NUREG/CR-6600 ORNL/TM-13548

Neutron Exposure Parameters For Capsule 10.05 in the Heavy-Section Steel Irradiation Program Tenth Irradiation Series

Prepared by I. Remoe, C.A. Baldwin, F.B.K. Kam

Oak Ridge National Laboratory

Prepared for U.S. Nuclear Regulatory Commission



7810230175 981031 PDR NUREG CR-6600 R PDR

OFOZ

AVAILABILITY NOTICE

Availability of Reference Materials Cited in NRC Publications

NRC publications in the NUREG series, NRC regulations, and *Title 10, Energy,* of the *Code of Federal Regulations,* may be purchased from one of the following sources:

- The Superintendent of Documents U.S. Government Printing Office P.O. Box 37082 Washington, DC 20402-9328 <http://www.access.gpo.gov/su_docs> 202-512-1800
- The National Technical Information Service Springfield, VA 22161-0002 <http://www.ntis.gov/ordernow> 703-487-4650

The NUREG series comprises (1) technical and administrative reports, including those prepared for international agreements, (2) brochures, (3) proceedings of conferences and workshops, (4) adjudications and other issuances of the Commission and Atomic Safety and Licensing Boards, and (5) books.

A single copy of each NRC draft report is available free, to the extent of supply, upon written request as follows:

Address: Office of the Chief Information Officer Reproduction and Distribution Services Section U.S. Nuclear Regulatory Commission Washington, DC 20555-0001 E-mail: <GRW1@NRC.GOV> Facsimile: 301-415-2289

A portion of NRC regulatory and technical information is available at NRC's World Wide Web site:

<http://www.nrc.gov>

All NRC documents released to the public are available for inspection or copying for a fee, in paper, microfiche, or, in some cases, diskette, from the Public Document Room (PDR): NRC Public Document Room 2121 L Street, N.W., Lower Level Washington, DC 20555-0001 <http://www.nrc.gov/NRC/PDR/pdr1.htm> 1-800-397-4209 or locally 202-634-3273

Microfiche of most NRC documents made publicly available since January 1981 may be found in the Local Public Document Rooms (LPDRs) located in the vicinity of nuclear power plants. The locations of the LPDRs may be obtained from the PDR (see previous paragraph) or through:

<http://www.nrc.gov/NRC/NUREGS/ SR1350/V9/lpdr/html>

Publicly released documents include, to name a few, NUREG-series reports; *Federal Register* notices; applicant, licensee, and vendor documents and correspondence; NRC correspondence and internal memoranda; bulletins and information notices; inspection and investigation reports; licensee event reports; and Commission papers and their attachments.

Documents available from public and special technical libraries include all open literature items, such as books, journal articles, and transactions, *Federal Register* notices, Federal and State legislation, and congressional reports. Such documents as theses, dissertations, foreign reports and translations, and non-NRC conference proceedings may be purchased from their sponsoring organization.

Copies of industry codes and standards used in a substantive manner in the NRC regulatory process are maintained at the NRC Library, Two White Flint North, 11545 Rockville Pike, Rockville, MD 20852-2738. These standards are available in the library for reference use by the public. Codes and standards are usually copyrighted and may be purchased from the originating organization or, if they are American National Standards, from—

American National Standards Institute 11 West 42nd Street New York, NY 10036-8002 <http://www.ansi.org> 212-642-4900

DISCLAIMER

This report was prepared under an international cooperative agreement for the exchange of technical information. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for any third party's use, or the results of such use, of any information, apparatus, product, or process disclosed in this report, or represents that its use by such third party would not infringe privately owned rights.

NUREG/CR-6600 ORNL/TM-13548

Neutron Exposure Parameters For Capsule 10.05 in the Heavy-Section Steel Irradiation Program Tenth Irradiation Series

Manuscript Completed: March 1998 Dete Published: October 1998

Prepared by I. Remec, C.A. Baldwin, F.B.K. Kam

Oak Ridge National Laboratory Managed by Lockheed Martin Energy Research Corp. Oak Ridge, TN 37831-6285

E.M. Hackett, NRC Project Manager

Prepared for Division of Reactor Project Management Office of Nuclear Reactor Regulation U.S. Nuclear Regulatory Commission Washington, DC 20555-0001 NRC Job Code L1098



Abstract

This report describes the computational methodology for the least-squares adjustment of dosimetry data from the HSSI 10.05 capsule with neutronics calculations. It presents exposure parameters for the metallurgical specimens irradiated in the capsule. The exposure parameters reported are the neutron fluence greater than 1.0 MeV, fluence greater than 0.1 MeV, and displacements per atom. Exposure parameter distributions are also described in terms of three-dimensional fitting functions. When fitting functions are used, it is recommended that an uncertainty of 6% (10) be associated with the exposure parameters.

Contents

Abstract				 •	• •	• •	• •	•	 •	• •	•	• •	•	 •	• •	• •	• •	• •	• •	 •	• •		• •	•				• •		•	iii
List of Figure	s												•																		vii
List of Tables													•																		ix
Acknowledge	nents								 •				•							 											xi
Foreword					• •															 					 •						xiii
Introduction																				 										•	1
Experiment D	Descrip	otion		 																	•						 •				1
Analysis Met	hodolo	ogy .		 																											4
Results and I	Discus	sion		 										 •												 •			•		10
Conclusion			•••	 			*										• •					•			 						21
References				 												•									 						21
Appendix				 																	•				 						23

Figures

1	Arrangement of metallurgical specimens in the HSSI 10.05 capsule	2
2	Arrangement of gradient wires in the HSSI 10.05 capsule	3
3	Location of the HSSI 10.05 capsule relative to the reactor core	5
4	Location of the HSSI 10.05 capsule relative to the reactor core	6
5	Materials between the core and the HSSI 10.05 capsule	7
6	1T compact tension specimen with chevron notch	9

Tables

1	Constants determined for the three-dimensional fits of exposure parameters for the HSSI 10.05 and HSSI 10.0D capsules	11
2	Exposure parameters for the metallurgical specimens in the HSSI 10.05 capsule	11
A.1	Activities of the dosimeters in the HSSI 10.05 capsule	24
A.2	Irradiation history for the HSSI 10.05 capsule	29
A.3	Activities of the removable dosimeter tube (RDT) dosimeters	31

Acknowledgments

The authors wish to thank Ilana Siman-Tov of the Oak Ridge National Laboratory (ORNL) Engineering Technology Division for providing engineering data. Support for this work was provided by W. R. Corwin of the ORNL Metals and Ceramics Division, with programmatic funding from the U.S. Nuclear Regulatory Commission. This support was essential to accomplishing our objectives and is gratefully acknowledged.

Foreword

The work reported here was performed at the Oak Ridge National Laboratory (ORNL) under the Heavy-Section Steel Irradiation (HSSI) Program, T. M. Rosseel, Program Manager. The program is sponsored by the Office of Nuclear Regulatory Research of the U.S. Nuclear Regulatory Commission (NRC). The technical monitor for the NRC is M. G. Vassilaros.

This report is designated HSSI Report 18. Reports in this series are listed below:

- F. M. Haggag, W. R. Corwin, and R. K. Nanstad, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Irradiation Effects on Strength and Toughness of Three-Wire Series-Arc Stainless Steel Weld Overlay Cladding, USNRC Report NUREG/CR-5511 (ORNL/TM-11439), February 1990.
- L. F. Miller, C. A. Baldwin, F. W. Stallman, and F. B. K. Kam, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Neutron Exposure Parameters for the Metallurgical Test Specimens in the Sixth Heavy-Section Steel Irradiation Series*, USNRC Report NUREG/CR-5409 (ORNL/TM-11267), March 1990.
- S. K. Iskander, W. R. Corwin, and R. K. Nanstad, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Results of Crack-Arrest Tests on Two Irradiated High-Copper Welds*, USNRC Report NUREG/CR-5584 (ORNL/TM-11575), December 1990.
- R. K. Nanstad and R. G. Berggren, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Irradiation Effects on Charpy Impact and Tensile Properties of Low Upper-Shelf Welds, HSSI Series 2 and 3, USNRC Report NUREG/CR-5696 (ORNL/TM-11804), August 1991.
- R. E. Stoller, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Modeling the Influence of Irradiation Temperature and Displacement Rate on Radiation-Induced Hardening in Ferritic Steels, USNRC Report NUREG/CR5859 (ORNL/TM-12073), August 1992.
- R. K. Nanstad, D. E. McCabe, and R. L. Swain, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Chemical Composition RT_{NDT} Determinations for Midland Weld* WF-70, USNRC Report NUREG/CR-5914 (ORNL-6740), December 1992.
- R. K. Nanstad, F. M. Haggag, D. E. McCabe, S. K. Iskander, K. O. Bowman, and B. H. Menke, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Irradiation Effects* on Fracture Toughness of Two High-Copper Submerged-Arc Welds, USNRC Report NUREG/CR-5913 (ORNL/TM-12156/V1), October 1992.
- S. K. Iskander, W. R. Corwin, and R. K. Nanstad, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Crack-Arrest Tests on Two Irradiated High-Copper Welds, USNRC Report NUREG/CR-6139 (ORNL/TM-12513), March 1994.
- R. E. Stoller, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., A Comparison of the Relative Importance of Copper Precipitates and Point Defects in Reactor Pressure Vessel Embrittlement, USNRC Report NUREG/CR-6231 (ORNL/TM-6811), December 1994.

- D. E. McCabe, R. K. Nanstad, S. K. Iskander, and R. L. Swain, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Unirradiated Material Properties of Midland Weld WF-70, USNRC Report NUREG/CR-6249 (ORNL/TM-12777), October 1994.
- P. M. Rice and R. E. Stoller, Lockheed Martin Energy Systems, Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Microstructural Characterization of Selected AEA/UCSB Model FeCuMn Alloys*, USNRC Report NUREG/CR-6332 (ORNL/TM-12980), June 1996.
- J. H. Giovanola and J. E. Crocker, SRI International, Fracture Toughness Testing with Cracked Round Bars: Feasibility Study, USNRC Report NUREG/CR-6342 (ORNL/SUB/94-DHK60), to be published.
- F. M. Haggag and R. K. Nanstad, Lockheed Martin Energy Systems, Oak Ridge Natl. Lab., Oak Ridge, Tenn., Effects of Thermal Aging and Neutron Irradiation on the Mechanical Properties of Three-Wire Stainless Steel Weld Overlay Cladding, USNRC Report NUREG/CR-6363 (ORNL/TM-13047), May 1997.
- M. A. Sokolov and D. J. Alexander, Lockheed Martin Energy Systems, Oak Ridge Natl. Lab., Oak Ridge, Tenn., An Improved Correlation Procedure for Subsize and Full-Size Charpy Impact Specimen Data, USNRC Report NUREG/CR-6379 (ORNL/TM-13088), March 1997.
- S. K. Iskander and R. E. Stoller, Lockheed Martin Energy Research Corporation, Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Results of Charpy V-Notch Impact Testing* of Structural Steel Specimens Irradiated at ~30°C to 1 ×10⁶ neutrons/cm² in a Commercial Reactor Cavity, USNRC Report NUREG/CR-6399 (ORNL-6886), April 1997.
- S. K. Iskander, P. O. Milella, and A. Pini, Lockheed Martin Energy Research Corporation, Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Results of Crack-Arrest Tests on Irradiated A 503 Class 3* Steel, USNRC Report NUREG/CR-6447 (ORNL-6894), to be published.
- P. Pareige, K. F. Russell, R.E. Stoller, and M. K, Miller, Lockheed Martin Energy Research Corporation, Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Influence of Long-Term Thermal Aging on* the Microstructural Evolution of Nuclear Reactor Pressure Vessel Materials: An Atom Probe Study, USNRC Report NUREG/CR-6537 (ORNL/TM-13406), to be published.
- 18. This report.

The HSSI Program includes both follow-on and the direct continuation of work that was performed under the Heavy-Section Steel Technology (HSST) Program. Previous HSST reports related to irradiation effects in pressure vessel materials and those containing unirradiated properties of materials used in HSSI and HSST irradiation programs are tabulated below as a convenience to the reader.

C. E. Childress, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Fabrication History of the First Two 12-in.-Thick A-533 Grade B, Class 1 Steel Plates of the Heavy-Section Steel Technology Program, ORNL-4313, February 1969.

T. R. Mager and F. O. Thomas, Westinghouse Electric Corporation, PWR Systems Division, Pittsburgn, Pa., Evaluation by Linear Elastic Fracture Mechanics of Radiation Damage to Pressure Vessel Steels, WCAP-7328 (Rev.), October 1969. P. N. Randall, TRW Systems Group, Redondo Beach, Calif., Gross Strain Measure of Fracture Toughness of Steels, HSSTP-TR-3, Nov. 1, 1969.

L. W. Loechel, Martin Marietta Corporation, Denver, Colo., The Effect of Testing Variables on the Transition Temperature in Steel, MCR-69-189, Nov. 20, 1969.

W. O. Shabbits, W. H. Pryle, and E. T. Wessel, Westinghouse Electric Corporation, PWR Systems Division, Pittsburgh, Pa., Heavy-Section Fracture Toughness Properties of A533 Grade B Class 1 Steel Plate and Submerged Arc Weldment, WCAP-7414, December 1969.

C. E. Childress, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Fabrication History of the Third and Fourth ASTM A-533 Steel Plates of the Heavy-Section Steel Technology Program, ORNL-4313-2, February 1970.

P. B. Crosley and E. J. Ripling, Materials Research Laboratory, Inc., Glenwood, Ill., Crack Arrest Fracture Toughness of A533 Grade B Class 1 Pressure Vessel Steel, HSSTP-TR-8, March 1970.

F. J. Loss, Naval Research Laboratory, Washington, D.C., Dynamic Tear Test Investigations of the Fracture Toughness of Thick-Section Steel, NRL-7056, May 14, 1970.

T. R. Mager, Westinghouse Electric Corporation, PWR Systems Division, Pitosburgh, Pa., Post-Irradiation Testing of 2T Compact Tension Specimens, WCAP-7561, August 1970.

F. J. Witt and R. G. Berggren, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Size Effects and Energy Disposition in Impact Specimen Testing of ASTM A533 Grade B Steel, ORNL/TM-3030, August 1970.

D. A. Canonico, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Transition Temperature Considerations for Thick-Wall Nuclear Pressure Vessels, ORNL/TM-3114, October 1970.

T. R. Mager, Westinghouse Electric Corporation, PWR Systems Division, Pittsburgh, Pa., Fracture Toughness Characterization Study of A533, Grade B, Class 1 Steel, WCAP-7578, October 1970.

W. O. Shabbits, Westinghouse Electric Corporation, PWR Systems Division, Pittsburgh, Pa., Dynamic Fracture Toughness Properties of Heavy-Section A533 Grade B Class 1 Steel Plate, WCAP-7623, December 1970.

C. E. Childress, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Fabrication Procedures and Acceptance Data for ASTM A-533 Welds and a 10-in.-Thick ASTM A-543 Plate of the Heavy Section Steel Technology Program, ORNL-TM-4313-3, January 1971.

D. A. Canonico and R. G. Berggren, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Tensile and Impact Properties of Thick-Section Plate and Weldments*, ORNL/TM-3211, January 1971.

C. W. Hunter and J. A. Williams, Hanford Eng. Dev. Lab., Richland, Wash., Fracture and Tensile Behavior of Neutron-Irradiated A533-B Pressure Vessel Steel, HEDL-TME-71-76, Feb. 6, 1971.

C. E. Childress, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Manual for ASTM A533 Grade B Class 1 Steel (HSST Plate 03) Provided to the International Atomic Energy Agency, ORNL/TM-3193, March 1971.

P. N. Randall, TRW Systems Group, Redondo Beach, Calif., Gross Strain Crack Tolerance of A533-B Steel, HSSTP-TR-14, May 1, 1971.

C. L. Segaser, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Feasibility Study, Irradiation of Heavy-Section Steel Specimens in the South Test Facility of the Oak Ridge Research Reactor, ORNL/TM-3234, May 1971.

H. T. Corten and R. H. Sailors, University of Illinois, Urbana, Ill., *Relationship Between Material Fracture Toughness Using Fracture Mechanics and Transition Temperature Tests*, T&AM Report 346, Aug. 1, 1971.

L. A. James and J. A. Williams, Hanford Eng. Dev. Lab., Richland, Wash., Heavy Section Steel Technology Program Technical Report No. 21, The Effect of Temperature and Neutron Irradiation Upon the Fatigue-Crack Propagation Behavior of ASTM A533 Grade B, Class 1 Steel, HEDL-TME 72-132, September 1972.

P. B. Crosley and E. J. Ripling, Materials Research Laboratory, Inc., Glenwood, Ill., Crack Arrest in an Increasing K-Field, HSSTP-TR-27, January 1973.

W. J. Stelzman and R. G. Berggren, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Radiation Strengthening and Embrittlement in Heavy-Section Steel Plates and Welds, ORNL-4871, June 1973.

J. M. Steichen and J. A. Williams, Hanford Eng. Dev. Lab., Richland, Wash., High Strain Rate Tensile Properties of Irradiated ASTM A533 Grade B Class 1 Press e Vessel Steel, HEDL-TME 73-74, July 1973.

J. A. Williams, Hanford Eng. Dev. Lab., Richland, Wash., *The Irradiation and Temperature Dependence of Tensile and Fracture Properties of ASTM A533, Grade B, Class 1 Steel Plate and Weldment*, HEDL-TME 73-75, August 1973.

J. A. Williams, Hanford Eng. Dev. Lab., Richland, Wash., Some Comments Related to the Effect of Rate on the Fracture Toughness of Irradiated ASTM A553-B Steel Based on Yield Strength Behavior, HEDL-SA 797, December 1974.

J. A. Williams, Hanford Eng. Dev. Lab., Richland, Wash., The Irradiated Fracture Toughness of ASTM A533, Grade B, Class 1 Steel Measured with a Four-Inch-Thick Compact Tension Specimen, HEDL-TME 75-10, January 1975.

J. G. Merkle, G. D. Whitman, and R. H. Bryan, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., An Evaluation of the HSST Program Intermediate Pressure Vessel Tests in Terms of Light-Water-Reactor Pressure Vessel Safety, ORNL/TM-5090, November 1975.

J. A. Davidson, L. J. Ceschini, R. P. Shogan, and G. V. Rao, Westinghouse Electric Corporation, Pittsburgh, Pa., The Irradiated Dynamic Fracture Toughness of ASTM A533. Grade B, Class 1 Steel Plate and Submerged Arc Weldment, WCAP-8775, October 1976.

J. A. Williams, Hanford Eng. Dev. Lab., Richland, Wash., *Tensile Properties of Irradiated and Unirradiated Welds of A533 Steel Plate and A508 Forgings*, NUREG/CR-1158 (ORNL/SUB-79/50917/2), July 1979.

J. A. Williams, Hanford Eng. Dev. Lab., Richland, Wash., The Ductile Fracture Toughness of Heavy-Section Steel Plate, NUREG/CR-0859, September 1979.

K. W. Carlson and J. A. Williams, Hanford Eng. Dev. Lab., Richland, Wash., The Effect of Crack Length and Side Grooves on the Ductile Fracture Toughness Properties of ASTM A533 Steel, NUREG/CR-1171 (ORNL/SUB-79/50917/3), October 1979.

G. A. Clarke, Westinghouse Electric Corp., Pittsburgh, Pa., An Evaluation of the Unloading Compliance Procedure for J-Integral Testing in the Hot Cell, Final Report, NUREG/CR-1070 (ORNL/SUB-7394/1), October 1979.

P. B. Crosley and E. J. Ripling, Materials Research Laboratory, Inc., Glenwood, Ill., *Development of a Standard Test for Measuring K_{la} with a Modified Compact Specimen*, NUREG/CR-2294 (ORNL/SUB-81/7755/1), August 1981.

H. A. Domian, Babcock and Wilcox Company, Alliance, Ohio, Vessel V-8 Repair and Preparation of Low Upper-Shelf Weldment, NUREG/CR-2676 (ORNL/SUB/81-85813/1), June 1982.

R. D. Cheverton, S. K. Iskander, and D. G. Ball, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *PWR Pressure Vessel Integrity During Overcooling Accidents: A Parametric Analysis*, NUREG/CR-2895 (ORNL/TM-7931), February 1983.

J. G. Merkle, Union Carbide Corp. Nuclear Div., Oak Ridge Natl. Lab., Oak Ridge, Tenn., An Examination of the Size Effects and Data Scatter Observed in Small Specimen Cleavage Fracture Toughness Testing, NUREG/CR-3672 (ORNL/TM-9088), April 1984.

W. R. Corwin, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Assessment of Radiation Effects Relating to Reactor Pressure Vessel Cladding, NUREG/CR-3671 (ORNL-6047), July 1984.

W. R. Corwin, R. G. Berggren, and R. K. Nanstad, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Charpy Toughness and Tensile Properties of a Neutron Irradiated Stainless Steel Submerged-Arc Weld Cladding Overlay, NUREG/CR-3927 (ORNL/TM-9709), September 1984.

J. J. McGowan, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Tensile Properties of Irradiated Nuclear Grade Pressure Vessel Plate and Welds for the Fourth HSST Irradiation Series, NUREG/CR-3978 (ORNL/TM-9516), January 1985.

J. J. McGowan, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Tensile Properties of Irradiated Nuclear Grade Pressure Vessel Welds for the Third HSST Irradiation Series*, NUREG/CR-4086 (ORNL/TM-9477), March 1985.

W. R. Corwin, G. C. Robinson, R. K. Nanstad, J. G. Merkle, R. G. Berggren, G. M. Goodwin, R. L. Swain, and T. D. Owings, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Effects of Stainless Steel Weld Overlay Cladding on the Structural Integrity of Flawed Steel Plates in Bending, Series 1*, NUREG/CR-4015 (ORNL/TM-9390), April 1985.

W. J. Stelzman, R. G. Berggren, and T. N. Jones, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., ORNL Characterization of Heavy-Section Steel Technology Program Plates 01, 02, and 03, NUREG/CR-4092 (ORNL/TM-9491), April 1985.

G. D. Whitman, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., Historical Summary of the Heavy-Section Steel Technology Program and Some Related Activities in Light-Water Reactor Pressure Vessel Safety Research, NUREG/CR-4489 (ORNL-6259), March 1986.

R. H. Bryan, B. R. Bass, S. E. Bolt, J. W. Bryson, J. G. Merkle, R. K. Nanstad, and G. C. Robinson, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Test of 6-in.-Thick Pressure Vessels. Series 3: Intermediate Test Vessel V-8A — Tearing Behavior of Low Upper-Shelf Material*, NUREG-CR-4760 (ORNL-6187), May 1987.

D. B. Barker, R. Chona, W. L. Fourney, and G. R. Irwin, University of Maryland, College Park, Md., A Report on the Round Robin Program Conducted to Evaluate the Proposed ASTM Standard Test Method for Determining the Plane Strain Crack Arrest Fracture Toughness, K_{la}, of Ferritic Materials, NUREG/CR-4966 (ORNL/SUB/79-7778/4), January 1988.

L. F. Miller, C. A. Baldwin, F. W. Stallman, and F. B. K. Kam, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Neutron Exposure Parameters for the Metallurgical Test Specimens in the Fifth Heavy-Section Steel Technology Irradiation Series Capsules*, NUREG/CR-5019 (ORNL/TM-10582), March 1988.

J. J. McGowan, R. K. Nanstad, and K. R. Thoms, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Characterization of Irradiated Current-Practice Welds and A533 Grade B Class 1 Plate for Nuclear Pressure Vessel Service*, NUREG/CR-4880 (ORNL-6484/V1 and V2), July 1988.

R. D. Cheverton, W. E. Pennell, G. C. Robinson, and R. K. Nanstad, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Impact of Radiation Embrittlement on Integrity of Pressure Vessel Supports for Two PWR Plants*, NUREG/CR-5320 (ORNL/TM-10966), February 1989.

J. G. Merkle, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., An Overview of the Low-Upper-Shelf Toughness Safety Margin Issue, NUREG/CR-5552 (ORNL/TM-11314), August 1990.

R. D. Cheverton, T. L. Dickson, J. G. Merkle, and R. K. Nanstad, Martin Marietta Energy Systems, Inc., Oak Ridge Natl. Lab., Oak Ridge, Tenn., *Review of Reactor Pressure Vessel Evaluation Report for Yankee Rowe Nuclear Power Station (YAEC No. 1735)*, NUREG/CR-5799 (ORNL/TM-11982), March 1992.

Neutron Exposure Parameters for Capsule 10.05 in the Heavy-Section Steel Irradiation Program Tenth Irradiation Series

I. Remec, C. A. Baldwin, and F. B. K. Kam

Introduction

A variety of experiments and analyses for assessing the effects of neutron irradiation on metallurgical test specimens have been sponsored by the U.S. Nuclear Regulatory Commission (NRC). Results from these investigations provide information that will lead to an improved understanding of the processes of neutron damage to pressure vessels and other structural materials. Thus, the lifetime of many nuclear reactors may be extended through knowledge gained from these experiments, and confidence in the accuracy of information relative to the integrity of reactor pressure vessels and of related components should be enhanced.

Capsules in the Heavy-Section Steel Irradiation (HSSI) program Tenth Series are being irradiated at a new facility installed at the University of Michigan's Ford Nuclear Reactor in Ann Arbor, Michigan. Initially, an extensive dosimetry experiment (HSSI 10.0D) was carried out in the facility to assess the neutron irradiation exposure rates and their distributions. The dosimetry experiment included a steel block that simulated a typical metallurgical capsule with a comprehensive set of dosimeters placed in key locations throughout the block. Following the dosimetry experiment, capsule HSSI 10.05 was irradiated. It contained an assortment of Charpy and compact tension [C(T)] specimens as well as neutron dosimeters. The capsule was irradiated for a total of 3596 hours at the full reactor core power of 2 MW. The accumulated neutron fluence (E > 1 MeV) at the locations of the crack tips and V-notches of the metallurgical specimens ranged from 3.5×10^{18} cm⁻² to 1.6×10^{19} cm⁻².

This report describes the computational methodology for the least-squares adjustment of the dosimetry data from the HSSI 10.05 capsule with neutronics calculations. For the metallurgical specimens contained in the capsule, exposure parameters are reported in terms of the neutron fluence greater than 1.0 MeV, fluence greater than 0.1 MeV, and displacements per atom (dpa).

Experiment Description

The HSSI 10.05 capsule contained an assortment of metallurgical specimens and neutron dosimeters arranged in a steel frame assembly as shown in Figs. 1 and 2. The steel frame was constructed in such a way as to form 16 cells, each identified by its column (A-D) and row (1-4) number. The metallurgical complement in the capsule consisted of Charpy specimens that were 1 in. thick [1T C(T)] and 0.5 in. thick [0.5T C(T)]. The neutron dosimetry in the capsule included radiometric monitors in the form of iron gradient wires and fission-radiometric dosimetry sets (FRDSs). Each FRDS contained two epithermal dosimeters (⁵⁹Co and ¹⁰⁹Ag), two fission dosimeters (²³⁷Np and ²³⁸U), and three threshold dosimeters (⁵⁸Ni, ⁵⁴Fe, and ⁶³Cu), all covered with a 0.89-mm-thick (0.035-in.-thick) gadolinium cover. Three FRDSs were included in the capsule. One was placed in the vertical plate between cells B-1 and C-1, and the other two were placed in the horizontal plate between cells B-2 and B-3. The locations of the iron gradient wires are illustrated in Fig. 2. Some of the gradient wires were placed in the aligned



1

Figure 1. Arrangement of metallurgical specimens in the HSSI 10.05 capsule.

NUREG/CR-6600

1

2

0.

1



-

Figure 2. Arrangement of gradient wires in the HSSI 10.05 capsule.

3

NUREG/CR-6600

1

notches of the metallurgical specimens, as close to the notch tips as possible. Other gradient wires were incorporated into the frame of the capsule to provide additional information about the neutron flux distribution.

In addition to the dosimetry inside the capsule, Fe and Co/Al gradient wires were irradiated in small tubes placed just behind the thermal shield on each side of the capsule (see Fig. 3). These removable dosimeter tubes (RDTs) can be withdrawn and replaced as desired during the capsule irradiation and are included to assess variations in fluence rate magnitude, which could be caused if there were significant changes in the core loading. For capsule 10.05, the RDTs were replaced once, approximately halfway through the capsule irradiation period.

The relative location of the capsule with respect to the reactor core is shown in Figs. 3 and 4. Various materials between the core and the capsule are shown in Fig. 5. The coordinate system shown in Figs. 3 and 4 is used throughout this report where activities or irradiation exposure parameters are listed and is consistent with the coordinate system used in the analysis of the HSSI 10.0D capsule.¹

Analysis Methodology

To determine the neutron irradiation exposure parameters, a neutron spectrum adjustment procedure was used that combines transport calculations of the neutron field and measurements using radiometric monitors. The input data required in this analysis consisted of the following:

- neutron fluence rate spectrum from transport calculations at each dosimetry location,
- measured activity of each dosimeter,
- cross section for each dosimetry reaction used,
- · location of each dosimetry set, and
- response function for each irradiation exposure parameter.

For each of the dosimetry locations in the capsule, a 47-group neutron spectrum was calculated using a flux-synthesis method that combines the results of two-dimensional and one-dimensional transport-theory calculations. For the analysis of the HSSI 10.05 capsule, transport calculations performed by Williams' for the HSSI 10.0D capsule were used.¹

[&]quot;M. L. Williams, Louisiana State University, Nuclear Science Center, personal communication to F. B. K. Kam.

ORNL-DWG 98-3487



WEST FACE

Figure 3. Location of the HSSI 10.05 capsule relative to the reactor core-horizontal cross section.

NUREG/CR-6600

NORTH FACE



Figure 4. Location of the HSSI 10.05 capsule relative to the reactor core-vertical cross section.

ORNL-DWG 98-3489



Figure 5. Materials between the core and the HSSI 10.05 capsule.

During capsule disassembly one gradient wire from cell A-1 was lost and the center horizontal gradient wire, X-2, jammed in its groove and could not be removed. All remaining dosimeters were recovered and measured. Before being counted with a high-resolution gamma-ray spectrometer, the gradient wires were cut into 2.54-cm (1-in.) or 1.27-cm (0.5-in.) pieces and weighed. Dosimeters in the FRDSs were precut and weighed before irradiation and required no additional preparation. The specific activities of the neutron dosimeters at the end of irradiation are given in the Appendix. The identifiers (IDs) for the gradient wires irradiated in the notches of the metallurgical specimens consist of the cell ID followed by the wire number and the piece number (e.g., A1-111-1 is a wire from cell A1, the wire number is 111, and the piece number is 1; this wire is shown in Fig. 2 in the top right corner of the capsule). IDs of wires irradiated inside the steel frame of the capsule consist of wire ID and piece number only. Table A.1 in the Appendix lists for each dosimeter the ID, the coordinates (x, y, and z), and the specific activity at the end of irradiation.

The 1T C(T) and 0.5T C(T) specimens used in the HSSI 10.05 capsule had chevron notches, as shown in Fig. 6. Because of the chevron shape of the notch, the thickness of steel between a gradient wire and the face of the capsule changes along the notch. Therefore, gradient wires located in the C(T) specimen notch tips experience a varying neutron flux caused by attenuation in the steel. The result is that the activation of the wire is greater than it would have been if the gap had been filled with steel. In the neutronics calculations, the interior of the capsule was modeled as a solid block of steel. If the presence of the gap were neglected in the adjustment calculations, the irradiation parameters derived from the procedure would be overestimated. To circumvent this difficulty, "effective" Y coordinates were calculated for gradient wires located in the C(T) specimen notch tips. The effective Y coordinates were obtained by using the average thickness of the steel in front of the gradient wires. The effective Y coordinate used for each dosimeter is listed in a footnote to Table A.1. The introduction of the effective coordinate is of course an approximation. Its suitability was assessed through a comparison of irradiation parameters from two separate adjustment runs. In one run, all the available dosimetry

measurements, including the gradient wires from CT specimens with the effective Y coordinates, were used. In the second adjustment run the gradient wires from CT specimens were not used. The adjusted fast flux values were calculated for all the locations of the dosimeters (as used in the first run). The differences in the fast neutron flux from the two runs were very small (on the order of a few tenths of a percent) at almost all locations. Higher differences (2 to 3%, with a maximum difference of 3.2%) were found at only a few locations, and in all cases they remained smaller than the standard deviation (10) of the adjusted fast flux. Therefore, the previously described approximation used for the gradient wires irradiated in CT specimens appears to be adequate.

The activation cross-section library and covariance information in 640 energy groups was created from the IRDF 90 and ENDF V dosimetry files. To account for the gadolinium cover, a modified set of cross sections was generated; the 640-group cross sections were multiplied by attenuation factors defined as:

(1)

 $AF = \exp \left[-\left(D \times AV/AT\right) \times TH \times CS\right],$

where

- AF = attenuation factor,
- D = density of cover material (7.9004 g/cm³ for Gd),
- AV = Avogadros number,
- AT = atomic weight (157.25 for Gd),
- TH = thickness of the cover (0.89 mm, 35 mil),
- CS = total absorption cross section of Gd (taken from the IRDF 90 file).

This formula is, of course, a crude approximation only and does not consider the geometry of the covers and the dosimeters. However, it appears to be reasonably accurate for the current application. The resulting cross sections were combined with the cross sections for bare dosimeters and were converted to 32 energy groups for use in the adjustment runs. Cross-section covariance matrixes were also converted to the 32-group structure. The computer code FLXPRO from the LSL-M2 code package was used for this purpose.²

Measured activities were converted to reaction rates by taking into account the reactor power vs time history of the irradiation. The computer code ACT from the LSL-M2 code package was used for this purpose.² The reactor power vs time history for the irradiation of the HSSI 10.05 capsule is given in Table A.2 of the Appendix.

The spectrum covariance matrix used for the adjustment runs was originally calculated for the simulated surveillance capsule position of the Oak Ridge Research Reactor Poolside Facility Metallurgical Experiment.^{3,4} The original calculation of the fluence variance-covariances covered only the range from 18 to 0.1 MeV. Therefore, two energy groups from 1.0×10^{-5} to 0.1 eV and from 0.1 eV to 0.1 MeV were added, with large variances of 150% and 75%, respectively, and small correlations of 0.1 and 0.2. The spectrum covariance matrix was converted in the group structure used in the adjustment with the computer code FLXPRO. Obviously the assumed spectrum variance-covariance information is only approximate; however, it does not appear to be critical for the analysis since comprehensive dosimetry measurements are available. In such cases the adjustment results are generally not sensitive to the details in the spectrum covariance matrix.



Figure 6. 1T compact tension specimen with chevron notch.

9

For the least-squares neutron spectrum adjustment calculations, computer code LSL-M2 was used. The adjustment runs provided the adjusted neutron spectrum at each dosimetry location. The neutron irradiation exposure rates selected to characterize the irradiation conditions were neutron fluence rate with energy greater than 1 MeV ($F_{E>1 MeV}$), neutron fluence rate with energy greater than 0.1 MeV ($F_{E>0.1 MeV}$), and dpa rate. Fluence rates, $F_{E>1 MeV}$ and $F_{E>0.1 MeV}$, were obtained as sums of group fluxes over the corresponding energy range. The dpa rate calculations required that cross sections taken from American Society for Testing and Materials (ASTM) E-693 be folded with the corresponding group fluxes and summed.⁵ These exposure parameters were determined for each dosimetry location.

Results and Discussion

The exposure parameters at each dosimeter location obtained from the adjustment runs were fitted to a three-dimensional function. Describing the spacial variation of the irradiation parameters by means of a fitting function is desirable because the values of exposure parameters are often needed at locations other than the dosimetry locations. The function used for fitting the irradiation parameters was of the form

$$F(x, y, z) = A \cos [B_x (x - x_0)] \cos [B_z (z - z_0)] \exp (-\lambda y).$$
⁽²⁾

The constants A, B_x , x_0 , B_z , z_0 , and λ were determined with least-squares fitting and are listed in Table 1 for each of the three irradiation parameters. Constants obtained for the HSSI 10.0D capsule are also listed in Table 1 for comparison. The fluence E > 1 MeV, fluence E > 0.1 MeV, and dpa for each metallurgical specimen were calculated using Eq. 2 and the capsule irradiation time of 3595.8 hours. The results are tabulated in Table 2 along with the specimen ID, specimen type, and coordinates. Exposure parameters at any other location (*x*, *y*, or *z*) can be readily calculated using Eq. 2 and the capsule irradiation time. The coordinates of the point where exposure parameters are needed must be given relative to the coordinate system shown in Figs. 3 and 4.

The normalization constants (A) obtained for the HSSI 10.05 capsule ranged from 7 to 10% less than comparable normalization constants obtained for the HSSI 10.0D capsule. The attenuation coefficients (λ) obtained for the HSSI 10.05 capsule also ranged from 9 to 19% less than comparable coefficients obtained for the HSSI 10.0D capsule. These differences in normalization constants and attenuation coefficients appear to be larger than one would expect. However, when irradiation parameters inside the capsule are calculated, the effects of the smaller normalization constants for the HSSI 10.05 capsule attenuation coefficients. To evaluate the effect of the different constants, the irradiation parameters for the metallurgical specimens in the HSSI 10.05 capsule were calculated using both sets of fitting constants. The maximum difference found at any metallurgical specimen location was 5.3%. Therefore, even though the differences in individual fitting parameters from the two experiments appear to be larger, the two sets of fitting parameters, when used in Eq. 2, give exposure parameters that are in good agreement.

	(A) Fitting pa	arameters for	FENIMEV		
A	B _x	x _o	B _z	z _o	λ
(cm ⁻² s ⁻¹)	(cm ⁻¹)	(cm)	(cm ⁻¹)	(cm)	(cm ⁻¹)
1.865 E+12	0.05995	5.525	0.04182	1.752	0.1548
2.021 E+12	0.06082	5.071	0.04252	2.030	0.1707
	(B) Fitting pa	rameters for	F E > 0.1 MeV		
A	B _x	x _o	B _z	z _o	λ
(cm ⁻² s ⁻¹)	(cm ⁻¹)	(cm)	(cm ⁻¹)	(cm)	(cm ⁻¹)
4.409 E+12	0.06761	3.808	0.04265	1.737	0.1039
4.887 E+12	0.06920	3.303	0.04337	1.706	
	(C) Fitting pa	rameters for	r dpa rate		
A	B _x	x _o	B _z	z _o	λ
(s ⁻¹)	(cm ⁻¹)	(cm)	(cm ⁻¹)	(cm)	(cm ⁻¹)
2.679E-09	0.06259	4.812	0.04213	1.751	0.1377
	A (cm ⁻² s ⁻¹) 1.865 E+12 2.021 E+12 2.021 E+12 A (cm ⁻² s ⁻¹) 4.409 E+12 4.887 E+12 A.887 E+12 A (s ⁻¹) 2.679E-09 2.800E 00	(A) Fitting part (A) Fitting part (cm ⁻² s ⁻¹) (cm ⁻¹) 1.865 E+12 0.05995 2.021 E+12 0.06082 (B) Fitting part (B) Fitting part (Cm ⁻² s ⁻¹) (cm ⁻¹) 4.409 E+12 0.06761 4.887 E+12 0.06920 (C) Fitting part (C) Fitti	(A) Fitting parameters for A B _x x ₀ (cm ⁻² s ⁻¹) (cm ⁻¹) (cm) 1.865 E+12 0.05995 5.525 2.021 E+12 0.06082 5.071 (B) Fitting parameters for A B _x x ₀ (cm ⁻² s ⁻¹) (cm ⁻¹) (cm) 4.409 E+12 0.06761 3.808 4.887 E+12 0.06920 3.303 (C) Fitting parameters for A B _x x ₀ (cm ⁻¹) (cm) 2.679E-09 0.06259 4.812	(A) Fitting parameters for F Ext MeV A Bx x_0 Bz (cm ⁻² s ⁻¹) (cm ⁻¹) (cm) (cm ⁻¹) 1.865 E+12 0.05995 5.525 0.04182 2.021 E+12 0.06082 5.071 0.04252 (B) Fitting parameters for F E>0.1 MeV A Bx x_0 Bz (Cm ⁻² s ⁻¹) (cm ⁻¹) (cm) (cm ⁻¹) 4.409 E+12 0.06761 3.808 0.04265 4.887 E+12 0.06920 3.303 0.04337 (C) Fitting parameters for dpa rate A Bx x_0 Bz (C) Fitting parameters for dpa rate A Bx x_0 Bz (C) Fitting parameters for dpa rate A Bx x_0 Bz (S ⁻¹) (cm ⁻¹) (cm) (cm ⁻¹) 2.679E-09 0.06259 4.812 0.04213 2.800E 00 0.06259 4.812 0.04213	(A) Fitting parameters for F Exit MeV A Bx x_0 Bz z_0 (cm ⁻² s ⁻¹) (cm ⁻¹) (cm) (cm ⁻¹) (cm) 1.865 E+12 0.05995 5.525 0.04182 1.752 2.021 E+12 0.06082 5.071 0.04252 2.030 (B) Fitting parameters for F E>0.1 MeV A Bx x_0 Bz z_0 (cm ⁻² s ⁻¹) (cm ⁻¹) (cm) (cm ⁻¹) (cm) 4.409 E+12 0.06761 3.808 0.04265 1.737 4.887 E+12 0.06920 3.303 0.04337 1.706 (C) Fitting parameters for dpa rate A Bx x_0 Bz z_0 (C) Fitting parameters for dpa rate A B_x x_0 Bz z_0 (C) Fitting parameters for dpa rate A B_x x_0 B_z z_0 (S ⁻¹) (cm ⁻¹) (cm) 0.06259 4.812 0.04213 1.7

Table 1. Constants determined for the three-dimensional fits' of exposure parameters for the HSSI 10.05 and HSSI 10.0D capsules'

 $F(x, y, z) = A \cos [B_x (x - x_0)] \cos [B_z (z - z_0)] \exp (-\lambda y)$.

Table 2. Exposure parameters for the metallurgical specimens in the HSSI 10.05 capsule.

	Specimen		Co	oordinate	S	Flu	California de la Calenda de	
Block	ID	Туре	X (cm)	Y (cm)	Z (cm)	(E > 1 MeV) (cm ⁻²)	(E > 0.1 MeV) (cm ⁻²)	dpa
A1	2CD0	Charpy	-10.83	3.66	26.09	4.00E+18	1.09E+19	6.06E-03
A1	2CD1	Charpy	-10.83	3.66	25.09	4.27E+18	1.16E+19	6.48E-03
A1	2CD2	Charpy	-10.83	3.66	24.09	4.53E+18	1.24E+19	6.88E-03
A1	2CD3	Charpy	-10.83	3.66	23.09	4.78E+18	1.31E+19	7.27E-03
A1	2CD4	Charpy	-10.83	3.66	22.09	0.03E+18	1.38E+19	7.65E-03
A1	2CD5	Charpy	-10.83	3.66	21.09	5.26E+18	1.45E+19	8.02E-03
A1	2CD6	Charpy	-9.83	3.66	26.09	4.35E+18	1.20E+19	6.61E-03
A1	2CD7	Charpy	-9.83	3.66	25.09	4.65E+18	1.28E+19	7.07E-03
A1	2CD8	Charpy	-9.83	3.66	24.09	4.93E+18	1.36E+19	7.51E-03
A1	2CD9	Charpy	-9.83	3.66	23.09	5.20E+18	1.45E+19	7.93E-03
A1	2CD10	Charpy	-9.83	3.66	22.09	5.47E+18	1.52E+19	8.35E-03
A1	2CD11	Charpy	-9.83	3.66	21.09	5.72E+18	1.60E+19	8.75E-03
A1	02D01	Charpy	-8.74	3.66	26.09	4.72E+18	1.31E+19	7.18E-03
A1	02D02	Charpy	-8.74	3.66	25.09	5.03E+18	1.40E+19	7.68E-03
A1	02D03	Charpy	-8.74	3.66	24.09	5.34E+18	1.49E+19	8.16E-03
A1	02D04	Charpy	-8.74	3.66	23.09	5.64E+18	1.58E+19	8.62E-03
A1	02D06	Charpy	-8.74	3.66	22.09	5.93E+18	1.67E+19	9.07E-03
A1	02D08	Charpy	-8.74	3.66	21.09	6.20E+18	1.75E+19	9.50E-03

Table 2. (continued)

	Specimen	NAME AND ADDRESS OF A DESCRIPTION OF A D	Co	ordinate	S	Flu	ence	
Block	ID	Type	X	Y	Z	(E > 1 MeV)	(E > 0.1 MeV)	
DIUCK	10	1)00	(cm)	(cm)	(cm)	(cm ⁻²)	(cm ⁻²)	dpa
A 4	2050	Charny	-7.65	3.66	26.09	5.06E+18	1.41E+19	7.72E-03
AI	ZCEU	Charpy	7.65	3.66	25.09	5.40E+18	1.52E+19	8.25E-03
A1	ZCET	Charpy	7.65	3.66	24.00	573E+18	161E+19	8.77E-03
A1	ZCEZ	Charpy	7.05	3.66	23.00	6 05E+18	171E+19	9.27E-03
A1	2CE3	Charpy	-7.00	3.00	23.00	6 365+18	1 80E+19	9 75E-03
A1	2CE4	Charpy	-7.00	3.00	22.09	0.30E+10	1 905+10	1 02E-02
A1	2CE5	Charpy	-7.65	3.66	21.09	0.000010	1.092+19	9 105 03
A1	2CE6	Charpy	-6.65	3.66	26.09	5.305+10	1.502+19	0.160-00
A1	2CE7	Charpy	-6.65	3.66	25.09	5.72E+18	1.612+19	8.752-03
A1	2CE8	Charpy	-6.65	3.66	24.09	6.07E+18	1.72E+19	9.29E-03
A1	2CE9	Charpy	-6.65	3.66	23.09	6.40E+18	1.82E+19	9.82E-03
A1	2CE10	Charpy	-6.65	3.66	22.09	6.73E+18	1.92E+19	1.03E-02
A1	2CE11	Charpy	-6.65	3.66	21.09	7.05E+18	2.01E+19	1.08E-02
Δ1	MWGHD	1TCT	-7.44	3.45	17.53	7.96E+18	2.26E+19	1.22E-02
A1	MW9HB	1TCT	-10.03	3.45	17.53	6.66E+18	1.85E+19	1.02E-02
B1	MW15A.11	Charpy	-5.00	3.66	26.09	5.81E+18	1.64E+19	8.88E-03
DI	MANA/15ALA	Charny	-5.00	3.66	25.09	6.19E+18	1.76E+19	9.48E-03
DI	MANA/45AIS	Charpy	-5.00	3.66	24.09	6.57E+18	1.87E+19	1.01E-02
B1	MW15AG5	Charpy	-5.00	3.66	23.09	6.94E+18	1.98E+19	1.06E-02
	MANAEACA	Charpy	-5.00	3.66	22.09	7 29E+18	2.09E+19	1.12E-02
BI	MVV15AG1	Charpy	-5.00	3.66	21.00	7 63E+18	2 19E+19	1.17E-02
81	MVV15BF2	Charpy	-5.00	3.00	21.00	1.002.10	2.102.10	
B1	MW15BG3	Charpy	-4.00	3.66	26.09	6.05E+18	1.71E+19	9.25E-03
B1	MW15B11	Charpy	-4.00	3.66	25.09	6.45E+18	1.83E+19	9.88E-03
B1	MW15AG3	Charpy	-4.00	3.66	24.09	6.85E+18	1.95E+19	1.05E-02
B1	MW/15815	Charpy	-4.00	3.66	23.09	7.23E+18	2.07E+19	1.11E-02
D1	M/A/15010	Charpy	-4 00	3.66	22.09	7.60E+18	2.18E+19	1.17E-02
B1	MW15BJ2	Charpy	-4.00	3.66	21.09	7.95E+18	2.29E+19	1.22E-02
04	02017	Charpy	-2.01	3.66	26.09	6 29E+18	1.78E+19	9.62E-03
DI	02017	Charpy	2.01	3.66	25.09	671E+18	1.91E+19	1.03E-02
81	02018	Charpy	-2.91	3.00	24.00	7 125+18	2035+19	1 09E-02
BI	02019	Charpy	-2.91	3.00	22.00	7.525+18	2 15 = + 10	1 15E-02
B1	02D20	Charpy	-2.91	3.00	23.08	7.022+10	2.75+10	1 21 5-02
B1	02D23	Charpy	-2.91	3.00	22.05	0.075+10	2.275+10	1 275.02
B1	02D25	Charpy	-2.91	3.66	21.09	8.2/E+18	2.302+19	1.275-02
B1	MW11AJ3	Charpy	-1.82	3.66	26.09	6.50E+18	1.84E+19	9.94E-03
B1	MW15AF2	Charpy	-1.82	3.66	25.09	6.94E+18	1.97E+19	1.06E-02
B1	MW9AB4	Charpy	-1.82	3.66	24.09	7.36E+18	2.10E+19	1.13E-02
B1	MW9BA2	Charpy	-1.82	3.66	23.09	7.77E+18	2.22E+19	1.19E-02
B1	MW9BB4	Charpy	-1.82	3.66	22.09	8.17E+18	2.34E+19	1.25E-02
B1	MW9AB1	Charpy	-1.82	3.66	21.09	8.55E+18	2.46E+19	1.31E-02
B1	MW11BF5	Charpy	-0.82	3.66	26.09	6.68E+18	1.88E+19	1.02E-02
B1	MW118G3	Charpy	-0.82	3.66	25.09	7.12E+16	2.02E+19	1.09E-02
B1	MW11812	Charpy	-0.82	3.66	24.09	7.56E+18	2.15E+19	1.16E-02
B1	MW11814	Charpy	-0.82	3.66	23.09	7.98E+18	2.28E+19	1.22E-02
B1	MW11BI5	Charpy	-0.82	3.66	22.09	8.38E+18	2.40E+19	1.29E-02
B1	MW11BJ1	Charpy	-0.82	3.66	21.09	8.78E+18	2.52E+19	1.35E-02
P1	MMAILER	ITCT	.1.62	3.45	17 53	1.02E+19	2 91E+19	1.56E-02
B1	MW11HD	1TCT	-4.21	3.45	17.53	9.33E+18	2.67E+19	1.43E-02
~	2005	Charmy	0.92	2.66	25.01	6 00E+18	1 965+10	1.07E-02
01	2005	Charpy	0.02	3.00	20.91	7 455+10	2 105+10	1 145-02
01	2006	Charpy	0.82	3.00	24.91	7.4005.10	2.100+19	1.215.02
01	2008	Charpy	0.82	3.66	23.91	1.906+18	2.242+19	1.212-02

Table 2. (continued)

Block ID Type X Y Z (E=>1 MeV) (E=>0 1 MeV) C1 2DD11 Charpy 0.62 3.66 2.911 8.38E+18 2.49E+18 1.28E+02 C1 2DD12 Charpy 0.82 3.66 2.911 8.38E+18 2.49E+18 1.48E+02 C1 2DD10 Charpy 0.82 3.66 1.911 9.54E+18 2.47E+18 1.49E+02 C1 4D310 Charpy 0.82 3.66 1.911 9.54E+18 2.48E+19 1.55E+02 C1 4D312 Charpy 0.82 3.66 1.911 0.06E+19 3.05E+19 1.58E+02 C1 4D314 Charpy 0.82 3.66 1.911 1.02E+13 2.32E+19 1.83E+02 C1 2DE12 Charpy 1.82 3.66 2.911 7.02E+18 2.32E+19 1.38E+02 C1 2DD1 Charpy 1.82 3.66 2.911 7.62E+18 2.36E+19 1.38E+02 <th>Automation development of the</th> <th>Specimen</th> <th>an in a second de la contra de la</th> <th>С</th> <th>oordinate</th> <th>es</th> <th>Flu</th> <th>ence</th> <th>NAN ANTIPATANAN ANTIPATAN ANTIPATAN</th>	Automation development of the	Specimen	an in a second de la contra de la	С	oordinate	es	Flu	ence	NAN ANTIPATANAN ANTIPATAN ANTIPATAN
(cm) (cm) (cm2) (cm3) (Block	ID	Type	X	Y	7	(F > 1 MeV)	(E > 0 1 Me\/)	
C1 2DD11 Charpy 0.82 3.66 22.91 8.33E+18 2.37E+18 1.28E-02 C1 2DD12 Charpy 0.82 3.66 21.91 8.75E+18 2.44E+19 1.34E-02 C1 2D310 Charpy 0.82 3.66 21.91 8.75E+18 2.44E+19 1.32E-02 C1 4D311 Charpy 0.82 3.66 19.91 9.1E+16 2.44E+19 1.32E-02 C1 4D313 Charpy 0.82 3.66 17.91 1.03E+19 3.05E+19 1.38E-02 C1 2DE12 Charpy 0.82 3.66 15.91 1.08E+19 3.03E+19 1.38E-02 C1 2DE12 Charpy 1.82 3.66 2.91 7.10E+18 2.98E+19 1.08E-02 C1 2DD1 Charpy 1.82 3.66 2.91 7.57E+16 2.38E+19 1.38E-02 C1 2DD2 Charpy 1.82 3.66 2.91 7.57E+16 2.38E+19				(cm)	(cm)	(cm)	(cm ⁻²)	(cm ⁻²)	doa
C1 2DD12 Charpy 0.82 3.66 21.91 6.75E+18 2.44E+19 1.42E+22 C1 2DE10 Charpy 0.82 3.66 10.91 9.15E+18 2.44E+19 1.42E+22 C1 4D310 Charpy 0.82 3.66 19.91 9.91E+18 2.44E+19 1.40E+22 C1 4D312 Charpy 0.82 3.66 19.91 9.91E+18 2.36E+19 1.32E+21 C1 4D314 Charpy 0.82 3.66 14.91 1.32E+19 3.14E+19 1.38E+22 C1 2DE12 Charpy 1.82 3.66 2.911 7.10E+18 1.99E+19 3.08E+22 C1 2DE12 Charpy 1.82 3.66 2.911 7.10E+18 1.99E+19 1.80E+02 C1 2DD1 Charpy 1.82 3.66 2.911 7.10E+18 2.99E+18 2.39E+19 1.22E+02 C1 2DD2 Charpy 1.82 3.66 1.911 0.82E+19	C1	2DD11	Charpy	0.82	3.66	22.91	8 33E+18	2 375+10	1 295 02
C1 2DE10 Charpy 0.82 3.86 20.91 0.15E+18 2.48E+19 1.48E+22 C1 4D310 Charpy 0.82 3.86 19.91 9.54E+18 2.36E+19 1.40E+22 C1 4D311 Charpy 0.82 3.66 19.91 0.3E+19 2.36E+19 1.3E+22 C1 4D313 Charpy 0.82 3.66 16.91 1.0BE+19 2.36E+19 1.3E+22 C1 4D315 Charpy 0.82 3.66 16.91 1.0DE+16 2.38E+19 1.7E+22 C1 2DE12 Charpy 1.82 3.66 2.91 7.1DE+18 2.38E+19 1.0BE+22 C1 2DD1 Charpy 1.82 3.66 2.91 7.7E+18 2.38E+19 1.3E+26 C1 2DD2 Charpy 1.82 3.66 2.91 8.6E+18 2.38E+19 1.6E+22 C1 2DD4 Charpy 1.82 3.66 1.91 1.6E+14 2.38E+19 1.6E+	C1	2DD12	Charpy	0.82	3.66	21.01	8 755+18	2.0/2+19	1.20E-02
C1 4D310 Charpy 5.82 5.86 1.8 5.12 1.8 2.73E+19 1.40E-02 C1 4D311 Charpy 0.82 3.66 19.91 0.01E+18 2.84E+19 1.28E+02 C1 4D313 Charpy 0.82 3.66 19.91 1.03E+19 3.06E+19 3.06E+19 3.06E+19 1.82E+02 C1 4D314 Charpy 0.82 3.66 15.91 1.06E+19 3.14E+19 1.28E+02 C1 2DE12 Charpy 1.82 3.66 2.91 7.10E+18 2.38E+19 1.78E+02 C1 2DD1 Charpy 1.82 3.66 2.91 7.57E+18 2.38E+19 1.28E+02 C1 2DD2 Charpy 1.82 3.66 2.91 7.57E+18 2.38E+19 1.28E+02 C1 2DD4 Charpy 1.82 3.66 2.91 1.04E+19 2.8E+19 1.8E+02 C1 2D14 Charpy 1.82 3.66 1.91 <td>C1</td> <td>2DE10</td> <td>Charpy</td> <td>0.82</td> <td>3.66</td> <td>20.01</td> <td>0.155+10</td> <td>2.495+19</td> <td>1.34E-02</td>	C1	2DE10	Charpy	0.82	3.66	20.01	0.155+10	2.495+19	1.34E-02
C1 AD311 Charpy Color Sobe B SH D SH <thd sh<="" th=""> <thd sh<="" th=""> <thd sh<="" th=""> <thd< td=""><td>C1</td><td>40310</td><td>Charpy</td><td>0.82</td><td>3.66</td><td>10.01</td><td>9.100+10</td><td>2.01E+19</td><td>1.40E-02</td></thd<></thd></thd></thd>	C1	40310	Charpy	0.82	3.66	10.01	9.100+10	2.01E+19	1.40E-02
C1 4D312 Charpy 0.82 3.66 17.91 0.311+18 2.266±19 1.685±02 C1 4D313 Charpy 0.82 3.66 17.91 1.035±19 2.365±19 1.685±02 C1 4D314 Charpy 0.82 3.66 15.91 1.065±19 3.145±19 1.685±02 C1 2DE12 Charpy 0.82 3.66 2.91 7.105±16 2.335±19 1.735±02 C1 2DD1 Charpy 1.82 3.66 2.91 7.575±18 2.36±19 1.385±02 C1 2DD1 Charpy 1.82 3.66 2.91 8.46±18 2.38±19 1.385±02 C1 2DD4 Charpy 1.82 3.66 2.91 8.46±18 2.38±19 1.48±02 C1 2D14 Charpy 1.82 3.66 1.91 1.96±18 2.96±19 1.48±02 C1 2B121 Charpy 1.82 3.66 1.91 1.96±18 2.96±19 1.48±02 <td>CI</td> <td>40311</td> <td>Charpy</td> <td>0.02</td> <td>3.00</td> <td>19.91</td> <td>9.045+18</td> <td>2.73E+19</td> <td>1.46E-02</td>	CI	40311	Charpy	0.02	3.00	19.91	9.045+18	2.73E+19	1.46E-02
C1 4D313 Charpy 0.82 3.66 1.91 1.03E+19 2.86E+19 1.88E-02 C1 4D314 Charpy 0.82 3.66 16.91 1.06E+19 3.16E+19 1.88E-02 C1 4D315 Charpy 0.82 3.66 14.91 1.12E+19 3.23E+19 1.88E-02 C1 2CE12 Charpy 1.82 3.66 2.91 7.0E+16 1.99E+19 1.8E-02 C1 2D00 Charpy 1.82 3.66 2.91 8.46E+18 2.38E+19 1.28E+02 C1 2D04 Charpy 1.82 3.66 2.91 8.46E+18 2.38E+19 1.38E-02 C1 2D04 Charpy 1.82 3.66 1.91 1.92E+18 2.46E+11 1.38E-02 C1 2B120 Charpy 1.82 3.66 1.91 1.92E+18 2.46E+19 1.48E-02 C1 2B122 Charpy 1.82 3.66 1.91 <th1.04e+19< th=""> 3.08E+19 1.</th1.04e+19<>	CI	40311	Champy	0.02	3.00	18.91	9.91E+18	2.84E+19	1.52E-02
C1 4D314 Charpy 0.82 3.66 10.91 1.06E+19 3.06E+19 1.68E+02 C1 4D315 Charpy 0.82 3.66 15.91 1.06E+19 3.14E+19 3.34E+19 1.75E+02 C1 2DE12 Charpy 1.82 3.66 24.91 7.07E+18 2.38E+19 1.75E+02 C1 2DD1 Charpy 1.82 3.66 2.91 7.07E+18 2.38E+19 1.38E+02 C1 2DD1 Charpy 1.82 3.66 2.91 8.46E+18 2.38E+19 1.38E+02 C1 2DD4 Charpy 1.82 3.66 2.91 8.46E+18 2.38E+19 1.48E+02 C1 2D14 Charpy 1.82 3.66 1.91 1.04E+1+2 2.38E+19 1.48E+02 C1 2B12 Charpy 1.82 3.66 1.91 1.04E+1+2 2.38E+19 1.68E+02 C1 2B124 Charpy 1.82 3.66 1.91 1.04E+19 <t< td=""><td>CI</td><td>40312</td><td>Charpy</td><td>0.82</td><td>3.00</td><td>17.91</td><td>1.03E+19</td><td>2.95E+19</td><td>1.58E-02</td></t<>	CI	40312	Charpy	0.82	3.00	17.91	1.03E+19	2.95E+19	1.58E-02
C1 4U314 Charpy 0.82 3.66 1.51 1.08E+19 3.14E+19 1.68E-02 C1 2D315 Charpy 1.82 3.66 2.41 1.75E+18 2.3E+19 1.73E-02 C1 2DD0 Charpy 1.82 3.66 2.41 7.75E+18 2.3E+19 1.13E-02 C1 2DD0 Charpy 1.82 3.66 2.291 8.46E+18 2.29E+19 1.38E-02 C1 2DD2 Charpy 1.82 3.66 2.01 8.96E+18 2.64E+19 1.38E-02 C1 2DD4 Charpy 1.82 3.66 2.01 9.29E+18 2.64E+19 1.48E+02 C1 2B120 Charpy 1.82 3.66 1.61 1.01E+19 3.08E+19 1.66E-02 C1 2B121 Charpy 1.82 3.66 1.61 1.14E+19 3.08E+19 1.66E-02 C1 2B123 Charpy 1.82 3.66 1.61 1.14E+19 3.08E+19 1.6	CI	40313	Charpy	0.82	3.66	16.91	1.06E+19	3.05E+19	1.63E-02
C1 4D315 Charpy 0.82 3.66 1.4.91 1.12E+19 3.23E+19 1.73E-02 C1 2DE12 Charpy 1.82 3.66 2.5.91 7.10E+16 1.99E+19 1.08E-02 C1 2DD1 Charpy 1.82 3.66 2.3.91 8.02E+18 2.3EE+19 1.22E-02 C1 2DD1 Charpy 1.82 3.66 2.3.91 8.02E+18 2.3EE+19 1.32E-02 C1 2DD4 Charpy 1.82 3.66 2.9.91 9.29E+18 2.3EE+19 1.32E-02 C1 2D14 Charpy 1.82 3.66 1.9.11 1.04E+16 2.9EE+19 1.60E-02 C1 2B120 Charpy 1.82 3.66 1.9.11 1.04E+16 2.9EE+19 1.60E-02 C1 2B123 Charpy 1.82 3.66 1.9.1 1.04E+16 2.9EE+19 1.60E-02 C1 02D36 Charpy 2.91 3.66 2.5.91 7.18E+18 2.0EE+19 <td>Ci</td> <td>40314</td> <td>Charpy</td> <td>0.82</td> <td>3.66</td> <td>15.91</td> <td>1.09E+19</td> <td>3.14E+19</td> <td>1.68E-02</td>	Ci	40314	Charpy	0.82	3.66	15.91	1.09E+19	3.14E+19	1.68E-02
C1 2DE12 Charpy 1.82 3.66 25.91 7.10E+18 1.99E+19 1.08E-02 C1 2DD0 Charpy 1.82 3.66 24.91 7.57E+18 2.13E+19 1.13E-02 C1 2DD0 Charpy 1.82 3.66 2.91 8.40E+18 2.26E+19 1.32E-02 C1 2DD2 Charpy 1.82 3.66 2.91 8.40E+18 2.52E+19 1.33E-02 C1 2DD4 Charpy 1.82 3.66 2.91 9.48E+18 2.52E+19 1.34E-02 C1 2B120 Charpy 1.82 3.66 1.91 1.04E+19 3.08E+19 1.64E-02 C1 2B121 Charpy 1.82 3.66 1.61 1.04E+19 3.08E+19 1.75E-02 C1 2D135 Charpy 2.91 3.66 2.591 7.19E+18 2.00E+19 1.09E-02 C1 02D36 Charpy 2.91 3.66 2.591 7.19E+18 2.00E+19 <t< td=""><td>C1</td><td>40315</td><td>Charpy</td><td>0.82</td><td>3.66</td><td>14.91</td><td>1.12E+19</td><td>3.23E+19</td><td>1.73E-02</td></t<>	C1	40315	Charpy	0.82	3.66	14.91	1.12E+19	3.23E+19	1.73E-02
C1 20E12 Charpy 182 3.66 24.91 7.57E+18 2.13E+16 1.15E-02 C1 20D0 Charpy 182 3.66 23.91 8.02E+18 2.36E+19 1.22E-02 C1 20D1 Charpy 182 3.66 21.91 8.02E+18 2.36E+19 1.22E-02 C1 20D4 Charpy 182 3.66 19.91 9.69E+18 2.46E+19 1.48E-02 C1 2014 Charpy 182 3.66 19.91 9.69E+18 2.46E+19 1.46E-02 C1 2812 Charpy 182 3.66 15.91 1.11E+19 3.8E+19 1.66E-02 C1 28122 Charpy 182 3.66 14.91 1.14E+19 3.20E+19 1.75E-02 C1 28123 Charpy 2.91 3.66 24.91 7.60E+18 2.14E+19 1.17E-02 C1 02D36 Charpy 2.91 3.66 2.91 3.75F+18 2.46E+19 1.4	C1	2DE12	Charpy	1.82	3.66	25.91	7.10E+18	1.99E+19	1 08E-02
C1 2DD0 Charpy 182 3.66 23.91 8.02E+18 2.26E+19 1.22E+02 C1 2DD1 Charpy 182 3.66 22.91 8.46E+18 2.32E+19 1.32E+02 C1 2DD2 Charpy 182 3.66 20.91 9.29E+18 2.36E+19 1.42E+02 C1 2DD4 Charpy 182 3.66 19.91 9.99E+18 2.76E+19 1.44E+02 C1 2B120 Charpy 1.82 3.66 16.91 1.0E+19 3.0E+19 1.66E+02 C1 2B121 Charpy 1.82 3.66 16.91 1.0E+19 3.0E+19 1.76E+02 C1 2B123 Charpy 1.82 3.66 15.91 7.19E+18 2.00E+19 1.09E+02 C1 02D35 Charpy 2.91 3.66 25.91 7.19E+18 2.26E+19 1.3E+02 C1 02D36 Charpy 2.91 3.66 2.91 3.65 2.91 3.65	C1	2CE12	Charpy	1.82	3.66	24.91	7.57E+18	2 13E+19	1 155-02
C1 2DD1 Charpy 182 3.66 22.01 8.46E+18 2.36E+19 1.22E-02 C1 2DD2 Charpy 182 3.66 21.91 8.46E+18 2.36E+19 1.32E-02 C1 2DD4 Charpy 182 3.66 19.91 9.69E+18 2.46E+19 1.48E-02 C1 2B120 Charpy 1.82 3.66 19.91 9.69E+18 2.46E+19 1.48E-02 C1 2B121 Charpy 1.82 3.66 16.91 1.04E+19 3.08E+19 1.06E-02 C1 2B122 Charpy 1.82 3.66 16.91 1.14E+19 3.18E+19 1.70E-02 C1 2D36 Charpy 2.91 3.66 25.91 7.19E+18 2.48E+19 1.37E-02 C1 02D36 Charpy 2.91 3.66 2.94 7.66E+18 2.14E+19 1.75E-02 C1 02D36 Charpy 2.91 3.66 2.91 7.9E+18 2.48E+19 <th< td=""><td>C1</td><td>2000</td><td>Charpy</td><td>1.82</td><td>3.66</td><td>23.91</td><td>8 02E+18</td><td>2 265+10</td><td>1 225 02</td></th<>	C1	2000	Charpy	1.82	3.66	23.91	8 02E+18	2 265+10	1 225 02
C1 2DD2 Charpy 182 3.66 21.91 8.96E+18 2.52E+19 1.36E+02 C1 2DD4 Charpy 182 3.66 20.91 9.29E+18 2.64E+19 1.42E+02 C1 2D16 Charpy 182 3.66 19.91 6.9E+18 2.76E+19 1.44E+02 C1 2B120 Charpy 182 3.66 16.91 1.04E+10 2.88E+19 1.60E+02 C1 2B122 Charpy 182 3.66 16.91 1.04E+19 3.08E+19 1.60E+02 C1 2B123 Charpy 182 3.66 14.91 1.14E+19 3.27E+19 1.75E-02 C1 02D35 Charpy 2.91 3.66 25.91 7.19E+18 2.00E+19 1.09E-02 C1 02D36 Charpy 2.91 3.66 2.91 3.76E+18 2.48E+19 1.37E-02 C1 02D36 Charpy 2.91 3.66 2.91 9.0E+18 2.44E+19 1.	C1	2DD1	Charpy	1.82	3.66	22.01	8 46E+18	2.200+19	1.220-02
C1 2DD4 Charpy 1.82 3.86 20.81 9.29E+18 2.64E+19 1.84E-02 C1 4D316 Charpy 1.82 3.66 19.91 9.69E+18 2.64E+19 1.48E-02 C1 2B120 Charpy 1.82 3.66 19.91 0.69E+18 2.64E+19 1.64E-02 C1 2B121 Charpy 1.82 3.66 16.91 1.04E+19 3.08E+19 1.66E-02 C1 2B122 Charpy 1.82 3.66 16.91 1.11E+19 3.18E+19 1.76E-02 C1 02D35 Charpy 2.91 3.66 2.91 7.19E+18 2.00E+19 1.09E-02 C1 02D36 Charpy 2.91 3.66 2.91 3.65 2.91 3.65 2.91 3.65 2.91 3.65 2.91 3.65 2.91 3.65 2.91 3.65 2.91 3.65 2.91 3.65 2.91 3.65 2.91 3.65 2.91 3.65	C1	2002	Chamy	1.82	3.66	21.01	0.400+10	2.395+19	1.29E-02
C1 AD316 Charpy 1.82 3.66 19.91 9.698+18 2.768+19 1.48E-02 C1 28120 Charpy 1.82 3.66 18.91 1.01E+19 2.87E+19 1.48E-02 C1 28121 Charpy 1.82 3.66 16.91 1.01E+19 3.08E+19 1.60E-02 C1 28122 Charpy 1.82 3.66 16.91 1.11E+19 3.08E+19 1.60E-02 C1 28124 Charpy 1.82 3.66 25.91 7.19E+18 2.00E+19 1.09E-02 C1 02D35 Charpy 2.91 3.66 22.91 7.19E+18 2.00E+19 1.09E-02 C1 02D40 Charpy 2.91 3.66 2.91 3.65 2.191 9.00E+18 2.46E+19 1.37E-02 C1 02D40 Charpy 2.91 3.66 19.91 9.41E+18 2.46E+19 1.42E-02 C1 02D42 Charpy 2.91 3.66 19.91 <	CI	2004	Charpy	1.02	3.00	21.91	0.090710	2.52E+19	1.36E-02
C1 40316 Charpy 1.8.2 3.66 19.91 9.09±18 2.76±19 1.84E-02 C1 28120 Charpy 1.82 3.66 17.91 1.04E+19 2.98E+19 1.66E-02 C1 28123 Charpy 1.82 3.66 16.91 1.04E+19 3.08E+19 1.65E-02 C1 28123 Charpy 1.82 3.66 15.91 1.11E+19 3.18E+19 1.75E-02 C1 02D36 Charpy 2.91 3.66 25.91 7.19E+18 2.00E+19 1.09E-02 C1 02D36 Charpy 2.91 3.66 23.91 8.12E+18 2.24E+19 1.17E-02 C1 02D36 Charpy 2.91 3.66 20.91 9.45E+18 2.41E+19 1.37E-02 C1 02D41 Charpy 2.91 3.66 1.91 9.00E+18 2.24E+19 1.37E-02 C1 02D41 Charpy 2.91 3.66 1.91 9.00E+18 2.4E+19 1.37E-02 C1 MW9AE1 Charpy 2.91 3.66	CI	40246	Charpy	1.02	3.00	20.91	9.29E+18	2.64E+19	1.42E-02
C1 28120 Charpy 1.82 3.86 18.91 1.04E+19 2.87E+19 1.54E-02 C1 28121 Charpy 1.82 3.66 16.91 1.04E+19 3.08E+19 1.65E-02 C1 28123 Charpy 1.82 3.66 15.91 1.11E+19 3.18E+19 1.70E-02 C1 02D35 Charpy 1.82 3.66 15.91 1.14E+19 3.27E+19 1.75E-02 C1 02D36 Charpy 2.91 3.66 24.91 7.66E+18 2.14E+19 1.31E-02 C1 02D38 Charpy 2.91 3.66 23.91 8.12E+18 2.44E+19 1.31E-02 C1 02D40 Charpy 2.91 3.66 20.91 9.41E+18 2.44E+19 1.31E-02 C1 02D41 Charpy 2.91 3.66 19.91 9.41E+18 2.46E+19 1.44E-02 C1 MW9AE3 Charpy 2.91 3.66 19.91 9.81E+18 2.76E+19 1.66E-02 C1 MW9AE3 Charpy 2.91 3.66	CI	40316	Charpy	1.82	3.66	19.91	9.69E+18	2.76E+19	1.48E-02
C1 28121 Charpy 1.82 3.66 17.91 1.04E+15 2.98E+19 1.60E-02 C1 28122 Charpy 1.82 3.66 16.91 1.14E+19 3.08E+19 1.75E-02 C1 28123 Charpy 1.82 3.66 15.91 1.14E+19 3.08E+19 1.75E-02 C1 02D35 Charpy 2.91 3.66 25.91 7.19E+18 2.00E+19 1.09E-02 C1 02D36 Charpy 2.91 3.66 24.91 7.66E+18 2.14E+19 1.17E-02 C1 02D36 Charpy 2.91 3.66 23.91 8.12E+18 2.28E+19 1.24E-02 C1 02D40 Charpy 2.91 3.66 20.91 9.41E+18 2.66E+19 1.34E-02 C1 02D41 Charpy 2.91 3.66 1.91 9.00E+18 2.66E+19 1.44E-02 C1 02D42 Charpy 2.91 3.66 18.91 1.02E+19 2.90E+19 1.56E-02 C1 MV9AE3 Charpy 2.91 3.66 <	CI	28120	Charpy	1.82	3.66	18.91	1.01E+19	2.87E+19	1.54E-02
C1 2B122 Charpy 1.82 3.66 16.91 1.08E+19 3.08E+19 1.65E-02 C1 2B123 Charpy 1.82 3.66 15.91 1.11E+19 3.18E+19 1.75E-02 C1 2B124 Charpy 1.82 3.66 14.91 1.14E+19 3.27E+19 1.75E-02 C1 02D35 Charpy 2.91 3.66 24.91 7.66E+18 2.14E+19 1.17E-02 C1 02D36 Charpy 2.91 3.66 24.91 7.66E+18 2.14E+19 1.31E-02 C1 02D40 Charpy 2.91 3.66 21.91 9.00E+18 2.46E+19 1.31E-02 C1 02D41 Charpy 2.91 3.66 1.91 9.00E+18 2.46E+19 1.31E-02 C1 02D42 Charpy 2.91 3.66 1.91 9.00E+18 2.66E+19 1.44E-02 C1 MW9AE2 Charpy 2.91 3.66 16.91 1.06E+19 3.00E+19 1.6E-02 C1 MW9AE3 Charpy 2.91 3.66 <t< td=""><td>C1</td><td>28121</td><td>Charpy</td><td>1.82</td><td>3.66</td><td>17.91</td><td>1.04E+10</td><td>2.98E+19</td><td>1.60E-02</td></t<>	C1	28121	Charpy	1.82	3.66	17.91	1.04E+10	2.98E+19	1.60E-02
C1 2B123 Charpy 1.82 3.66 15.91 1.11E+19 3.18E+19 1.70E-02 C1 2B124 Charpy 2.91 3.66 25.91 7.19E+18 2.00E+19 1.09E-02 C1 02D36 Charpy 2.91 3.66 25.91 7.66E+18 2.14E+19 1.77E-02 C1 02D36 Charpy 2.91 3.66 23.91 8.12E+18 2.28E+19 1.24E-02 C1 02D40 Charpy 2.91 3.66 2.91 9.00E+18 2.64E+19 1.37E-02 C1 02D41 Charpy 2.91 3.66 19.91 9.0DE+18 2.84E+19 1.05E-02 C1 MW9AE2 Charpy 2.91 3.66 18.91 1.02E+19 2.90E+19 1.56E-02 C1 MW9AE3 Charpy 2.91 3.66 16.91 1.06E+19 3.10E+19 1.77E-02 C1 MW9AE4 Charpy 2.91 3.66 14.91 1.12E+19 3.20E+19	C1	2B122	Charpy	1.82	3.66	16.91	1.08E+19	3.08E+19	1.65E-02
C1 2B124 Charpy 1.82 3.66 14.91 1.14E+19 3.27E+19 1.75E-02 C1 02D35 Charpy 2.91 3.66 25.91 7.19E+18 2.00E+19 1.09E-02 C1 02D36 Charpy 2.91 3.66 24.91 7.66E+18 2.14E+19 1.17E-02 C1 02D40 Charpy 2.91 3.66 22.91 8.57E+18 2.41E+19 1.31E-02 C1 02D42 Charpy 2.91 3.66 20.91 9.0E+18 2.54E+19 1.37E-02 C1 0ZD42 Charpy 2.91 3.66 19.91 9.81E+18 2.78E+19 1.50E-02 C1 MW9AE3 Charpy 2.91 3.66 15.91 1.00E+19 3.00E+19 1.72E-02 C1 MW9AE4 Charpy 2.91 3.66 15.91 1.12E+19 3.0E+19 1.72E-02 C1 MW9AE4 Charpy 4.00 3.66 2.91 7.3E+18 2.15E+19	C1	2B123	Charpy	1.82	3.66	15.91	1.11E+19	3.18E+19	1.70E-02
C1 02D35 Charpy 2.91 3.66 25.91 7.19E+18 2.00E+19 1.09E-02 C1 02D38 Charpy 2.91 3.66 23.91 8.12E+18 2.24E+19 1.17E-02 C1 02D38 Charpy 2.91 3.66 23.91 8.57E+18 2.41E+19 1.17E-02 C1 02D40 Charpy 2.91 3.66 21.91 9.00E+18 2.54E+19 1.37E-02 C1 02D42 Charpy 2.91 3.66 1.91 9.00E+18 2.54E+19 1.37E-02 C1 MV9AE1 Charpy 2.91 3.66 18.91 1.02E+19 2.06E+19 1.56E-02 C1 MV9AE3 Charpy 2.91 3.66 16.91 3.00E+19 3.11E+19 1.67E-02 C1 MV9AE4 Charpy 2.91 3.66 16.91 1.02E+19 3.02E+19 1.7E-02 C1 MV07A Charpy 2.91 3.66 16.91 1.15E+19 1.17E-02	C1	2B124	Charpy	1.82	3.66	14.91	1.14E+19	3.27E+19	1.75E-02
C1 02D36 Charpy 2.91 3.66 24.91 7.66E+18 2.14E+19 1.17E-02 C1 02D38 Charpy 2.91 3.66 23.91 8.12E+18 2.14E+19 1.31E-02 C1 02D40 Charpy 2.91 3.66 23.91 8.57E+18 2.41E+19 1.31E-02 C1 02D41 Charpy 2.91 3.66 20.91 9.41E+18 2.78E+19 1.37E-02 C1 02D42 Charpy 2.91 3.66 1.91 9.00E+18 2.54E+19 1.56E-02 C1 MW9AE2 Charpy 2.91 3.66 18.91 1.02E+19 2.90E+19 1.56E-02 C1 MW9AE3 Charpy 2.91 3.66 15.91 1.12E+19 3.00E+19 1.67E-02 C1 MW9AE5 Charpy 2.91 3.66 15.91 1.12E+19 3.00E+19 1.77E-02 C1 MW0AE5 Charpy 4.00 3.66 25.91 7.2EE+18 2.00E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66	C1	02D35	Charpy	2.91	3.66	25.91	7 19E+18	2 005+10	1 005 02
C1 O2D38 Charpy 2.91 3.66 23.91 8.12E+18 2.28E+19 1.24E-02 C1 O2D40 Charpy 2.91 3.66 22.91 8.57E+18 2.4E+19 1.37E-02 C1 O2D41 Charpy 2.91 3.66 22.91 8.57E+18 2.4E+19 1.37E-02 C1 O2D42 Charpy 2.91 3.66 2.91 9.41E+18 2.66E+19 1.44E-02 C1 MW9AE1 Charpy 2.91 3.66 18.91 1.02E+19 2.90E+19 1.56E-02 C1 MW9AE3 Charpy 2.91 3.66 18.91 1.02E+19 3.00E+19 1.62E-02 C1 MW9AE4 Charpy 2.91 3.66 16.91 1.09E+19 3.10E+19 1.77E-02 C1 MW9AE5 Charpy 2.91 3.66 25.91 7.25E+18 2.00E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19	C1	02036	Charpy	2.01	3.66	24.01	7.665+10	2.002+19	1.092-02
C1 C2D40 Charpy 2.91 3.66 2.3.91 6.12±+16 2.45±+19 1.32±-02 C1 C2D41 Charpy 2.91 3.66 22.91 8.57±+18 2.41±+19 1.31±-02 C1 OZD42 Charpy 2.91 3.66 22.91 9.06±+18 2.56±+19 1.37±-02 C1 OZD42 Charpy 2.91 3.66 19.91 9.41±+18 2.66±+19 1.44±-02 C1 MW9AE1 Charpy 2.91 3.66 18.91 1.02±+19 2.90±+19 1.56±-02 C1 MW9AE2 Charpy 2.91 3.66 15.91 1.12±+19 3.00±+19 1.62±-02 C1 MW9AE5 Charpy 2.91 3.66 15.91 1.12±+19 3.00±+19 1.72±-02 C1 MW9AE3 Charpy 4.00 3.66 24.91 7.3±+18 2.05±+19 1.77±-02 C1 WC07A Charpy 4.00 3.66 24.91 1.15±+19 3.30±+19 <td>CI</td> <td>02030</td> <td>Charpy</td> <td>2.01</td> <td>3.66</td> <td>22.01</td> <td>0 100 10</td> <td>2.146+19</td> <td>1.1/E-02</td>	CI	02030	Charpy	2.01	3.66	22.01	0 100 10	2.146+19	1.1/E-02
C1 OZD40 Charpy 2.91 3.66 22.91 9.57E+18 2.41E+19 1.31E-02 C1 OZD41 Charpy 2.91 3.66 21.91 9.00E+18 2.54E+19 1.37E-02 C1 OZD42 Charpy 2.91 3.66 19.91 9.81E+18 2.66E+19 1.44E-02 C1 MW9AE1 Charpy 2.91 3.66 19.91 9.81E+18 2.78E+19 1.50E-02 C1 MW9AE3 Charpy 2.91 3.66 16.91 1.02E+19 3.00E+19 1.6E-02 C1 MW9AE4 Charpy 2.91 3.66 16.91 1.02E+19 3.00E+19 1.77E-02 C1 MW9AE5 Charpy 2.91 3.66 14.91 1.15E+19 3.30E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.10E-02 C1 WC07C Charpy 4.00 3.66 23.91 8.48E+18 2.4E+19	C1	02030	Charpy	2.01	3.00	23.91	0.120+10	2.28E+19	1.24E-02
C1 O2D41 Charpy 2.91 3.66 21.91 9.00E+18 2.54E+19 1.37E-02 C1 MW9AE1 Charpy 2.91 3.66 19.91 9.81E+18 2.66E+19 1.44E-02 C1 MW9AE2 Charpy 2.91 3.66 19.91 9.81E+18 2.78E+19 1.50E-02 C1 MW9AE3 Charpy 2.91 3.66 17.91 1.06E+19 3.00E+19 1.62E-02 C1 MW9AE4 Charpy 2.91 3.66 17.91 1.06E+19 3.00E+19 1.62E-02 C1 MW9AE5 Charpy 2.91 3.66 15.91 1.12E+19 3.20E+19 1.72E-02 C1 MW08E5 Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.10E-02 C1 WC07A Charpy 4.00 3.66 23.91 8.19E+18 2.35E+19 1.37E-02 C1 WC07C Charpy 4.00 3.66 29.91 7.75E+18 2.00E+19<	01	02040	Charpy	2.91	3.00	22.91	0.07E+18	2.41E+19	1.31E-02
C1 02042 Charpy 2.91 3.66 20.91 9.41E+18 2.66E+19 1.44E-02 C1 MW9AE1 Charpy 2.91 3.66 19.91 9.81E+18 2.78E+19 1.50E-02 C1 MW9AE3 Charpy 2.91 3.66 19.91 1.02E+19 2.90E+19 1.56E-02 C1 MW9AE3 Charpy 2.91 3.66 17.91 1.00E+19 3.11E+19 1.62E-02 C1 MW9AE5 Charpy 2.91 3.66 16.91 1.09E+19 3.11E+19 1.62E-02 C1 MW9AE5 Charpy 2.91 3.66 14.91 1.15E+19 3.00E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.10E-02 C1 WC07C Charpy 4.00 3.66 23.91 8.19E+18 2.42E+19 1.31E-02 C1 WC07C Charpy 4.00 3.66 2.91 9.07E+18 2.42E+19 <td>01</td> <td>02041</td> <td>Charpy</td> <td>2.91</td> <td>3.66</td> <td>21.91</td> <td>9.00E+18</td> <td>2.54E+19</td> <td>1.37E-02</td>	01	02041	Charpy	2.91	3.66	21.91	9.00E+18	2.54E+19	1.37E-02
C1 MW9AE1 Charpy 2.91 3.66 19.91 9.81E+18 2.78E+19 1.50E-02 C1 MW9AE2 Charpy 2.91 3.66 18.91 1.02E+19 2.90E+19 1.56E-02 C1 MW9AE3 Charpy 2.91 3.66 16.91 1.09E+19 3.11E+19 1.62E-02 C1 MW9AE5 Charpy 2.91 3.66 16.91 1.09E+19 3.11E+19 1.62E-02 C1 MW9AE5 Charpy 2.91 3.66 15.91 1.12E+19 3.20E+19 1.72E-02 C1 MW07D Charpy 2.91 3.66 14.91 1.15E+19 3.20E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.77E-02 C1 WC07C Charpy 4.00 3.66 23.91 8.19E+18 2.18E+19 1.31E+02 C1 HC42 Charpy 4.00 3.66 2.91 9.07E+18 2.42E+19 <td>Ci</td> <td>02042</td> <td>Charpy</td> <td>2.91</td> <td>3.66</td> <td>20.91</td> <td>9.41E+18</td> <td>2.66E+19</td> <td>1.44E-02</td>	Ci	02042	Charpy	2.91	3.66	20.91	9.41E+18	2.66E+19	1.44E-02
C1 MW9AE2 Charpy 2.91 3.66 18.91 1.02E+19 2.90E+19 1.68E-02 C1 MW9AE3 Charpy 2.91 3.66 17.91 1.06E+19 3.00E+19 1.62E-02 C1 MW9AE5 Charpy 2.91 3.66 16.91 1.09E+19 3.11E+19 1.67E-02 C1 MW9AE5 Charpy 2.91 3.66 15.91 1.12E+19 3.20E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.0E-02 C1 WC07B Charpy 4.00 3.66 23.91 8.19E+18 2.15E+19 1.24E+02 C1 WC07C Charpy 4.00 3.66 21.91 9.07E+18 2.54E+19 1.36E-02 C1 HC42 Charpy 4.00 3.66 20.91 9.49E+18 2.47E+19 1.36E-02 C1 NC34CF3 Charpy 4.00 3.66 19.91 9.49E+18 2.67E+19 <td>C1</td> <td>MW9AE1</td> <td>Charpy</td> <td>2.91</td> <td>3.66</td> <td>19.91</td> <td>9.81E+18</td> <td>2.78E+19</td> <td>1.50E-02</td>	C1	MW9AE1	Charpy	2.91	3.66	19.91	9.81E+18	2.78E+19	1.50E-02
C1 MW9AE3 Charpy 2.91 3.66 17.91 1.06E+19 3.00E+19 1.62E-02 C1 MW9AE4 Charpy 2.91 3.66 16.91 1.09E+19 3.11E+19 1.62E-02 C1 MW9BD1 Charpy 2.91 3.66 15.91 1.12E+19 3.20E+19 1.72E-02 C1 WC07A Charpy 2.91 3.66 14.91 1.15E+19 3.30E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.17E-02 C1 WC07C Charpy 4.00 3.66 23.91 8.19E+18 2.3E+19 1.24E-02 C1 WC07C Charpy 4.00 3.66 20.91 9.49E+18 2.42E+19 1.31E+02 C1 MC34CF1 Charpy 4.00 3.66 20.91 9.49E+18 2.67E+19 1.68E-02 C1 NC34CF3 Charpy 4.00 3.66 19.91 9.39E+18 2.79E+19<	C1	MW9AE2	Charpy	2.91	3.66	18.91	1.02E+19	2.90E+19	1.56E-02
C1 MW9AE4 Charpy 2.91 3.66 16.91 1.09E+19 3.11E+19 1.67E-02 C1 MW9AE5 Charpy 2.91 3.66 15.91 1.12E+19 3.20E+19 1.72E-02 C1 MW9BD1 Charpy 2.91 3.66 14.91 1.15E+19 3.30E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.10E-02 C1 WC07B Charpy 4.00 3.66 24.91 7.73E+18 2.15E+19 1.24E-02 C1 WC07C Charpy 4.00 3.66 22.91 8.64E+18 2.42E+19 1.31E-02 C1 MC34CF1 Charpy 4.00 3.66 20.91 9.49E+18 2.67E+19 1.45E-02 C1 NC34CF3 Charpy 4.00 3.66 19.91 9.89E+18 2.67E+19 1.57E-02 C1 NC34CF3 Charpy 4.00 3.66 17.91 1.06E+19 3.01E+	C1	MW9AE3	Charpy	2.91	3.66	17.91	1.06E+19	3.00E+19	1.62E-02
C1 MW9AE5 Charpy 2.91 3.66 15.91 1.12E+19 3.20E+19 1.72E-02 C1 MW9BD1 Charpy 2.91 3.66 14.91 1.15E+19 3.30E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.17E-02 C1 WC07C Charpy 4.00 3.66 23.91 8.19E+18 2.15E+19 1.17E-02 C1 WC07C Charpy 4.00 3.66 23.91 8.19E+18 2.42E+19 1.31E-02 C1 GC44 Charpy 4.00 3.66 23.91 8.64E+18 2.42E+19 1.38E-02 C1 NC34CF1 Charpy 4.00 3.66 20.91 9.49E+18 2.67E+19 1.57E-02 C1 NC34CF3 Charpy 4.00 3.66 19.91 9.89E+18 2.90E+19 1.57E-02 C1 NC34DF2 Charpy 4.00 3.66 16.91 1.06E+19 3.01E+19	C1	MW9AE4	Charpy	2.91	3.66	16.91	1.09E+19	3.11E+19	1.67E-02
C1 MW9BD1 Charpy 2.91 3.66 14.91 1.15E+19 3.30E+19 1.77E-02 C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.10E-02 C1 WC07C Charpy 4.00 3.66 24.91 7.73E+18 2.15E+19 1.17E-02 C1 WC07C Charpy 4.00 3.66 23.91 8.19E+18 2.28E+19 1.24E-02 C1 GC44 Charpy 4.00 3.66 22.91 8.64E+18 2.42E+19 1.31E-02 C1 HC42 Charpy 4.00 3.66 20.91 9.49E+18 2.67E+19 1.38E-02 C1 NC34CF1 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.63E+02 C1 NC34DF2 Charpy 4.00 3.66 16.91 1.10E+19 3.01E+19 </td <td>C1</td> <td>MW9AE5</td> <td>Charpy</td> <td>2.91</td> <td>3.66</td> <td>15.91</td> <td>1.12E+19</td> <td>3.20E+19</td> <td>1.72E-02</td>	C1	MW9AE5	Charpy	2.91	3.66	15.91	1.12E+19	3.20E+19	1.72E-02
C1 WC07A Charpy 4.00 3.66 25.91 7.25E+18 2.00E+19 1.10E-02 C1 WC07B Charpy 4.00 3.66 24.91 7.73E+18 2.15E+19 1.17E-02 C1 WC07C Charpy 4.00 3.66 23.91 8.19E+18 2.28E+19 1.24E-02 C1 GC44 Charpy 4.00 3.66 22.91 8.64E+18 2.42E+19 1.31E-02 C1 HC42 Charpy 4.00 3.66 20.91 9.07E+18 2.54E+19 1.38E-02 C1 NC34CF1 Charpy 4.00 3.66 19.91 9.89E+18 2.67E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 18.91 1.03E+19 2.90E+19 1.57E-02 C1 NC34DF5 Charpy 4.00 3.66 16.91 1.10E+19 3.01E+19 1.68E-02 C1 NC34DF5 Charpy 4.00 3.66 15.91 1.31E+19 3.21E+19<	C1	MW9BD1	Charpy	2.91	3.66	14.91	1.15E+19	3.30E+19	1.77E-02
C1 WC07B Charpy 4.00 3.66 24.91 7.73E+18 2.00E+19 1.10E-02 C1 WC07C Charpy 4.00 3.66 23.91 7.73E+18 2.15E+19 1.17E-02 C1 WC07C Charpy 4.00 3.66 23.91 8.19E+18 2.28E+19 1.24E-02 C1 GC44 Charpy 4.00 3.66 22.91 8.64E+18 2.42E+19 1.31E-02 C1 HC42 Charpy 4.00 3.66 21.91 9.07E+18 2.54E+19 1.38E-02 C1 NC34CF3 Charpy 4.00 3.66 19.91 9.89E+18 2.67E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 18.91 1.03E+19 2.00E+19 1.57E-02 C1 NC34DF2 Charpy 4.00 3.66 15.91 1.13E+19 3.01E+19 1.68E-02 C1 NC34H15 Charpy 4.00 3.66 15.91 1.16E+19 3.02E+19<	C1	WC07A	Charny	4.00	3.66	25.01	7 255+19	2 005+10	1 105 02
C1 WC07B Charpy 4.00 3.66 24.91 7.73E+16 2.13E+19 1.17E-02 C1 WC07B Charpy 4.00 3.66 23.91 8.19E+18 2.28E+19 1.24E-02 C1 GC44 Charpy 4.00 3.66 22.91 8.64E+18 2.42E+19 1.31E-02 C1 HC42 Charpy 4.00 3.66 21.91 9.07E+18 2.64E+19 1.38E-02 C1 NC34CF1 Charpy 4.00 3.66 20.91 9.49E+18 2.67E+19 1.45E-02 C1 NC34CF5 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 19.91 9.49E+19 3.01E+19 1.63E-02 C1 NC34DF2 Charpy 4.00 3.66 17.91 1.06E+19 3.01E+19 1.77E-02 C1 NC34JI1 Charpy 4.00 3.66 14.91 1.16E+19 3.30E+1	CI	WC07R	Charpy	4.00	3.66	24.01	7 735+10	2.000+19	1.100-02
C1 WC07C Charpy 4.00 3.66 23.91 8.19E+18 2.28E+19 1.24E-02 C1 GC44 Charpy 4.00 3.66 22.91 8.64E+18 2.42E+19 1.31E-02 C1 HC42 Charpy 4.00 3.66 22.91 8.64E+18 2.42E+19 1.31E-02 C1 NC34CF1 Charpy 4.00 3.66 20.91 9.49E+18 2.67E+19 1.35E-02 C1 NC34CF3 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 18.91 1.03E+19 2.90E+19 1.57E-02 C1 NC34DF2 Charpy 4.00 3.66 16.91 1.10E+19 3.01E+19 1.63E-02 C1 NC34DF5 Charpy 4.00 3.66 15.91 1.3E+19 3.21E+19 1.73E-02 C1 NC34JI1 Charpy 4.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC06A Charpy 5.00 3.66 <td>CI</td> <td>WC07D</td> <td>Charpy</td> <td>4.00</td> <td>3.00</td> <td>24.91</td> <td>7.73E+18</td> <td>2.156+19</td> <td>1.1/E-02</td>	CI	WC07D	Charpy	4.00	3.00	24.91	7.73E+18	2.156+19	1.1/E-02
C1 GC44 Charpy 4.00 3.66 22.91 8.84E+18 2.42E+19 1.31E-02 C1 HC42 Charpy 4.00 3.66 21.91 9.07E+18 2.54E+19 1.38E-02 C1 NC34CF1 Charpy 4.00 3.66 20.91 9.49E+18 2.67E+19 1.45E-02 C1 NC34CF3 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 18.91 1.03E+19 2.90E+19 1.57E-02 C1 NC34DF2 Charpy 4.00 3.66 16.91 1.10E+19 3.01E+19 1.63E-02 C1 NC34DF5 Charpy 4.00 3.66 15.91 1.13E+19 3.21E+19 1.73E-02 C1 NC34H15 Charpy 4.00 3.66 14.91 1.16E+19 3.01E+19 1.68E-02 C1 NC34J11 Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC06A Charpy 5.00 3.66<	C1	WCOTC	Charpy	4.00	3.00	23.91	8.19E+18	2.28E+19	1.24E-02
C1 HC42 Charpy 4.00 3.66 21.91 9.07E+18 2.54E+19 1.38E-02 C1 NC34CF1 Charpy 4.00 3.66 20.91 9.49E+18 2.67E+19 1.45E-02 C1 NC34CF3 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 17.91 1.06E+19 3.01E+19 1.63E-02 C1 NC34DF5 Charpy 4.00 3.66 15.91 1.10E+19 3.11E+19 1.68E-02 C1 NC34J11 Charpy 4.00 3.66 15.91 1.13E+19 3.21E+19 1.73E-02 C1 NC34J11 Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC06A Charpy 5.00 3.66 23.91 8.22E+18 2.28E+19 1.25E-02 C1 WC06C Charpy 5.00 3.66	Ci	GC44	Charpy	4.00	3.66	22.91	8.54E+18	2.42E+19	1.31E-02
C1 NC34CF1 Charpy 4.00 3.66 20.91 9.49E+18 2.67E+19 1.45E-02 C1 NC34CF3 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 17.91 1.03E+19 2.90E+19 1.57E-02 C1 NC34DF2 Charpy 4.00 3.66 16.91 1.10E+19 3.01E+19 1.63E-02 C1 NC34DF5 Charpy 4.00 3.66 16.91 1.10E+19 3.11E+19 1.68E-02 C1 NC34H15 Charpy 4.00 3.66 15.91 1.13E+19 3.21E+19 1.73E-02 C1 NC34J11 Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC06A Charpy 5.00 3.66 24.91 7.75E+18 2.14E+19 1.25E-02 C1 WC06C Charpy 5.00 3	C1	HC42	Charpy	4.00	3.66	21.91	9.07E+18	2.54E+19	1.38E-02
C1 NC34CF3 Charpy 4.00 3.66 19.91 9.89E+18 2.79E+19 1.51E-02 C1 NC34CF5 Charpy 4.00 3.66 18.91 1.03E+19 2.90E+19 1.57E-02 C1 NC34DF2 Charpy 4.00 3.66 17.91 1.06E+19 3.01E+19 1.63E-02 C1 NC34DF5 Charpy 4.00 3.66 16.91 1.10E+19 3.11E+19 1.63E-02 C1 NC34DF5 Charpy 4.00 3.66 15.91 1.13E+19 3.21E+19 1.73E-02 C1 NC34JI1 Charpy 4.00 3.66 14.91 1.16E+19 3.30E+19 1.78E-02 C1 WC06A Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC06C Charpy 5.00 3.66 24.91 7.75E+18 2.14E+19 1.17E-02 C1 WC06C Charpy 5.00 3.66 22.91 8.67E+18 2.41E+19 1.32E-02 C1 WC06D Charpy 5.00 3.66<	C1	NC34CF1	Charpy	4.00	3.66	20.91	9.49E+18	2.67E+19	1.45E-02
C1 NC34CF5 Charpy 4.00 3.66 18.91 1.03E+19 2.90E+19 1.57E-02 C1 NC34DF2 Charpy 4.00 3.66 17.91 1.06E+19 3.01E+19 1.63E-02 C1 NC34DF5 Charpy 4.00 3.66 16.91 1.10E+19 3.11E+19 1.63E-02 C1 NC34JF5 Charpy 4.00 3.66 15.91 1.13E+19 3.21E+19 1.73E-02 C1 NC34JI1 Charpy 4.00 3.66 15.91 1.13E+19 3.21E+19 1.73E-02 C1 NC34JI1 Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC06A Charpy 5.00 3.66 24.91 7.75E+18 2.14E+19 1.17E-02 C1 WC06C Charpy 5.00 3.66 23.91 8.22E+18 2.28E+19 1.25E-02 C1 WC06D Charpy 5.00 3.66 21.91 9.10E+18 2.41E+19 1.32E-02 C1 WC06D Charpy 5.00 3.66<	C1	NC34CF3	Charpy	4.00	3.66	19.91	9.89E+18	2.79E+19	1.51E-02
C1 NC34DF2 Charpy 4.00 3.66 17.91 1.06E+19 3.01E+19 1.63E-02 C1 NC34DF5 Charpy 4.00 3.66 16.91 1.10E+19 3.11E+19 1.68E-02 C1 NC34HI5 Charpy 4.00 3.66 15.91 1.13E+19 3.21E+19 1.73E-02 C1 NC34JI1 Charpy 4.00 3.66 14.91 1.16E+19 3.30E+19 1.73E-02 C1 WC06A Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC07D Charpy 5.00 3.66 24.91 7.75E+18 2.14E+19 1.17E-02 C1 WC06C Charpy 5.00 3.66 23.91 8.22E+18 2.28E+19 1.25E-02 C1 WC06D Charpy 5.00 3.66 21.91 9.10E+18 2.41E+19 1.32E-02 C1 WC06D Charpy 5.00 3.66 20.91 9.52E+18 2.66E+1	C1	NC34CF5	Charpy	4.00	3.66	18.91	1.03E+19	2.90E+19	1.57E-02
C1 NC34DF5 Charpy 4.00 3.66 16.91 1.10E+19 3.11E+19 1.68E-02 C1 NC34HI5 Charpy 4.00 3.66 15.91 1.13E+19 3.21E+19 1.73E-02 C1 NC34JI1 Charpy 4.00 3.66 14.91 1.16E+19 3.30E+19 1.78E-02 C1 WC06A Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC07D Charpy 5.00 3.66 24.91 7.75E+18 2.14E+19 1.17E-02 C1 WC06C Charpy 5.00 3.66 23.91 8.22E+18 2.28E+19 1.25E-02 C1 WC06D Charpy 5.00 3.66 21.91 9.10E+18 2.41E+19 1.32E-02 C1 WC06D Charpy 5.00 3.66 20.91 8.67E+18 2.41E+19 1.32E-02 C1 NC34JI2 Charpy 5.00 3.66 20.91 9.52E+18 2.66E+1	C1	NC34DF2	Charpy	4.00	3.66	17.91	1.06E+19	3.01E+19	1.63E-02
C1 NC34HI5 Charpy 4.00 3.66 15.91 1.13E+19 3.21E+19 1.73E-02 C1 NC34JI1 Charpy 4.00 3.66 14.91 1.16E+19 3.30E+19 1.73E-02 C1 WC06A Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC07D Charpy 5.00 3.66 24.91 7.75E+18 2.14E+19 1.17E-02 C1 WC06C Charpy 5.00 3.66 23.91 8.22E+18 2.28E+19 1.25E-02 C1 WC06D Charpy 5.00 3.66 22.91 8.67E+18 2.41E+19 1.32E-02 C1 WC06D Charpy 5.00 3.66 22.91 8.67E+18 2.41E+19 1.32E-02 C1 NC34JI2 Charpy 5.00 3.66 20.91 9.10E+18 2.54E+19 1.38E-02 C1 NC34JI3 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+1	C1	NC34DF5	Charpy	4.00	3.66	16.91	1.10E+19	3.11E+19	1.68E-02
C1 NC34JI1 Charpy 4.00 3.66 14.91 1.16E+19 3.30E+19 1.78E-02 C1 WC06A Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC07D Charpy 5.00 3.66 24.91 7.75E+18 2.14E+19 1.17E-02 C1 WC06C Charpy 5.00 3.66 23.91 8.22E+18 2.28E+19 1.25E-02 C1 WC06D Charpy 5.00 3.66 22.91 8.67E+18 2.41E+19 1.32E-02 C1 WC06D Charpy 5.00 3.66 21.91 9.10E+18 2.41E+19 1.32E-02 C1 NC34JI2 Charpy 5.00 3.66 20.91 9.52E+18 2.66E+19 1.38E-02 C1 NC34JI3 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+19 1.51E-02 C1 NC34JI4 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+1	C1	NC34HI5	Charpy	4.00	3.66	15.91	1 13E+19	321E+19	1.73E-02
C1 WC06A Charpy 5.00 3.66 25.91 7.28E+18 2.00E+19 1.10E-02 C1 WC07D Charpy 5.00 3.66 24.91 7.75E+18 2.14E+19 1.17E-02 C1 WC06C Charpy 5.00 3.66 23.91 8.22E+18 2.28E+19 1.25E-02 C1 WC06D Charpy 5.00 3.66 22.91 8.67E+18 2.41E+19 1.32E-02 C1 WC06D Charpy 5.00 3.66 22.91 8.67E+18 2.41E+19 1.32E-02 C1 NC34JI2 Charpy 5.00 3.66 20.91 9.10E+18 2.54E+19 1.38E-02 C1 NC34JI3 Charpy 5.00 3.66 20.91 9.52E+18 2.66E+19 1.45E-02 C1 NC34JI4 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+19 1.51E-02 C1 NC34JI5 Charpy 5.00 3.66 18.91 1.03E+19 2.89E+1	C1	NC34JI1	Charpy	4.00	3.66	14.91	1.16E+19	3.30E+19	1.78E-02
C1 WC00A Charpy 5.00 3.66 25.91 7.28±18 2.00±19 1.10E-02 C1 WC07D Charpy 5.00 3.66 24.91 7.75±18 2.14±19 1.17E-02 C1 WC06C Charpy 5.00 3.66 23.91 8.22±18 2.28±19 1.25E-02 C1 WC06D Charpy 5.00 3.66 22.91 8.67±18 2.41±19 1.32E-02 C1 NC34JI2 Charpy 5.00 3.66 21.91 9.10±18 2.54±19 1.38E-02 C1 NC34JI3 Charpy 5.00 3.66 20.91 9.52±18 2.66±19 1.45E-02 C1 NC34JI3 Charpy 5.00 3.66 19.91 9.93±18 2.78±19 1.51E-02 C1 NC34JI4 Charpy 5.00 3.66 18.91 1.03±19 2.89±19 1.57E-02 C1 NC34JI5 Charpy 5.00 3.66 17.91 1.07±19 3.00±19 <	~	1410004	Charme	E 00	2.00	05.04	7 005 . 40	2.005.40	1 105 00
C1 WC07D Charpy 5.00 3.65 24.91 7.75E+18 2.14E+19 1.17E-02 C1 WC06C Charpy 5.00 3.66 23.91 8.22E+18 2.28E+19 1.25E-02 C1 WC06D Charpy 5.00 3.66 22.91 8.67E+18 2.41E+19 1.32E-02 C1 NC34JI2 Charpy 5.00 3.66 21.91 9.10E+18 2.54E+19 1.32E-02 C1 NC34JI3 Charpy 5.00 3.66 20.91 9.52E+18 2.66E+19 1.45E-02 C1 NC34JI4 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+19 1.51E-02 C1 NC34JI5 Charpy 5.00 3.66 18.91 1.03E+19 2.89E+19 1.57E-02 C1 NC34BH2 Charpy 5.00 3.66 17.91 1.07E+19 3.00E+19 1.63E-02	01	WCOBA	Charpy	5.00	3.66	25.91	7.28E+18	2.00E+19	1.10E-02
C1 WC06C Charpy 5.00 3.66 23.91 8.22E+18 2.28E+19 1.25E-02 C1 WC06D Charpy 5.00 3.66 22.91 8.67E+18 2.41E+19 1.32E-02 C1 NC34JI2 Charpy 5.00 3.66 21.91 9.10E+18 2.41E+19 1.32E-02 C1 NC34JI2 Charpy 5.00 3.66 21.91 9.10E+18 2.54E+19 1.38E-02 C1 NC34JI3 Charpy 5.00 3.66 20.91 9.52E+18 2.66E+19 1.45E-02 C1 NC34JI4 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+19 1.51E-02 C1 NC34JI5 Charpy 5.00 3.66 18.91 1.03E+19 2.89E+19 1.57E-02 C1 NC34BH2 Charpy 5.00 3.66 17.91 1.07E+19 3.00E+19 1.63E-02	CI	WC07D	Charpy	5.00	3.66	24.91	7.75E+18	2.14E+19	1.17E-02
C1 WC06D Charpy 5.00 3.66 22.91 8.67E+18 2.41E+19 1.32E-02 C1 NC34JI2 Charpy 5.00 3.66 21.91 9.10E+18 2.54E+19 1.38E-02 C1 NC34JI3 Charpy 5.00 3.66 20.91 9.52E+18 2.66E+19 1.45E-02 C1 NC34JI4 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+19 1.51E-02 C1 NC34JI5 Charpy 5.00 3.66 18.91 1.03E+19 2.89E+19 1.57E-02 C1 NC34BH2 Charpy 5.00 3.66 17.91 1.07E+19 3.00E+19 1.63E-02	C1	WC06C	Charpy	5.00	3.66	23.91	8.22E+18	2.28E+19	1.25E-02
C1 NC34JI2 Charpy 5.00 3.66 21.91 9.10E+18 2.54E+19 1.38E-02 C1 NC34JI3 Charpy 5.00 3.66 20.91 9.52E+18 2.66E+19 1.45E-02 C1 NC34JI4 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+19 1.51E-02 C1 NC34JI5 Charpy 5.00 3.66 18.91 1.03E+19 2.89E+19 1.57E-02 C1 NC34BH2 Charpy 5.00 3.66 17.91 1.07E+19 3.00E+19 1.63E-02	C1	WC06D	Charpy	5.00	3.66	22.91	8.67E+18	2.41E+19	1.32E-02
C1 NC34JI3 Charpy 5.00 3.66 20.91 9.52E+18 2.66E+19 1.45E-02 C1 NC34JI4 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+19 1.51E-02 C1 NC34JI5 Charpy 5.00 3.66 18.91 1.03E+19 2.89E+19 1.57E-02 C1 NC34BH2 Charpy 5.00 3.66 17.91 1.07E+19 3.00E+19 1.63E-02	C1	NC34JI2	Charpy	5.00	3.66	21.91	9.10E+18	2.54E+19	1.38E-02
C1 NC34JI4 Charpy 5.00 3.66 19.91 9.93E+18 2.78E+19 1.51E-02 C1 NC34JI5 Charpy 5.00 3.66 18.91 1.03E+19 2.89E+19 1.57E-02 C1 NC34BH2 Charpy 5.00 3.66 17.91 1.07E+19 3.00E+19 1.63E-02	C1	NC34JI3	Charpy	5.00	3.66	20.91	9.52E+18	2.66E+19	1.45E-02
C1 NC34JI5 Charpy 5.00 3.66 18.91 1.03E+19 2.89E+19 1.57E-02 C1 NC34BH2 Charpy 5.00 3.66 17.91 1.07E+19 3.00E+19 1.63E-02	C1	NC34JI4	Charpy	5.00	3.66	19.91	9.93E+18	2.78E+19	1.51E-02
C1 NC34BH2 Charpy 5.00 3.66 17.91 1.07E+19 3.00E+19 1.63E-02	C1	NC34,115	Charpy	5.00	3.66	18.91	1.03E+19	2.89E+19	1.57E-02
	C1	NC34BH2	Charpy	5.00	3.66	17.91	1.07E+19	3.00E+19	1.63E-02

Table 2. (continued)

	Specimen	phonesis warms and only and and and and	Co	ordinate	S	Flu	ence	
Dieck	ID	Type	X	Y	Z	(E > 1 MeV)	(E > 0.1 MeV)	
BIOCK	10	Type	(cm)	(cm)	(cm)	(cm ⁻²)	(cm ⁻²)	dpa
C1	NC24885	Charny	5.00	3.66	16.91	1.10E+19	3.10E+19	1.68E-02
01	NC34BE5	Charpy	5.00	3.66	15.91	1.14E+19	3.20E+19	1.73E-02
C1	NC34BE3	Charpy	5.00	3.66	14.91	1.17E+19	3.29E+19	1.78E-02
-	115440	Charny	6.65	3.66	26.09	7.17E+18	1.94E+19	1.08E-02
01	HFA12	Charpy	6.65	3.66	25.09	7.65E+18	2.08E+19	1.15E-02
DI	HFA13	Charpy	6.65	3.66	24.09	8.12E+18	2.22E+19	1.22E-02
01	HFA14	Charpy	6.65	3.66	23.09	8.57E+18	2.35E+19	1.29E-02
DI	HFAID	Charpy	6.65	3.66	22.09	9.01E+18	2.47E+19	1.36E-02
01	MFA10	Charpy	6.65	3.66	21.09	9.43E+18	2.60E+19	1.43E-02
D1	HFA17	Charpy	0.05	5.00	21.00	0.402.70		
D1	HFA18	Charpy	7.65	3.66	26.09	7.13E+18	1.91E+19	1.07E-02
D1	HFA19	Charpy	7.65	3.66	25.09	7.61E+18	2.05E+19	1.14E-02
D1	HFA20	Charpy	7.65	3.66	24.09	8.07E+18	2.18E+19	1.21E-02
DI	HFA21	Charpy	7.65	3.66	23.09	8.52E+18	2.31E+19	1.282-02
D1	HFA22	Charpy	7.65	3.66	22.09	8.96E+18	2.44E+19	1.35E-02
D1	HFA23	Charpy	7.65	3.66	21.09	9.38E+18	2.56E+19	1.41E-02
-	NCOLAEA	Charpy	8 74	3.66	26.09	7.06E+18	1.87E+19	1.05E-02
Di	NC3TAE4	Charpy	8 74	3.66	25.09	7.53E+18	2.00E+19	1.13E-02
DI	NC31BE4	Chamy	874	3.66	24.09	7.99E+18	2.13E+19	1.20E-02
01	NCSIDES	Chamy	8 74	3.66	23.09	8.43E+18	2.26E+19	1.26E-02
DI	NCSIDES	Charpy	8 74	3.66	22.09	8.86E+18	2.38E+19	1.33E-02
D1	NC31AA3	Charpy	8.74	3.66	21.09	9.28E+18	2.50E+19	1.39E-02
			0.00	0.00	00.00	0055+19	1 925+10	1 03E-02
D1	FTLB10	Charpy	9.83	3.66	26.09	7 425+19	1 055+10	1 105-02
D1	FTLB09	Charpy	9.83	3.00	25.09	7.425+10	2075+10	1 17E-02
D1	FTLB08	Charpy	9.83	3.00	24.09	0.07E+10	2 20E+19	1 24E-02
D1	FTLB05	Charpy	9.83	3.00	23.09	0.31E+10 0.72E+18	2 32 5+10	1 30E-02
D1	FTLB03	Charpy	9.83	3.00	22.09	0.132+10	2.435+10	1.37E-02
D1	FTLB02	Charpy	9.83	3.00	21.09	6.935+18	1 765+10	1.01E-02
D1	FTLB16	Charpy	10.03	3.00	20.09	7 20E+18	1 89E+19	1.08E-02
D1	FTLB15	Charpy	10.03	3.00	23.09	7 735+18	2 01E+19	1.15E-02
D1	FTLB14	Charpy	10.03	3.00	23.00	8 16E+18	2 13E+19	1.21E-02
DI	FILB13	Charpy	10.03	3.00	23.09	8 58E+18	2 24E+19	1.28E-02
DI	FTLB12	Charpy	10.63	3.00	21.09	8 98E+18	2.35E+19	1.34E-02
D1	FILBII	Charpy	10.65	3.00	21.08	0.502 + 10	2.002.10	
D1	MW9HC	1TCT	7.44	3.45	17.53	1.11E+19	3.02E+19	1.67E-02
D1	MW90D	1TCT	10.03	3.45	17.53	1.08E+19	2.84E+19	1.61E-02
42	MW9ID	1TCT	-8.27	3.45	12.50	8.62E+18	2.45E+19	1.32E-02
A2	MW11KD	1TCT	-8.27	3.45	9.96	9.02E+18	2.56E+19	1.38E-02
A2	MWAIC	1TCT	-8.27	3.45	7.42	9.31E+18	2.65E+19	1.43E-02
A2	MW11KC	1TCT	-8.27	3.45	4.88	9.49E+18	2.70E+19	1.46E-02
A2	MW9JB	1TCT	-8.27	3.45	2.34	9.57E+18	2.73E+19	1.47E-02

Table 2. (continued)

	Specimen	AND THE REPORT OF THE REPORT OF THE REPORT OF THE	C	oordinate	es	Flu	ence	Reaction with the second statements of
Block	ID	Type	X	Y	7	(E > 1 MOV)	(E > 0 1 Main)	
			(cm)	(cm)	(cm)	(cm ⁻²)	(C > 0.1 MeV)	doa
B2	AVISJA	1TCT	-2 16	3.45	12.50	1 145+10	2 205 . 10	upa
B2	MW11IC	1TCT	-2 16	3.45	0.06	1.146+19	3.29E+19	1.76E-02
82	MW9.IC	ITCT	2.10	2 45	9.90	1.19E+19	3.44E+19	1.84E-02
B2	MW/11ID	ITCT	-2.10	0.40	1.42	1.23E+19	3.56E+19	1.90E-02
82	MANOKD	ATCT	-2.10	3.45	4.88	1.26E+19	3.63E+19	1.94E-02
DZ	MAAAUD	inci	-2.10	3.45	2.34	1.27E+19	3.66E+19	1.95E-02
C2	NC31AA2	Charpy	2.04	3.66	12.57	1.20E+19	3.47E+19	1.85E-02
C2	NC31AA4	Charpy	2.04	3.66	11.57	1.23E+19	3.54E+19	1.89E-02
C2	NC31AB1	Charpy	2.04	3.66	10.57	1.25E+19	3.60E+19	1.92E-02
C2	NC31AB2	Charpy	2.04	3.66	9.57	1.27E+19	3.66E+19	1.95E-02
C2	NC31AB3	Charpy	2.04	3.66	8.57	1.29E+19	3.71E+19	1.98E-02
C2	NC31AB5	Charpy	2.04	3.66	7.57	1.30E+19	3.75E+19	2 00E-02
C2	NC31AF4	Charpy	2.04	3.66	6.57	1.31E+19	3 79E+19	2 02E-02
C2	NC31AH2	Charpy	2.04	3.66	5.57	1.32E+19	3 82E+19	2045-02
C2	NC31AH4	Charpy	2.04	3.66	4.57	1.33E+19	3 845+10	2.046-02
C2	NC31BA2	Charpy	2.04	3.66	3.57	1 34E+10	3 865+10	2.000-02
C2	NC31BB3	Charpy	2 04	3.66	2 57	1 345+10	3.000-19	2.000-02
C2	NC31884	Charpy	2.04	3.66	1.57	1 345+10	3.075+10	2.000-02
	11001004	Ondryy	2.04	5.00	1.07	1.346+19	3.8/E+19	2.06E-02
C2	NC31DF4	Charpy	3.04	3.66	12.57	1.22E+19	3.49E+19	1.87E-02
C2	2DE0	Charpy	3.04	3.66	11.57	1.24E+19	3 56E+19	1 91E-02
C2	NC34AA5	Charpy	3.04	3.66	10.57	1 26E+19	3.625+10	1 945-02
C2	2DE2	Charpy	3.04	3.66	9.57	1 28E+10	3 685+10	1.075.02
C2	NC34BH4	Charpy	3.04	3.66	8 57	1 305+10	3.735+10	1.872-02
C2	2DE1	Charny	3.04	3.66	7.57	1 31 540	3.732+19	2.000-02
C2	NC34CEA	Charpy	3.04	3.66	6.57	1.315-10	3.702+19	2.02E-02
C2	2053	Charpy	3.04	3.66	5.57	1.335+19	3.01E+19	2.04E-02
02	NC34664	Charpy	3.04	3.00	0.07	1.345+19	3.842+19	2.05E-02
02	2054	Charpy	3.04	3.00	4.07	1.346+19	3.87E+19	2.07E-02
02	LUE4	Charpy	3.04	3.00	3.57	1.35E+19	3.88E+19	2.07E-02
02	NIVY TIDE 4	Charpy	3.04	3.00	2.57	1.35E+19	3.89E+19	2.08E-02
62	NC34004	Charpy	3.04	3.00	1.57	1.35E+19	3.90E+19	2.08E-02
C2	MW9AC1	Charpy	4.04	3.66	12.57	1.23E+19	3.49E+19	1.88E-02
C2	MWSAC2	Charpy	4.04	3.66	11.57	1.25E+19	3.56E+19	1.91E-02
C2	MW9AC3	Charpy	4.04	3.66	10.57	1.27E+19	3.63E+19	1.95E-02
C2	MW9AC4	Charpy	4.04	3.66	9.57	1.29E+19	3.68E+19	1.98E-02
C2	MW9AC5	Charpy	4.04	3.66	8.57	1.31E+19	3.74E+19	2.01E-02
C2	MW9AI1	Charpy	4.04	3.66	7.57	1.32E+19	3.78E+19	2.03E-02
C2	MW9A12	Charpy	4.04	3.66	6.57	1.34E+19	3.82E+19	2.05E-02
C2	MW9A13	Charpy	4.04	3.66	5.57	1.35E+19	3.85E+19	2.06E-02
C2	MVV9AI4	Charpy	4.04	3.66	4.57	1.35E+19	3.87E+19	2 08E-02
C2	MW9AI5	Charpy	4.04	3.66	3.57	1.36E+19	3 89E+19	2 09E-02
C2	MW9BF2	Charpy	4.04	3.66	2 57	1.365+19	3 90E+19	2 005-02
C2	MW9BF5	Charpy	4.04	3.66	1.57	1.36E+19	3.90E+19	2.09E-02
02	720412	1/27.07	6.74	2.92	13.14	1 285+10	3 805 . 10	2 07E 00
02	720404	1/2T-CT	6.74	2.02	13.14	1.300+19	3.092+19	2.07E-02
02	730104	1/21-01	0.74	2.02	10.00	1.422+19	3.782+19	2.13E-02
02	720405	1/21-01	0.74	2.82	10.60	1.45E+19	3.88E+19	2.17E-02
02	73QH05	1/21-01	6.74	2.82	9.33	1.48E+19	3.96E+19	2.228-02
DZ	MV9HEA	1/21-CT	6.74	2.82	8.06	1.50E+19	4.02E+19	2.25E-02
D2	MW11LFB	1/2T-CT	6.74	2.82	6.79	1.52E+19	4.08E+19	2.288-02
D2	MW9LEB	1/2T-CT	6.74	2.82	5.52	1.54E+19	4.12E+19	2.31E-02
D2	MW11JFB	1/2T-CT	6.74	2.82	4.25	1.55E+19	4.15E+19	2.32E-02
D2	MW9HFA	1/2T-CT	6.74	2.82	2.98	1.55E+19	4.17E+19	2.33E-02
D2	MW11KFAB	1/2T-CT	6.74	2.82	1.71	1.56E+19	4.18E+19	2.34E-02
D2	72PH10	1/2T-CT	6.74	5.36	13.14	9.34E+18	2.84E+19	1.46E-02
D2	73QH03	1/2T-CT	6.74	5.36	11.87	9.58E+18	2.91E+19	1.50E-02
D2	72PH04	1/2T-CT	6.74	5.36	10.60	9.79E+18	2.98E+19	1.53E-02

Table 2. (continued)

Specimen		Co	ordinate	S	Flu	A 19 YO AND A		
Block	ID	Type	X	Y	Z	(E > 1 MeV)	(E > 0.1 MeV)	
DIOCK	iC	.)pc	(cm)	(cm)	(cm)	(cm ⁻²)	(cm ⁻²)	dpa
00	720442	1/2T.CT	6.74	5.36	9.33	9.98E+18	3.04E+19	1.56E-02
DZ	ANA/44LED	1/2T.CT	674	5.36	8.06	1.01E+19	3.09E+19	1.59E-02
DZ	MWITHED	1/21-CT	6.74	5.36	6.70	1035+19	3 13E+19	1.61E-02
D2	MW9IEA	1/21-01	0.74	5.30	5.52	1.045+10	3 17E+19	1 63E-02
D2	MW11MCA	1/21-01	0.74	5.30	0.02	1.045+10	3 105+10	1 64E-02
D2	MW9KFB	1/21-01	6.74	5.30	4.20	1.042+18	3.190+10	1645.02
D2	MW11HFB	1/2T-CT	6.74	5.36	2.98	1.055+19	3.200+19	1.046-02
D2	MW9JEA	1/2T-CT	6.74	5.36	1.71	1.05E+19	3.212+19	1.002-02
D2	72PH09	1/2T-CT	9.80	2.82	13.14	1.34E+19	3.46E+19	1.99E-02
D2	73QH02	1/2T-CT	9.80	2.82	11.87	1.38E+19	3.55E+19	2.04E-02
D2	72PH08	1/2T-CT	9.80	2.82	10.60	1.41E+19	3.64E+19	2.09E-02
D2	73QH14	1/2T-CT	9.80	2.82	9.33	1.43E+19	3.71E+19	2.13E-02
02	MWOCEA	1/2T-CT	9.80	2.82	8.06	1.46E+19	3.77E+19	2.16E-02
02	MANATIER	1/2T-CT	9.80	2.82	6.79	1.48E+19	3.82E+19	2.19E-02
Da	MANOIEA	1/21-01	9.80	2.82	5 52	1.49E+19	3.86E+19	2.21E-02
DZ	MINUTA	1/2T CT	0.80	2.82	4 25	1 50E+19	3.89E+19	2.23E-02
26	MVV111FB	1/21-01 4/07 CT	0.00	2.02	2.08	1.51E+19	3.91E+19	2 24E-02
D2	MVV9LFA	1/21-01	9.00	2.02	1.71	1.51E+10	3 91E+19	2 24E-02
D2	MW11MDB	1/21-01	9.60	2.02	1.71	1.012+10	0.012.10	Au the The Whe
02	730411	1/2T-CT	9.80	5.36	13.14	9.05E+18	2.66E+19	1.40E-02
02	700414	1/2T-CT	9.80	5.36	11.87	9.29E+18	2.73E+19	1.44E-02
02	720114	1/27-07	9.80	5.36	10.6	9.50E+18	2.79E+19	1.47E-02
DZ DZ	730007	1/2T-CT	0.00	5 36	0 33	9 68E+18	2 85E+19	1.50E-02
DZ	72PHU7	1/21-01	9.50	5.30	9.06	0.84E+18	2 90E+19	1.528-02
D2	MW90FA	1/21-01	9.80	5.30	6.00	0.065+18	2 04E+10	1 54E-02
D2	MW11JFA	1/21-01	9.80	5.30	0.79	9.902+10	2.046+10	1 565.02
D2	MW9JFB	1/2T-CT	9.80	5.30	5.52	1.016+19	2.9/2+19	1.502-02
D2	MW11HEA	1/2T-CT	9.80	5.36	4.25	1.012+19	2.992+19	1.572-02
D2	MW9JEB	1/2T-CT	9.80	5.36	2.98	1.02E+19	3.00E+19	1.505-02
D2	MW9HEB	1/2T-CT	9.80	5.36	1.71	1.02E+19	3.01E+19	1.585-02
A3	MW9LA	1TCT	-8.27	3.45	-0.89	9.52E+18	2.71E+19	1.46E-02
A3	MW9LC	1TCT	-8.27	3.45	-3.43	9.35E+18	2.66E+19	1.44E-02
A3	MW11JA	1TCT	-8.27	3.45	-5.97	9.08E+18	2.58E+19	1.39E-02
A3	MW11JD	1TCT	-8.27	3.45	-8.51	8.71E+18	2.47E+19	1.34E-02
A3	MW9LD	1TCT	-8.27	3.45	-11.05	8.24E+18	2.33E+19	1.26E-02
R3	MWOKD	1TCT	-2.16	3.45	-0.89	1.26E+19	3.64E+19	1.94E-02
83	MMAKC	1TCT	-2 16	3 45	-3.43	1.24E+19	3.58E+19	1.91E-02
00	MAA/111C	ITCT	-2 16	3 45	-5.97	1.20E+19	3.47E+19	1.85E-02
83	MANDIR	ATCT	-2.10	3 45	-8.51	1 15E+19	3.32E+19	1.77E-02
B3 B3	MW11LB	1TCT	-2.16	3.45	-11.05	1.09E+19	3.13E+19	1.68E-02
	NOOLDDE	Chamu	2.04	2.66	0.07	1 34E+10	3 865+19	2 06F-02
C3	NC31BB5	Charpy	2.04	3.00	-0.07	1 235+10	3.84E+19	2 05E-02
C3	NC31BF1	Charpy	2.04	3.00	-1.07	1.335+10	3 825+10	2 04E-02
C3	NC34BB2	Charpy	2.04	3.00	-2.07	1.325+19	3.025+10	2.075.02
C3	NC34BF4	Charpy	2.04	3.66	-3.07	1.312+19	3.792+19	2.020-02
C3	NC34BF5	Charpy	2.04	3.66	-4.07	1.30E+19	3.75E+19	2.00E-02
C3	NC34BH1	Charpy	2.04	3.66	-5.07	1.29E+19	3./1E+19	1.982-02
C3	NC34AB2	Charpy	2.04	3.66	-6.07	1.27E+19	3.66E+19	1.95E-02
C3	NC34AB4	Charpy	2.04	3.66	-7.07	1.25E+19	3.60E+19	1.92E-02
C3	NC34AE4	Charpy	2.04	3.66	-8.07	1.23E+19	3.54E+19	1.89E-02
C3	NC34AE5	Charpy	2.04	3.66	-9.07	1.20E+19	3.47E+19	1.85E-02
C3	NC34AF1	Charpy	2.04	3.66	-10.07	1.18E+19	3.39E+19	1.81E-02
C3	NC34AF2	Charpy	2.04	3.66	-11.07	1.15E+19	3.31E+19	1.77E-02
C3	NC31BA4	Charpy	3.04	3.66	-0.07	1.35E+19	3.88E+19	2.07E-02
C3	2DE5	Charpy	3.04	3.66	-1.07	1.34E+19	3.87E+19	2.07E-02
C3	NC31BB1	Charpy	3.04	3.66	-2.07	1.34E+19	3.84E+19	2.05E-02

Table 2. (continued)

	Specimen		С	oordinate	es	Flu	ence	
Block	ID	Туре	X	Y	7	(F > 1 MeV)	(E > 0.1 MoV)	
			(cm)	(cm)	(cm)	(cm ⁻²)	(cm ⁻²)	dpa
C3	2DE6	Charpy	3.04	3.66	-3.07	1.33E+19	3.81E+10	2045.02
C3	NC31BH3	Charpy	3.04	3.66	-4.07	1.31E+19	3 785+10	2.046-02
C3	2DE7	Charpy	3.04	3.66	-5.07	1 30E+10	3 735+10	2.02E-02
C3	NC34BE1	Charpy	3.04	3.66	-8.07	1 285+10	3.735+19	2.002-02
C3	2DE8	Charpy	3.04	3.66	-7.07	1 265+10	3.000+19	1.9/E-02
C3	NC31BH5	Charpy	3.04	3.66	8.07	1.200+19	3.522+19	1.94E-02
C3	2DE9	Charpy	3.04	3.66	-0.07	1.245+19	3.56E+19	1.91E-02
C3	MW118F1	Charpy	3.04	3.66	10.07	1.222+19	3.49E+19	1.87E-02
C3	NC31BF3	Charpy	3.04	3.66	-11.07	1.192+19	3.41E+19	1.83E-02
				0.00	11.07	1.102.113	3.33E+19	1.78E-02
C3	MW9BJ1	Charpy	4.04	3.66	-0.07	1.36E+19	3.89E+19	2.09E-02
C3	MW11AA2	Charpy	4.04	3.66	-1.07	1.35E+19	3.87E+19	2.08E-02
C3	MW11AA3	Charpy	4.04	3.66	-2.07	1.35E+19	3.85E+19	2.06E-02
C3	MW11AB2	Charpy	4.04	3.66	-3.07	1.34E+19	3.82E+19	2 05E-02
C3	MW11AB4	Charpy	4.04	3.66	-4.07	1.32E+19	3.78E+19	2 03E-02
C3	MW11AF5	Charpy	4.04	3.66	-5.07	1.31E+19	3.74E+19	2 01E-02
C3	MW11AG4	Charpy	4.04	3.66	-6.07	1.29E+19	3.69E+19	1 98E-02
C3	MW11AG5	Charpy	4.04	3.66	-7.07	1.27E+19	3 63E+19	1 955-02
C3	MW11AJ2	Charpy	4.04	3.66	-8.07	1 25E+19	3 56E+10	1.015-02
C3	MW118B1	Charpy	4.04	3.66	-9.07	1 235+10	3 405+10	1.912-02
C3	MW11884	Charpy	4.04	3.66	-10.07	1 20E+19	3 425+10	1.845.02
C3	MW11BB5	Charpy	4.04	3.66	-11.07	1.17E+19	3.33E+19	1.79E-02
							0.002.10	1.106-06
D3	MW11LD	1TCT	8.27	3.45	-0.89	1.39E+19	3.78E+19	2.09E-02
D3	MW9NC	1TCT	8.27	3.45	-3.43	1.36E+19	3.71E+19	2.06E-02
D3	MW9NA	1TCT	8.27	3.45	-5.97	1.32E+19	3.60E+19	1.99E-02
D3	MW11JC	1TCT	8.27	3.45	-8.51	1.27E+19	3.45E+19	1.91E-02
D3	MW9NB	1TCT	8.27	3.45	-11.05	1.20E+19	3.25E+19	1.81E-02
A4	72WP214	Charpy	-10.83	3.66	-19.59	4 78F+18	1 32E+19	7 27E-03
A4	72WP215	Charpy	-10.83	3.66	-20.59	4 53E+18	1 245+10	6.90E.03
A4	72WP216	Charpy	-10.83	3.66	-21 59	4 27E+18	1 175+10	6.00E-03
AA	72WP217	Charpy	-10.83	3.66	-22 50	4.00E+18	1.005+10	0.400-03
AA	72WP218	Charpy	-10.83	3.66	23.50	3 735+18	1.092+19	6.00E-03
AA	72WP219	Charpy	-10.83	3.66	-20.50	3 455+19	0.295+19	5.04E-03
Ad	72W/P220	Charpy	-0.83	3.66	10.50	5.40E+10	9.20E+10	5.20E-03
AA	72W/P221	Charpy	-9.83	3.66	-20.50	4 025+10	1.402+19	7.945-03
44	72\A/D222	Charpy	-9.03	3.66	-20.59	4.950-10	1.372+19	7.51E-03
64	7210/0223	Charpy	-9.00	3.66	-21.59	4 255+10	1.200+19	7.07E-03
A 4	7211/0224	Charpy	-9.03	3.00	-22.59	4.300+18	1.20E+19	0.61E-03
M4 A4	7214/0225	Charpy	-9.03	3.00	-23.59	4.00E+18	1.11E+19	6.15E-03
~*	12445220	Charpy	-9.03	3.00	-24.09	3.755+10	1.02E+19	5.07E-03
A4	02D09	Charpy	-8.74	3.66	-19.59	5.64E+18	1.58E+19	8.62E-03
A4	02D10	Charpy	-8.74	3.66	-20.59	5.34E+18	1.50E+19	8.16E-03
A4	02011	Charpy	-8.74	3.66	-21.59	5.03E+18	1.40E+19	7.68E-03
A4	02D12	Charpy	-8.74	3.66	-22.59	4.72E+18	1.31E+19	7.18E-03
A4	02D14	Charpy	-8.74	3.66	-23.59	4.39E+18	1.22E+19	6.68E-03
A4	02D16	Charpy	-8.74	3.66	-24.59	4.06E+18	1.12E+19	6.16E-03
٨٨	72WP226	Charny	.7 65	3.66	.10 50	6 055+18	1715+10	0 27E 02
AA	72\A/P227	Charpy	7.65	3.66	20.50	5 725+ 9	1.625+10	8 77E 02
0.4	7214/0220	Charpy	-7.05	3.00	20.59	5.405+40	1.020+19	0.772-03
A4	72001220	Charpy	-7.00	3.00	-21.59	5.402+18	1.020+19	7.705.00
A4	7200229	Charpy	-7.05	3.00	-22.59	5.00E+18	1.422+19	7.722-03
A4	7200230	Charpy	-7.65	3.66	-23.59	4./1E+18	1.31E+19	7.18E-03
A4	130025	Charpy	-7.65	3.66	-24.59	4.36E+18	1.21E+19	6.62E-03
A4	73WP6	Charpy	-6.65	3.66	-19.59	6.40E+18	1.82E+19	9.82E-03
A4	73WN16	Charpy	-6.65	3.66	-20.59	6.07E+18	1.72E+19	9.29E-03

Table 2. (continued)

NAT STREET, STATUTED IN STREET	Specimen	ana matang ang ang ang ang ang ang ang ang ang	Co	ordinate	S	Flu	ence	
Disale	in	Type	X	Y	Z	(E > 1 MeV)	(E > 0.1 MeV)	
Block	1D	Type	(cm)	(cm)	(cm)	(cm ⁻²)	(cm ⁻²)	dpa
		Chamu	6.65	3.66	-21.59	5.72E+18	1.62E+19	8.75E-03
A4	73WF311	Charpy	-0.05	3.66	.22 59	5.36E+18	1.51E+19	8.19E-03
A4	73WF312	Charpy	-0.05	3.00	22.50	4 99E+18	1.40E+19	7.61E-03
A4	73WF313	Charpy	-0.05	3.00	-23.00	4.61E+18	1 28E+19	7.02E-03
A4	73WF314	Charpy	-6.65	3.66	-24.59	4.012+10	1.202.110	1.022 00
	ARA/1144A	1TCT	-7.44	3.45	-16.03	7.42E+18	2.10E+19	1.14E-02
A4	MW9OC	1TCT	-10.03	3.45	-16.03	6.20E+18	1.72E+19	9.45E-03
		01	E 00	3.66	-19 59	6 94E+18	1.98E+19	1.07E-02
84	02D05	Charpy	-5.00	3.00	-10.50	6 57E+18	1.87E+19	1.01E-02
B4	02D07	Charpy	-5.00	3.00	-20.59	0.072+10	1 785+19	9495-03
84	02D13	Charpy	-5.00	3.66	-21.59	0.192+10	1.00010	8 88E-03
R4	02D15	Charpy	-5.00	3.66	-22.59	5.81E+18	1.046+19	0.000-00
BA	02021	Charpy	-5.00	3.66	-23.59	5.41E+18	1.52E+19	0.20E-03
B4	02D22	Charpy	-5.00	3.66	-24.59	5.00E+18	1.40E+19	7.61E-03
		Charmy	4.00	3.86	-19 59	7.23E+18	2.07E+19	1.11E-02
84	02D24	Charpy	-4.00	3.00	20.50	6 85E+18	1.95E+19	1.05E-02
B4	02D29	Charpy	-4.00	3.00	-20.00	6 455+18	1.84E+19	9 89E-03
B4	02D31	Charpy	-4.00	3.66	-21.59	0.400+10	1 715+10	0.25E-03
B4	02D32	Charpy	-4.00	3.66	-22.59	6.05E+18	1.716+19	9.200-03
R4	02D37	Charpy	-4.00	3.66	-23.59	5.63E+18	1.59E+19	8.60E-03
B4	02D39	Charpy	-4.00	3.66	-24.59	5.21E+18	1.46E+19	7.94E-03
	00000	Charny	.2 01	3.66	-19 59	7.52E+18	2.15E+19	1.15E-02
84	02026	Charpy	-2.91	3.66	20.50	7 12E+18	2 03E+19	1.09E-02
B4	02D27	Charpy	-2.91	3.00	-20.00	6 715+18	1 01E+10	1.03E-02
B4	02D28	Charpy	-2.91	3.00	-21.59	0.712+10	1 795+10	9.62E-03
B4	02D30	Charpy	-2.91	3.66	-22.59	0.292+18	1.705-19	9.02E-03
B4	02D33	Charpy	-2.91	3.66	-23.59	5.86E+18	1.056+19	0.940-03
B4	02D34	Charpy	-2.91	3.66	-24.59	5.42E+18	1.52E+19	8.25E-03
	02045	Charny	-1.82	3.66	-19.59	7.77E+18	2.222+19	1.19E-02
84	02045	Chamy	1.82	3.66	-20 59	7.36E+18	2.10E+19	1.13E-02
64	02047	Charpy	1.02	3.66	-21 59	6 94E+18	1.97E+19	1.06E-02
B4	02D48	Charpy	-1.02	3.00	22.50	6 50E+18	1 84E+19	9.94E-03
24	WC12C	Charpy	-1.82	3.00	-22.09	6.00E+10	1715+10	9 24E-03
B4	WC14A	Charpy	-1.82	3.66	-23.59	0.000+10	1.712+10	8 535-03
B4	WC14B	Charpy	-1.82	3.66	-24.59	5.60E+18	1.576+19	0.556-05
R4	WC12D	Charpy	-0.82	3.66	-19.59	7.98E+18	2.28E+19	1.22E-02
04	WCIAD	Charpy	-0.82	3.66	-20.59	7.56E+18	2.15E+19	1.16E-02
84	VVC14D	Charpy	0.82	3.66	-21 59	7.12E+18	2.02E+19	1.09E-02
84	WC14E	Charpy	-0.02	3.66	22 50	6 68E+18	1.89E+19	1.02E-02
B4	99A-5559	Charpy	-0.02	3.00	22.50	6 225+18	1755+19	9 48E-03
84	99A-5560	Charpy	-0.82	3.00	-23.59	0.22E+10	1615+10	8 74E-03
B4	99A-5561	Charpy	-0.82	3.66	-24.59	5.75E+10	1.012+13	0.142-05
B4	MW90B	1TCT	-1.62	3.45	-16.03	9.47E+18	2.70E+19	1.45E-02
B4	MW9CA	1TCT	-4.21	3.45	-16.03	8.69E+18	2.48E+19	1.33E-02
~	7014/5040	Charpy	0.82	3.66	-13.47	1.06E+19	3.05E+19	1.63E-02
64	73005310	Charpy	0.02	3.66	14 47	1.02E+19	2 94E+19	1.57E-02
C4	73WF319	Charpy	0.82	3.00	- 100,007	0.0000000	2 845+10	1.52E-02
C4	73WF320	Charpy	0.82	3.00	-15.47	9.095+10	2.042+10	1 465.02
C4	73WF321	Charpy	0.82	3.66	-16.47	9.526+18	2.752+18	1 405 02
C4	73WF322	Charpy	0.82	3.66	-17.47	9.13E+18	2.012+19	1.402-02
C4	73WF323	Charpy	0.82	3.66	-18.47	8.72E+18	2.49E+19	1.34E-02
C4	73WF334	Charpy	0.82	3.66	-19.47	8.30E+18	2.36E+19	1.27E-02
CA	73WF337	Charpy	0.82	3.66	-20.47	7.87E+18	2.23E+19	1.20E-02
CA	7314/5339	Charpy	0.82	3.66	-21.47	7.42E+18	2.10E+19	1.13E-02
CA	72\//5220	Charpy	0.82	3.66	-22.47	6.96E+18	1.96E+19	1.06E-02
C.4	7214/5240	Charpy	0.82	3.66	-23 47	6.49E+18	1.82E+19	9.88E-03
04	7300-340	Charpy	0.02	3.66	.24 47	6 01E+18	1.67E+19	9.12E-03
64	1344-353	Charpy	0.02	0.00	24.41	0.011.10	1.	

Table 2. (continued)

	Specimen		С	oordinate	es	Flu		
Block	ID	Туре	X	Y	Z	(E > 1 MeV)	(E > 0.1 MeV)	
		WATCHINE IN THE OWNER WATCHING IN THE REAL PROPERTY OF	(cm)	(cm)	(cm)	(cm ⁻²)	(cm ⁻²)	dpa
C4	7014/5055	Ohanni	1.00				and a second particular production of the product of the second data and an	
04	73VVF355	Charpy	1.82	3.66	-13.47	1.07E+19	3.08E+19	1.65E-02
04	73WF356	Charpy	1.82	3.66	-14.47	1.04E+19	2.98E+19	1.60E-02
64	73WF357	Charpy	1.82	3.66	-15.47	1.00E+19	2.87E+19	1.54E-02
C4	73WF358	Charpy	1.82	3.66	-16.47	9.66E+18	2.76E+19	1.48E-02
C4	73WF370	Charpy	1.82	3.66	-17.47	9.27E+18	2.64E+19	1.42E-02
C4	73W311	Charpy	1.82	3.66	-18.47	8.86E+18	2.52E+19	1.36E-02
C4	73W363	Charpy	1.82	3.66	-19.47	8.43E+18	2.39E+19	1.29E-02
C4	73W433	Charpy	1.82	3.66	-20.47	7.99E+18	2.26E+19	1.22E-02
C4	73W463	Charpy	1.82	3.66	-21.47	7.54E+18	2.12E+19	1 15E-02
C4	73W536	Charpy	1.82	3.66	-22.47	7.07E+18	1 98E+19	1 08E-02
C4	73W538	Charpy	1.82	3.66	-23.47	6.59E+18	1 84E+19	1.00E-02
C4	73W539	Charpy	1.82	3.66	-24.47	6.10E+18	1.69E+19	9.25E-03
C4	MW98D2	Charpy	2.91	3.66	-13.47	1.09E+19	3 10E+19	1 67E-02
C4	MW9BD3	Charpy	2.91	3.66	-14.47	1.05E+19	3.00E+19	1.615.02
C4	MW9BD4	Charpy	2.91	3.66	-15.47	1.02E+10	2 905+10	1.012-02
C4	MW9BD5	Charpy	2.91	3.66	-16.47	0 785+18	2.092+19	1.502-02
C4	MW9CE1	Charpy	2.91	3.66	17 47	0.205+10	2.700+19	1.50E-02
C4	MW9CE2	Charpy	2.01	3.86	19 47	9.395+10	2.000+19	1.43E-02
C4	MWQCE3	Charpy	2.01	3.66	-10.47	0.9/2+10	2.04E+19	1.37E-02
CA	MINOCEA	Charpy	2.91	3.00	-19.47	8.54E+18	2.41E+19	1.30E-02
CA	MANOCES	Charpy	2.91	3.50	-20.47	8.09E+18	2.27E+19	1.23E-02
CA	NIVAACED	Charpy	2.91	3.00	-21.47	7.63E+18	2.14E+19	1.16E-02
04	NCSTAFT	Charpy	2.91	3.66	-22.47	7.16E+18	2.00E+19	1.09E-02
64	NC31AF3	Charpy	2.91	3.66	-23.47	6.67E+18	1.85E+19	1.01E-02
C4	NC31AE2	Charpy	2.91	3.66	-24.47	6.18E+18	1.70E+19	9.35E-03
C4	73W701	Charpy	4.00	3.66	-13.47	1.10E+19	3.11E+19	1.68E-02
C4	73W702	Charpy	4.00	3.66	-14.47	1.06E+19	3.01E+19	1.62E-02
C4	73W704	Charpy	4.00	3.66	-15.47	1.02E+19	2.90E+19	1.56E-02
C4	73W705	Charpy	4.00	3.66	-16.47	9.86E+18	2.78E+19	1.50E-02
C4	73W707	Charpy	4.00	3.66	-17.47	9.46E+18	2.66E+19	1.44E-02
C4	73W709	Charpy	4.00	3.66	-18.47	9.04E+18	2.54E+19	1.38E-02
C4	73W710	Charpy	4.00	3.66	-19.47	8.61E+18	2.41E+19	1.31E-02
C4	73W712	Charpy	4.00	3.66	-20.47	8.16E+18	2.28E+19	1.24E-02
C4	73W714	Charpy	4.00	3.66	-21.47	7.70E+18	2.14E+19	1.17E-02
C4	73W715	Charpy	4.00	3.66	-22.47	7.22E+18	2.00E+19	1.09E-02
C4	73W716	Charpy	4.00	3.66	-23.47	673E+18	1865+19	1.025-02
C4	73W718	Charpy	4.00	3.66	-24.47	6.23E+18	1.71E+19	9.40E-03
C4	73W541	Charpy	5.00	3.66	-13.47	1.10E+19	3 10E+19	1.68E-02
C4	99-5528	Charpy	5.00	3.66	-14 47	107E+19	3 00E+19	1.625.02
C4	99-5529	Charpy	5.00	3.66	-15 47	103E+19	2 895+19	1.575-02
C4	99-5530	Charpy	5.00	3.66	-16.47	9 90E+18	2 775+10	1.515.02
CA	99-5531	Charpy	5.00	3.66	17 47	0.500+10	2.772+19	1.512-02
C4	99-5532	Charpy	5.00	3.66	18 47	0.0000+10	2.002+19	1.446-02
CA	00.6533	Charpy	5.00	3.66	10.47	9.002+10	2.036+19	1.30E-02
CA	00 5534	Charpy	5.00	3.00	-19.47	0.042+10	2.402+19	1.31E-02
CA	00 6525	Charpy	5.00	3.00	-20.47	0.192+10	2.2/E+19	1.24E-02
CA	99-0000	Charpy	5.00	3.00	-21.47	7.725+18	2.13E+19	1.178-02
04	99-5536	Charpy	5.00	3.00	-22.47	7.25E+18	1.99E+19	1.10E-02
C4	99-5638	Charpy	5.00	3.66	-23.47	6.75E+18 6.25E+18	1.85E+19 1.70E+19	1.02E-02 9.41E-03
-	MOOOD	Charma	0.00	2.00	10.00	0.000		
04	WCOSD	Charpy	6.65	3.66	-19.59	8.57E+18	2.35E+19	1.29E-02
04	WC08C	Charpy	6.65	3.66	-20.59	8.12E+18	2.22E+19	1.22E-02
04	WC08B	Charpy	6.65	3.66	-21.59	7.65E+18	2.09E+19	1.15E-02
04	WC08A	Charpy	6.65	3.66	-22.59	7.17E+18	1.95E+19	1.08E-02
04	WC12A	Charpy	6.65	3.66	-23.59	6.68E+18	1.80E+19	1.00E-02

Table 2.	(continued)
----------	-------------

Specimen			Co	ordinate	S	Flu		
Block	ID	Туре	X (cm)	Y (cm)	Z (cm)	(E > 1 MeV) (cm ⁻²)	(E > 0.1 MeV) (cm ⁻²)	dpa
D4	WC13D	Charpy	6.65	3.66	-24.59	6.18E+18	1.66E+19	9.26E-03
DA	WC068	Charpy	7.65	3.66	-19.59	8.52E+18	2.32E+19	1.28E-02
DA	WC14C	Charpy	7.65	3.66	-20.59	8.07E+18	2.19E+19	1.21E-02
04	WC12B	Charpy	7.65	3.66	-21.59	7.61E+18	2.05E+19	1.14E-02
04	WCOZE	Charpy	7.65	3.66	-22.59	7.13E+18	1.92E+19	1.07E-02
04	WCORE	Charpy	7.65	3.66	-23.59	6.64E+18	1.78E+19	9.94E-03
D4	72WP201	Charpy	7.65	3.66	-24.59	6.14E+18	1.63E+19	9.17E-03
-	NC24AH2	Charpy	8.74	3.66	-19.59	8.43E+18	2.26E+19	1.26E-02
04	NCOMARIZ	Charpy	874	3.66	-20.59	7.99E+18	2.14E+19	1.20E-02
DA	NC34AHS	Charpy	874	3.66	-21.59	7.53E+18	2.01E+19	1.13E-02
04	NCOMPAG	Chamy	8.74	3.66	-22.59	7.06E+18	1.87E+19	1.05E-02
04	NC34BAS	Charpy	8 74	3.66	-23.59	6.57E+18	1.74E+19	9.80E-03
D4 D4	NC34DF3	Charpy	8.74	3.66	-24.59	6.08E+18	1.60E+19	9.04E-03
-	2014/0202	Chamy	9.83	3.66	-19 59	8.31E+18	2.20E+19	1.24E-02
04	72002202	Charpy	0.83	3.66	-20.59	7.87E+18	2.08E+19	1.17E-02
04	7200203	Charpy	0.83	3.66	-21 59	7.42E+18	1.95E+19	1.10E-02
D4	7200204	Charpy	0.83	3.66	-22 59	6.95E+18	1.82E+19	1.03E-02
D4	72WP205	Charpy	0.83	3.66	-23 59	6.48E+18	1.69E+19	9.61E-03
D4	72WP208	Charpy	9.83	3.66	-24.59	5.99E+18	1.55E+19	8.86E-03
	7014/0000	Charny	10.83	3.66	-19 59	8.16E+18	2.13E+19	1.21E-02
04	72WP208	Charpy	10.03	3.66	-20 59	7 73E+18	2.01E+19	1.15E-02
D4	72WP209	Charpy	10.83	3.66	-21 59	7 29E+18	1.89E+19	1.08E-02
D4	7200-210	Charpy	10.03	3.00	-22 59	6.83E+18	1.76E+19	1.01E-02
D4	72WP211	Charpy	10.03	3.00	-22.50	6 36E+18	1.64E+19	9.39E-03
D4	72WP212	Charpy	10.03	3.00	24.50	5 88E+18	1.50E+19	8.67E-03
D4	72WP213	Charpy	10.83	3.00	-24.08	0.002.10		
04	MW11HC	1TCT	7.44	3.45	-16.03	1.03E+19	2.81E+19	1.56E-02
D4	MW9HA	1TCT	10.03	3.45	-16.03	1.00E+19	2.64E+19	1.50E-02

The most likely reason for the different fitting parameters obtained for the HSSI 10.0D and HSSI 10.05 capsules is the arrangement of dosimeters in the two capsules. The difference that appears to be most important is the inclusion of dosimeters near the face of the capsule next to the core. In the HSSI 10.05 capsule, some dosimeters were located within 1.0 cm of the capsule face. In the HSSI 10.0D capsule, the closest dosimeter was located 2.25 cm from the capsule face. To test this hypothesis, a separate adjustment run was made for the HSSI 10.05 capsule omitting all dosimeters that were located within 2.25 cm of the face of the capsule. Three-dimensional fitting constants derived from the test run were closer to the values obtained for the HSSI 10.0D experiment. For example, for the fast flux (E > 1 MeV), the normalization constant A and the attenuation constant λ were only 3.1% and 1.7% smaller than the respective values for the HSSI 10.0D experiment. The good agreement between the attenuation coefficients supports the hypothesis. The flux magnitude and hence the normalization constant A are also in good agreement but may be affected by other differences in the irradiations such as reactor core loadings.

Uncertainties are not accurately propagated through all the computational sequences, and there may be biases that are not recognized. However, uncertainties obtained from the least-squares adjustment procedure take into account estimated uncertainties of neutronics calculations and measured activities. Uncertainties for the exposure parameter rates obtained from the adjustment calculations at the locations of the dosimeters are approximately 4% (1 σ). When irradiation exposure rates are calculated

from Eq. 2, uncertainties arising from the three-dimensional fitting should also be considered. Differences between the exposure parameter rates at the dosimetry locations, as obtained from the adjustment and as calculated from the fitting function, are on the order of 1% (averaged over all dosimetry locations) and at some points reach approximately 4%. Therefore, for the irradiation exposure parameters obtained from Eq. 2, an uncertainty of 6% (1 σ) is considered to be a good estimate.

Conclusion

The irradiation exposure parameter distributions in the HSSI 10.05 capsule were determined. Exposure parameters were reported for all the metallurgical specimens at the important notch-tip locations and in the form of three-dimensional fitting functions. It is recommended that an uncertainty of 6% (1 σ) be associated with the exposure parameters obtained from the three-dimensional fits.

References

- I. Remec, C. A. Baldwin, and F. B. K. Kam, Lockheed Martin Energy Research Corporation, Oak Ridge Natl. Lab., Oak Ridge, Tenn., Neutron Exposure Parameters for the Dosimetry Capsule in the HSSI Program Tention and Series, USNRC Report NUREG/CR-6601 (ORNL/TM-13549), October 1998.
- F. W. Stallmann, Lockie J Martin Energy Research Corporation, Oak Ridge Natl. Lab., Oak Ridge, Tenn., LSL-M2: A Computer Program for Least-Squares Logarithmic Adjustment of Neutron Spectra, USNRC Report NUREG/CR-4349 (ORNL/TM-9933), March 1986.
- 3. R. E. Maerker et al., Electric Power Research Institute, Palo Alto, Calif., Revision and Extension of the Data Base in the LEPRICON Dosimetry Methodology, EPRI NP-3841, January 1985.
- 4. F. W. Stallmann, Lockheed Martin Energy Research Corporation, Oak Ridge Natl. Lab., Oak Ridge, Tenn., Determination of the Damage Exposure Parameter Values in the PSF Metallurgical Irradiation Experiment, USNRC Report NUREG/CR-3841 (ORNL/TM-9166), October 1984.
- 5. American Society for Testing and Materials (ASTM), E-693, Standard Practice for Characterizing Neutron Exposures in Ferritic Steels in Terms of Displacements Per Atom (DPA), Annual Book of ASTM Standards.

Appendix

The data included in this Appendix should be sufficient for another organization to recalculate the exposure parameters if fluence rate spectra are available or if neutronics calculations are performed. In particular, the data included herein are (1) specific activities of each dosimeter at the end of irradiation (Table A.1), (2) coordinates of each dosimeter relative to the coordinate system shown in Figs. 3 and 4 (Table A.1), and (3) the irradiation history of the capsule (Table A.2). Specific activities of the removable dosimeter tube (RDT) dosimeters are also given (Table A.3). Only the north RDT was installed during the second part of irradiation because of damage to the south RDT holder.

a subserved, the descent of some particular stand of the	THE PARTY CONTRACTOR OF A	Co	ordinates		Activity*
		X	Yt	Z	at EOI**
Dosimeter ID	Reaction	(cm)	(cm)	(cm)	(bd/mg)
A1 111 1	Fe-54 (n.p) Mn-54	-10.33	3.66	25.59	3.96E+03
A1-111-1	Fe-54 (n.p) Mn-54	-10.33	3.66	23.59	4.25E+03
A1-111-2	Fe-54 (n.p) Mn-54	-10.33	3.66	21.59	4.65E+03
A1-11-01	Fe-54 (n.p) Mn-54	-7.44	4.41	17.53	6.25E+03
A1-11-02	Fe-54 (n,p) Mn-54	-10.03	4.41	17.53	5.45E+03
B1-121-1	Fe-54 (n.p) Mn-54	-4.50	3.66	25.59	5.18E+03
B1-121-2	Fe-54 (n.p) Mn-54	-4.50	3.66	23.59	5.71E+03
B1-121-2	Fe-54 (n.p) Mn-54	-4.50	3.66	21.59	6.26E+03
B1-122-1	Fe-54 (n.p) Mn-54	-1.32	3.66	25.59	5.88E+03
B1-122-1	Fe-54 (n.p) Mn-54	-1.32	3.66	23.59	6.52E+03
D1-122-2	Fe-54 (n.p) Mn-54	-1.32	3.66	21.59	7.09E+03
D1-122-5	Fe-54 (n p) Mn-54	-1.62	4.41	17.53	7.85E+03
B1-12-02	Fe-54 (n,p) Mn-54	-4.21	4.41	17.53	7.17E+03
C1 11 01	Fe-54 (n p) Mn-54	1.32	3.66	25.27	6.12E+03
01-11-01	Fe-54 (n p) Mn-54	1.32	3.66	22.87	6.82E+03
C1-11-02	Fe-54 (n.p) Mr-54	1.32	3.66	20.47	7.80E+03
C1-11-03	Fe-54 (n.p) Mn-54	1.32	3.66	18.07	8.45E+03
01-11-04	Fo.54 (n.p) Mp-54	1.32	3.66	15.67	8.90E+03
C1-11-05	Fe-54 (n.p) Mn-54	4.50	3.66	25.27	6.45E+03
01-12-01	Fe-54 (n.p) Mn-54	4.50	3.66	22.87	7.23E+03
01-12-02	Fe-54 (n p) Mn-54	4.50	3.66	20.47	8.07E+03
01-12-03	Fo.54 (n.p) Mn-54	4.50	3.66	18.07	8.82E+03
C1-12-04 C1-12-05	Fe-54 (n,p) Mn-54	4.50	3.66	15.67	9.29E+03
		7 15	3.66	25 59	6.37E+03
D1-131-1	Fe-54 (n,p) Mn-54	7.15	3.66	23.59	7.18E+03
D1-131-2	Fe-54 (n,p) Mn-54	7.15	3.66	21.59	7.98E+03
D1-131-3	Fe-54 (n,p) Mn-54	10.33	3.66	25 59	6.45E+03
D1-132-1	Fe-54 (n,p) Mn-54	10.33	3.66	23.59	7 16E+03
D1-132-2	Fe-54 (n,p) Mn-54	10.33	3.00	21.59	7.70E+03
D1-132-3	Fe-54 (n,p) Mn-54	10.33	4 4 1	17 53	9.01E+03
D1-13-01	Fe-54 (n,p) Mn-54	7.44	A A 1	17 53	9 04E+03
D1-13-02	Fe-54 (n,p) Mn-54	1.44	4.41	11.00	
A2-211-1	Fe-54 (n.p) Mn-54	-8.27	4.41	12.32	6.71E+03
A2-211-2	Fe-54 (n.p) Mn-54	-8.27	4.41	9.82	6.85E+03
A2-211-3	Fe-54 (n.p) Mn-54	-8.27	4.41	7.32	6.95E+03
A2-211-4	Fe-54 (n.p) Mn-54	-8.27	4.41	4.82	7.15E+03
A2-211-5	Fe-54 (n,p) Mn-54	-8.27	4.41	2.32	6.96E+03
B2-221-1	Fe-54 (n.p) Mn-54	-2.16	4.41	12.32	8.53E+03
B2-221-2	Fe-54 (n.p) Mn-54	-2.16	4.41	9.82	8.71E+03
B2-221-2	Fe-54 (n.p) Mn-54	-2.16	4.41	7.32	8.96E+03
B2-221-4	Fe-54 (n n) Mn-54	-2.16	4.41	4.82	9.12E+03
82-221-5	Fe-54 (n.p) Mn-54	-2.16	4.41	2.32	9.02E+03

Table A.1. Activities of the dosimeters in the HSSI 10.05 capsule

. 00

NUREG/CR-6600

, I

Contraction of a state of the second state of the state of the second state of the sec		C	oordinate	s	Activity*
Dosimeter		X	Y [†]	Z	at EOI**
ID	Reaction	(cm)	(cm)	(cm)	(Bq/mg)
C2-21-01	Fe-54 (n,p) Mn-54	2.53	3.66	11.87	9 90E+03
C2-21-02	Fe-54 (n,p) Mn-54	2.54	3.66	9 47	1.03E+04
C2-21-03	Fe-54 (n,p) Mn-54	2.53	3.66	7.07	1.05E+04
C2-21-04	Fe-54 (n,p) Mn-54	2.54	3.66	4.67	1.05E+04
C2-21-05	Fe-54 (n,p) Mn-54	2.54	3.66	2.27	1.05E+04
D2-231-1	Fe-54 (n,p) Mn-54	6.74	2.18	12.32	1.35E+04
D2-231-2	Fe-54 (n,p) Mn-54	6.74	2.18	9.82	1.44E+04
D2-231-3	Fe-54 (n,p) Mn-54	6.74	2.18	7.32	1.42E+04
D2-231-4	Fe-54 (n,p) Mn-54	6.74	2.18	4.82	1.40E+04
D2-231-5	Fe-54 (n,p) Mn-54	6.74	2.18	2.32	1.43E+04
D2-233-1	Fe-54 (n,p) Mn-54	9.80	2.18	12.32	1.31E+04
D2-233-2	Fe-54 (n,p) Mn-54	9.80	2.18	9.82	1.38E+04
D2-233-3	Fe-54 (n,p) Mn-54	9 80	2.18	7.32	1.41E+04
D2-233-4	Fe-54 (n,p) Mn-54	9.80	2.18	4.82	1.41E+04
D2-233-5	Fe-54 (n,p) Mn-54	9.80	2.18	2.32	1.40E+04
D2-234-1	Fe-54 (n,p) Mn-54	9.80	5.99	12.32	6.95E+03
D2-234-2	Fe-54 (n,p) Mn-54	9.80	5.99	9.82	7.16E+03
D2-234-3	Fe-54 (n,p) Mn-54	9.80	5.99	7.32	7.50E+03
D2-234-4	Fe-54 (n,p) Mn-54	9.80	5.99	4.82	7.57E+03
D2-234-5	Fe-54 (n,p) Mn-54	9.80	5.99	2.32	7.45E+03
A3-311-1	Fe-54 (n,p) Mn-54	-8.27	4.41	-0.82	6.89E+03
A3-311-2	Fe-54 (n,p) Mn-54	-8.27	4.41	-3.32	6.74E+03
A3-311-3	Fe-54 (n,p) Mn-54	-8.27	4.41	-5.82	6.69E+03
A3-311-4	Fe-54 (n,p) Mn-54	-8.27	4.41	-8.32	6.48E+03
A3-311-5	Fe-54 (n,p) Mn-54	-8.27	4.41	-10.82	6.10E+03
B3-321-1	Fe-54 (n,p) Mn-54	-2.16	4.41	-0.82	9.03E+03
B3-321-2	Fe-54 (n,p) Mn-54	-2.18	4.41	-3.32	8.97E+03
B3-321-3	Fe-54 (n,p) Mn-54	-2.16	4.41	-5.82	8.81E+03
B3-321-4	Fe-54 (n,p) Mn-54	-2.16	4.41	-8.32	8.35E+03
B3-321-5	Fe-54 (n,p) Mn-54	-2.16	4.41	-10.82	7.66E+03
C3-31-01	Fe-54 (n,p) Mn-54	2.54	3.66	-0.77	1.03E+04
C3-31-02	Fe-54 (n,p) Mn-54	2.54	3.66	-3.17	1.04E+04
C3-31-03	Fe-54 (n,p) Mn-54	2.54	3.66	-5.57	1.02E+04
C3-31-04	Fe-54 (n,p) Mn-54	2.54	3.66	-7.97	9.79E+03
C3-31-05	Fe-54 (n,p) Mn-54	2.54	3.66	-10.37	9.30E+03
D3-331-1	Fe-54 (n,p) Mn-54	8.27	4.41	-0.82	1.07E+04
D3-331-2	Fe-54 (n,p) Mn-54	8.27	4.41	-3.32	1.06E+04
D3-331-3	Fe-54 (n,p) Mn-54	8.27	4.41	-5.82	1.03E+04
D3-331-4	Fe-54 (n,p) Mn-54	8.27	4.41	-8.32	9.94E+03
D3-331-5	Fe-54 (n,p) Mn-54	8.27	4.41	-10.82	9.33E+03
A4-211-1	Fe-54 (n.p) Mn-54	-10.33	3.66	-20.09	3.98E+03
A4-211-2	Fe-54 (n,p) Mn-54	-10.33	3.66	-22.09	3.57E+03
A4-211-3	Fe-54 (n,p) Mn-54	-10.33	3.66	-24.09	3.10E+03

Table A.1 (continued)

approach and belowing the or any address of the set of t	and a summing of the summer state in the summer of the summer states and the summer summer summer summer summer	Co	ordinates		Activity*
Desimator		×	Yt	Z	at EOI**
Dosimeter	Reaction	(cm)	(cm)	(cm)	(Bq/mg)
10	En Ed (n n) Man 54	-7 15	3.66	-20.09	4.73E+03
A4-212-1	Fe-54 (n,p) Mn-54	-7 15	3.66	-22.09	4.23E+03
A4-212-2	Fe-54 (n,p) Mn-54	-7 15	3.66	-24.09	3.75E+03
A4-212-3	Fe-54 (n,p) Mn-54	-7 44	4.41	-16.03	5.67E+03
A4-21-01	Fe-54 (n,p) Mn-54	-10.03	4.41	-16.03	4.89E+03
A4-21-02	re-54 (n,p) Mir-54	10.00			
D4 004 4	Eq.54 (n n) Mn-54	-4.50	3.66	-20.09	5.43E+03
B4-221-1	Ee-54 (n.p) Mn-54	-4.50	3.66	-22.09	4.89E+03
D4-221-2	Fe-54 (n.p) Mn-54	-4.50	3.66	-24.09	4.16E+03
B4-221-3	Fe-54 (n.p) Mn-54	-1.32	3.66	-20.09	6.03E+03
D4-222-1	Fe-54 (n.p) Mn-54	-1.32	3.66	-22.09	5.25E+03
D4-222-2	Fe-54 (n.p) Mn-54	-1.32	3.66	-24.09	4.46E+03
D4-222-01	Fe-54 (n p) Mn-54	-1.62	4.41	-16.03	6.99E+03
D4-22-01	Fe-54 (n p) Mn-54	-4.21	4.41	-16.03	6.41E+03
04-22-02	10.04 (11.0) 1111 01				
C4-41-01	Fe-54 (n.p) Mn-54	1.32	3.66	-14.17	8.11E+03
C4-41-07	Fe-54 (n.p) Mn-54	1.32	3.66	-16.57	7.54E+03
CA-41-02	Fe-54 (n.p) Mn-54	1.32	3.66	-18.97	6.65E+03
C4-41-04	Fe-54 (n.p) Mn-54	1.32	3.66	-21.37	5.73E+03
CA-41-05	Fe-54 (n.p) Mn-54	1.32	3.66	-23.77	4.96E+03
CA-42-01	Fe-54 (n.p) Mn-54	4.50	3.66	-14.17	8.57E+03
CA-42-07	Fe-54 (n.p) Mn-54	4.50	3.66	-16.57	7.81E+03
CA-42-02	Fe-54 (n.p) Mn-54	4.50	3.66	-18.97	7.02E+03
C4-42-04	Fe-54 (n.p) Mn-54	4.50	3.66	-21.37	6.07E+03
C4-42-05	Fe-54 (n.p) Mn-54	4.50	3.66	-23.77	5.25E+03
011200					0 775.00
D4-231-1	Fe-54 (n,p) Mn-54	7.15	3.66	-20.09	6.77E+03
D4-231-2	Fe-54 (n,p) Mn-54	7.15	3.66	-22.09	6.00E+03
D4-231-3	Fe-54 (n,p) Mn-54	7.15	3.66	-24.09	5.14E+03
D4-232-1	Fe-54 (n,p) Mn-54	10.33	3.66	-20.09	6.75E+03
D4-232-2	Fe-54 (n,p) Mn-54	10.33	3.66	-22.09	5.972+03
D4-232-3	Fe-54 (n,p) Mn-54	10.33	3.66	-24.09	5.17E+03
D4-23-01	Fe-54 (n,p) Mn-54	10.03	4.41	-16.03	8.05E+03
D4-23-02	Fe-54 (n,p) Mn-54	7.44	4.41	-16.03	0.04E+03
		0.04	4.54	22.07	101E+04
Y-1-1	Fe-54 (n,p) Mn-54	0.24	1.04	23.97	7 93E+03
Y-1-2	Fe-54 (n,p) Mn-54	0.24	2.79	23.97	5.81E+03
Y-1-3	Fe-54 (n,p) Mn-54	0.24	4.04	23.97	4 51E+03
Y-1-4	Fe-54 (n,p) Mn-54	0.24	0.20	23.07	3 60E+03
Y-1-5	Fe-54 (n,p) Mn-54	0.24	7 70	23.07	3 22E+03
Y-1-6	Fe-54 (n,p) Mn-54	0.24	1.19	1 99	1.63E+04
Y-2-1	Fe-54 (n,p) Mn-54	1.40	2 70	1 99	123E+04
Y-2-2	Fe-54 (n,p) Mn-54	1.40	4.04	1.99	9.46E+03
Y-2-3	Fe-54 (n,p) Mn-54	1.40	5.29	1 99	7.19E+03
Y-2-4	Fe-54 (n,p) Mn-54	1.40	6.54	1 99	5.83E+03
Y-2-5	Fe-54 (n,p) Mn-54	1.40	7 70	1 99	4.91E+03
Y-2-6	Fe-54 (n,p) Mn-54	0.24	1.54	-22 46	8.37E+03
Y-3-1	Fe-54 (n,p) Mn-54	-0.24	2 79	-22 46	6.34E+03
Y-3-2	Fe-54 (n,p) Mn-54	-0.24	4 04	-22.46	4.90E+03
Y-3-3	Fe-54 (n,p) Mn-54	-0.24	5 29	-22.46	3.79E+03
Y-3-4	re-54 (n,p) Mn-54	.24	0. de 0		

Table A.1 (continued)

N

NUREG/CR-6600

1

ю

		C	Coordinate	es	Activity*
Dosimeter		X	Y [†]	Z	at EOI**
ID	Reaction	(cm)	(cm)	(cm)	(Bq/mg)
Y-3-5	Fe-54 (n,p) Mn-54	-0.24	6.54	-22 46	2 98E+03
Y-3-6	Fe-54 (n,p) Mn-54	-0.24	7.79	-22.46	2.59E+03
X-1-01	Fe-54 (n,p) Mn-54	11.53	1.00	14 15	1716+04
X-1-02	Fe-54 (n,p) Mn-54	9.50	1.00	14 15	170E+04
X-1-03	Fe-54 (n,p) Mn-54	6.96	1.00	14.15	1 72E+04
X-1-04	Fe-54 (n,p) Mn-54	4.42	1.00	14.15	1.71E+04
X-1-05	Fe-54 (n,p) Mn-54	1.88	1.00	14.15	1.62E+04
X-1-06	Fe-54 (n,p) Mn-54	-0.66	1.00	14.15	1.55E+04
X-1-07	Fe-54 (n,p) Mn-54	-3.20	1.00	14.15	1.42E+04
X-1-08	Fe-54 (n,p) Mn-54	-5.74	1.00	14.15	1.26E+04
X-1-09	Fe-54 (n,p) Mn-54	-8.28	1.00	14.15	1.16E+04
X-1-10	Fe-54 (n,p) Mn-54	-10.82	1.00	14.15	9.63E+03
X-3-01	Fe-54 (n,p) Mn-54	11.53	1.00	-12.65	1.55E+04
X-3-02	Fe-54 (n,p) Mn-54	9.50	1.00	-12.65	1.61E+04
X-3-03	Fe-54 (n,p) Mn-54	6.96	1.00	-12.65	1.61E+04
X-3-04	Fe-54 (n,p) Mn-54	4.42	1.00	-12.65	1.57E+04
X-3-05	Fe-54 (n,p) Mn-54	1.88	1.00	-12.65	1.52E+04
X-3-06	Fe-54 (n,p) Mn-54	-0.66	1.00	-12.65	1.43E+04
X-3-07	Fe-54 (n,p) Mn-54	-3.20	1.00	-12.65	1.30E+04
X-3-08	Fe-54 (n,p) Mn-54	-5.74	1.00	-12.65	1.18E+04
X-3-09	Fe-54 (n,p) Mn-54	-8.28	1.00	-12.65	1.04E+04
X-3-10	Fe-54 (n,p) Mn-54	-10.32	1.00	-12.65	8.79E+03
FRDS21	Co-59 (n,g) Co-60	0.00	3.02	20.85	4.70E+03
FRDS21	Ag-109 (n,g) Ag-110m	0.00	3.02	20.85	9.31E+03
FRDS21	Np-237 (n,f) Zr-95	0.00	3.02	20.85	1.29E+05
FRDS21	Np-237 (n,f) Ru-106	0.00	3.02	20.85	2.25E+04
FRDS21	Np-237 (n,f) Cs-137	0.00	3.02	20.85	3.04E+03
FRDS21	Np-237 (n,f) Ce-144	0.00	3.02	20.85	4.87E+04
FRDS21	U-238 (n,f) Zr-95	0.00	3.02	20.85	1.67E+04
FRUS21	U-238 (n,f) Ru-106	0.00	3.02	20.85	4.28E+03
FRUSZ1	U-238 (n,f) CS-137	0.00	3.02	20.85	4.321+02
EPDS21	0-230 (n,1) Ce-144	0.00	3.02	20.85	8.56E+03
FRDS21	Fe 54 (n,p) Co-56	0.00	3.02	20.85	2.77E+05
FRDS21	Cu 63 (n,p) MI-54	0.00	3.02	20.85	8.01E+03
FRDS22	Co-59 (n,a) Co-60	0.00	3.02	20.00	1.230+02
FRDS22	Ag-109 (n.g) Ag-110m	-2.10	3.45	0.75	1.10E+04
FRDS22	Nn-237 (n f) 7r-95	-2.10	3.45	0.75	1.102+04
FRDS22	Np-237 (n f) Ru-106	-2.10	3.45	0.75	2.57E+04
FRDS22	Np-237 (n f) Cs-137	-2.10	3.45	0.75	3 45 5+03
FRDS22	Np-237 (n.f) Ce-144	-2 16	3.45	0.75	5.59E+04
FRDS22	U-238 (n f) Zr-95	-2 16	3.45	0.75	1 95E+04
FRDS22	U-238 (n.f) Ru-106	-2.16	3.45	0.75	5.05E+03
FRDS22	U-238 (n.f) Cs-137	-2.16	3.45	0.75	5.03E+02
FRDS22	U-238 (n.f) Ce-144	-2.16	3.45	0.75	1.01E+04
FRDS22	Ni-58 (n.p) Co-58	-2.16	3.45	0.75	3.12E+05

Table A.1 (continued)

CANDANIANA KANGKANANA ANALA NA PATRA S		C	oordinates	S	Activity*
Dosimeter	Reaction	X (cm)	Y [†] (cm)	Z (cm)	at EOI** (Bq/mg)
EPDS22	Fe-54 (n.p) Mn-54	-2.16	3.45	0.75	9.86E+03
FRDS22	Cu-63 (n,a) Co-60	-2.16	3.45	0.75	1.39E+02
EDDS24	Co-59 (n g) Co-60	-2.16	1.38	0.75	7.97E+03
EPDS24	Ag-109 (n.g) Ag-110m	-2.16	1.38	0.75	1.66E+04
FRDS24	Nin-237 (n f) 7r-95	-2.16	1.38	0.75	2.06E+05
FRUS24	No-237 (n f) Ru-106	-2.16	1.38	0.75	3.65E+04
FRUS24	No.237 (n.f) Cs-137	-2.16	1.38	0.75	4.82E+03
FRUS24	No.237 (n.f) Ce-144	-2.16	1.38	0.75	7.91E+04
FRUS24	11,238 (n f) 7r-95	-2 16	1.38	0.75	3.02E+04
FRU524	11.238 (n f) Bu-106	-2 16	1.38	0.75	7.43E+03
FRD524	11 238 (n f) Ce-137	-2 16	1.38	0.75	7.31E+02
FRDS24	U-238 (11,1) 05-157	-2 16	1.38	0.75	1.47E+04
FRDS24	Ni 58 (n n) Co 58	-2 16	1.38	0.75	4.68E+05
FRDS24	Fa Ed (n,p) Ma Ed	-2.16	1 38	0.75	1.54E+04
FRDS24	Cu 62 (n,p) Mn-54	-2.16	1 38	0.75	2.28E+02
FRDS24	Cu-03 (n,a) CO-00	-2.10	1.00	0.10	Contraction in the local data

Table A.1 (continued)

*For the Co and Ag monitors, diluted Al alloys were used. Co/Al was 0.1 wt % Co, and Ag/Al was 0.173 wt % Ag. Activities listed are per milligram of alloy. The fission product activities for the ²³⁷NP and ²³⁸U monitors are given per milligram of ²³⁷Np and ²³⁸U, respectively. Activities of all other monitors are given per milligram of chemically pure target material.

The 1T C(T) and 0.5T C(T) specimens had chevron notches. Because of the chevron, the thickness of the steel that shields the gradient wire inserted in the notch is changing along the notch. To take this into account in the neutronics analysis, the listed Y coordinates of the gradient wires in the C(T) specimens were replaced with "effective" coordinates as follows: 5.99 cm was changed to 5.67 cm, 4.41 cm was changed to 3.89 cm, and 2.18 cm was changed to 2.14 cm. The effective Y coordinates give the average thickness of the steel between the gradient wires and the front of the capsule.

**End of irradiation (EOI) for the HSSI 10.05 capsule is 03/05/93 at 23:54.

	Beginning		En	End		
Cycle	Date	Time	Date	Time	full power*	
340B	04/15/92	14:34	04/15/92	18:04	1	
341A	05/05/92	09:02	05/05/92	16:28	1	
	05/06/92	09:40	05/06/92	14.10	1	
	05/06/92	14:55	05/06/92	16.58	1	
	05/07/92	08:53	05/07/92	23:45	-	
341E	05/12/92	15:29	05/12/92	17:04	-	
	05/13/92	10:38	05/21/02	22:45	1	
342A	05/27/92	00.00	06/02/02	23.40	1	
	06/02/92	13.51	06/02/92	00.15	1	
342B	06/09/92	17:30	00/04/92	23:43	1	
0420	06/10/02	14:45	06/09/92	18:35	1	
3438	07/08/02	14.40	06/14/92	12:18	1	
3446	07/00/92	17:06	07/17/92	23:45	1	
Detet	07/22/92	18:26	07/23/92	10:45	1	
	07/23/92	12:43	07/30/92	10:53	1	
	07/30/92	16:49	07/31/92	12:31	1	
	07/31/92	15:38	07/31/92	23:45	1	
344B	08/06/92	07:49	08/12/92	14:32	1	
	08/12/92	15:42	08/14/92	23:47	1	
345A	08/20/92	13:02	08/28/92	23:45	1	
345B	09/02/92	09:31	09/04/92	23:45	1	
	09/08/92	15:00	09/10/92	15:18	1	
	09/10/92	15:24	09/11/92	23:45	1	
346A	09/16/92	14:06	09/16/92	15.12	1	
	09/16/92	15:29	09/25/92	23:45	-	
346B	09/30/92	09.49	00/20/02	21:06		
	10/01/92	13:00	10/04/02	10.52		
	10/04/92	11.16	10/04/02	11.30	1	
RDT788	10/04/92	11:45	10/04/92	11.30	1	
withdrawn	10/04/02	11.40	10/00/92	22:51	1	
3474	10/10/02	44.40	40/40/00			
54114	10/19/92	14.13	10/19/92	14:23	1	
	10/19/92	14:41	10/22/92	09:40	1	
	10/22/92	10.20	10/22/92	13:38	1	
2470	10/22/92	14:05	10/23/92	10:00	1	
34/8	10/28/92	09:22	10/29/92	13:36	1	
	10/29/92	14:32	10/30/92	15:08	1	
	10/30/92	15:39	11/01/92	12:33	1	
	11/01/92	13:03	11/04/92	10:27	1	
	11/04/92	10:38	11/05/92	08:15	1	
348A	11/11/92	18:13	11/12/92	10:45	1	
	11/12/92	11:39	11/16/92	10:10	1	
	11/16/92	10:25	11/17/92	14:15	1	
	11/18/92	09:35	11/20/92	23:45	1	
348B	11/25/92	13:37	11/25/92	23:45	1	
	11/30/92	08:15	12/02/02	10:10	1	
	12/02/92	10:27	12/04/02	12:45	1	
349A	12/11/02	12:44	12/12/02	13.15	1	
	12/12/02	11:20	12/12/92	00.13	1	
	12/12/02	10:45	12/13/92	19:07	1	
	12/15/92	19.45	12/16/92	08:01	1	
3400	12/10/92	17:07	12/18/92	10:20	1	
3490	01/05/93	09:14	01/08/93	23:45	1	

1

Table A.2. Irradiation history for the HSSI 10.05 capsule

NUREG/CR-6600

.

4

	Beginning		End	Fraction of	
Cucle	Date	Time	Date	Time	full power*
2504	01/14/93	10:45	01/14/93	16:06	1
350A	01/14/93	16:09	01/15/93	08:52	1
	01/15/03	09:50	01/22/93	23:45	1
2500	01/27/93	10:06	02/05/93	08:45	1
3500	02/10/93	13:03	02/18/93	09:44	1
351A	02/18/93	09:59	02/18/93	11:59	1
	02/18/93	14:35	02/19/93	08:28	1
	02/10/03	09:20	02/19/93	12:34	1
254D	02/25/03	04.28	02/26/93	09:01	1
3516	02/20/93	10:18	02/27/93	10:50	1
	02/27/03	10:55	03/01/93	16:53	1
	02/21/93	17.14	03/04/93	11:37	1
	03/04/93	11:45	03/05/93	23:45	1

Table A.2 (continued)

*Core full power is 2 MW.

٠

		Coordinat	es	Spec	ific activity at I	EOI [†]
Reaction	X (cm)	Y (cm)	Z* (cm);	RDT 7 (Bq/mg)	RDT 8 (Bg/mg)	RDT 9 (Ba/ma)
Fe-54 (n,p) Mn-54	-17.14	-0.96	24.13	3 09E+3	a state of the second se	
Fe-54 (n,p) Mn-54	-17.14	-0.96	13.97	4.55E+3		
Fe-54 (n,p) Mn-54	-17.14	-0.96	2.81	5.12E+3		
Fe-54 (I.,p) Mn-54	-17.14	-0.96	-3.81	5 11E+3		
Fe-54 (n,p) Mn-54	-17.14	-0.96	-13.97	4 28E+3		
Fe-54 (n,p) Mn-54	-17.14	-0.96	-24.13	2.71E+3		
Co-59 (n,g) Co-60	-17.14	-0.96	24.13	1.69E+4		
Co-59 (n,g) Co-60	-17.14	-0.96	13.97	2.93E+4		
Co-59 (n,g) Co-60	-17.14	-0.96	3.81	3.26E+4		
Co-59 (n,g) Co-60	-17.14	-0.96	-3.81	3.23E+4		
Co-59 (n,g) Co-60	-17.14	-0.96	-13.97	2.75E+4		
Co-59 (n,g) Co-60	-17.14	-0.96	-24.13	1.81E+4		
Fe-54 (n,p) Mn-54	17.14	-0.96	24.13		7 10E+3	7 865+3
Fe-54 (n,p) Mn-54	17.14	-0.96	13.97		1.055+4	1045+3
Fe-54 (n,p) Mn-54	17.14	-0.96	3.81		1 20E+4	1 125+4
Fe-54 (n,p) Mn-54	17.14	-0.96	-3.81		1 185+4	1.136+4
Fe-54 (n.p) Mn-54	17.14	-0.96	-13.97		0.025+3	9 04E+3
Fe-54 (n,p) Mn-54	17.14	-0.96	-24.13		6.28E+3	4.97E+3
Co-59 (n,g) Co-60	17.14	-0.96	24.13		2 465+4	2 555+4
Co-59 (n,g) Co-60	17.14	-0.96	13.97		A 42E+4	2.00E+4
Co-59 (n,g) Co-60	17.14	-0.96	3.81		5 105+4	4.290+4
Co-59 (n,g, Co-60	17.14	-0.96	-3.81		5 11E+4	4.745+4
Co-59 (n,g) Co-60	17.14	-0.96	-13.97		4 26E+4	3615+4
Co-59 (n,g) Co-60	17.14	-0.96	-24.13		2 65E+4	2 12 5+4
and any second transfers and Webcompany second states a super-	Colorester C., a service of a particular backware	CONTRACTOR DATA OF LOSS OF CONTRACTOR OF CONTRACTOR OF	second department of the	And the local process of the second statement with the second second second second second second second second	E.OUL TH	6.12014

Table A.3. Activities of the removable dosimeter tube (RDT) dosimeters

*The uncertainty in the axial position of the RDT is ± 2.54 cm (1 in.).

7

2

13

[†]The 3nd of irradiation (EOI) for RDTs 7 and 8 is 10/8/92 at 22:51; for RDT 9 the end of irradiation is 03/05/93 at 23:54.

BIBLIOGRAPHIC DATA SHEET (See Instructions on the reverse) 2. TITLE AND SUBTITLE	MISSION 1. REPORT NUMBER		
2. TITLE AND SUBTITLE	(Asaigned by NRC, Add Vol., Supp., Re and Addendum Numbers, if any.)		
	NUREG/CR-6600		
Neutron Exposure Parameters for Capsule 10.05 in the Heavy-Section	CRNL/TM-13548		
Steel mediation Program Lenth Irradiation Series	3. DATE REPORT PUBLISHED		
	MONTH YEAR		
	October 1998		
	A. FIN OR GRANT NUMBER		
AUTHOR(S)	6. TYPE OF REPORT		
I. Remec, C.A. Baldwin, F.B.K. Kam			
	Technical		
	7. PERIOD COVERED (Inclusive Detes)		
PERFORMING ORGANIZATION - NAME AND ADDRESS (IN NRC. provide Division Office or Particle 11.5. Martine 12			
provide name and mailing address.)	tory Commission, and mailing address; if contractor,		
Oak Ridge National Laboratory			
Oak Ridge, TN 37831-8285			
SPOMSORING ORGANIZATION - NAME AND ADDRESS (If MRC, type "Same as above", if contractor, provide MEC Division	Den of Design (1.0 Martin Design)		
Division of Frankrasia Testing and the second	n, once or region. U.S. Nuclear Risgulatory Commission		
Christon of Engineering Technology			
Omce of Nuclear Regulatory Research			
Weshington, DC 20555 cood			
SUPPLEMENTARY NOTES			
FM Hankatt NBC Droitet Manager	ne a series de la faire de la de la deserre de la faire de la f		
ABSTRACT (200 million and a local			
This report describes the computational methodology for the least-square data from the HSSI 10.05 capsule with neutronics calculations. It present metallurgical specimens irradiated in the capsule. The exposure parameter fluence greater than 1.0 MeV, fluence greater than 0.1 MeV, and displace parameter distributions are also described in terms of three-dimensional f functions are used, it is recommended that an uncertainty of 6% (10) be a parameters.	es adjustment of dosimetry c exposure parameters for the ers reported are the neutron ements per atom. Exposure fitting functions. When fitting associated with the exposure		
EY WORDS/DESCRIPTORS (List words or phrases that will assist researchers in locating the report.)	13. AVAILABILITY STATEMENT		
CEY WORDS/DESCRIPTORS (List words or phreases that will assist researchers in locating the report.) tosimetry reutronics calculations	13. AVAILABILITY STATEMENT Unlimited		
EY WORDS/DESCRIPTORS (List words or phrases that will assist researchers in locating the report.) dosimetry neutronics calculations east-squares fitting	13. AVAILABILITY STATEMENT UNIImited 14. SECURITY CLASSIFICATION		
CEY WORDS/DESCRIPTORS (List words or phrases that will easist researchers in locating the report.) dosimetry neutronics calculations east-squares fitting tradiation	13. AVAILABILITY STATEMENT UNSimited 14. SECURITY CLASSIFICATION (This Pege)		
TEY WORDS/DESCRIPTORS (List words or phrases that will essist researchers in locating the report.) losimetry seutronics calculations seast-squares fitting radiation xposure parameter distributions	13. AVAILABILITY STATEMENT UNlimited 14. SECURITY CLASSIFICATION (This Pege) Unclassified		
EY WORDS/DESCRIPTORS (List words or phrases that will essist researchers in locating the report.) losimetry eutronics calculations east-squares fitting radiation xposure parameter distributions	13. AVAILABILITY STATEMENT UNlimited 14. SECURITY CLASSIFICATION (This Page) Unclassified (This Report) Unclassified		
REY WORDS/DESCRIPTORS (List words or phrases that will essist researchers in locating the report.) dosimetry neutronics calculations east-squares fitting tradiation exposure parameter distributions	13. AVAILABILITY STATEMENT Unlimited 14. SECURITY CLASSIFICATION (This Page) Unclassified (This Report) Unclassified 15. NUMBER OF PAGES		
CEY WORDS/DESCRIPTORS (List words or phreases that will assist researchers in locating the report.) dosimetry neutronics calculations east-squares fitting madiation exposure parameter distributions	13. AVAILABILITY STATEMENT Unlimited 14. SECURITY CLASSIFICATION (This Pege) Unclassified (This Report) Unclassified 15. NUMBER OF PAGES		



Federal Recycling Program

NEUTRON EXPOSURE PARAMETERS FOR CAPSULE 10.05 IN THE HEAVY-SECTION STEEL IRRADIATION PROGRAM TENTH IRRADIATION SERIES

UCTUBER 1998

1

UNITED STATES NUCLEAR REGULATORY COMMISSION WASHINGTON, DC 20555-0001

.

OFFICIAL BUSINESS PENALTY FOR PRIVATE USE, \$300 120555154486 1 1AN1R5 US NRC-OCIO DIV-INFORMATION MANAGEMENT TPS-PDR-NUREG 2WFN-6E7 WASHINGTON DC 20555 FIRST CLASS MAIL POSTAGE AND FEES PAID USNRC PERMIT NO. G-67