

UNITED STATES NUCLEAR REGULATORY COMMISSION WASHINGTON, D. C. 20555

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No comments

MAY 1 3 1985

FEMORANDUM FOR: Dennis M. Crutchfield, Assistant Director

Division of Licensing

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Robert Scsnak, Acting Assistant Director

for Components and Structures Engineering

Division of Engineering

SUPCECT:

FINAL CRAFT OF THE RIVER BEND UNIT 1 TECHNICAL

SPECIFICATION

As requested in your memo dated April 19, 1985, on above subject, we have reviewed the River Bend Technical Specification 3.3.7.2 on Seismic Instrumentation and 3.7.10 on Structural Settlement. We find these Technical Specifications, as written, are acceptable and no changes are required. A copy of these Technical Specifications is attached.

> F. Cherry for Robert Bosnak, Acting Assistant Director for Components and Structures Engineering Division of Engineering

Enclosure: As stated

cc: J. Knight

G. Lear

L. Heller

P. Kuc

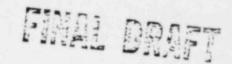
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INSTRUMENTATION

SEISMIC MONITORING INSTRUMENTATION



LIMITING CONDITION FOR OPERATION

3.3.7.2 The seismic monitoring instrumentation shown in Table 3.3.7.2-1 shall

APPLICABILITY: At all times.

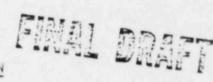
ACTION:

- a. With one or more of the above required seismic monitoring instruments to the Commission pursuant to Specification 6.9.2 within the next restoring the instrument(s) to OPERABLE status.
- b. The provisions of Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

- 4.3.7.2.1 Each of the above required seismic monitoring instruments shall be demonstrated OPERABLE by the performance of the CHANNEL CHECK, CHANNEL FUNCTIONAL TEST and CHANNEL CALIBRATION operations at the Trequencies shown in
- 4.3.7.2.2 Each of the above required seismic monitoring instruments actuated during a seismic event greater than or equal to 0.01g shall be restored to OPERABLE status within 24 hours and a CHANNEL CALIBRATION performed within 5 days and analyzed to determine the magnitude of the vibratory ground motion. A Special tion 6.9.2 within 10 days describing the magnitude, frequency spectrum and resultant effect upon unit features important to safety.

TABLE 3.3.7.2-1



SEISMIC MONITORING INSTRUMENTATION

	STRUMENTS AND SENSOR LOCATIONS	MEASUREMENT RANGE	MINIMUM INSTRUMENTS OPERABLE
1.	Triaxial Time-History Accelerographs		OPERABLE
	a. Reactor Bldg Mat EL 70'0" b. Reactor Bldg Ext Shield Wall EL 232'0"	0 ± 1.0 g	ı
	 Reactor Bidg Drywell EL 151'0" Free Field - Grade Level 	0 ± 1.0 g 0 ± 1.0 g 0 ± 1.0 g	1 1
2.	Triaxial Peak Accelerographs		*
	 Reactor Bldg SLCS Storage Tank Reactor Bldg - RHR Inj. Piping Aux. Bldg Service Water Piping 	0 ± 10.0 g 0 ± 10.0 g 0 ± 10.0 g	1
3.	Triaxial Seismic Switches	- 10.0 g	1
	a. Reactor Bldg Mat El 70'0"	0.025 to 0.25 g	,(a)
.	Triaxial Response-Spectrum Recorders		
	a. Reactor Bldg Mat EL 70'0" b. Reactor Bldg Floor EL 141'0" c. Auxiliary Bldg Mat EL 70'0" d. Auxiliary Bldg Floor EL 141'0"	0 ± 2 g 0 ± 2 g 0 ± 2 g 0 ± 2 g	1(a)-

⁽a) with reactor control room indication and annunciation.

TABLE 4.3.7.2-1 SEISMIC MONITORING INSTRUMENTATION SURVEILLANCE REQUIREMENTS

IN	ISTRUMENTS AND SENSOR LOCATIONS	CHANNEL CHECK	CHANNEL FUNCTIONAL	CHANNEL
	Triaxial Time-History Accelerograph	s	TEST _	CALIBRATION
	a. Reactor Bldg. Mat EL 70'0" b. Reactor Bldg. Exit Shield Wall EL 232'0" c. Reactor Bldg. Drywell EL 151'0' d. Free Field-Grade Level	M M	SA	R R
2.	Triaxial Peak Accelerographs	М	\$A	R
3.	a. Reactor Bldg. SLCS Storage Tank b. Reactor Bldg RHR Inj. Piping c. Aux. Bldg. Service Water Piping Triaxial Seismic Switches		NA NA NA	R R R
4.	a. Reactor Bldg. Mat EL 70'0" Triaxial Response-Spectrum Recorders	M(a)	SA	R
(a)-	a. Reactor Bldg. Mat EL 70'0' b. Reactor Bldg. Floor EL 141'0" c. Auxiliary Bldg. Mat EL 70'0" d. Auxiliary Bldg. Floor EL 141.0"	M NA NA NA	SA SA NA NA	R R R

⁽a) Except seismis trigger.

PLANT SYSTEMS

3/4.7.10 STRUCTURAL SETTLEMENT

FIREL DRRFT

LIMITING CONDITION FOR OPERATION

- 3.7.10 Structural settlement of the following structures shall be within the predicted values as shown in Table 3.7.10-1.
 - a. Reactor Building
 - b. Auxiliary Building
 - c. Fuel Building
 - Control Building d.
 - e. Diesel Generator Building
 - Standby Cooling Tower, Basin and Pump House

APPLICABILITY: At all times.

ACTION:

With the measured structual settlement of any of the above required structures outside of the predicted settlement, prepare and submit a Special Report to the Commission pursuant to Specification 6.9.2 within the next 30 days providing a record of the settlement measurements and the predicted settlement, an analysis to demonstrate the continued structural integrity of the affected structure(s) and plans to monitor the settlement of the affected structure(s) in the future.

SURVEILLANCE REQUIREMENTS

- 4.7.10 The structural settlement of the above required structures shall be demonstrated to be within the predicted settlement values:
 - At least once per 92 days, using at least three markers per structure, until there is essentially no movement during those 92 days.
 - b. At least once per 24 months, using at least one marker per structure,
 - Following any seismic event equal to or greater than an Operational Basis Earthquake (OBE), using at least three markers per structure.



UNITED STATES NUCLEAR REGULATORY COMMISSION WASHINGTON, D. C. 20555

May 13, 1985

MEMORANDUM FOR: Dennis M. Crutchfield, Assistant Director

for Safety Assessment, DL

FROM:

R. Wayne Houston, Assistant Director

for Reactor Safety, DSI

SUBJECT:

REVIEW OF THE TECHNICAL SPECIFICATIONS FOR THE

RIVER BEND GENERATING STATION

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The Containment Systems Branch (CSB) has completed its review of those portions of the River Bend Generating Station Technical Specifications that fall within its review responsibility. Enclosed is a marked-up copy of the affected Technical Specifications (T.S.).

The bulk of the suggested changes are either editorial in nature or clarifications. A few, however, are more substantive and are summarized below.

Item 3.6.1.9 and 3.6.2.7:

These T.S. are interim criteria for the first cycle. The applicant has committed to an information gathering program during the first cycle to develop a basis for future usage of the containment and drywell purge system and to propose consistent T.S. for any changes. As written, the interim criteria will end 3 months after completion of the first refueling outage. A 1000 hour limitation will become effective after this time if no T.S. changes are proposed.

Item 3.6.2.7:

Since the applicant has not provided assurance that the drywell purge valves will close under accident conditions, the valves should be locked closed until the valves are properly qualified. This qualification program is currently unscheduled by the applicant.

CONTACT: F. Eltawila, CSB: DSI

x29488

It should be noted that this T.S. restriction may cause undue hardship during the initial heat-up test period due to the potential release of ammonia from drywell insulation. The staff will work closely with the applicant to seek resolution of this difficulty.

> R. Wayne Houston, Assistant Director for Reactor Safety, DSI

cc w/o enclosure: R. Bernero H. Thompson T. Novak

W. Butler

S. Stern

E. Butcher

cc w/ enclosure:

D. Houston

PRESSURE BOUNDARY LEAKAGE

1.30 PRESSURE BOUNDARY LEAKAGE shall be leakage through a non-isolable fault in a reactor coolant system component body, pipe wall or vessel wall.

PRIMARY CONTAINMENT INTEGRITY - FUEL HANDLING

- 1.31 PRIMARY CONTAINMENT INTEGRITY FUEL HANDLING shall exist when:
 - a. All containment penetrations required to be closed during accident conditions are closed by at least one manual valve, blind flange, or deactivated automatic valve secured in its closed position.
 - b. All containment hatches are closed.
 - c. Each containment air lock is in compliance with the requirements of Specification 3.6.1.4. | OPERATIONAL CONDITIONS

PRIMARY CONTAINMENT INTEGRITY - OPERATING (Mades 1, 2 and 3)

- 1.32 PRIMARY CONTAINMENT INTEGRITY OPERATING shall exist when:
 - a. All containment penetrations required to be closed during accident conditions are either:
 - Capable of being closed by an OPERABLE containment automatic isolation system, or
 - Closed by at least one manual valve, blind flange, or deactivated automatic valve secured in its closed position, except, as provided in Specification 3.6.4.
 - -b. All containment equipment hatches are closed and sealed.
 - c. Each containment air lock is in compliance with the requirements of Specification 3.6.1.4.
 - d. The containment leakage rates are within the limits of Specification 3.6.1.2.
 - e. The suppression pool is in compliance with the requirements of Specification 3.6.3.1.
 - f. The sealing mechanism associated with each primary containment penetration; e.g., welds, bellows or 0-rings, is OPERABLE.

PROCESS CONTROL PROGRAM (PCP)

1.33 The PROCESS CONTROL PROGRAM shall contain the current formula, sampling, analyses, tests, and determinations to be made to ensure that the processing and packaging of solid radioactive wastes based on demonstrated processing of actual or simulated wet solid wastes will be accomplished in such a way as to assure compliance with 10 CFR Part 20, 10 CFR Part 61, 10 CFR Part 71 and

Federal and State regulations and other requirements governing the disposal of the radioactive waste.

RATED THERMAL POWER

1.34 RATED THERMAL POWER shall be a total reactor core heat transfer rate to the reactor coolant of 2894 MWT.

REACTOR PROTECTION SYSTEM RESPONSE TIME

1.35 REACTOR PROTECTION SYSTEM RESPONSE TIME shall be the time interval from when the monitored parameter exceeds its trip setpoint at the channel sensor until de-energization of the scram pilot valve solenoids. The response time may be measured by any series of sequential, overlapping or total steps such that the entire response time is measured.

REPORTABLE EVENT

1.36 A REPORTABLE EVENT shall be any of those conditions specified in 10 CFR 50.73.

ROD DENSITY

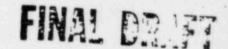
1.37 ROD DENSITY shall be the number of control rod notches inserted as a fraction of the total number of control rod notches. All rods fully inserted is equivalent to 100% ROD DENSITY.

SECONDARY CONTAINMENT INTEGRITY - FUEL BUILDING

- 1.38 SECONDARY CONTAINMENT INTEGRITY FUEL BUILDING shall exist when:
 - All Fuel Building penetrations required to be closed during accident conditions are closed by valves, blind flanges, or dampers secured in position.
 - b. All Fuel Building equipment hatch covers are installed.
 - c. The Fuel Building Charcoal Filtration System is in compliance with the requirements of Specification 3/4.6.5.6.
 - d. At least one door in each access to the Fuel Building is closed, except for routine entry and exit of personnel and equipment.
 - e. The pressure within the Fuel Building is maintained in compliance with the requirements of Specification 4.6.5.1.2.a.

SECONDARY CONTAINMENT INTEGRITY - OPERATING (MODES) 1, 2 and 3)

- 1.39 SECONDARY CONTAINMENT INTEGRITY OPERATING shall exist when:
 - All Auxiliary Building penetrations, Fuel Building penetrations and Shield Building annulus penetrations required to be closed during accident conditions are either:



PRIMARY CONTAINMENT INTEGRITY - FUEL HANDLING

LIMITING CONDITION FOR OPERATION

3.6.1.2 PRIMARY CONTAINMENT INTEGRITY - FUEL HANDLING shall be maintained.

APPLICABILITY: OPERATIONAL CONDITION*

ACTION:

Without PRIMARY CONTAINMENT INTEGRITY - FUEL HANDLING, suspend handling of irradiated fuel in the primary containment, CORE ALTERATIONS and operations with a potential

SURVEILLANCE REQUIREMENTS

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4.6.1.2 PRIMARY CONTAINMENT INTEGRITY - FUEL HANDLINGY Shall be demonstrated:

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Within 24 hours prior to and at least once per chift in OPERATIONAL CONDITION* by verifying that all primary containment penetrations chown in Table 3.6.41 required to be closed during accident conditions are closed by hatches, valves, blind flanges, or deactivated automatic valves secured in position.

b. By verifying each containment air lock is in compliance with the requirements of Specification 3.6.1.4.

When handling irradiated fuel in the primary containment and during CORE ALTERATIONS and operations with a potential for draining the reactor vessel.

PRIMARY CONTAINMENT LEAKAGE

LIMITING CONDITION FOR OPERATION

- 3.6.1.3 Primary containment leakage rates shall be limited to:
 - a. An overall integrated leakage rate of less than or equal to La, 0.26 percent by weight of the primary containment air per 24 hours at Pa, 7.6 psig.
 - b. A combined leakage rate of less than 0.60 La for all penetrations and all valves subject to Type B and C tests when pressurized in accordance with Table 3.6.4-1 of Specification 3.5.4.
 - c. A leakage rate of less than 340 scfh for each of the valve groups identified below when tested in accordance with the surveillance requirements of 4.6.1.3.f.
 - 1. Division I MS-PLCS Valves and Division I PVLCS Valves
 - 2. Division II MS-PLCS Valves and Division II PVLCS Valves
 - 3. Division I MSPLCS Valves and all first outboard PVLCS Valves
 - d. A combined leakage rate of less than or equal to 13,500 cc/hr for all penetrations shown in Table 3.6.1.3-1 as annulus bypass leakage paths when pressurized to Pa, 7.6 psig.
 - A combined leakage rate of less than or equal to 170,000 cc/hr, for all valves shown in Table 3.6.4-1 to be equipped with PVLCS, when pressurized to Pa, 7.6 psig.

 Secondary contempt appara teatroin fall, and X

A combined leakage rate of less than or equal to 1 gpm times the total number of containment isolation valves in hydrostatically tested lines at Pa, 7.6 psig.

OPERATING

APPLICABILITY: When PRIMARY CONTAINMENT INTEGRITY is required per Specifica-

ACTION:

With:

- a. The measured overall integrated primary containment leakage rate equaling or exceeding 0.75 La or;
- b. The measured combined leakage rate for all penetrations and all valves subject to Type B and C tests exceeding 0.6) La, or
- c. The measured leakage rate greater than or equal to 340 scfh for each valve grouping identified in 3.6.1.3.c.1, 3.6.1.3.c.2 or 3.6.1.3.c.3,

LIMITING CONDITION FOR OPERATION (Continued)

ACTION (Continued)

d. The combined leakage rate for all penetrations shown in Table 3.6.1.3-1 as annulus bypass leakage paths exceeding 13,500 cc/hr,

e. The combined leakage rate, for all valves shown in Jable 3.6.4-1 to be equipped with PYLCS, exceeding 170,000 cc/hr, or

f. The measured combined leakage rate for all containment isolation valves in hydrostatically tested lines per Table 3.6.4-1 which penetrate the primary containment exceeding 1 gpm times the total number of such valves,

restore:

- a. The overall integrated leakage rate(s) to less than 0.75 La as applicable, and
- b. The combined leakage rate for all penetrations and all valves subject to Type B and C tests to less than or equal to 0.60 La, and
- c. The measured leakage rate to less than 340 scfh for each of the valve groupings identified in 3.6.1.3.c.1, 3.6.1.3.c.2, and 3.6.1.3.c.3
- d. The combined leakage rate for all penetrations shown in Table 3.6.1.3-1 as annulus bypass leakage paths to less than or equal to 13,500 cc/hr and

e. The combined leakage rate, for all valves shown in Table 3.6.4-1 to be equipped with PVLCS to less than or equal to 170,000 cc/hr, and

f. The combined leakage rate for all per Table 3.6.4-1 containment isolation valves in hydrostatically tested lines per Table 3.6.4-1 which penetrate the primary containment to less than or equal to 1 gpm times the total number of such valves,

prior to increasing reactor coolant system temperature above 200°F.

SURVEILLANCE REQUIREMENTS

- 4.6.1.3 The primary containment leakage rates shall be demonstrated at the following test schedule and shall be determined in conformance with the criteria specified in Appendix J of 10 CFR 50 using the methods and provisions of ANSI N45.4 (1972):
 - a. Three Type A Overall Integrated Containment Leakage Rate tests shall be conducted at 40 \pm 10 month intervals during shutdown at Pa, 7.6 psig, during each 10-year service period. The third test of each set shall be conducted during the shutdown for the 10-year plant inservice inspection.

SURVEILLANCE REQUIREMENTS (Continued)

- b. If any periodic Type A test fails to meet 0.75 La, the test schedule for subsequent Type A tests shall be reviewed and approved by the Commission. If two consecutive Type A tests fail to meet 0.75 La, a Type A test shall be performed at least every 18 months until two consecutive Type A tests meet 0.75 La, at which time the above test schedule may be resumed.
- c. The accuracy of each Type A test shall be verified by a supplemental test which:
 - 1. Confirms the accuracy of the test by verifying that the difference between the supplemental test data and the Type A test data is within 0.25 $L_a \cdot [L_c \pm (\frac{1}{am} + L_o) \le 0.25 L_a]$ where $L_c = \text{supplemental test results}$; $L_c = \text{superimposed leakage}$; $L_{am} = \text{measured Type A leakage}$.
 - Has duration sufficient to establish accurately the change in leakage rate between the Type A test and the supplemental test.
 - Requires the quantity of gas injected into the primary containment or bled from the primary containment during the supplemental test to be between 0.75 La and 1.25 La.
- d. Type B and C tests shall be conducted with gas at Pa, 7.6 psig*, at intervals no greater than 24 months except for tests involving:
 - 1. Air locks,
 - Main steam positive leakage control system (MS-PLCS) valves and PVLCS valves,
 - 3. Penetrations using continuous leakage monitoring systems,
 - Primary containment isolation valves in hydrostatically tested lines per Table 3.6.4-1 which penetrate the primary containment, and
 - Purge supply and exhaust isolation valves with resilient material seals.
- e. Air locks shall be tested and demonstrated OPERABLE per Surveillance Requirement 4.6.1.4.

Total sealing air leakage into the primary containment at a test pressure of 11.5 psid for main steam isolation valves and #3 psid for penetration leakage control system sealed valves shall be tested at least once per 18 months.

*Unless a hydrostatic test is required per Table 3.6.4-1.

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SURVEILLANCE REQUIREMENTS (Continued)

- g. Type B periodic tests are not required for penetrations continuouslymonitored by the Primary Containment Penetration Procesurization System,provided the system is OPERABLE per Specification 3.5.1.9.
- Type B test; for electrical penetrations employing a continuous leakage monitoring system shall be conducted at Pa, 7.6 psig, at intervals no greater than once per 3 years.
- Leakage from isolation valves that are sealed with the PVLCS may be excluded when determining the combined leakage rate sported the seal with the seal system capacity is adequate to maintain system pressure for at least 30 days. This leakage , o.c. La.
- Primary containment isolation valves in hydrostatically tested lines per Table 3.6.4-1 which penetrate the primary containment shall be leak tested at least once per 18 months.
- Furge supply and exhaust isolation valves with resilient material seals shall be tested and demonstrated OPERABLE per Surveillance Requirement 4.6.1.9.3.
- K.Y. The provisions of Specification 4.0.2 are not applicable to Specifications 4.6.1.3.a, 4.6.1.3.b, 4.6.1.3.d, 4.6.1.3.e and 4.6.1.3.K.

TABLE 3.6.1.3-1

ANNULUS BYPASS LEAKAGE PATHS

1. LEAKAGE PATHS TO THE FUEL BUILDING

PENETRATION

Containment air lock 1JRE*DRA2

2. LEAKAGE PATHS TO THE AUXILIARY BUILDING

PENETRATION	VALVE NO. (DIV. 1)	VALVE NO. (DIV. 2)
1KJB*Z31	1HVR*AOV165	1HVR*AOV123
1KJB*605E	1CMS*SOV31A	1CMS*50V350
1KJE*605F	1CMS*SOV \$310	1CMS*SOV35A
1KJB*601B	1SSR*SOV131	1SSR*SOV130
Containment air lock	1JRB*DR	
CRD removal hatch		

PRIMARY CONTAINMENT AIR LOCKS

LIMITING CONDITION FOR OPERATION

- 3.6.1.4 Each primary containment air lock shall be OPERABLE with:
 - a. Both doors closed except when the air lock is being used for normal transit entry and exit through the containment, then at least one air lock door shall be closed, and
 - b. An overall air lock leakage rate in compliance with the limits of Specification 3.6.1.3.d when pressurized to Pa, 7.6 psig, and
 - c. The inflatable seal system air flask pressure $\geq \frac{90}{100}$ psig.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2*, 3, and #.

ACTION:

- a. With one primary containment air lock door inoperable:
 - Maintain at least the OPERABLE air lock door closed and either restore the inoperable air lock door to OPERABLE status within 24 hours or lock the OPERABLE air lock door closed.
 - Operation may then continue until performance of the next required overall air lock leakage test provided that the OPERABLE air lock door is verified to be locked closed at least once per 31 days.
 - 3. Otherwise, be in at least HOT SHUTDOWN within the next 12 hours and in COLD ShuTDOWN within the following 24 hours.
 - 4. Otherwise in Operational Condition at ** (INTERT A)

 5 M. The provisions of Specification 3.0.4 are not applicable.
- b. With a primary containment air lock inoperable, except as a result of an inoperable air lock door, maintain at least one air lock door closed; I. In OPERATE in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.
- c. With one primary containment air lock door inflatable seal system air flask pressure instrumentation channel inoperable, restore the inoperable channel to OPERABLE status within 7 days or verify air flask pressures to be > 100 psig at least once per 12 hours.

"See Special Test Exception 3.10.1.

#When irradiated fuel is being handled in the tesandary containment and during CORE ALTERATIONS and operations with a potential for draining the reactor vessel.

The tesandary containment and during the reactor vessel.

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suspend all operations involving handling of irradiated fuel in the containment, CORE ALTERATIONS, and operations with a potential for draining the reactor vessel.

SURVEILLANCE REQUIREMENTS

- 4.6.1.4 Each primary containment air lock shall be demonstrated OPERABLE:
 - Within 72 hours following each closing, except when the air lock is being used for multiple entries, then at least once per 72 hours, by verifying seal leakage rate is in compliance with the Timits in Specification 3.6.1.3.d when the gap between the door seals is pressurized to Pa, 7.6 psig.
 - By conducting an overall air lock leakage test at Pa, 7.6 psig, and verifying that the overall air lock leakage rate is within its limit:
 - At least once per 6 months,*
 - Prior to establishing PRIMARY CONTAINMENT INTEGRITY OPERATING when maintenance has been performed on the air lock that could when the air lock sealing capability #
 - At least once per 6 months by verifying that only one door in each air lock can be opened at a time.
 - By verifying the door inflatable seal system OPERABLE by:
 - At least once per 7 days, verifying seal air flask pressure to be greater than or equal to 60 psig.
 - At least once per 18 months, conducting a seal pneumatic system leak test and verifying that system pressure does not decay more than 1.56 psig from 100 psig within 24 hours. 1.28 90

The provisions of Specification 4.0.2 are not applicable.

#Exemption to Appendix 3 of 10 CFR 50.

PRIMARY CONTAINMENT INTERNAL PRESSURE

FINAL DRAFT

LIMITING CONDITION FOR OPERATION

3.6.1.7 Primary containment internal pressure shall be maintained between -0.3 and +0.3 psig.

AFPLICABILITY: OPERATIONAL CONDITIONS 1, 2, and 3.

ACTION:

with the primary containment to condain internal outside of the specified limits, restore the differential pressure the limits within 1 hour or be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.

SURVEILLANCE REQUIREMENTS

4.6.1.7 The primary containment internal pressure shall be determined to be within the limits at least once per 12 hours.

PRIMARY CONTAINMENT AVERAGE AIR TEMPERATURE

FINAL DRAFT

LIMITING CONDITION FOR OPERATION

3.6.1.8 Primary containment average air temperature shall not exceed 100°F.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2 and 3.

ACTION:

With the primary containment average air temperature greater than $\frac{90}{100}$ °F, reduce the average air temperature to within the limit within 8 hours or be in at least following 24 hours.

SURVEILLANCE REQUIREMENTS

4.6.1.8 The primary containment average air temperature shall be the arithmetical average of the temperatures at the following locations and shall be determined to be within the limit at least once per 24 hours:

	Elevation	Azimuth*
à.	~167'	~ 72°
b.	~167'	~108°
c.	~167'	~ 37°
d.	~122'	~170°
е.	~119'	~ 15°
f.	~119'	~ 270°
g.	~119'	~ 66°
h.	~119'	~117°
i.	~119'	~219°
j.	~119'	~322°

[&]quot;At least one reading from each elevation is required for an average calculation. However, if all instrumentation is OPERABLE, all readings should be used in the

PRIMARY CONTAINMENT PURGE SYSTEM

FINAL DRAFT

LIMITING CONDITION FOR OPERATION

- 3.6.1.9 The primary containment purge 36 inch supply and exhaust isolation valves shall be OPERABLE and closed except:
 - a. Each 36 inch purge valve may be open for purge system operation with such operation limited to 2000 hours per 365 days for reducing airborne activity and pressure control, and
 - b. If the SGTS is in the purge flow path then both trains of the SGTS must be OPERABLE, but only one train of SGTS may be operating in the purge flow path.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2, and 3.

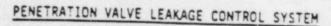
ACTION:

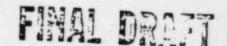
- a. With a 36 inch primary containment punge supply and/or exhaust isolation valve(s) open for more than 2000 hours per 365 days, close and/or seal the 36 inch valve(s) or otherwise isolate the penetration within 4 hours or be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.
- b. With both SGTS trains in operation in the purge flow path and/or without both SGTS OPERABLE with one SGTS in the purge flow path, discontinue 36 inch purge system operation and close the open 36 inch valve(s) or otherwise isolate the penetration(s) within 4 hours or be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.
- with a primary containment purge supply and/or exhaust isolation valve(s) with resilient material seals having a measured leakage rate exceeding the limit of Surveillance Requirement 4.6.1.9.3, restore the inoperable valve(s) to OPERABLE status within 24 hours or be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.

SURVEILLANCE REQUIREMENTS

- 4.6.1.9.1 Each 36 inch primary containment purge supply and exhaust isolation valve shall be verified to be cealed closed at least once per 31 days.
- 4.6.1.9.2 The cumulative time that the 36 inch primary containment purge supply and/or exhaust isolation valves have been open during the past 365 days shall be determined at least once per 7 days.
- # April colde for the period from initial criticality to 3 months after the Completion of the 15' refueling outage, otherwise, 1000 hours fix 36- 14

 RIVER BEND UNIT 1 3/4 6-14





LIMITING CONDITION FOR OPERATION

3.6.1.10 Two independent penetration valve leakage control system (PVLCS) divisions shall be OPERABLE.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2 and 3.

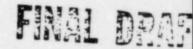
ACTION:

With one PVLCS division inoperable, restore the inoperable division to OPERABLE status within 7 days or be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.

SURVEILLANCE REQUIREMENTS

- 4.6.1.10 Each PVLCS division shall be demonstrated OPERABLE:
 - a. At least once per 24 hours by verifying division PVLCS accumulator pressure greater than or equal to 101 psig.
 - b. During each COLD SHUTDOWN, if not performed within the previous 92 days, by cycling each remote, manual and automatic motor operated valve through at least one complete cycle of full travel.
 - c. At least once per 18 months by1
 - Performance of a functional test which includes simulated actuation of the system throughout its operating sequence, and verifying that each automatic valve actuates to its correct position and that a sealing pressure greater than or equal to 27 psig is established in each sealing valve, and
 - 2. Leakage from valves equipped with the PVLCS will be included in computation of 0.6 La.

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SURVEILLANCE REQUIREMENTS (Continued)

- e. By verifying the personnel door inflatable seal system OPERABLE by:
 - At least once per 7 days verifying seal air flask pressure to be greater than or equa to 100 psig.
 - At least once per 18 months conducting a seal pneumatic system leak test and verifying that system pressure does not decay more than 1:16 psig from 100 psig within 24 hours.

DRYWELL AIR LOCKS

FINAL DRAFT

LIMITING CONDITION FOR OPERATION

3.6.2.3 The drywell air lock shall be OPERABLE with:

- a. Both doors closed except when the air lock is being used for normal transit entry and exit through the drywell, then at least one air lock door shall
- An overall air lock leakage rate of less than or equal to 11.85 scf per hour at 3.0 psid, and
- c. The inflatable seal system air flask pressure > 100 psig.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2*, and 3.

ACTION:

- a. With one drywell air lock door inoperable:
 - Maintain at least the OPERABLE air lock door closed and either restore the inoperable air lock door to OPERABLE status within 24 hours or lock the OPERABLE air lock door closed.
 - Operation may then continue provided that the OPERABLE air lock door is verified to be locked closed at least once per 31 days.
- in COLD SHUTDOWN within the following 24 hours.
 - 4. The provisions of Specification 3.0.4 are not applicable.
- b. With the drywell air lock inoperable, except as a result of an inoperable air lock door, maintain at least one air lock door closed; restore the inoperable air lock to OPERABLE status within 24 hours or be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.

with one inoperable drywell air lock door inflatable seal system air flask pressure instrumentation channel, restore the inoperable channel to OPERABLE status within 7 days or verify air flask pressure to be > 100 psig at least once per 12 hours.

*See Special Test Exception 3.10.1.

SURVETLLANCE REQUIREMENTS

- 4.6.2.3 The drywell air lock shall be demonstrated OPERABLE:
 - a. Within 72 hours following each closing, except when the air lock is being used for multiple entries, then at least once per 72 hours, by verifying seal leakage rate less than or equal to 4.05 scf per hour when the gap between the door seals is pressurized to 3.0 psid.
 - b. By pressurizing the air lock to 19.2 psig and conducting an overall air lock leakage test at 3.0 psid and verifying that the overall air lock
 - 1. At least once per 6 months
 - Prior to establishing DRYWELL INTEGRITY when maintenance has been performed on the air lock that could affect the air lock sealing capability.
 - c. By verifying that only one door in the air lock can be opened at a time. prior to drywell entry if not performed within the past six months.
 - d. By verifying the door inflatable seal system OPERABLE by:
 - 1. At least once per 7 days verifying seal air flask pressure to be greater than or equal to 100 psig.
 - 2. At least once per 18 months conducting a seal pneumatic system leak test and verifying that system pressure does not decay more than 1 psig from 100 psig within 24 hours.

The provisions of Specification 4.0.2 are not applicable.

^{*} The requirement to pressurize the air lack to 19.2 psig need only be conducted at a frequency of at least once per 18 months.

DRYWELL VENT AND PURGE

FINAL DRAFT

LIMITING CONDITION FOR OPERATION

The drywell vent and purge system supply and exhaust valves shall be closed except, while in OPERATIONAL CONDITION 3, the drywell vent and purge system 24 inch valves may be open during operation of the drywell vent and purge mode of the containment cooling system for up to 90 hours per 365 days for the purpose of reducing drywell airborne radioactivity levels prior to and during personnel entries or for controlling drywell pressure. The drywell may be vented for up to 9 hours per 365 days in OPERATIONAL CONDITIONS 1 and 2, for controlling drywell pressure by opening the 24 inch drywell purge supply or exhaust valves; however, only one line may be open at a time.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2 and 3.

ACTION:

- in OPERATIONAL CONDITIONS 1 and 2 and the 36 inch primary containment purge system supply or exhaust valves open drywell vent and purge system valves or he in at least HOT SHUTDOWN within the next 12 hours.
- b. With the drywell vent and purge system supply or exhaust valves open during OPERATIONAL CONDITIONS 1 and 2 for more than 5 hours per 365 days, immediately close the drywell vent valves or be in at least HOT SHUTDOWN within the next 12 hours.
- c. With both the drywell purge supply and exhaust valves open at the same time in OPERATIONAL CONDITIONS 1 and 2, immediately isolate either the supply or exhaust line; otherwise, be in at least HOT SHUTDOWN within the next 12 hours.
- d. With the drywell vent or purge mode of the containment cooling system in operation, during OPERATIONAL CONDITION 3, for more than 90 hours per 365 days, immediately close the drywell vent and purge 24 inch valves or be in at least COLD SHUTDOWN within the next 24 hours.
- # Applicable for the period from initial criticality to 3 months of the
 the completion of the 15t refueling ordings, otherwise these values
 About the broked closed and verified to be closed on 1 to the
 These values shall be pealed closed until the qualification is

 # These values shall be pealed closed until the qualification is

SURVEILLANCE REQUIREMENTS

- 4.6.2.7 At least once per 7 days, determine the cumulative time that:
 - The drywell vent and purge system supply or exhaust valves have been open during OPERATIONAL CONDITIONS 1 and 2 during the past 365 days.
 - The drywell vent and purge mode of the containment excling system has been in operation during OPERATIONAL CONDITION 3 within the past



FINAL DRAFT

LIMITING CONDITION FOR OPERATION (Continued)

ACTION: (Continued)

- 2. With the suppression pool average water temperature greater than:
 - a) 95°F for more than 24 hours and THERMAL POWER greater than 1% of RATED THERMAL POWER, be in at least HOT SHUTDOWN within 12 hours and in COLD SHUTDOWN within the next 24 hours.
 - b) 110°F, place the reactor mode switch in the Shutdown position and operate at least one residual heat removal loop in the suppression pool cooling mode.
- With the suppression pool average water temperature greater than 120°F, depressurize the reactor pressure vessel to less than 200 psig within 12 hours.
- c. With only one suppression chamber water level indicator OPERABLE and/or with fewer than eight suppression pool water temperature indicators, one in each of eight locations, OPERABLE, restore the inoperable indicator(s) to OPERABLE status whithin 7 days crearly suppression chamber water level and/or temperature to be within the limits at least once per 12 hours.
- with no suppression chamber water level indicators OPERABLE and/or with fever than seven suppression pool water temperature indicators, covering at least seven locations, OPERABLE, restore at least one water level indicator and at least six water temperature indicators to OPERABLE status within 48 hours or be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.

SURVEILLANCE REQUIREMENTS

- 4.6.3.1 The suppression pool shall be demonstrated OPERABLE:
 - a. By verifying the suppression pool water volume to be within the limits at least once per 24 hours.
 - b. At least once per 24 hours, in OPERATIONAL CONDITION 1 or 2, by verifying the suppression pool average water temperature to be less than or equal to 95°F, except:
 - At least once per 5 minutes, during testing which adds heat to the suppression pool, by verifying the suppression pool average water temperature less than or equal to 105°F.

FINAL DRAFT

3/4.6.4 PRIMARY CONTAINMENT AND DRYWELL ISOLATION VALVES

LIMITING CONDITION FOR OPERATION

3.6.4 The primary containment and drywell isolation valves in Table 3.6.4-1 shall be OPERABLE with isolation times less than or equal to those shown in Table 3.6.4-1.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2, and 3

ACTION:

With one or more of the primary containment or drywell isolation valves shown in Table 3.6.4-1 inoperable, maintain at least one isolation valve OPERABLE in each affected penetration that is open and within 4 hours either:

- Restore the inoperable valve(s) to OPERABLE status, or
- Isolate each affected penetration by use of at least one deactivated automatic valve secured in the isolated position,* or
- 3. Isolate each affected penetration by use of at least one closed manual x least one closed manual

Otherwise, be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.

SURVEILLANCE REQUIREMENTS

- 4.6.4.1 Each isolation valve shown in Table 3.6.4-1 shall be demonstrated OPERABLE prior to returning the valve to service, after maintenance, repair or replacament work is performed on the valve or its associated actuator, control or power circuit, by cycling the valve through at least one complete cycle of full travel and verifying the specified isolation time.
- 4.6.4.2 Each automatic isolation valve shown in Table 3.6.4-1 shall be demonstrated OPERABLE during COLD SHUTDOWN or REFUELING at least once per 18 months by verifying that, on an isolation test signal, each automatic isolation valve actuates to its isolation position.
- 4.6.4.3 The isolation time of each power operated or automatic valve shown in Table 3.6.4-1 shall be determined to be within its limit when tested pursuant to Specification 4.0.5.

*Isolation valves closed to satisfy these requirements may be reopened on an intermittent basis under administrative controls.

The provisions of specification 3.0.4 are mat applicable provided that the affected penetration is esolated in accordance with ACTIETY 2:

RIVER BEND - UNIT 1, and provided that the associated APR 2 8 1962.

River BEND - UNIT 1 applicable, we declared inoperable and the applicable and the applicable.

ACTION statements for that suptem are performed

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

VALVE NUMBER	PENETRATION NUMBER	VALVE GROUP	ISOLATION TIME (Seconds)	SECOMDARY CONTAINMENT BYPASS PATH(+) (Yes/No)	
matic Ical	lation Wal				

a. Automatic Isolation Valves

1. Primary Containment (a) (Continued)

1G33*MOVF028	1KJ8*24	715	20.0	(6)
1G33*MOVF040	1KJB*Z6		20.9	Yes(f)
1G33*MOVF001(b)(J)	1KJ8*Z7	7 15	24.2	No
1G33*MOVF053(h) 1G33*MOVF034(h)	1KJB*Z129	7 16	19.8	No
1G33*MOVF034(h)	1KJB*Z4	7 15	5.5	No
1633*MOVF039(h)		7 15	20.9	Yes (f)
1G33*MOVF004(h)(J)	1KJB*Z6	7 15	24.2	No
1G33*MOVF054(h)	1KJB*Z7	7	6.6	No
1WCS*MOV178	1KJB*Z129	7 15	5.5	No
	1KJ8*Z5	1	12.1	Yes (f)
1WCS*MOV172	1KJ8*75	1	12.6	ves (f)
1E22*MOVF023(J)	1KJB*2.1	1	50	Yes (f)
IE12*MOVFO24A(J)	1KJB*Z24A	10		No
1E12*MOVFO11A(J)	1KJB*Z24A	10	63.8	No
1E21*MOVF012(J)	1KJ9*Z24A		34.1	No
1E12*#OVF024B(J)	1KJB*Z24B	10	57.2	No
1E12*MOVF011B(J)	1KJB*724B	10	63.8	No
1E12*MOVF021(J)		10	30.8	No
1SFC*MOV119	1KJB*Z24C	10	97.9	No
1SFC*MOV120	1KJ8226 1KJB#226	1	68	. No
15FC*MOV122	1KJB227 1KJB#227	1	62;7	No
	1KJB*Z27	1	63 8	
1SFC*MOV139	1KJ8220 1KJ8 * 228	1	39.6	No
1SFC*MOV121	1KJB220 1KJB#228	1	39.6	No
		- 3 844	37.0	No

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

	NUMBER	PENETRATION NUMBER	VALVE GROUP	ISOLATION TIME (Seconds)	SECONDARY CONTAINNENT BYPASS PATH(f) (Yes/No)
a	. Automatic Isol	ation Valves			
	1. Primary Co	ntainment(a) (Cont	inued)		
1DFR # 10 10 11 11 11 11 11 11 11 11 11 11 11	DFR*AOV102(b) DFR*AOV101(b) DER*AOV127(b) DER*AOV126(b) FPW*MOV121 SAS*MOV106 CCP*MOV138 CCP*MOV158 CCP*MOV159 SWP*MOV5A SWP*MOV5A SWP*MOV5B IVN*MOV128 IVN*MOV127 NS*MOV125	1KJB*735, 1 DRB 1KJB*235, 1 DRB 1KJB*238, 1 DRB 1KJB*238, 1 DRB 1KJB*241 1KJB*244 1KJB*246 1KJB*246 1KJB*249 1KJB*249 1KJB*253A 1KJB*253A 1KJB*253B 1KJB*2131 1KJB*2131 1KJB*2132	# 236 1 # 239 1	N/A N/A N/A 34.1 22.0 18.7 22.0 23.1 24.2 50.6 53.9 31.9 28.6 27.5 22.0	No No No No Yes (f) Yes (f) No No No No No Yes (f) Yes (f) Yes (f)

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

NUMBER	PENETRATION NUMBER	VALVE GROUP	ISOLATION TIME (Seconds)	SECONDARY CONTAINMEN BYPASS PATI
a. Automatic Iso	lation Valves			(Yes/No)
	ontainment (a) (Conti	inued)		
1E51*MOVF063(b) 1E51*MOVF076(b) 1E51*MOVF064 1E51*MOVF077 1E51*MOVF078 1HVR*A0V165 1HVR*A0V123 1HVR*A0V128 1HVR*A0V166	1KJB*Z15 1KJB*Z15 1KJB*Z15 1KJB*Z16 1KJB*Z17 1KJB*Z18B,C 1KJB*Z31 1KJB*Z31 1KJB*Z33	2 2 2 2 3 3 8 8 8	9.9 13.4 9.9 30.5 14.2 16.5 3	No No No No No No No
1SSR*SOV130 1SSR*SOV131	1KJB*Z501B 1KJB*Z601B	8 10 1 10 1	3 3 3	No No

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

à.	VALVE NUMBER Automatic Iso	PENETRATION NUMBER	VALVE GROUP	MAXIMUM ISOLATION TIME (Seconds)	SECONDARY CONTAINMENT BYPASS PAIH(+) (Yes/No)
	2. Drywell(k	(Continued)			
1CPM 1CPM 1CPM 1CPM 1CPM 1CPM 1B33	1*M0V2A 1*M0V4A 1*M0V4B 1*M0V3A 1*M0V1A 1*M0V3B 1*M0V1B *A0VF019	1DRB*Z57A 1DRB*Z57A 1DRB*Z57B 1DRB*Z57B 1DRB*Z58A 1DRB*Z58A 1DRB*Z58B 1DRB*Z58B 1DRB*Z58B 1DRB*Z449 1DRB*Z449	10 1 10 1 10 1 10 1 10 1 10 1 10 1 9	33 33 33 33 33 33 33 5	No No No No No No No

FINAL DRAF

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

VALVE

PENETRATION NUMBER

SECONDARY
CONTAINMENT
BYPASS PATH(#)
(Yes/No)

Manual Isolation Valves

1. Primary Containment(a)

1KJ8*721A	1KJB*221B	1KJB*2602A	1KJB*Z602B	1KJ8*26020	1KJR*Z602F	1KJB*Z603A	1KJB*2603A	1KJ8*2603C	JKJ8*Z603C	1KJ8*2605A	1KJ8*Z6058	1KJB*2606A	1KJB*2606B	1KJB*2606C	1KJB*26060	1KJB*2606E	1KJ8*2606F	1KJB*221A	1KJ8*2218	1KJB*253	1K.TR. 2F2	1KTR 3E3	18.38 # 2525
																				(6)	3(e)	(e)	(e)
1E12*F099A	1E12*F0998	BA. WALL	OIA.WANT	ILSV-V64	TI WC #VI Z	ILMS-VI4	ILMS VIZ	II MCAUIK	ICMC#U2	ICMC#U2	LAS AS	PIA NAME	Cuc ture	CMC ALLE	CIA AID	L SV V65	HVK-VIB	E124VE044B	15 VI 044B	SWP * 50V552A(e)	SWP . SOV5528 (e)	SWP . SOV552C (e)	SWP * 50V552 D(e)

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(Yes/No) CONTAINMENT SECONDARY

PENETRATION

CONTAINMENT AND DRYWELL ISOLATION VALVES

TABLE 3.6.4-1 (Continued)

NUMBER

NUMBER VALVE

Yes (f)

Primary Containment(a) (Continued)

Manual Isolation Valves

10R8*Z10

KJ8*29,

117*8CX KJ8*212

1E22*MCVF015(e)(J)
1E22*MOVF015(e)(J)
1E22*MOVF012(e)(J)
1E21*MOVF005(b)(e)
1E51*MOVF008(e)
1E51*MOVF018(e)(J)
1E51*MOVF013(b)(e)

1KJ8*Z38

87*8CX

K.38*23A

1FWS*MOV7A(e)

NO NO NO

10R8*Z130

KJ8*7119.

IKJ8*221A

1E12*HOVF027A(e) 1E12*HOVF042A(e) 1E12*HOVF027B(e)

1KJB*2218

1KJB*2218

1K.38*223A

1612*MOVF0428(e) 1612*MOVF042C(e) 1612*MOVF073A(e)(J) 1612*MOVF064A(e)(J) 1612*MOVF064A(e)(J) 1621*MOVF064A(e)(J) 1558*S0V139(e)

1KJB*221C

1KJB*223B

1KJB"221A

KJ8*218A

KJ8*217

10R8*214

IKJ8*213,

14.1842258 1KJB + 213B 1KJB*224A

1KJB*224A IKJB*2248

KJB*125A IKJB*224C KJB*2258

1E12*MOVF064B(e)(J) 1E12*MOVF004A(e)(J) 1E12*MOVF004A(e)(J) 1E12*MOVF004B(e)(J)

KJ8*225C

1KJB * 2.11

1DFR * MOVING (e)(J)

*

2 4 7990

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

VALVE	PE
NUMBER	

PENETRATION NUMBER

SECONDARY
CONTAINMENT
BYPASS PATH(+)
(Yes/No)

b. Manual Isolation Valves

1. Primary Containment (a) (Continued)

1C11*MOVF083(e)	14 104700
1(*P*MOV104(e)	1KJB*729
1cpp*HOV105(e)	1KJB*Z33
1SWP*MOV567A(e)	1KJ8*Z33
15WP MUV50/A(P)	1KJB*252A
15MP*MOV5078(e) 15MP*MOV81A(e)	1KJB*752B
ALBACHALIST	1KJB*Z53A
1SWP*MOVBIB(e)	1KJB*Z538
15W2*MOV503A(e)	1KJ8*Z53A
1SWP*MGV5038(e) 1SVV*MOV18(e)	1KJB*Z53B
ISVV*MOVIB(e)	1KJB*Z102
1SVV*MOVIA(E)	1KJB*7103
1CPP*SOV140(e)	1KJB*Z31
1CMS*50V350(e)	
1CMS*SOV318(e)	1KJB*Z601E
1CMS*SOV358(e)	1KJ8*Z601E
1CMS*SOV31D(e)	1KJB*Z601F
1CMS*SOV35C(e)	1KJB*7601F
1CM2,200,32(%)	1KJB*2605E
1CMS*SOV31A(e)	1KJB*Z605E
1CMS*SOV35A(e)	1KJB*2605F
1CMS*SOV31C(e)	1KJB*Z605F

No No No No No

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

VALVE NUMBER	PENETRATION NUMBER	SECONDAR; CONTAINMENT BYPASS PATH(+) (Yes/No)
b. Manual Isolation V	lalves	
2. Drywell(k)		
1SA5*V489	1DR8*Z45	
11AS*V79	10RB*Z47	No
1HVM*V542	10RB*Z54	No
15WP*V205	1DR8*Z54	No
JSWP*V206		No
1SVV*V53	10R8*Z55	No
1RCS*V132	10RB*7112	No
1RCS*V131	1088*7152	No
1RCS*V162	1DRB*Z153	No
1RCS*V156	1098*2154	No
1RCS*V187	1DRB^Z155	llo
1RCS*V186	10RB*Z156	No
IRCS*V217	1088*2157	No
RCS*V211	1DRB*Z158	No
ICHS*SOV34A(2)	1DR6*Z159	Ho
1CMS*SOV34B(e)	10R8*Z500	No
ICMS*SOV34C (e)	1DRB*Z430	No Proces
CMS*SOV34D (*)	1DR8*Z499	No.
	(P) 10R8*Z428	No No
1CM5*50V34A-1CM5 450V3:	1000 5333	No and American
CH3 30.326	1DR8*Z335 :	No In
		40 Pere
1 SVV * V50	1DRB # 2107	. 0
	20/10- 210/	No 30
		access.

14.0842234 1 K JB . 2 2 3 8

IKJB*2238

IE 12*RVI 6559 (6)

IE 12*RVF 025C (h)

KJB*2238

IKJB*723A KJB*223A Yes (#)

Yes (f)

TABLE 3.5.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

Drur	LENE	A 25 00	5
	•		
		a	=

BYPASS PATHEES

(Yes/No)

CONTAINMENT SECOMDARY

Other Isolation Valves

Primary Containment(a)

1KJB*23A

KJ8*23A 1KJ8*238 1KJ8*Z38

18 21 * V FO 10 A 1821 * AOV F 03 2 B 1821 * AOV F 03 2 B 1821 * AOV F 04 2 B 1821 * AOV F 010 B (b) 1822 * AOV F

3333

Mo No

KJ8*29, 10R8*219

117*8CX

KJB*211 113*8LX No No

1KJ8*Z19,10R8*Z130 1KJ8*Z19,10R8*Z130 1KJ8*Z19,10R8*Z130

No

1KJB*221C, 1DRB*222C

IKJ8*220

1KJB*223A IKJB*223A

IKJB*123A

1K.JB*223A KJB*223A IKJB*223A

1E22*RVF039(h) 1E21*A0VF006(b)(c) 1E51*A0VF065(b)(c) 1E51*A0VF066(b)(c) 1E22*RVF035(h.)

1612*A0VF041C(b)(c) IE12*RVF055A(L) 1E12*RVF025A(L) 1E12*RVF017A (4

IRHS*RV38 (L) 1E12*RVF005 1E21*RVF018 1£21*9VF031 1E12*RVF035

IWC S # RVI 4 4

IWCS * RVISY

1KJB# 24

1KJB#25

.

2 5

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

VALVE PENETRATION SECONDARY CONTAINMENT BYPASS PATH(+)

(Yes/No)

c. Other Isolation Valves

1. Primary Containment (a) (Continued)

1E12*RVF0258 (L)	1KJB*Z238	
1E12*RVF030(h)	1KJB*223B	
1E12*RVF101(L)	1KJB*Z238	
1E12*RVF017B(h)	1KJ8*7238	
1SFC*V101	1KJB*Z26	
15FC*V350		
1SFC*V351	1KJB*Z27	
1C11*VF122	1KJ8*Z28	
10ER*V4	1KJ8*Z29	
10FR*V180	1KJ8*Z38	
1FPW*V263	1KJ8*Z35	
1SAS*V486	1KJB*Z41	
11AS*V80	1KJB*Z44	
1CCP*V118	1KJB*Z46	
1CCP*V160	1KJB*Z48	
	1KJ8*Z49	
1SWP*V174	1KJB*Z52A	
15WP*V175	1KJB*Z52B	
15VV*V9	1KJB*Z102	
15VV*V31	1KJB*2103	i
1HVN*V1316	1KJ8*Z131	
IHVN*V541	1KJB*Z132	i
1CNS*V86	1KJB*Z134	1
	1400 7174	-0

No No No Yes (f) No Yes (f)

No No

No

No

No No

Yes (f) Yes (f) Yes (f)

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TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

	VALVE NUMBER	PENETRATION NUMBER	SECONDARY CONTAINMENT BYPASS PATH(+) (Yes/No)
С.	Other Isolation Valves		
	2. Drywell(k)		
	1*RVF047A	1DRB*7136	No

1B21*RVF047A	1000\$7136
1821*RVF041A	1DRB*Z136
1821*RVF051G	1DRA*Z137
1821*RVF041L	1DRB*Z138
1821*RVF047C	10RB*Z139
1021 RVF 04/L	10RB*Z140
1B21*RVF041G	1DRB*Z141
1821*RVF051C	1DR8*Z142
1B21*RVF041C	1DR8*Z143
1821*RVF047B	1DRB*Z144
1821*RVF0418	1DRB*Z145
1B21*RVF051B	1DRB*2146
1B21*RVF041F	1DRB*2147
1B21*RVF047F	10RB*7148
1821*RVF0410	
1821*RVF047D	10RB*7149
1821*RVF051D	1DRB*7150
1E12*AOVFO41A(C)	10RB*Z151
1E12*A0VF041B(c)	1DRB*122A
TETS MONITORING	1DRB*7228

No No No No No

No

No No

No

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Ne

No

No

No

No

No

No

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

15WP*RV119

1C41*VF006

1C41*VF007

1CCP*V133

1C41*VEXXF004A

1C41*VERXF004B

VALVE NUMBER	PENETRATION NUMBER	SECONDARY CONTAINMENT BYPASS PATH(+) (Yes/No)
c. Other Isolation	Valves	
2. Drywell(k) (Continued)	
1DFR*V4 1DFR*V3 1DFR*V1 1DFR*V2	10RB*Z37A 10RB*Z37A 10RB*Z37B 10RB*Z37B	No No No
10ER*V15 1DER*V16	1DRB*Z40A 1DRB*Z40A 1DRB*Z40B	No No
1DER*V17 1SAS*V487 11AS*V78 ICCP*V119	1G28*Z408 10R8*Z45 10R8*Z47	Ho Ho Ho
	1088*750	

1DR8*Z50

10R8*Z54

10R8*756

10RB*Z56

10RB*Z56

10R8*Z56

1088*751

SES 9 2 54

TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

VALVE NUMBER PENETRATION NUMBER SECOMDARY
CONTAINMENT
BYPASS PATH(+)
(Yes/No)

c. Other Isolation Valves

2. Drywell^(k) (Continued)

1821*VF036A	
1821*VF036F	1088*2107
	10RB*Z107
1821*VF036G	1DRB*2107
1821*VF036P	1DRB*Z107
1821*VF039C	1DRB*Z107
1B21*VF039H	10RB*Z107
1B21*VF039K	
1B21*VF0395	10RB*7107
1821*VF036J	1DRB*Z107
	10R8*Z112
1821*VF036L	1DR8*7112
1821*VF036M	1DRB*Z112
1821*VF036N	1DRB*Z112
1821*VF036R	10RB*2112
1821*VF0398	1DRB*Z112
1821*VF0390	
1821*VF039E	10RB*Z112
1833*VF013A	1DRB*Z112
	1DRB*Z133
1833*VF017A	1DRB*Z133
1833*VF013B	1DR6*Z135
1833*VF017B	10RB*Z135
1CMS*V41	10RB*Z427
1CMS*V40	
	10R8*7501

No No

No No No

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TABLE 3.6.4-1 (Continued)

CONTAINMENT AND DRYWELL ISOLATION VALVES

NOTES

- Subject to test pressure of 7.6 psig.
- (b) Also isolates the drywell.
- Testable check valve.
- Opens on isolation signal.
- Receives a remote manual isolation signal.
- This line is sealed by the penetration valve leakage control system, (PVL25).
- This valve sealed by the main steam positive leakage control system (MS-PLCS).
- (h) Not subject to Type C leakage tests. Values will be indicated with type A test. Also isolates on high nonregenerative heat exchanger outlet temperature (RWCU).
- Valve is hydrostatically leak tested. Valves 633*MOVF001 & F004 are the only velves from group 7 that isolate on the standby liquid control system initiation signal,
- (k) Test pressure not applicable to these valves.

CONTAINMENT SYSTEMS

SURVEILLANCE REQUIREMENTS (Continued)

c. At least once per 18 months:

1. Verifying that one standby gas treatment subsystem will draw down the Shield Building Annulus and the Auxiliary Building to greater than or equal to 0.3 and 0.25 inches of vacuum water tively, and,

2. Operating one standby gas treatment subsystem for one hour and maintaining the Shield Building annulus and the Auxiliary Building gauge and flow rate not exceeding 2000 and 5000 cfm, respectively.

3. Verifying that one Fuel Building ventilation subsystem will draw down the Fuel Building to greater than 0.25 inches of vacuum water gauge in less than or equal to 26 seconds, and

4. Operating one Fuel Building ventilation subsystem for one hour and maintaining greater than or equal to 0.25 inches of vacuum water gauge in the Fuel Building at anflow rate not exceeding 5000 cfm.

(and verify in leakage)

CONTAINMENT SYSTEMS

3/4.6.5 SECONDARY CONTAINMENT

SECONDARY CONTAINMENT INTEGRITY - FUEL BUILDING

LIMITING CONDITION FOR OPERATION

3.6.5.2 SECONDARY CONTAINMENT INTEGRITY - FUEL BUILDING shall-be minimained.

APPLICABILITY: OPERATIONAL CONDITIONS Operational Condition *

ACTION:

Without SECONDARY CONTAINMENT INTEGRITY - FUEL BUILDING suspend handling of irradiated fuel in the Fuel Building. The provisions of Specification 3.0.3 are not applicable.

SURVEILLANCE REQUIREMENTS

- 4.6.5.2 SECONDARY CONTAINMENT INTEGRITY FUEL BUILDING shall be demonstrated within 24 hours prior to and at least once per 7 days during handling of irradiated fuel in the Fuel Building by verifying that:
 - The pressure within the Fuel Building is less than or equal to 0.25 inches of vacuum water gauge.
 - b. All Fuel Building equipment hatch covers are installed.
 - c. At least one door in each access to the Fuel Building is closed except for routine entry and exit.
 - d. All Fuel Building penetrations, except the Fuel Building Ventilation System charcoal filtration system penetrations, required to be closed during Fuel Handling accident conditions are closed by valves, blind flanges, or dampers secured in position.

^{*}When irradiated fuel is being handled in the Fuel Building.

CONTAINMENT SYSTEMS

SECONDARY CONTAINMENT AUTOMATIC ISOLATION DAMPERS

LIMITING CONDITION FOR OPERATION

3.6.5.3 The secondary containment ventilation system automatic isolation dampers shown in Table 3.6.5.3-1 shall be OPERABLE with isolation times less than or equal to the times shown in Table 3.6.5.3-1.

APPLICABILITY: As shown in Table 3.6.5.3-1.

ACTION:

With one or more of the secondary containment ventilation system automatic isolation dampers shown in Table 3.6.5.3-1 inoperable, maintain at least one isolation damper OPERABLE in each affected penetration that is open, and within 8 hours either:

- a. Restore the inoperable damper(s) to OPERABLE status, or
- b. Isolate each affected penetration by use of at least one deactivated automatic damper secured in the isolation position, or
- c. Isolate each affected penetration by use of at least one closed manual valve or blind flange.

Otherwise, in OPERATIONAL CONDITION 1, 2 or 3, be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.

Otherwise, in Operational Condition *, suspend handling of irradiated fuel in the secondary containment, CORE ALTERATIONS and operations with a potential for draining the reactor vessel. The provisions of Specification 3.0.3 are not applicable.

Fuel Building

SURVEILLANCE REQUIREMENTS

4.6.5.3 Each secondary containment ventilation system automatic isolation damper shown in Table 3.6.5.3-1 shall be demonstrated OPERABLE:

a. Prior to returning the damper to service after maintenance, repair or replacement work is performed on the damper or its associated actuator, control or power circuit, by cycling the damper through at least one complete cycle of full travel and verifying the specified isolation time.

When irradiated fuel is being handled in the secondary containment and during the partitions and operations with a potential for draining the reactor vessel.

The protocomes exacute and 3.0.4 are not applicable protocold at the affected perstaction to established an accordance with ACTION 6.4 1/2.

RIVER BEND - UNIT 1

3/4 6-52

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CONTAINMENT SYSTEMS

FINAL DOAST

STANDBY GAS TREATMENT SYSTEM LIMITING CONDITION FOR OPERATION

3.6.5.4 Two independent standby gas treatment subsystems shall be OPERABLE.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2, and 3.

ACTION:

With one standby gas treatment subsystem inoperable, restore the inoperable subsystem to OPERABLE status within 7 days or in OPERATIONAL COMDITION 1, be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.

SURVEILLANCE REQUIREMENTS

- 4.6.5.4 Each standby gas treatment subsystem shall be demonstrated OPERABLE:
 - a. At least once per 31 days by initiating, from the control room, flow through the HEPA filters and charcoal adsorbers and verifying that the subsystem operates for at least 10 hours with the heaters

CONTAINMENT SYSTEMS

FINAL DRAFT

FUEL BUILDING VENTILATION LIMITING CONDITION FOR OPERATION

3.6.5.6 Two independent Fuel Building Ventilation Charcoal Filtration subsystems shall be OPERABLE, and in OPERATIONAL, CONDITION *, one operating in the emergency mode.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2, 3 and *.

ACTION:

- a. With one Fuel Building Ventilation Charcoal Filtration subsystem inoperable, restore the inoperable subsystem to OPERABLE status within 7 days, or:
 - In OPERATIONAL CONDITION 1, 2 or 3, be in at least HOT SHUTDOWN within the next 12 hours and in COLD SHUTDOWN within the following 24 hours.
- 2. In Operational Condition *, suspend handling of irradiated fuel in the secondary containment, CORE ALTERATIONS and operations with a potential for draining the reactor vessel. The provisions of Specification 3.0.3 are not applicable.
- b. With both Fuel Building Ventilation Charcoal Filtration subsystems inoperable or with one not operating in the emergency mode in Operational Condition 2, suspend handling of irradiated fuel in the endary containment, CORE ALTERATIONS or operations with a potential for draining the reactor vessel. The provisions of Specification 3.0.3. are not applicable.

SURVEILLANCE REQUIREMENTS

- 4.6.5.6 Each Fuel Building Ventilation Charcoal Filtration subsystem shall be demonstrate OPE: BLE:
 - a. At least once per 12 hours in OPERATIONAL CONDITION *, by verifying one Fuel Building Ventilation Charcoal Filtration System operation.
 - b. At least once per 31 days by initiating, from the control room, flow through the HEPA filters and charcoal adsorbers and verifying that the subsystem operates for at least 10 hours with the heaters GPERABLE.

*When irradiated fuel is being handled in the secondary containment and ouring CORE ALTERATIONS and operations with a potential for draining the reactor vessel.

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SURVEILLANCE REQUIREMENTS (Continued)

- c. At least once per 18 months or (1) after any structural maintenance on the HEPA filter or charcoal adsorber housings or (2) following painting, fire or chemical release in any ventilation zone communicating with the subsystem b/:
 - 1. Verifying that the subsystem satisfies the in-place penetration and bypass leakage testing acceptance criterion of less than 0.05%, using the test procedure guidance in Regulatory Positions C.5.a, C.5.c and C.5.d of Regulatory Guide 1.52, Revision 2, March 1978, and a system flow rate of 10,000 cfm ± 10%.
 - Verifying within 31 days after removal that a laboratory analysis of a representative carbon sample obtained in accordance with Regulatory Position C.6.b of Regulatory Guide 1.52, Revision 2, March 1978, meets the laboratory testing criteria of Regulatory Position C.6.a of Regulatory Guide 1.52, Revision 2, March 1978, for a methyl iodide penetration of less than 0.175%; and
 - Verifying a subsystem flow rate of 10,000 cfm ± 10% during system operation when tested in accordance with ANSI N510-1975.
- d. After every 720 hours of charcoal adsorber operation, by verifying within 31 days after removal that a laboratory analysis of a representative carbon sample obtained in accordance with Regulatory Position C.6.b of Regulatory Guide 1.52, Revision 2, March 1978, meets the laboratory testing criteria of Regulatory Position C.6.a of Regulatory Guide 1.52, Revision 2, March 1978, for a methyl iodide penetration of less than 0.175%.
- Te. At least once per 18 months by:
 - Performing a system functional test which includes simulated automatic actuation of the system throughout its emergency operating sequence for the:
 - a) LOCA, and Fuel Emidence
 - b) Annulus ventilation exhaust high radiation signal.
 - Verifying that the pressure drop across the combined HEPA filters and charcoal adsorber banks is less than 8 inches water gauge while the filter train is operating at a flow rate of 10,000 cfm ± 10%.
 - Verifying that the subsystem stats and isolation dampers actuate to isolate the normal flow path and to divert flow through the charcoal filters on each of the following test signals:

CONTAINMENT SYSTEMS

3/4.6.6 ATMOSPHERE CONTROL

PRIMARY CONTAINMENT HYDROGEN RECOMBINER SYSTEMS

LIMITING CONDITION FOR OPERATION

3.6.6.1 Two independent primary containment hydrogen recombiner systems shall be OPERABLE.

APPLICABILITY: OPERATIONAL CONDITIONS 1 and 2.

ACTION:

With one primary containment hydrogen recombiner system inoperable, restore the inoperable system to OPERABLE status within 30 days or be in at least HOT SHUTDOWN within the next 12 hours.

SURVEILLANCE REQUIREMENTS

4.6.6.1 Each primary containment hydrogen recombiner system shall be demon-

- a. At least once per 6 months by verifying, during a recombiner system functional test that the minimum heater sheath temperature increases to greater than or equal to 700°F within 90 minutes and montain the
- b. At least once per 18 months by:
 - Performing a CHANNEL CALIBRATION of all control room recombiner indication instrumentation and control circuits.
 - Verifying through a visual examination that there is no evidence of abnormal conditions within the recombiner enclosure; i.e., loose wiring or structural connections, deposits of foreign materials, etc.
 - 3. Verifying the integrity of all heater electrical circuits by performing a resistance-to-ground test within 30 minutes following the above required functional test. The resistance to ground for any heater phase shall be greater than or equal to 10,000 ohms.
 - 4. Verifying, during a recombiner system functional test, that the heater sheath temperature increases to greater than or equal to 1215°F within 5 hours and man Lac. If for 4 for

TABLE 3.5.6.3-1 HYDROGEN IGNITERS AND LOCATIONS

IGNITER*	DIVISION	ELEVATION	AZIMUTH	CENTERLINE OF REACTOR	
NORMALLY ACC	ESSIBLE			OF REACTOR	
Open Areas					
Containment					
1A 1B 2A 2B 3A 3B 4A 4B 5A 5B 6A 6B 7A 7B 8A 8B 9B 10B 11B 12A 12B 14A 15D 20B 22A 22B 23A 24B 24B 26B 27B 27B 27B 27B 27B 27B 27B 27		EL 255-0 EL 255-0 EL 255-0 EL 250-0 EL 239-0 EL 173-6 FL 173-6 FL 173-6 FL 173-6 EL 173-6 EL 173-6 EL 173-6 EL 173-6 EL 172-6 EL 150-0 EL 170-0 EL 170-0 EL 150-0 EL 170-0 EL 170-0	9.0 90.0 180.0 270.0 337.5 22.5 67.5 112.5 157.5 202.5 247.5 292.5 315.0 0.0 45.0 90.0 135.0 180.0 225.0 270.0 27.0 64.0 88.9 117.8 115.0 153.9 238.0 213.7 213.7 63.0 84.0 153.0 145.0 153.9 219.7 212.0 293.9 319.0 25.1 27.7 63.0 84.0 153.0 145.0 153.0 153.9 219.7 219.5	20.0' 20.0' 20.0' 20.0' 20.0' 38.0' 38.0' 38.0' 38.0' 38.0' 38.0' 38.0' 56.0'	×
*Prefix is 1HC	S*IGNOIA- for	11 / 4 / 4 / 4 / 4 / 4 / 4 / 4 / 4 / 4 /			

TABLE 3.6.6.3-1 (Continued)

HYDROGEN IGNITERS AND LOCATIONS

IGNITER*	DIVISION	ELEVATION	AZIMUTH	DIST. FROM CENTERLINE OF REACTOR
NORMALLY A	ACCESSIBLE (Continu	ued)		
Open Areas	3			
Containmen	nt (Continued)			
25A 25B 27A 27B 32A 32B 33A 33B 34A 34B	II II II II II II II	EL 159-6 EL 151-0 EL 151-0 153-4 EL 152-7 EL 126-0 130-0 EL 126-0 EL 126-0 EL 126-0 EL 126-0 EL 139-4	210.0 238.0 321.1 294.8 65.0 30.0 116.0 /15.0 90.0 180.0 209.0	50.0' 59.0' 50.0' 46.2' 52.3' 60.0' 53.4' 60.0' 60.0' 60.0' 47.0' 54.2'
358 38A	ıi I	EL 136-0	155.1 170.7	45.0
388 39A 39B -43A A3B 44A	II II II	EL 139-4 EL 126-0 EL 126-6 EL 130-0 EL 110-0 108-9 EL 110-0 108-0 EL 112-4 112-5	240.5 270.0 297.0 298.5 325.0 328.0 5.0 39.0	54.0' 60.0' 60.0' 51.3' 55.4' 49.8' 34.5' 49.8' 44.5'
448 45A 45B	II I	EL 111-3 109-0 EL 111-4 110-0 EL 112-5	90.0 95.0	49.8' 39.5'
46A 46B 47A	II I	EL 112-5 EL 112-5 EL 112-5	121.5 117.0 159.0 155.0 180.0 176.0 207.0 204.0	49.8' 44.5' 49.8' 44.5' 49.8' 41.5'
478 48A 48B	II I	EL 112-5 EL 111-4/09-6 EL 111-4/09-6	243.0 244.0 270.0 261.0 299.0 297.0	49.8' 39.5' 49.8' 39.5'

^{*}Prefix is 1HCS*IGNO1A- for all igniters.

TABLE 3.6.6.3-1 (Continued)

HYDROGEN IGNITERS AND LOCATIONS

IGNITER*	DIVISION	ELEVATION	AZIMUTH	DIST. FROM CENTERLINE
NORMALLY I	NACCESSIBLE		ALTHOUGH	OF REACTOR
Open Areas				-
Drywell				
28A 28B 29A 39B 30A 30B 40A 40B 41A 41B 42A 42B 49A 49B 50A 50B 51A 51B		EL 156-0 EL 156-0 EL 156-0 EL 156-0 EL 156-0 EL 138-8 EL 133-1 EL 139-10 EL 133-5 EL 138-11 EL 135-10 EL 116-8 EL 116-7 EL 116-7 EL 116-7 EL 116-6	0.0 58.5 125.0 180.0 233.0 306.0 293.3 359.2 60.4 129.9 179.0 240.0 354.5 66.8 113.4 180.0 247.3 292.9	24.8' 23.9' 33.9' 21.5' 25.0' 22.0' 21.0' 25.0' 21.6' 21.8' 23.0' 22.0' 26.0' 20.9' 21.2' 21.0' 20.8' 21.2'
	_			
RWCU Heat Exc	changer Room			
11A 21A 21B	1 1 1	EL 166-6 EL 165-0 167-4 EL 165-0 167-6	20.8 338.7 33 8 .1	50.5' 49.4' 48.0' 43.3' 43.4'
Contaminated	Equip. Store Room			43.4
13A 13B	II	EL 167-3 EL 167-3	52.1 123.6	29.2' 32.4'

^{*}Prefix is 1HCS*IGNO1A for all igniters.

TABLE 3.6.6.3-1 (Continued)

HYDROGEN IGNITERS AND LOCATIONS

IGNITER	211131011	ELEVATION	AZIMUTH	DIST.	RLINE
NORMALLY	INACCESSIBLE (Con	tinued)		OF REA	CTOR
	Areas (Continued)			-	
	trol Area				
164	-	40.00			
168		Et 173-0 Et 172-0	259.9	50.8	
RWCU Val	ve Nest and Pump Ro		290.9	53.0	
17A	1	170-6	298.4	40.0	
178	II	El. 172 0 EL 173 0	296.3	42.91	
RWCU Filt	er Demin A Room	172-0	242.5	38.5	
184	I				
188	ıi	EL 173-0 EL 173-0	235.3	31.6'	
RWCU Filt	er Demin B Room	173-0	260.1	23.3'	
19A	1		303.9	31.3'	
198	ΙΪ	EL 175-6 EL 174-6	286.1	27.11	
_ RWCU Backs	wash Room	1,40	282.3	23.5'	
26A	I	157-6			
268	II	EL 155-8 EL 150-0	247.5	49.6	
Main Steam	Tunnel	21 130-0	276.1	46.8'	
31A					
318	I	EL 126-0	341.9	51.5'	
SFC Piping	and Valve Area	EL 126-0	`17.4	53.5	
36A 36B	I	EL 136-0	166.2 166.3	56.4'	
	Hatch Area	EL 136-0	185.6	57.3'	
35A	ī				
358	п	EL 136-0	155.1	46.6'	
*Prefix is	1HCS*IGNO1A- for a	EL 136-0 11 igniters.	174.7	45.0'	

TABLE 3.6.6.3-1 (Continued) HYDROGEN IGNITERS AND LOCATIONS

IGNITER*	DIVISION INACCESSIBLE (Cont.	ELEVATION	AZIMUTH	DIST. FROM CENTERLINE OF REACTOR
	Areas (Continued)			-
	nsfer Tube Area			
37A 37B	II I	EL 135-0 EL 134-0	202.1	39.9"
Upper Fue	1 Pool Valve Room		201.3	49.4'
52A 52B	II	EL 179-3 EL 179-3	80.5 138.8	30.3'

^{*}Prefix is 1HCS*IGNO1A- for all igniters.

TABLE 3.6.6.3-2 HYDROGEN IGNITERS AND ASSOCIATED CIRCUITS## DIVISION I (a)

CIRCUIT 1	CIRCUIT 2	CIRCUIT 3	CIRCUIT 4	CIRCUIT 5
8A 7A 3A 4A	9A 10A 6A 5A 2A	49A# 50A# 41A# 29A# 28A#	51A# 42A# 40A# 30A#	44A 32A 33A 22A 11A# 13A#

CIRCUIT 6	CIRCUIT 7	CIRCUIT 8	CIRCUIT 9	CIRCUIT 10
46A 35A# 45A 23A 12A 14A	36A# 34A 25A 26A# 24A	37A# 48A 39A 17A# 16A	47A 38A 18A# 20A 15A	43A 31A# 27A 21A# 19A#

#Igniters in inaccessible areas ##Prefix is 1HCS*IGNO1A— for all igniters. (a)A minimum of 48 igniters shall be OPERABLE.

TABLE 3.6.6.3-2 (Continued)

HYDROGEN IGNITERS AND ASSOCIATED CIRCUITS## (Continued) DIVISION II(a)

CIRCUIT 1	CIRCUIT 2	CIRCUIT 3	CIRCUIT	
78 88 38 48 18	98 108 58 68 28	498# 508# 418# 408# 288#	51B# 42B# 29B# 30B#	438 318# 328 218# 118 528#

CIRCUIT 6	CIRCUIT 7	CIRCUIT 8	CIRCUIT 9	CIRCUIT 10
448 458 338 238 228 128	358# 368# 348 248 138# 148	468 258 178# 188# 158	378# 488 388 198#	478 398 268# 278 208

#Igniters in inaccessible areas ##Prefix is 1HCS*IGNO1A for all igniters. (a)A minimum of 48 igniters shall be OPERABLE. BASES

3/4.6.1 CONTAINMENT

3/4.6.1.1 and 3/4.6.1.2 PRIMARY CONTAINMENT INTEGRITY

PRIMARY CONTAINMENT INTEGRITY (OPERATING and FUEL HANDLING) ensures that the release of radioactive materials from the primary containment atmosphere will be restricted to those leakage paths and associated leak rates assumed in the accident analyses. This restriction, in conjunction with the leakage rate of 10 CFR Part 100 during accident conditions.

3/4.6.1.3 PRIMARY CONTAINMENT LEAKAGE

The limitations on primary containment leakage rates ensure that the total primary containment leakage volume will not exceed the value assumed in the accident analyses at the peak accident pressure of 7.6 psig, Pa. As an added to less than or equal to 0.75 La during performance of the periodic tests to between leakage tests.

Operating experience with the main steam line isolation valves has indicated that degradation has occasionally occurred in the leak tightness of the valves; therefore the special requirement for testing these valves.

The surveillance testing for measuring leakage rates is consistent with the requirements of Appendix J to 10 CFR 50 with the exception of exemption(s) granted for main steam isolation valve leak testing.

3/4.6.1.4 PRIMARY CONTAINMENT AIR LOCKS

The limitations on closure and leak rate for the primary containment air locks are required to meet the restrictions on PRIMARY CONTAINMENT INTEGRITY-tions 3.6.1.1 and 3.6.1.3. The specification makes allowances for the fact that there may be long periods of time when the air locks will be in a closed and secured position during reactor operation. Only one closed door in each air lock is required to maintain the integrity of the primary containment.