



Department of Energy
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UMTRAP GEN

FEDERAL EXPRESS

Mr. Paul H. Lohaus
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Dear Paul,

The Ad Hoc Cell Design Working Group held a meeting with NRC personnel in Washington, DC, on October 20, 1988. As a result of this meeting, the enclosed report was prepared by G.R. Thiers, MK-E, and presents summary conclusions to be implemented by DOE on a site-by-site basis for the UMTRA Project in areas concerning rock erosion protection material particle size limits and procedures for absorption and sodium soundness field tests. These field tests will support DOE site certification for remedial actions through specification development and compliance; development of site specific Remedial Action Inspection Plans (RAIP); and follow-on Field Quality Control and Quality Assurance requirements.

Your responsive review and comment is requested. Your coordinated response with URFO would be appreciated.

For your information, Mr. T. Johnson, who was present at the October 20, 1988, meeting was given an advance copy of the enclosed information for his use. If you have any further questions please call me at (505) 844-3941.

Sincerely,

John R. D'Antonio
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PARTICLE SIZE LIMITS AND PROCEDURES FOR
ABSORPTION AND SODIUM SOUNDNESS TESTS

PROBLEM 3 - PARTICLE SIZE LIMITS

As shown on attached Tables 1 and 2, and Ref. 1, Page 47, the absorption and sodium sulfate soundness loss values for the coarse (plus No. 4) fraction of a given crushed rock generally differ from the corresponding values measured on the fine fraction. The difference is especially important for bedding on the UMTRA project, where the ratio of fine fraction to coarse fraction can be as large as 60/40.

In many cases the differences in absorption and soundness will result in significant differences in rock quality scores, sometimes determining whether a material can be used in frequently saturated areas, and often affecting the oversizing percentage. Absorption is sometimes higher for the fine fraction (Table 1), and soundness loss may be higher (Table 2, Sheets 1 and 2) or lower (Table 2, Sheet 3 and Ref. 1, Page 47).

For UMTRA designs submitted to date the larger of the two values measured for a given sample, (generally the value for the fine fraction), has been used in computing the rock quality score for that sample. This contrasts with the approach used by the USBR in the tests on which the scoring system is based (Ref. 2, Tables 1 and 7), in that those tests were run on the following particle sizes (Ref. 3):

- o Absorption Tests: 3-inch cubes.
- o Soundness Tests : No. 4 to 1.5-inch material.

Thus minus No. 4 material was not used in the tests on which the scoring system is based, so that the results of tests on minus No. 4 material are not comparable to the results used in developing the rating system.

PROBLEM 2 - TEST PROCEDURES

Sodium Soundness: A comparison of Refs. 4, 5 and 6 indicates the following differences between ASTM and USBR procedures for sodium soundness tests on plus No. 4 material:

	<u>ASTM C 88</u>	<u>USBR</u>
<u>Sample Weight (gm)</u>		
No. 4 to 3/8"	300 \pm 5	100 \pm 2.5
3/8" to 3/4"	1000 \pm 10	500 \pm 17.5
3/4" to 1-1/2"	1500 \pm 50	2000 \pm 50

Sieve Used to Determine Loss

No. 4 to 3/8" aggregate	No. 5	No. 4
3/8" to 3/4" aggregate	5/16"	3/8"
3/4" to 1-1/2" aggregate	5/8"	3/4"

Weighting to Determine
Weighted Average Loss

No. 4 to 3/8"	Use grading	20%
3/8" to 3/4"	of sample	30%
3/4" to 1-1/2"	as received	50%

These are the only significant differences between the test procedures.

Specific Gravity, Absorption, and L.A. Abrasion: For specific gravity, absorption and LA abrasion tests the USBR uses ASTM procedures (Ref. 4).

SOLUTION

In cases where the fine portion of a given material is derived from the same parent rock as the coarse portion, the absorption and soundness results from the coarse fraction can be used in developing rock quality scores for the material. This is generally the case for material obtained by blasting and crushing rock from a relatively homogeneous strata, and may be true for some alluvial deposits. The petrographic analysis should delineate the relative homogeneity of a given alluvial deposit.

When the fine and coarse materials are derived from different parent rock sources the ideal approach will be to test samples of the parent rock in the same size range as used by the USBR. This will seldom be possible. Alternatively if separate criteria for fine material (differing from the criteria for coarse material based on the USBR tests) were available, such criteria could be applied. ASTM Standard C-233, "Standard Specification for Concrete Aggregates", does contain an upper limit of 10% for sodium sulfate soundness loss for fine aggregate; but this is essentially the same as applying the present scoring system, under which a 10% soundness loss gives a test score of 50%, the same as the minimum acceptable overall score. Other explicit criteria for fine aggregate have not been found. Therefore in the absence of separate criteria or representative larger samples it will be necessary to test samples of the largest-sized available representative material.

To correspond to the tests on which the scoring system is based the USBR procedure for sodium soundness tests (Ref. 5) should be used.

SUMMARY

1. In cases where the fine portion of a given material is derived from the same parent rock as the coarse fraction, test representative material in the following particle size ranges:

- o Absorption Tests: 2-inch to 4-inch.
- o Soundness Tests : No. 4 to 1.5-inch.

2. Where the fine and coarse fractions are derived from different parent rock sources, test representative samples in the following particle size ranges:

- o Coarse material: as given above.
- o Fine fraction:
 - If the parent rock is available in suitable sizes, test this rock in the size ranges given above.
 - In other cases test the fine fraction in the largest size range available.

This approach is more directly supported by past experience and will result in more realistic designs.

3. Use USBR procedures for sodium soundness test. (Ref. 5).

REFERENCES

1. Fookes, P. G., C. S. Gourley, and C. Ohikere (1988), "Rock Weathering in Engineering Time", Quarterly Journal of Engineering Geology, London, Vol. 21, pp. 33-57.
2. DePuy, G. W. (1965), "Petrographic Investigations of Rock Durability and Comparison of Various Test Procedures", Engineering Geology, Bulletin of the Association of Engineering Geologists, Vol. 2, No. 2, pp. 31-46.
3. DePuy, G. W. (1988), Phone Conversation with G. R. Thiers, Morrison-Knudsen Engineers, Inc., San Francisco, California, 20 January.
4. ASTM (1988), "Standard Test Method for Soundness of Aggregate by Use of Sodium Sulfate or Magnesium Sulfate", Designation C88-83, American Society for Testing and Materials, Volume 04.02.
5. USBR (1961), Concrete Manual, 6th Edition, U.S. Department of the Interior, Water and Power Resources Service.
6. Hess, Robert (1988), USBR, Denver, Phone Conversation with G. R. Thiers, Morrison-Knudsen Engineers, Inc., San Francisco, California, 28 November.
7. Hess, Robert (1988), USBR, Denver, Phone Conversation with G. R. Thiers, Morrison-Knudsen Engineers, Inc., San Francisco, California, 29 November.

TABLE 1
(Sheet 1 of 2)
COMPARISON OF ABSORPTION VALUES
FOR VARIOUS ROCK SIZES

SOURCE OF ROCK: PEPPERLING QUARRY, LAKEVIEW, OREGON

<u>Sample No.</u>	<u>Large Riprap</u>	<u>Small Riprap</u>	<u>Bedding</u>
<u>1987</u>			
Riprap D1A, B, C	0.64		
Riprap C1A, B	0.31		
Riprap B-1		0.48	
Riprap B-2		0.15	
Riprap B-3		0.25	
Riprap B-4		0.39	
Riprap A-1		0.64	
Riprap A-2		0.77	
Riprap A-3		0.76	
<u>1988</u>			
Bedding B-1 (1)			1.24
Bedding B-1 (2)			1.00
Bedding B-1 (2')			2.98
Bedding B-1 (3)			1.43
Bedding B-2 (1)			2.53
Bedding B-2 (2)			1.37
Bedding B-2 (3)			1.48
Riprap B (1)		1.04	
Riprap B (2)		1.10	
Riprap B (3)		<u>2.13</u>	
Average (All Samples)	0.43	0.77	1.72
Average (1988 Only)		1.42	1.72

TABLE 1
(Sheet 2 of 2)
COMPARISON OF ABSORPTION VALUES
FOR VARIOUS ROCK SIZES

SOURCE OF ROCK: SHEER'S PIT, LAKEVIEW, OREGON

<u>Sample No.</u>	<u>Large Riprap</u>	<u>Small Riprap</u>	<u>Bedding</u>
2		0.26	
T-B-001	0.27		
M-B-001	0.26		
B-1-A			0.86
B-1-B			0.94
B-2-A			0.65
B-2-B	<u> </u>	<u> </u>	<u>0.59</u>
Average	0.26	0.26	0.76

TABLE 2
(Sheet 1 of 3)
COMPARISON OF SODIUM SULFATE SOUNDNESS VALUES
FOR COARSE AND FINE FRACTIONS

SOURCE OF ROCK: PEPPERLING QUARRY, LAKEVIEW, OREGON

<u>Sample No.</u>	<u>Coarse Fraction</u>		<u>Fine Fraction</u>	
	<u>Large Riprap</u>	<u>Small Riprap</u>	<u>Bedding</u>	
<u>1987</u>				
Riprap D1A, B, C	0.51			
Riprap C1A, B	0.75			
Riprap B-1		0.56		
Riprap B-2		0.13		
Riprap B-3		2.11		
Riprap B-4		0.89		
Riprap A-1		3.07		
Riprap A-2		1.36		
Riprap A-3		0.54		
<u>1988</u>				
Bedding B-1 (1)			1.2	7.2
Bedding B-1 (2)			3.9	11.9
Bedding B-1 (2')			1.9	17.3
Bedding B-1 (3)			6.9	9.4
Bedding B-2 (1)			5.4	6.7
Bedding B-2 (2)			3.7	7.0
Bedding B-2 (3)			5.7	8.5
Riprap B (1)		1.4		6.4
Riprap B (2)		1.9		11.1
Riprap B (3)		<u>2.6</u>		<u>9.8</u>
Average (All Samples)	0.63	1.46	4.1	9.5
Average (1988 Only)		1.97	4.1	9.5

TABLE 2
(Sheet 2 of 3)
COMPARISON OF SODIUM SULFATE SOUNDNESS VALUES
FOR COARSE AND FINE FRACTIONS

SOURCE OF ROCK: SHEER'S PIT, LAKEVIEW, OREGON

<u>Sample No.</u>	<u>Coarse Fraction</u>		<u>Bedding</u>	<u>Fine Fraction</u>
	<u>Large Riprap</u>	<u>Small Riprap</u>		
<u>1988</u>				
2		4.8		8.1
T-B-001	0.7			-
M-B-001	0.2			-
B-1-A			0.9	4.2
B-1-B			1.4	4.8
B-2-A			1.0	2.2
B-2-B			<u>0.8</u>	<u>4.0</u>
Average	0.45	4.8	1.0	4.7

SOURCE OF ROCK: CHOATE'S QUARRY, LAKEVIEW, OREGON

B-1		0.4	7.0
B-2		0.7	5.5
B-1-N		0.6	4.3
B-2-N		0.4	4.5
B-1-S		0.3	1.2
B-2-S		<u>0.2</u>	<u>2.9</u>
Average		0.5	4.2

TABLE 2
(Sheet 3 of 3)
COMPARISON OF SODIUM SULFATE SOUNDNESS VALUES
FOR COARSE AND FINE FRACTIONS

ADDITIONAL ROCK SOURCES

<u>Source</u>	<u>Coarse Fraction</u>	<u>Fine Fraction</u>
West Pawelekille Quarry, Texas	0.2	4.0
Redland Worth, San Pedro, Texas	0.06	0.02
Tordilla Hill Quarry (East), Texas	5.8	0.8
Tordilla Hill Quarry (West), Texas	0.4	0.6
Tordilla Hill Quarry (N. East), Texas	2.0	0.08
Tordilla Hill Quarry (North), Texas	0.3	0.6
Knippa Quarry, Texas	3.3	1.2



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