



CALCULATION COVER SHEET

Calculation No. 100031-C-04

Project: North Anna SSI Analysis of ISFSI Pad

Calculation Title: Sliding and Overturning Factor of Safety

References: See page 48

Attachments: See Table of Contents, page 2

Total Number of Pages (Including Cover Sheet):

90

Revision Number	Approval Date	Description of Revision	Originator	Checker	Approver
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SHEET NO. 2

JOB NO. 100031.01 JOB North Anna SSI Analysis of ISFSI Pad

BY APA DATE 6/12/97

CALC. NO. 100031C04R0 SUBJECT Sliding and Overturning Factor of Safety CHK'D DJD DATE 6/12/97

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ATTACHMENT A: COMPUTER INPUT AND OUTPUT FILES ..	41 PAGES
ATTACHMENT B: DIGITIZED FILES	9DISKETTES + 1 PAGE



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SHEET NO. 3

JOB NO. 100031.01 JOB North Anna SSI Analysis of ISFSI Pad

BY APA DATE 6/12/97

CALC. NO. 100031C04R0 SUBJECT Sliding and Overturning Factor of Safety CHK'D DDD DATE 6/12/97

1.0 Purpose

The purpose of this calculation is to document the calculation of sliding and overturning factor of safety of the casks. SASSI [1,2] modules ANALYS and MOTION were used to calculate the acceleration time histories at the mass points of the beams modeling the casks.

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2.0 Analyses

Modules ANALYS and MOTION were used to calculate the acceleration time histories at the nodal points corresponding to the center of the casks in the quarter model used for the SSI analysis of the ISFSI pad.

Program SASSI requires that one independent analysis should be performed for each input direction. Thus, the results for each direction need to be combined. In this case, due to the symmetry in the geometry, the results in the 2 directions orthogonal to the input direction are practically negligible. However, for completeness, the time histories in one direction due to the input in the three directions were added (e.g., x due to x, x due to y, and x due to z).

To calculate the time histories of the factor of safety and casks base shear and moment, the following formulas were used:

Base Shear: $S_i = W \cdot A_i$ $i=x,y$ A_i acceleration time history in g's, $W = 230$ kips

Base Moment: $M_{xx} = 8 \cdot W \cdot A_y - I_{xx} \cdot A_{xx}$ A_{ii} rotational acceleration time history in g's
 $M_{yy} = 8 \cdot W \cdot A_x + I_{yy} \cdot A_{yy}$

FS sliding: $FS_s = (S_x^2 + S_y^2)^{1/2} / (0.3 \cdot W \cdot [1 - A_z])$, coefficient of friction = 0.3

FS overturning: $FS_o = (M_{xx}^2 + M_{yy}^2)^{1/2} / (4 \cdot W \cdot [1 - A_z])$

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3.0 Results

Tables 3-1, 3-2, and 3-3 give the maximum acceleration at the center of the casks for each of the input directions and their time of occurrence. There, it can be seen that the three orthogonal directions are practically uncoupled. Reference 3 should be used for element and node identification.

Figures 3-1, 3-2, and 3-3 show, for the cask defined at node 231, the base shear load in the longitudinal direction, the base shear load in the transverse direction, and the vertical load due to the input in the 3 directions. Figures 3-4 and 3-5 show the time histories of the inverse of the sliding and overturning factors of safety (1/FS) based on those shear and axial loads.

Figure 3-6 to 3-10, 3-11 to 3-15, 3-16 to 3-20, 3-21 to 3-25, 3-26 to 3-30, and 3-31 to 3-35 show the same sets of results for nodes 232, 233, 234, 235, 236, and 237, respectively.

According to these figures, the lowest factor of safety for overturning is about $1/0.6 = 1.67$ at 3.71 seconds and higher than about 2 the rest of the time. ✓

According to these figures, the lowest factor of safety for sliding occurs for the casks defined at node 231 (close to the center of the pad) at time 3.71 seconds and it is slightly higher than one. However, it should be noted that the ground motions in the x and y directions have an extreme peak occurring at the same time at 3.71 seconds (Reference 4) even though they are statistically independent. This situation is very unrealistic and it is due to the fact that these motions correspond to artificially generated time histories. At any other time, the factor of safety is higher than 1.25. This value represents a more realistic factor of safety since it is calculated in a region with extreme peaks in both directions but they do not occur at the same time.

This higher than one value can be confirmed if this factor of safety is estimated by using the 100-40-40 rule suggested in the ASCE Standard 4-86 (Reference 5) to combine the effects of the maximum forces induced by each direction of the input motion. This combination rule recognizes the fact that having an extreme peak in both input directions is unrealistic. At node 231 the maximum accelerations in each direction are:

$$A_x = 0.227g$$

$$A_y = 0.227g$$

$$A_z = 0.124g$$



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Assuming (100%x, 40%y, 40%z)

$$FSs = 0.3 * (1 - 0.050) / (0.227^2 + 0.091^2)^{1/2} = 1.165 \quad \checkmark$$

Assuming (40%x, 100%y, 40%z)

$$FSs = 0.3 * (1 - 0.050) / (0.091^2 + 0.227^2)^{1/2} = 1.165 \quad -$$

Assuming (40%x, 40%y, 100%z)

$$FSs = 0.3 * (1 - 0.124) / (0.091^2 + 0.091^2)^{1/2} = 2.042 \quad \checkmark$$

Thus, the use of this combination rule gives a minimum factor of safety for sliding of 1.165.



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Table 3-1 Input X Direction: Maximum Absolute Acceleration (g's)

N.P.	X	AT TIME	Y	AT TIME	Z	AT TIME
198	0.2155	6.6400	0.0001	10.0300	0.0022	9.3800
203	0.2152	6.6400	0.0003	9.7400	0.0044	9.5500
208	0.2145	6.6400	0.0005	5.9100	0.0047	5.8300
213	0.2137	6.6400	0.0006	10.3400	0.0057	5.8200
218	0.2121	6.6400	0.0005	6.6600	0.0067	5.9500
223	0.2095	3.7100	0.0010	6.6600	0.0070	6.2700
228	0.2093	3.7100	0.0018	5.7900	0.0243	5.7300
231	0.2276	6.6400	0.0009	10.0300	0.0022	9.3800
232	0.2285	9.1000	0.0021	9.7400	0.0044	9.5500
233	0.2302	9.1000	0.0039	5.9100	0.0047	5.8300
234	0.2283	9.1000	0.0035	5.9000	0.0057	5.8200
235	0.2259	6.6400	0.0034	6.1500	0.0067	5.9500
236	0.2178	9.1000	0.0091	5.8700	0.0070	6.2700
237	0.2411	9.1000	0.0142	5.7900	0.0244	5.7300



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Table 3-1 (cont.) Maximum Absolute Angular Accelerations (Rads/Sec/Sec/g)

N.P.	XX	AT TIME	YY	AT TIME	ZZ	AT TIME
198	0.0001	10.0300	0.0031	5.7100	0.0000	5.7200
203	0.0002	9.2600	0.0029	5.7100	0.0000	5.7200
208	0.0004	5.9100	0.0030	5.7100	0.0000	5.7200
213	0.0004	5.9000	0.0031	5.7100	0.0000	5.7200
218	0.0004	6.1500	0.0028	5.7100	0.0000	5.7200
223	0.0010	5.8700	0.0026	5.7100	0.0000	5.7200
228	0.0015	5.7900	0.0056	5.7200	0.0000	5.7200
231	0.0001	10.0300	0.0035	5.7100	0.0000	5.7200
232	0.0002	9.2600	0.0033	5.7100	0.0000	5.7200
233	0.0004	5.9100	0.0034	5.7100	0.0000	5.7200
234	0.0004	5.9000	0.0035	5.7100	0.0000	5.7200
235	0.0004	6.1500	0.0032	5.7100	0.0000	5.7200
236	0.0010	5.8700	0.0030	5.7100	0.0000	5.7200
237	0.0016	5.7900	0.0060	5.7200	0.0000	5.7200



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Table 3-2. Input Y Direction. Maximum Absolute Acceleration (g's)

N.P.	X	AT TIME	Y	AT TIME	Z	AT TIME
198	0.0005	8.0900	0.1960	3.7100	0.0366	14.2600
203	0.0014	8.0800	0.1961	3.7100	0.0372	14.2600
208	0.0018	9.2400	0.1960	3.7100	0.0381	14.2600
213	0.0024	9.2400	0.1961	3.7100	0.0388	7.5100
218	0.0029	9.2300	0.1954	3.7100	0.0390	7.5100
223	0.0040	7.9400	0.1879	7.2400	0.0373	7.5000
228	0.0047	9.0900	0.1884	3.7100	0.0283	7.5000
231	0.0015	8.2500	0.2238	10.2200	0.0367	14.2600
232	0.0032	8.2500	0.2246	4.3500	0.0373	14.2600
233	0.0031	5.2000	0.2278	4.3500	0.0381	14.2600
234	0.0038	9.2400	0.2309	4.3500	0.0389	7.5100
235	0.0065	8.0800	0.2328	4.3500	0.0390	7.5100
236	0.0106	8.0700	0.2282	4.3400	0.0374	7.5000
237	0.0153	8.0400	0.2240	4.3400	0.0284	7.5000



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Table 3-2 (cont.) Maximum Absolute Angular Accelerations (Rads/Sec/Sec/g)

N.P.	XX	AT TIME	YY	AT TIME	ZZ	AT TIME
198	0.0069	14.2000	0.0001	8.2500	0.0001	4.4400
203	0.0070	14.2000	0.0003	8.2900	0.0002	4.4400
208	0.0072	14.2000	0.0003	4.9800	0.0003	8.0800
213	0.0073	14.2000	0.0003	7.6500	0.0003	9.2400
218	0.0070	14.2000	0.0006	7.6400	0.0004	4.6100
223	0.0067	7.4500	0.0010	7.5800	0.0006	5.2700
228	0.0061	7.4400	0.0016	7.5600	0.0007	14.2100
231	0.0074	14.2000	0.0001	8.2500	0.0001	4.4400
232	0.0075	14.2000	0.0003	8.2900	0.0002	4.4400
233	0.0076	14.2000	0.0003	4.9800	0.0003	8.0800
234	0.0077	14.2000	0.0004	7.6500	0.0003	9.2400
235	0.0075	14.2000	0.0007	7.6400	0.0004	4.6100
236	0.0071	7.4500	0.0011	8.0700	0.0006	5.2700
237	0.0065	7.4400	0.0017	7.5600	0.0007	14.2100



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Table 3-3. Input Z Direction. Maximum Absolute Acceleration (g's)

N.P.	X	AT TIME	Y	AT TIME	Z	AT TIME
198	0.0006	3.7300	0.0033	7.9900	0.1335	7.2500
203	0.0019	5.7200	0.0032	7.9900	0.1333	7.2500
208	0.0030	5.7200	0.0031	7.9900	0.1315	7.2500
213	0.0036	5.7200	0.0031	5.6800	0.1295	7.2500
218	0.0037	5.7200	0.0032	5.7400	0.1294	7.2500
223	0.0039	5.9400	0.0034	5.7400	0.1304	7.2500
228	0.0058	5.7300	0.0027	1.9800	0.1287	7.2500
231	0.0024	8.4500	0.0263	7.9900	0.1336	7.2500
232	0.0058	3.7900	0.0255	7.9900	0.1334	7.2500
233	0.0062	3.7800	0.0244	5.6800	0.1316	7.2500
234	0.0066	5.7600	0.0243	5.6800	0.1295	7.2500
235	0.0064	8.2100	0.0253	5.7400	0.1294	7.2500
236	0.0087	5.8900	0.0268	5.7400	0.1304	7.2500
237	0.0221	5.6800	0.0205	1.9800	0.1288	7.2500



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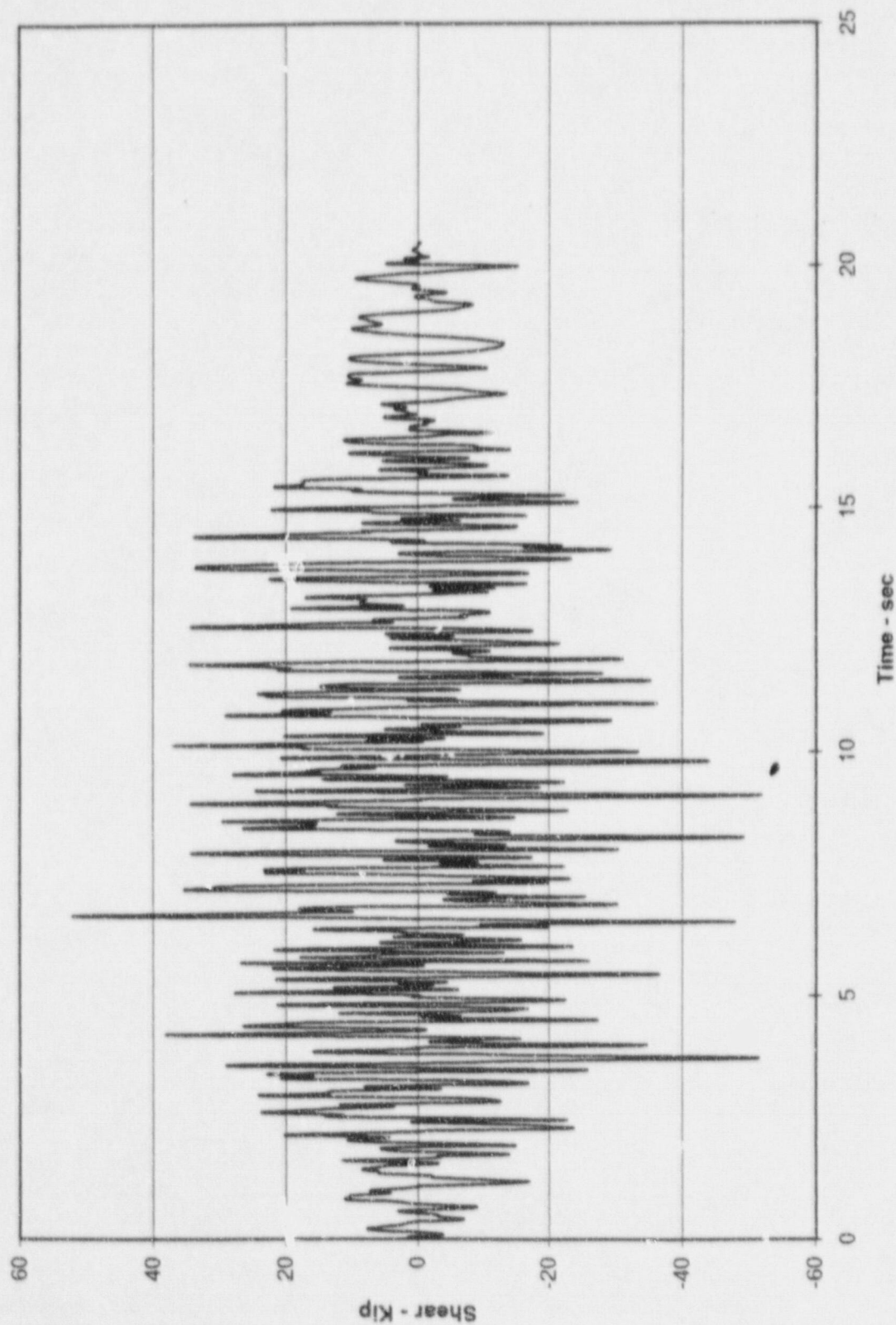
SHEET NO. 12JOB NO. 100031.01 JOB North Anna SSI Analysis of ISFSI PadBY APA DATE 6/12/97CALC. NO. 100031CC4R0 SUBJECT Sliding and Overturning Factor of SafetyCHK'D DJD DATE 6/12/97

Table 3-3 (cont.) Maximum Absolute Angular Accelerations (Rads/Sec/Sec/g)

N.P.	XX	AT TIME	YY	AT TIME	ZZ	AT TIME
198	0.0028	7.9900	0.0002	6.1000	0.0000	8.5100
203	0.0027	7.9900	0.0005	3.7900	0.0000	8.4500
208	0.0026	5.6800	0.0006	3.7800	0.0000	2.1000
213	0.0026	5.6800	0.0005	8.1200	0.0000	8.3400
218	0.0027	5.7400	0.0006	8.1600	0.0000	2.3500
223	0.0029	5.7400	0.0009	8.1300	0.0000	2.0600
228	0.0022	5.6800	0.0021	5.6800	0.0000	5.7400
231	0.0029	7.9900	0.0002	6.0400	0.0000	8.5100
232	0.0028	7.9900	0.0005	3.7900	0.0000	8.4500
233	0.0027	5.6800	0.0006	3.7800	0.0000	2.1000
234	0.0027	5.6800	0.0006	8.1200	0.0000	8.3400
235	0.0028	5.7400	0.0007	8.1600	0.0000	2.3500
236	0.0030	5.7400	0.0009	8.1300	0.0000	2.0600
237	0.0023	1.9800	0.0022	5.6800	0.0000	5.7400

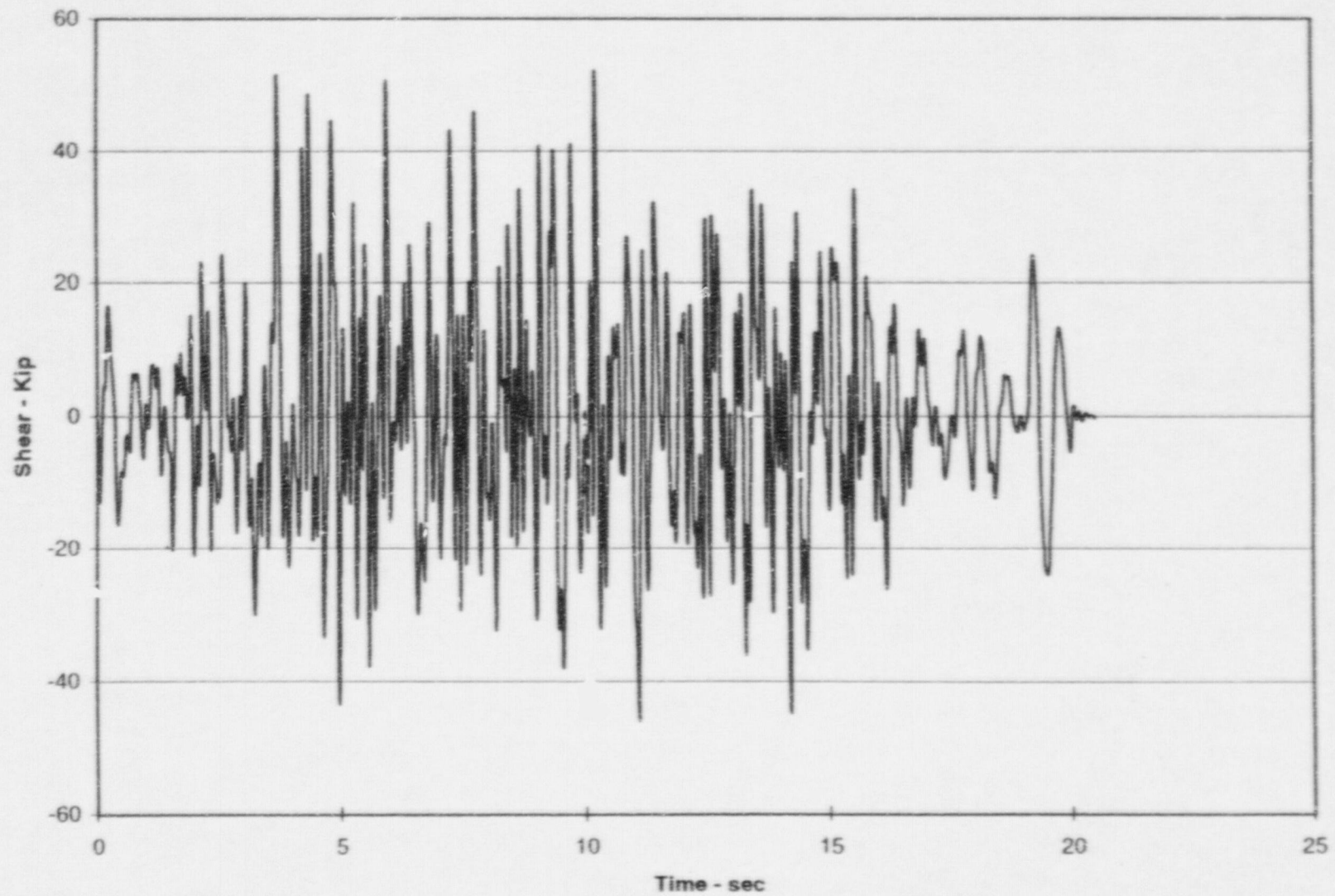
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Figure 3-1. Node 231 - Shear X Direction



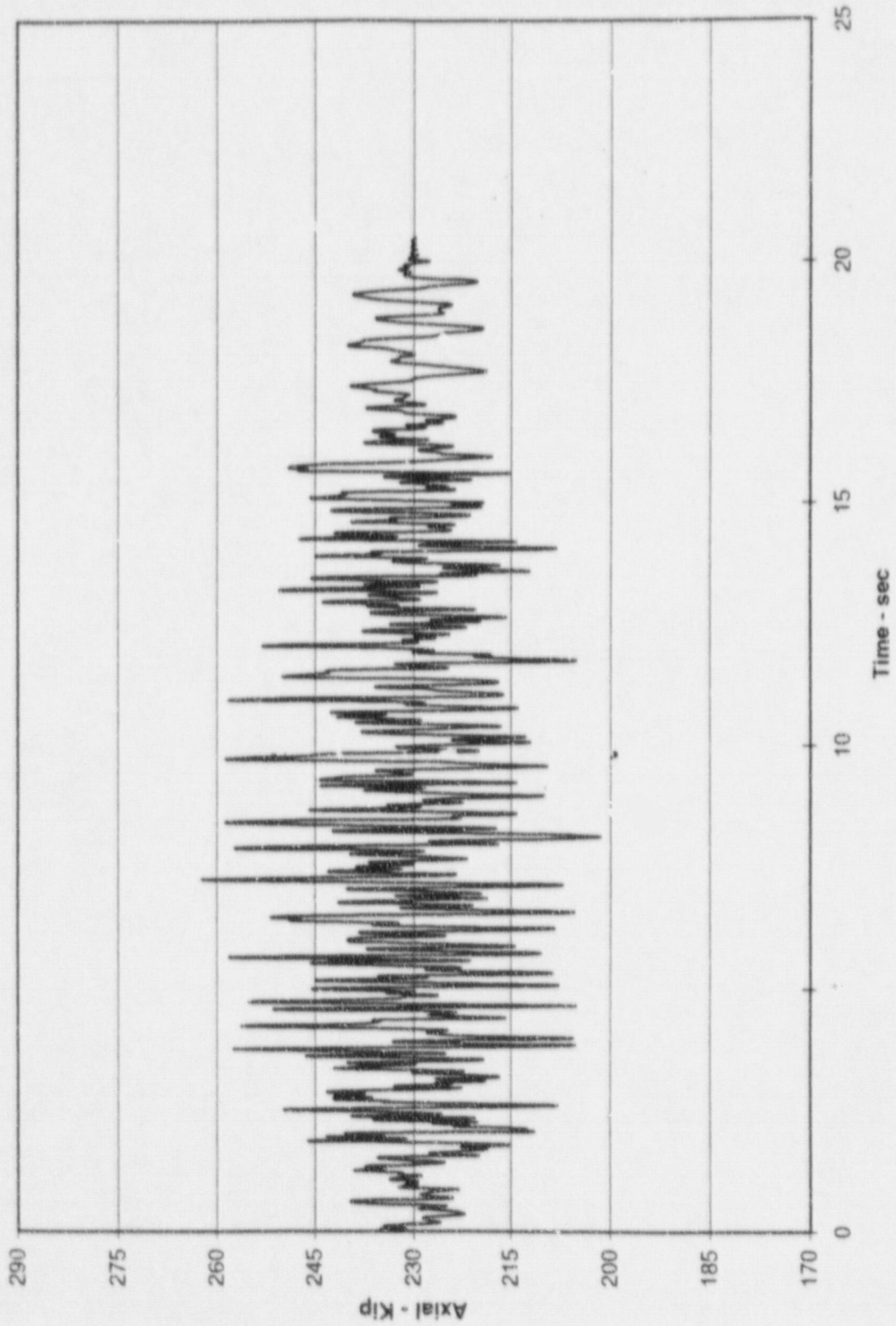
BY: APA 6/12/97
CHK: DJB 6/12/97

Figure 3-2. Node 231 - Shear Y Direction



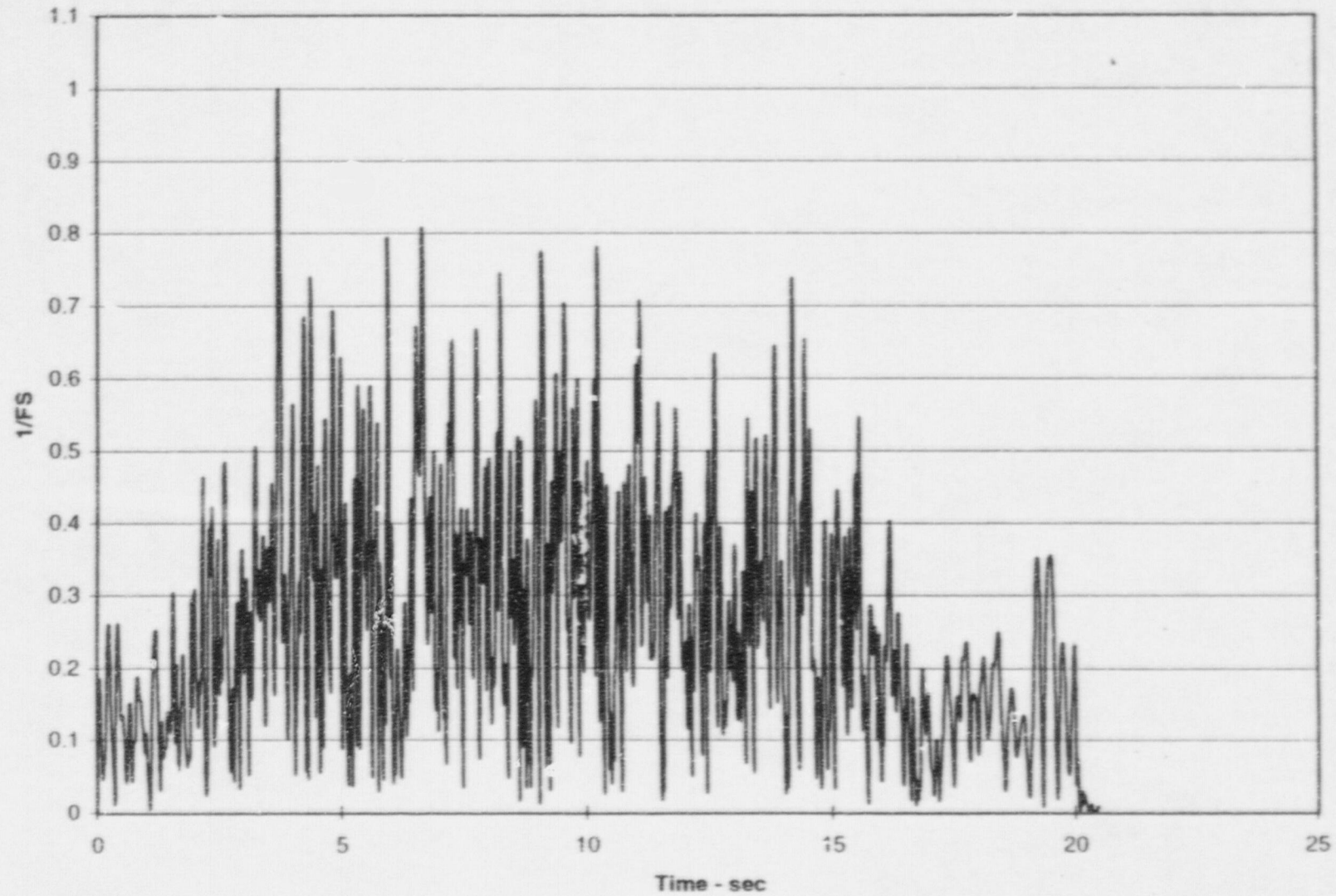
BY: AEA 6/12/97
CHK: DDD 6/12/97

Figure 3-3. Node 231 - Axial Load



BY: APA 6/12/97
CHK: DJD 6/12/97

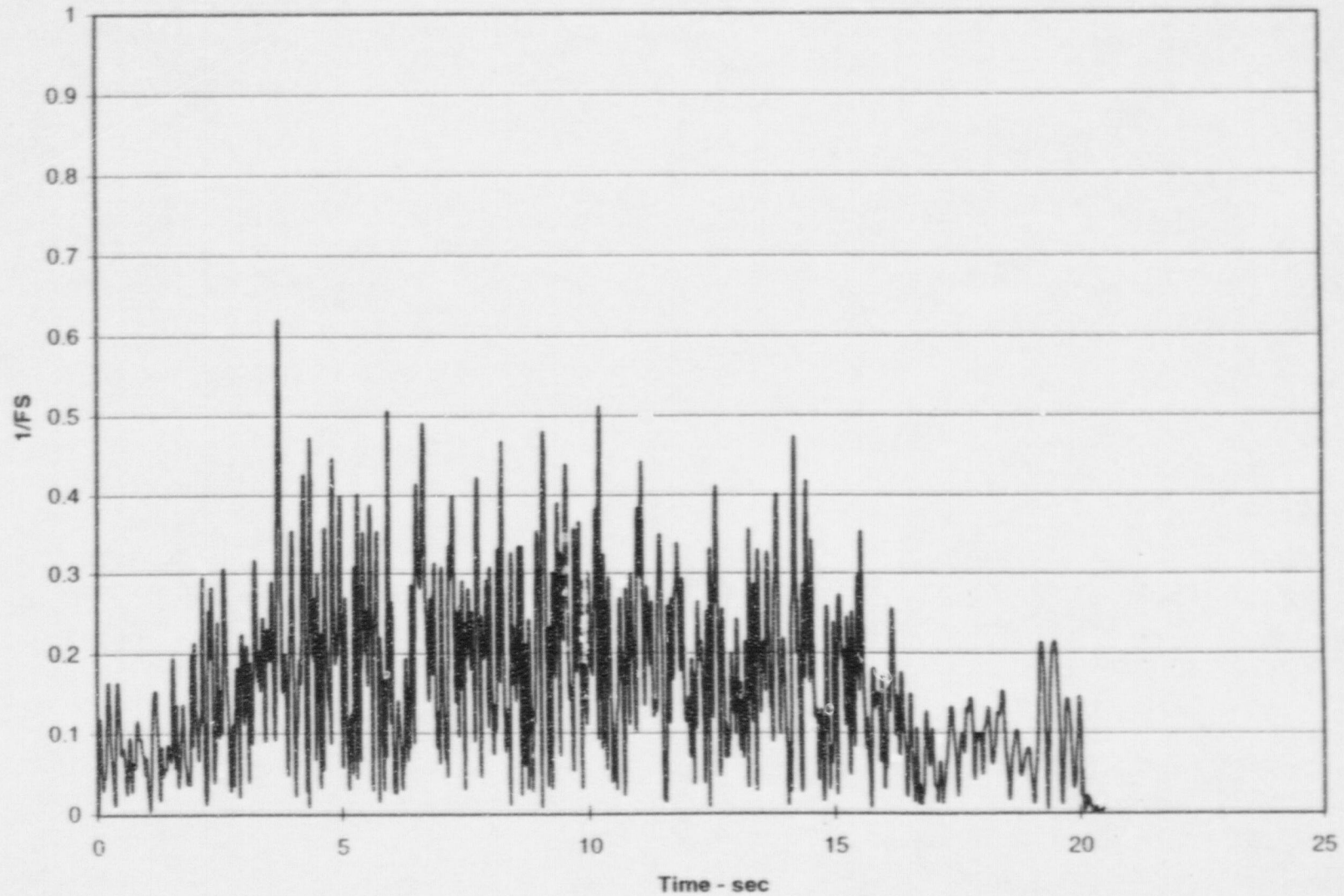
Figure 3-4. Node 231 - Sliding Factor of Safety



By: ADA 6/12/07
CHK: DTD 6/12/07

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Figure 3-5. Node 231 - Overturning Factor of Safety



BY: AFA 6/12/97
CHK: DTD 6/12/97

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BY: APA 6/12/97
CHK: DJD 6/12/97

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Channel (3)

Figure 3-6. Node 232 - Shear X Direction

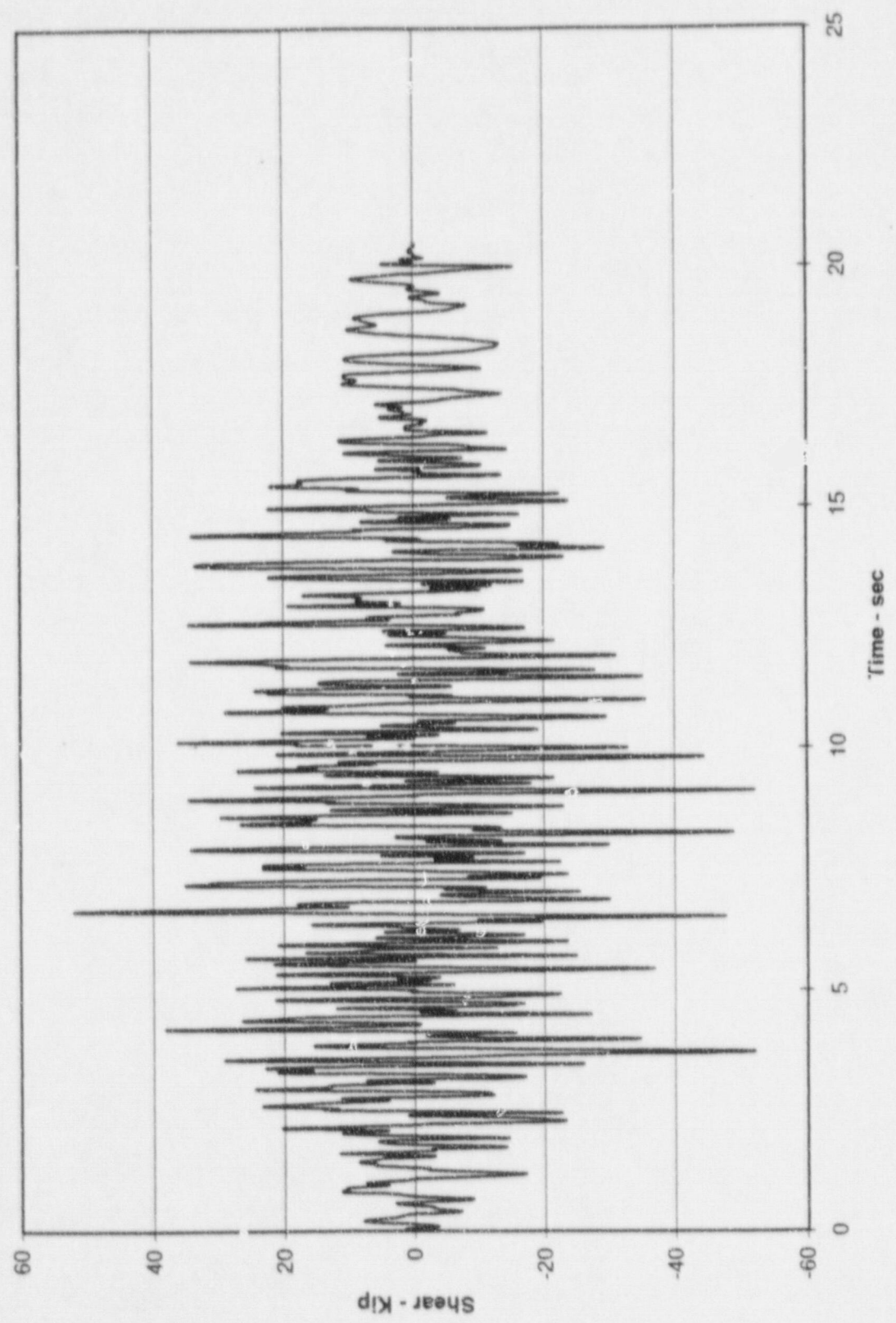
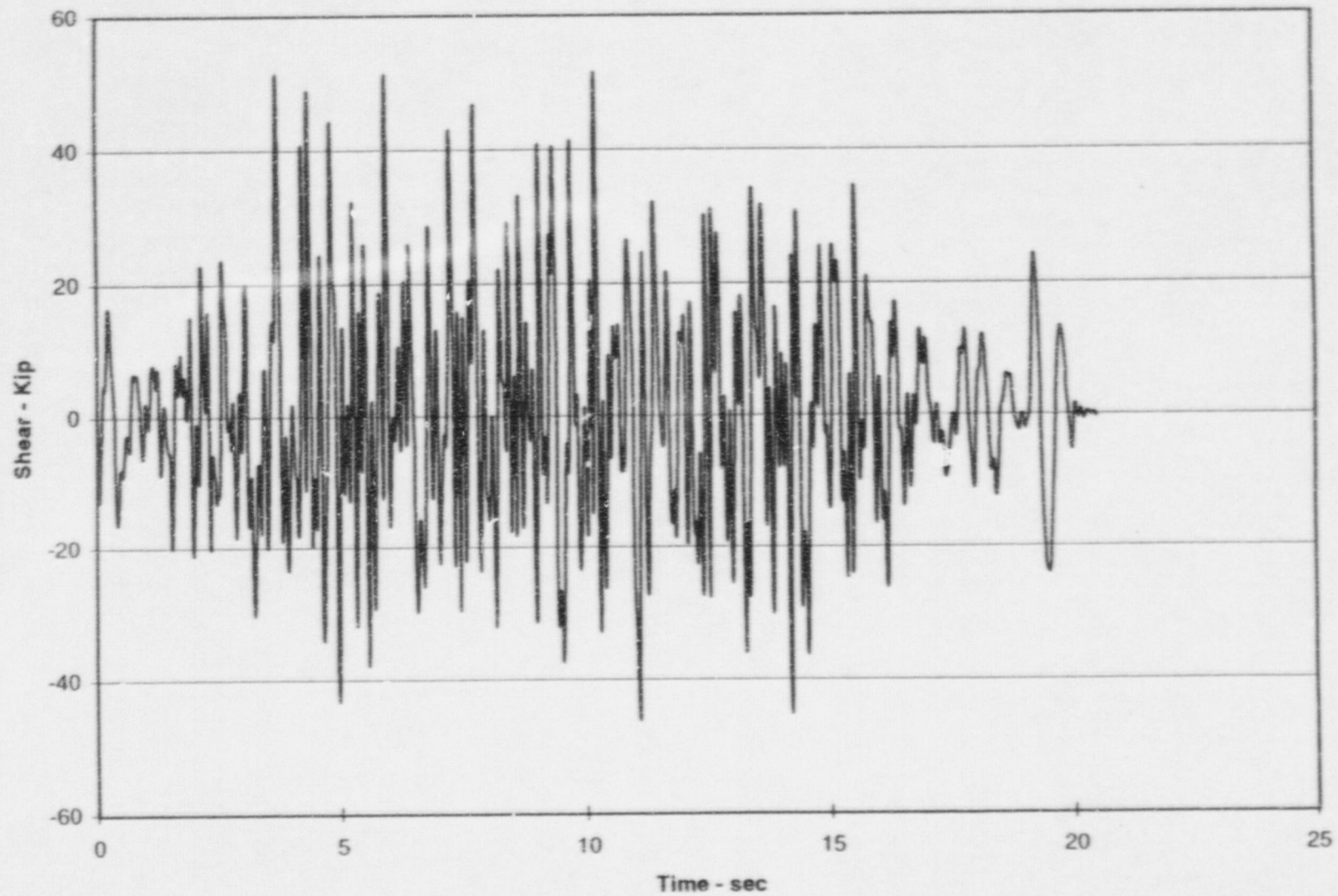


Figure 3-7. Node 232 - Shear Y Direction

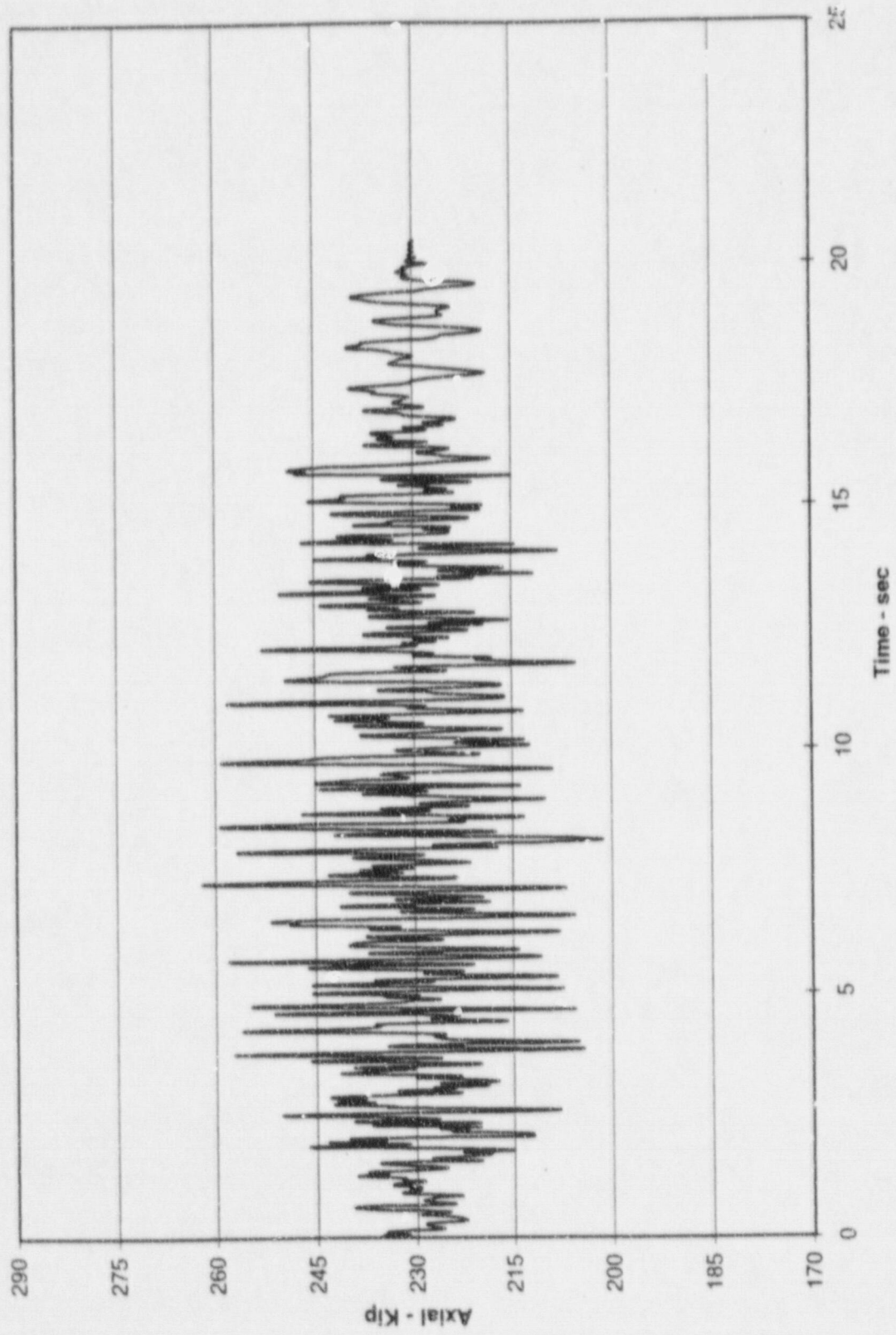


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BY: HPA 6/12/97
CHK: EOD 6/12/97

BY: APA 6/12/97
CHK: DJD 6/12/97

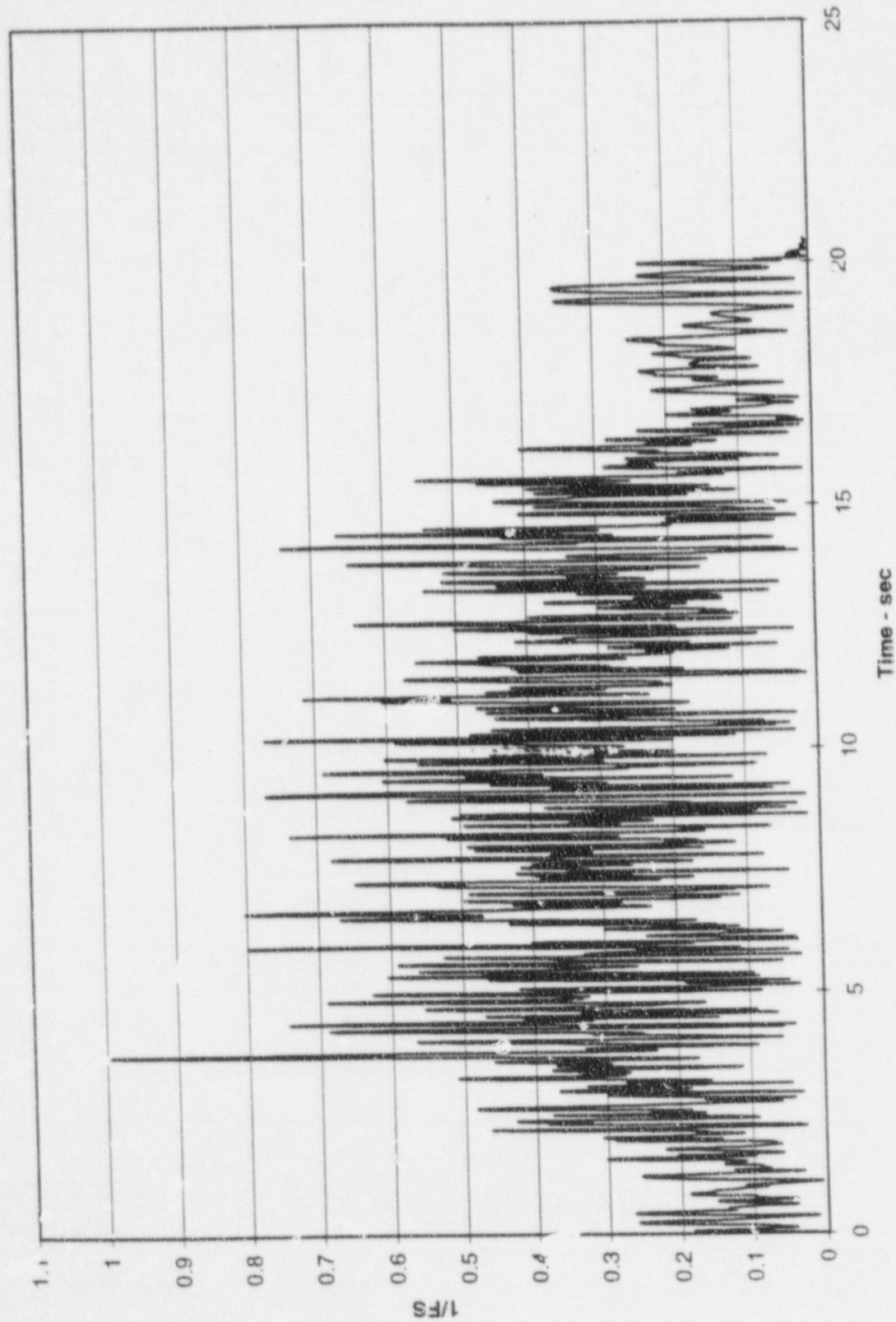
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Figure 3-8. Node 232 - Axial Load



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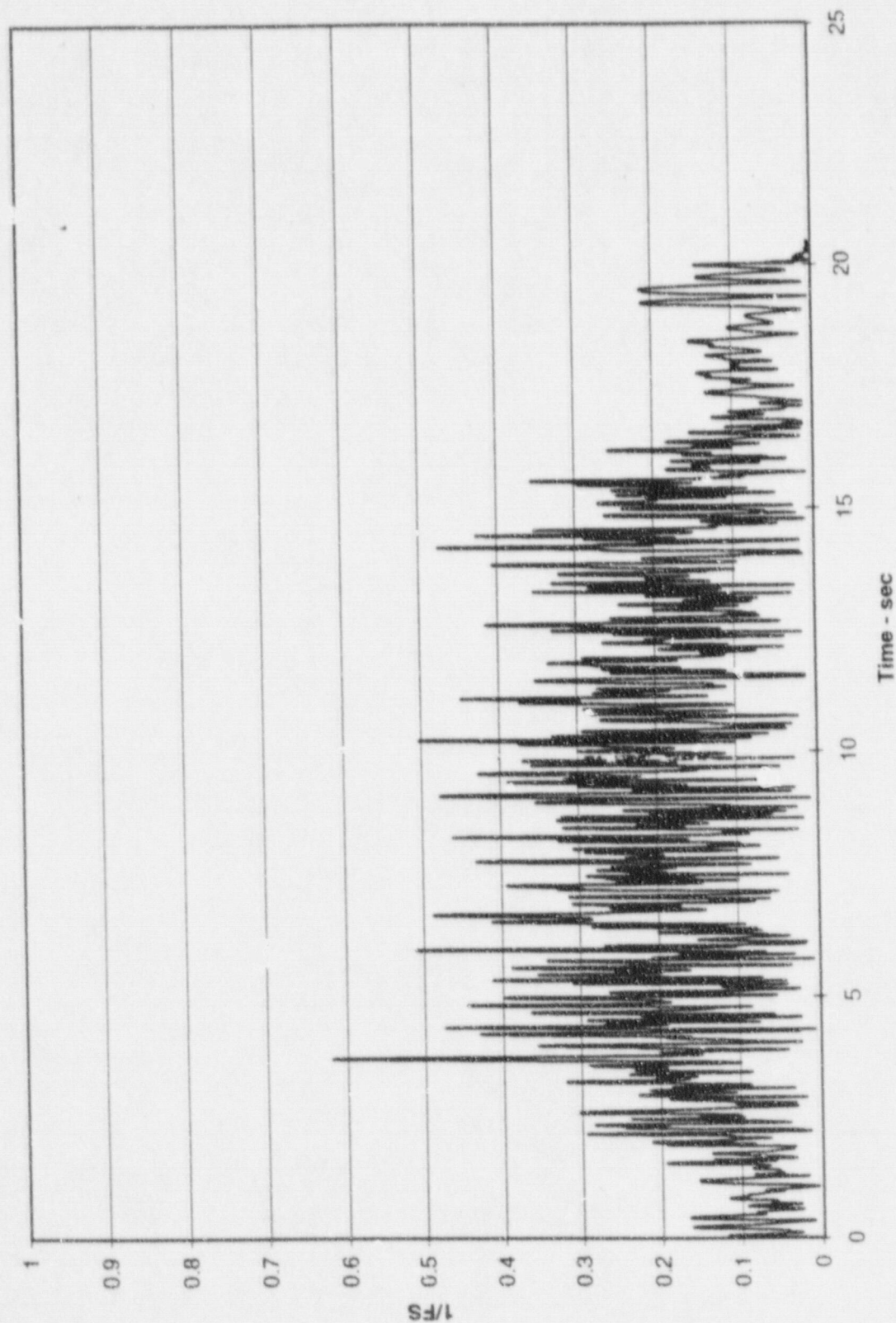
Figure 3-9. Node 232 - Sliding Factor of Safety



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BY: APA 6/12/97
CHK: DJD 6/12/97

C. .1 (2)

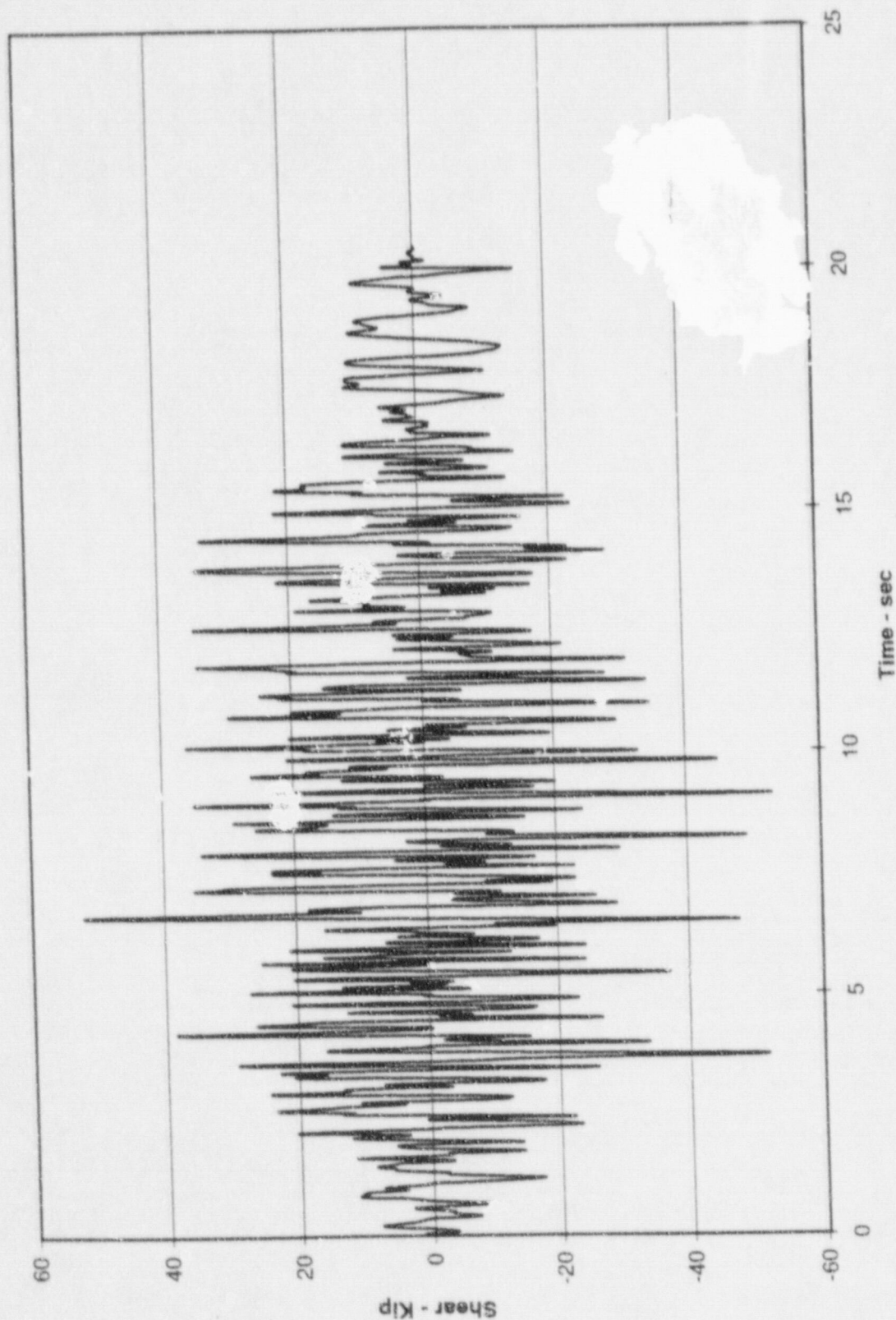
Figure 3-10. Node 232 - Overturning Factor of Safety



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BY: APA 6/12/97
CHK: DJD 6/12/97

1.22

Figure 3-11. Node 233 - Shear X Direction



1000 31204

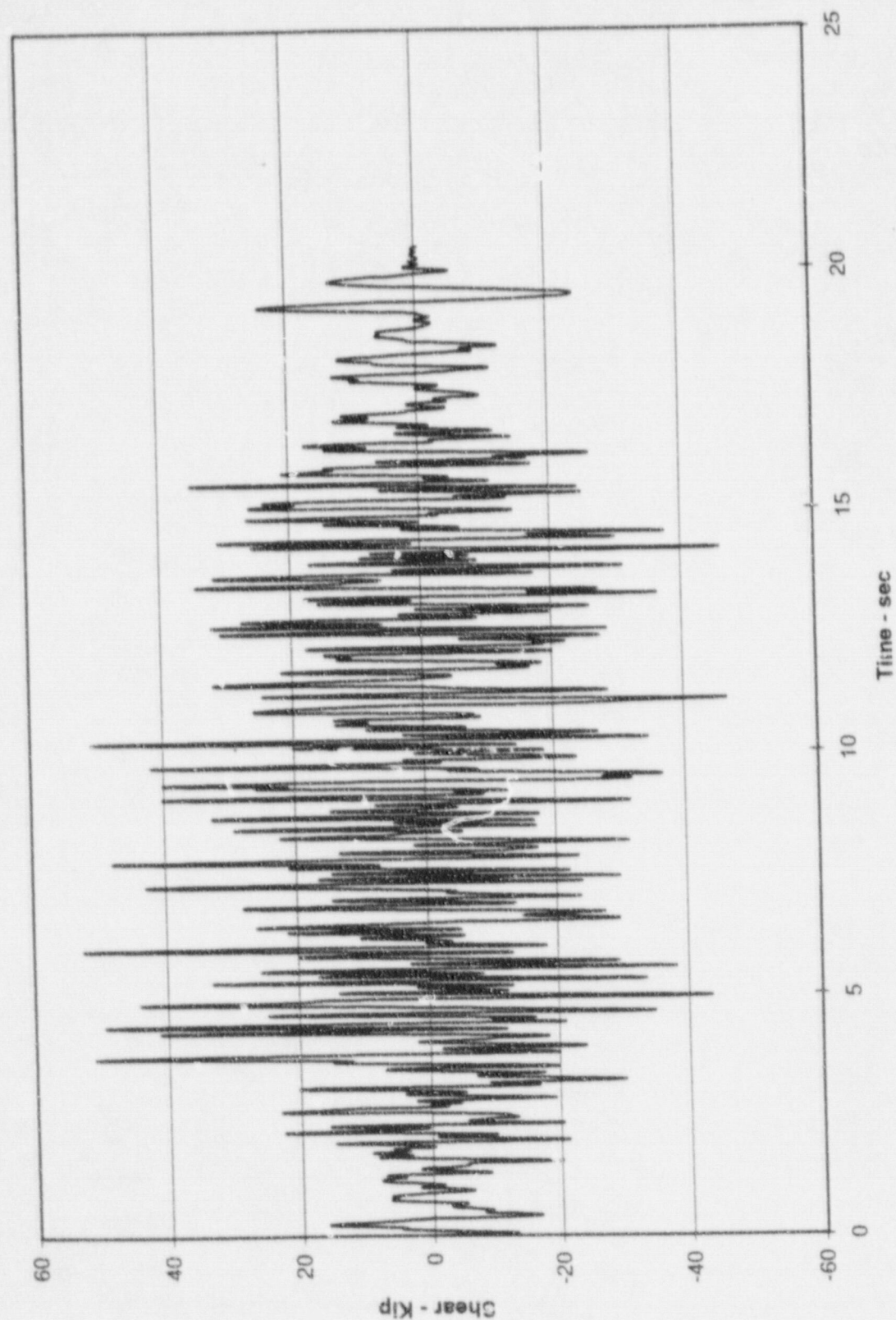
BY: APA 6/12/97

CHK: DDD 6/12/97

P. 20

Chart 1 (A)

Figure 3-12. Node 233 - Shear Y Direction

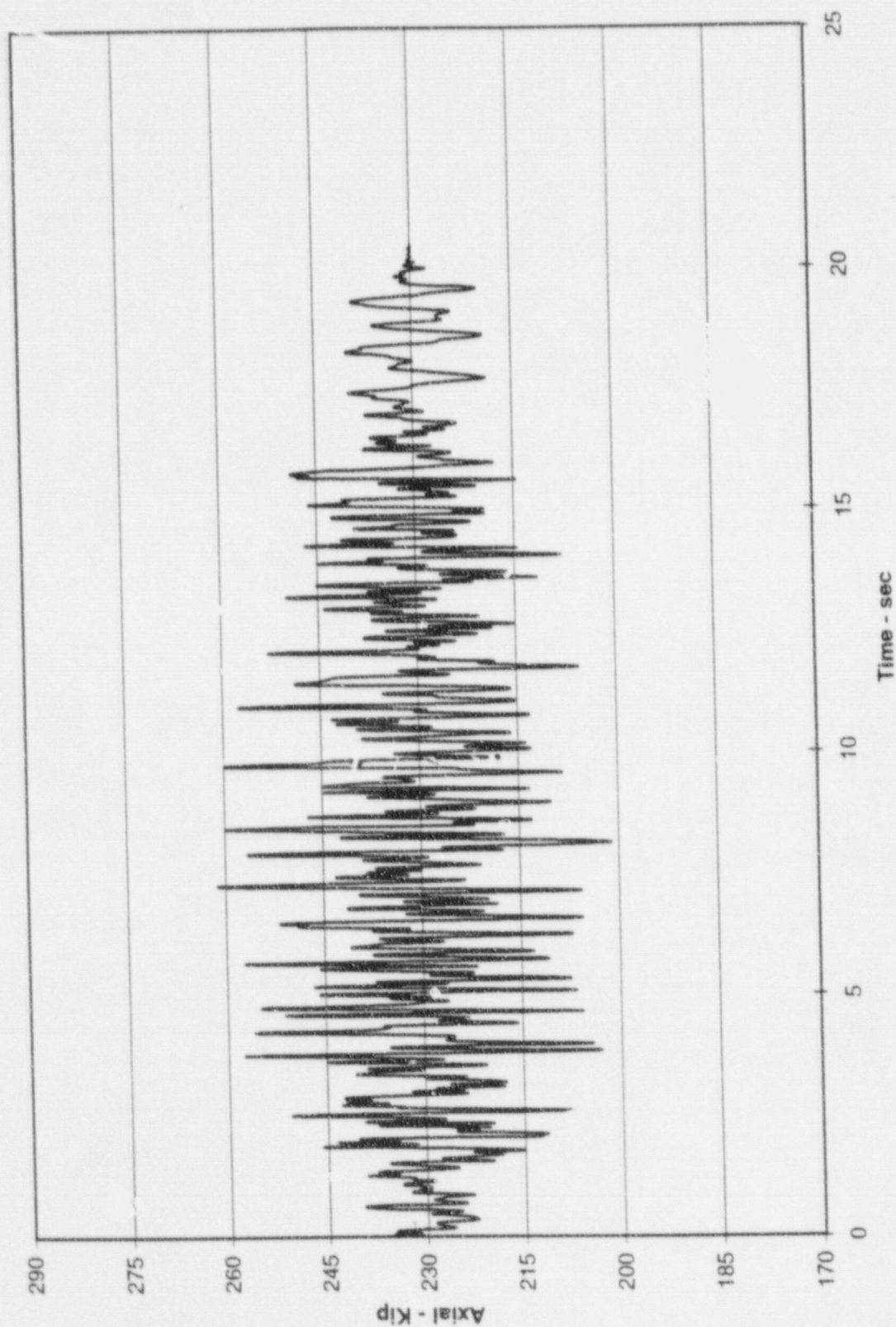


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CHK. DSD 6/12/97

1.67

Chart1 (5)

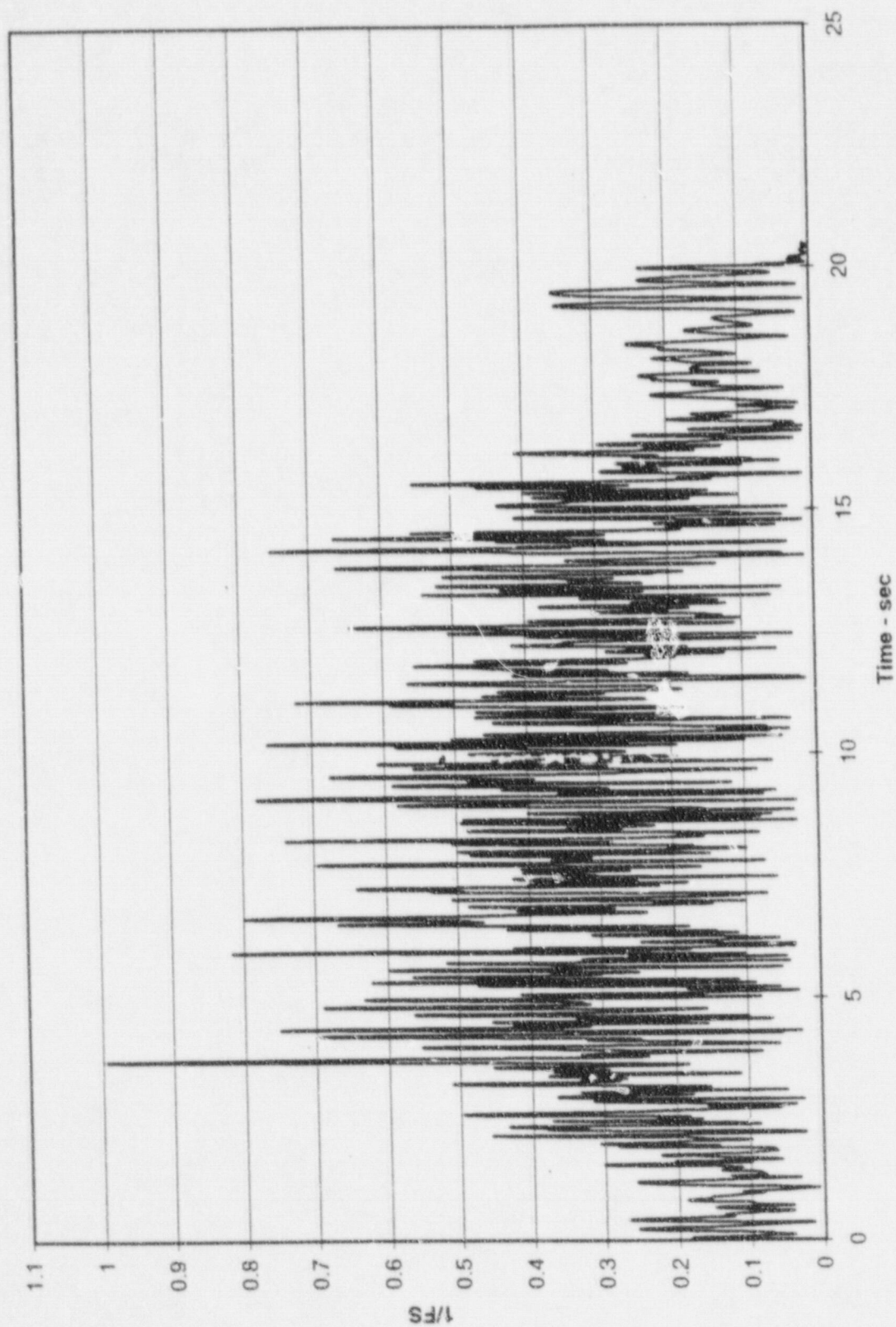
Figure 3-13. Node 233 - Axial Load



BY: HPA 6/12/97
CHK: ZJD 6/12/97

Unit 1

Figure 3-14. Node 233 - Sliding Factor of Safety

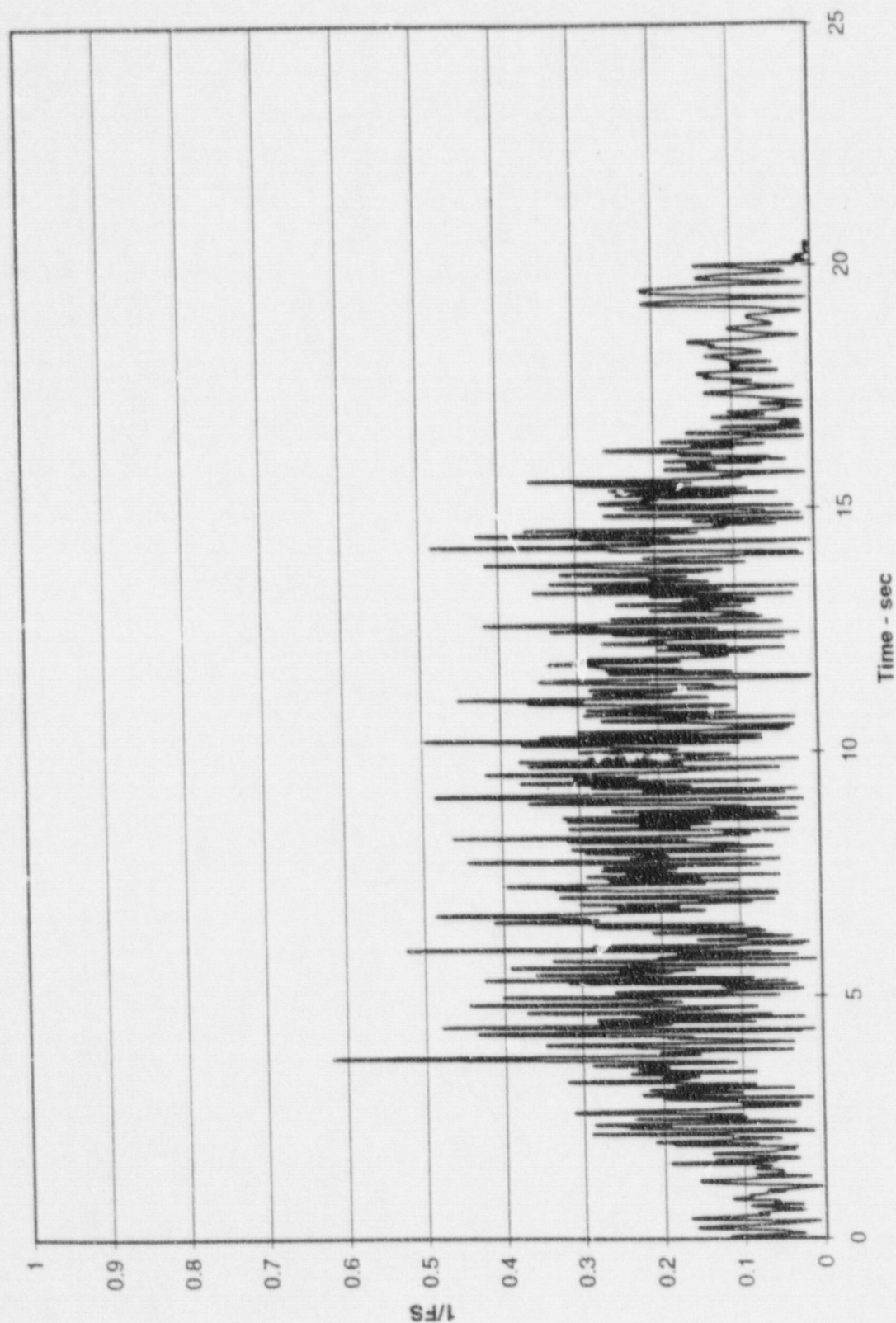


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CHK: DTD 6/12/97

P.26

Chart 1 (2)

Figure 3-15. Node 233 - Overturning Factor of Safety

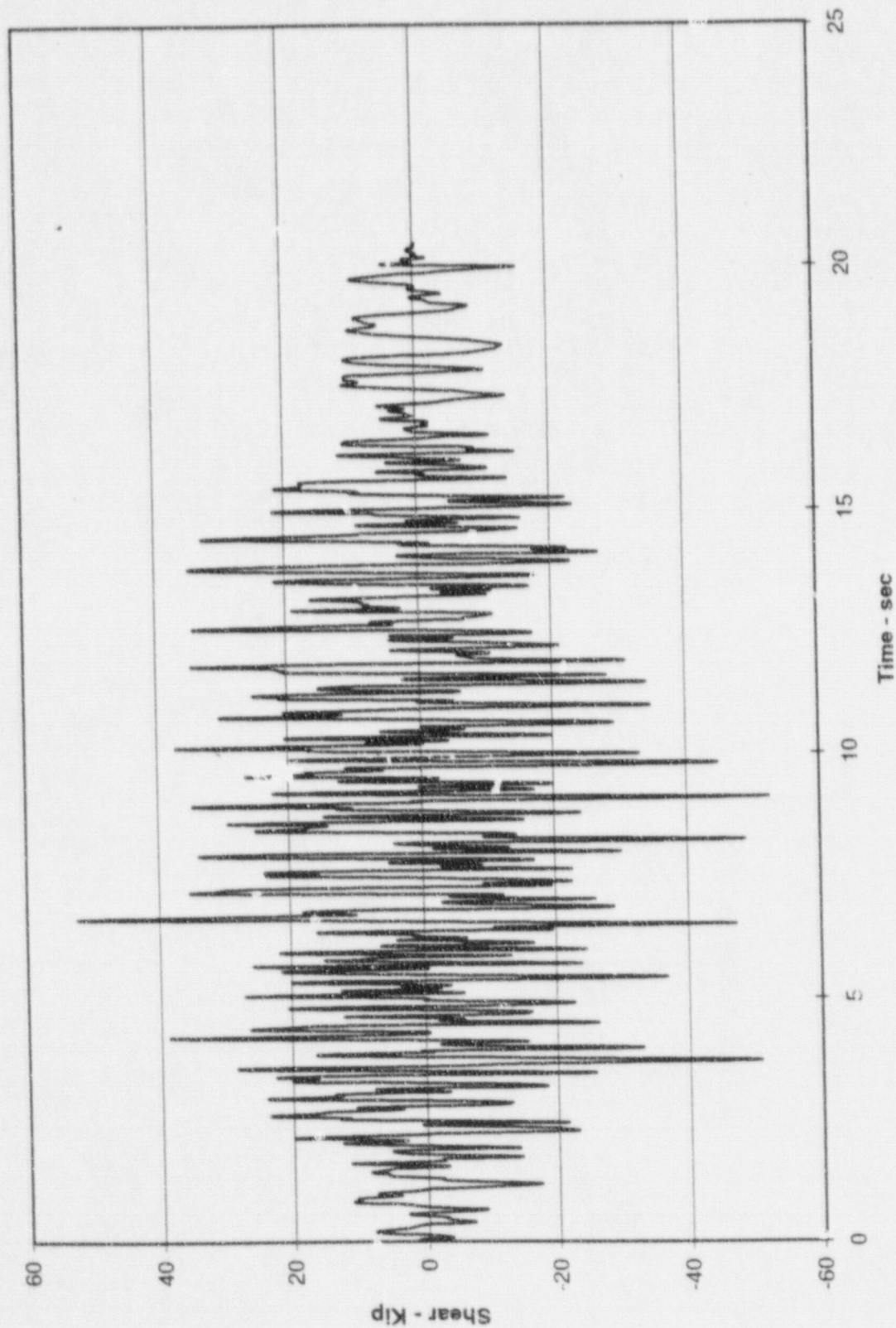


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BY: APA 6/12/97
CHK: DSD 6/12/97

P. 1

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Figure 3-16. Node 234 - Shear X Direction

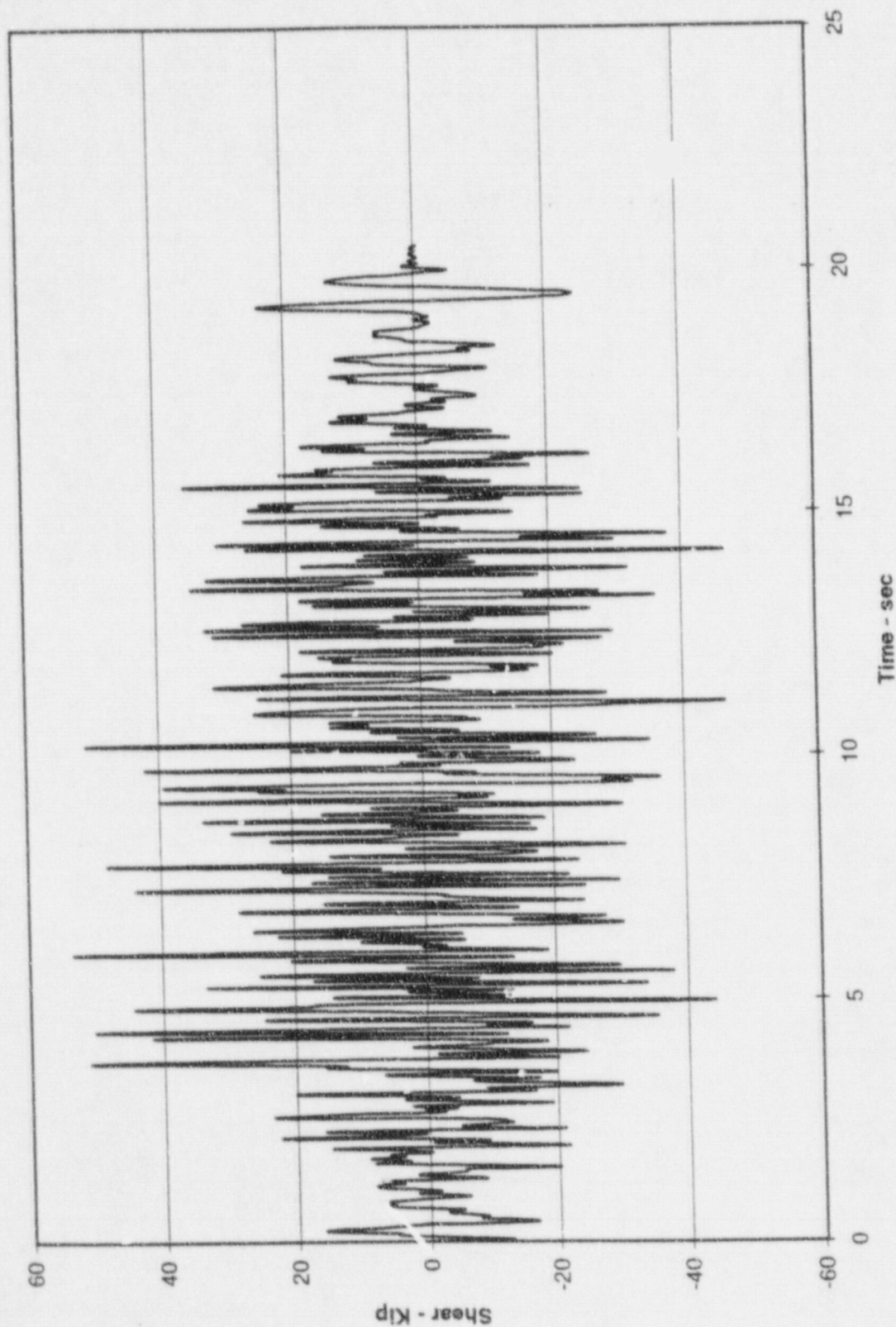


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BY: APA 6/12/97
CHK: DJD 6/12/97

P.20

Client1 (4)

Figure 3-17. Node 234 - Shear Y Direction

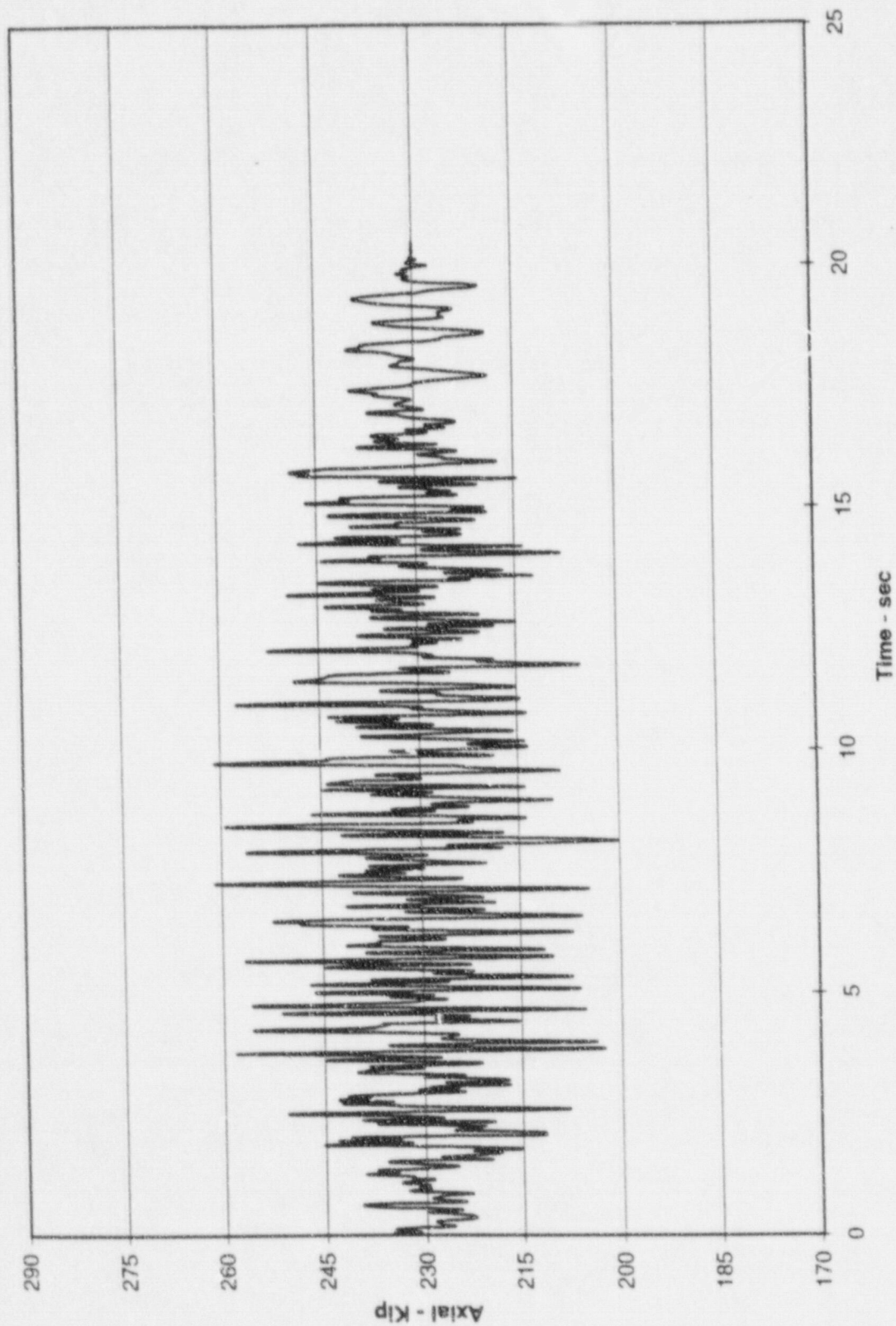


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P.24

Cross11 (5)

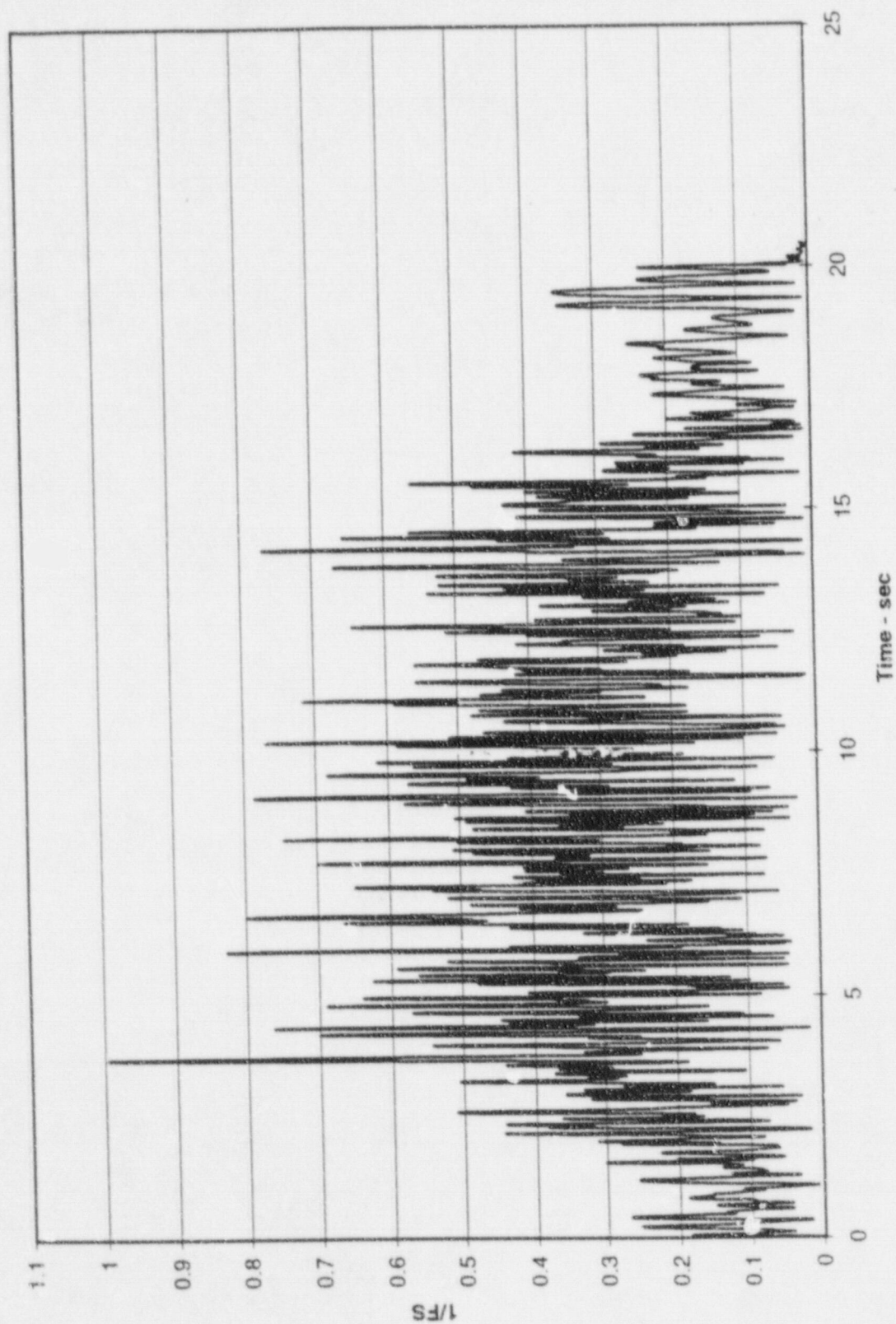
Figure 3-18. Node 234 - Axial Load



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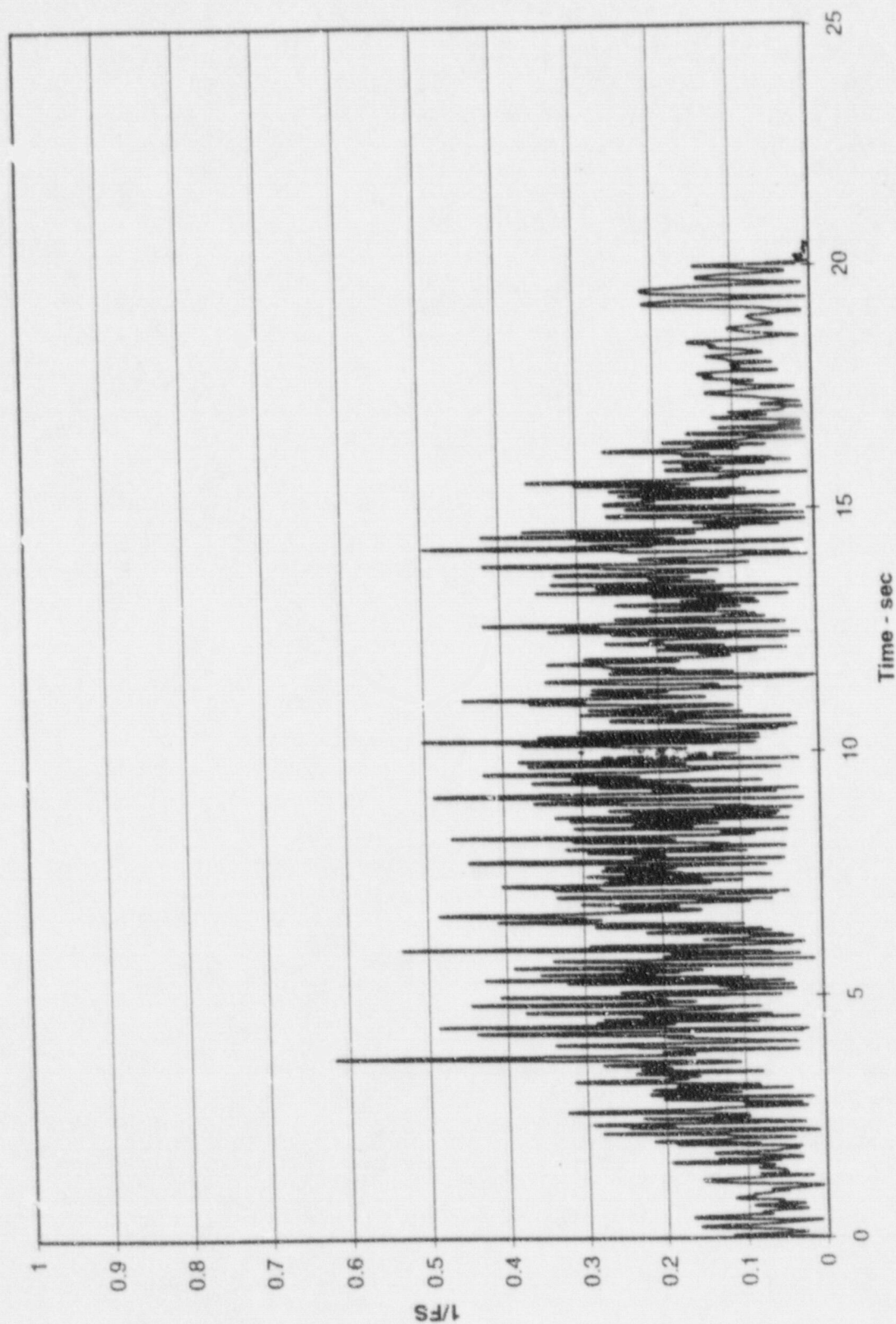
Figure 3-19. Node 234 - Sliding Factor of Safety



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BY: ADA 6/12/97
CHK: DTD 6/12/97

Channel (2)

Figure 3-20. Node 234- Overturning Factor of Safety

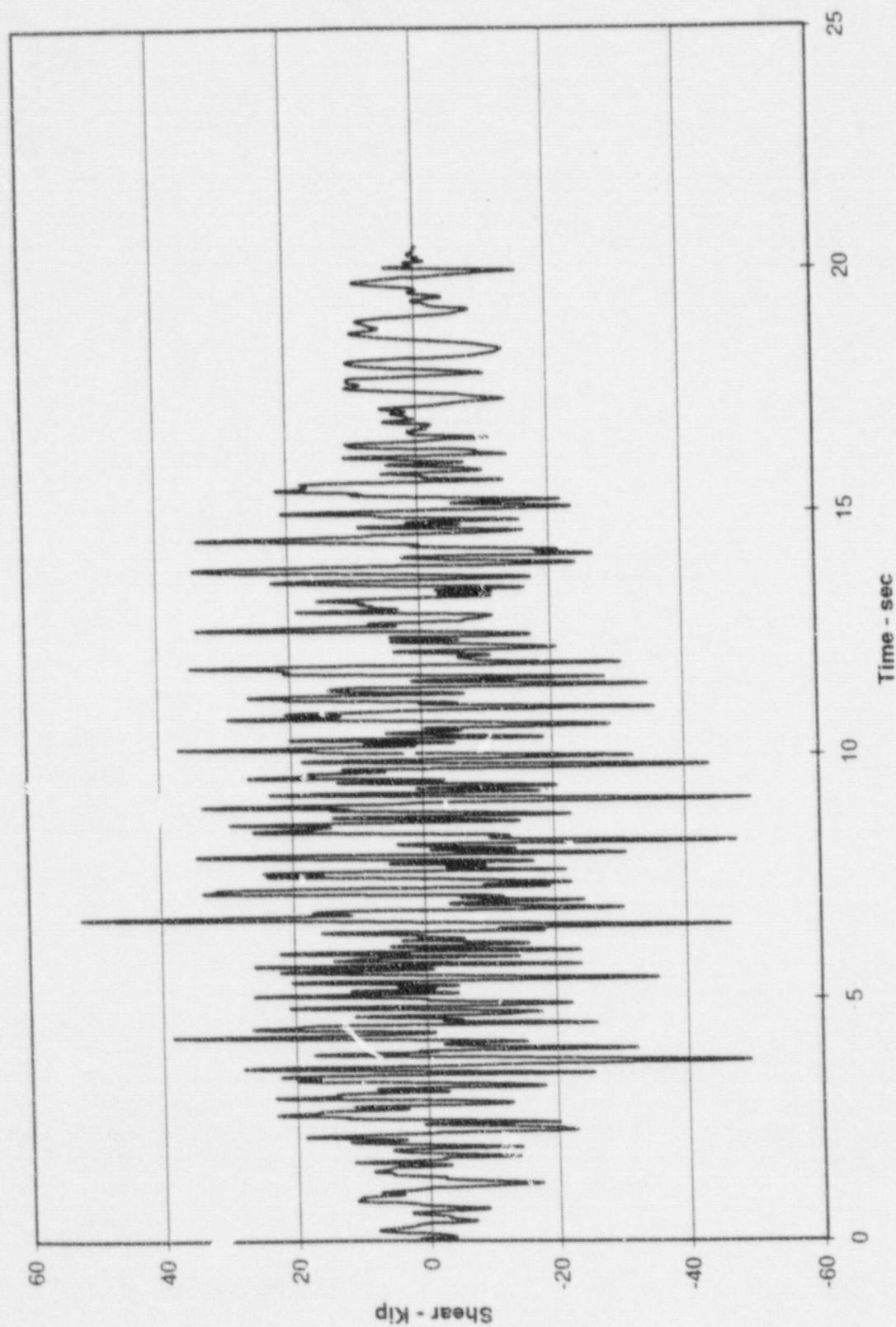


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BY: ABA 6/12/97
CHK: DTD 6/12/97

1.16

Channel (3)

Figure 3-21. Node 235 - Shear X Direction

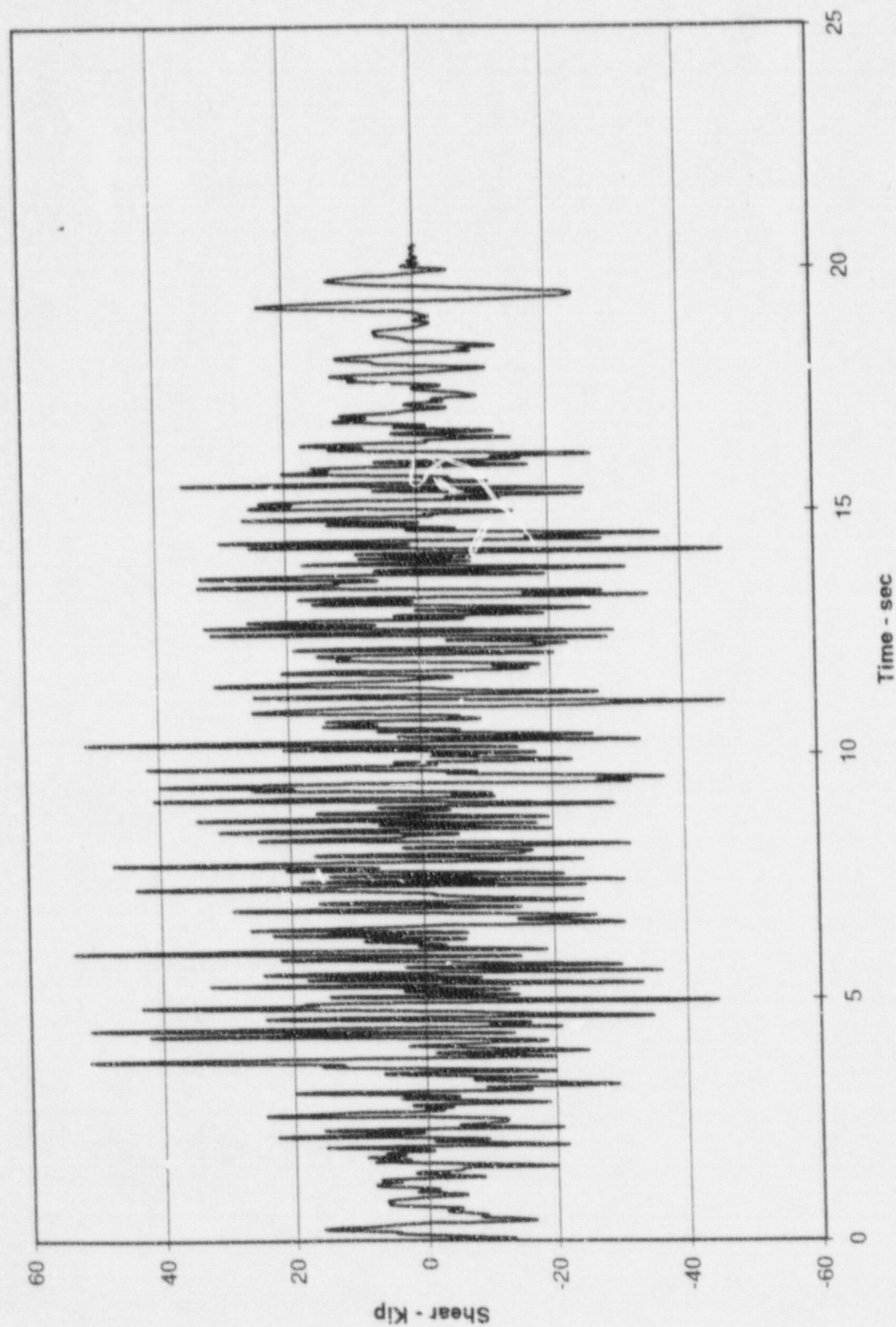


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CHK: ZJD 6/12/97

P.22

C. 1 (4)

Figure 3.2. Node 235 - Shear Y Direction



100031-C-04
BY: APA 6/12/97
CHK: DSD 6/12/97

1.27

100031-C-04
BY: APA 6/12/97
CHK: DJD 6/12/97

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C. .1 (5)

Figure 3-23. Node 235 - Axial Load

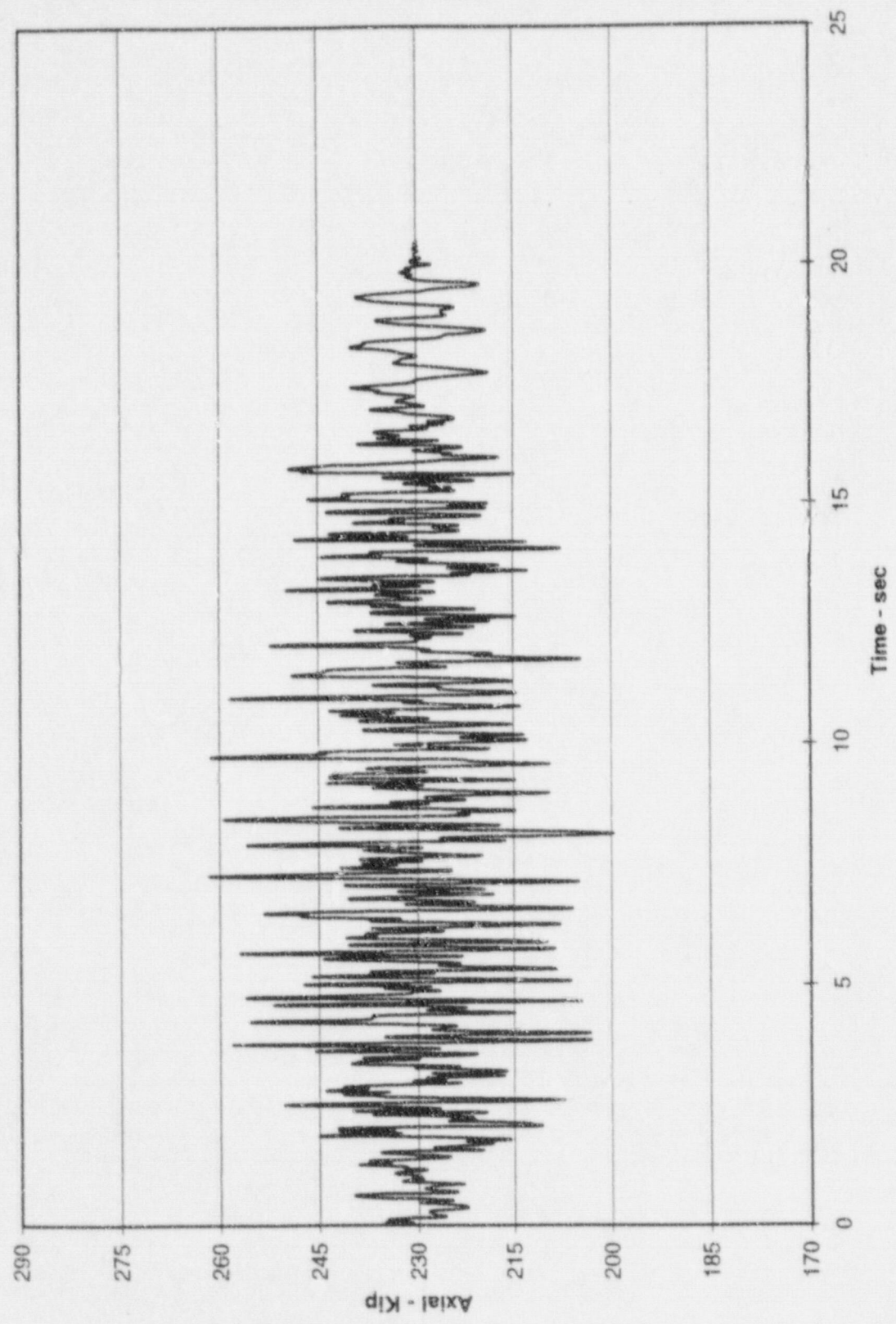
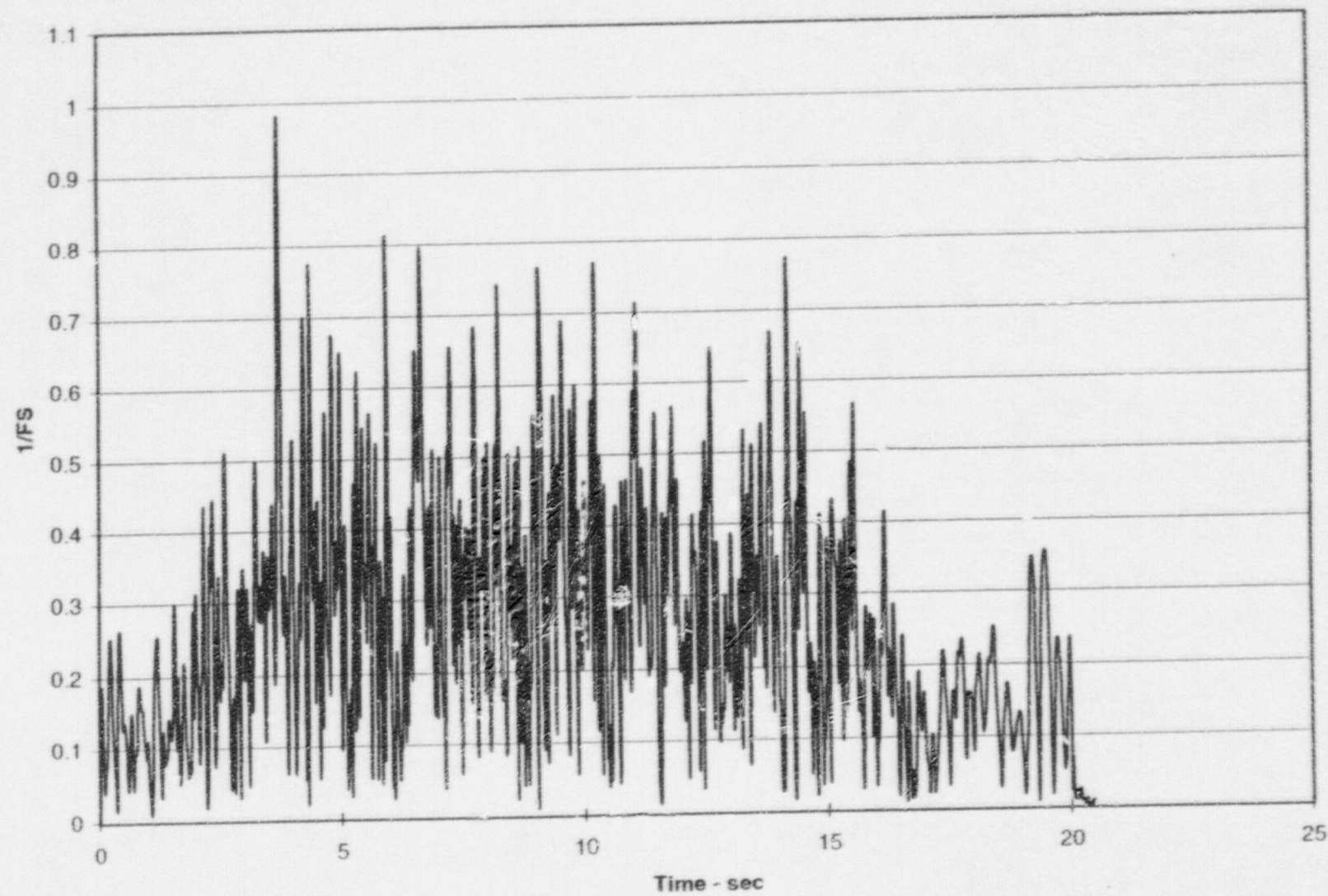
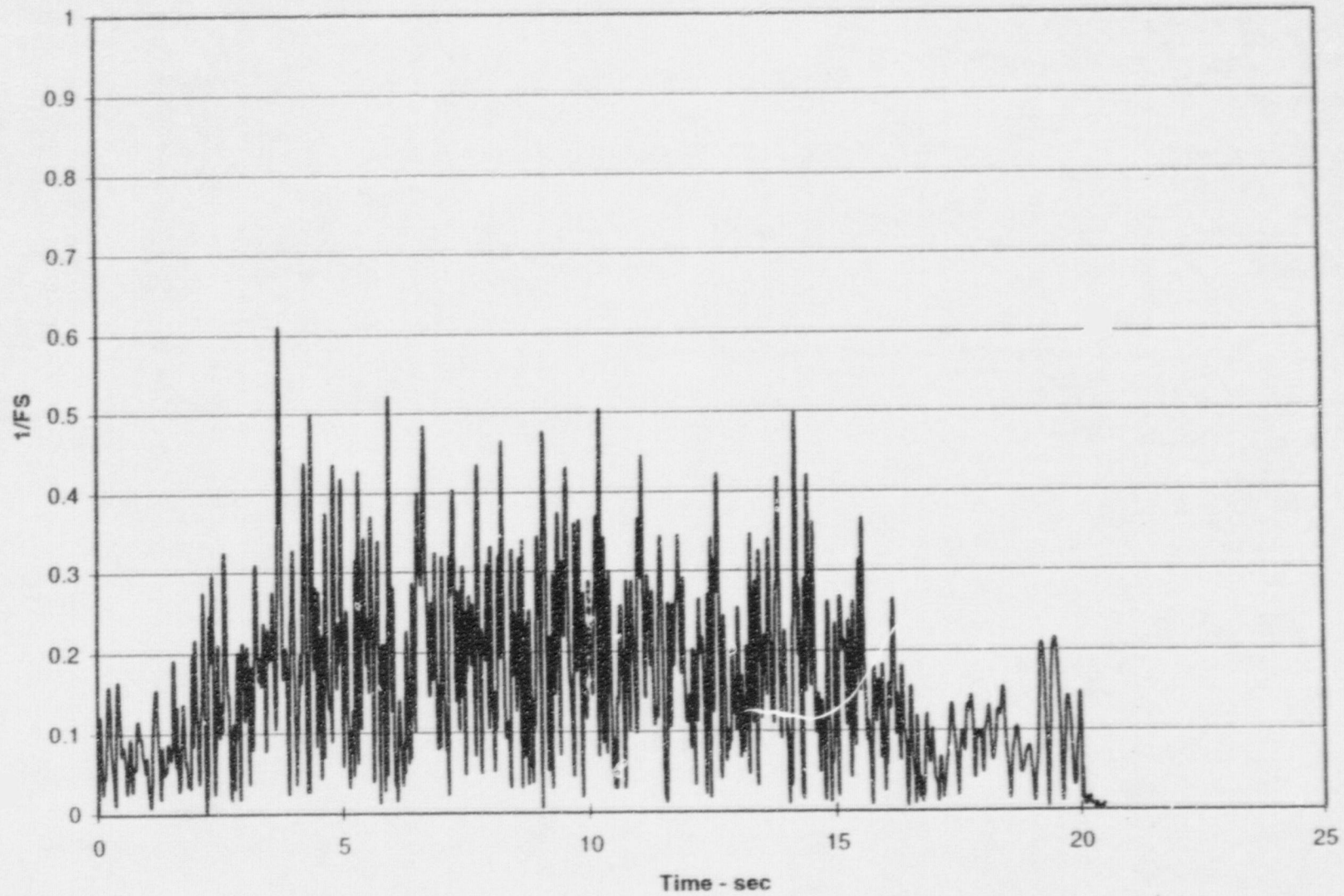


Figure 3-24. Node 235 - Sliding Factor of Safety



100021-C-D5
BY: ADA 6/12/97
CHK: PDD 6/12/97

Figure 3-25. Node 235 - Overturning Factor of Safety



100051-C-47
 BY: AFA 6/12/97
 CHK: DDD 6/12/97

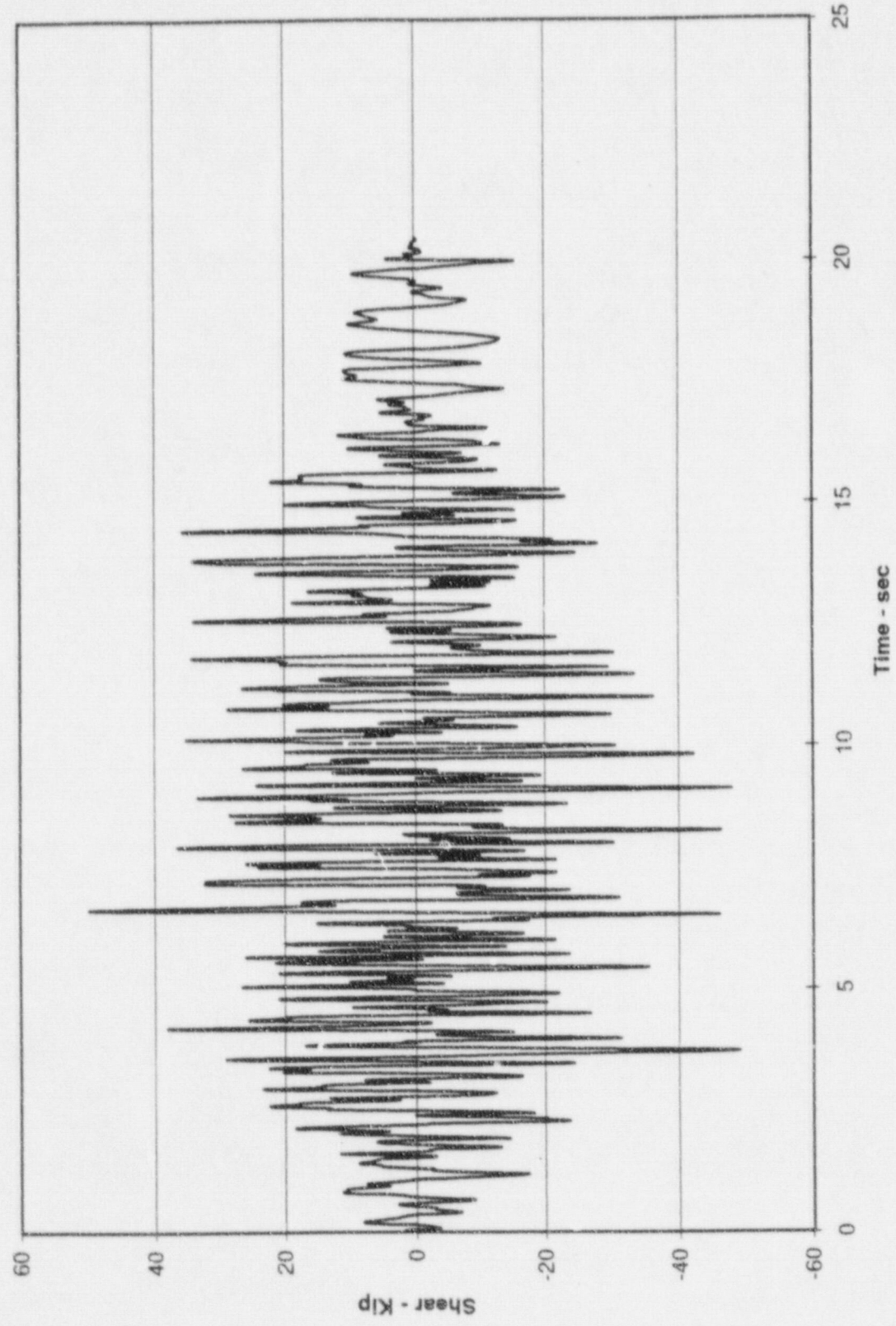
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100031-C-UT
BY: APA 6/12/97
CHK: DJD 6/12/97

P. 30

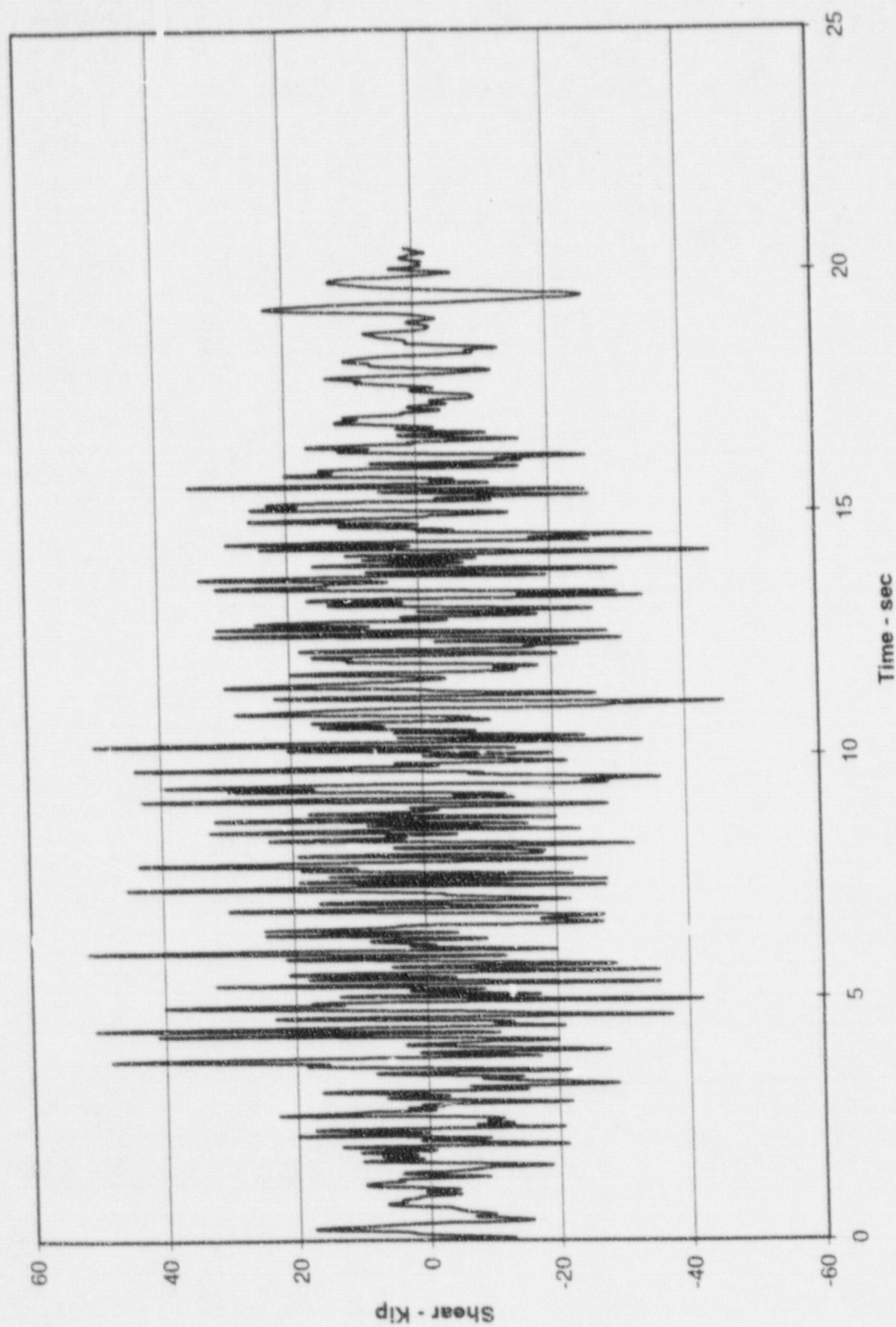
Clm...l (3)

Figure 3-26. Node 236 - Shear X Direction



C. 1 (4)

Figure 3-27. Node 236 - Shear Y Direction

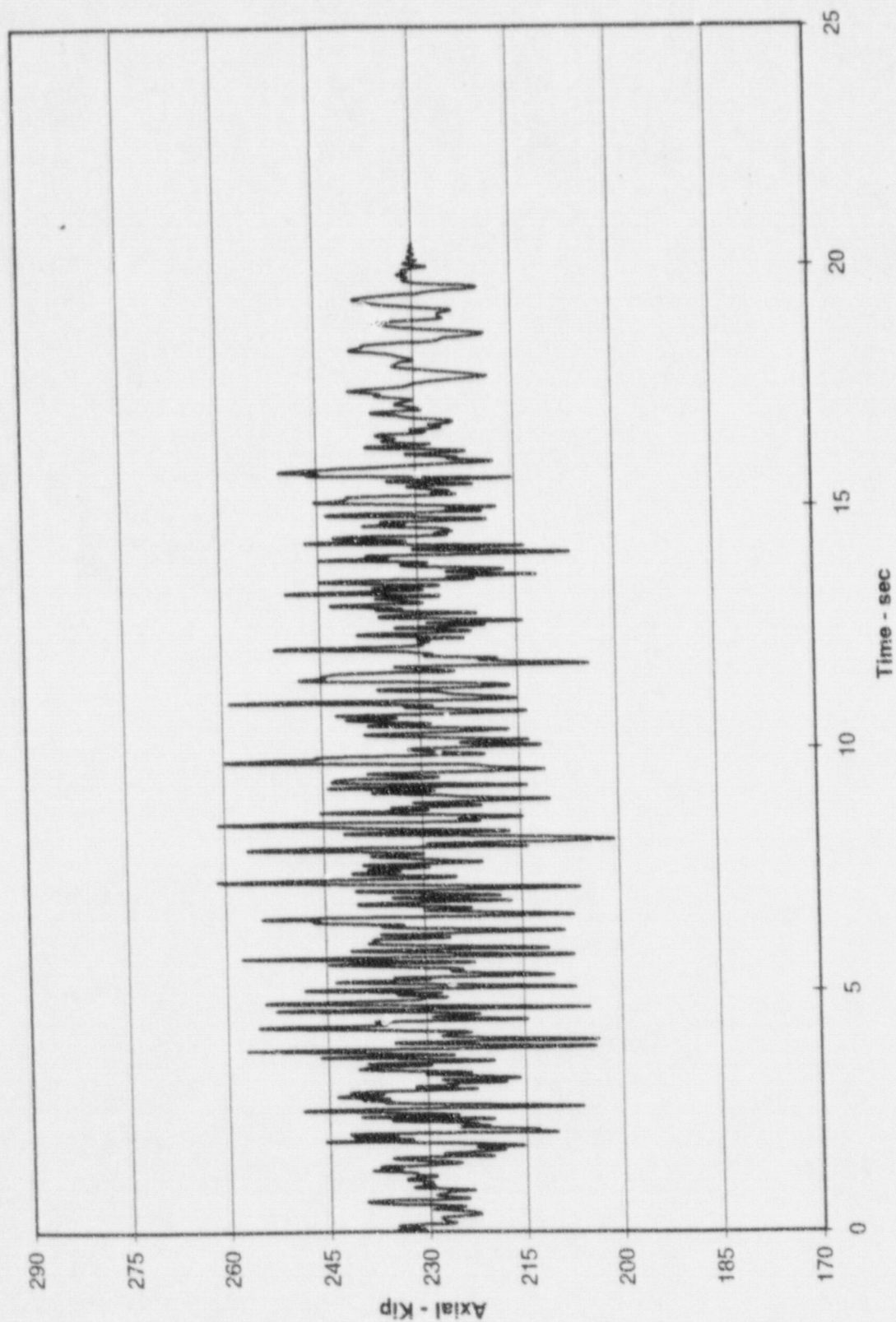


1000 SI-C-04
BY: APA 6/12/97
CHK: DJD 6/12/97

P. 31

C. 1 (5)

Figure 3-28. Node 236 - Axial Load



1000 51-C-04
BY: APA 6/12/97
CHK: DDD 6/12/97

P.40

1000 21-0-04
BY: APA 6/12/97
CHK: DTD 2/12/97

1.71

Figure 3-29. Node 236 - Sliding Factor of Safety

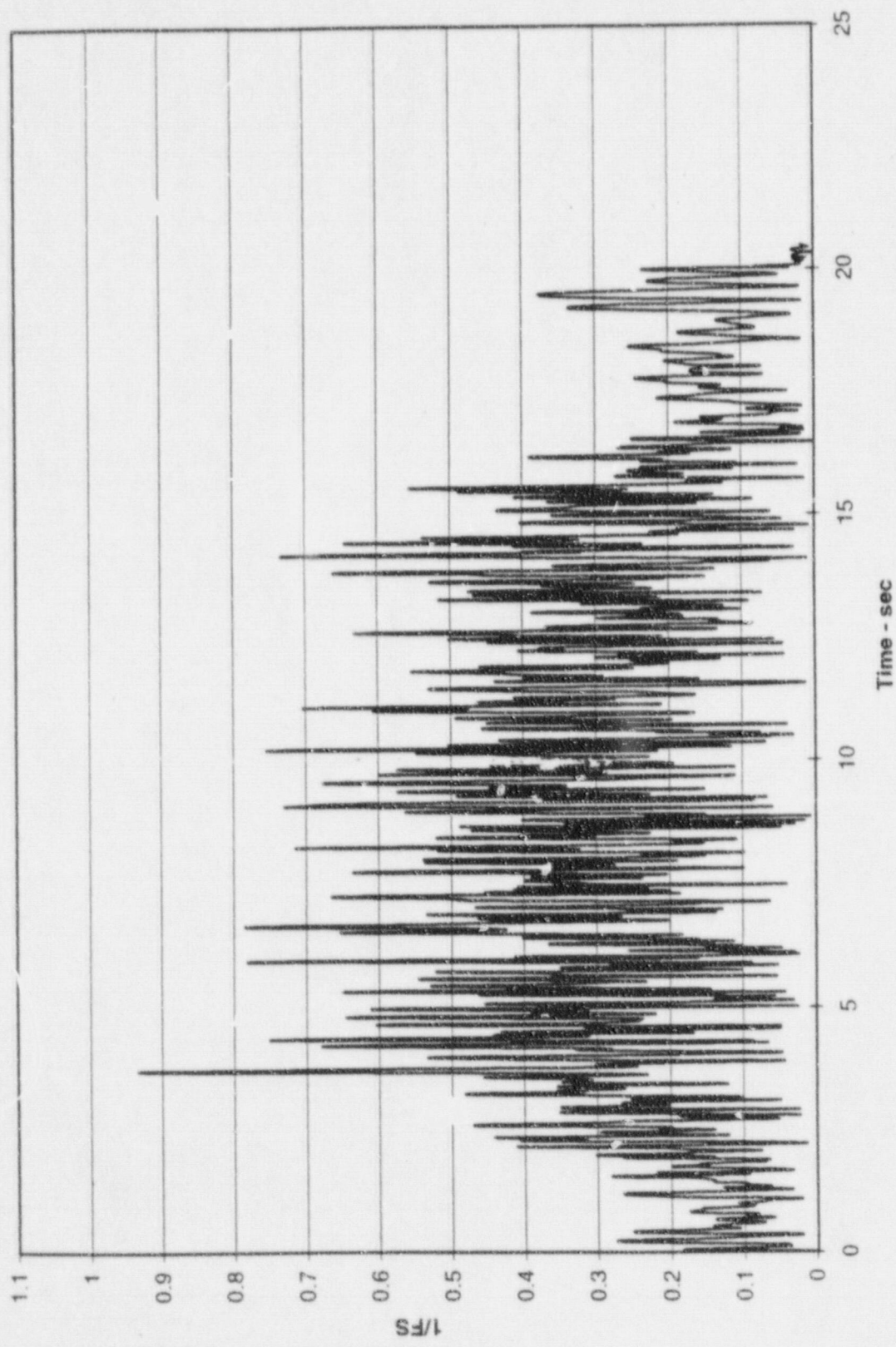
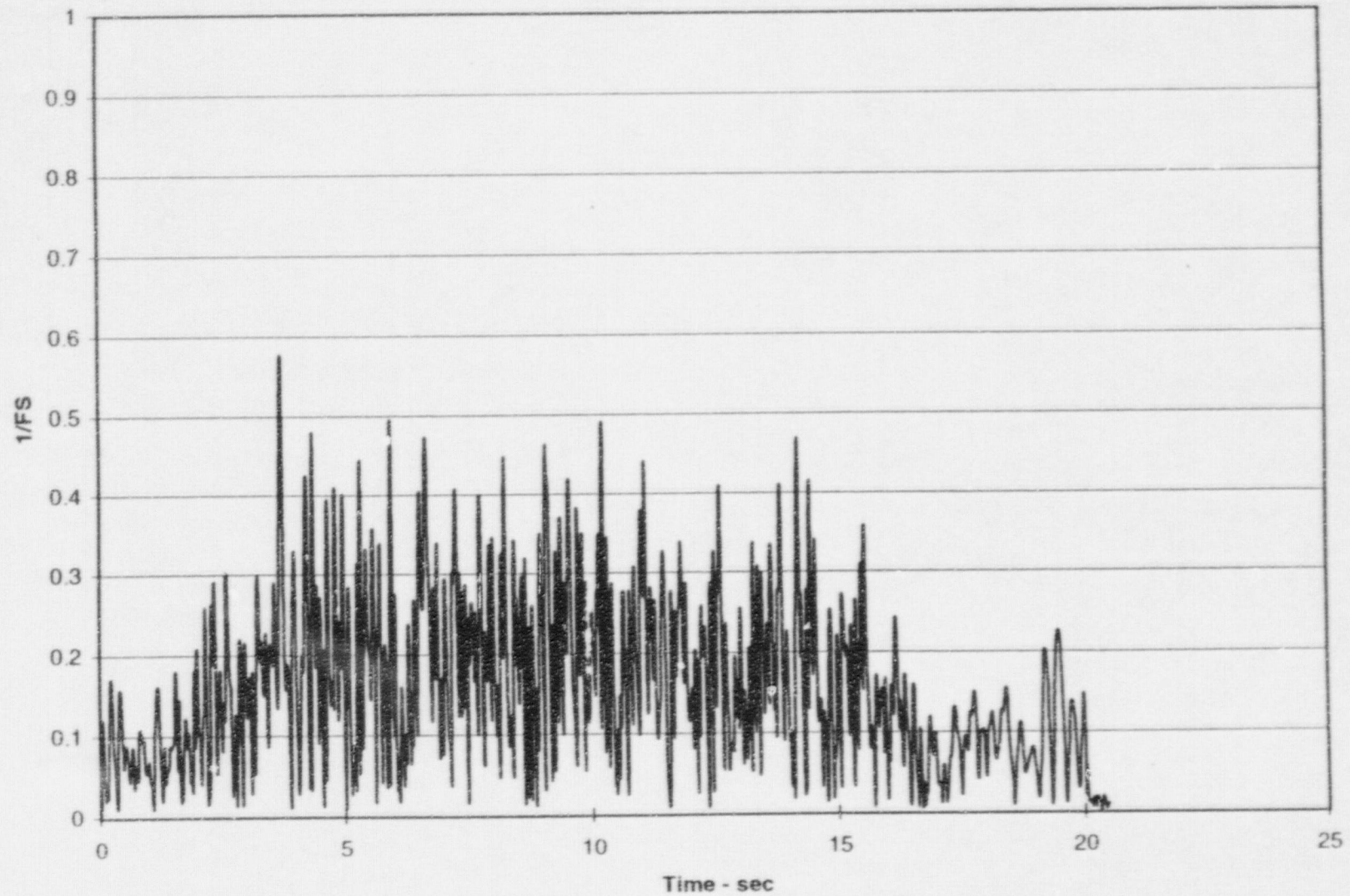


Figure 3-30. Node 236 - Overturning Factor of Safety



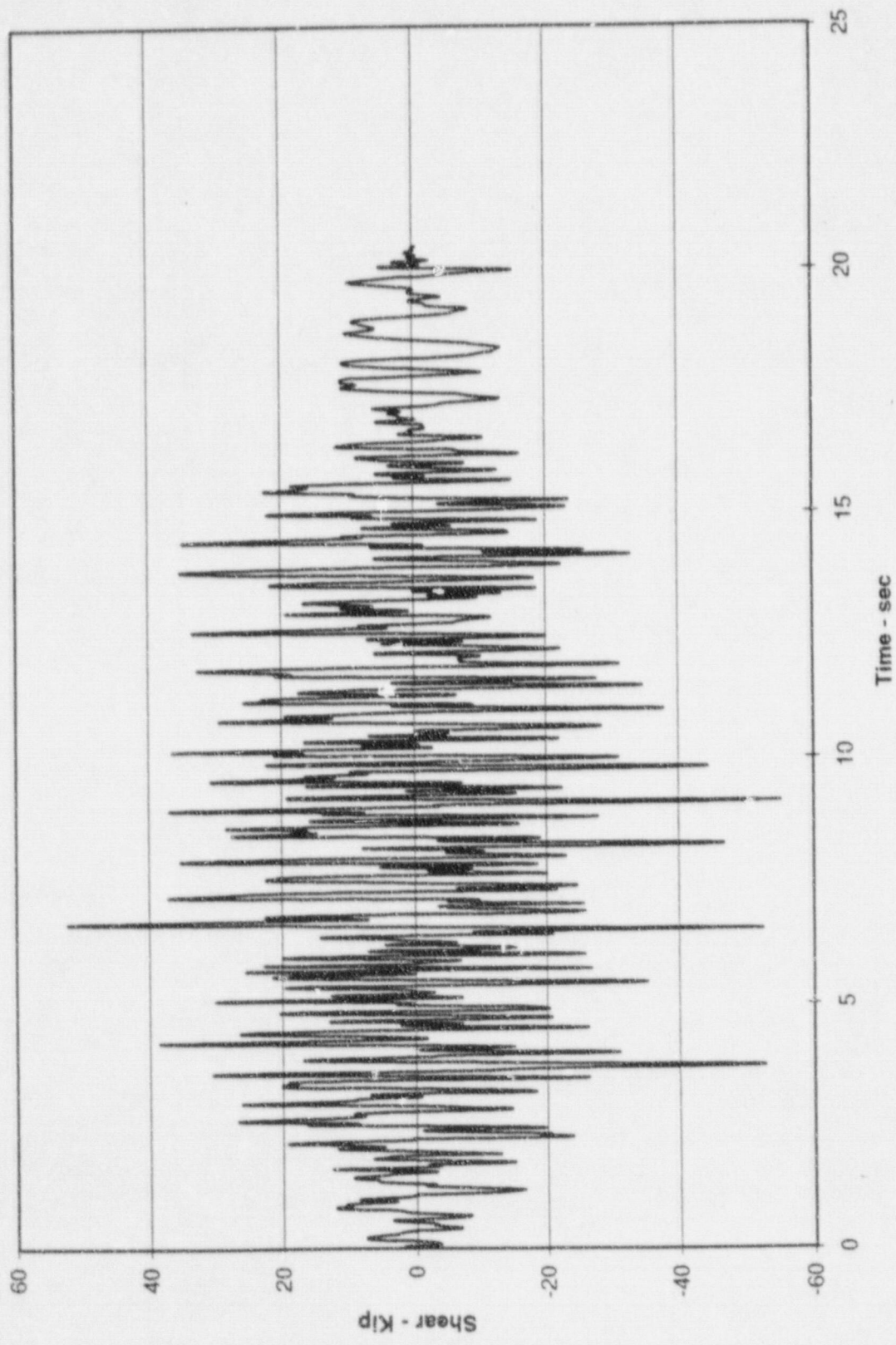
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BY: APA 6/12/97
CHK: DDD 6/12/97

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Chart 1 (3)

Figure 3-31. Node 237 - Shear X Direction

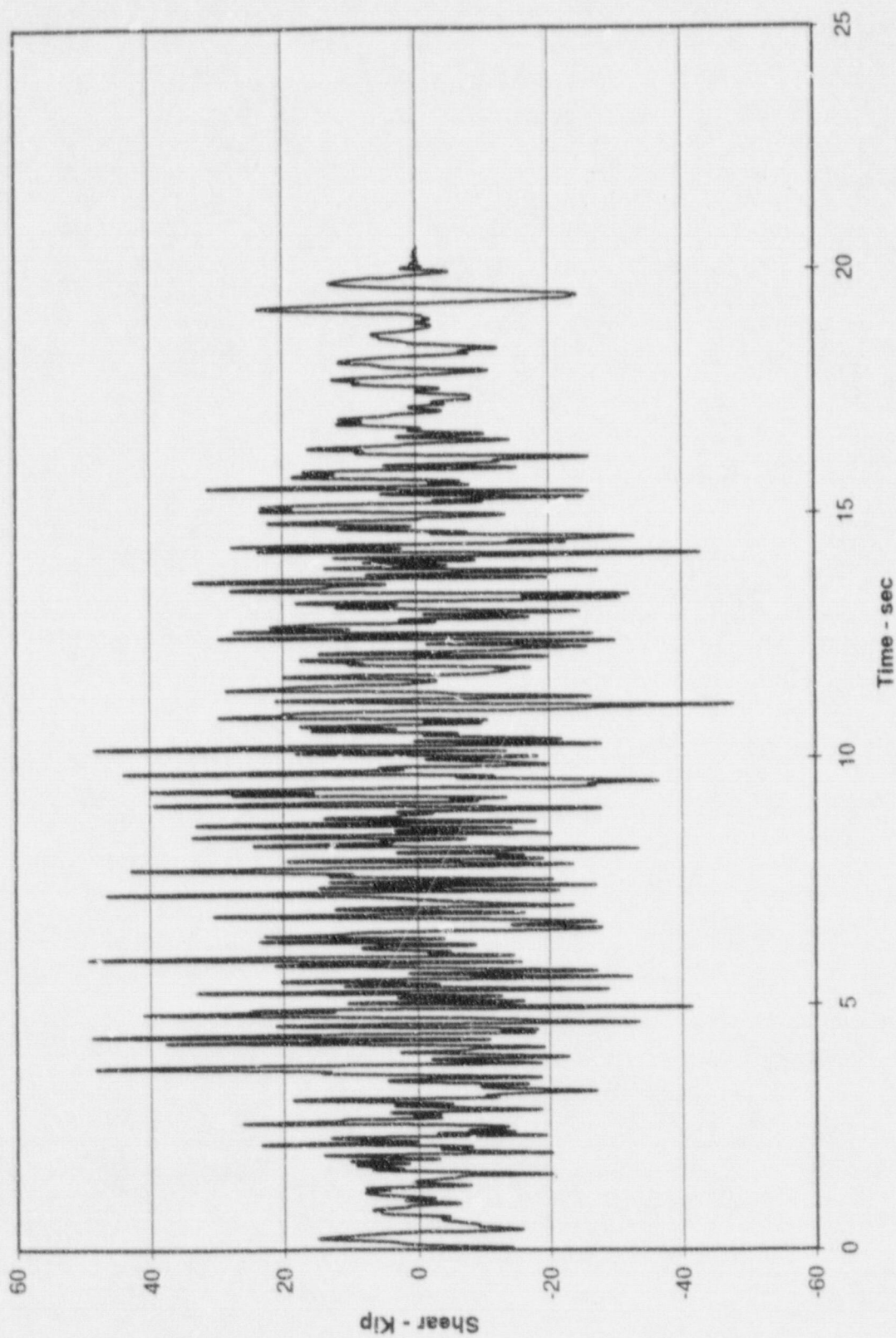


1000 51-L-UT
BY: APA 6/12/97
CHK: LTD 6/12/97

K.44

C. .1 (4)

Figure 3-32. Node 237 - Shear Y Direction



100051-C-04
BY: APA 6/12/97
CHK: DSD 6/12/97

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C...1 (5)

Figure 3-33. Node 237 - Axial Load

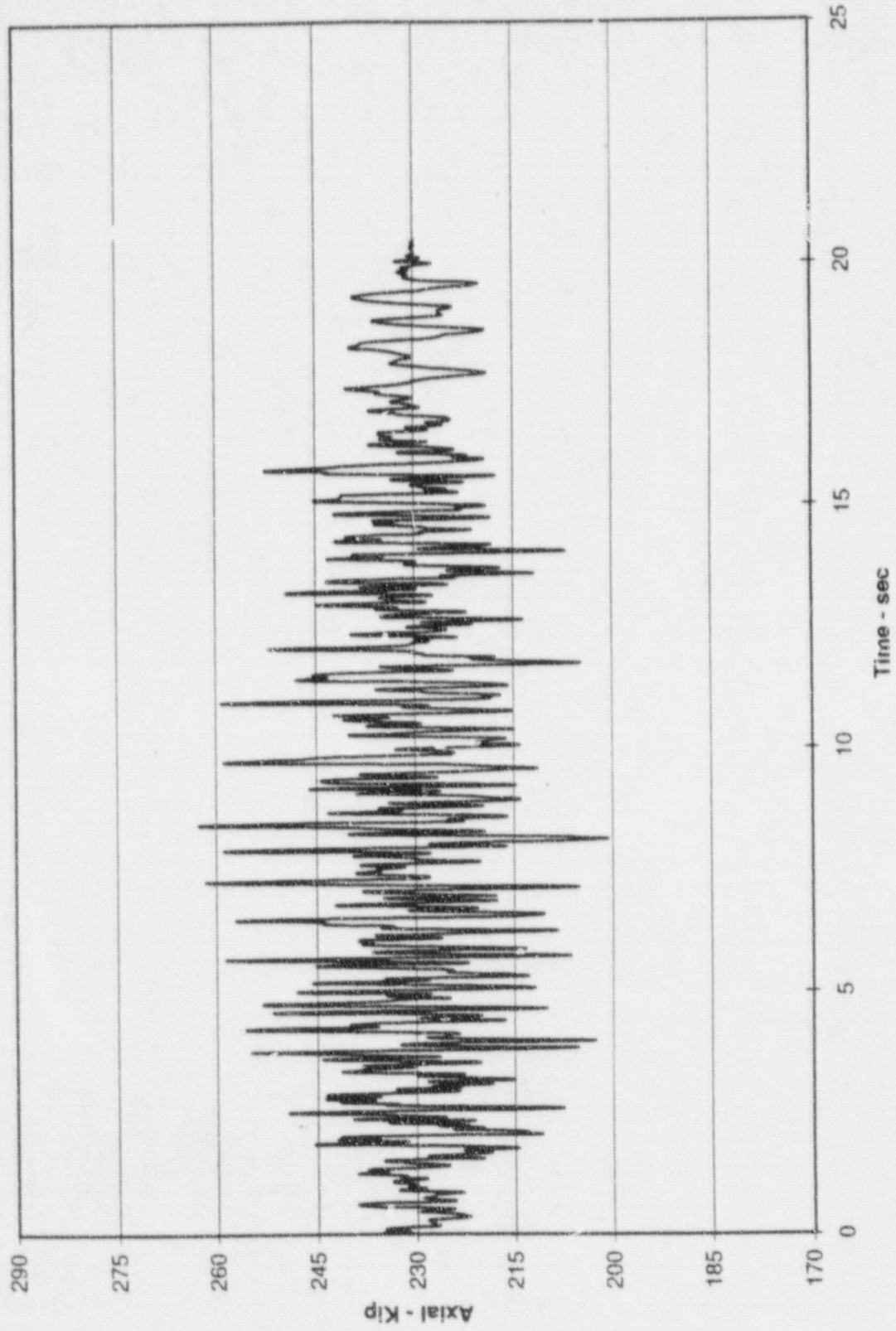
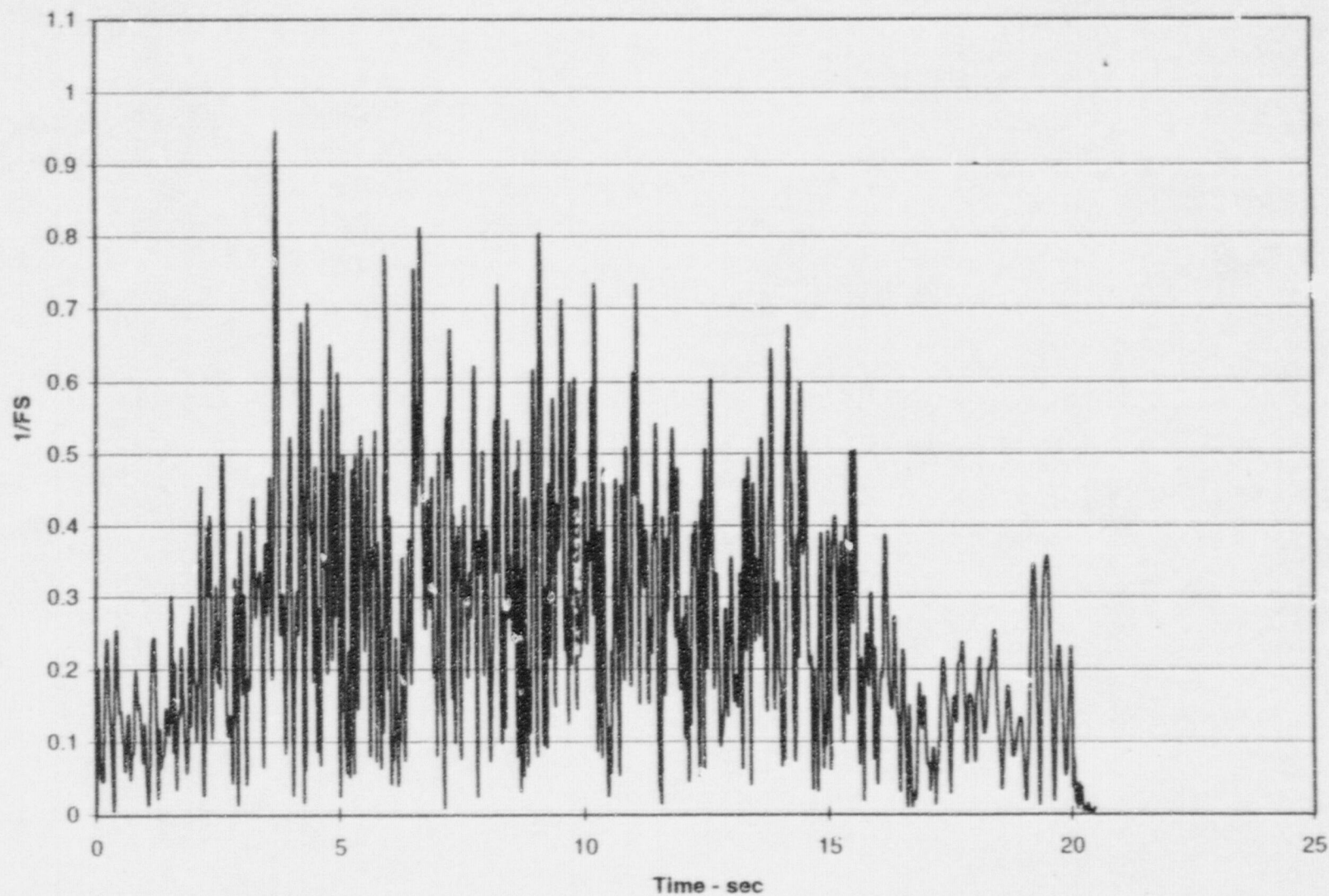


Figure 3-34. Node 237 - Sliding Factor of Safety

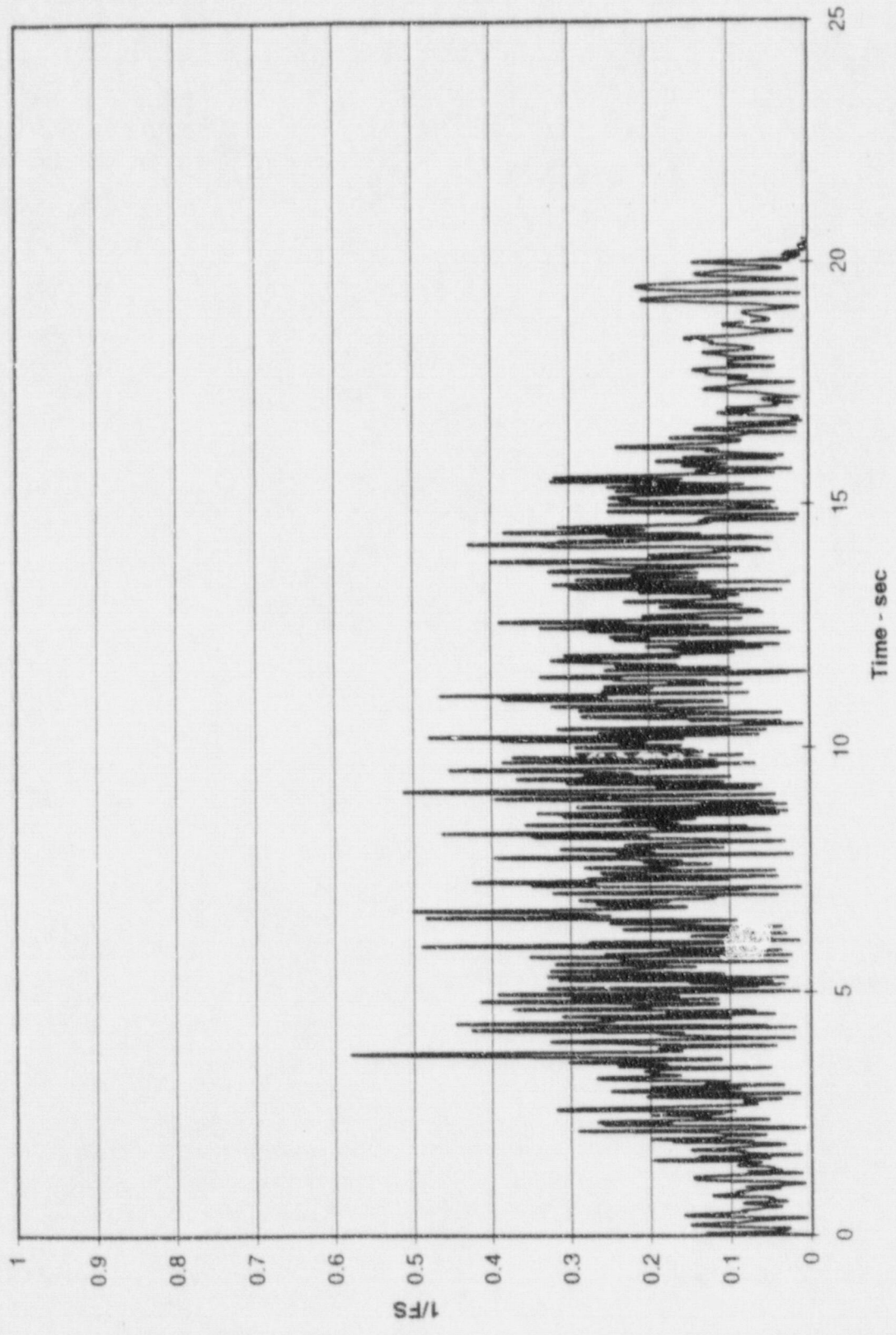


100051-C-UT
BY: ABA 6/12/97
CHK: JDD 6/12/97

1000 21-6-04
By: APA 6/12/07
CHK: DJD 6/12/07

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Figure 3-35. Node 237 - Overturning Factor of Safety





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CALC. NO. 100031C04R0 SUBJECT Sliding and Overturning Factor of Safety

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4.0 References

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2. EQE Calculation 100031-C-06 Rev 0, June 1997, Project Specific Verification of Computer Code SUPER SASSI/PC.
3. EQE Calculation 100031-C-03 Rev 0, June 1997, Pad Model and Input to Module HOUSE.
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5. ASCE Standard 4-86. Seismic Analysis of Safety-Related Nuclear Structures and Commentary on Standard for seismic Analysis of Safety-Related Nuclear Structures, September 1986.



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ATTACHMENT A

COMPUTER INPUT AND OUTPUT FILES

File Name	Description	Pages	Date
analysx	Input to ANALYS, x direction	1	5/09/97 15:13
analysx.out	Output of ANALYS, x direction	2	5/13/97 20:57
motionx	Input to MOTION, x direction	3	5/13/97 11:39
mxred.out	Output* of MOTION, x direction	7	6/06/97 10:10
analysy	Input to ANALYS, y direction	1	5/09/97 15:13
analysy.out	Output of ANALYS, y direction	2	5/13/97 23:59
motiony	Input to MOTION, y direction	3	5/13/97 10:55
myred.out	Output* of MOTION, y direction	7	6/06/97 10:01
analysz	Input to ANALYS, z direction	1	5/09/97 15:14
analysz.out	Output of ANALYS, z direction	2	5/14/97 03:15
motionz	Input to MOTION, z direction	3	5/13/97 10:56
mzred.out	Output* of MOTION, z direction	8	6/06/97 10:19

* Time histories have been deleted for printing purposes. The complete files (zipped) are in included diskettes.

TOTAL PAGES, INCLUDING COVER
SHEET

41 Sheets

Note: Signature at the top of this sheet signifies that all contained documents have been verified.

Variable	Mean	Standard Deviation	Minimum	Maximum
Age	35.5	10.5	25	45
Gender	1.5	0.5	1	2
Education	12.5	1.5	11	14
Income	35000	15000	20000	50000
Health	1.5	0.5	1	2
Marital Status	1.5	0.5	1	2
Occupation	1.5	0.5	1	2
Religion	1.5	0.5	1	2
Smoking	1.5	0.5	1	2
Drinking	1.5	0.5	1	2
Exercise	1.5	0.5	1	2
Stress	1.5	0.5	1	2
Sleep	1.5	0.5	1	2
Diet	1.5	0.5	1	2
Family Size	2.5	1.5	1	4
Home Ownership	1.5	0.5	1	2
Auto Ownership	1.5	0.5	1	2
Travel Frequency	1.5	0.5	1	2
Work Hours	40	10	30	50
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Life Satisfaction	1.5	0.5	1	2
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80.00	85.00	5.00
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NUMBER OF JOURNAL PRINTS	210
NUMBER OF AT-RISK GRADE PRINTS	195
NUMBER OF INTERMEDIATE PRINTS	195
NUMBER OF INTERMEDIATE PRINTS	0
NUMBER OF 5TH-8TH GRADE	2
ACCELERATION OF GRAVITY	32.2
2-CORRELATION OF 5TH GRADE	0.5
2-CORRELATION OF 5TH GRADE	0

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FILE: ANIMATION

Page: 5

0.011525-0.014059 0.06119 0.07465 0.034514 0.037281 0.035313 0.022313
0.039064-0.025961 0.023197 0.020374 0.017203 0.012286 0.028831 0.024771
0.000266 0.003956 0.007141 0.010959 0.015976 0.022285 0.028155 0.022256
0.014511 0.027717 0.044264 0.053917 0.061734 0.061769 0.051216 0.015959

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Page 13

194	0.0713	4.1740	0.0713	5.7403	0.0713	5.7403
213	0.0952	4.1403	0.0739	5.7403	0.0739	5.7403
228	0.0974	5.8403	0.0739	5.7403	0.0739	5.7403
233	0.0952	5.8403	0.0739	5.7403	0.0739	5.7403
238	0.0714	4.1403	0.0739	5.7403	0.0739	5.7403
223	0.0910	5.8403	0.0739	5.7403	0.0739	5.7403
228	0.0915	5.7403	0.0739	5.7403	0.0739	5.7403
233	0.0953	4.1403	0.0739	5.7403	0.0739	5.7403
233	0.0952	4.1403	0.0739	5.7403	0.0739	5.7403
233	0.0914	5.8403	0.0739	5.7403	0.0739	5.7403
234	0.0914	5.8403	0.0739	5.7403	0.0739	5.7403
235	0.0914	4.1403	0.0739	5.7403	0.0739	5.7403
236	0.0910	5.8403	0.0739	5.7403	0.0739	5.7403
237	0.0914	5.7403	0.0739	5.7403	0.0739	5.7403

BLANKS IN THE ABOVE TABLE ARE DUE TO WHERE OUTPUT WAS NOT REQUESTED

File: ANALYSIS.OUT

Page: 3

MAXIMUM NUMBER OF TERMS IN A BLOCK = 10000
 MAXIMUM NUMBER OF TERMS IN A BLOCK = 10000
 NUMBER OF ELEMENTS IN STRUCTURAL SYSTEM = 10000
 NUMBER OF ELEMENTS IN EXCAVATED SOIL SYSTEM = 10000

NUMBER OF BLOCKS IN STIFFNESS OF SOFT TIE = 1
 NUMBER OF BLOCKS IN STIFFNESS OF EXCAVATED SOIL = 1
 NUMBER OF BLOCKS IN K21 OF EXCAVATED SOIL = 1

MAXIMUM TIME SPACE USED IN K-FILE = 1000000

TABLET - 100001-C-04 North Area ISPSI Pad Analysis - Analyt 1

TABLE 1

100001-C-04 North Area ISPSI Pad Analysis - Analyt 1

FLEXIBILITY - IMPEDANCE DATA

ACCELERATION OF GRAVITY = 32.20
 MAX. NUMBER OF LAYER INTERFACE = 1
 RADIUS OF CENTRAL ELEMENT IN PILE = 1.0
 NUMBER OF D/F IN TRANS. DIRECTION = 44
 NUMBER OF ANALYSIS = 1

FREQUENCIES OF ANALYSIS

NUMBER OF FREQUENCIES = 15
 FREQUENCY STEP = 0.049

FREQUENCY NUMBER	FREQUENCY (HZ)	CIRCUIT FREQUENCY (RAD/SEC)	PERIOD (SEC)
2	0.9766E-01	0.6134E+00	0.1628E+02
10	0.4883E+00	0.3548E+01	0.2048E+01
20	0.9766E+00	0.6134E+01	0.1628E+01
40	0.2002E+01	0.1258E+02	0.8955E+00
60	0.2979E+01	0.1871E+02	0.5357E+00
80	0.4004E+01	0.2554E+02	0.2498E+00
100	0.4980E+01	0.3129E+02	0.2048E+00
120	0.6006E+01	0.3778E+02	0.1645E+00
140	0.6982E+01	0.4387E+02	0.1273E+00
160	0.8008E+01	0.5011E+02	0.1228E+00
180	0.9034E+01	0.5593E+02	0.1238E+00
200	0.9034E+01	0.5593E+02	0.1238E+00
220	0.9034E+01	0.5593E+02	0.1238E+00
240	0.9034E+01	0.5593E+02	0.1238E+00
260	0.9034E+01	0.5593E+02	0.1238E+00
280	0.9034E+01	0.5593E+02	0.1238E+00
300	0.9034E+01	0.5593E+02	0.1238E+00
320	0.9034E+01	0.5593E+02	0.1238E+00
340	0.9034E+01	0.5593E+02	0.1238E+00
360	0.9034E+01	0.5593E+02	0.1238E+00
380	0.9034E+01	0.5593E+02	0.1238E+00
400	0.9034E+01	0.5593E+02	0.1238E+00
420	0.9034E+01	0.5593E+02	0.1238E+00
440	0.9034E+01	0.5593E+02	0.1238E+00
460	0.9034E+01	0.5593E+02	0.1238E+00
480	0.9034E+01	0.5593E+02	0.1238E+00
500	0.9034E+01	0.5593E+02	0.1238E+00
520	0.9034E+01	0.5593E+02	0.1238E+00
540	0.9034E+01	0.5593E+02	0.1238E+00
560	0.9034E+01	0.5593E+02	0.1238E+00
580	0.9034E+01	0.5593E+02	0.1238E+00
600	0.9034E+01	0.5593E+02	0.1238E+00

TABLET - 100001-C-04 North Area ISPSI Pad Analysis - Analyt 1

COMPUTED FREQUENCIES

FREQUENCY NUMBER	FREQUENCY (HZ)	TIME
2	0.9766E-01	5.10
10	0.4883E+00	5.17
20	0.9766E+00	5.15
40	0.2002E+01	5.19
60	0.2979E+01	5.14
80	0.4004E+01	5.21
100	0.4980E+01	5.17
120	0.6006E+01	5.24
140	0.6982E+01	5.20
160	0.8008E+01	5.23
180	0.9034E+01	5.18

File: ANALYSIS.OUT

Page: 4

170	0.9034E+01	5.17
180	0.9034E+01	5.14
190	0.9034E+01	5.17
200	0.9034E+01	5.17
220	0.9034E+01	5.17
240	0.9034E+01	5.17
260	0.9034E+01	5.17
280	0.9034E+01	5.17
300	0.9034E+01	5.17
320	0.9034E+01	5.17
340	0.9034E+01	5.17
360	0.9034E+01	5.17
380	0.9034E+01	5.17
400	0.9034E+01	5.17
420	0.9034E+01	5.17
440	0.9034E+01	5.17
460	0.9034E+01	5.17
480	0.9034E+01	5.17
500	0.9034E+01	5.17
520	0.9034E+01	5.17
540	0.9034E+01	5.17
560	0.9034E+01	5.17
580	0.9034E+01	5.17
600	0.9034E+01	5.17

TABLET - 100001-C-04 North Area ISPSI Pad Analysis - Analyt 1

OVERALL TIME LOG

INPUT DATA FROM CAPS AND TAPES	0.15
FORM (F.W.M.) FOR K21	0.00
FORM FLEXIBILITY MATRIX	48.66
FORM IMPEDANCE MATRIX	46.78
FORM (F.W.M.) FOR EXCAVATED SOIL	0.00
FORM (F.W.M.) FOR STRUCTURE	18.78
FORM (F.W.M.) IMPEDANCE MATRIX AND PEOPLE	40.83
FORM FREE FIELD MOTION	0.00
FORM IMPEDANCE MATRIX (F.W.M.) LOAD VECTOR	14.77
FORM FOR TRANSFER FUNCTIONS	11.46
FORM FINAL TRANSFER FUNCTION TAPES	0.04
PRINT ALL TRANSFER FUNCTIONS	0.00
TOTAL SOLUTION TIME	192.78

TABLET - 100001-C-04 North Area ISPSI Pad Analysis - Analyt 1

OUTPUT TAPE INFORMATION

LOGICAL TAPE WRITTEN	TAPE 5
TOTAL NO. OF WORDS	42585481
TOTAL NO. OF RECORDS	75
TOTAL NO. OF SECTORS	102278
LOGICAL TAPE WRITTEN	TAPE 6
TOTAL NO. OF WORDS	182372
TOTAL NO. OF RECORDS	1297
TOTAL NO. OF SECTORS	357

FILE: A:\NOTION

Page: 5

0.034869 0.043660 0.046929 0.04740 0.053226 0.053248 0.053815
0.051821 0.050471 0.048424 0.04560 0.036928 0.031979 0.027433
0.023299 0.019421 0.015202 0.0110 0.00584 0.00012 0.002985 0.005806
-0.008467 0.011598 0.015352 0.0190 0.011182 0.011956 0.005643

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See 171100 - 1970010 - 24 North Avenue 19711 East Avenue 1971100

ACCELERATION MEASUREMENTS AT 10000 RPM 119

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Following time history is saved in Table 12

ALL INFORMATION CONTAINED HEREIN IS UNCLASSIFIED
DATE 08-20-2008 BY 60322 UCBAW

LOCATION - 100311-C-04 North Anna 15511 Pad Area, 900 - West end of

FOLLOWING TIME HISTORY IS SAVED ON TAPE 12

95. OF POLYESTERS - 20.48

Labelled - 100031-C-04 North Avenue 1500 Paul Annelysse Apartment 4

1. The first step is to identify the key components of the system. This involves understanding the inputs, outputs, and internal processes. For example, in a manufacturing system, the inputs might be raw materials and labor, the outputs might be finished products, and the internal processes might involve assembly and quality control.

NO. OF POINTS = 2000

.....

Author	Year	Country	Sample Size	Study Design	Findings
Alm and Nilsson	1995	Sweden	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Bjork et al.	1998	Sweden	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Chen et al.	2000	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2001	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2002	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2003	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2004	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2005	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2006	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2007	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2008	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2009	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2010	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2011	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2012	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2013	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2014	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2015	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2016	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2017	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2018	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2019	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2020	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2021	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2022	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2023	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2024	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics
Costa et al.	2025	USA	1,000	Longitudinal	Increased risk of alcoholism in children of alcoholics

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Page: 5

FILE: A:\Z\MOTIONZ

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0.002861 0.003686 0.005425 0.007736 0.008224 0.009112 0.008412 0.007516
0.004533 0.003267 0.003434 0.004863 0.005417 0.007111 0.005462 0.005577
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FOLLOWING TIME LIST IS BASED ON TABLE:
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 (F 0.10% = 1.0)

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FOLLOWING TIME HISTORY IS SAVED TO FILE 1:

ACCEPTED FOR PUBLICATION IN THE JOURNAL OF THE ROYAL SOCIETY OF MEDICINE

DOI: 10.1093/rsm/107.1.118

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0-7980-30 0 302606 0 00000 0 00000 0 00000 0 00000 0 00000
0-7130 - 00033 - C-4 North Area 1651 Ford Ave., s/w - Motion 2

0 000042-0 000054-0 000342-0 000342-0 000009-0 000011-0 000152-0
K11100 - 105031-C-54 North Anna (SPS) Rad Area, site - Mod 1,000 2

-0.009001 0.682794 0.00186 1.000199 0.000063 0.000153 -3.000128 -0.000355
with 0 - 195631 C-04 North Anna 1951 Rad Analys; sig = Not too z

-0.604256 ± 0.059110; $\chi^2/df = 1.3715$; $\rho = 0.3719$; $\rho = 0.16764$; $\rho = 0.14574$; $\rho = 0.12687$; $\rho = 0.12672$
 8-11:00 - 10:00:11; 24 North Anna 1895; Feb 2004; 5018 - Modico 2

0.00315-0.00082; $\phi = 22.14^\circ$; $\phi_{\text{crit}} = 45.2243$; $\phi_{\text{max}} = 0.00116$; $\phi_{\text{min}} = 0.00249$.
 0.1110 - 11.0011; $\phi = 0.4$ North Area 13951 Red Road, g14 - Mod 100 E

0.00018-0.00020, 0.00716-0.00723, 0.00026-0.00043, 0.00042-0.00044
SECTION: 100031-C-01 North Anna 1951 Pad Analysis - Moisture

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A. C. LEVANT AND R. J. W. WILSON • 223

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 01991 00 02051 00 02111 00 02171 00 02231 00 02291 00 02351 00
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 02831 00 02891 00 02951 00 03011 00 03071 00 03131 00 03191 00
 03251 00 03311 00 03371 00 03431 00 03491 00 03551 00 03611 00
 03671 00 03731 00 03791 00 03851 00 03911 00 03971 00 04031 00
 04091 00 04151 00 04211 00 04271 00 04331 00 04391 00 04451 00
 04511 00 04571 00 04631 00 04691 00 04751 00 04811 00 04871 00
 04931 00 04991 00 05051 00 05111 00 05171 00 05231 00 05291 00
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 05771 00 05831 00 05891 00 05951 00 06011 00 06071 00 06131 00
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 15851 00 15911 00 15971 00 16031 00 16091 00 16151 00 16211 00
 16271 00 16331 00 16391 00 16451 00 16511 00 16571 00 16631 00
 16691 00 16751 00 16811 00 16871 00 16931 00 16991 00 17051 00
 17111 00 17171 00 17231 00 17291 00 17351 00 17411 00 17471 00
 17531 00 17591 00 17651 00 17711 00 17771 00 17831 00 17891 00
 17951 00 18011 00 18071 00 18131 00 18191 00 18251 00 18311 00
 18371 00 18431 00 18491 00 18551 00 18611 00 18671 00 18731 00
 18791 00 18851 00 18911 00 18971 00 19031 00 19091 00 19151 00
 19211 00 19271 00 19331 00 19391 00 19451 00 19511 00 19571 00
 19631 00 19691 00 19751 00 19811 00 19871 00 19931 00 19991 00
 20051 00 20111 00 20171 00 20231 00 20291 00 20351 00 20411 00
 20471 00 20531 00 20591 00 20651 00 20711 00 20771 00 20831 00
 20891 00 20951 00 21011 00 21071 00 21131 00 21191 00 21251 00
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 21731 00 21791 00 21851 00 21911 00 21971 00 22031 00 22091 00
 22151 00 22211 00 22271 00 22331 00 22391 00 22451 00 22511 00
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 22991 00 23051 00 23111 00 23171 00 23231 00 23291 00 23351 00
 23411 00 23471 00 23531 00 23591 00 23651 00 23711 00 23771 00
 23831 00 23891 00 23951 00 24011 00 24071 00 24131 00 24191 00
 24251 00 24311 00 24371 00 24431 00 24491 00 24551 00 24611 00
 24671 00 24731 00 24791 00 24851 00 24911 00 24971 00 25031 00
 25091 00 25151 00 25211 00 25271 00 25331 00 25391 00 25451 00
 25511 00 25571 00 25631 00 25691 00 25751 00 25811 00 25871 00
 25931 00 25991 00 26051 00 26111 00 26171 00 26231 00 26291 00
 26351 00 26411 00 26471 00 26531 00 26591 00 26651 00 26711 00
 26771 00 26831 00 26891 00 26951 00 27011 00 27071 00 27131 00
 27

```

C      000064-0.00049-0.00033-0.00024-0.00023-0.00017-0.00010-0.00008
TIME = 100033 - C North Anna SFPS Pad Analysis - Motion 2
FILLING TIME MUST BE SAVED ON TAPE 2

```

```

C 00022 0 003058 0 000056 0 000000 0 000018 0.000004 0.000141 0.000174
INTEGRAL = 1.00031 C-04 North Anna 1SP3; Pad Analysis - Motion =
FALLING TIME MUST-YT IS SAVED ON TAPE 12

```

0 000000 0 000000 0 000001 0 000000 0 000001 0 000001 0 000001
10-71-01 10001 C-04 North Area 19731 Pad Analysis - Net ion C
F-LL-2495, TIME HIST-01 IS SAVED ON TAPE 12

3 301195 5 500121 0 500015 0 500040 0 000163 0 001195 0 000183 0 000119
 14 7115 1 100011 0 14 North Area ISPSI Pad Analysis - Motion =
 FULL XING TIME HISTORY IS SAVED ON TAPE 12

0 000415 0 000767 0 000436 0 000437 0 000438 0 000439 0 000440 0 000441
100710 - 100031 C 04 North Anna 18521 Pad Road, via - Motion 2

1



EQE INTERNATIONAL

SHEET NO. _____ B1

JOB NO. 100031.01 JOB North Anna SSI Analysis of ISFSI Pad BY ABA DATE 6/12/97CALC. NO. 100031C04R0 SUBJECT Sliding and Overturning Factor of Safety CHK'D DD DATE 6/12/97

ATTACHMENT B

DIGITIZED FILES

File Name	Description	Date
analysx	Input to ANALYS, x direction	5/09/97 15:13
analysx.out	Output of ANALYS, x direction	5/13/97 20:57
motionx	Input to MOTION, x direction	5/13/97 11:39
mxred.out	Output* of MOTION, x direction	6/06/97 10:10
analysy	Input to ANALYS, y direction	5/09/97 15:13
analysy.out	Output of ANALYS, y direction	5/13/97 23:59
motiony	Input to MOTION, y direction	5/13/97 10:55
myred.out	Output* of MOTION, y direction	6/06/97 10:01
analysz	Input to ANALYS, z direction	5/09/97 15:14
analysz.out	Output of ANALYS, z direction	5/14/97 03:15
motionz	Input to MOTION, z direction	5/13/97 10:56
mzred.out	Output* of MOTION, z direction	6/06/97 10:19
mxzip.zip	Zipped output of MOTION, x direction	6/06/97 09:19
myzip.zip	Zipped output of MOTION, y direction	6/06/97 09:20
mzzip.zip	Zipped output of MOTION, z direction	6/06/97 09:21
acc231.xls	Excel file, node 231	6/09/97 13:20
acc232a.xls	Excel file, node 232	6/09/97 13:23
acc233a.xls	Excel file, node 233	6/09/97 13:26
acc234a.xls	Excel file, node 234	6/09/97 13:29
acc235a.xls	Excel file, node 235	6/09/97 13:32
acc236a.xls	Excel file, node 236	6/09/97 13:38
acc237a.xls	Excel file, node 237	6/09/97 13:41

TOTAL PAGES, INCLUDING COVER
SHEET

9 Diskettes and 1
Sheet

Note: Signature at the top of this sheet signifies that all contained documents have been verified.