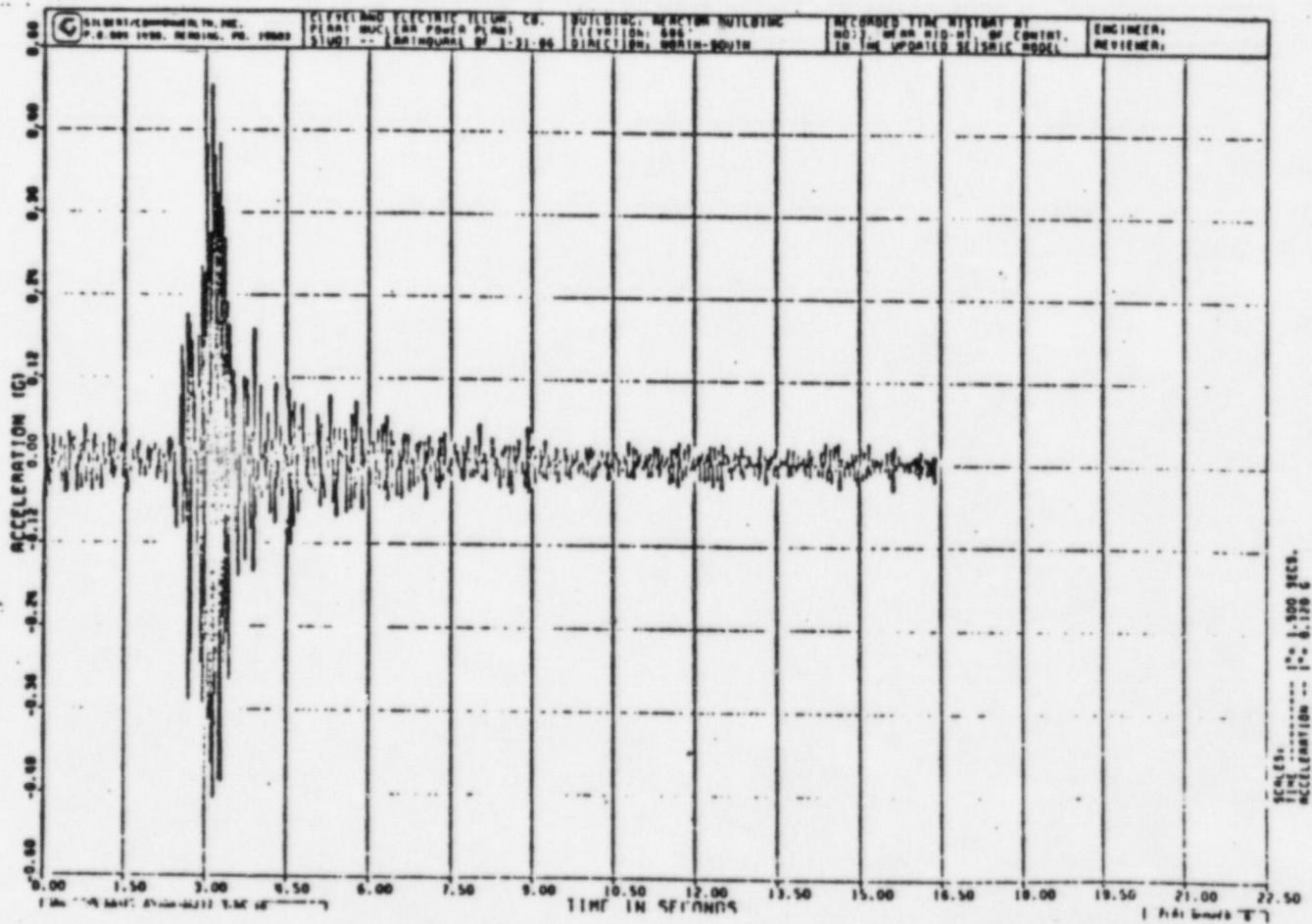
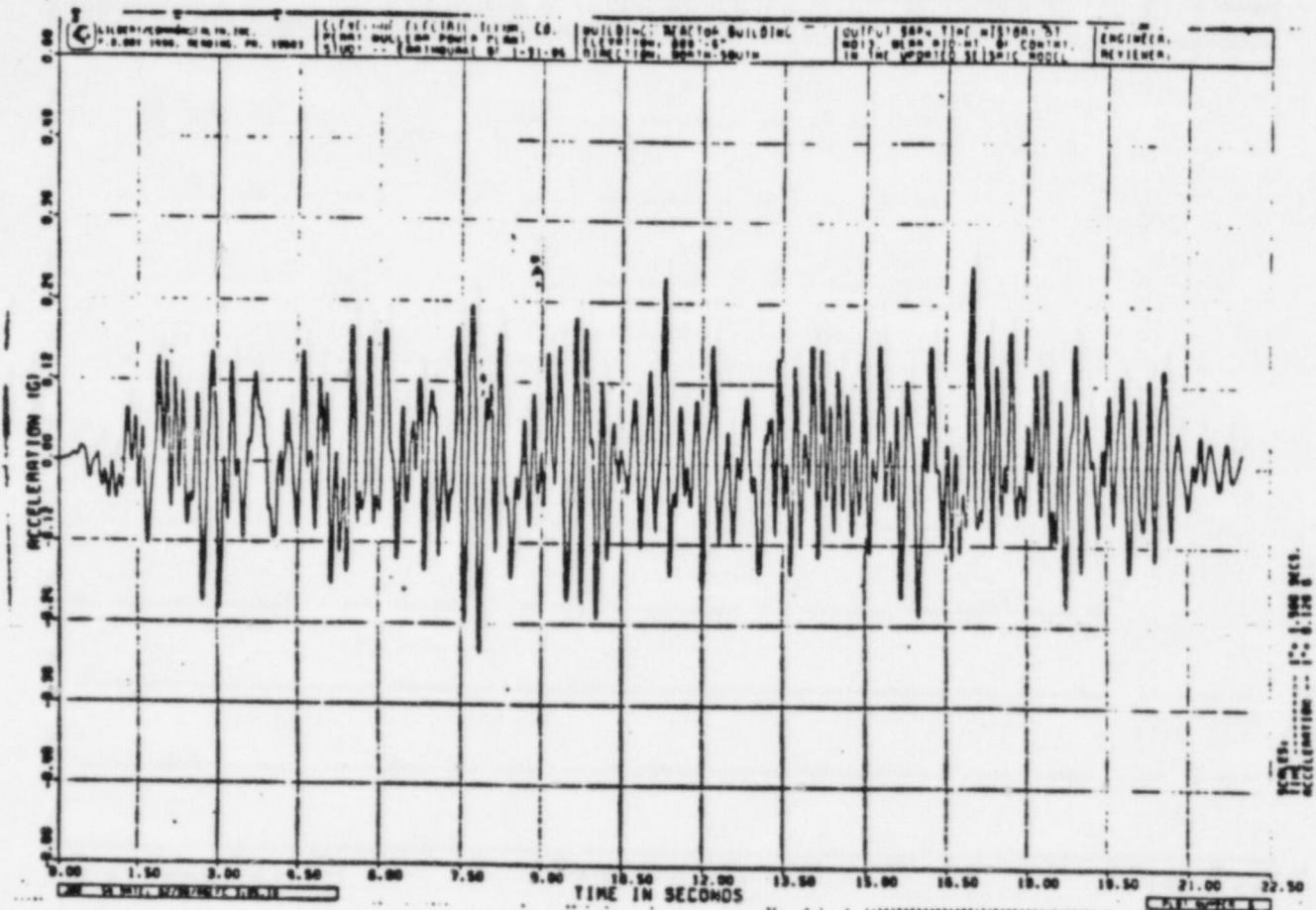
Reactant N.S.



Basement E-W

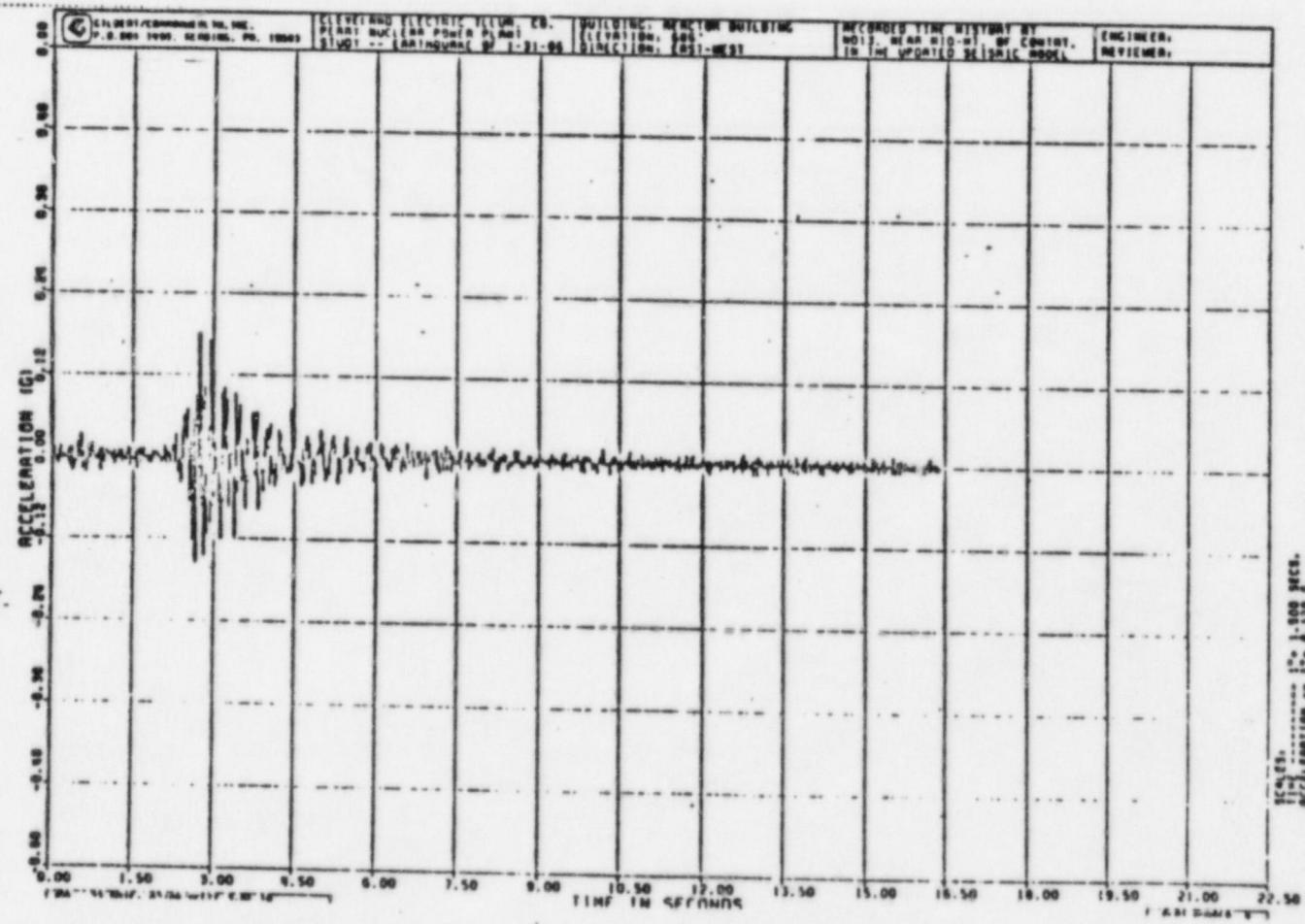
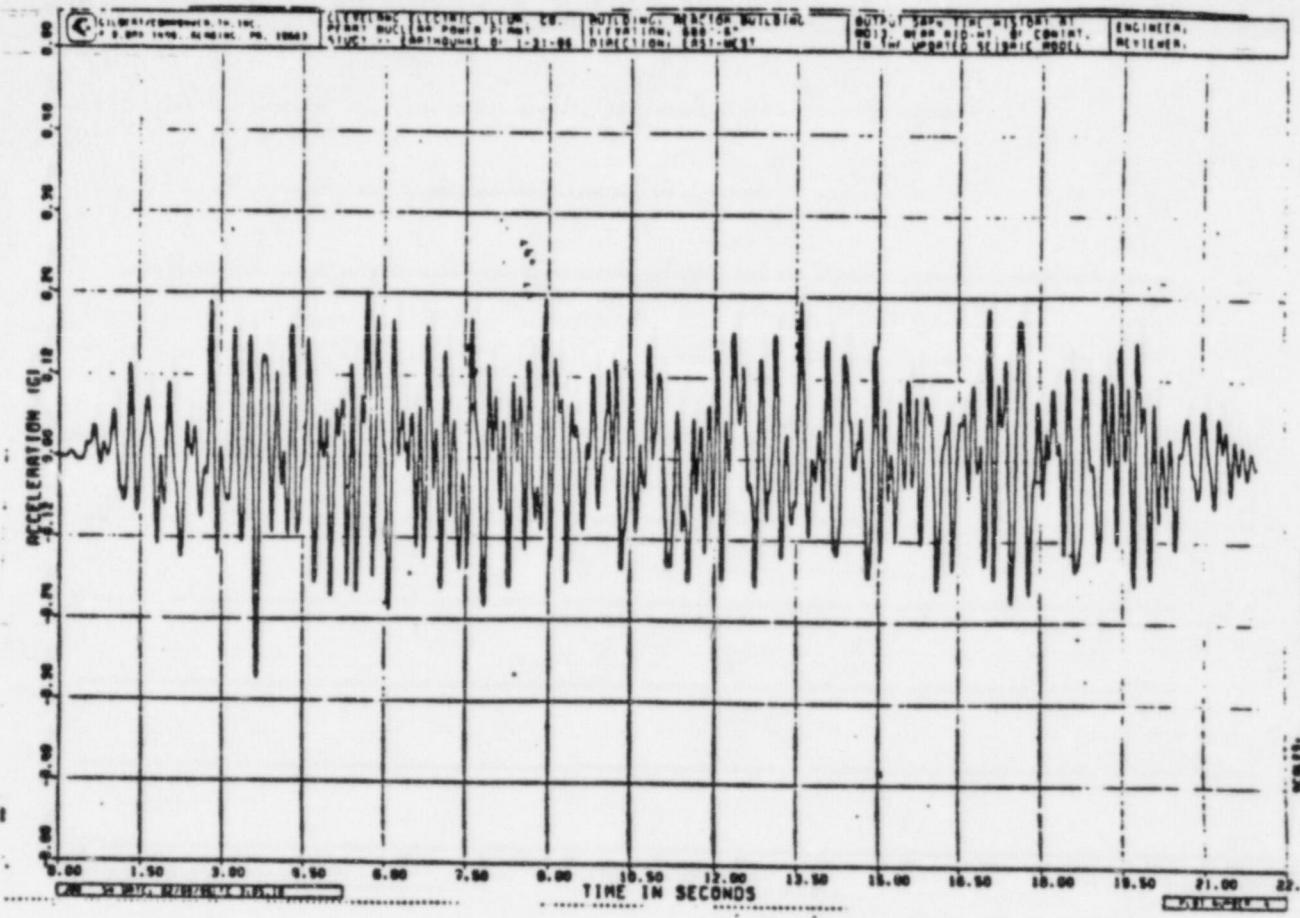


Basement Vert.

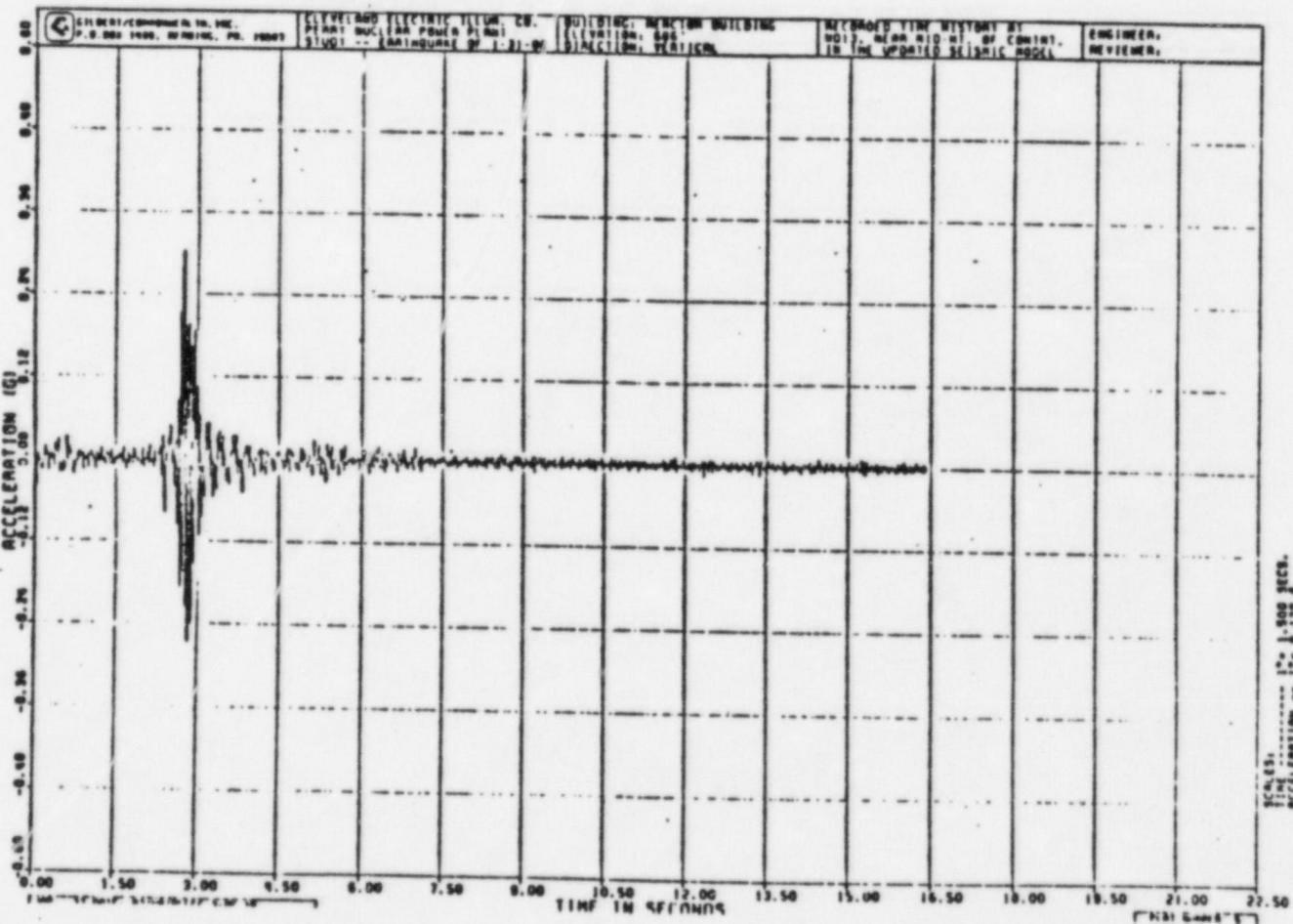
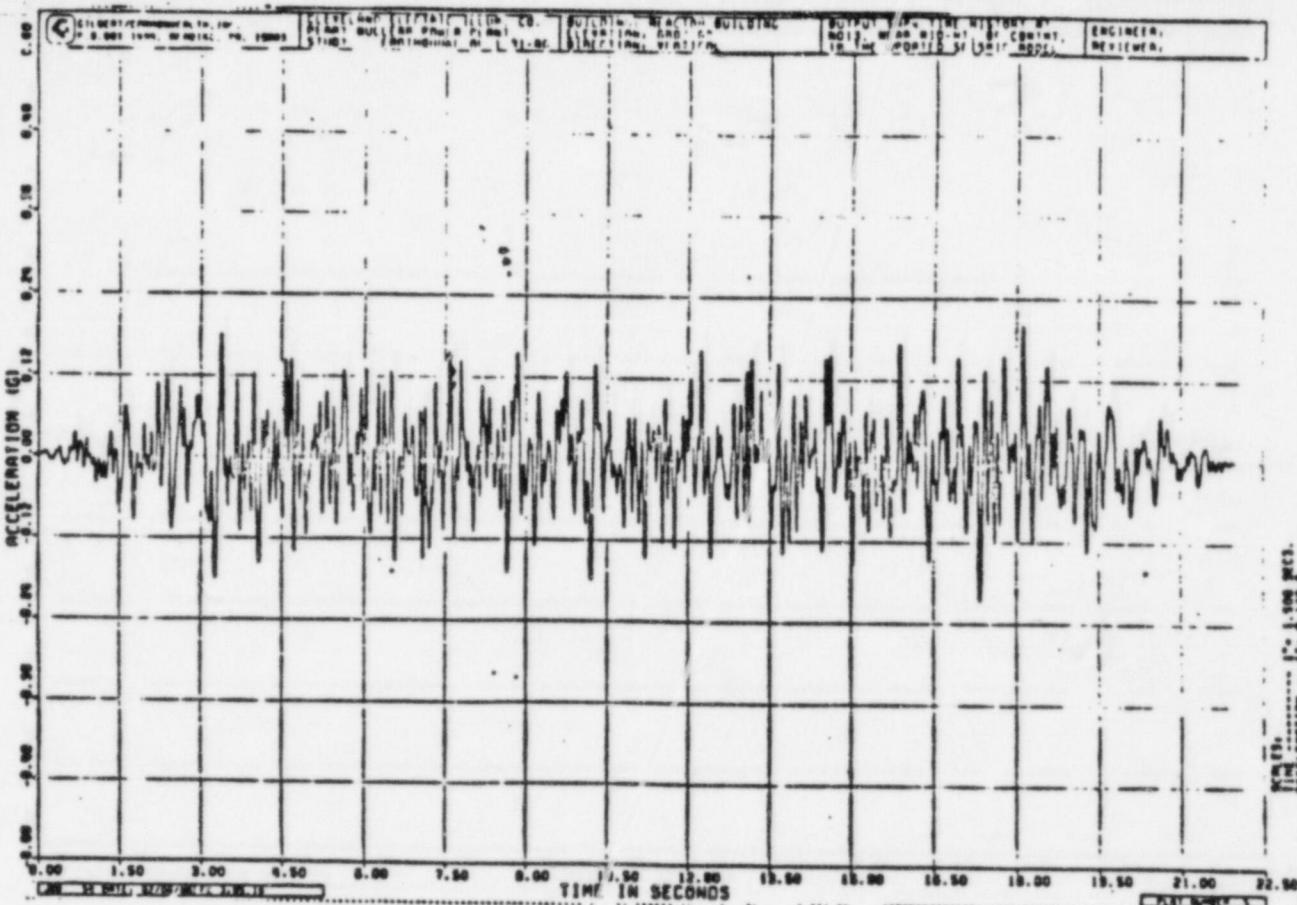


W: Elev

N-S



Hi fitfit  
E-W



H-1 ELEV.

VRRT

## SEISMIC DESIGN BASIS

- BROAD BAND FREQUENCY DESIGN  
RESPONSE SPECTRA
- SMOOTHED, 84 PERCENTILE  
SPECTRA
- COMPOSITE TIME HISTORIES WITH  
LONG DURATIONS AND HIGH  
ENERGY

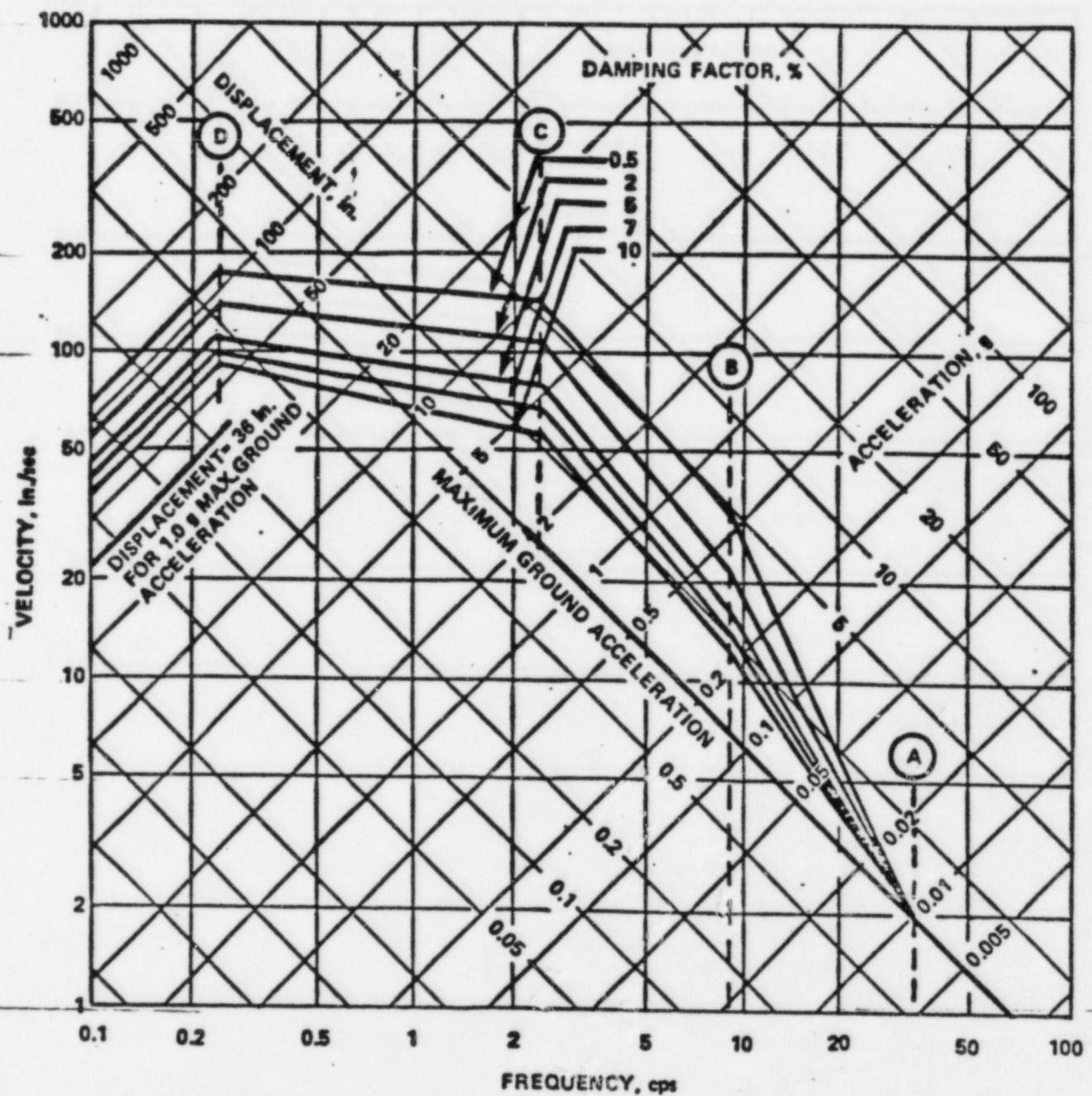
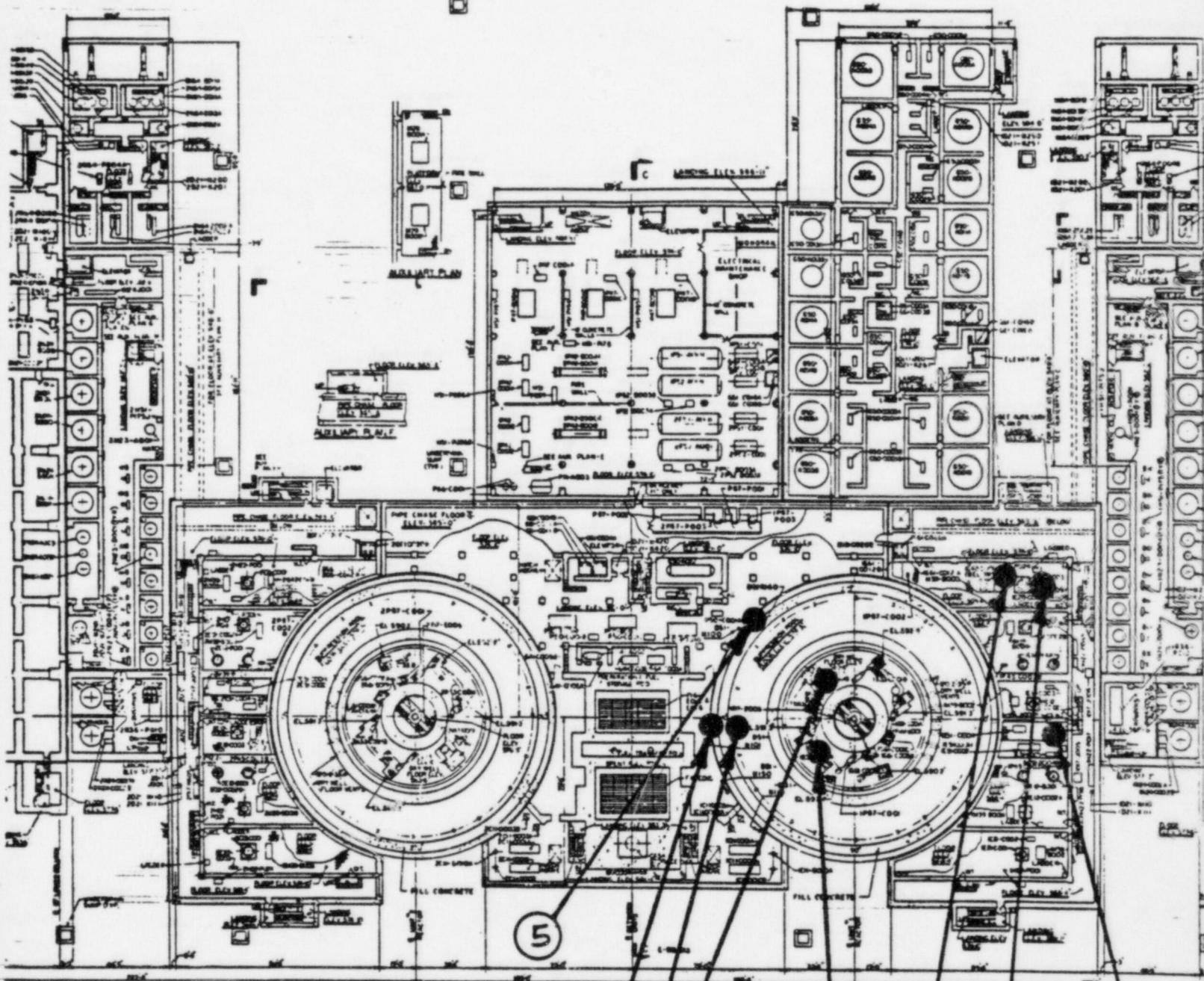
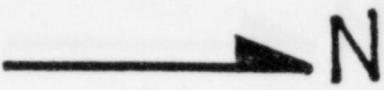
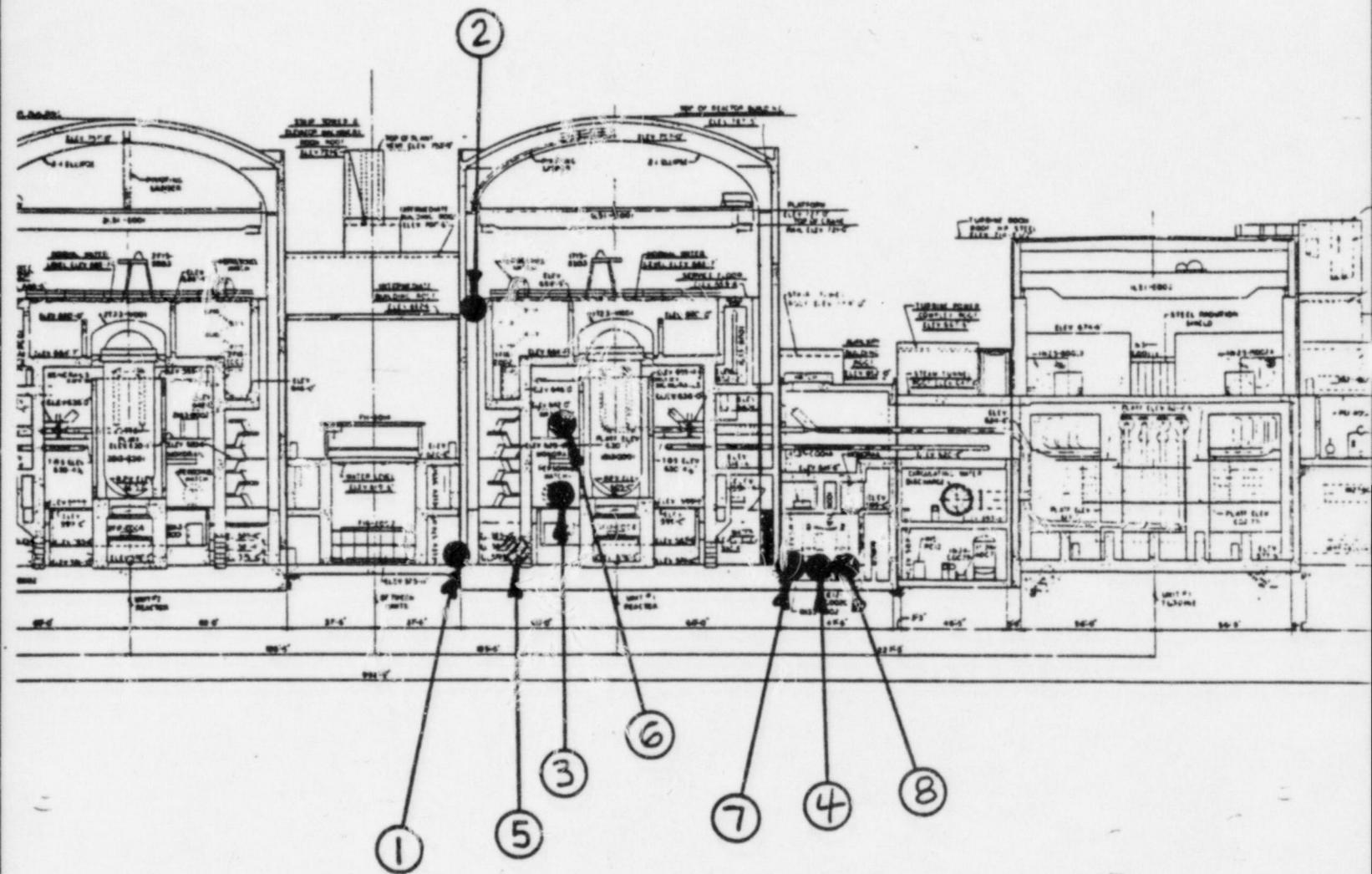


FIGURE 1. HORIZONTAL DESIGN RESPONSE SPECTRA – SCALED TO 1g HORIZONTAL GROUND ACCELERATION



KEY:

- ① Instrument #D51-N101
- ② Instrument #D51-N111
- ③ Instrument #D51-R120
- ④ Instrument #D51-R140
- ⑤ Instrument #D51-R160
- ⑥ Instrument #D51-R170
- ⑦ Instrument #D51-R180
- ⑧ Instrument #D51-R190



1. #D51-N101 R/B Foundation Mat, El. 575', Az. 175°
2. #D51-N111 R/B Containment Vessel, El. 686', Az. 174°
3. #D51-R120 Reactor Recirc Pump, El. 605', Az. 145°
4. #D51-R140 A/B Foundation Mat, El. 568'
5. #D51-R160 R/B Foundation Mat, El. 574' Az. 225°
6. #D51-R170 R/B Platform, El. 630' Az. 238°
7. #D51-R180 A/B Foundation Mat, El. 568'
8. #D51-R190 A/B Foundation Mat, El. 568'



**PERRY NUCLEAR POWER PLANT UNIT NO. 1**  
**SEISMIC MONITORING INSTRUMENTATION**

TABLE IV

Instrument Number	Type	Manufacturer / Model Number	Location	References
D51-N101	(1)	Kinemetrics / SMA-3	Reactor Building Foundation Mat Elevation 575'-10" Azimuth 175°	Figures A and B
D51-N111	(1)	Kinemetrics / SMA-3	Reactor Building Containment Vessel Elevation 686'-0" Azimuth 174°	Figures A and C
D51-R120	(2)	Engdahl / PAR-400	Reactor Recirculation Pump ( Inside Drywell, Reactor Building ) Elevation 605'-0" ( Approximately ) Azimuth 145°	Figures A and D
D51-R130	(2)	Engdahl / PAR-400	OUT OF SERVICE	
D51-R140	(2)	Engdahl / PAR-400	Auxiliary Building Foundation Mat ( HPCS Pump Room ) Elevation 568'-4"	Figures A and E

1. Triaxial Time-History Accelerograph
2. Triaxial Peak Accelerograph
3. Triaxial Response Spectrum Recorder

**PERRY NUCLEAR POWER PLANT UNIT NO. 1**  
**SEISMIC MONITORING INSTRUMENTATION**

TABLE IV

Instrument Number	Type	Manufacturer / Model Number	Location	References
D51-R160	(3)	Engdahl / PSR-1200-H / V-12A	Reactor Building Foundation Mat Elevation 574'-10" Azimuth 225°	Figures A and F
D51-R170	(3)	Engdahl / PSR-1200-H / V	Reactor Building 630' Platform ( Inside Drywell ) Elevation 630'-1" Azimuth 238°	Figures A and G
D51-R180	(3)	Engdahl / PSR-1200-H / V	Auxiliary Building Foundation Mat ( HPCS Pump Room ) Elevation 568'-4"	Figures A and H
D51-R190	(3)	Engdahl / PSR-1200-H / V	Auxiliary Building Foundation Mat ( RCIC Pump Room ) Elevation 568'-4"	Figures A and J

1. Triaxial Time-History Accelerograph
2. Triaxial Peak Accelerograph
3. Triaxial Response Spectrum Recorder

## ZPA COMPARISON

- ZERO PERIOD ACCELERATION
- RECORDED ZPA'S VARY FROM  
BELOW OBE VALUES TO 74% OF  
SSE VALUES
- EXCEPT AT CONTAINMENT VESSEL  
ELEVATION 686'
- BUT RELATIVE DISPLACEMENTS  
AND STRESSES HERE (AS WELL AS  
ALL OTHER LOCATIONS) ARE LOW

~~below~~ below  
OBE design  
value

### REASON:

- HIGH FREQUENCY AND LOW  
ENERGY OF THE 1986  
EARTHQUAKE

TABLE II  
Comparison of Design ZPA's<sup>1</sup> VS Recorded ZPA's  
(Expressed in g values)

		Auxiliary Building Foundation Mat Elevation 568' PAR 400 (Engdahl) D51-R140	Reactor Building Foundation Mat Elevation 574'-10" SMA-3 (Kinematics) D51-N101	Reactor Building Recirculation Pump Elevation 605" PAR 400 (Engdahl) D51-R120	Reactor Building Platform Elevation 630' Inside Drywell PSR 1200 (Engdahl) D51-R170	Reactor Building Containment Vessel Elevation 686' SMA-3 (Kinematics) D51-N111
NS	Recorded	.17	.18	.32	.09	.55
	SSE	.17	.18	1.06	.48	.40
	OBE	.10	.10	.86	.40	.24
EW	Recorded	.06	.10	.11	.16	.18
	SSE	.20	.18	1.06	.48	.40
	OBE	.10	.10	.86	.40	.24
VERT.	Recorded	.03	.11	.05	Note 2	.30
	SSE	.20	.18	.47	.28	.24
	OBE	.10	.10	.38	.16	.15
SRSS <sup>3</sup>	Recorded	.18	.23	.34	Note 2	.65
	SSE <sup>4</sup>	.33	.31	1.57	.73	.62
	OBE	.17	.17	1.27	.59	.37

1. Zero period acceleration

2. ZPA indeterminable from available data

3. Square-root-of-the-sum of the squares

4. Licensing basis is SSE

TABLE I  
**Comparison of Design Displacements<sup>1</sup> VS Recorded Displacements<sup>1</sup>**  
 (Expressed in centimeters / one inch = 2.54 cm)

		COLUMN 1	COLUMN 2	COLUMN 2 minus COLUMN 1
		Reactor Building Foundation Mat Elevation 574'-10" SMA-3 (Kinematics) D51-N101	Reactor Building Containment Vessel Elevation 686' SMA-3 (kinematics) D51-N111	Relative Displacements for the Containment Vessel
NS	Recorded	0.09	0.17	0.08
	SSE	0.044	0.28	0.24
	OBE	0.023	0.17	0.15
EW	Recorded	0.16	0.21	0.05
	SSE	0.044	0.28	0.24
	OBE	0.023	0.17	0.15
VERT.	Recorded	0.05	0.07	0.02
	SSE	0.02	0.37	0.017
	OBE	0.013	0.022	0.009
SRSS <sup>2</sup>	Recorded	—	—	0.1
	SSE	—	—	0.34
	OBE	—	—	0.21

1. Displacements based on same time-step to determine relative displacements
2. Square-root-of-the-sum of the squares

## RESPONSE SPECTRA COMPARISON

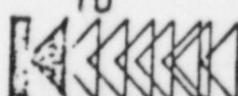
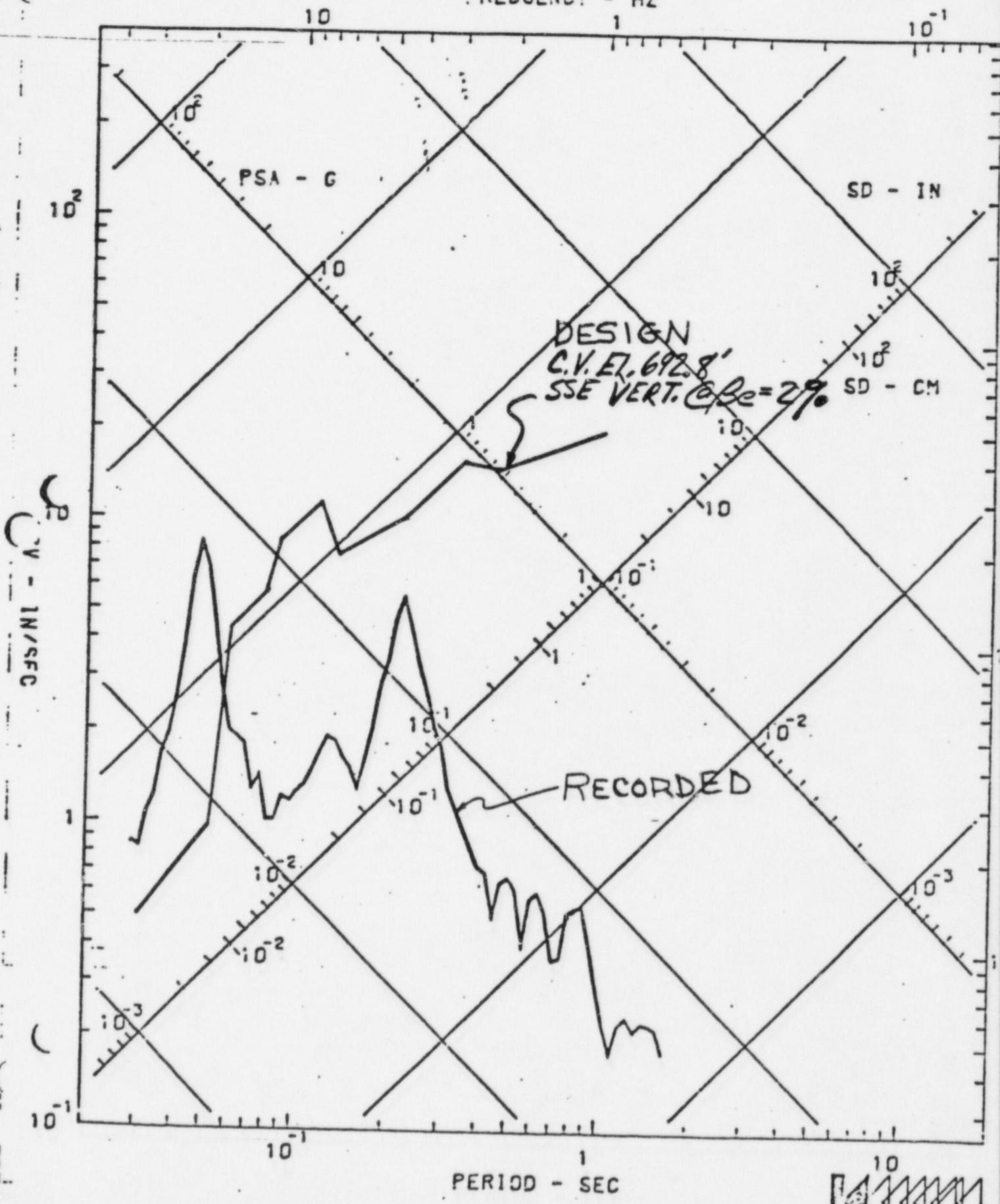
- PERRY DESIGN RESPONSE SPECTRA ARE FAR ABOVE THE RECORDED SPECTRA IN THE FREQUENCY REGION BELOW 14 Hz.
- CERTAIN RECORDED RESPONSE SPECTRA EXCEED DESIGN SPECTRA VALUES IN THE REGION AROUND 20 Hz.
- CORRESPONDING SMALL DISPLACEMENTS  
(EXAMPLE: 3/100 INCHES OR BELOW AT FOUNDATION MAT)
- NO ENGINEERING SIGNIFICANCE
- RECORDED VELOCITY SPECTRA SHOW MUCH LESS ENERGY THAN THE DESIGN RESPONSE SPECTRA

11AB002

## PERRY NUCLEAR POWER PLANT

COMP UP

SMAJS/N 165

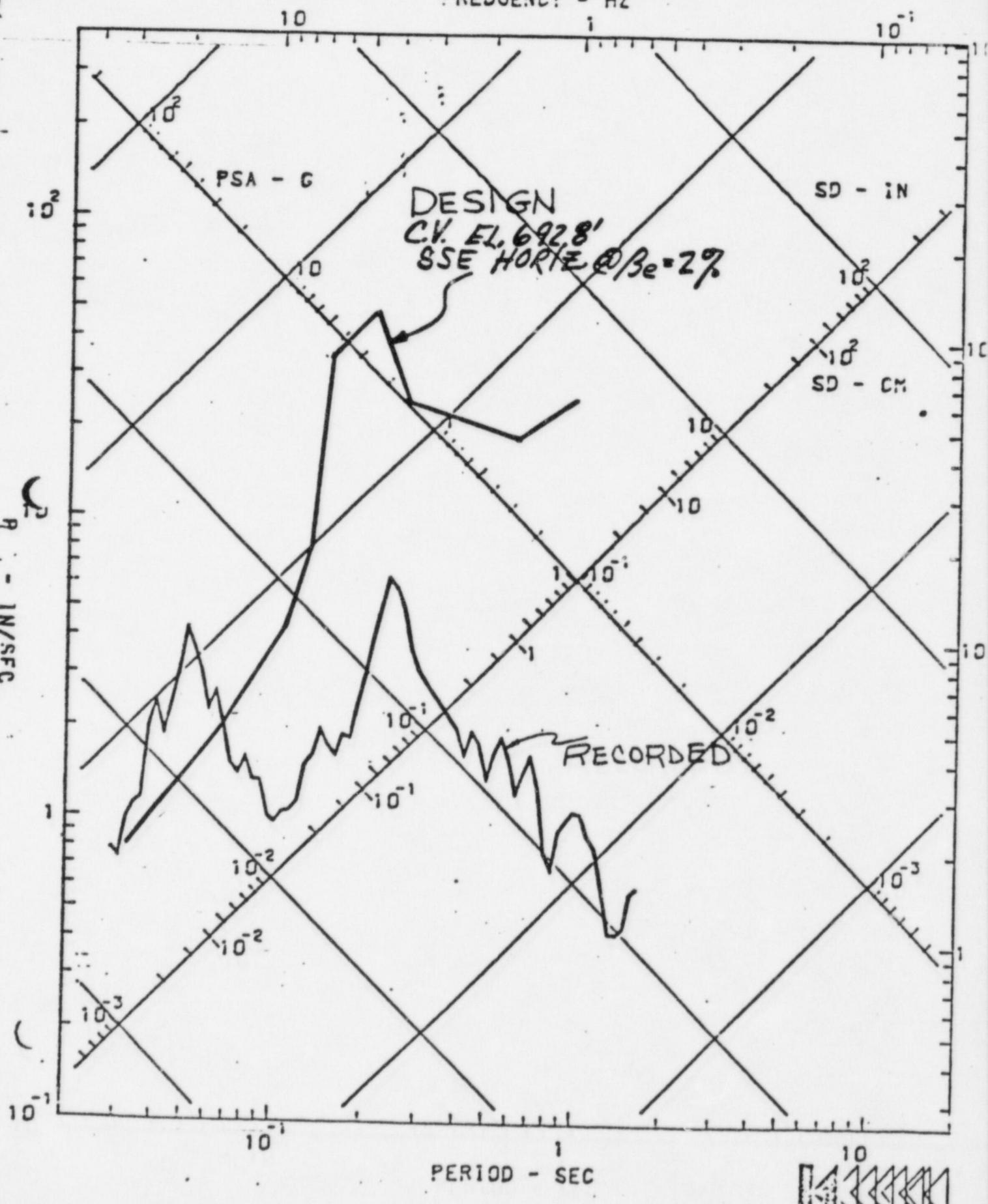
DAMPING VALUES ARE 2 PERCENT OF CRITICAL  
FREQUENCY - HZ

11A6002

PERRY NUCLEAR POWER PLANT

COMP WEST

SMA35/N 165-2

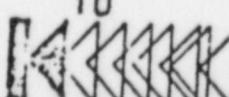
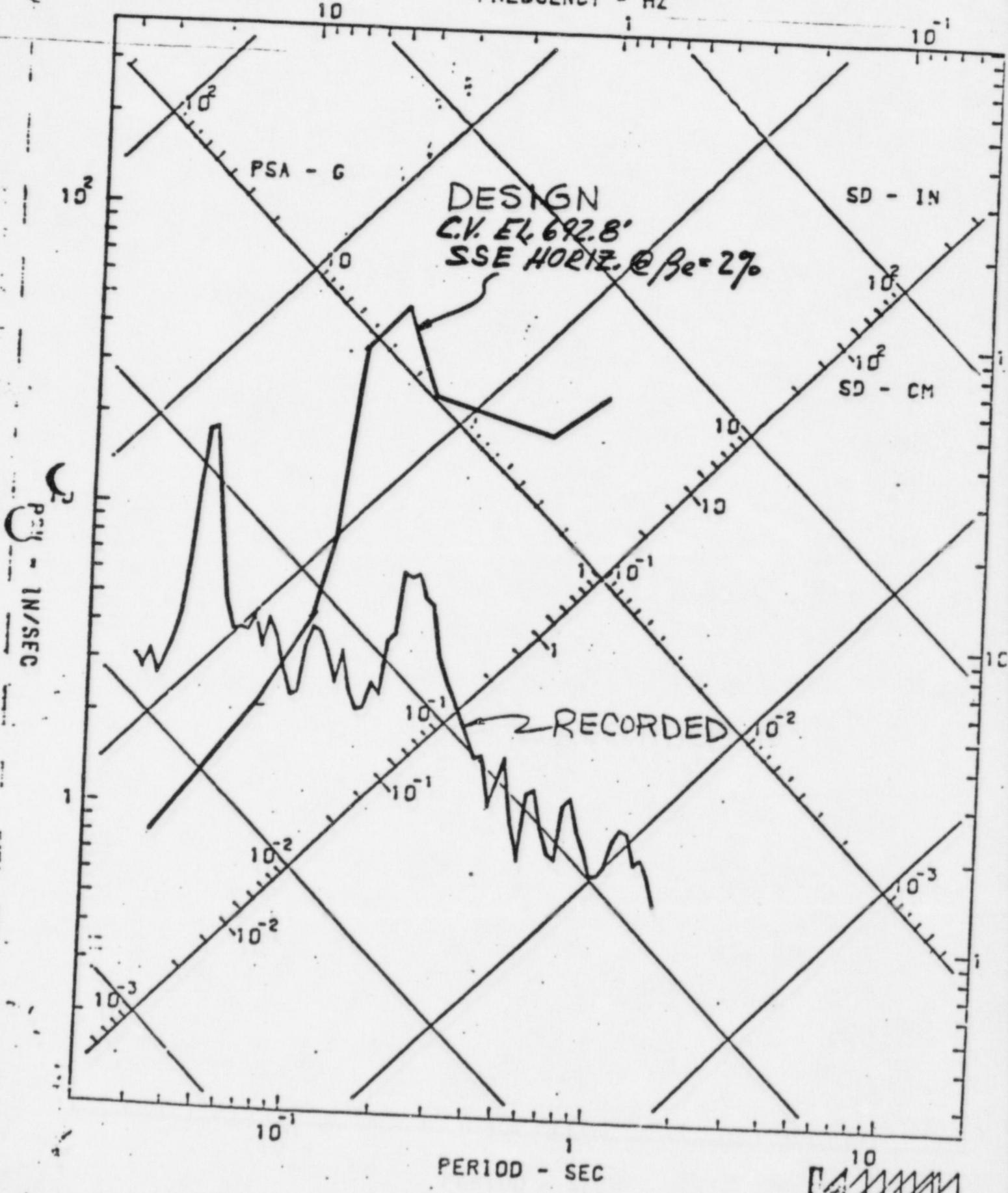
DAMPING VALUES ARE 2 PERCENT OF CRITICAL  
FREQUENCY - HZ

IIA8002

## PERRY NUCLEAR POWER PLANT

COMP SOUTH

SMA35/N 165

DAMPING VALUES ARE 2 PERCENT OF CRITICAL  
FREQUENCY - HZ

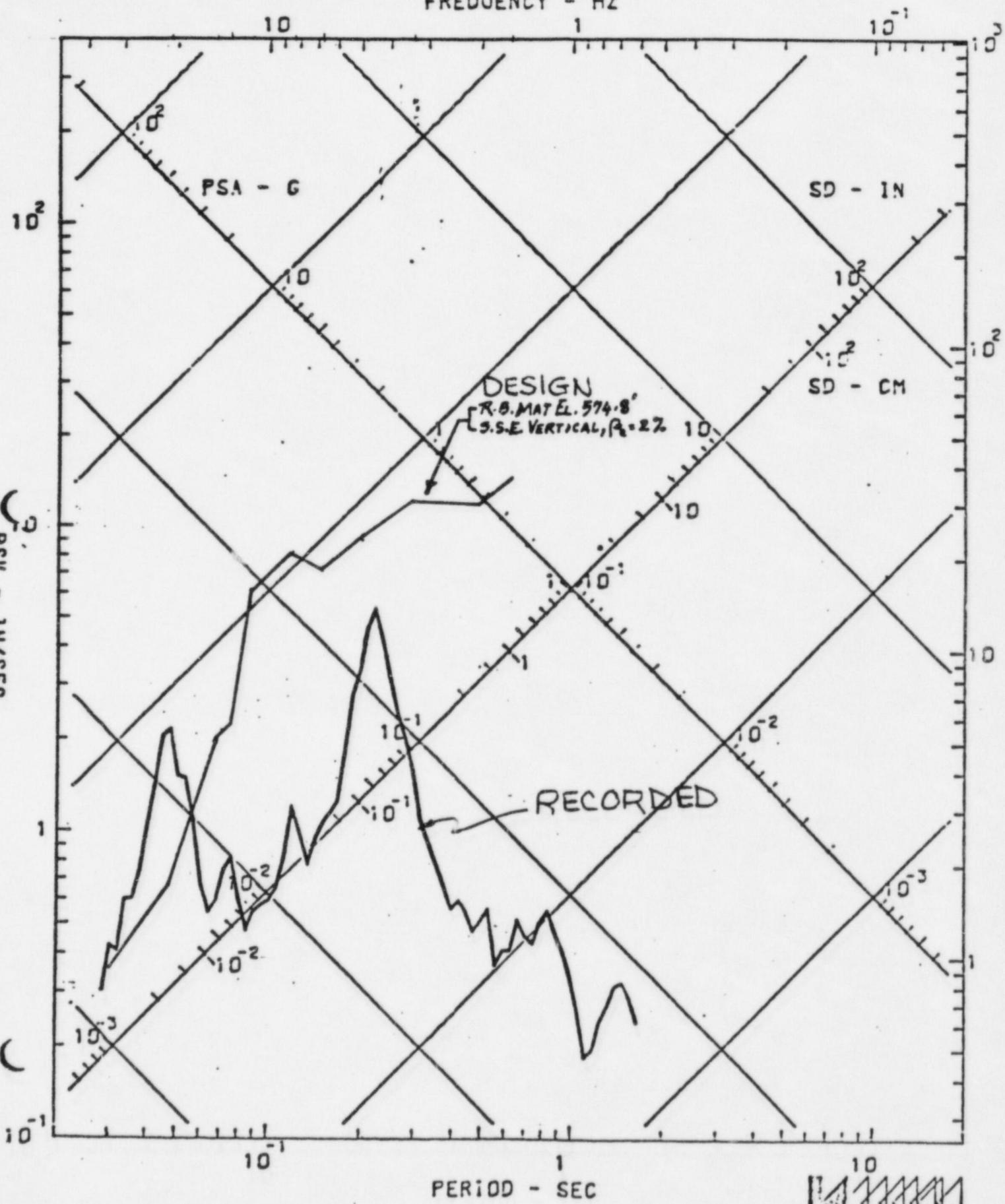
IIAB001

## PERRY NUCLEAR POWER PLANT

COMP UP

SMADE/N 165-1V

DAMPING VALUES ARE 2 PERCENT OF CRITICAL  
FREQUENCY - HZ



ML 5.5 EARTHQUAKE JANUARY 31, 1986

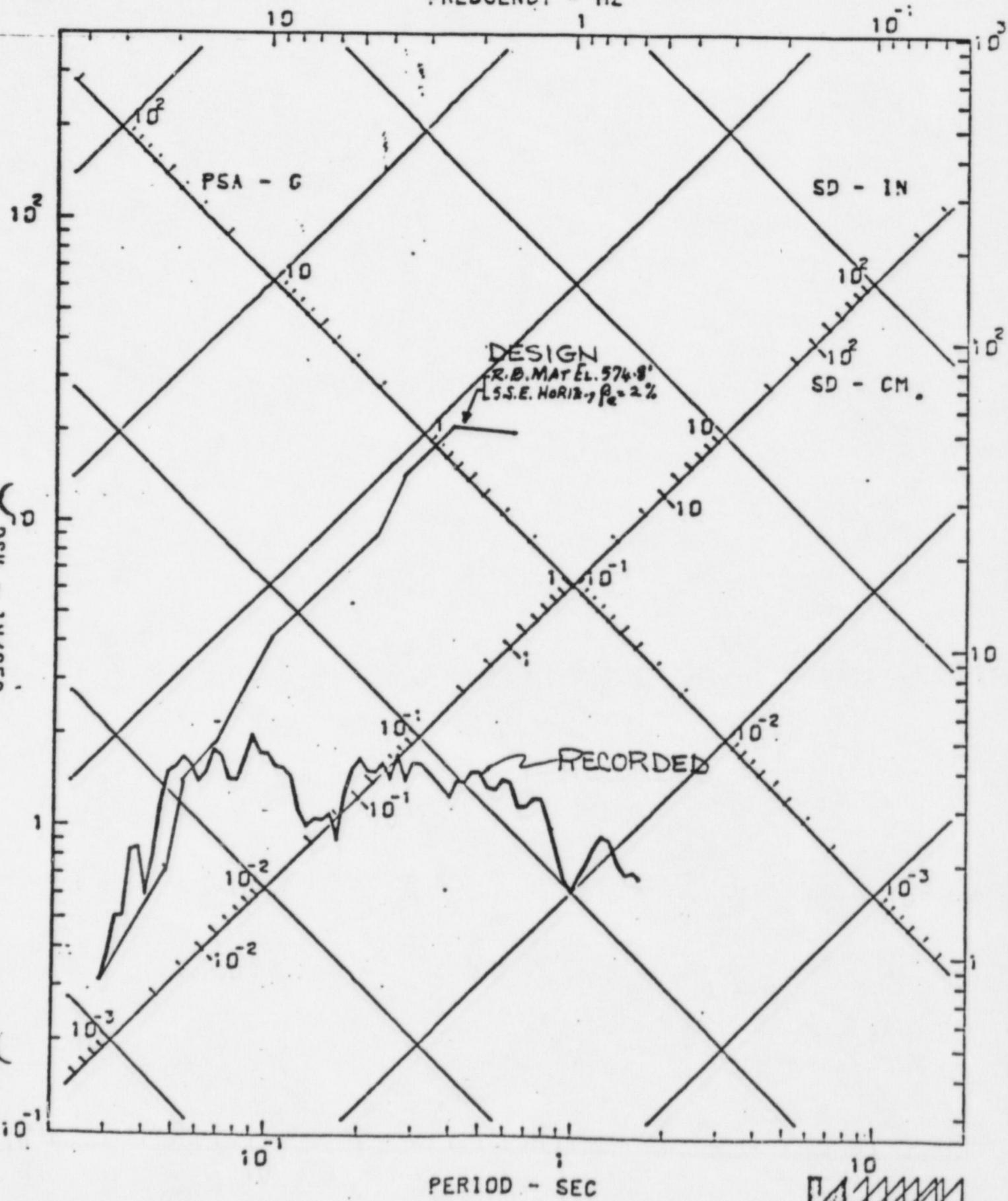
ICCBQ01

PERRY NUCLEAR POWER PLANT

COMP WEST

SMA3S/N 165-1T

DAMPING VALUES ARE 2 PERCENT OF CRITICAL  
FREQUENCY - Hz



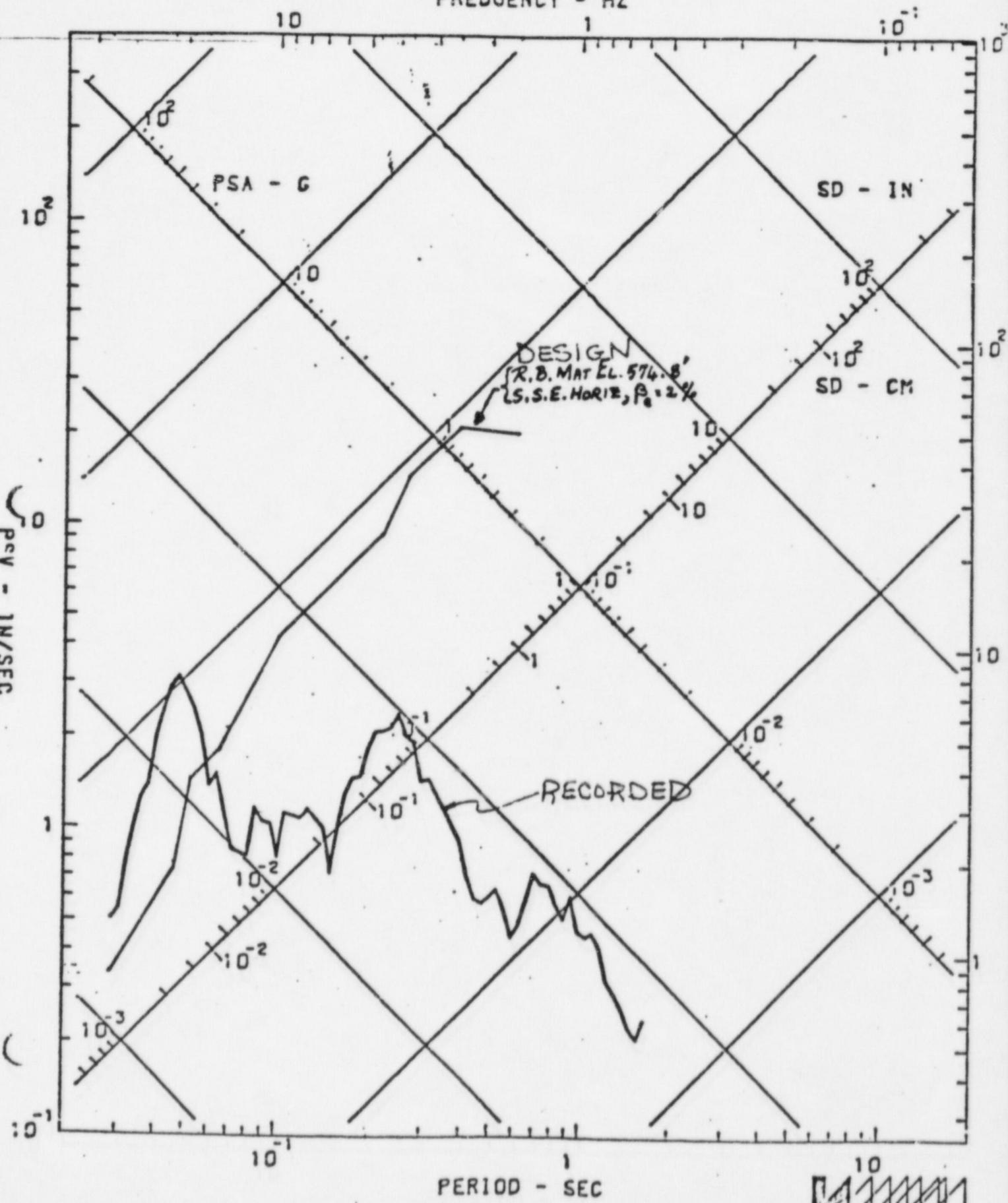
143300

IIA8001

## PERRY NUCLEAR POWER PLANT

COMP SOUTH

SMAJS/N 165-1L

DAMPING VALUES ARE 2 PERCENT OF CRITICAL  
FREQUENCY - HZ

## VERIFICATION OF THE LACK OF ENGINEERING SIGNIFICANCE OF THE 1986 OHIO EARTHQUAKE

- PROOF TEST - PLANT STRUCTURES UNAFFECTED  
- PLANT EQUIPMENT UNAFFECTED
- OTHER INDUSTRIAL CRITERIA CONFIRM THE CONCLUSIONS
  - PILE DRIVING OR BLASTING OPERATIONS - USE 1 INCH/SEC. PARTICLE VELOCITY AS THE NON-DAMAGE THRESHOLD FOR NON-ENGINEERED STRUCTURES
  - THE RECORDED MAXIMUM ACCELERATION AT THE PERRY FOUNDATION MAT IS ONLY 0.87 INCH /SEC.
- IEEE 344 PROHIBITS QUALIFICATION BY SHOCK-TYPE TESTING (LOW ENERGY, HIGH FREQUENCY, SHORT DURATION)

*Basis  
Qual.  
considered  
impact of  
strong motion  
earthquake -*

## BUILT IN CONSERVATISMS OF PLANT DESIGN

- BROADENING AND ENVELOPING PROCESS OF FLOOR RESPONSE SPECTRA.
- EQUIPMENT QUALIFICATION BY GENERIC TESTS.
- STRAIN HARDENING NOT ACCOUNTED FOR AND STATIC ALLOWABLES USED FOR DYNAMIC LOADS.
- LOADING COMBINATIONS.
- PRIMARY STRESSES VS. SECONDARY STRESSES.
- DAMPING VALUES.
- RESPONSES OF EL CENTRO STEAM PLANT.

## CONCLUSION

### THE 1986 OHIO EARTHQUAKE:

- HIGH FREQUENCIES
- SHORT DURATION
- LOW ENERGY
- LOW VELOCITY
- SMALL DISPLACEMENT

No need to concern  
with hydrodynamic loads  
because of the insignificant  
deformation capacity needed is  
design response spectra -  
G.A. in process of finalizing  
stems and responses -

margin ground motion criteria  
when to be completed?

## SUMMARY AND CONCLUSIONS

- o PROOF TEST OF SEISMIC DESIGN
  - JANUARY 31, 1986 EARTHQUAKE -  
INTENSITY VI, 4.96 RICHTER
  - PLANT STRUCTURES AND SYSTEMS  
UNAFFECTED BY EARTHQUAKE
- o NO CHANGE TO CONCLUSIONS ON GEOLOGY AND SEISMOLOGY
  - DESIGN EARTHQUAKE BOUNDS JANUARY 1986 EVENT  
(MAGNITUDE, ENERGY ETC.)
  - INCLUSION OF RECENT EVENT WOULD NOT CHANGE  
DESIGN SPECTRUM
- o PLANT SEISMIC CAPABILITY ABLE TO ACCOMODATE JANUARY  
EARTHQUAKE
  - SHORT DURATION, HIGH FREQUENCY, LOW ENERGY  
LOW VELOCITY, SMALL DISPLACEMENT
  - MEASURED RESPONSE EXCEEDANCES OF NO  
ENGINEERING SIGNIFICANCE
- o FOLLOW ON ACTIVITIES
  - CONFIRMATORY PROGRAMS
  - SUPPORT OF GENERIC, INDUSTRY STUDIES
  - SOG, SQUG, EPRI

cc:	H. Denton	S. Brocoum
	D. Eisenhut	L. Heller
	R. Bernero	N. Chokshi
	W. Butler	L. Shao, RES
	G. Lainas	G. Bagchi
<del>J.</del>	Stefano	G. Giese Koch
	S. Stern	P. T. Kuo
	T. Speis	R. Rothman
	B. Sheron	A. Lee
	N. Anderson	P. Sobel
	Lic. Div. Directors	R. Hermann
	Lic. Div. A/Ds	C. P. Tan
	G. Arlotto, RES	
	J. Richardson, RES	
	C. Paperiello, Reg. III	

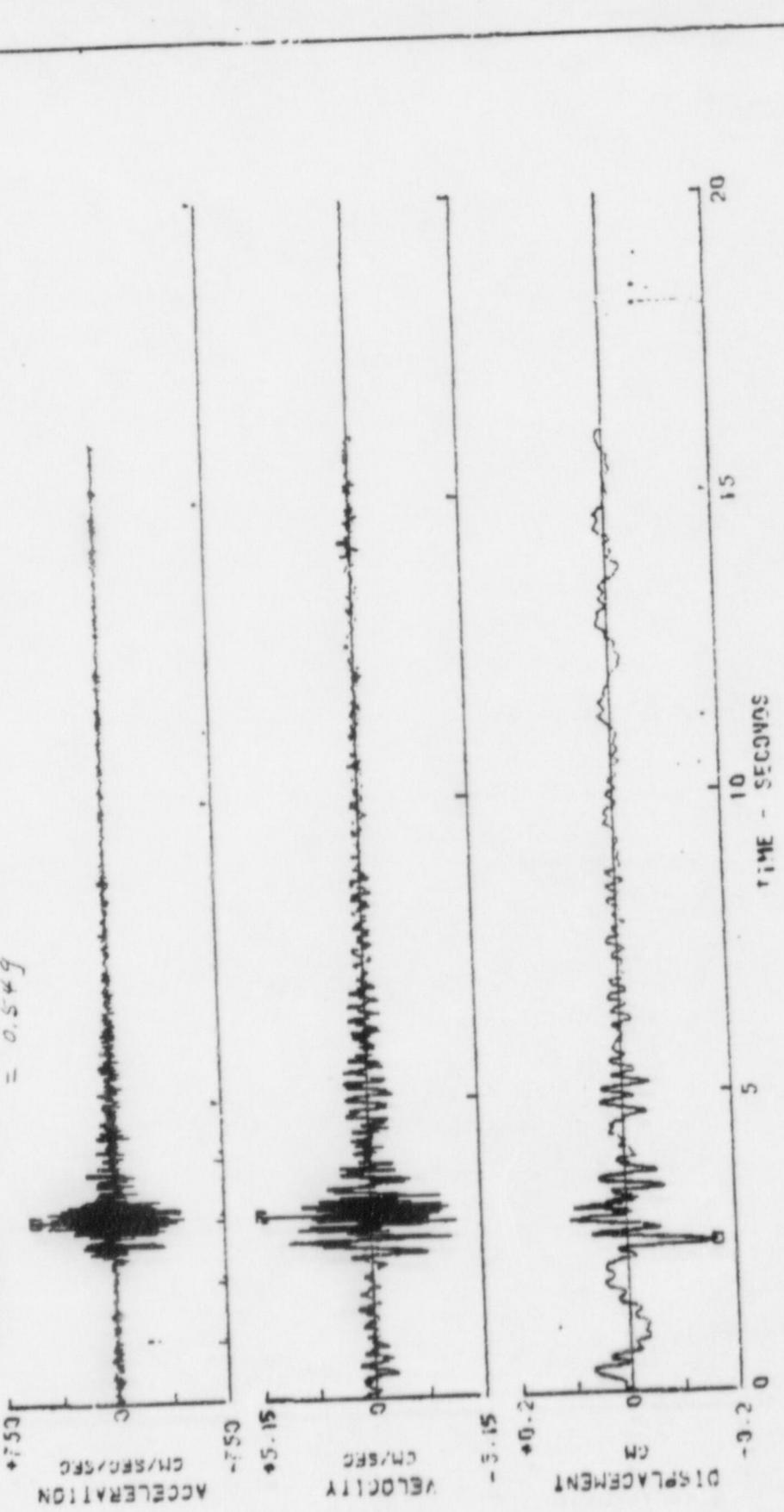


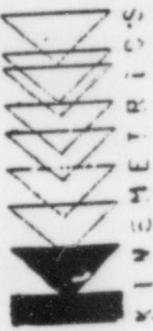
682, Contingent  
N/024 - 5/24

682, Contingent  
N/024 - 5/24

ML 5.0 EARTHQUAKE JANUARY 31, 1985

DEBRI NUCLEAR PLANT  
ACCELEROMETER IS BAND-PASSED FILTERED BETWEEN 0.400-  
0.433 AND 2.25 AND 3.00 HERTZ  
ACCELERATION VALUES: ACCEL = 0.355-0.7 CM/SEC/SEC  
VELOCITIES: VEL = 0.5-1.3 CM/SEC SEC  
DISPLACEMENTS: DISPL = 0.17 CM





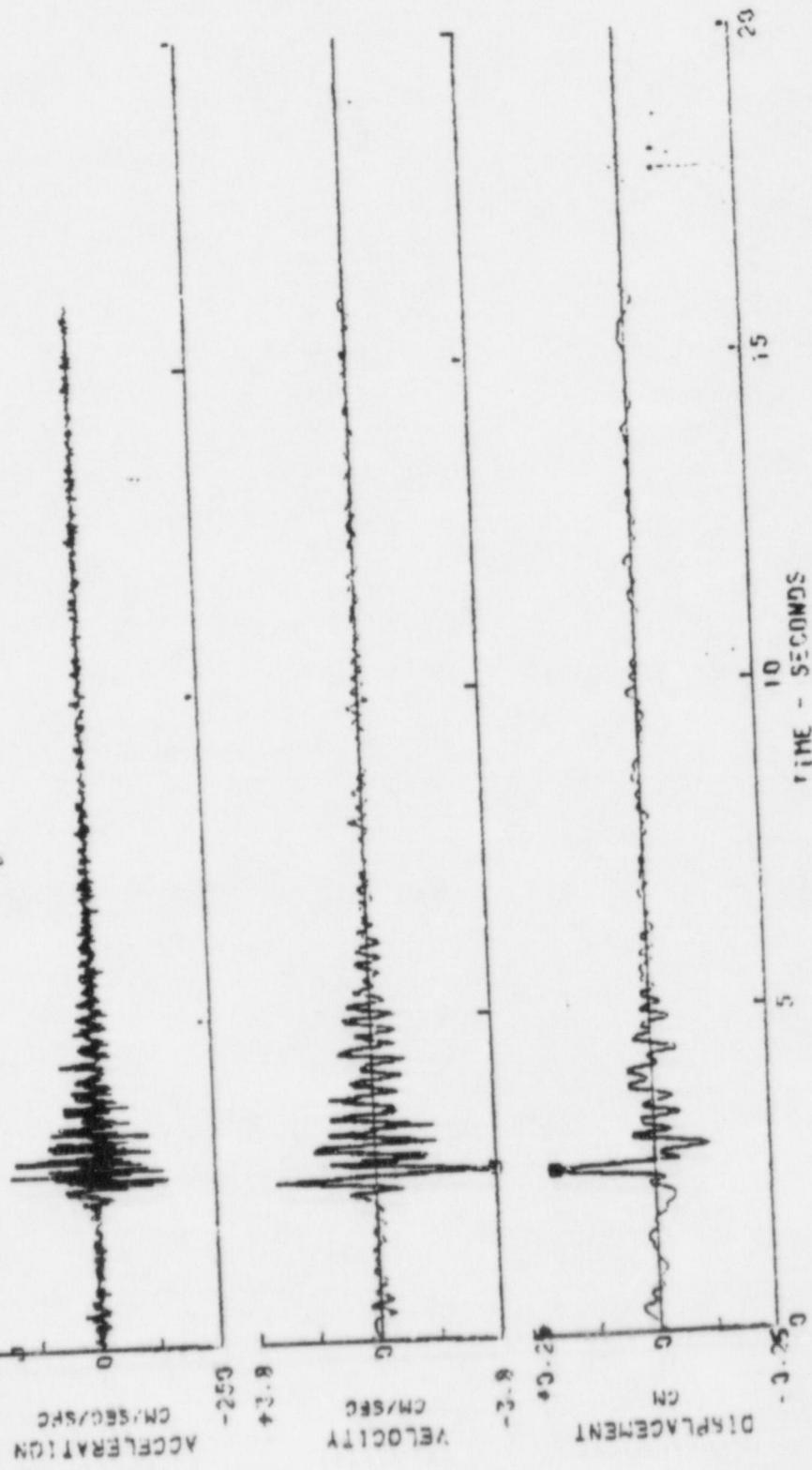
INSTRUMENTS

62-L Containment

East - West

ML 5.0 EARTHQUAKE JANUARY 31, 1985  
PERRY NUCLEAR POWER PLANT COMP WEST  
ACCELEROMETER IS BAND-PASS FILTERED BETWEEN 0.00- 3.625 AND  
PEAK VALUES: ACCEL = +17.9 .35 CM/SEC. SEC VEL = -3.77 CM/SEC SEC

$$= 0.183 g$$



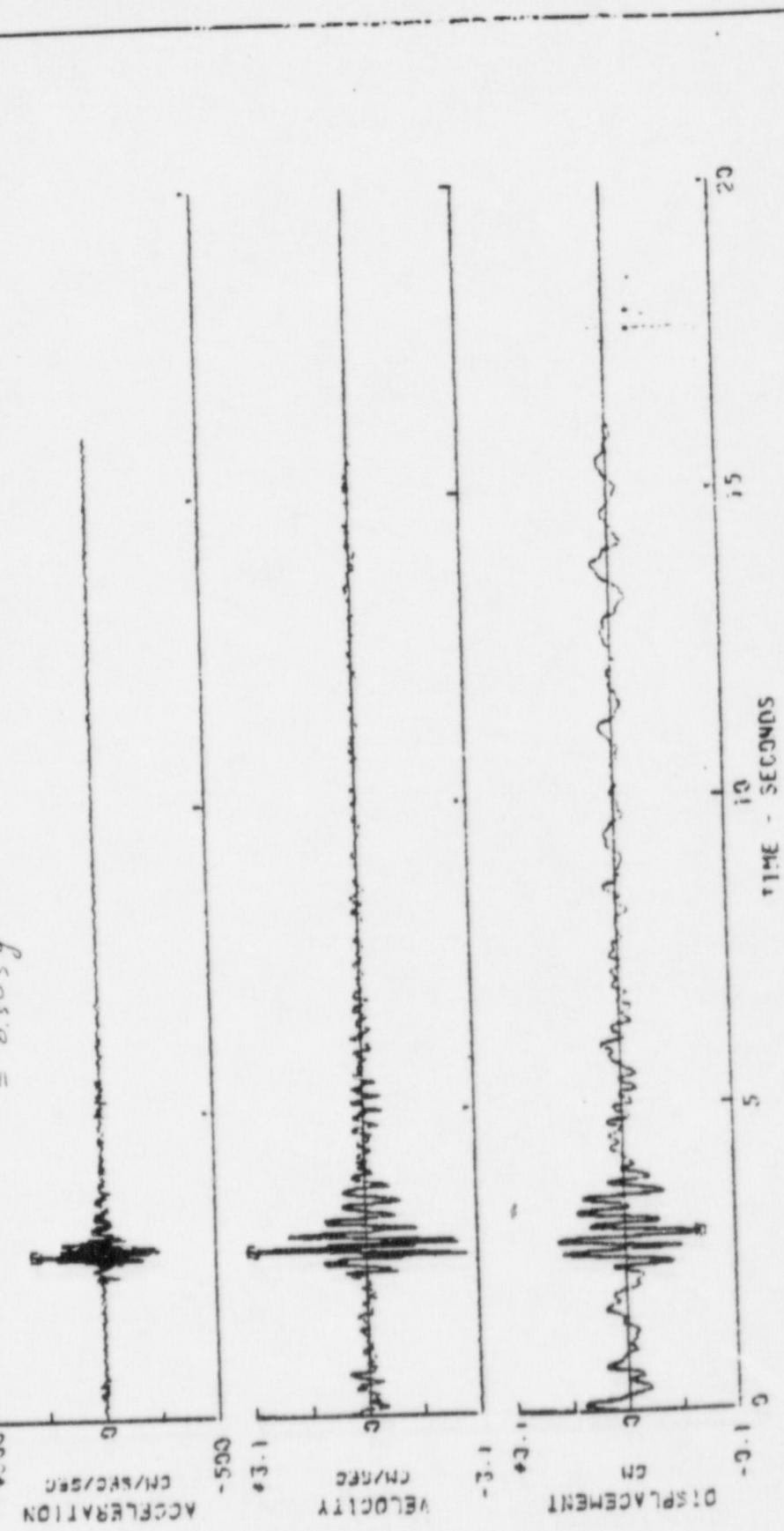


KINEMETRICS  
682, Cont.

ML 5.0 EARTHQUAKE JANUARY 31, 1986

114900Z PERIN NUCLEAR COFFEE PLANT  
ACCELERGRAM IS BAND-PASS FILTERED BETWEEN 0.400- 3.625 AND  
0 PEAK VALUES: ACCEL = 0.207-0.21 G/SEC/SEC

$$\text{PEAK VALUE} = \text{ACCEL} \times 2.36 \text{ SEC/SEC} = 0.303 g$$



ML 5.0 EARTHQUAKE JANUARY 31, 1986

NORTH-SOUTH  
575

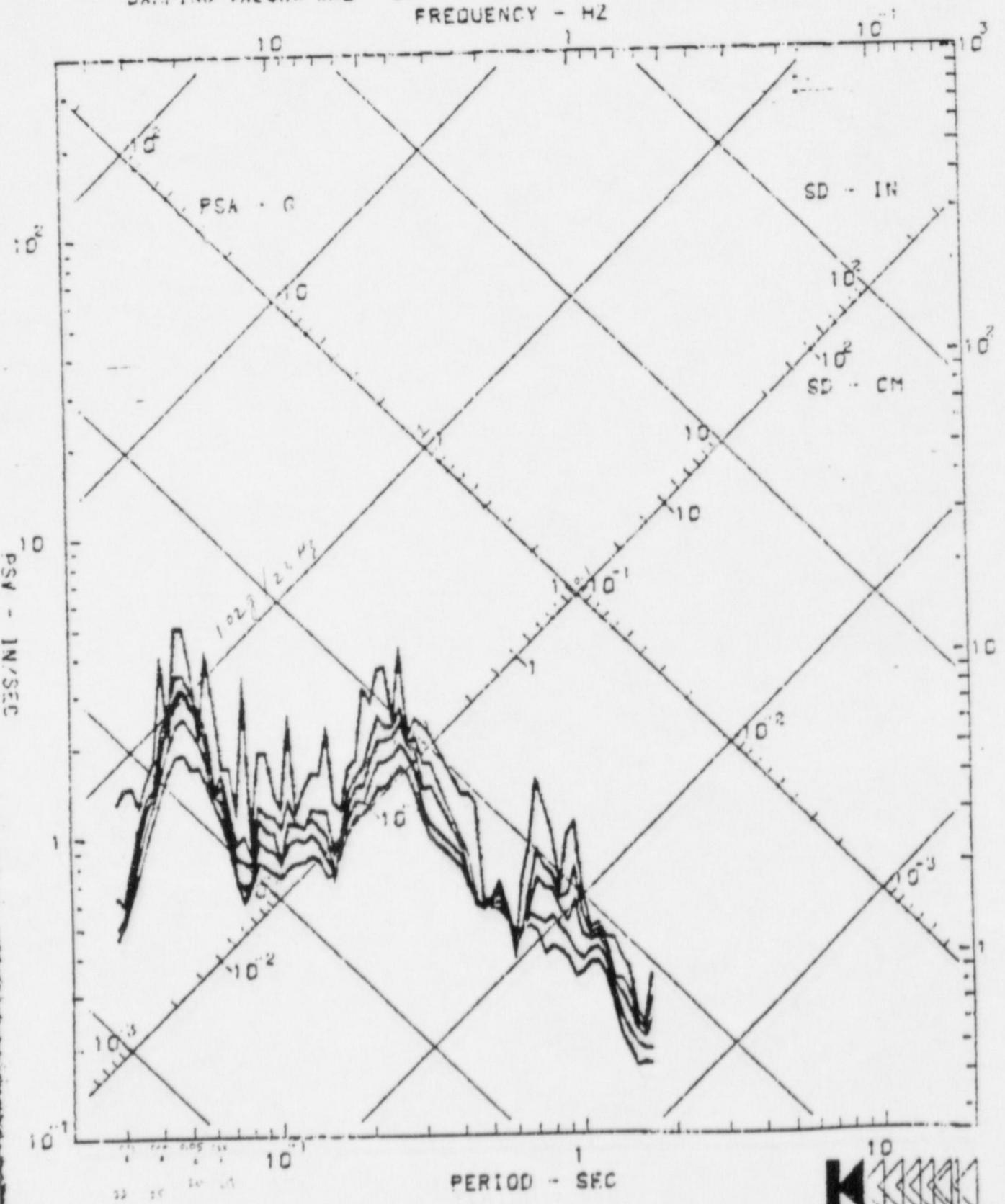
11AR001

PERRY NUCLEAR POWER PLANT

COMP SOUTH

SMA3S/N 165-1L

DAMPING VALUES ARE 0, 1, 2, 4, 7 PERCENT OF CRITICAL  
FREQUENCY - HZ



ML 5.0 EARTHQUAKE JANUARY 31, 1986

EAST-WEST 575'

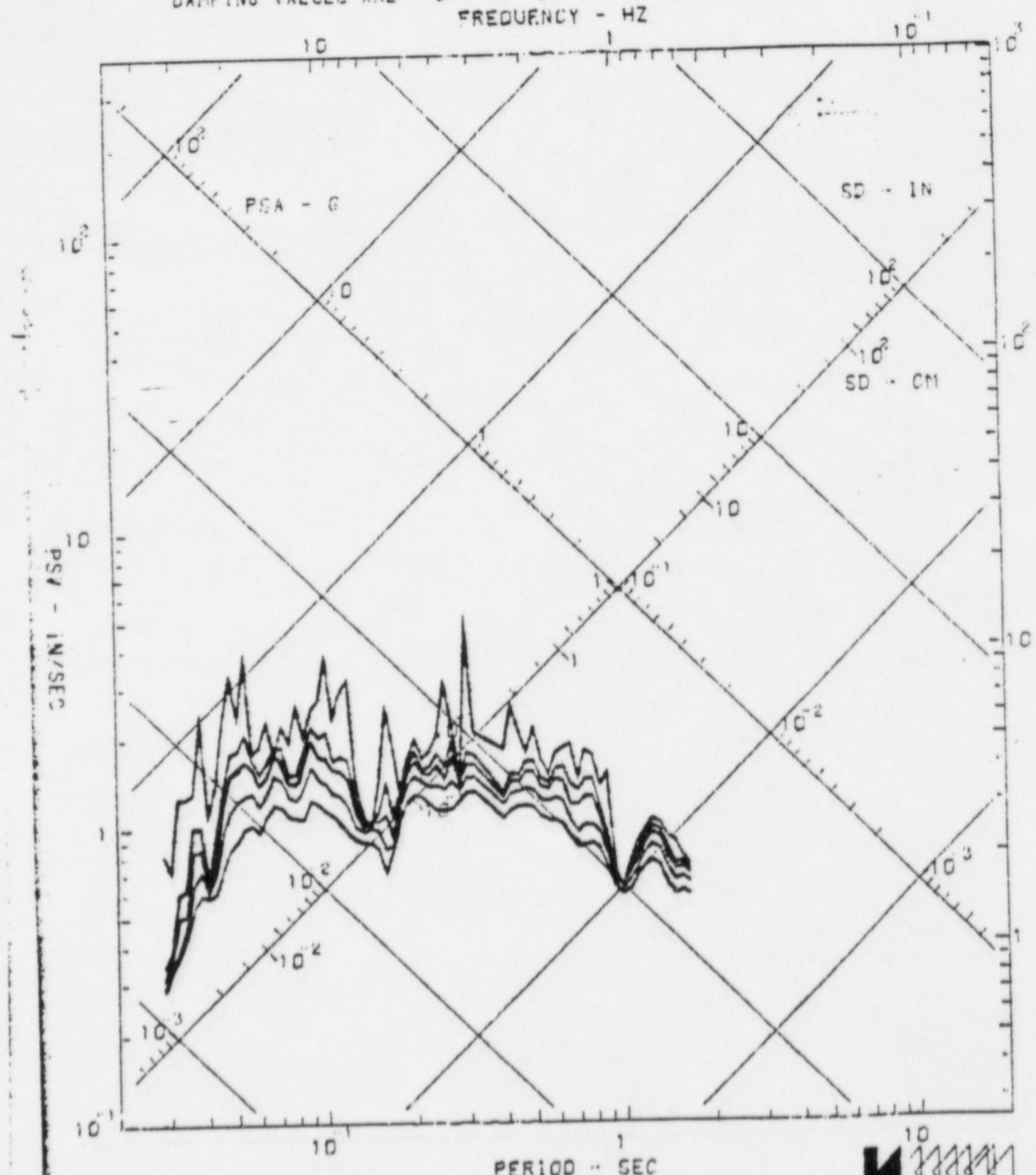
114800

PERRY NUCLEAR POWER PLANT

COMP WEST

SMABSN 165-1T

DAMPING VALUES ARE 0., 1., 2., 4., 7 PERCENT OF CRITICAL  
FREQUENCY - HZ



10<sup>-1</sup> 10<sup>0</sup> 10<sup>1</sup>

PERIOD = SEC



ML 5.0 EARTHQUAKE JANUARY 31, 1986

VERT. 575'

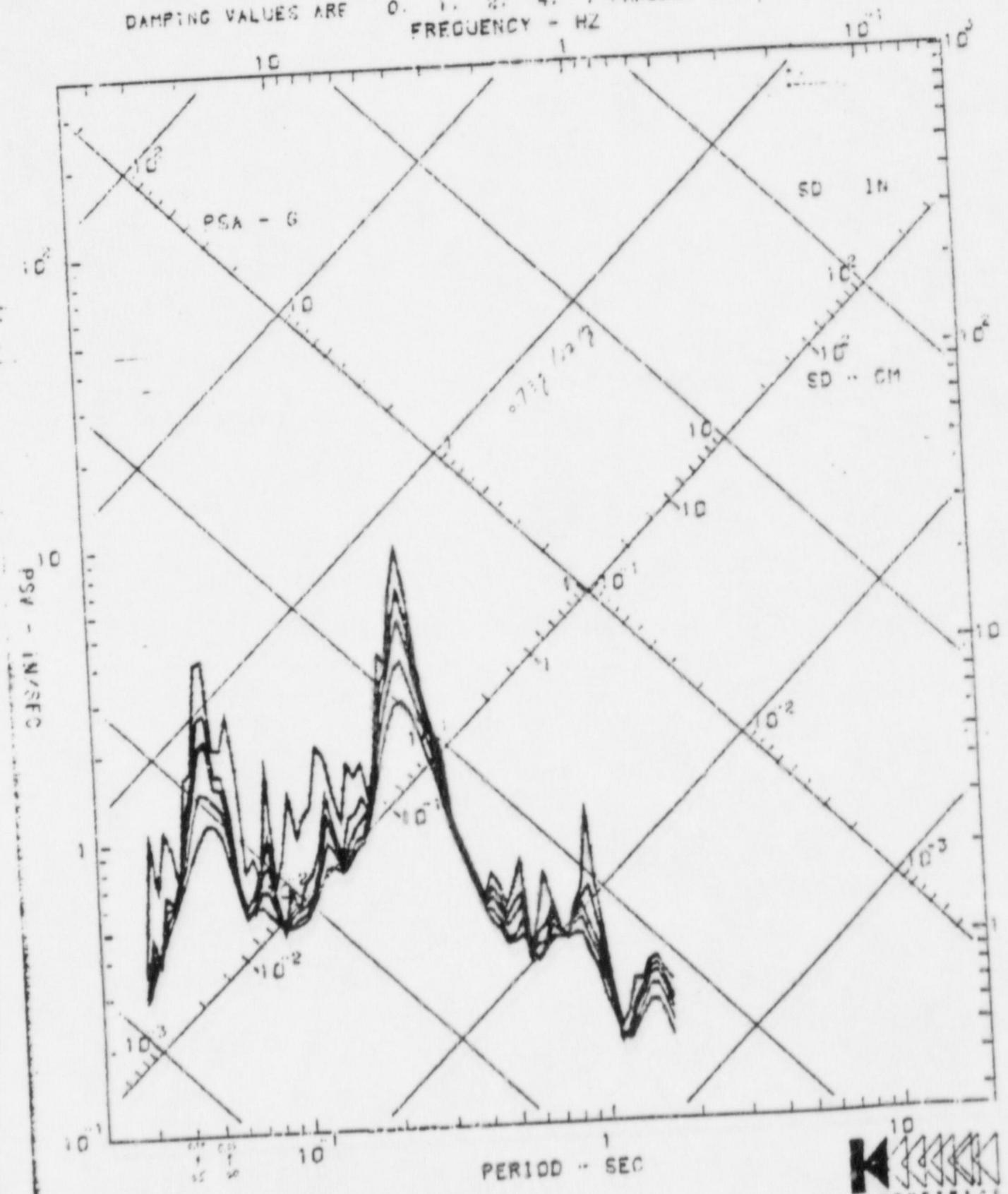
PERRY NUCLEAR POWER PLANT

COMP UP

SMASS/N 165-IV

11A8001

DAMPING VALUES ARE 0, 1, 2, 4, 7 PERCENT OF CRITICAL  
FREQUENCY - HZ



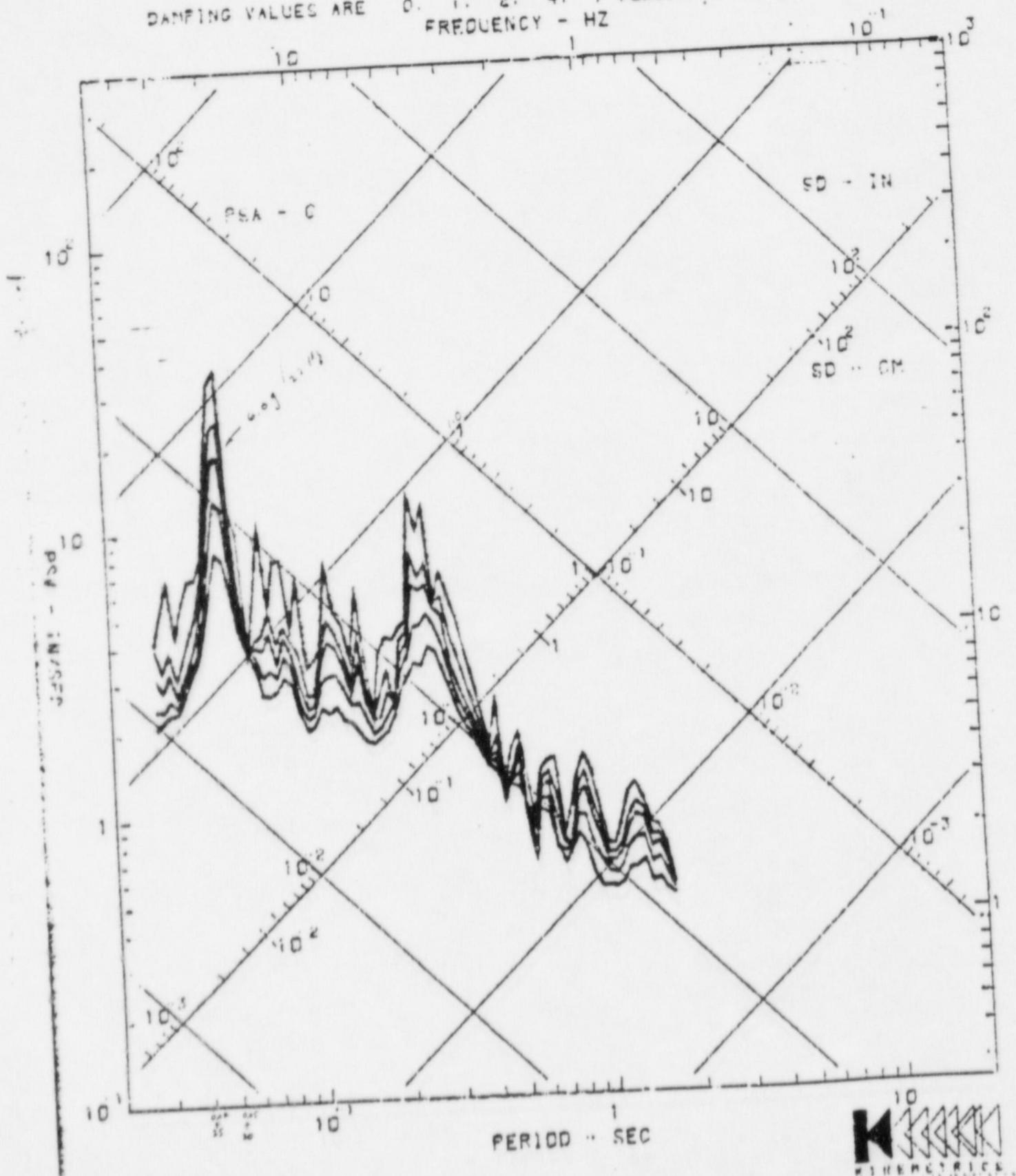
ML 5.0 EARTHQUAKE JANUARY 31, 1986  
NORTH-SOUTH 682'

PERRY NUCLEAR POWER PLANT

COMP SOUTH SMASS/N 105-24

11AR00Z

DAMPING VALUES ARE 0, 1, 2, 4, 7 PERCENT OF CRITICAL  
FREQUENCY - HZ



ML 5.0 EARTHQUAKE JANUARY 31, 1986

EAST-WEST 682'

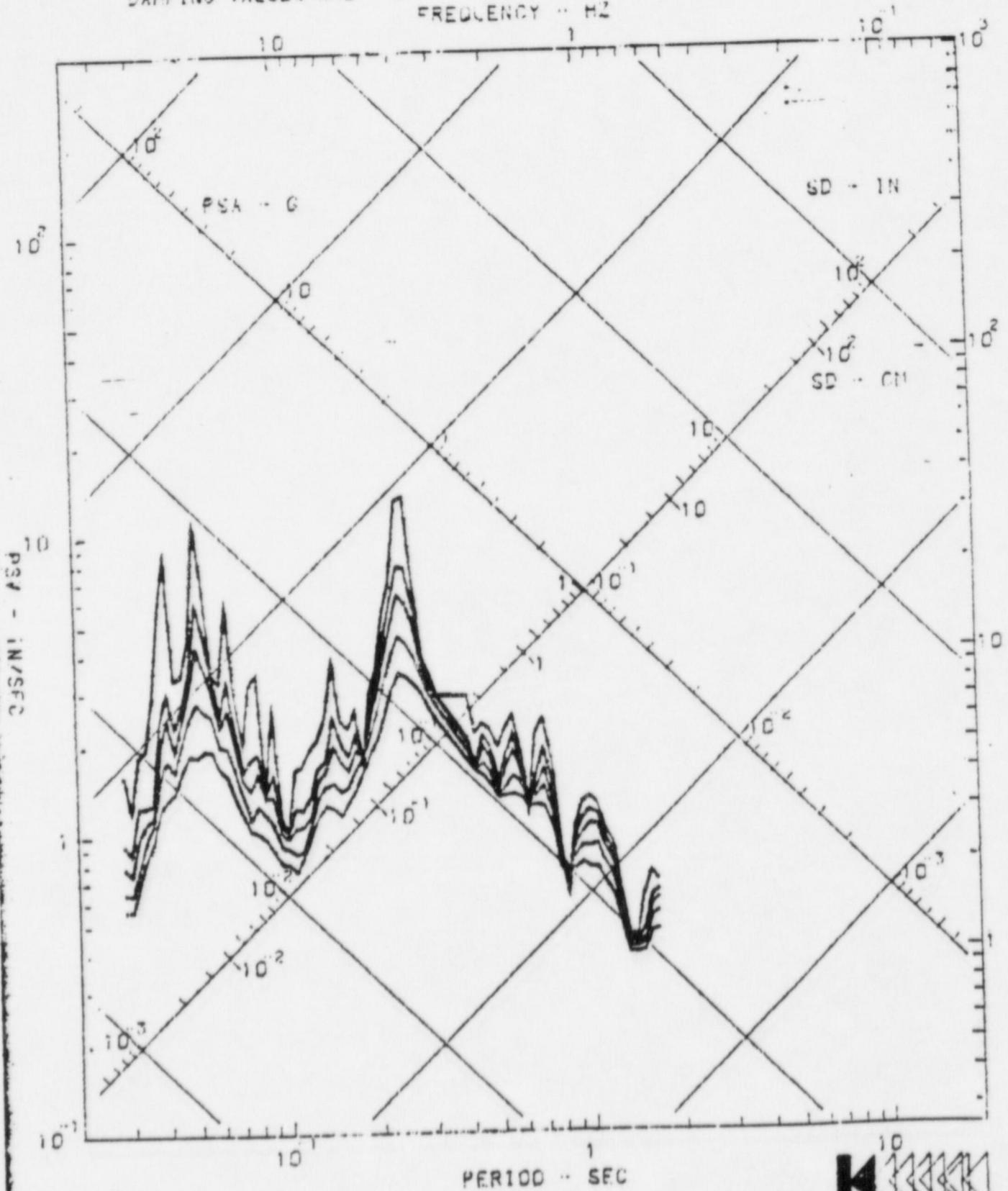
114800Z

PERRY NUCLEAR POWER PLANT

COMP WEST

SMA35/N 165-ET

DAMPING VALUES ARE 0, 1, 2, 4, 7 PERCENT OF CRITICAL  
FREQUENCY = HZ



ML 5.0 EARTHQUAKE JANUARY 31, 1985

VERT. 682'

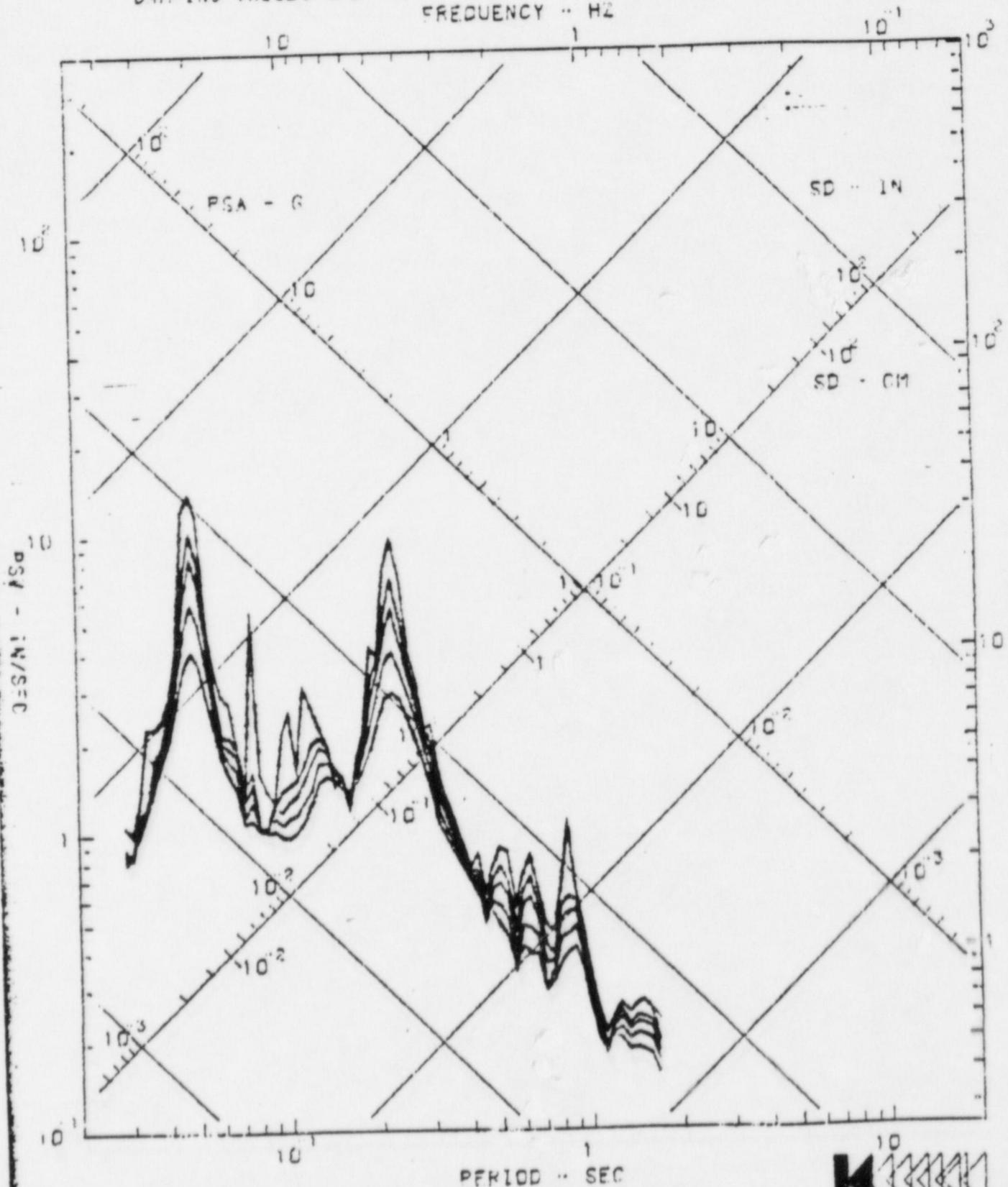
11A800K

PERRY NUCLEAR POWER PLANT

COMP UP

SHACKIN 165-2V

DAMPING VALUES ARE 0. 1. 2. 4. 7 PERCENT OF CRITICAL  
FREQUENCY = HZ



2/2/86 Walk-down

grade level: 620'

T. Y. Chang

C Air compressor for instrumentation tripped.

Make: Worthington Centrifugal Compressor

Type: CAP-15

Serial no. T96714

Location Control Complex

Elevation: 574'

There are 1 instrumentation compressor & 1 air compressor for each unit. All 4 are connected to a common header. Any one will provide enough compressed air for both units.

Unit 1 has set pt 16 mil & 2 vibrat. monitors (set pt 18 mil) are to measure shaft deflection, but both were not triggered by the earthquake. The applicant believed that however the earthquake caused the trip.

\*Bentley Nevada Corp  
Model 5075-14

C Main generator breaker tripped because of trip of no. 60 relay (Turbine generator protection)

No. 60 relay ← <sup>Both on "generator"</sup> relay panel → 40-1 relay (relay

by GE Hitachi \* type (toggle type) No. 60 Model 115000-1  
located: Control room No. 40-1 room

Elevation: 654' Impedance type over current voltage relays  
Safety Related: no location: Control room

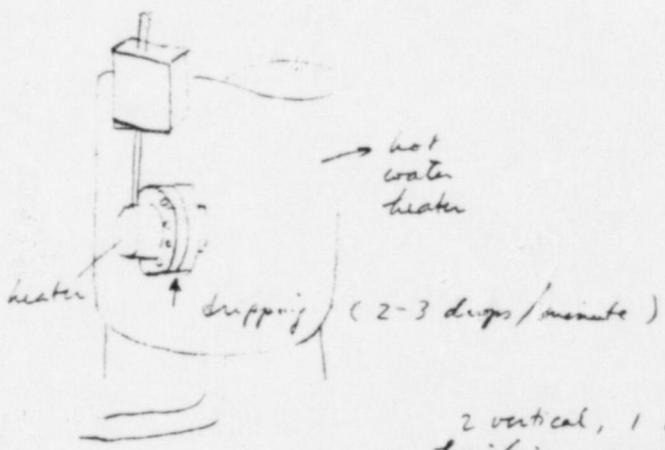
Elevation: 654', Safety Related no

No. 60 relay (lockout relay) tripped because of trip of no. 40-1 relay. At the time of earthquake, the turbine generator was not operating. There was no voltage on 40-1 since turbine was not working, and the disk was flopping there when earthquake came and caused the trip. Applicant said that had the generator been working, the relay probably would not have tripped. The trip is anticipated in view of the fact that the generator was not working.

- (3) Auxiliary Boiler tripped -  
 make: Burn Corp. shut off valve (Maxon) shut.  
 location: aux boiler room  
 Elevation: 620'  
 This aux boiler tripped because of trip of No. 86 relay. (Tripped during transfer from aux. transformer to main transformer - by design)

- (4) Hot water heater pipe flange leaked.

location: Rad Waste Bldg  
 Elev. 623' <sup>see attached floor plan</sup>

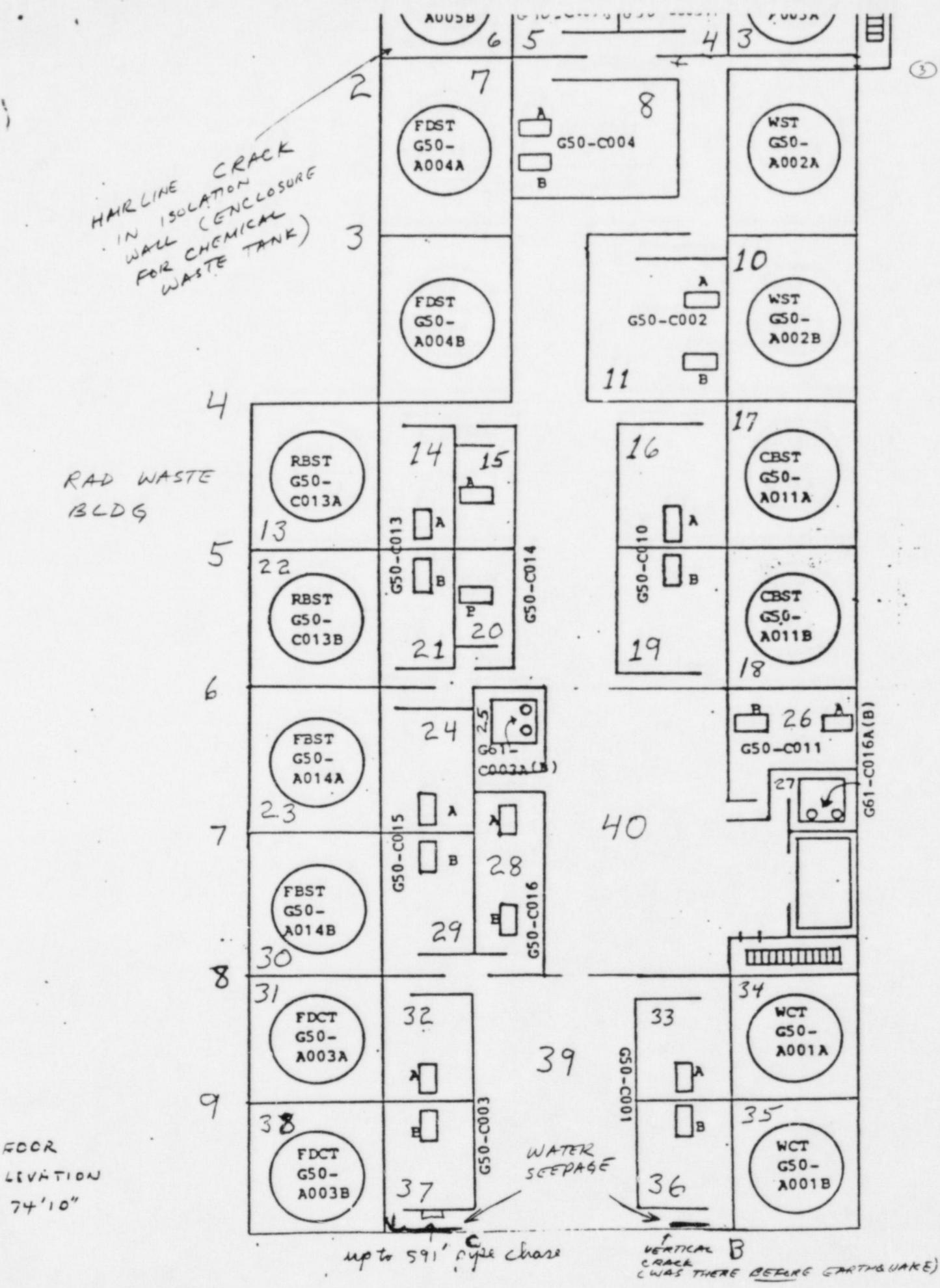


This heater provides clean steam to evaporator, etc.  
 nothing to do with radiation waste  
 knew definitely we didn't

- Wall crack for enclosure of chemical waste tank (2' reinforced concrete wall) <sup>Don't know whether to repair or not</sup>  
 wall crack in aux. bldg.
- Seepage through Rad Waste room wall. <sup>from ground water</sup> (ground

- (5) Suppression pool level indicator

right after earthquake, water level rose 1" → 1½", measured at 4 places <sup>A-111 valve leakage</sup> Water level rose 1" → 1½" on ~~Saturday night~~ still looking into this (recalibration?)



RAD WASTE  
BLDG

GSI-AUUS GSI-AUUA



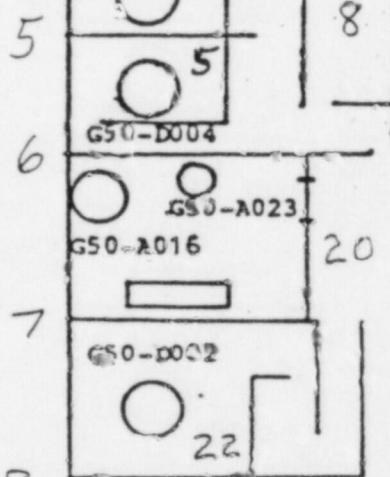
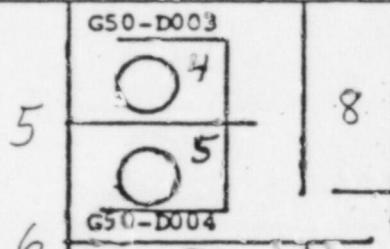
Transfer Cart Area

Solidified Drum Storage

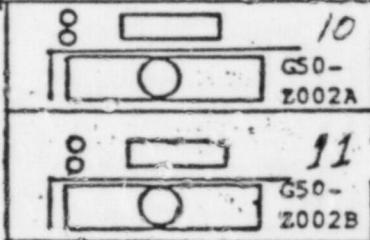
compactor

Low Level Radwaste Storage

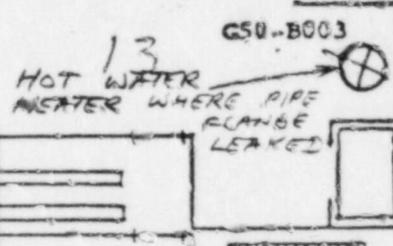
4



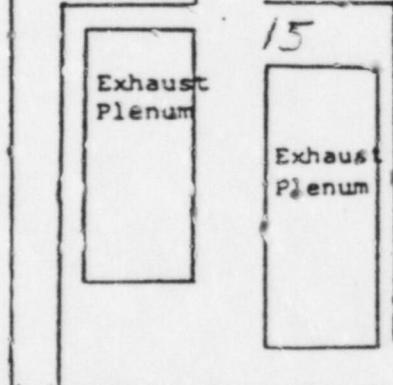
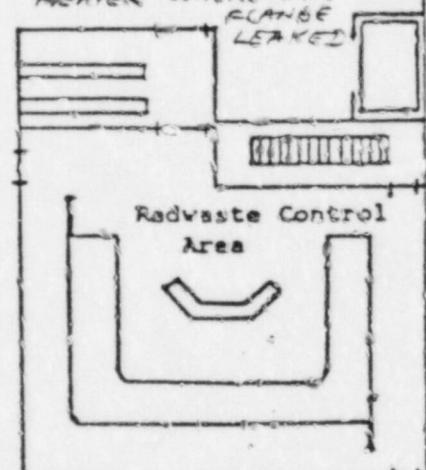
12



3



20



15

Supply Plenum P34-Z001

16

C

B

FLOOR  
ELEVATION  
622' 6"



*John Stefano*

UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20585

FEB 25 1986

MEMORANDUM FOR: Robert J. Bosnak, Chief  
Engineering Issues Branch  
DSRO, NRR

Frank J. Congel, Chief  
Reliability and Risk Assessment Branch  
DSRO, NRR

FROM: T. Y. Chang, Task Manager  
Leon Reiter, Sr. Reliability and Risk Analyst  
DSRO, NRR

SUBJECT: REPORT OF QUICK RESPONSE TRIP TO OBSERVE EFFECTS OF THE  
NORTHERN OHIO EARTHQUAKE ON THE PERRY NUCLEAR POWER PLANT

Background

An earthquake occurred at 11:48 a.m. on January 31, 1986 near the Perry Nuclear Power Plant in Northern Ohio. Preliminary information from USGS indicated that the earthquake had a body-wave magnitude ( $m_b$ ) of 5.0, and the epicenter is located approximately 12 miles south of the Perry site.

The Perry Plant is a General Electric BWR-6 with a Mark III containment. It is not yet licensed. Nuclear fuel is on site but has not been loaded into the reactor core. The owner of the plant is Cleveland Electric and Illuminating Company (CEI). The utility was performing pre-operational tests and according to CEI, most of the safety related systems were running when the earthquake occurred. Although Perry is not an operating plant and is not required to do so, CEI immediately activated the emergency plan in order to assess facility damage and personnel injuries. No injuries occurred. In addition, NRC and other relevant federal and local agencies were notified of this event. The plant was switched to the recovery mode in the afternoon of January 31, 1986. The recovery organization is shown in enclosure 1. A detailed walkdown inspection involving about 40, and at times 65, people was conducted for the whole plant, which covered buildings, equipment, instrumentation, piping systems, etc. Only minor damage was found (see preliminary findings below). The inspection was completed at 2:00 a.m. on February 1, 1986.

An Augmented Inspection Team (AIT) from NRC Region III and staff from NRR were sent to the Perry site on the morning of February 1. The team from NRR consisted of John Stefano (Perry Project Manager), Leon Reiter and T. Y. Chang (both from DSRO). They left Perry on the evening of February 2. The Region III group was led by Carl Paperiello (Director of the Region III Reactor Safety Division). The NRC team held several meetings with the CEI engineering and licensing staff, the Architect/Engineer (Gilbert Associates), CEI consultants (Weston Geophysical) and suppliers of the seismic monitoring instrumentation (Kinematics, and Engdahl Enterprises). A list of meeting

-00303441  
11/2/86 2/1/86

A/62

attendees is attached as enclosure 2. The NRC team members reviewed preliminary seismic recordings and conducted a walk-through inspection of buildings and equipment.

#### PRELIMINARY FINDINGS

##### 1. Seismic Records:

The plant had nine sets of seismic monitoring instrumentation on the site when the earthquake occurred. All but one were operating and recorded the earthquake. They are of three different types: triaxial time-history accelerographs (made by Kinemetrics), triaxial peak response spectra recorders, and triaxial peak accelerographs (both made by Engdahl Enterprises). A list of these instruments and their locations is attached as enclosure 3.

There were some difficulties in interpreting data obtained from the Engdahl peak response recorder. Each of these instruments has 12 tuned reeds, each tipped with a diamond stylus which makes scratches on a recording plate. Some of these instruments are wired to annunciators in the control room. Each annunciator has one set of 12 amber lights and one set of 12 red lights, with each set of lights marked with the corresponding 12 tuned reed frequencies. These amber lights and red lights are pre-set to be activated at FSAR values of 2/3 OBE spectral accelerations and full OBE spectral accelerations respectively for the corresponding tuned reeds. The recording plates have been in these instruments for about a year, and spurious annunications have occurred previously when there were no earthquakes. Paul Engdahl, President of Engdahl Enterprises, was present at Perry during the visit and helped interpret the data obtained from the scratched plates. Enclosure 4 shows the preliminary data from the Engdahl instruments in the reactor building and the auxiliary building as plotted on the FSAR spectra. The 2% damping spectra curves should be used for comparison since the reeds have a built-in 2% damping.

There were some concerns about the way the Kinemetrics instruments were installed at the reactor base mat level. The instruments are not located on the mat, rather they are positioned on brackets bolted on the containment wall 9" above the mat. A "ring" test done by Kinemetrics proved that the brackets are rigid enough to render the data valid.

Partial preliminary time history data obtained from the Kinemetrics instruments located at the reactor building foundation (575') and on the containment vessel annulus (682') and the associated response spectra generated by Kinemetrics are shown in enclosure 5. Note that the grade level of the plant is at 620'.

Enclosures 4 and 5 indicate that there is a strong possibility that both OBE and SSE design response spectra may have been exceeded in the frequency range of approximately 16 Hz and above. The design basis for SSE is a Regulatory Guide 1.60 design response spectra anchored at 0.15g, with the OBE spectra

anchored at 0.075g. Preliminary data indicated a Zero Period Acceleration (ZPA) value of 0.18g at the reactor base mat. These recorded data are being further studied by the NRC and CEI consultants and instrument suppliers.

## 2. Results of Preliminary Plant Inspection

Damage to the Perry Plant was assessed by CEI and found to be limited to hair line cracks in rad waste and auxiliary building walls and a pipe flange leak in a hot water heater in the rad waste building. In most cases CEI was not able to determine whether or not these cracks were there before the earthquake. The hot water heater supplies clean non-radioactive steam to an evaporator, and the leakage rate was estimated to be about 20 drops per minute. In addition, a rotating disc type protective relay for the turbine generators tripped, which in turn caused an auxiliary boiler to trip. Since the turbine generators were not in operation at the time of the earthquake, there was no voltage across the relay and, therefore, the rotating disc was hanging loose there. It tripped due to the earthquake motion which would be expected. An instrument air compressor tripped; however, one of the three other instrument/service air compressors in the plant automatically started. There was also an indication that suppression pool water level indicators might have malfunctioned during and after the earthquake. CEI is still looking into this matter. Seepage of ground water through the junction of wall and floor and through cracks in the wall was also observed in the rad waste building after the earthquake. The seepage was not considered severe.

The NRC staff participated in a walk-down of the plant to inspect for damage and anomalies. The NRC staff walk-down observations are recorded in enclosure 6.

## CONCLUSIONS

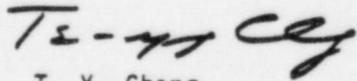
1. No damage of any significance was observed at the Perry plant by the NRC staff during the trip.
2. Based on the preliminary records of seismic monitoring instruments at the plant, the staff concluded that there is a strong possibility that the OBE and SSE design response spectra (FSAR values) may have been exceeded in the frequency range above approximately 16 Hz. It has been pointed out that the high frequency range of Regulatory Guide 1.60 spectra is not as conservative as the lower frequency range. However, the records obtained at Perry are still puzzling since the seismic instrumentation on the containment wall at 682 (about 107' above base mat) still shows exceedance of FSAR floor spectra in the frequency range higher than approximately 16 Hz. One would normally expect that the responses in the frequency ranges higher than the building fundamental frequency would be filtered out by the building.

Further analyses and study of the seismic data by CEI staff engineers and consultants may yield new information on this matter. It should be kept in mind that response spectra do not present all the information

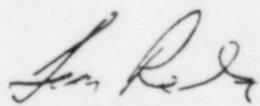
about an earthquake. The energy content as a function of frequency is better represented by the Power Spectral Density (PSD), which is an important indicator of damage potential. Another damage potential indicator is the duration of the earthquake. On both accounts, the effects of the earthquake on the Perry plant were observed to be minimal. Normally responses in the high frequency range do not have much energy content. Furthermore, the peak time history reading at the base mat lasted for only about one half second.

NRC AND SQUG FOLLOW-UP ACTIONS

1. The location, aftershocks and travel mechanism of the earthquake sequence will have to be examined and compared with previous seismicity so as to determine if there is any impact upon the adequacy of assumptions made in the Safety Evaluation Report.
2. DSRO/NRR had a meeting with representatives of the Division of BWR Licensing on 2/3/86 to brief them of the findings at Perry. It was decided that since the investigation of the effects of this earthquake on Perry is plant-specific, the BWR Licensing Division should take the lead. DSRO will perform an oversight function and provide technical assistance if needed. R. Hermann and L. Reiter were appointed as team leaders in the structural/mechanical and geoscience areas respectively. A permanent review team is being formed to review the effects of this earthquake on the structural, equipment and geoscience aspects of the Perry plant.
3. A BWR site investigation team was sent to Perry on 2/6/86. This team consists of A. Lee (Engineering Branch/BWR Licensing Division/NRR) and J. Singh (INEL contractor), and will perform an independent review of safety related equipment.
4. Seismic Qualification Utility Group (SQUG) will send a team to Perry on 2/10/86 to collect seismic experience data. This information could be useful for the on-going Unresolved Safety Issue (USI) A-46, "Seismic Qualification of Equipment in Operating Plants."
5. As the analysis and review of the earthquake, and recorded data proceed, additional recommendations to specific generic issues may be forthcoming. among these presently being considered include increased use of parameters other than peak accelerations and response spectra to better reflect the damage potential of earthquake ground motion and a clearer definition of OBE and/or SSE exceedance and their implications.



T. Y. Chang  
Task Manager



Leon Reiter  
Sr. Reliability and Risk  
Analyst

cc: See Page 5.

cc:	H. Denton	S. Brocoulm
	D. Eisenhut	L. Heller
	R. Bernero	N. Chokshi
	W. Butler	L. Shao, RES
	G. Lainas	G. Bagchi
	J. Stefano	G. Giese Koch
	S. Stern	P. T. Kuo
	T. Speis	R. Rothman
	B. Sheron	A. Lee
	N. Anderson	P. Sobel
	Lic. Div. Directors	R. Hermann
	Lic. Div. A/Ds	C. P. Tan
	G. Arlotto, RES	
	J. Richardson, RES	
	C. Paperiello, Reg. III	

## RECOVERY ORGANIZATION

RECOVERY  
MANAGER

M. R. EDELMAN

M. D. LYSER  
A. KAPLAN

EMERGENCY PLAN	OPERATIONS	MAINTENANCE AND WORK ORDERS	ENGINEERING	LICENSING	PUBLIC RELATIONS AND MEDIA
S. F. KENSICKI	R. A. STRATMAN	D. J. TAKACS	F. R. STEAD	E. M. BUZZELLI	W. E. COLEMAN
M. W. GMYREK		M. COHEN G. R. LEIDICH	L. D. BECK		R. L. FARRELL

## ENCLOSURE 2

MEETING ATTENDANCEFebruary 1, 1986 - TEC

<u>NAME</u>	<u>COMPANY</u>	<u>POSITION</u>
N. J. Lehman	CEI	Staff Analyst
J. J. Waldron	CEI	Manager, Technical Dept.
K. A. Connaughton	NRC	Resident Inspector
J. W. Muffett	NRC, Region III	Plant System Section Section Chief
J. J. Harrison	NRC, Region III	Chief, Eng. Branch, DRS
C. J. Paperiello (Team leader)	NRC, Region III	Director, Div. Reactor Safet
C. R. Angstadt	CEI	Lead Structural Engineer
E. M. Buzzelli	CEI	Sr. Licensing Engineer
K. R. Pech	CEI	Gen. Sup. Eng., Nucl Constr.
M. N. Gmyrek	CEI	Sr. Operations Coordinator
R. A. Stratman	CEI	Gen. Supervisor, Operations
H. L. Williams	CEI	Executive Vice President
A. Kaplan	CEI	V.P. Nuclear Operations Div.
M. D. Lyster	CEI	Manager, PPOD
F. R. Stead	CEI	Manager, NED
B. A. Stiles	CEI	Community Relations Asst.
John J. Stefano	NRC/NRR	Perry Project Manager
Leon Reiter	NRC/NRR	Sr. Reliability & Pipe Analyst
T. Y. Chang	NRC/NRR	Task Manager
W. E. Coleman	CEI	GSE, Community Relations
G. R. Leidich	CEI	GSE, Outage Management
D. J. Takacs	CEI	Gen. Sup., Maintenance
J. A. Grobe	NRC	Sr. Resident Inspector
M. J. Hayner	CEI	Licensing Engineer

Attendance - February 1, 1986 - TEC

NAME	COMPANY	POSITION
M. H. Minns	CEI	Licensing Engineer
R. G. Schuerger	CEI	Chairman, NSRC
E. N. Levine	Weston Geophysical	Seismologist, Consultant to CEI
Gabriel Leblanc	Weston Geophysical	Seismologist, Consultant to CEI
Steve Kensicki	CEI	Technical Superintendent
Bill Kanda	CEI	GSE, Technical
Dan Hulbert	CEI	Emergency Planning Sup.
George Siegel	Kinnemetrics	Field Operations Sup.
Vince Concel	CEI	PPTD System Engr. Lead
Paul Engdahl	Engdahl Enterprises	President
Roger Alley	Gilbert, Inc.	Project Structural Eng.
Frank Kocsis	CEI	Independent Safety Eng.
Cyril Shuster	CEI	Manager, QA
Ronald L. Farrell	CEI	Manager, PPSD
Murray R. Edelman	CEI	V.P., Nuclear Group

**FINAL DRAFT**TABLE 3.3.7.2-1SEISMIC MONITORING INSTRUMENTATION

<u>INSTRUMENTS AND SENSOR LOCATIONS</u>	<u>MEASUREMENT RANGE</u>	<u>MINIMUM INSTRUMENTS OPERABLE</u>
<b>Triaxial Time-History Accelerographs</b>		
(a) ✓ D51-N101 Reactor Building Foundation	0.01 - 1.0g	1
(b) ✓ D51-N111 Containment Vessel	0.01 - 1.0g	1(b)
c. D51-N100 Reactor Building Foundation	0.005 - 0.02g	1
d. D51-N110 Reactor Building Foundation	0.005 - 0.02g	1(b)
<b>Triaxial Peak Accelerographs</b>		
(a) ✓ D51-R120 Reactor Recirculation Pump	0.05 - 1.0g	1
(b) ✓ D51-R130 HPCS Piping in Reactor Building	0.05 - 1.0g	1
(c) ✓ D51-R140 HPCS Pump Base Mat	0.05 - 1.0g	1
<b>Triaxial Seismic Switches</b>		
a. ✓ D51-N150 Reactor Building Foundation	0.025 - 0.25g	1(a)
<b>Triaxial Response-Spectrum Recorders</b>		
(a) ✓ D51-R160 Reactor Building Foundation	2 - 25.4 Hz	1(a)
(b) ✓ D51-R170 Reactor Recirculation Piping Support	2 - 25.4 Hz	1
c. ✓ D51-R180 HPCS Pump Base Mat	2 - 25.4 Hz	1
d. ✓ D51-R190 RCIC Pump Base Mat	2 - 25.4 Hz	1

(a) With control room annunciation.

(b) Seismic trigger with control room annunciation.

2 CYCLES X 10 DIVISIONS PER INCH

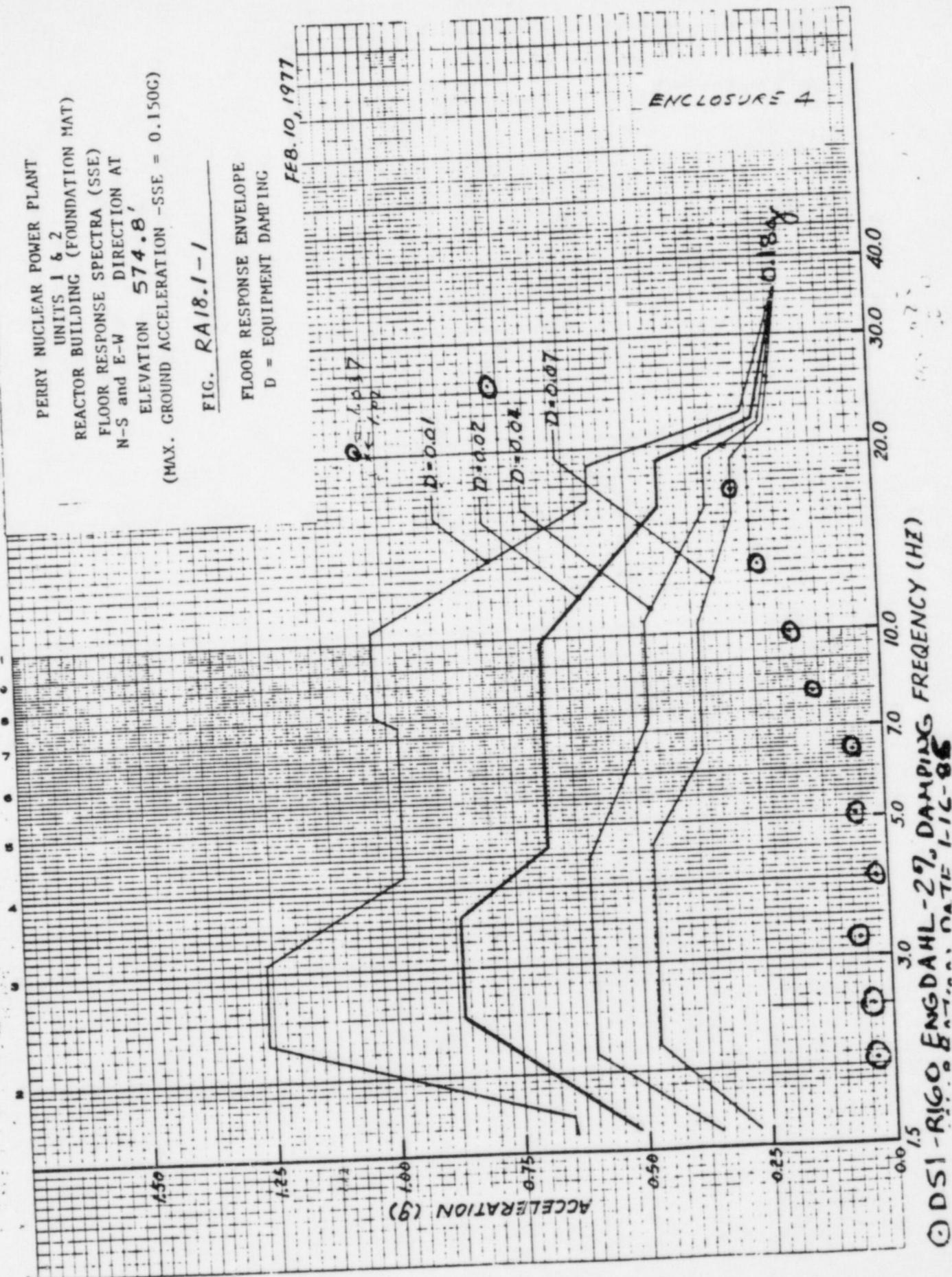
PERRY NUCLEAR POWER PLANT  
UNITS 1 & 2  
REACTOR BUILDING (FOUNDATION MAT)  
FLOOR RESPONSE SPECTRA (SSE)  
N-S and E-W DIRECTION AT  
ELEVATION 574.8'  
(MAX. GROUND ACCELERATION -SSE = 0.150G)

FIG. RA18.1-1

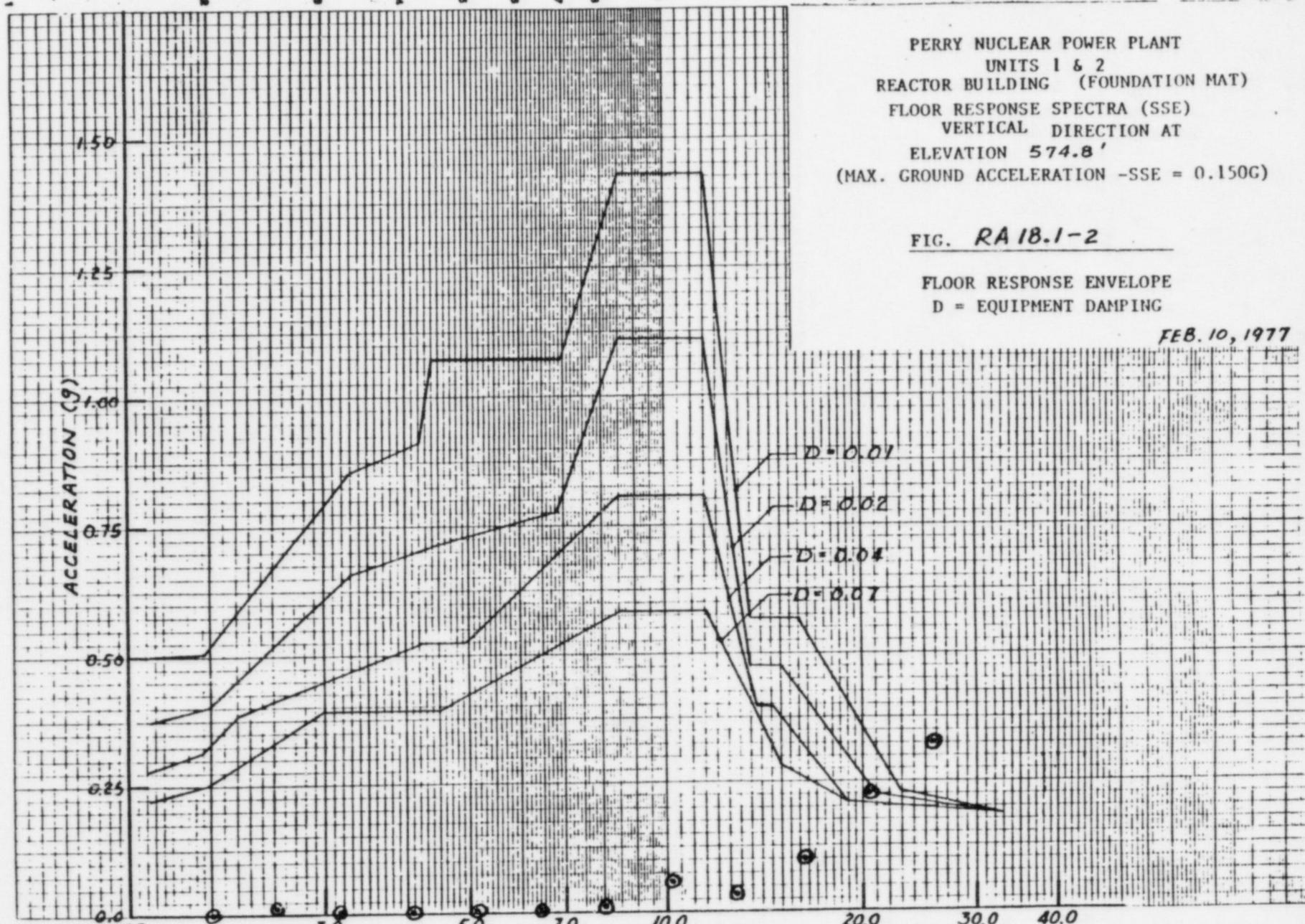
FLOOR RESPONSE ENVELOPE  
D = EQUIPMENT DAMPING

FEB. 10, 1977

ENCLOSURE 4



2 CYCLES X 10 DIVISIONS PER INCH



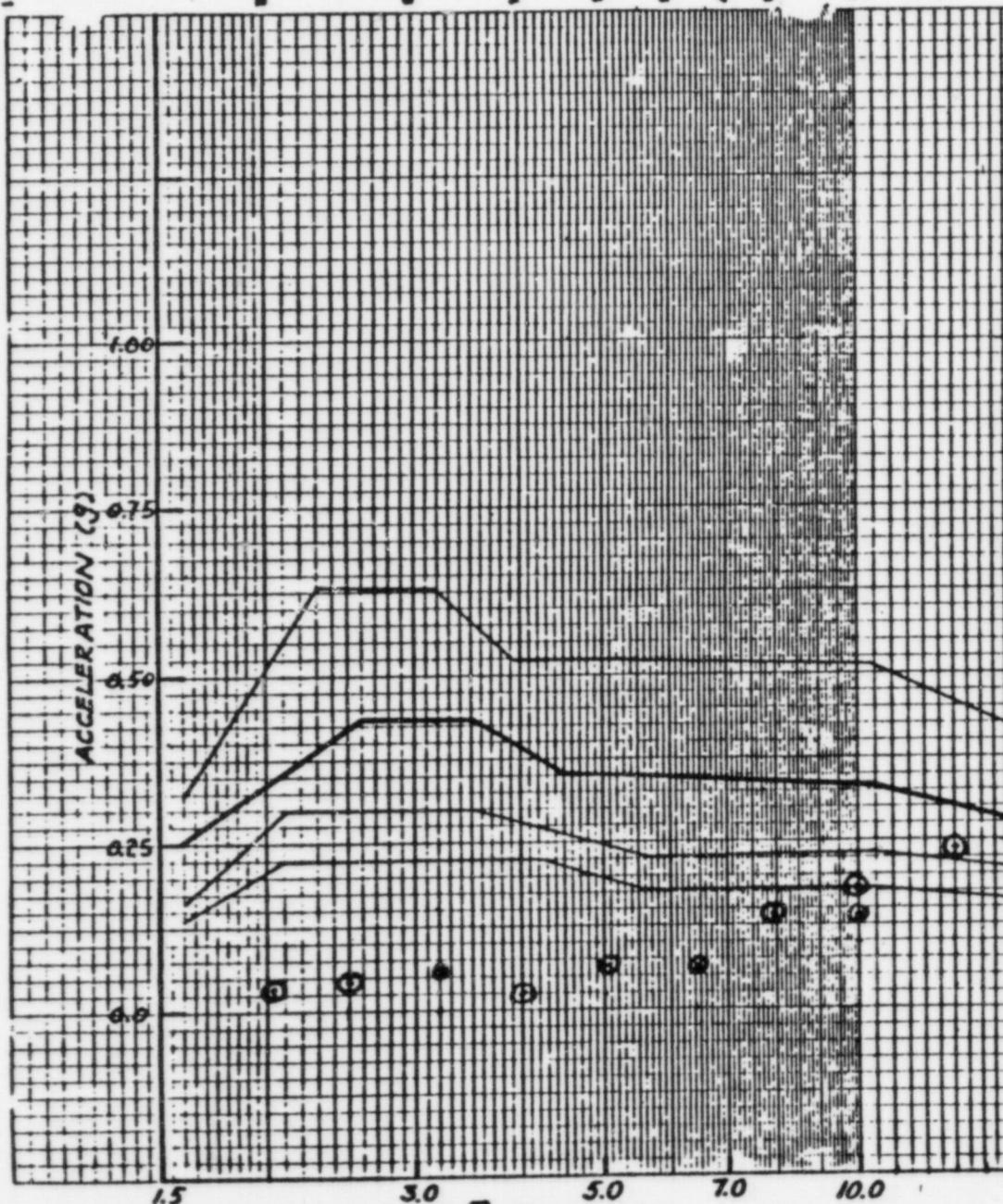
PERRY NUCLEAR POWER PLANT  
UNITS 1 & 2  
REACTOR BUILDING (FOUNDATION MAT)  
FLOOR RESPONSE SPECTRA (SSE)  
VERTICAL DIRECTION AT  
ELEVATION 574.8'  
(MAX. GROUND ACCELERATION -SSE = 0.150G)

FIG. RA 18.1-2

FLOOR RESPONSE ENVELOPE  
D = EQUIPMENT DAMPING

FEB. 10, 1977

DSI-R160 ENGOAHL - 2% DAMPING, FREQUENCY (HZ)  
CALIBRATION DATE 1-11-85

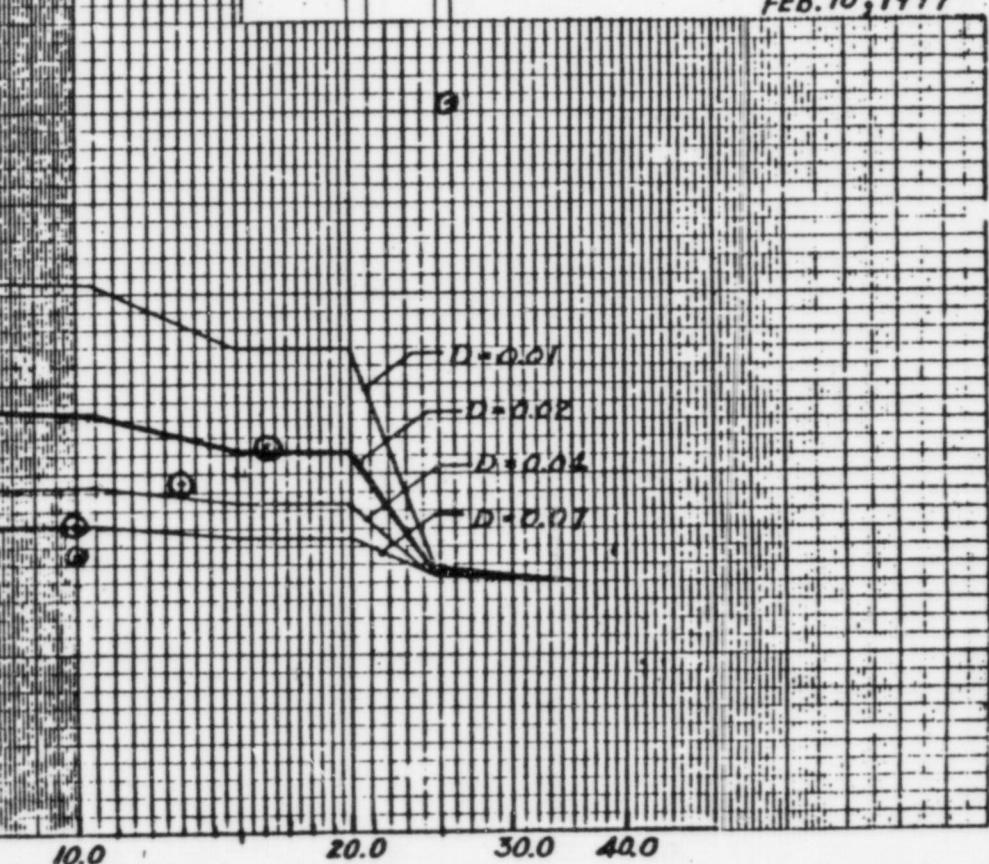


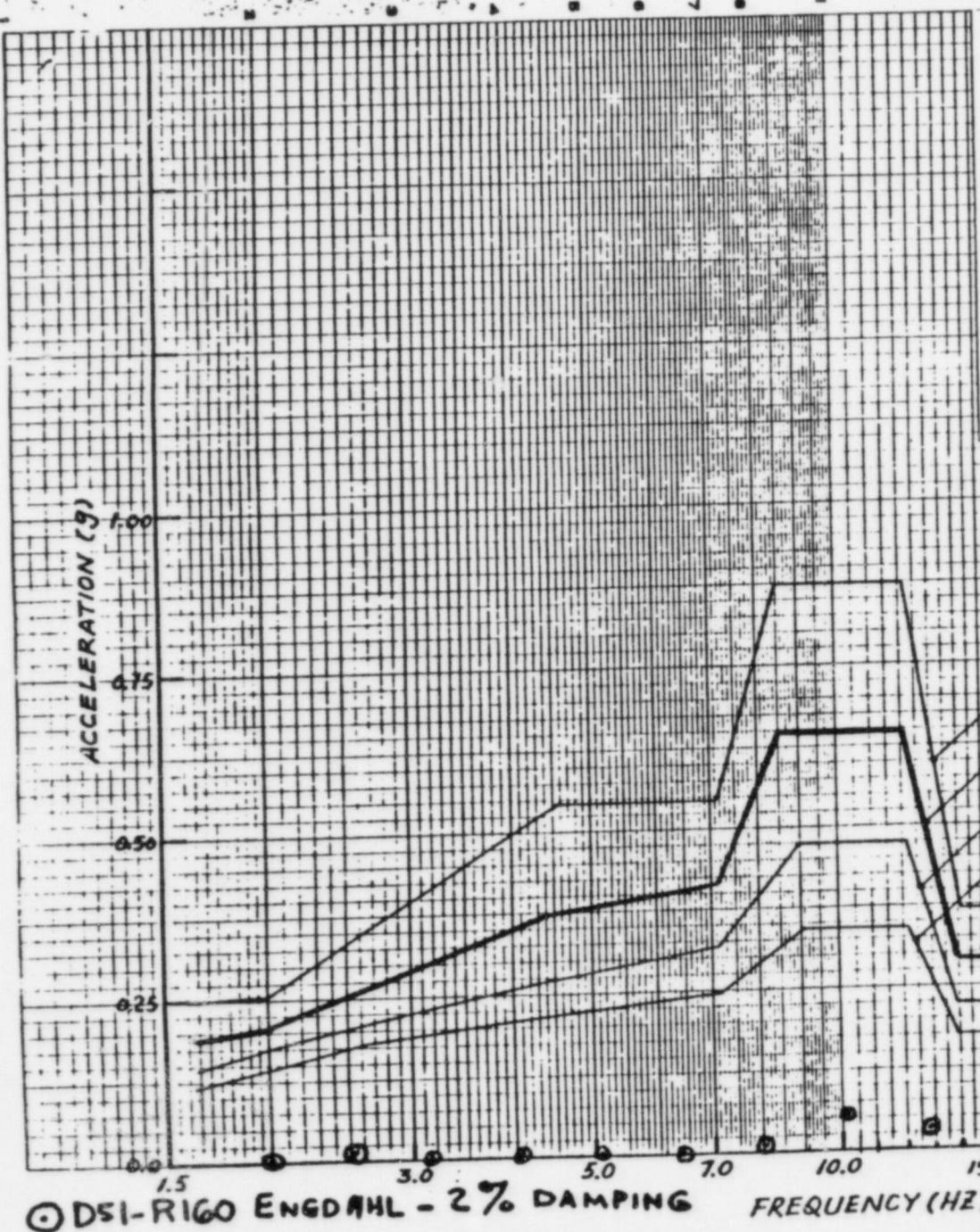
PERRY NUCLEAR POWER PLANT  
UNITS 1 & 2  
REACTOR BUILDING (FOUNDATION MAT)  
FLOOR RESPONSE SPECTRA (OBE)  
N-S and E-W DIRECTION AT  
ELEVATION 574.8'  
(MAX. GROUND ACCELERATION -OBE = 0.075G)

FIG. RA 10.1-3

FLOOR RESPONSE ENVELOPE  
D = EQUIPMENT DAMPING

FEB. 10, 1977





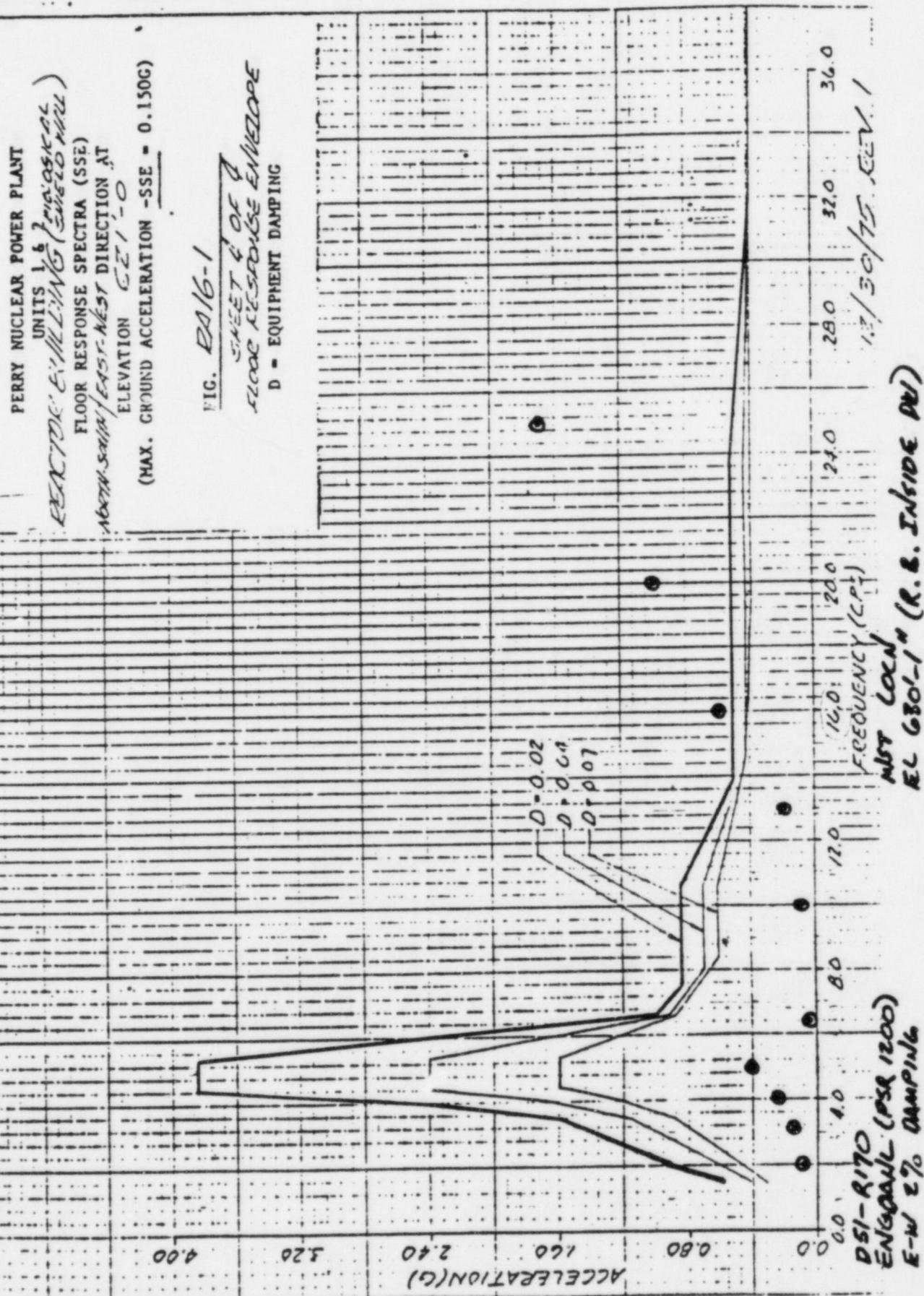
PERRY NUCLEAR POWER PLANT  
 UNITS 1 & 2  
 REACTOR BUILDING (FOUNDATION MAT)  
 FLOOR RESPONSE SPECTRA (OBE)  
 VERTICAL DIRECTION AT  
 ELEVATION 574.8'  
 (MAX. GROUND ACCELERATION -OBE = 0.075G)

FIG. RA18.1-4

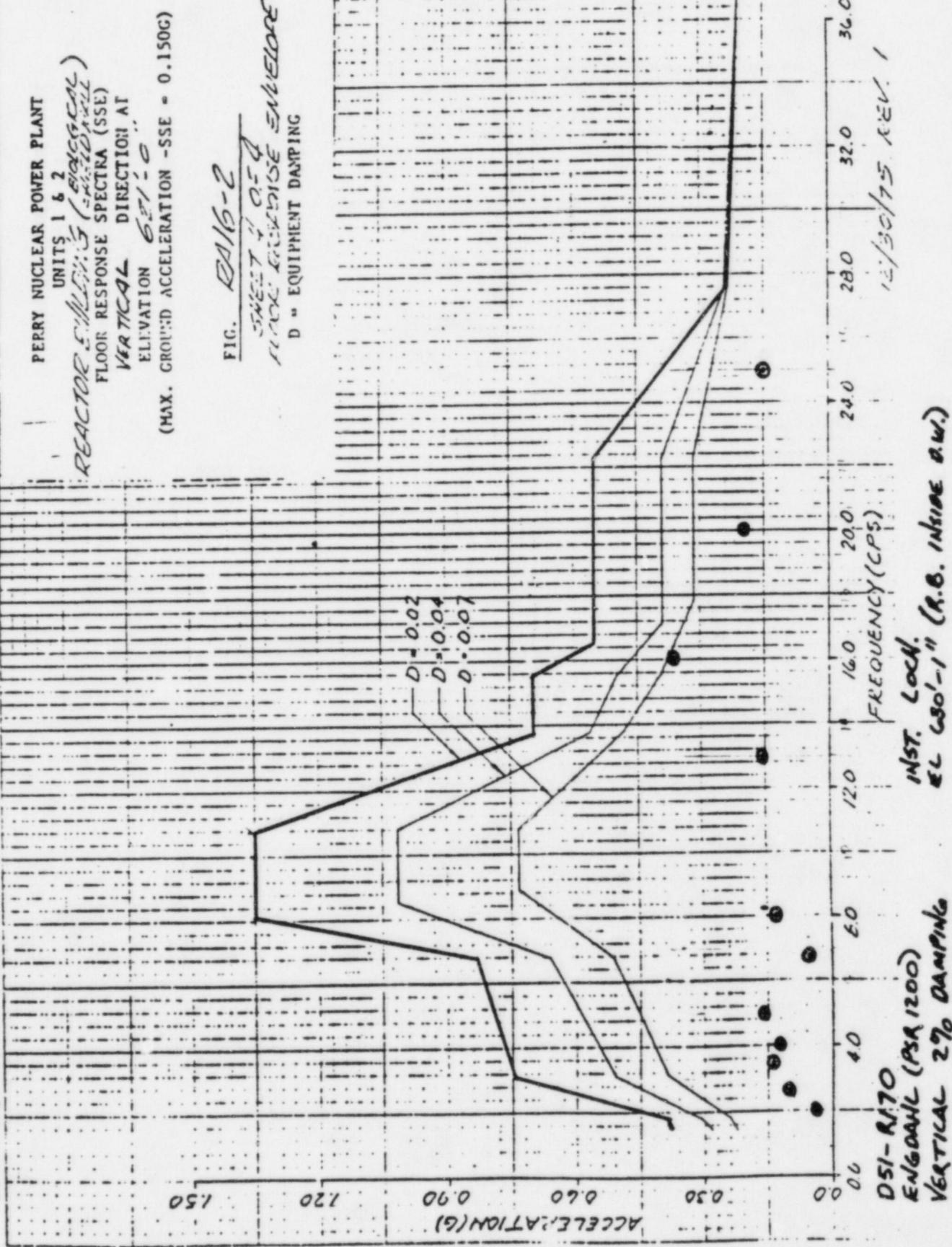
FLOOR RESPONSE ENVELOPE  
 D = EQUIPMENT DAMPING

FEB. 10, 1977

ACCELERATION RATE 1.80.8C



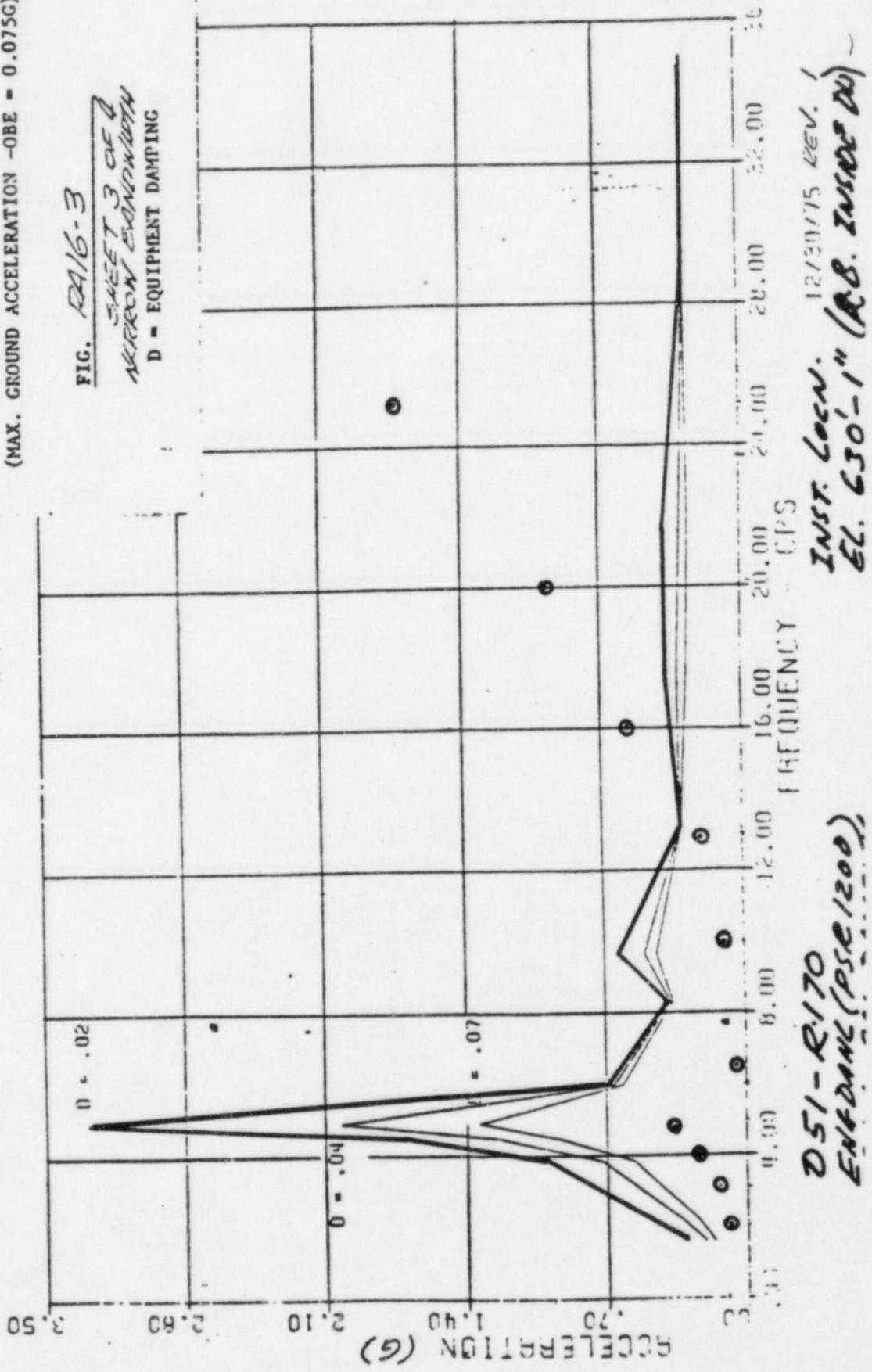
CALIBRATION DATE 1-30-86



ACCELERATION DATA

PERRY NUCLEAR POWER PLANT  
UNITS 1 & 2  
REACTOR BUILDING (ENCLOSURE)  
FLOOR RESPONSE SPECTRA (OBE)  
NORTH-SOUTH, EAST-WEST DIRECTION AT  
ELEVATION 27'-0"  
(MAX. GROUND ACCELERATION -OBE = 0.075G)

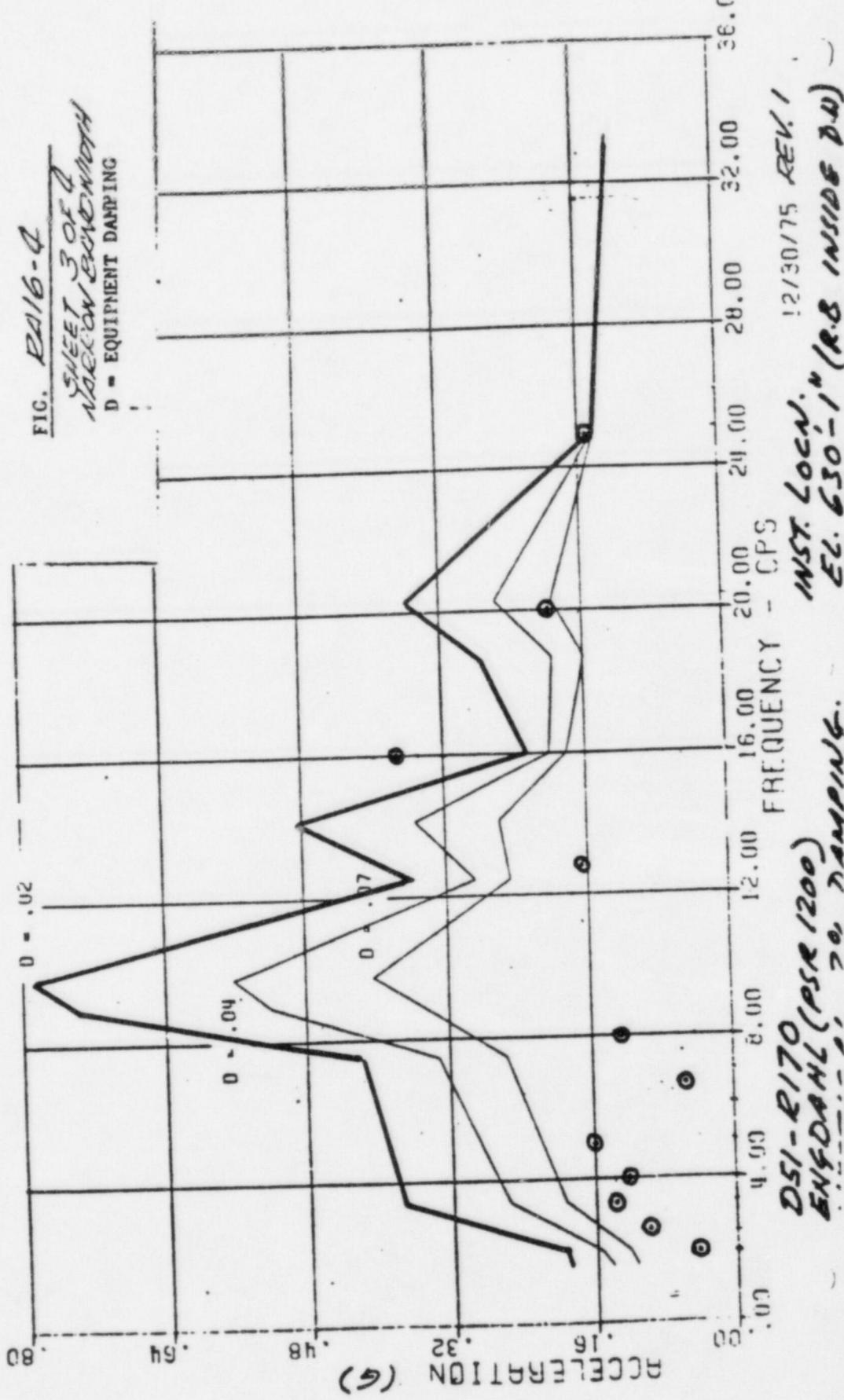
FIG. RA16-3  
WEEK 3 OF 7  
ACTION ENVELOPE  
D = EQUIPMENT DAMPING



CALCULATION 1.30 .SPC  
DATE

PERRY NUCLEAR POWER PLANT  
UNITS 1 & 2  
REACTOR BUILDING (FIELD LEVEL)  
FLOOR RESPONSE SPECTRA (OBE)  
VERTICAL DIRECTION AT  
ELEVATION 62'-0"  
(MAX. GROUND ACCELERATION -OBE = 0.075G)

FIG. E216-4  
SHEET 3 OF 7  
ECCENTRICITY  
D = EQUIPMENT DAMPING



D51-R170  
ENR'DAHL (PSSR 1200)  
MST. LOCN: E30-1" (R.B. INSTRUMENTS)  
E2. E30-1" (R.B. INSTRUMENTS)

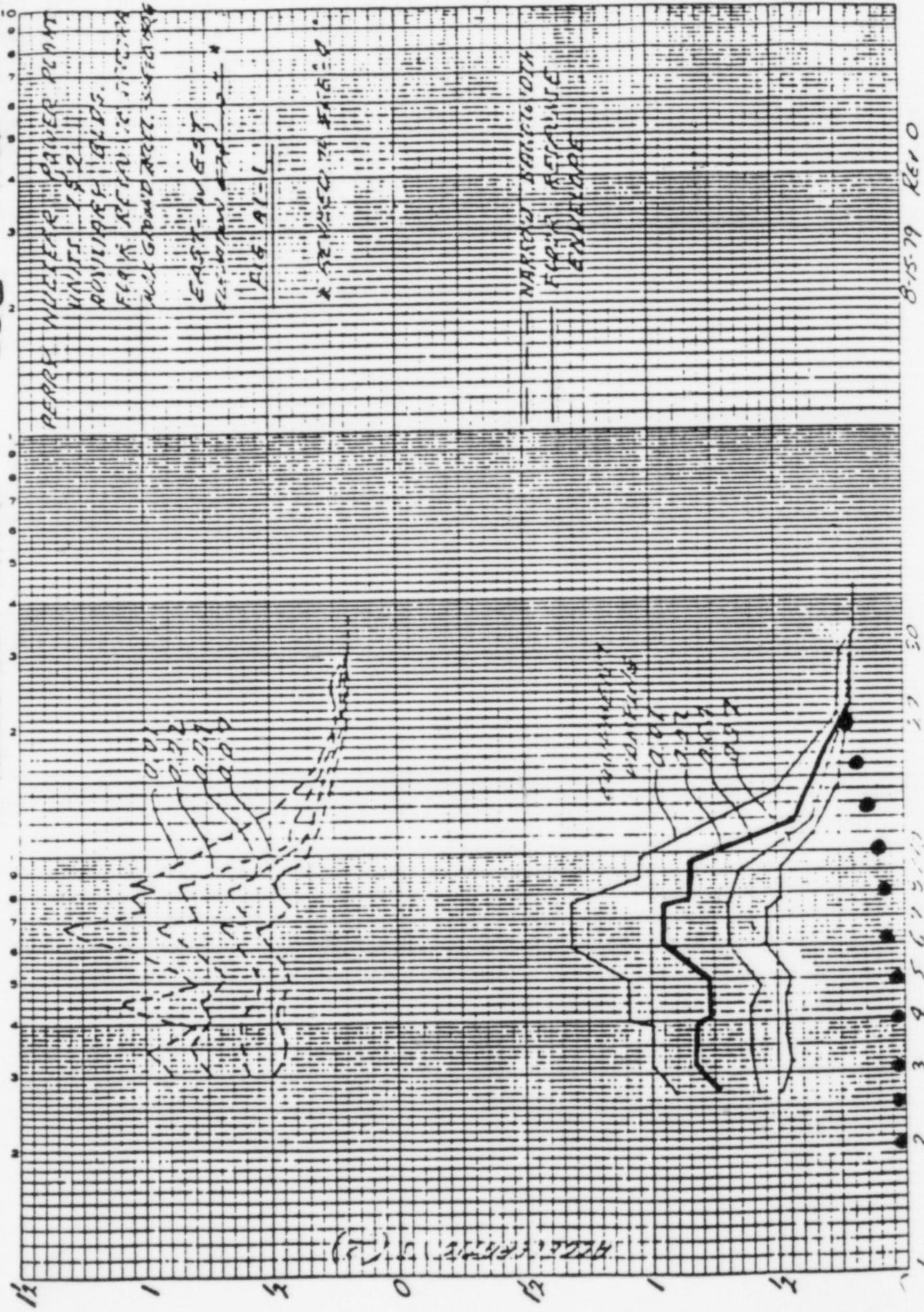
12/30/75 REV. 1  
MST. LOCN: E30-1" (R.B. INSTRUMENTS)

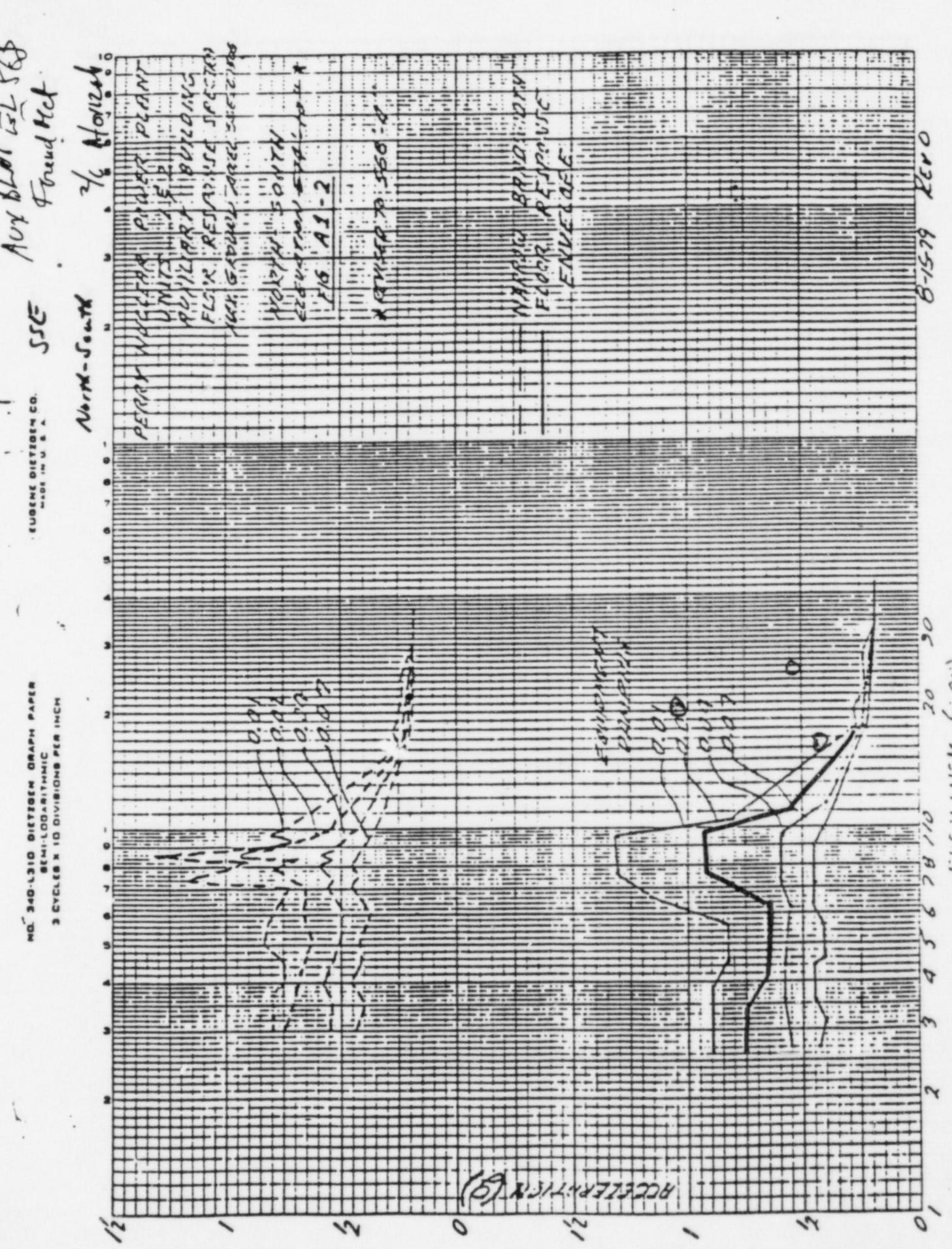
D51-RI90

NO. 740-110 DIASTATION GRAPH PAPER  
SEMI-LOGARITHMIC  
3 CYCLES = 10 DIVISIONS PER INCH

EUGENE DIESTATION CO.  
MADE IN U.S.A.

• Recorded Data



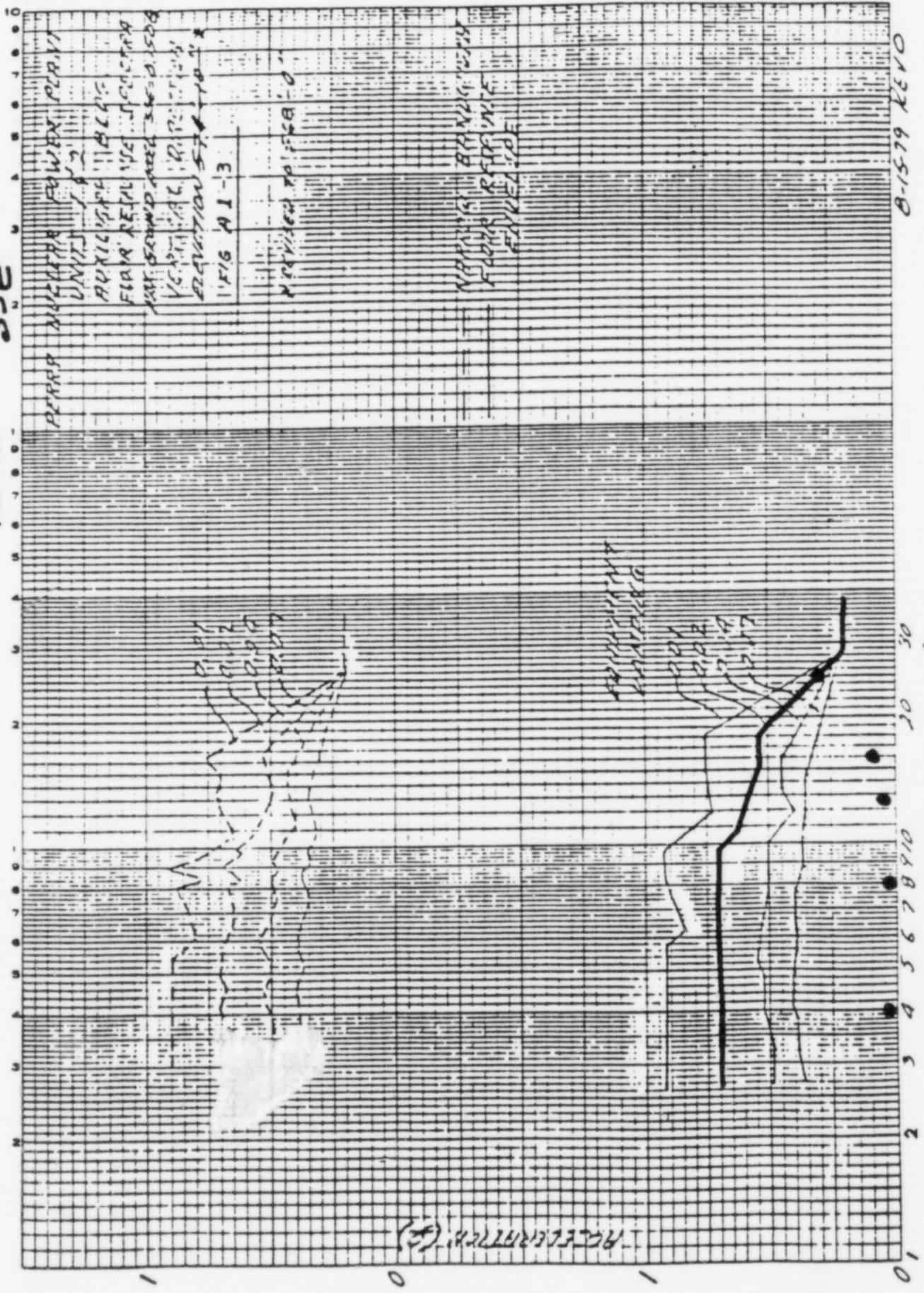


*DSI-R190*

NO. 340-L310 DISSIPATIVE GRAPH PAPER  
SYNLOGARITHMIC  
2 CYCLES X 10 DIVISIONS PER INCH

EUGENE DIETRICH CO.  
MADE IN U.S.A.

Aux Bldg, El. 568'  
Foundation MTR  
SSE



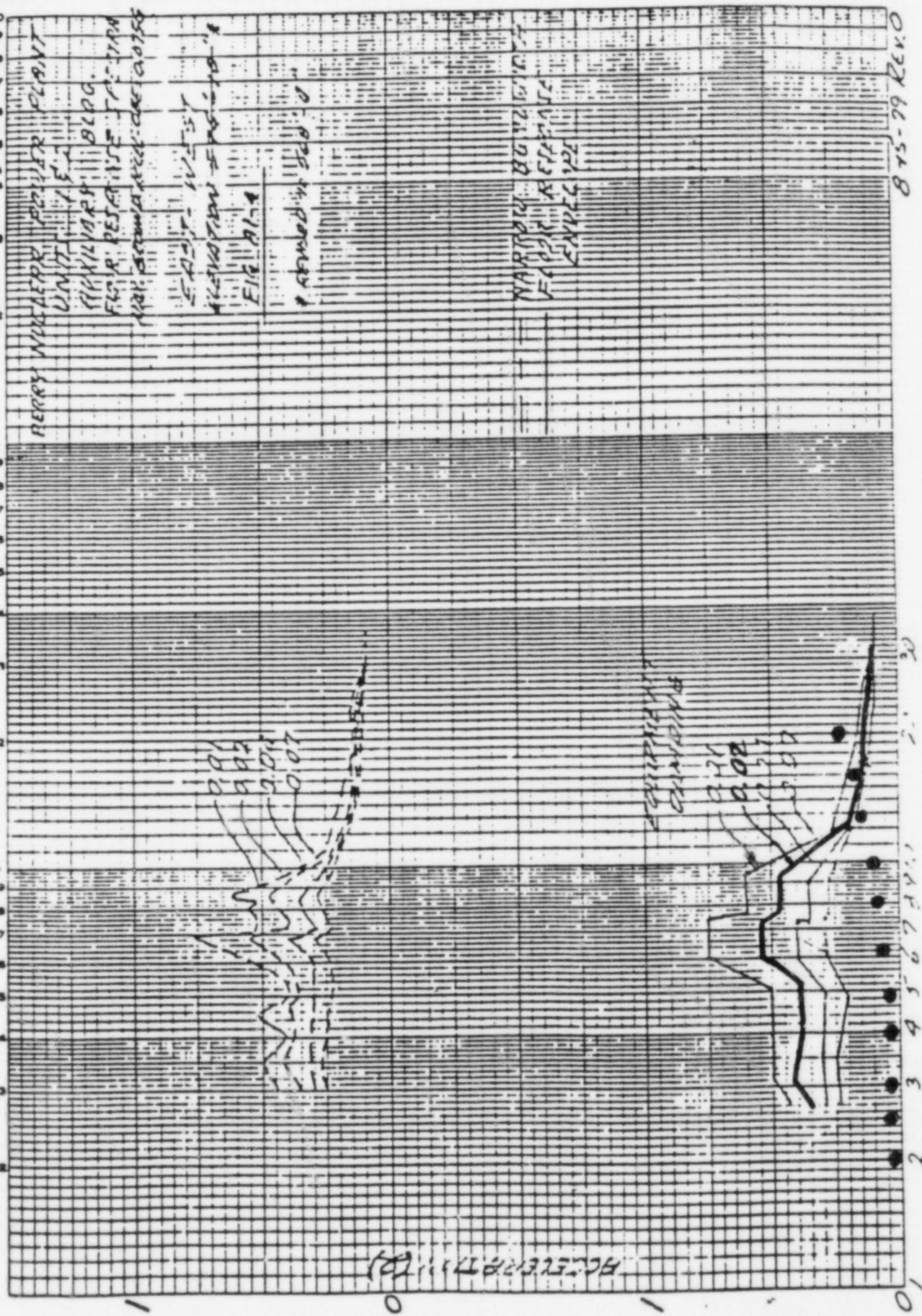
DSI-R190  
EUG DATA  
#PSR-1200

NO. 340-1310 DIAZINE GRAPH PAPER  
SEMI-LOGARITHMIC  
3 CYCLES X 10 DIVISIONS PER INCH

• Recorded Data

EUGEN DITZELIN CO.  
MADE IN U. S. A.

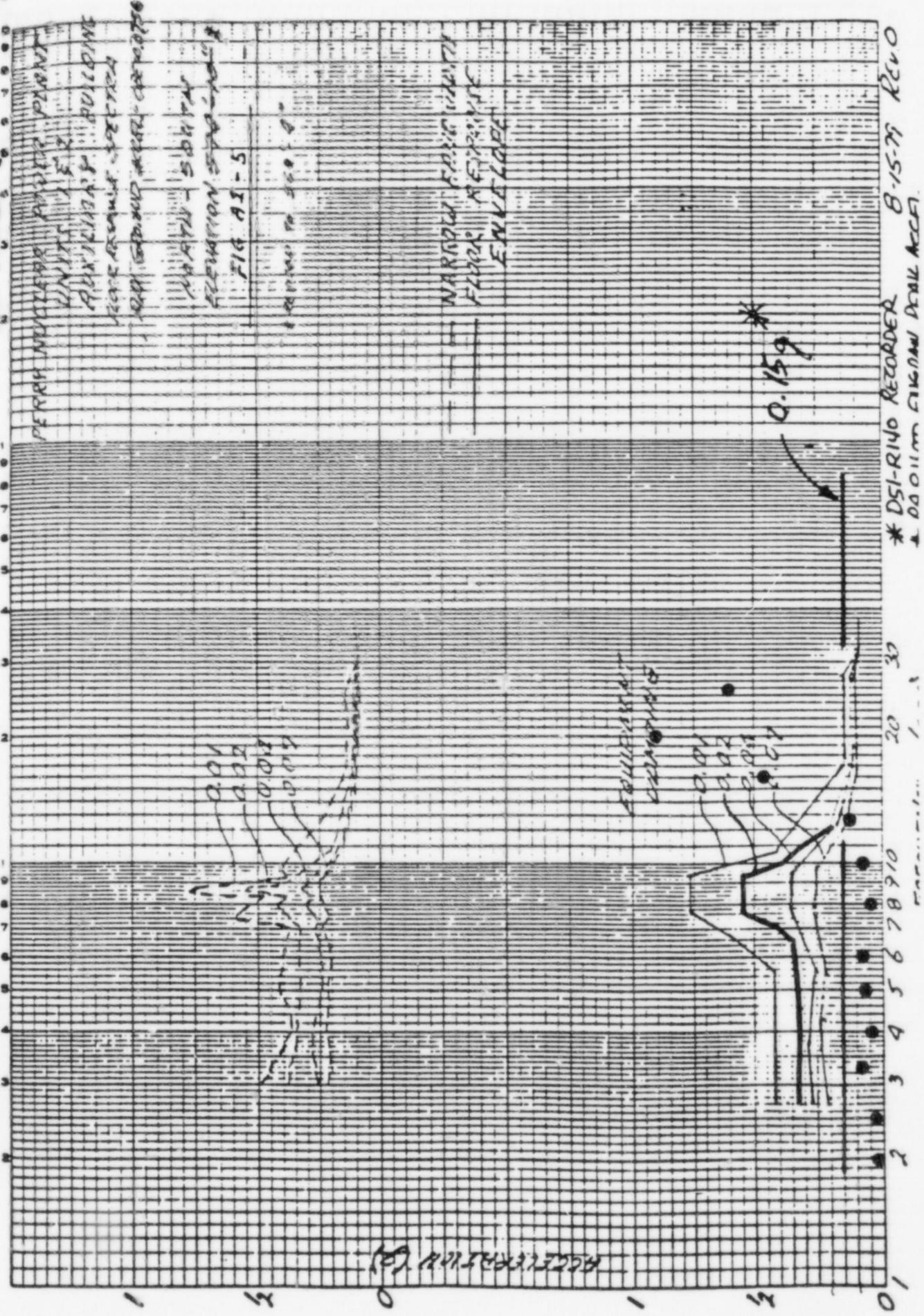
Aux Bdg # 568'-011  
Found Nat  
ABE (2%) EAST-WEST



INSTR. # DS1-R180 (1% D/A)  
MODEL # PSR-11200 (ENG DAHL)  
CALIB DATE : 1-14-85

DATA PRO  
RECOV

NORTH - SOUTH  
AUX BLDG. - OOE (075.3)  
E2. 56.8' (FDN. MAT)



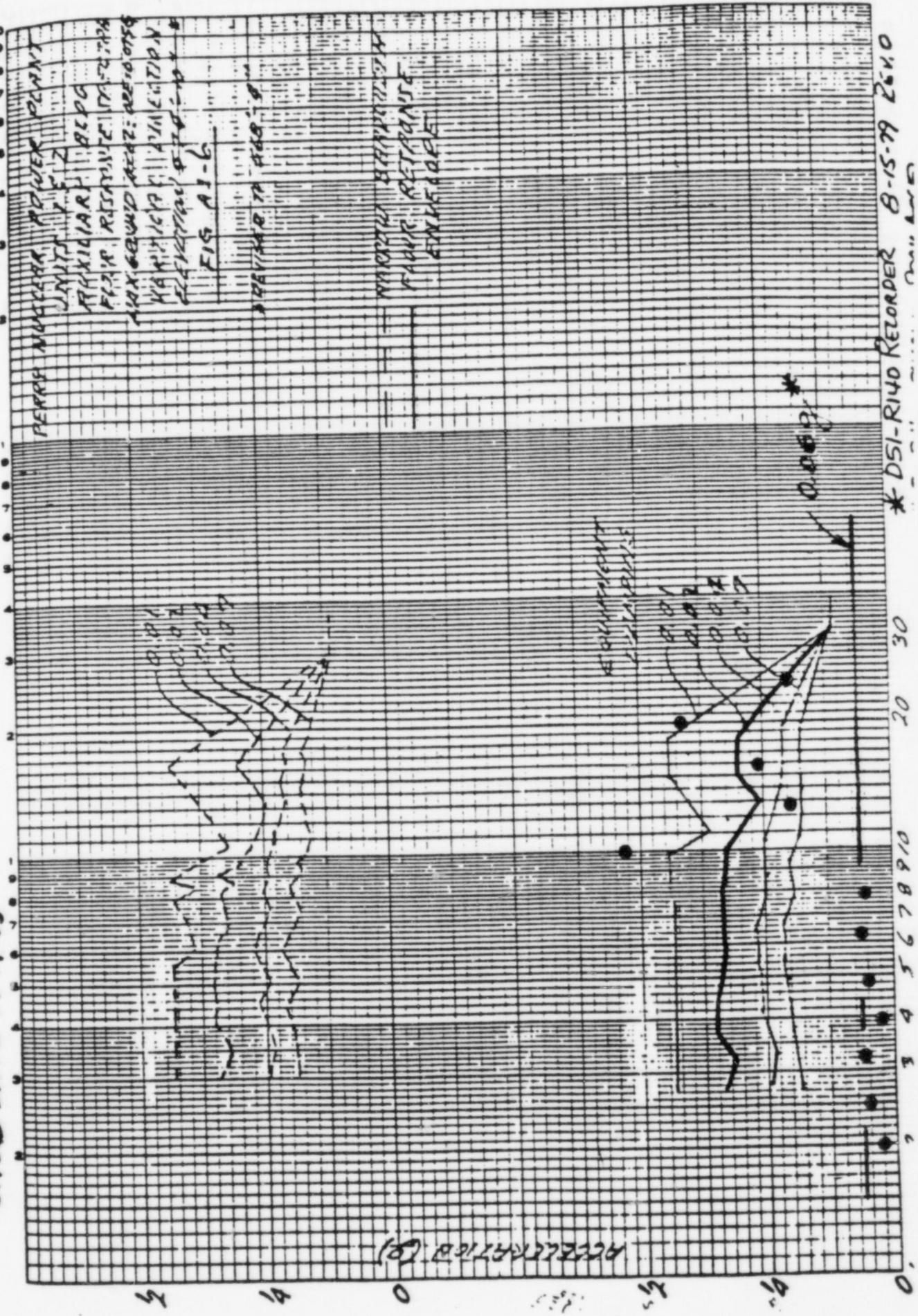
\* DS1-R140 RECORDED 8-15-77 Rev 0

\* 0.001mm increment Dacel Accel

INSTR # D51-R80 (2% DAMP)  
MORDER # PSR-1200  
CAB DATE: 1-14-85

DATA PROW RECORDER

EAST-WEST  
AUX BLOG-OBE (.075g)  
EL 568' (FAN. NAT.)



\* D51-R140 Recorder

8-15-79 2610

PROCESSING NOTESgrade level  
620'

## 1. Sensor Locations:

SMA-3 S/N 165-1  $\Rightarrow$  Reactor Bldg  
(D51-N101) Foundation,  
545'SMA-3 S/N 165-2  $\Rightarrow$  Containment  
(D51-N111) Vessel Annulus,  
682'2. These plots are preliminary,  
as they have not been  
QC - checked. However, no  
changes are anticipated.R. Nigbor  
Kinematics  
2/3/86



VINCENT E. J. C. S.

575' Reactor Foundation

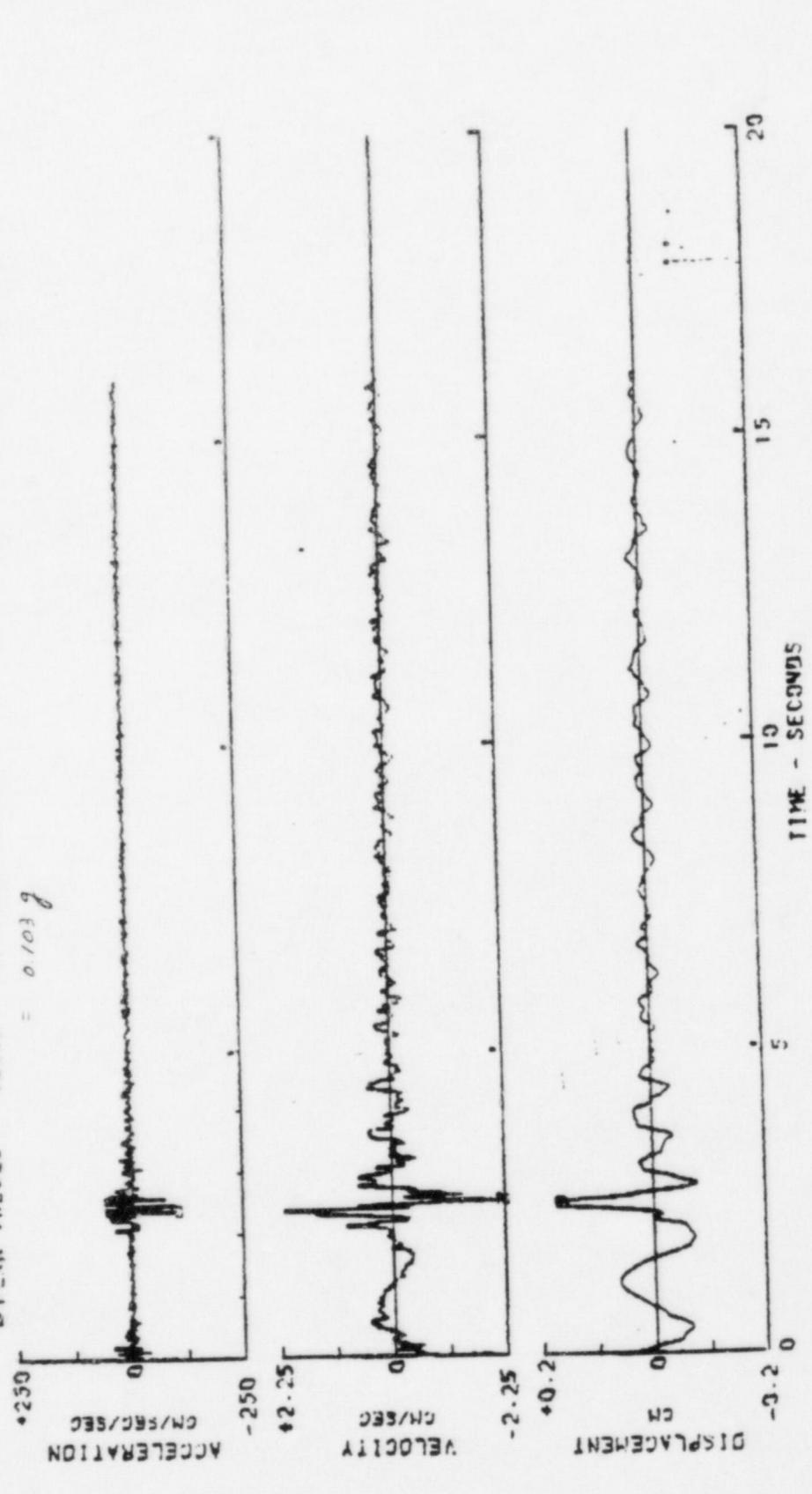
Ground motion

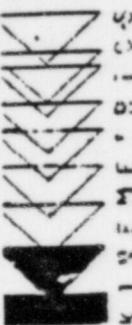
575' Reactor Foundation

Ground motion

575' Reactor Foundation

ML 5.0 EARTHQUAKE JANUARY 31, 1986  
PERIOD: 0.033 SEC.  
ACCELERATION IS 15 BAND-PASSED 0.033-0.035 AND  
VELOCITY IS 12 CM/SEC/SEC; WEL = 2.31 CM/SEC;  
DISPLACEMENT IS 0.16 CM; 31SP = 4.16 CM  
31ASPI = 35.33-40.30 METER/SEC<sup>2</sup>





KINSEY GEOPHYSICS  
575' Reactor Building  
Foundation

MI. 5.0 EARTHQUAKE JANUARY 31, 1986

PERRY NUCLEAR POWER PLANT COMP SOUTH SHWATZ 165-1L  
ACCELEROMETER IS BAND-PASS FILTERED BETWEEN 0.400-0.625 AND 35.30-40.00 HERTZ  
PEAK VALUES: ACCEL = 177.21 CM/SEC/SEC VEL = +1.74 CM/SEC DISPL = 0.36 CM

$$= 0.1419 \rightarrow 0.159$$

