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# CHARM: A Model for Aerosol Behavior in Time Varying Thermal-Hydraulic Conditions

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Prepared by C.J. Wheatley

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Prepared for  
U.S. Nuclear Regulatory  
Commission

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## ABSTRACT

CHARM is a computer model for the behavior of a one component aerosol in a single region with time-varying external conditions. It treats particle agglomeration due to Brownian motion, gravity and turbulence, and particle deposition due to Brownian motion, gravity, turbulence, thermophoresis and diffusiophoresis. Turbulence properties are estimated for flow through a region of arbitrary cross-sectional shape, with aerodynamically rough or smooth walls at any Reynolds number. The gas can be of any composition. The time-varying external conditions allowed for are the temperature, pressure and velocity of the gas, wall temperatures, and the rate, mass median radius and geometric standard deviation of the source. The model is simply modified to enable this list to be extended if needed. A new method of solving the governing equations, based on the finite element collocation method, enables the time-varying conditions to be treated accurately and economically. We describe in detail the models, the numerical methods, the execution of the computer code (including how to write the input data file and interpret results), and how to make simple modifications to the model. We discuss how the model could be implemented as a submodel of a larger one and what further work needs to be done to enable it to efficiently treat multicomponent aerosols, and condensation onto and evaporation from particles.

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## 1 INTRODUCTION

The work which has culminated in the production of the aerosol model CHARM described in this manual originates from the need to consider hypothetical accidents in power generating nuclear reactors for the purposes of assessing safety standards. Some of these hypothetical accidents are classified as severe, in which the reactor core, as a consequence of overheating, becomes severely degraded and fission products are released into the primary circuit and possibly into the containment building and the environment. It is essential to these assessments to calculate the transport of fission products from the fuel to their eventual destination. Many of them can be transported as aerosols for which agglomeration and deposition are important mechanisms to be considered. The behavior of the aerosol is coupled to the thermal-hydraulic conditions which can vary considerably both spatially and temporally; variations in temperature, pressure and turbulence are particularly important. Condensation onto and vaporization of the aerosol and self-heating due to radioactive decay of the fission products can also occur. Many computational cells and many aerosol components must be considered.

This poses a significant computational problem. The model we describe solves one aspect of this: how to efficiently compute aerosol agglomeration and deposition taking account of the time varying thermal-hydraulic conditions. Numerical methods for treating this were formulated and assessed by the author (Wheatley, 1988) who showed that one in particular, based on the finite-element collocation method, can give satisfactorily accurate results for practical problems and yet requires only modest computational overhead to update the agglomeration kernel to take account of time-dependencies in the external conditions.

CHARM is a modest extension of the computer code used by the author to assess the collocation method. It models aerosol behavior in a single computational cell; time-varying external conditions are assumed to have been calculated in advance and are supplied as data to the model. The aerosol particles have a single, constant composition and can agglomerate, deposit on surfaces and leak from the cell. A time-varying source of particles can also exist within the cell. The agglomeration and deposition models in MAEROS (Gelbard, 1982) have been used in CHARM. However, models have been added to treat deposition by turbulence and to estimate boundary layer thicknesses and turbulence properties of the flow field. These extensions in conjunction with improvements to the input and output subroutines will enable the model to be widely used for practical problems.

Of course, this only goes part-way to modeling aerosol behavior in the wider context as discussed above. Principally, multicomponent and vaporization effects are ignored. However, it was considered worth-while to develop such a model based on the previous work of the author for the following reasons:

- i We know of no other model which is able to efficiently treat aerosol behavior in time-varying external conditions. As an example, it can be applied to aerosols moving through a pipe with temperature variations along its length. Perhaps more important, it can be used to study whether variations of the external variables with time are important to aerosol behavior.
- ii It can be used to study alternatives to the physical models: turbulent deposition in particular for which there is some uncertainty.
- iii With minor modification, it can be incorporated into multi-cell models such as VICTORIA (Crimley et al., 1988) thereby enabling aerosol behavior to be fully coupled to the thermal-hydraulics and other phenomena - though, of course, simplifying assumptions have to be made about how to treat the particle composition, and condensation and evaporation.
- iv With further development of methods, it could form the basis of a model which efficiently treats multicomponent and vaporization effects also.

We envisage, therefore, that CHARM could be used as it is or with minor modification, incorporated as part of another model, or extended in some major way to treat multicomponent and vaporization effects. To meet all these possible needs, we will describe in detail the models in CHARM, the numerical methods we use, how to compose the input data file and interpret the output, and how to execute and make minor modifications to the code. We include supplementary details about the overall operation of the model, what the subroutines do and a compiler source listing. We also discuss in general terms how it could be incorporated into multi-cell models, the developments needed to treat efficiently multicomponent and vaporization effects, and how it might form the basis of a model to treat these effects.



## 2 DESCRIPTION OF THE MODEL

### 2.1 Overview

The governing equation of the aerosol phenomena treated by CHARM is the following

$$\frac{\partial C(m,t)}{\partial t} = \frac{1}{2} \int_0^m K(\mu, m-\mu, t) C(\mu, t) C(m-\mu, t) d\mu - C(m,t) \int_0^\infty K(\mu, m, t) C(\mu, t) d\mu - R(m,t) C(m,t) + S(m,t) \quad (1)$$

where  $C(m,t)$  is the aerosol number concentration distribution. It is defined so that  $C(m,t)dm$  is the number of particles per unit volume with mass in the range  $m$  to  $m + dm$  at time  $t$ . Drake (1972) gives an excellent survey of this equation.

$K$  is the agglomeration kernel; it is symmetric and takes account of particle-particle collisions due to Brownian motion, differential gravitational settling, and turbulence. The integrand of the first term with  $K$  corresponds to production of particles of mass  $m$  due to collision and coalescence of particles of masses  $m - \mu$  and  $\mu$ . The integrand of the succeeding term corresponds to destruction of particles of mass  $m$  due to collision and coalescence with particles of mass  $\mu$ .  $K$  can depend explicitly on time through changes in the external conditions; gas temperature, pressure and velocity are particularly important.

$R$  is the removal rate for particles of mass  $m$ . Leakage, and deposition onto surfaces induced by thermophoresis, diffusiophoresis, gravitational settling, Brownian diffusion, and turbulence all contribute to  $R$  which, like  $K$ , may be time-dependent.

$S$  is the number concentration source rate for particles of mass  $m$ .

Implicit in Eq. (1) are four assumptions which we briefly mention. First, the aerosol is well-mixed throughout the cell. This may require the flow in the cell to be turbulent to promote mixing or the cell to be a small part of a larger region within which the aerosol exists and the aerosol has nearly uniform properties within the cell by virtue of its small size. Second, particles are characterized by their mass only. i.e. particles can have a shape which is a function of  $m$  but particles of given mass all have the same shape. Clearly, this breaks down when particles having the same mass have different shapes. This affects agglomeration and deposition rates. Such dependence, however, would be extremely difficult to treat computationally. Third, boundary layers and their effect on deposition are not treated in detail. Fourth, particles do not break-up into smaller particles.

Detailed expressions for K, R and S will be considered in the succeeding subsections where the primary aim will be to give formulae in detail as they appear in CHARM and to reference their origin. We will indicate ranges of validity and possible uncertainties where appropriate. We recall that we have chosen to base the models in CHARM on those in MAEROS except where extensions have been made to estimate relevant flow parameters and turbulent deposition. A good survey of these and similar models is given in Dunbar et al. (1984). We use S.I. units throughout except for molecular weights, which have units kg / kmole, and in the table in Section 4.4 where we show the units explicitly.

## 2.2 Gas properties

Agglomeration and deposition rates depend on properties of the gas in the bulk of the cell and adjacent to surfaces, where they are relevant to the calculation of diffusiophoresis. Some of the formulae we give are specific to air. However, we note that they are isolated in a single subroutine in CHARM and so are easily changed to accommodate other gases. Standard gas kinetic formulae can be used to combine component properties to obtain estimates for mixtures.

The gas density For the bulk gas, the temperature, T, pressure, P, and average molecular weight,  $W_g$ , are supplied as input to the model (when a gas has more than one component the average molecular weight is just the mass of one mole of the mixture). The density,  $\rho_g$ , is calculated assuming the gas to be ideal as follows

$$\rho_g = \frac{PW_g}{10^3 RT} \quad (2)$$

The factor  $10^3$  is included because  $W_g$  has units kg / kmole.

The dynamic viscosity  $\eta_g$  is estimated from a correlation of data for air. The correlation is as follows

$$\eta_g = \eta_r \left[ \frac{T}{T_{r1}} \right]^{3/2} \frac{1}{1 + T/T_{r1}} \quad (3)$$

where  $\eta_r$  and  $T_{r1}$  are constants with values  $1.565 \times 10^{-6}$  and 114.0 respectively. It would be a simple matter to replace this with correlations for other gases or mixtures of gases.

The mean free path  $l$  is calculated from standard kinetic theory as follows

$$l = \eta_g \left[ \frac{2}{P\rho_g} \right]^{1/2} \quad (4)$$

The vapor diffusivity For the calculation of deposition by diffusiophoresis we need properties of the gas adjacent to surfaces where we suppose a vapor is present which is either condensing onto or evaporating from the nearby surface. The diffusivity of the vapor in the gas is estimated from a correlation of data for diffusion of water vapor in air as follows

$$D_v = D_v \frac{P_r}{\bar{P}} \left[ \frac{T}{T_{r2}} \right]^{1.04}, \quad (5)$$

where  $D_v$ ,  $P_r$  and  $T_{r2}$  are constants with values  $2.11 \times 10^{-6}$ ,  $1.01325 \times 10^6$  and 273.15 respectively. It would be straightforward to replace this with correlations for other vapors and other gas mixtures.

The vapor concentration The concentration of the vapor in the vapor/gas mixture adjacent to a surface,  $c_s$ , where the subscript s can stand for c, w or f according to whether the surface is the ceiling, wall or floor (see Sub-section 2.6 for the definition of these surfaces), is estimated from the ideal gas law as follows

$$c_s = \frac{f_s P W_v}{10^3 R T_s}, \quad (6)$$

where  $f_s$  is the molar fraction of the vapor in the mixture,  $W_v$  is the molecular weight of the vapor and  $T_s$  is the temperature of the mixture adjacent to the surface.

### 2.3 Flow properties

Turbulence parameters of the bulk flow are needed for estimating agglomeration and deposition rates. Viscous and diffusion boundary layer thicknesses are needed for estimating Brownian and thermophoresis deposition.

The friction velocity  $u_*$  is calculated from formulae based on those given in Schlichting (1979) for flow through a cylindrical pipe of any aerodynamic roughness and others for flow through aerodynamically smooth pipes of arbitrary cross-sectional shape. We will indicate in more detail below where extensions have been made. By definition,  $u_*$  in terms of the Fanning friction factor,  $f_*$ , is given by

$$u_* = U \left[ \frac{f_*}{2} \right]^{1/2}, \quad (7)$$

where  $U$  is the mean flow speed in the cell relative to surfaces in the cell, usually the cell walls.

The Fanning friction factor  $f_s$  is implicitly determined from a correlation established by Colbrook (1939) for flow through cylindrical pipes of any aerodynamic roughness. The correlation is

$$\frac{1}{2\sqrt{f_s}} = 1.74 - 2 \log_{10} \left[ \frac{2z_s}{d_b} + \frac{18.7}{\text{Re} \sqrt{f_s}} \right], \quad (8)$$

where  $z_s$  is the equivalent sand roughness of the pipe surface adjacent to the flow,  $d_b$  is the diameter of the pipe, and Re is the pipe Reynolds number equal to  $\rho_g d_b U / \eta_g$ .

This correlation reduces to the quadratic resistance formula for fully rough flow ( $\rho_g z_s u_s / \eta_g > 70$ ), derived by von Karman, and Prandtl's universal law of friction for smooth pipes ( $\rho_g z_s u_s / \eta_g < 5$ ). In either limit, the correlation has been verified up to Reynolds numbers which exceed  $10^6$  and there is theoretical justification for extrapolating the correlation to much larger Reynolds numbers.

The equivalent sand roughness  $z_s$  equals the height of protrusions on sand roughened pipes of equivalent roughness (this originates from the pioneering experiments of Nikuradse who measured the pressure drop along pipes roughened with sand of varying grades at Reynolds numbers ranging from somewhat less than  $10^3$  to greater than  $10^6$ ).  $z_s$  in general must be determined empirically but values have been established for common materials which we give in the table below, reproduced from Schlichting (1979).

$z_s$ for some common materials	
material	$z_s$ (m)
reinforced concrete	.0003 - .003
cast iron	.00026
galvanized steel	.00015
structural and forged steel	.000045
drawn pipes	.0000015

Note that certain types of protrusion, such as regularly spaced ribs perpendicular to the flow, can give rise to values of  $z_s$  significantly larger than the height of the protrusion.

The hydraulic diameter  $d_b$  is just the diameter of the pipe. However, experiments by a number of authors have shown that the Fanning friction factor of aerodynamically smooth pipes of non-circular cross-section (such as square, rectangular, triangular and annuli) equals that of circular pipes over a wide range of Reynolds number when  $d_b$  is generalized as given in Eq. (9) below,

despite the complications of secondary flows induced in non-circular pipes.  $d_h$  in general is given by

$$d_h = \frac{4A}{p} \quad (9)$$

where  $A$  is the cross-sectional area and  $p$  is the "wetted" perimeter of the pipe perpendicular to the flow. We use this generalization for aerodynamically rough pipes also, even though it has only been verified for smooth pipes.

The critical Reynolds number The above formulae for  $u_*$  are valid when the flow is turbulent and fully developed which, for a cylindrical pipe, is the case when  $Re \geq 2300$  and well downstream of the pipe inlet. For convenience, we calculate  $u_*$  from these formulae when  $Re \geq 2300$  irrespective of the cross-sectional shape of the pipe and the downstream distance from the inlet (and other axial changes). We note that the critical Reynolds number (based on  $d_h$  given by Eq. (9)) in general depends on the pipe shape.

We do not have a treatment for other turbulent flows, non-fully developed flows in particular, and simply assume that  $u_*$  is zero when  $Re < 2300$ .

The turbulent energy dissipation rate per unit mass  $\epsilon_*$  is estimated by equating the rate of energy consumption needed to promote steady flow along a pipe of given length to the rate of energy dissipation due to turbulence with the result

$$\epsilon_* = \frac{4Uu_*^3}{d_h} \quad (10)$$

For fully developed turbulent flow in pipes, Laufer (1954) shows that direct viscous energy dissipation is negligible compared to energy dissipation due to turbulence. Consequently, the above formula is valid and provides an estimate of the turbulent energy dissipation rate averaged of the pipe cross section. We note, however, that Laufer also showed the turbulent energy dissipation rate varies considerably with distance from the pipe centre, being least in the core region and greatest near the wall. An alternative weighting in the averaging process can therefore lead to a substantially different estimate of  $\epsilon_*$  but we retain Eq. (10) in the absence of any present indication that an alternative weighting should be used.

The viscous boundary layer thickness  $\delta_*$  is estimated from (Monin and Yaglom, 1971)

$$\delta_* = \frac{\eta_g}{\rho_g u_*} \quad (11)$$

An empirical constant of ~5 might have been included in the numerator on the right hand side of Eq. (11) (Monin and Yaglom, 1971) but we prefer to leave this out since other empirical constants in the equations in which  $\delta_*$  appears make this redundant.

The diffusion boundary thickness  $\delta_D$  is needed later for estimating deposition by Brownian diffusion from a turbulent flow. It is estimated from (Keller, 1973)

$$\delta_D = \delta_* / Sc^{1/3} , \quad (12)$$

where Sc is the particle Schmidt number given by

$$Sc = \frac{\eta_g}{kTB} . \quad (13)$$

k is the Boltzmann constant and B is the particle mobility defined in Sub-section 2.5.

#### 2.4 Initial and source distributions

For convenience we use analytic formulae for these although more general formulations could be accommodated. The initial and source number concentration distribution are chosen to be log-normal. Consequently, the initial density distribution,  $Y(m,t) = mC(m,t)$ , is given by

$$Y(m,t) = \frac{N}{(2\pi)^{1/2} \log_e(\sigma^2)} e^{-\{\log_e^2(m/m_g)/2\log_e^2(\sigma^2)\}} . \quad (14)$$

where the moments N,  $\sigma$  and  $m_g$  are defined in Sub-section 3.3. These moments, however, are not the most convenient to specify values for and so we choose instead  $\rho$ ,  $\sigma$  and  $r_{se}$  as the primary parameters.  $\rho$  and  $\sigma$  are defined in Sub-section 3.3 also.  $r_{se}$  is the radius of the spherically equivalent particle of mass  $m_{se}$  and density  $\rho_p$ .

N and  $m_g$  in terms of  $\rho$  and  $r_{se}$  are

$$m_{se} = \frac{4}{3} \pi \rho_p r_{se}^3 , \quad (15)$$

$$N = \frac{\rho}{m_{se}} e^{\log_e^2(\sigma^2)/2} , \quad (16)$$

and

$$m_g = m_{se} e^{-\log_e^2(\sigma^2)} . \quad (17)$$

Similar expressions apply for the source density distribution,  $mS(m,t)$ , except  $N$  and  $\rho$  are replaced by  $dN/dt$  and  $d\rho/dt$  where these are, respectively, the number concentration generation rate (the number generation rate divided by the cell volume) and the density generation rate (the mass generation rate divided by the cell volume) of the source. Note that we use the same symbols for other moments of both the airborne and source distributions.

## 2.5 Particle mobilities

The particle mobility,  $B$ , is estimated from Stoke's mobility law,  $B_{St}$ , with a slip correction due to Cunningham (1910),  $Cu$ , as follows

$$B = B_{St} Cu . \quad (18)$$

$B_{St}$  is given by

$$B_{St} = \frac{1}{6\pi\chi_d\eta_a r} , \quad (19)$$

where the dynamic shape factor,  $\chi_d$ , is an empirical dimensionless correction factor introduced to account for the aerodynamic effects associated with non-spherical particles, and  $r$  is the radius of the spherically equivalent particle of mass  $m$ .

$Cu$  is given by

$$Cu = 1 + k_a Kn + k_q Kn e^{-k_b/Kn} , \quad (20)$$

where  $Kn$  is the particle Knudsen number which equals  $1/r$  (i.e. the mean free path/the equivalent particle radius) and  $k_a$ ,  $k_q$  and  $k_b$  are empirical dimensionless constants. The default values we use for  $k_q$  and  $k_b$  (0.4 and 1.1 respectively) are from Davies (1945). Our default value for  $k_a$  is slightly larger than the value obtained by Davies (1.37 c.f. 1.257).

## 2.6 Deposition rates

Five deposition mechanisms are considered which we describe in turn. We describe how the contributions are combined at the end of this sub-section.

We shall use ceiling, wall, and floor to denote surfaces exposed to aerosol (within the cell and at the cell boundaries) which are horizontal and downward facing, vertical, and horizontal and upward facing respectively. Surfaces of given orientation are not distinguished in temperature.

The deposition velocity due to gravitational settling  $v_g$  is given by

$$v_G = g m B , \quad (21)$$

where  $g$  is the acceleration due to gravity. Strictly,  $(\rho_p - \rho_g)/\rho_p$  should appear as a multiplicative factor in this equation but, keeping to our constraint to duplicate the models in MAEROS, we ignore this small error.

The deposition velocity due to turbulence  $v_*$  is estimated from a correlation of the Liu and Agarwal (1974) data for deposition in smooth pipes. We first define the dimensionless deposition velocity,  $\tilde{v}_*$ , and the dimensionless relaxation time,  $\tilde{\tau}$ , by

$$v_* = \tilde{v}_* u_* \quad (22)$$

and

$$\tilde{\tau} = \tau \rho_g u_*^2 / \eta_g , \quad (23)$$

where  $\tau$  is the particle relaxation time given by

$$\tau = \frac{2\rho_p r^2 C_u}{9\eta_g \chi_d} = mB . \quad (24)$$

For  $\tilde{\tau}$  between  $\sim 1$  to  $\sim 10$  the Liu and Agarwal data are well correlated by

$$\tilde{v}_{*1} = 6 \times 10^{-4} \tilde{\tau}^2 \quad (25)$$

For  $\tilde{\tau}$  between  $\sim 30$  to  $\sim 1000$  their data are well correlated by

$$\tilde{v}_{*2} = .213 \tilde{\tau}^{-1/8} \quad (26)$$

By combining  $\tilde{v}_{*1}$  and  $\tilde{v}_{*2}$ , we find a good correlation across the whole range of  $\tilde{\tau}$  to be as follows

$$1/\tilde{v}_*^2 = 1/\tilde{v}_{*1}^2 + 1/\tilde{v}_{*2}^2 . \quad (27)$$

This correlation is applied in CHARM without restriction on  $\tilde{\tau}$ .

Liu and Agarwal concluded that the dominant deposition mechanism in their experiments was penetration of the laminar sub-layer by particle inertia generated from the turbulence. They showed that the contribution from Brownian diffusion across the laminar sub-layer was always negligible for the particle sizes examined. Therefore, we assume this latter mechanism is not accounted for in our estimate for  $v_*$ . It can be important for small particles and so we treat it next as a separate contribution.



The deposition velocity due to Brownian diffusion  $v_B$  takes account of Brownian diffusion across the laminar sub-layer from a turbulent flow. It is given by

$$v_B = .0594 kTB/\delta_D = .0594 u_* Sc^{-2/3}, \quad (28)$$

where  $kTB$  is the Stokes-Einstein particle diffusivity. The factor .059 is a departure from MAEROS; it is a dimensionless empirical correction factor from Brockmann et al. (1982).

We note that our treatment of turbulent deposition, including Brownian deposition from a turbulent flow, does not distinguish aerodynamically rough or smooth surfaces. In fact, the Liu and Agarwal experiments were done in aerodynamically smooth pipes. And, it is clear from the Brownian deposition formula that a laminar sub-layer is supposed to exist so this also is applicable to aerodynamically smooth surfaces. However, experiments by Wells and Chamberlain (1957) and Chamberlain (1967) show deposition is increased when surfaces are rough. We, therefore, need to consider generalizing our treatment.

Hahn et al. (1985) show the correlation of Kader and Yaglom (1977), which is applicable to deposition of submicron particles to rough surfaces, agrees with experiment over a wide range of particle Schmidt numbers. This appears to be a suitable candidate with which to generalize our equation for  $v_B$ . However, the situation for  $v_s$  appears to be less clear and requires further study.

The thermophoretic deposition velocity  $v_{Ts}$ , where  $s$  can stand for  $c$ ,  $w$  or  $f$ , is estimated from

$$v_{Ts} = \frac{T - T_s}{T} \frac{9\pi\eta_g^2 r B Br}{\rho_g \delta_s}, \quad (29)$$

where  $Br$  is a dimensionless factor obtained by Brock (1962) given by

$$Br = b_k \frac{1}{1 + 3b_m Kn} \frac{1}{2 + 1/(a_g/a_p + b_t Kn)}, \quad (30)$$

where  $b_k$ ,  $b_m$  and  $b_t$  are dimensionless constants (1.0, 1.37 and 1.0 respectively) and  $a_g$  and  $a_p$  are the thermal conductivities of the gas and particle material respectively.

Note the temperature gradient has been approximated as  $(T - T_s)/\delta_s$  where, following Dunbar et al. (1984) and in the absence of any specific model in MAEROS,  $\delta_s$  is chosen as an estimate of the distance over which the bulk gas temperature decreases to the surface temperature. It would clearly be better to use the thermal boundary layer thickness instead but the error introduced by using  $\delta_s$  is most likely small compared to other uncertainties.

This and similar formulae for  $v_{Ts}$  have been reviewed by Derjaguin and Yalamov (1972). From comparisons with experiment they conclude that the Brock correction factor leads to underestimates of  $v_{Ts}$  for particles with  $Kn \lesssim 1$  by a factor  $\approx 2$ . A different transport mechanism applies for particles with  $Kn \gg 1$ . Derjaguin and Yalamov obtain an estimate for  $v_{Ts}$  in this limit which they show to agree with experiment. The formula above overestimates  $v_{Ts}$  in this limit by a factor of order  $Kn$ .

The diffusiophoretic deposition velocity  $v_{Ds}$ , where  $s$  can stand for  $c$ ,  $w$  or  $f$ , is estimated from

$$v_{Ds} = D_v \frac{dc_s}{dx} \frac{1}{c_s} \frac{f_s}{f_s + (1 - f_s)\sqrt{W_g/W_v}} \quad (31)$$

where  $dc_s/dx$  is the outward facing vapor concentration gradient near the ceiling, wall or floor according to whether  $s$  equals  $c$ ,  $w$  or  $f$ . Comparison with Derjaguin and Yalamov (1972) shows this estimate to be applicable in the limit  $Kn \gtrsim 1$  and  $f_s \ll 1$  and when the flow of vapor to or from the surface is purely diffusive. Note that we could estimate  $dc_s/dx$  in a similar way to that used to estimate the temperature gradient in the formula for  $v_{Ts}$ .

The net deposition velocity to any surface  $v_s$  is estimated by combining the contributions in the following way

$$v_c = v_B + v_* + v_{Tc} + v_{Dc} - v_G \quad (32)$$

$$v_w = v_B + v_* + v_{Tw} + v_{Dw} \quad (33)$$

and

$$v_f = v_B + v_* + v_{Tf} + v_{Df} + v_G \quad (34)$$

Note that since either or both of  $v_{Ts}$  and  $v_{Ds}$  could be negative (i.e. when  $T_s$  is greater than  $T$  or  $dc_s/dx$  is negative) and  $v_G$  is subtracted in Eq. (32), some of the  $v_s$  may be negative. We therefore only apply the equations above when the result for  $v_s$  is positive and otherwise set  $v_s$  to zero.

The deposition rate to a surface per unit cell volume,  $\lambda_s$ , is given by

$$\lambda_s = v_s A_s / V \quad (35)$$

where  $A_s$  is the area of surface  $s$  exposed to aerosol.  $R(m,t)$  is then given by

$$R(m,t) = \lambda_c + \lambda_w + \lambda_f + \lambda_l \quad (36)$$

where  $\lambda_1$  is the cell leakage rate, defined as the number of volume changes in the cell per second.

We have not included all possible deposition mechanisms in our treatment above. Examples left out are: Brownian diffusion in a laminar flow; deposition mechanisms associated with electrostatic charges; and inertial deposition due to non-linear mean streamlines (streamlines may be non-linear due to bends in the flow path or secondary flows induced by turbulence, which can occur in straight flow paths). This last mechanism can be important and would be an obvious next candidate for which to find a suitable treatment.

## 2.7 Agglomeration rates

Four agglomeration mechanisms are considered which are described in turn. We start by giving the formula for a commonly occurring factor and we describe at the end of this sub-section how the contributions for each mechanism are combined. For notational convenience the agglomeration rate formulae are given corresponding to the  $j^{\text{th}}$  and  $k^{\text{th}}$  collocation points (see Sub-section 3.1 for their definition).

The particle terminal velocity  $u_G$  is the terminal velocity due to gravity of a particle of mass  $m$  and is estimated as

$$u_G = gmB . \quad (37)$$

Notice this is just  $v_G$  but we prefer to use a different symbol here to avoid confusion. As for  $v_G$ , a factor  $(\rho_p - \rho_g)/\rho_p$  should be included but we ignore this small error to keep the equation identical to that used in MAERUS.

The Brownian agglomeration rate  $\phi_B$  is estimated as

$$\phi_B(m_j, m_k) = 4\pi kT (B_j + B_k) \chi_c(r_j + r_k) Fu(m_j, m_k) , \quad (38)$$

where  $B_j$  and  $B_k$  are the particle mobilities at the  $j^{\text{th}}$  and  $k^{\text{th}}$  collocation points respectively,  $\chi_c$  is the collision shape factor which corrects the collision cross-section of particles when they depart from sphericity and  $Fu$  is a factor originally introduced by Fuchs (1964) to correct for particles small in size compared to the molecular mean free path.  $Fu$  is given by

$$1/Fu(m_j, m_k) = 1/Fu_1(m_j, m_k) + 1/Fu_2(m_j, m_k) , \quad (39)$$

where  $Fu_1$  is

$$Fu_1(m_j, m_k) = \chi_* \frac{r_j + r_k}{kT(B_j + B_k)} \left[ \frac{8kT}{\pi} \left( \frac{1}{m_j} + \frac{1}{m_k} \right) \right]^{1/2} . \quad (40)$$

$Fu_2$  is modified from unity according to Sitarski and Seinfeld (1977)

$$Fu_2(m_j, m_k) = 1 + \frac{2\sqrt{(\bar{a}_j^2 + \bar{a}_k^2)}}{r_j + r_k}, \quad (41)$$

where  $\bar{a}$  is

$$\bar{a} = \frac{(r+a)^3 - (r^2+a^2)^{3/2}}{3ra} - r \quad (42)$$

and

$$a = B \left[ \frac{2kTm}{\pi} \right]^{1/2} \quad (43)$$

$\chi_s$  in Eq. 40 is the particle-particle sticking efficiency which is the probability that particles stick to one another when they collide. Note that it is included as a multiplicative factor in Eq. (41) only, as is done in the MAEROS model. It is not clear why it is not included in Eq. (42) also.

The gravitational agglomeration rate  $\phi_G$  is estimated as

$$\phi_G(m_j, m_k) = \pi \chi_s \chi_{Fu} \chi_c^2 (r_j + r_k)^2 |u_G(m_j) - u_G(m_k)| \quad (44)$$

It arises from collisions of particles travelling under the influence of gravity at different terminal velocities.

The collision efficiency This is a correction factor which is applied to account for the deflection of the particle stream lines from straight-lines when they approach one another. We use the correction factor derived by Fuchs (1964),  $\chi_{Fu}$ , given by

$$\chi_{Fu}(m_j, m_k) = \frac{3}{2} \frac{\min(r_j, r_k)^2}{(r_j + r_k)^2}, \quad (45)$$

where *min* stands for the minimum value of  $r_j$  and  $r_k$ .  $r_j$  and  $r_k$  are just the radii of the equivalent spherical particles evaluated at the  $j^{\text{th}}$  and  $k^{\text{th}}$  collocation point respectively.

We note that the formula above is the same as that derived by Pruppacher and Klett (1978) except the factor 3/2 is replaced by 1/2. Dunbar et al. (1984) have reviewed these formulae and conclude that the Pruppacher and Klett formula, though still based on a number of approximations, has firmer foundation.

The turbulent shear agglomeration rate  $\phi_{.S}$  is estimated from (Saffman and Turner, 1956)

$$\phi_{.S}(m_j, m_k) = \chi_s \chi_c^3 (r_j + r_k)^3 \left[ \frac{8\rho_g \pi \epsilon_*}{15\eta_g} \right]^{1/2} \quad (46)$$

It accounts for the action of turbulent shear causing particles which follow the instantaneous stream lines to collide with one another.

The turbulent inertia agglomeration rate  $\phi_{.I}$  is estimated from (Saffman and Turner, 1956)

$$\phi_{.I}(m_j, m_k) = \chi_s \chi_c^2 (r_j + r_k)^2 \left[ \frac{512\rho_g \pi^3 \epsilon_*^3}{15\eta_g} \right]^{1/4} |u_G(m_j) - u_G(m_k)|/g \quad (47)$$

It accounts for particles colliding with one another when, due to their inertia, they are unable to follow the instantaneous stream lines.

In principle, a collision efficiency factor should be included in  $\phi_{.S}$  and  $\phi_{.I}$ , analogously to that included in  $\phi_G$ . Dunbar et al. (1984) assume this factor is the same as that which appears in  $\phi_G$  (here estimated as  $\chi_{Fu}$ ). However, it is by no means clear that the same factor applies since the flow field near to particles approaching one another due to gravity is not the same as that when particles approach one another due to turbulence. We leave this factor out, as in MAEROS.

The combined agglomeration rate The contributions defined above are combined as follows

$$K(m_j, m_k, t) = \phi_B(m_j, m_k) + \phi_G(m_j, m_k) + \{\phi_{.S}(m_j, m_k)^2 + \phi_{.I}(m_j, m_k)^2\}^{1/2} \quad (48)$$

According to Saffman and Turner, the turbulence contributions are added quadratically. However, Dunbar et al. (1984) point out that the reasoning used by Saffman and Turner also applies to the gravitational contribution which should therefore be added to  $K(m_j, m_k, t)$  in the same way. We do not do this to maintain consistency with MAEROS.

We conclude by noting that we have not included all possible agglomeration mechanisms. Examples left-out are agglomeration in laminar shear flows and body force effects (e.g. van der Waals and electrostatic forces). See Drake (1972) for a review.

### 3 THE NUMERICAL METHOD

#### 3.1 Discretization of the governing equations

We discretize Eq. (1) with respect to mass using the collocation finite-element method. In this method the governing equation is required to hold at a set of collocation points only ( $n$  in total). A finite-element expansion based on values of variables at the collocation points is used. Here, this will be needed for the estimation of the agglomeration integrals.

The particular method we use is identical to that studied by the author (Wheatley, 1988) who showed that accurate solutions to the equation could be obtained with a small number of collocation points and the agglomeration kernel evaluated on the  $n^2$  pairs of collocation points only. Consequently, the agglomeration kernel, which is in general time-dependent, can be economically recalculated as the integration of the equation advances in time.

We discretize  $m$  on a logarithmic scale as follows

$$\log_e(m_i) = \log_e(m_1) + (i-1)h, \quad i=1, \dots, n. \quad (49)$$

$h$  is a constant which can be found from  $m_1$ ,  $m_n$ , the smallest and largest values of discretize mass respectively, and  $n$ . We choose  $h$  to be constant (i.e. independent of  $i$ ) for reasons explained in Wheatley (1988).

With this choice for  $m_i$  it is convenient to choose the mass distribution, given by  $Y(m,t) = mC(m,t)$ , as the dependent variable in Eq. (1), which becomes

$$\begin{aligned} \frac{\partial Y(m,t)}{\partial t} = & \int_0^m K(\mu, m-\mu, t) Y(\mu, t) Y(m-\mu, t) d\log_e(\mu) \\ & - Y(m,t) \int_0^\infty K(\mu, m, t) Y(\mu, t) d\log_e(\mu) - R(m,t) Y(m,t) + mS(m,t), \quad (50) \end{aligned}$$

where we have used  $K(\mu, \nu, t) = K(\nu, \mu, t)$  and, for economy of display here and later, the integration limits are shown for  $\mu$  rather than  $\log_e(\mu)$ .

When this equation is evaluated at the points  $m_i$ ,  $i = 1, \dots, n$ , we can see that although the extended trapezoidal rule could be used to estimate the second integral on the right hand side the first integral will be troublesome. This is where a finite-element expansion is needed. We choose to expand the integrands as follows

$$K(\mu, \nu, t) Y(\mu, t) Y(\nu, t) \approx \sum_{j,k} K_{jk} Y_j Y_k g_j(\log_e(\mu)) g_k(\log_e(\nu)), \quad (51)$$

where  $Y_i$  and  $K_{ij}$  are shorthand for  $Y(m_i, t)$  and  $K(m_i, m_j, t)$  respectively and the  $i^{\text{th}}$  element  $g_i$  is defined in terms of a basic element  $g$  ( $g$  is also used to denote the acceleration due to gravity but no confusion should arise) by

$$g_i(x) = g((x-x_i)/h) \quad (52)$$

and  $x_i$  is  $\log_e(m_i)$ . The precise form of  $g$  will be discussed later but we note here that we always choose it so that  $g(0) = 1$  and  $g(\pm 1), g(\pm 2), g(\pm 3), \dots = 0$ . This guarantees that the expansion in Eq. (51) is consistent in the sense that the equation is satisfied identically when  $\mu$  and  $\nu$  are located at any of the collocation points.

We have chosen the particular expansion in Eq. (51) for three reasons. First, it entails the agglomeration kernel to be evaluated only at the collocation points. Second, since  $K$  and  $Y$  have not been expanded separately, the summations which result in the discretized equation are at most over two indices which cuts down on computational labor. And third, as we shall see, we obtain the same result for the second integral in Eq. (50) as that obtained by applying the trapezoidal rule. (It was shown in Wheatley (1988) that the trapezoidal rule is particularly accurate for integrals of this type.)

We now use Eq. (51) in Eq. (50) which we evaluate at the  $i^{\text{th}}$  collocation point to obtain the following closed set of equations, being the discretized form of the aerosol equation

$$\frac{\partial Y_i}{\partial t} = \sum_{j,k} P_{jk}^i K_{jk} Y_j Y_k - Y_i \sum_j D_j^i K_{ij} Y_j - R_i Y_i + m_i S_i, \quad (53)$$

where  $R_i$  and  $S_i$  are shorthand for  $R(m_i, t)$  and  $S(m_i, t)$  respectively and we have used  $g_j(x_k) = \delta_{jk}$ , where  $\delta_{jk}$  is the Kronecker delta. The terms with  $P_{jk}^i$  and  $D_j^i$  correspond to the particle production and destruction terms respectively on the right hand side of Eq. (50). The indices in  $P_{jk}^i$  and  $D_j^i$  run from 1 to  $n$ .

$D_j^i$  is

$$D_j^i = \int_0^\infty g_j(\log_e(\mu)) d\log_e(\mu) = h \int_{-\infty}^\infty g(x) dx = h, \quad (54)$$

as desired, where we require  $g(x)$  to be chosen so that  $\int_{-\infty}^\infty g(x) dx = 1$ . (The superscript in  $D_j^i$  is clearly redundant but we retain it to maintain notational consistency with Wheatley, 1988.)

$P_{jk}^i$  is

$$P_{jk}^i = n_{jk} \int_0^{m_i} g_j(\log_e(\mu)) g_k(\log_e(m_i - \mu)) d\log_e(\mu). \quad (55)$$

This is simplified somewhat by making the transformation  $y = \log_e(\mu/m_j)/h$  to obtain

$$P_{jk}^i = h n_{jk} \int_{-\infty}^j g(y) g\left(\frac{1}{h} \log_e(1 - e^{(y-j)/h}) + k\right) dy, \quad (56)$$

where  $j = i - j$  and  $k = i - k$ . The integral must be calculated numerically and the integration range must be divided-up into sub-ranges since  $g$  is generally non-smooth - see under CHARMCOE in Appendix B for details. The indices in the coefficient  $P_{jk}^i$  in principle take all values from 1, ...n, however, only a small fraction of the coefficients are non-zero. It is straightforward to find the conditions on  $i$ ,  $j$  and  $k$  for this to be so. It can be shown that they depend only on  $j$  and  $k$ . The non-zero values of the coefficients are conveniently stored consecutively using an indexing based on the derived conditions.

The multiplicative factor  $n_{jk}$  is introduced as a correction to conserve mass as we now discuss.

By integrating Eq. (50) with respect to  $m$  from 0 to  $\infty$  the following mass balance equation is obtained

$$\frac{\partial \rho}{\partial t} = - \int_0^{\infty} R(m,t) Y(m,t) dm + \int_0^{\infty} m S(m,t) dm. \quad (57)$$

This equation multiplied by the volume states that the rate of increase of airborne mass equals the rate supplied by sources less the rate removed by deposition and leakage. Clearly, the agglomeration terms have cancelled as one would expect. However, this is not the case for the discretized equivalent to Eq. (57) without the factor  $n_{jk}$  in  $P_{jk}^i$ . In many applications, the removal and source terms in Eq. (50) can be small compared to the agglomeration terms. It is consequently important that the agglomeration terms cancel exactly to ensure that the removal and source terms are not swamped by cancellation errors. We therefore choose  $n_{jk}$  to achieve this.

The trapezoidal rule is used to estimate  $\rho$  (Eq. (67) in Sub-section 3.3) from which we obtain our discretized form of the mass balance equation

$$\frac{\partial \rho}{\partial t} = h \left\{ \sum_{i,j,k} m_i P_{jk}^i K_{jk} Y_j Y_k - \sum_{i,j} m_i D_j^i K_{ij} Y_i Y_j - \sum_i m_i R_i Y + \sum_i m_i^2 S_i \right\}. \quad (58)$$

The first two terms on the right hand side must cancel exactly, whatever the values of  $Y_i$  for  $i = 1, \dots, n$ . A sufficient condition is therefore to require that the sum of all coefficients of terms involving  $Y_r Y_s$  for any  $r$  and  $s$  must be zero. We find that  $P_{jk}^i$  and  $D_j^i$  must be related by



$$\sum_i m_i (P_{rs}^i + P_{sr}^i) = m_r D_s^r + m_s D_r^s = h (m_r + m_s) . \quad (59)$$

We see this amounts to  $n(n+1)/2$  constraints on  $n_{rs}$  only. It is therefore convenient to choose it to be symmetric.

Six options for  $g$  are provided in CHARM. The element shown by Wheatley (1988) to give the best results when  $n$  is small is

$$\begin{aligned} g(x) &= 1 - |x| , & |x| < 1 \\ g(x) &= 0 , & |x| \geq 1 \end{aligned} \quad (60)$$

It gives rise to continuous piece-wise linear finite-element expansions. It has the particular advantage here that  $g$  is non-negative everywhere and so all the  $P_{jk}^i$  are non-negative. This is sufficient to ensure that no component of the solution of the discretized equation changes sign, as must be so on physical grounds. See Appendix D for details of the other basic elements.

### 3.2 The solution method

The ODE's are solved with the Fortran subroutine DEBDF written by Shampine and Watts (1979). It is based on the variable order backward differentiation method for stiff ODE's due to Hindmarsh.  $n + 5$  coupled ODE's are solved in all; the additional five equations are integrators for the source mass, the leaked mass, and the masses deposited on the wall, floor and ceiling respectively.

The local absolute error in  $Y_i$  is constrained during the integration as follows

$$\delta Y_i < \epsilon/h \text{ minimum}(N, \rho/m_i) , \quad (61)$$

where  $\epsilon$  is a relative tolerance parameter supplied by the user. This test is designed to result in estimates for  $N$  and  $\rho$  with a relative accuracy equal to or less than  $\epsilon$ . It is more efficient than requiring  $\delta Y_i < \epsilon Y_i$  since it is not necessary to integrate the tails of the distribution as accurately as the bulk in order to obtain accurate estimates for the quantities of main interest.

However, the chosen tolerance criterion permits components of  $Y$  to become negative, even though the discretized equation may not admit a change of sign. We have not found this to be troublesome when using the linear finite-element but we cannot rule-out that changes of sign may cause difficulties in some cases. Substituting  $\log_e Y_i$  for  $Y_i$  as the independent variable or tightening the tolerance required of  $\delta Y_i$  in the tails may solve the trouble should it arise.

### 3.3 Moments of the discretized distribution

The moments we consider are  $\rho$ , the aerosol density,  $N$ , the aerosol number concentration,  $m_{50}$ , the mass median mass,  $m_g$ , the geometric mean mass, and  $\sigma$ , the cube root of the geometric standard deviation with respect to mass. These are defined by

$$\rho = \int_0^{\infty} mY(m,t)d\log_e(m) , \quad (62)$$

$$N = \int_0^{\infty} Y(m,t)d\log_e(m) , \quad (63)$$

$$\rho/2 = \int_0^{m_{50}} mY(m,t)d\log_e(m) , \quad (64)$$

$$N \log_e(m_g) = \int_0^{\infty} \log_e(m)Y(m,t)d\log_e(m) , \quad (65)$$

and

$$N \log_e^2(\sigma^3) = \int_0^{\infty} \log_e^2(m/m_g)Y(m,t)d\log_e(m) . \quad (66)$$

The definitions of  $m_g$  and  $\sigma$  are based on the number concentration distribution; the cube power in the equation for  $\sigma$  is conventional.

$\rho$  times the cell volume is the total airborne aerosol mass. Similarly,  $N$  times the cell volume is the total number of airborne aerosol particles.  $m_{50}$  is sometimes called the mass median particle size. Approximately half the airborne particles have mass less than  $m_g$ .  $\sigma$  is a measure of the spread of the distribution. For a log-normal number distribution 68% of the particles have masses in the range  $m_g/\sigma^3$  to  $m_g\sigma^3$  and 68% of the airborne mass derives from particles with masses in the range  $m_{50}/\sigma^3$  to  $m_{50}\sigma^3$ . Often, these relationships hold reasonably well for distributions found in practice.

We now consider the numerical estimation of these moments. Their evaluation with the extended trapezoidal rule is straightforward for all except  $m_{50}$  and illustrated only for  $\rho$ . The estimate for  $\rho$  is

$$\rho = h \sum_i m_i Y_i , \quad (67)$$

where  $Y_i$  is shorthand for  $Y(m_i,t)$  and the summation extends over all values for which the indicated index is defined.  $Y(m,t)$  has been assumed to decrease to negligible value between  $m_1$  and  $m_1 e^{-h}$  and between  $m_n$  and  $m_n e^h$ .

$m_{50}$  generally lies between adjacent grid points so we estimate the integral in Eq. (64) by using a finite-element expansion for the integrand. When the linear finite-element is chosen, this is equivalent to using the extended trapezoidal

rule to estimate the contribution to the integral up to the grid point immediately below  $m_{50}$  and then using linear interpolation between the grid points either side of  $m_{50}$  to estimate the remainder.

### 3.4 The treatment of time-dependencies

We refer here to time-dependent input variables which we suppose are to be supplied as tables of values at discrete times. There are two aspects to this. First, how are values to be estimated at intermediate times and, second, how should these time-dependencies be handled within the model.

With regard to the first aspect, we desire the flexibility to treat both continuous and discontinuous variations. For example, the source mass release rate may change discontinuously at certain times and vary continuously otherwise. This is simply handled by linearly interpolating between data points supplied at consecutive (non-equal) times and requiring two sets of data points to be supplied at discontinuities, one set to be used for interpolation before the discontinuity, and the second to be used for interpolation after the discontinuity. It is convenient to use constant extrapolation from the extreme data points when they do not span the range of times covered in the calculational problem. Further details are given in Sub-section 4.2.

With regard to the second aspect, we anticipate that it can be too costly computationally in some cases to continuously update the time-dependent variables and those that depend on them during the integration of the governing equations, despite the efficient treatment of the agglomeration kernel by the discretization method we use. So, although the option to continuously update these variables can be provided, some alternative must be allowed for. The simplest alternative, and the one we choose, is to update these variables at discrete times and otherwise to keep them constant. Further details are given in Sub-section 4.2 - also see the discussion in Sub-section 6.4.

## 4 THE INPUT DATA FILE

### 4.1 Overview

Input data is read from tape4 (FORTRAN unit number 4) which is assigned to the file CHARMPAT on the local file area. The file is assumed to have no more than 72 columns per line.

The data is read with list directed read statements with a loop over each statement to cause reading to restart at the next line when a character other than a ",", or "/" is encountered on the current line. This permits considerable flexibility over the format of the data file. The salient points are as follows:

- i Lines with characters other than a ",", or "/" and not counting free format numbers are ignored. A character can therefore be intentionally inserted into a line to enable it to be treated as a comment line. For example a "\$" could be inserted in column 1, as is done in the example considered in Sub-section 4.4.
- ii All data items are read in free format. For example, this allows the real number 1.0 to be entered as 1, 1.0 or 1.e0 and any number of spaces can separate data items which, for a single read list, can be entered on more than one concurrent line. It is important that data items are entered with an acceptable format since otherwise the current line will be treated as a comment line and reading for the current read list will recommence at the next line.
- iii Items in a read list can be skipped by inserting a space followed by a comma (,) where the data item would otherwise go. The remainder of the read list can be skipped by inserting a "/". This allows default values to be assigned to variables merely by skipping over those variables when they occur in the read lists.

The reader is referred to the ANSI standard for Fortran 77 (American National Standards Institute, 1978) for detailed rules regarding what permissible formats the data may take consistent with list directed read statements. However, with the example in Sub-section 4.4 the user should find it easy to compose his or her own data files.

Some data items are checked for valid values (see Sub-section 6.5 for details) but generally this is not done. Guidance is given in the next sub-section on suitable values for all data items.

All data items must have S. I. units except molecular weights must have units kg / kmole (i.e. g / mole).

A number of input variables are treated as time-dependent. The user must enter a table of times to which corresponding values of these variables must be entered later in the file. Interpolation formulae are used in the model to estimate values of these variables at any time between zero (the start of the problem) and the problem end time. The minimum and maximum times in the table need not span the time period of the problem. Variables are extrapolated with constant values when this happens. Adjacent times in the table can be equal to enable variables to change discontinuously. If fewer values for a variable are entered than needed then missing values are copied from preceding values in the supplied table. A default value exists for the first data item of each variable.

In the next sub-section we will define the variables in each read list in turn, give acceptable ranges and, where appropriate, recommend values. Default values of all data items are given in Sub-section 4.3 and we discuss an example in Sub-section 4.4.

#### 4.2 Detailed description

In the following, all variables in one read list are shown on a single line.

##### Output flags

A group of output variables is associated with each flag, as described in Section 5. The values of the variables in each group will be written on the output file OUT every  $q^{\text{th}}$  output step, where  $q$  is the value of the flag corresponding to the group. Variables independent of time are only written at the zeroth time step. No information is written when the flag is zero. The flags must be integers and are read in the following order:

cell properties	gas properties	aerosol constants
source moments	source distributions	flow properties
masses	radii	mobilities
deposition rates	agglomeration rates	
indexing	production coefficients	normalization factors
mass balances	tolerances	
moments	number distribution	mass distribution

##### Time step information

Output is written at intervals given by  $\text{TIMESTEP}(i)$  until the problem time equals  $\text{TIMEEND}(i)$ , when output is written at  $\text{TIMEEND}(i)$  and  $i$  is increased by 1.

The last value of TIMEEND, TIMEEND(NTIME), defines the time at which the calculation stops.

NTIME must be a positive integer no greater than 20. TIMESTEP(i) and TIMEEND(i) must be positive real numbers and NTIME values each must be entered. Consecutive values of TIMEEND must increase. These variables are read in the following order:

NTIME  
TIMESTEP(1), TIMEEND(1), TIMESTEP(2), TIMEEND(2), etc.

#### Number of columns on the output file

The output file, OUT, can be written with either a maximum of 80 or 132 columns per line. Enter an integer value on one line. Any integer not equal to 80 is interpreted to mean that the file can have up to 132 characters per line.

#### Times at which data for the time-dependent variables are to be provided

See the general discussion in the preceding sub-section. Values for the time-dependent variables are to be supplied corresponding to the times TIMEDATA(1) to TIMEDATA(NDATA). NDATA is the number of data points per variable and must be a positive integer no greater than 20. Consecutive values of TIMEDATA must not decrease. These variables are read in the following order:

NDATA  
TIMEDATA(1), TIMEDATA(2), etc.

#### Frequency with which the time-dependent variables are to be revised

The quantity to be entered here (THHSTEP) is the maximum time which is allowed to elapse since the time-dependent variables were last revised before they are revised again. THHSTEP must be a non-negative real number. The time-dependent variables are revised continuously when THHSTEP is zero.

#### Cell data

The aerosol evolves in a region called here a cell. We refer to all upward facing horizontal surfaces, vertical surfaces and downward facing horizontal surfaces within the cell as the ceiling (c), wall (w) and floor (f) respectively.

The surface areas must be non-negative real numbers and entered in the following order:

$A_c$  $A_w$  $A_f$ 

The surface temperatures are treated as time-dependent variables. They must be non-negative real numbers and no more than NDATA sets of values in the following order must be entered:

$$T_c(1), T_w(1), T_f(1), T_c(2), T_w(2), T_f(2), \text{ etc.}$$

The cell volume, which is defined as the volume of free space within the cell, must be a positive real number and the leak rate, which is defined as the number of volume changes of gas in the cell per second, must be a non-negative real number. They must be entered in the following order:

 $V$  $\lambda_1$ 

The hydraulic diameter and the equivalent sand roughness are defined in Subsection 2.3. They must be non-negative real numbers and entered in the following order:

 $d_h$  $z_s$ 

#### Gas data

The gas temperature, pressure and velocity are treated as time-dependent variables. The temperature, pressure and, gas and vapor molecular weights must be positive numbers and the remaining variables must be non-negative real numbers. The data must be entered in the following order:

$$T(1), P(1), U(1), T(2), P(2), U(2), \text{ etc.}$$
 $W_g$  $f_c$  $\frac{dc_c}{dx}$  $a_g$  $f_w$  $\frac{dc_w}{dx}$  $W_v$  $f_f$  $\frac{dc_f}{dx}$

### Boundary layer data

These data provide an option for the user to over-ride the calculation of boundary layer thicknesses in the model. This can be done by setting the value of BLFLAG to be non-zero and providing values for  $\delta_*$  and  $\delta_D$ . A single value only is required for  $\delta_D$  which is assumed to apply irrespective of particle size. BLFLAG must be integer and  $\delta_*$  and  $\delta_D$  must be non-negative real numbers. Deposition by thermophoresis is ignored when  $\delta_*$  is zero and deposition by Brownian diffusion is ignored when  $\delta_D$  is zero. The data must be entered in the following order:

BLFLAG	$\delta_*$	$\delta_D$
--------	------------	------------

### Initial aerosol

The initial aerosol is assumed to be log-normal in the number concentration distribution and is parameterized by the moments  $\sigma$ ,  $r_{50}$  and  $\rho$  (see Sub-section 3.3 for the definition of these quantities).  $\sigma$  and  $r_{50}$  must be positive real numbers and  $\rho$  must be a non-negative real number. They must be entered in the following order:

$\sigma$	$r_{50}$	$\rho$
----------	----------	--------

### Source aerosol

The source aerosol is assumed to be log-normal in the number concentration distribution and is parameterized by the moments  $\sigma$ ,  $r_{50}$  and  $d\rho/dt$ .  $d\rho/dt$  is defined to be the mass release rate of the source divided by the cell volume. The moments are treated as time-dependent variables.  $\sigma$  and  $r_{50}$  must be positive real numbers and  $d\rho/dt$  must be a non-negative real number. They must be entered in the following order:

$\sigma(1)$ ,  $r_{50}(1)$ ,  $\rho(1)$ ,  $\sigma(2)$ ,  $r_{50}(2)$ ,  $\rho(2)$ , etc.

### Definition of collocation points

The collocation points can be specified in two ways. The first is to specify the number of points and the masses of the lower and upper points. Alternatively, values for  $e^h$ ,  $m_1$  and  $m_n$  can be specified. In either case, the model will calculate the intermediate points according to Eq. (49) (except  $m_n$  may be increased slightly in the second case). The second option is selected when the input value for  $n$  is set to zero.



$m_1$  and  $m_n$  should be chosen so that the aerosol mass and number distributions are comfortably encompassed between the two values.  $e^b$  should not be chosen so large that the distributions span only a small number of points. See Sub-sections 6.3 and 6.4 for further guidance on how to choose values for these quantities. The defaults set by the model will be reasonably satisfactory in most cases.

One of six different basic elements can be selected by assigning a value to NELEMENT. Element 2 is the linear finite-element which should be used in all normal circumstances. Element 3 may be useful when very accurate results are required but it will give unreliable results when the collocation point spacing is large. The other elements (NELEMENT = 1, 4, 5 and 6) were included as options during development of the numerical method and have since not been removed. We do not recommend using any of these alternative options.

$n$  must be a non-negative integer and  $e^b$ ,  $m_1$  and  $m_n$  must be positive real numbers.  $n$  is set to 100 when a value greater than 100 is specified in the input or when the second option is selected and the calculated number of points exceeds 100. NELEMENT must be a positive integer no greater than 6. These variables must be entered in the following order:

$n$	$e^b$
$m_1$	$m_n$
NELEMENT	

#### Tolerance specifications

$\epsilon$  is a relative error parameter. It is used to set tolerances for the integration of the differential equations and set a relative tolerance for the location of zeros of functions and the values of integrals.  $\eta$  defines an absolute tolerance on the value of a function whose zero is sought.  $\zeta$  determines when bisection is used in favor of inverse quadratic interpolation to locate the zero of a function.

A reasonable range from which to select a value for  $\epsilon$  is  $10^{-8}$  to  $10^{-6}$ . The model may not work satisfactorily when  $\epsilon$  is made too large or too small. A value of  $10^{-6}$  has so far proved to be generally satisfactory. Further guidance on choosing  $\epsilon$  is given in Sub-sections 6.3 and 6.4. We would recommend that the user always use the default values for  $\eta$  and  $\zeta$ .

Up to MAXCALLS evaluations of a function can be made in an attempt to locate its zero to the desired tolerance. This may need to be increased over the default value when  $\epsilon$  is made very small.

MAXTRYS determines how many integration steps are attempted by DEBDF to integrate the equations to the next specified time (the number of attempted steps is 500 times MAXTRYS). This may need to be increased over the default value when  $\epsilon$  is made exceedingly small or when output is required infrequently.

MAXCALLS and MAXTRYS must be positive integers.  $\epsilon$  must be a positive real number and  $\eta$  and  $\zeta$  must be real numbers.

These variables must be entered in the following order:

$\epsilon$	MAXCALLS	MAXTRYS
$\eta$	$\zeta$	

#### Aerosol physics data

These comprise physical properties of the aerosol material and constants which appear in the models for agglomeration and deposition.  $\chi_s$ ,  $k_a$ ,  $k_q$ ,  $k_b$  and  $b_k$  must be non-negative real numbers and the remaining data items must be positive real numbers.  $\chi_c$  and  $\chi_d$  are unity for spherical particles and greater than unity otherwise. These data items must be entered in the following order:

$\rho_p$	$a_p$	
$\chi_c$	$\chi_d$	$\chi_s$
$k_a$	$k_q$	$k_b$
$b_k$	$b_m$	$b_t$

#### 4.3 The default data

We have described in Sub-section 4.1 how default values for data items can be assigned. This will be illustrated in the example in Sub-section 4.4. Here we define the default values.

It is convenient to do this by constructing a data file, shown below, whose effect is to assign all data items with their default values. This will make it easy for the user to decide when he or she needs to over-ride a default value. Of course, the data file which follows would not be used in practice since the default values can be assigned in their entirety merely by putting a / in column 1 of every line of the data file corresponding to a read list.

Some values require explanation. THYSTEP is assigned an exceedingly large value ( $10^{10}$ ) so that the time-dependent variables are recalculated only when a new set of interpolation formulae apply which, when NDATA is 1, will not occur. All temperatures and the pressure are standard (i.e. 20°C and 1 standard atmosphere). The value assigned to the equivalent sand roughness is that for

structural and forged steel - see Sub-section 2.3 for clarification. The gas in the bulk of the cell is taken to be pure air and the vapor adjacent to surfaces promoting diffusio-phoresis is taken to be steam. The aerosol particle properties are for sodium oxide and the remaining aerosol physics data are the default values used in MAEROS.

### The default input data

```

S .....
S Input data file for the CHARM aerosol code
S .....
S
S Output flags
S .....
S
S cell properties      gas properties      aerosol constants
S      1                1                1
S
S source moments      source distribution      flow properties
S      1                0                1
S
S masses              radii              mobilities
S      1                1                0
S
S deposition rates    agglomeration rates
S      0                0
S
S indexing            production coefficients      normalization factors
S      0                0                0
S
S mass balances        tolerances
S      1                0
S
S moments              number distribution      mass distribution
S      1                0                0
S
S Time step information
S .....
S
S ntime
S      1
S
S timestep      timeend
S      10.e0      10.e0
S
S Number of columns on output file
S .....
S
S      80
S
S Times when time-dependent data is provided
S .....
S
S ndata
S      1
S
S times in consecutive order
S
S      0.e0
S
S Frequency with which the time-dependent variables are to be revised
S .....
S
S 1.e10
S
S Cell data
S .....

```

```

$
$ ceiling area          wall area          floor area
$   0.e0              0.e0              0.e0
$
$ ceiling temp.        wall temp.        floor temp.
$ 293.15e0           293.15e0         293.15e0/
$
$ volume              leak rate
$ 1.e5               0.e0
$
$ hydraulic diameter    equivalent roughness
$ 0.e0              4.5e-5
$
$ Gas data
$ *****
$
$ temperature          pressure          velocity
$ 293.15e0           1.01325e5         0.e0/
$
$ molecular weight      thermal conductivity      vapor molecular weight
$ 28.96e0            .0255e0           18.015e0
$
$ vapor mole fraction near the...
$ ceiling            wall            floor
$ 0.e0              0.e0            0.e0
$
$ vapor conc. gradient (kg/m**4) near the...
$ ceiling            wall            floor
$ 0.e0              0.e0            0.e0
$
$ Boundary layer data
$ *****
$
$ b.l. flag           viscous b.l.           diffusion b.l.
$ 0                  0.e0                 0.e0
$
$ Initial aerosol
$ *****
$
$ sigma              rad50              density
$ 2.e0              .5e-8              0.e0
$
$ Source aerosol
$ *****
$
$ sigma              rad50              density generation rate
$ 2.e0              .5e-8              0.e0/
$
$ Definition of collocation points
$ *****
$
$ ncoll            spacing
$ 0                10.e0
$
$ mlower           mupper
$ 4.e-21          4.e-9
$
$ element number
$ 2
$
$ Tolerance specification
$ *****
$
$ eps              maxcalls          maxtrys
$ 1.e-6            30                10
$
$ eta              zeta
$ 0.e0            .5e0
$

```

```

$ Aerosol physics data
$ *****
$
$ particle density          particle thermal conductivity
      2.8e3                  .6375e0
$
$ collision shape factor    dynamic shape factor      sticking efficiency
      1.e0                   1.e0                          1.e0
$
$ a knudsen-weber          q knudsen-weber          b knudsen-weber
      1.37e0                 .4e0                      1.1e0
$
$ k brock                  cm brock                  ct brock
      1.e0                   1.37e0                     1.e0
$
$ *****
$ End of the input data file
$ *****

```

---

#### 4.4 An example

The preceding discussion is illustrated with an example. The physical problem we consider is that of a sodium pool fire releasing sodium oxide aerosol into a containment building for 10 hours. The details of the problem are taken from Dunbar et al. (1984) and are reproduced in the table below. This is also the test problem considered in Wheatley (1988). The data file for this problem is shown at the end of this sub-section; it was used to generate the output file shown in Appendix A and is discussed in Sub-section 5.3 (We note two minor differences with the calculations presented in Wheatley (1988). First, the factor 0.0594 in Eq. (28) was not included and, second,  $b_k$ ,  $b_m$  and  $b_t$  were chosen as 1.0, 1.0 and 2.48 respectively to enable like-for-like comparisons with results given in Dunbar et al. obtained from the PARDISEKO model).

### Parameters for the example problem.

---

Aerosol composition	Sodium oxide
Particle density	2800 kgm <sup>-3</sup>
Source distribution	Log-normal in C(m,t)
Source rate	2 tonnes per hour
Source $\sigma$	2 (no units)
Source $r_{50}$	.5 $\mu\text{m}$
Source duration	10 hours
Problem duration	34 hours
Containment volume	180000 m <sup>3</sup>
Wall area	20000 m <sup>2</sup>
Floor area	2800 m <sup>2</sup>
Wall and floor temperatures	90 °C
Containment leak rate	1% by volume per day
Gas composition	Air
Gas temperature	100 °C
Pressure	100000 Pa
Turbulent energy dissipation rate	0. m <sup>2</sup> s <sup>-3</sup>

---

It can be seen from the file that liberal use has been made of the ability to add comment lines. This enables a title, labels and explanations to be included to clarify the file. It is recommended that this is always done.

Some of the output flags have been assigned the value 100. This is done because although the variables assigned to these flags are in general time-dependent they are constant for this particular data file. The value 100 is chosen to exceed the number of output steps and so these variables are written on the output file at the zeroth step only.

The time step information is chosen so that output is written at 5 minute intervals for the first hour and also for half an hour after the source emission rate has decreased to zero (at 10 hours). Output is otherwise written at hourly intervals.

The only dependent variable to change with time is the source emission rate which is constant except at 10 hours when it changes discontinuously. NDATA is therefore 2 and the corresponding two times are both 10 hours. THYSTEP is assigned the default value 10<sup>10</sup> so the time-dependent variables are recalculated only at 10 hours.

The cell and gas data are straightforward to follow. The comma beneath the label CEILING AREA causes the ceiling area to be assigned its default value of zero.

The values assigned to the hydraulic diameter and the equivalent sand roughness are irrelevant since the gas velocity is zero. Only one set of data values is entered for the gas temperature, pressure and velocity since these are constant throughout the calculation. The line with these values must be terminated with a "/", as shown, so that the current read list is terminated and reading continues with the next read list (the vapor mole fractions). There is no diffusiophoresis in the problem so the vapor mole fractions and concentration gradients are assigned default values of zero.

The boundary layer flag is set to unity so that values can be assigned to the boundary layer thicknesses. There is no initial aerosol so default values are assigned to the moments of the initial aerosol.

As noted previously, the mass generation rate of the source aerosol changes discontinuously at 10 hours so two values are entered for this quantity; the first value applies up to 10 hours and the second applies after 10 hours. Note that the commas in the second line of data cause  $\sigma(2)$  and  $r_{60}(2)$  to be assigned their values in the previous line.

The tolerance variables are assigned default values. For the aerosol physics data, the collision and dynamic shape factors are increased to 1.5 but the sticking efficiency is assigned its default value.

### The example input data file

```

$ .....
$ Input data file for the CHARM aerosol code
$ .....
$
$ ..... The example input data file. ....
$ *** The sodium pool fire problem from Dunbar et al. (1984). ***
$ .....
$
$ Output flags
$ .....
$
$   cell properties      gas properties      aerosol constants
$     100                100                1
$
$   source moments      source distribution    flow properties
$     1                  100                100
$
$     masses            radii                mobilities
$     1                  1                  100
$
$   deposition rates    agglomeration rates
$     100                100
$
$     indexing          production coefficients    normalization factors
$     1                  1                1
$
$   mass balances      tolerances
$     1                  1
$
$     moments          number distribution      mass distribution

```

```

      1              3              3
$
$ Time step information
$ *****
$
$ ntime
$   4
$
$ timestep      timeend
$   300.e0      3600.e0
$   3600.e0     36000.e0
$   300.e0      37800.e0
$   3600.e0     122400.e0
$
$ Number of columns on output file
$ *****
$
$   80
$
$ Times when time-dependent data is provided
$ *****
$
$ ndata
$   2
$
$ times in consecutive order
$
$ 36000.e0 36000.e0
$
$ Frequency with which the time-dependent variables are to be revised
$ *****
$
$ /
$
$ Cell data
$ *****
$
$ ceiling area      wall area      floor area
$                   20.e3          2.8e3
$
$ ceiling temp.    wall temp.    floor temp.
$   363.15e0      363.15e0    363.15e0/
$
$ volume           leak rate
$ 180000.e0        1.1574074074e-7
$
$ hydraulic diameter      equivalent roughness
$ /
$
$ Gas data
$ *****
$
$ temperature      pressure      velocity
$   373.15e0        1.e5/
$
$ molecular weight      thermal conductivity      vapor molecular weight
$ /
$
$ vapor mole fraction near the...
$ ceiling      wall      floor
$ /
$
$ vapor conc. gradient (kg/m**4) near the...
$ ceiling      wall      floor
$ /
$
$ Boundary layer data
$ *****
$

```



```

$ b.l. flag          viscous b.l.          diffusion b.l.
  1                  1.e-3                  1.e-4
$
$ Initial aerosol
$ *****
$
$   sigma          rad50          density
/
$
$ Source aerosol
$ *****
$
$   sigma          rad50          density generation rate
  2.e0            .5e-8          3.086419753e-8
  ,              ,              0.e2/
$
$ Definition of collocation points
$ *****
$
$   ncoll          spacing
/
$
$   mlower          mupper
/
$
$   element number
/
$
$ Tolerance specification
$ *****
$
$   eps            maxcalls          maxtrys
/
$
$   eta            zeta
/
$
$ Aerosol physics data
$ *****
$
$   particle density          particle thermal conductivity
/
$
$   collision shape factor    dynamic shape factor    sticking efficiency
  1.5e0                      1.5e0/
$
$   a knudsen-weber          q knudsen-weber          b knudsen-weber
/
$
$   k brock                  cm brock                  ct brock
/
$
$ *****
$ End of the input data file
$ *****

```

---

## 5 OUTPUT FILES

### 5.1 Overview

Output is written to two files.

The first is tape5 (Fortran unit number 5) which is the terminal when the model is executed interactively. The output will comprise: a copy of the input data file (which provides an identity for the succeeding output), one line of information for each successful integration to a time when output has been requested (to enable the progress of the calculation to be monitored), and error messages. The file is assumed to have a width of no more than 80 characters and no form control characters are written.

The second is tape6 (Fortran unit number 6) which is identified with the file OUT. OUT will appear in the local file area, over writing any pre-existing file of that name. It can be sent to an output device, viewed with an editor or permanently stored for later use. The output will comprise: a copy of the input data file, one line of information (identical to that written on tape5) for each successful integration to a time when output has been requested, computational results or information, and error messages. The file is assumed to have a width no greater than 80 or 132 characters, according to the value of COLUMNS chosen by the user, and no form control characters are written.

The one line of information and the succeeding computational results are described in detail in the remainder of this section. Error messages are discussed in Sub-section 6.5.

The one line of information comprises: the output step number, the current time and a mass check. The output step number starts at zero (i.e. at time equals zero) and increases by unity each time the governing equations have been integrated to a time when output has been requested. The mass check provides a measure of how accurately the governing equations have been solved. It is a mass balance (in kg) and with perfect arithmetic should be exactly zero.

We conclude this sub-section with some general points about the computational results.

Quantities appearing on the output have S. I. units throughout except molecular weights have units kg / kmole.

The computational results or information are divided into 20 groups. The output flags set by the user in the input data file determine which groups are written, except that the first group, the mass budget, is always written. Of the

remainder, some comprise entirely time-independent quantities and are therefore only written at the zeroth output step and only if the corresponding output flag has a value different from zero. Some groups comprise entirely quantities which are (or may be, depending on the thermal-hydraulic conditions) time-dependent. If the output flag corresponding to each of these groups is non-zero then the group is written in its entirety when the output step number is a multiple of the flag. A few groups comprise a mixture of time-independent and time-dependent quantities. Generally, the time-independent quantities are written at the zeroth step only otherwise the groups are treated as though they comprise entirely time-dependent quantities.

This scheme provides the user with considerable flexibility over what information is written without the necessity of always writing exceedingly large output files.

## 5.2 Definition of output groups and variables

In this sub-section, we describe what information is written for each group in order of appearance on the output file. The titles in brackets in what follows are those which appear on the output file corresponding to the defined variables.

### The mass budget

This group comprises the airborne aerosol mass and the accumulated mass (since time equals zero) on floor, wall and ceiling, leaked and released from the source.

### Airborne aerosol moments

This group comprises  $\sigma$  (SIGMA),  $r_{50}$  (RAD50),  $\rho$  (MDENSITY),  $N$  (NDENSITY),  $m_g$  (GEOMMEAN), and  $m_{50}$  (MASS50) for the airborne aerosol.

### Source moments

This group comprises  $\sigma$  (SIGMA),  $r_{50}$  (RAD50),  $d\rho/dt$  (MDENSITY),  $dN/dt$  (NDENSITY),  $m_g$  (GEOMMEAN), and  $m_{50}$  (MASS50) for the source.

### The airborne mass distribution

This group comprises  $m_i Y_i$  for  $i = 1, \dots, n$ .

### The airborne number distribution

This group comprises  $Y_i$  for  $i = 1, \dots, n$ .

### The source mass and number distributions

This group comprises  $m_i^2 S_i$  and  $m_i S_i$  for  $i = 1, \dots, n$ .

### Collocation information

This group comprises the identification number of the chosen basic finite-element (NELEMENT), the half-width of this element (HWIDTH),  $n$  (NCOLL),  $m_{i+1}/m_i$  i.e.  $e^h$  (SPACING), and  $m_n/m_1$  (RANGE).

### Indexing for the production coefficients

This group comprises the information which enables all values of  $i$ ,  $j$  and  $k$  to be found for which  $P_{jk}^i$  is non-zero. The value of  $P_{jk}^i$  depends only on the values of  $j = i - j$  (JBAR) and  $k = i - k$  (KBAR). The following quantities are written for each permissible value of  $j$ : the minimum and maximum values of  $k$  for which  $P_{jk}^i$  is non-zero (KBARMIN and KBARMAX), the number of these values (NKBAR), and an index (INDEX) which is used to locate the non-zero values of  $P_{jk}^i$  stored consecutively in a one-dimensional array.

### The production coefficients

This group comprises all non-zero values of  $P_{jk}^i$ .  $\text{INDEX}(j)+k$  is the position of  $P_{jk}^i$  in the list;  $j$  and  $k$  must lie in valid ranges which can be determined from the previous output group.

### The normalization factors

This group comprises all values of  $n_{jk}$ . They are written in the following order:  $n_{11}, n_{12}, n_{13}, \dots, n_{21}, n_{22}$ , etc.

### The collocation points

This group comprises  $m_i$  for  $i = 1, \dots, n$ .

### Particle radii

This group comprises  $r_i$  for  $i = 1, \dots, n$ .

### Tolerance information

This group comprises  $\epsilon$  (EPS),  $\eta$  (ETA),  $\zeta$  (ZETA), the maximum number of function calls CO5WHE can make in order to find one zero (MAXCALLS), and the maximum number of times DEBDF will be called to integrate the governing equations to the next requested time (MAXTRYS).

### Aerosol physics data

This group comprises  $\chi_c$  (CSHPFCTR),  $\chi_d$  (DSHPFCTR),  $\chi_s$  (STICKEFF),  $k_a$  (AKNUDWEB),  $k_g$  (QKNUDWEB),  $k_b$  (BKNUDWEB),  $\rho_p$  (PDENSITY),  $\alpha_p$  (PTHRMCN),  $b_k$  (KBROCK),  $b_m$  (CMBROCK) and  $b_t$  (CTBROCK).

### Cell data

This group comprises V (VOLUME),  $\lambda_1$  (LEAKR...d),  $d_b$  (HYDRDIAM),  $z_w$  (EQVROUGH),  $A_c$  (AREACLNG),  $A_w$  (AREAWALL),  $A_f$  (AREAFLO),  $T_c$  (TEMPCLNG),  $T_w$  (TEMPWALL) and  $T_f$  (TEMPFLOR).

### Gas data

This group comprises T (TEMP), P (PRESS), U (VELOCITY),  $\rho_g$  (GDENSITY),  $\eta_g$  (DYNVISC),  $i$  (MNFRPATH),  $w_g$  (MOLWT),  $\alpha_g$  (GTHRMCN),  $w_w$  (MOLWT),  $D_v$  (DIFFUSV),  $f_c$  (VMFRCLNG),  $f_w$  (VMFRWALL),  $f_f$  (VMFRFLOR),  $dc_c/dx$  (VCGRCLNG),  $dc_w/dx$  (VCGRWALL),  $dc_f/dx$  (VCGRFLOR),  $c_c$  (VCONCLNG),  $c_w$  (VCONWALL) and  $c_f$  (VCONFLOR).

### Flow data

This group comprises  $\epsilon_s$  (EDDYDISS),  $u_s$  (USTAR),  $\delta_s$  (VBLTHICK) and  $\delta_{Di}$  for  $i = 1 \dots n$  (DBLTHICK).

### Particle mobilities

This group comprises  $B_i$  for  $i = 1, \dots, n$  (MOBILITY).

### Deposition rates

This group comprises  $\lambda_{ci}$  for  $i = 1, \dots, n$ ,  $\lambda_{wi}$  for  $i = 1, \dots, n$  and  $\lambda_{fi}$  for  $i = 1, \dots, n$ .

### The agglomeration kernel

This group comprises all values of  $K_{jk}$ . They are written in the following order:  $K_{11}, K_{12}, K_{13}, \dots, K_{21}, K_{22}$ , etc.

### 5.3 An example

An example output file, OUT, is shown in Appendix A. It was obtained from the example input data file considered in Sub-section 4.4. In addition to illustrating the previous discussion we have included it in full to assist users in the validation of their implementations of CEARM. We expect it to be straightforward to follow so we only make a few points of clarification here.

Since all the output flags are non-zero, all input data items, except the data for the time-dependent external variables, are shown at the zeroth step on the output file, whether assigned values in the input data file or not. This enables all the parameters of the problem, including all model constants, to be verified.

The collocation information was derived entirely from default values. This will be adequate in most cases, however, we would recommend repeating the calculation with a larger values of  $n$  in order to check that the results have converged sufficiently well in this parameter. See Sub-section 6.4.

It can be seen that all the normalization factors except  $n_{nn}$  are close to unity. This provides confidence in the calculations resulting in the production coefficients.  $n_{nn}$  is significantly different from unity because there are no collocation points beyond  $m_n$ .

At output steps 1 and beyond one can see that the mass balance (MASS CHECK) is never larger than the order of  $4 \times 10^{-6}$  kg which is satisfactorily small in relation to the total mass of aerosol released by the source,  $2 \times 10^4$  kg. This is a good indication that  $\epsilon$  is suitably small ( $10^{-6}$ ). Nevertheless, we would recommend repeating the calculation with a different value of  $\epsilon$ , say  $10^{-4}$  or  $10^{-8}$ , in order to check that the results have converged sufficiently well as a function of this parameter. See Sub-section 6.4.

For the first hour and also for half an hour beyond the termination of the source, output is written every 5 minutes so that detail is not lost during these rapid transients. The remaining output is written at hourly intervals.

One can also see that the aerosol mass and number distributions have only been written every third output step. This can amount to a considerable saving of paper when  $n$  is large! It can be seen from the distributions that  $Y_1$  and  $Y_n$  always remain small compared to  $N$ , and  $m_1 Y_1$  and  $m_n Y_n$  always remain small compared to  $\rho$ . This indicates that  $m_1$  and  $m_n$  have been chosen suitably small and large respectively.

## 6 EXECUTION

### 6.1 Machine attributes

The information given here may be helpful to those who wish to implement the model on a non-Cray computer or under an operating system different from CTSS (the Cray Time-Sharing System).

CHARM was developed and tested entirely on Cray-1 and Cray-XMP computers. The operating system used was CTSS, developed at the Los Alamos National Laboratories, USA.

The standard word length is 64 bits, which is used for integers and single precision real numbers. Double precision real numbers use 128 bits.

Of particular importance are the exponent range and the number of significant digits of single precision real numbers. They have 15 exponent bits which give a range  $10^{-2486}$  to  $10^{2486}$  and 48 mantissa bits which gives just over 14 significant decimal digits.

We have used the Cray Fortran compiler version 1.14f with code optimization and vectorization. However, with the exception that up to 8 characters are used for symbol names to enhance readability, the code is written in standard ANSI Fortran 77 and no vectorization specific subroutines or functions are used.

Three CLAMS (Common Los Alamos Mathematics Software) library subroutines are called which are not supplied with the source. Sufficient guidance is given in the documentation here to enable alternatives to be implemented without too much difficulty should this be necessary.

### 6.2 On-line execution

We will assume here and in Sub-section 6.3 that the user is using a Cray computer with CTSS.

The user is supplied with a HISTORIAN PLUS source file called CHARMHIS (this is done so that modifications can be made to the model with a minimum of difficulty - an introduction to HISTORIAN PLUS is given in Section 7). An executable image can be made from CHARMHIS with the following commands:

```
historn(i=charmhis,c=charmft)
cft i=charmft,b=charmldr,maxblock=2560
ldr i=charmldr,x=charm
```

The HISTORIAN PLUS command, HISTORN, causes the HISTORIAN PLUS source file to be translated into a compiler source file CHARMCFT. Next, the Cray Fortran command, CFT, causes CHARMCFT to be translated into a binary relocatable file, CHARMLDR (the MAXBLOCK option sets the maximum code block size for optimization and vectorization). Lastly, the executable image, CHARM, is created from CHARMLDR with the loader command, LDR.

CHARM can be executed by typing the following:

```
charm
```

The default cpu time (1.0) and priority (1.0) are assumed. Alternatively, the following could be entered:

```
charm / t p
```

where t is the cpu time allocation in minutes and p is a priority with value in the range 0.001 to 5.0.

The data file CHARMDAT must be present on the local file area before the image is executed.

Output will appear on the terminal and the file OUT will be created. OUT can be printed, viewed or stored after execution is complete.

### 6.3 Machine resources

We are concerned here with memory requirements and computing time. We emphasize that any particular values we give are specific to the compiler and machine we use. However, the general aspects of this discussion may be more widely useful.

The executable code requires just over 76k decimal words of memory (1 word = 8 bytes). The space needed for variables is dominated by just three arrays which require just over 32k words of memory. Savings can be made by inhibiting vectorization and optimization (at the expense of cpu time) and by reducing the maximum allowed value of n (presently 100) and reducing array dimensions correspondingly.

The cpu time required by the model depends on a number of factors. In general, however, the cpu time will be dominated by one or both the time taken to solve the ODE's and the time taken to update the time-dependent variables.

Clearly, important factors are the problem duration and the stiffness of the ODE's to be solved. High or very transient source mass release rates tend to



cause stiffness. Often, however, these aspects are beyond the control of the user.

Important factors within the control of the user are the accuracy specified for the integration of the ODE's (i.e. the size of  $\epsilon$ ), the number of collocation points, and the precise way the time-dependent variables are to be handled.

The cpu time will increase with decreasing  $\epsilon$  but the strength of the dependence is not immediately apparent. In calculations in which the cpu time was dominated by the integration of the ODE's we have found only modest increases in cpu time e.g. < 40% when  $\epsilon$  was reduced from  $10^{-6}$  to  $10^{-8}$ . This is believed to be due to the use of a high order integration method which is thereby capable of giving significant improvements in accuracy with modest reductions in the integration time step.

The cpu time can be very strongly dependent on the specified number of collocation points. Again, in calculations in which the cpu time was dominated by the integration of the ODE's, we have found the cpu time to depend on  $n$  to a power midway between 2 and 3. This is largely due to the need of the ODE solver to solve an  $n \times n$  system of linear equations for each integration step. We would recommend that a calculation should first be done with  $n$  equal to 10 or so to obtain a base line for the cpu time and to check that the problem has been properly formulated before doing a calculation with a much larger value of  $n$ .

The cpu time can be dominated by the time taken to update the time-dependent variables when they are updated at frequent intervals. An example which illustrates this was considered in detail in Wheatley (1988). In some cases it may be advantageous to update the time-dependent variables continuously (i.e. set THYSTEP equal to zero) rather than have them updated at small time intervals since there is an overhead associated with each time the ODE solver is reset (see the description of CHARM in Appendix B).

Clearly there is a trade-off between accuracy of the results and cpu time which is dictated by the values chosen for  $\epsilon$ ,  $n$  and THYSTEP. Optimum values for these quantities depend on the needs of individual users and may need careful consideration. See the next sub-section also.

#### 6.4 Accuracy

There are three parameters which strongly affect the accuracy of the results. These are  $\epsilon$ ,  $e^b$  (which is related to  $n$ ) and THYSTEP. We assume that  $m_1$  and  $m_2$  are always chosen so that they do not compromise the accuracy (see Sub-section 4.2). The precise way these quantities are related to the accuracy of the

results does not concern us here, instead we consider how the accuracy can be established, which we recommend always should be done.

First, one should decide what the important output quantities are. Often, these are the variables in the mass balance output group which can usually be obtained to given accuracy with less demand on computing resources than the airborne aerosol moments or the airborne aerosol distribution, for example.

Second, one should decide what level of accuracy is required. Often, input data and modelling uncertainties do not warrant high accuracy; 2 or 3 significant figures are usually quite satisfactory. However, higher accuracy may be needed to be sure the calculation is numerically stable and has converged.

The number of accurate significant digits can be established by doing repeat calculations in turn with  $\epsilon$  reduced by a factor of 100,  $e^h$  increased by a factor of 2 and (if appropriate) THYSTEP reduced by a factor of two and in each case establishing how many significant digits in the results remain unchanged when compared with the base calculation. Note that there is little point in choosing THYSTEP much smaller than the minimum time period between consecutive non-equal values of TIMEDATA.

### 6.5 Error messages

Error messages are written on tapes (Fortran unit numbers) 5 and 6. Either they arise from fatal errors, in which case execution of the model stops, or they are warnings arising from errors which may not be serious. The messages on tape 5 may be accompanied by System generated error messages when the model is run under CTSS.

Whenever any of these messages occurs a golden rule is always to first check the input data file for errors. However, should this not prove to cure the problem, in the following we give explanations of what each of the error messages mean and suggest likely causes.

We assume that the user has not modified CHARM. If this is not so and the trouble was not solved with the hints below then the user is advised to carefully check his or her code modifications.

\*\*\* CHARMIN fails: NTIME is le 0 or gt than 20 \*\*\*

Fatal. NTIME is limited by an array dimension to be positive and no greater than 20. Check the input data file!

\*\*\* CHARMIN fails: NDATA is le 0 or gt 20 \*\*\*

Fatal. NDATA is limited by array dimensions to be positive and no greater than 20. Check the input data file!

\*\*\* CHARMIN warning: end-of-file read - could be an error in the data \*\*\*

Non-fatal. If the input data file has been read correctly and is of the right length then CHARMIN should not go on to read the end-of-file marker. Check the input data file!

\*\*\* CHARMIND fails: NONZERO is XXX \*\*\*

Fatal. The number of non-zero production coefficients is limited by an array dimension to 300. The error occurs when the limit is exceeded. This may arise when a large number of collocation points have been specified and/or one of the higher order elements has been chosen. Check the input data file or increase the dimension of the array PIJK in the common block COEF.

\*\*\* CHARMCOE fails: YLOWER is ge YUPPER \*\*\*

Fatal. YLOWER and YUPPER are the lower and upper limits of integration in the integral for the production coefficients. They are chosen so that the integrand is non-zero everywhere between the limits. The indexing calculated in CHARMIND and the logic at the start of CHARMCOE should guarantee that this error never occurs. Non-occurrence of this message provides confidence that this part of the calculation has been done correctly.

\*\*\* CHARMCOE warning: IERROR is -1 \*\*\*

Non-fatal. IERROR is an error flag generated by GAUSS. The value -1 indicates that the lower and upper limits of the integration range are too close to enable the requested tolerance for the integral to be met. This may arise if the mass range of the collocation points is exceedingly large but should not normally occur. Check the input data file! The consequent error in the production coefficient is unlikely to be significant in the subsequent calculations.

\*\*\* CHARMCOE warning: IERROR is 2 \*\*\*

Non-fatal. IERROR is an error flag generated by GAUS8. The value 2 indicates that GAUS8 was unable to calculate the integral to the requested tolerance. Experience has shown this is usually due to the presence of rounding error in the integrand. This may arise if the mass range for the collocation points is exceedingly large but should not normally occur. Check the input data file! The consequent error in the production coefficient is unlikely to be significant in the subsequent calculations.

\*\*\* CHARMFLO fails: IFAIL is 1 \*\*\*

Fatal. IFAIL is an error flag generated by COSWHE. The value 1 means that the function CHARMFAN, for which the location of a zero has been requested, has the same sign at the lower and upper limits of the search range. This should not occur when reasonable values for the equivalent sand roughness, the hydraulic diameter and the flow speed have been chosen. Check the input data file!

\*\*\* CHARMFLO fails: IFAIL is 2 \*\*\*

Fatal. IFAIL is an error flag generated by COSWHE. The value 2 means that COSWHE was unable to locate the zero of CHARMFAN to the specified tolerance after MAXCALLS evaluations of it. Check the tolerance specifications in the input data file!

\*\*\* CHARMDIF fails: LRWORK is too small \*\*\*

Fatal. LRWORK is the dimension of a real work array required by CHARMDIF. This error will not occur unless the user has modified the code to allow the maximum number of collocation points to exceed 100 and failed to increase the dimension of the array RWORK accordingly.

\*\*\* CHARMDIF fails: LIWORK is too small \*\*\*

Fatal. LIWORK is the dimension of an integer work array required by CHARMDIF. This error will not occur unless the user has modified the code to allow the maximum number of collocation points to exceed 100 and failed to increase the dimension of the array IWORK accordingly.

\*\*\* CHARMDIF fails: IDID is -1 \*\*\*

Fatal. IDID is an error flag generated by DEBDF. The value -1 indicates that MAXTRYS times 500 integration steps have been attempted without succeeding in integrating to the time requested of DEBDF. Check that the requested output times are at reasonable intervals. Check the tolerance parameter EPS; it should not be too small. Check the initial and source aerosol distributions, especially the airborne density and the source emission rate. If all these seem reasonable then increase MAXTRYS.

\*\*\* CHARMDIF fails: IDID is -2 \*\*\*

Fatal. IDID is an error flag generated by DEBDF. The value -2 indicates that the error tolerances requested of DEBDF are too stringent. Check the value of EPS specified in the input data file.

\*\*\* CHARMDIF fails: IDID is -3 \*\*\*

Fatal. IDID is an error flag generated by DEBDF. The value -3 indicates that the computed solution has a zero component with a zero component in the absolute error test for that component. This is unlikely to arise but may do so when no airborne and source aerosols exist. Check the input data file!

\*\*\* CHARMDIF fails: IDID is -6 \*\*\*

Fatal. IDID is an error flag generated by DEBDF. The value -6 indicates that DEBDF had repeated convergence test failures on the last attempted step. Check that the problem as specified in the input data file is physically realistic.

\*\*\* CHARMDIF fails: IDID is -7 \*\*\*

Fatal. IDID is an error flag generated by DEBDF. The value -7 indicates that DEBDF had repeated error test failures on the last attempted step. Check that the problem as specified in the input data file is physically realistic.

\*\*\* CHARMDIF fails: IDID is -33 \*\*\*

Fatal. IDID is an error flag generated by DEBDF. The value -33 indicates that DEBDF encountered trouble from which it cannot recover. DEBDF will print a message on tape5 explaining the trouble. It is usually caused by invalid input to DEBDF. This error is not expected to occur unless CHARM has been modified by the user.

\*\*\* CHARMMOM fails: IFAIL is 1 \*\*\*

Fatal. IFAIL is an error flag generated by CO5WHE. The value 1 means that the function CHARMM50, for which the location of a zero has been requested, has the same sign at the lower and upper limits of the search range. This should not normally occur. Check the input data file! The source and initial aerosols may not be physically realistic or the collocation points may have been badly chosen.

\*\*\* CHARMMOM fails: IFAIL is 2 \*\*\*

Fatal. IFAIL is an error flag generated by CO5WHE. The value 2 means that CO5WHE was unable to locate the zero of CHARMM50 to the specified tolerance after MAXCALLS evaluations of it. Check the tolerance specifications in the input data file!

\*\*\* CHARMOU warning: the mass fraction in the top bin is XXX \*\*\*

Non-fatal. This is written when greater than 10% of the airborne aerosol mass is associated with the last collocation point. Check the collocation point specifications and the problem specification in the input data file.

\*\*\* CHARMOU warning: the mass fraction in the bottom bin is XXX \*\*\*

Non-fatal. This is printed when greater than 10% of the airborne aerosol mass is associated with the first collocation point. Check the collocation point specifications and the problem specification in the input data file.

\*\*\* CHARMOU warning: the number fraction in the top bin is XXX \*\*\*

Non-fatal. This is printed when greater than 10% of the airborne particles are associated with the last collocation point. Check the collocation point specifications and the problem specification in the input data file.

\*\*\* CHARMOU warning: the number fraction in the bottom bin is XXX \*\*\*

Non-fatal. This is printed when greater than 10% of the airborne particles are associated with the first collocation point. Check the collocation point specifications and the problem specification in the input data file.

## 7 CODE MODIFICATIONS

### 7.1 Scope

Although CHARM can be applied to a wide range of aerosol problems without modification, we expect situations will arise when the user will find it desirable to make relatively minor modifications to the model to suit his or her specific purposes. The sort of modifications we have in mind are: changes to the physical models for gas and flow properties and agglomeration and deposition rates; adding an output file to interface with graph plotting routines; adding variables to the existing input and output subroutines; replacing the library subroutines GAUSS, SSORT and DEBDF with alternatives; and adding new variables to those treated as time-dependent. Such modifications can be done with little difficulty. We outline here a general approach which we recommend should always be followed and give two examples. The treatment of multicomponent aerosols, condensation and evaporation would require non-trivial extensions to CHARM and considerable development work should an efficient treatment be desired. This is discussed in Section 9.

### 7.2 General method

The general method we advocate is to use a software package such as HISTORIAN PLUS (OPCODE Inc., 1985) or UPDATE (CRAY Research Inc. 1984) which will automatically execute and keep track of changes made to CHARM. Thereby, changes for a single purpose can be kept in a single compact file, revoked at any time to restore the original model and added to others with ease.

You will see from the compiler source listing in Appendix D that each line of code has a label in columns 73-80. These were generated by HISTORIAN PLUS (but are equally compatible with UPDATE). To modify the code, a modification file is made which comprises a sequence of commands (subsequently called directives to conform with HISTORIAN PLUS nomenclature) referring to these labels. HISTORIAN PLUS is then used to execute the directives in conjunction with the HISTORIAN PLUS source file to generate a new compiler source.

A basic list of HISTORIAN PLUS directives is as follows (the corresponding UPDATE directives are similar):

- \*/ Anything following this on the same line is a comment.
- \*insert "label" The lines of Fortran following this directive are inserted after the line in the source labelled with "label".
- \*before "label" The lines of Fortran following this directive are inserted before the line in the source labelled with "label".
- \*delete "label" The line in the source with label "label" is deleted and replaced with the lines of Fortran following this directive.

- \*ident "name" This is required at the start of the modification file. "name" is used to generate labels for the Fortran which is inserted according to the succeeding directives.
- \*call "name" This can appear anywhere in the lines of Fortran which follow the *insert*, *before* and *delete* directives and causes the block of Fortran in the source with labels generated from "name" to be inserted at this point. The block of Fortran must have been identified originally as suitable for copying in this way (i.e. it must have been defined as a "common deck"). All common blocks in the source were generated from "common decks".
- \*read "fname" The sequence of directives in the file "fname" are read.

Details of these and other directives can be found in the reference manual for HISTORIAN PLUS but it is hoped that the above outline and the examples which follow will serve to illustrate the utility of the approach.

### 7.3 Two examples

The first example shows how to obtain values of the dimensionless relaxation time on the output file. This may be desired to determine whether the correlation for turbulent deposition is being used within its range of validity. The HISTORIAN PLUS modification file, USERMOD1, is:

```

*/
*/ Modifications to CHARM to output the dimensionless relaxation time.
*/
*ident relax
*insert agglom.3
      +                ,dimrel(100)
*insert chmdep.77
      dimrel(icoll)=dimrelax
*insert chmout.339
      if(columns.eq. 80)write(ntape6,9056)
      if(columns.eq.132)write(ntape6,8056)
      if(columns.eq. 80)write(ntape6,9003)(i,dimrel(i),i=1,ncoll)
      if(columns.eq.132)write(ntape6,8003)(i,dimrel(i),i=1,ncoll)
*insert chmout.518
9056 format('Dimensionless relaxation times...',/
      +5(4x,' dimrelax '))
*insert chmout.539
8056 format('Dimensionless relaxation times...',/
      +8(4x,' dimrelax '))

```



The first insert directive causes a new array DIMREL to be included in the common block labelled AGGLOM which appears in the subroutines CHARMDEP and CHARMOUT. The succeeding inserts should be relatively straightforward to follow in conjunction with the source listing.

This modification file can be implemented with the following HISTORIAN PLUS commands:

```
historian(i=charmhis,n=charmopl)
historian(i=usermod1,p=charmopl,c=charmcft,f)
```

CHARMHIS is the HISTORIAN PLUS file. The first command creates a binary old-program-library which contains the information HISTORIAN PLUS needs for subsequent modification runs. The second command is a modification run which generates the file CHARMCFT which can be read by a Fortran compiler. f at the end of this command indicates that nothing must be left-out of the CHARMCFT file.

The second example shows how the code can be modified to make the leakage rate a time-dependent variable. The modification file, USERMOD2, is:

```
*/
*/ Modifications to CHARM to enable the leak rate to depend on time.
*/
*ident leakrate
*insert thrmhydr.10
      +                ,lkrta0(20),lkrta1(20),lkrtdata(20)
*insert thrmhydr.11
      +                ,lkrta0,lkrta1,lkrtdata
*delete chmin.119
14   read(ntape4,*,err=14,end=100)volume
34   read(ntape4,*,err=34,end=100)(lkrtdata(idata),idata=1,ndata)
*insert chmblo.81
      data lkrtdata/0.e0,19*-1.e0/
*insert chmith.56
      call charwth(lkrta0,lkrta1,lkrtdata)
*insert chmuth.25
      leakrate = lkrta0(ithhy) + lkrta1(ithhy) * timemean
*delete chmout.267
*insert chmout.272
      write(ntape6,9030)volume,leakrate
```

The first two insert directives add three real arrays, a data array and two interpolation formulae coefficient arrays, to the THRMHYDR common block. The

delete directive which follows causes VOLUME to be read on one line of the data file and the leak rate data to be read on subsequent lines. The next three insert directives result in, in turn, the leak rate data array to be initialized, the coefficients in the interpolation formulae for the leak rate to be calculated from the data and the leak rate to be calculated from the interpolation formulae. The last two directives allow the leak rate to be written on the output file more than once.

This modification file can be implemented in the same way as the first example except that USERMOD1 must be replaced by USERMOD2 in the arguments of the HISTORIAN PLUS commands. Alternatively, the two files USERMOD1 and USERMOD2 can be implemented in conjunction by defining a third file called USERMODS which reads:

```
*read usermod1  
*read usermod2
```

USERMOD1 must now be replaced by USERMODS in the arguments of the HISTORIAN PLUS commands.

## 8 CHARM AS A SUB-MODEL OF A LARGER MODEL

We discuss here some general aspects of how CHARM could be implemented as a sub-model of a larger model. Though some modifications to CHARM would be needed, most of the subroutines would not be affected as a consequence of the modular design of the code. The details, of course, will depend on the particular application.

In general we envisage the subsuming model to be one which calculates at least velocities, pressures and temperatures of the flow and surface temperatures, in each cell of a multicell problem, and convection and possibly mixing of aerosol from cell to cell (the cells could be Eulerian or Lagrangian). In some applications the gas composition may not be constant and we suppose this would also be calculated for the bulk gas and adjacent to walls when a component of the gas is condensing or evaporating there.

The role of CHARM in this general context would be to calculate aerosol behavior within each cell, much as is done now for one cell only. This has to be done explicitly, by which we mean the aerosol equations are solved separately from the equations governing the thermal-hydraulics and aerosol transport during each time step. The problem is therefore seen as two-fold: time step control; and arranging the data interface between CHARM and the subsuming model and input and output.

Without condensation or evaporation of the aerosol, aerosol behavior within a cell will not affect the thermal-hydraulics to any significant extent except possibly in strong thermal radiation fields (of course, the converse is not true). This means the maximum allowable thermal-hydraulic time step need not be reduced as a consequence of the presence of aerosol. Some limit may need to be applied, however, when the thermal-hydraulic conditions change considerably over one time step. There is two way coupling between aerosol behavior within a cell and cell to cell transport of aerosol which could in some cases call for the maximum allowable aerosol transport time step to be reduced. There are no internal constraints on the CHARM time step which is simply chosen to match the subsuming model time step.

Two way coupling can exist between intra-cell aerosol processes and the thermal-hydraulics when condensation and evaporation of the aerosol can occur (Clement, 1984). This can entail severe time step limitations or else require that the split between the thermal-hydraulic calculations and the intra-cell aerosol calculations is modified. Since CHARM in its present version does not treat condensation and evaporation, this need not concern us further here.

We assume the subsuming model is able to supply CHARM with thermal-hydraulic information and an aerosol distribution, derived from the aerosol transport calculations, for each cell corresponding to an instant of time in the problem. We assume also that this data is not conveniently supplied for two instants of problem time simultaneously. This eliminates the possibility of interpolating data in time during the calculations done by CHARM. The subroutines CHARMITH, CHARMWTH, CHARMUTH, CHARMSLN and CHARMZLN are therefore not needed (we suppose the source distribution is to be supplied by the subsuming model) and, during one time step, the agglomeration kernel, deposition and source rates need be calculated only once per cell. The ODE solver in CHARM has to be reinitialized at the start of each time step for each cell. All this means the main program, CHARM, can be considerably simplified.

All the data which depends on cell location and/or time has to be supplied to CHARM at the start of each time step for each cell. This data includes: the thermal-hydraulic data, the cell geometry and associated data such as the surface roughness and leak rate, the aerosol distribution, the source distribution, and the gas composition when it is time-dependent. The aerosol distribution has to be resupplied to the subsuming model at the end of the time step. Small negative components (see Sub-section 3.2) could be set to zero and the distribution renormalized to exactly conserve mass. Deposited and leaked masses and moments of the distribution could also be supplied when these are not to be output by CHARM.

The cell and time-independent data includes: the collocation information and quantities derived from this such as  $P_{jk}^i$  and  $n_{jk}$ , the aerosol physics data and the tolerance data. Input data relevant to this category can be read by CHARM and this category of data can be stored within CHARM. CHARMIN and CHARMBLO can therefore be considerably simplified. The subroutines which calculate the derived data need be called once only.

As noted in Sub-section 6.3, just three arrays make up nearly one half the size of the executable code. It may be important with some machines and depending on the size of the subsuming model to make sure these arrays do not take up more space than needed. This can be done by making the dimensions of these arrays dynamic and having the subsuming model provide space for them.

## 9 EXTENSIONS TO CHARM

### 9.1 Multicomponent aerosols

We discuss what further work needs to be done to enable CHARM to efficiently treat multicomponent aerosols.

When the aerosol has variable composition and is composed of  $s$  components and agglomeration and deposition for particles of given mass can be adequately characterized by their average composition then the aerosol behavior can be characterized by a system of  $s$  coupled integro-differential equations (Simons, 1982). The discretization method described in Section 3 for a single component aerosol is simply generalized to discretize this new system of equations. A system of  $n \times s$  coupled ODE's results. Directly solving this system of equations can pose a problem when the equations are stiff and  $s$  is large since the solution time of stiff ODE solvers is approximately proportional to  $(n \times s)^3$ . For example, Grimley et al. (1988) consider 40 or so components for which the computing time would be increased by a factor of order  $10^4$  over that for a one component aerosol.

An alternative to the direct method of solution is, by exploiting the special structure of the Jacobian, to reduce the equations to a set of  $n$  coupled ODE's to be solved first and  $s-1$  sets of  $n$  coupled linear ODE's whose solution depends on the solution obtained to the first set of ODE's. An example of this approach was considered by Stock et al. (1987) who compared the two methods. However, they considered a two component aerosol only and the discretization method was not the same for the two solution methods. It is therefore unclear from their results which solution method would be most efficient in general.

So, further assessment of the two methods is needed to determine which is optimum. The modifications required of CHARM to treat multicomponent aerosols using either of the two solution methods are believed to be straightforward.

### 9.2 Condensation and evaporation - one species

We now discuss how CHARM could be extended to treat condensation and evaporation of one component onto and from the aerosol.

Extra terms need to be added to the aerosol equations to treat condensation and evaporation. These terms cause the equations to become exceedingly stiff. Considerable progress with this problem has been made recently by Gelbard (1987) who treats an aerosol with one volatile component. His method is to split the problem into two parts and treat each part in separate numerical steps. The first part deals with condensation and evaporation only and is based on the

method of characteristics. Particles of different size are coupled only through mass and energy balances within the volume. The second part deals with agglomeration, deposition and leakage only, as considered in this manual.

It would seem essential to split the problem in this way if a collocation method is used to treat the agglomeration terms since evaporation and condensation introduce into Eq. (1) a term of the form  $\frac{\partial}{\partial m} C(m,t)E(m,t)$ , where  $E(m,t)$  is the particle growth law. This term is ill-defined at the grid points in the collocation method. A finite difference approximation could of course be attempted for these terms but it seems likely that it would lead to poor results when  $e^h$  is large in comparison with unity. In any case, many fixed grid methods introduce artificial spreading of the aerosol distribution when the aerosol is evolving dominantly by condensation and evaporation (Tsang and Brock, 1983) which, as Gelbard points out, is largely overcome with his method of splitting.

### 9.3 Condensation and evaporation - many species

However, further work is required to treat aerosols with more than one volatile component, particularly when chemical reactions in the vapor phase must be taken into account. The problem here is the computational cost involved in maintaining chemical equilibrium in the vapor phase during the condensation and evaporation step.

## 10 CONCLUSIONS

We have described the models in CHARM and given detailed information to enable others to use and modify the code.

We have tried to ensure the code is "bug" free, both by design of the code architecture, transparency of the FORTRAN (we do not claim always to have succeeded in this respect!), and by testing. However, we cannot guarantee that it is free of bugs. Should you find bugs or encounter difficulties associated with the way the code operates, please communicate your findings to the author so that other users may enjoy the benefits.

We would also be happy to receive details of applications or developments you make of CHARM. Indeed, we hope Section 2 makes clear that there is considerable scope for developing the models for the gas and flow properties, and agglomeration and deposition.

Despite the lengthy details about CHARM included here, we do not wish to leave the impression that the code is difficult to use or modify. On the contrary, we have gone to some length in the design of the code to ensure the opposite. Try it!

We believe that the code can form the basis of extensions to treat multicomponent aerosols, condensation and evaporation as was discussed in section 9. However, further development and testing of methods is needed should a computationally efficient model be desired.

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## APPENDIX A - THE EXAMPLE OUTPUT DATA FILES

We list here the output files obtained from the example input data file shown in Sub-section 4.4. We have removed the copies of the input data file from both output files. These output files are discussed in Sub-section 5.3.

The first file was written on the terminal. Following this you would also see:

```
charm    ctss time    3.356 seconds
cpu=     3.003 i/o=   .245 mem=     .109
```

The second file is the main output file, OUT.

The file written on the terminal

---

step no. =	0	time =	0.0000e+00	mass check =	0.0000e+00
step no. =	1	time =	3.0000e+02	mass check =	-6.3442e-08
step no. =	2	time =	6.0000e+02	mass check =	-7.1820e-08
step no. =	3	time =	9.0000e+02	mass check =	-3.5321e-07
step no. =	4	time =	1.2000e+03	mass check =	-3.5668e-07
step no. =	5	time =	1.5000e+03	mass check =	-3.6546e-07
step no. =	6	time =	1.8000e+03	mass check =	-3.7419e-07
step no. =	7	time =	2.1000e+03	mass check =	-3.2025e-07
step no. =	8	time =	2.4000e+03	mass check =	-1.1730e-07
step no. =	9	time =	2.7000e+03	mass check =	-3.6089e-06
step no. =	10	time =	3.0000e+03	mass check =	-3.6441e-06
step no. =	11	time =	3.3000e+03	mass check =	-3.8971e-06
step no. =	12	time =	3.6000e+03	mass check =	-3.8432e-06
step no. =	13	time =	7.2000e+03	mass check =	-3.1102e-05
step no. =	14	time =	1.0800e+04	mass check =	5.0609e-05
step no. =	15	time =	1.4400e+04	mass check =	4.7371e-05
step no. =	16	time =	1.8000e+04	mass check =	4.8542e-05
step no. =	17	time =	2.1600e+04	mass check =	4.5610e-05
step no. =	18	time =	2.5200e+04	mass check =	4.5708e-05
step no. =	19	time =	2.8800e+04	mass check =	4.7011e-05
step no. =	20	time =	3.2400e+04	mass check =	4.7252e-05
step no. =	21	time =	3.6000e+04	mass check =	4.6496e-05
step no. =	22	time =	3.6300e+04	mass check =	4.1648e-05
step no. =	23	time =	3.6600e+04	mass check =	4.1020e-05
step no. =	24	time =	3.6900e+04	mass check =	4.0848e-05
step no. =	25	time =	3.7200e+04	mass check =	4.1042e-05
step no. =	26	time =	3.7500e+04	mass check =	4.1395e-05
step no. =	27	time =	3.7800e+04	mass check =	4.2287e-05
step no. =	28	time =	4.1400e+04	mass check =	4.5807e-05
step no. =	29	time =	4.5000e+04	mass check =	4.5840e-05
step no. =	30	time =	4.8600e+04	mass check =	4.5914e-05
step no. =	31	time =	5.2200e+04	mass check =	4.6001e-05
step no. =	32	time =	5.5800e+04	mass check =	4.5963e-05
step no. =	33	time =	5.9400e+04	mass check =	4.5963e-05
step no. =	34	time =	6.3000e+04	mass check =	4.5646e-05
step no. =	35	time =	6.6600e+04	mass check =	4.6273e-05
step no. =	36	time =	7.0200e+04	mass check =	4.6034e-05
step no. =	37	time =	7.3800e+04	mass check =	4.5466e-05
step no. =	38	time =	7.7400e+04	mass check =	4.5340e-05
step no. =	39	time =	8.1000e+04	mass check =	4.5453e-05
step no. =	40	time =	8.4600e+04	mass check =	4.5437e-05
step no. =	41	time =	8.8200e+04	mass check =	4.5415e-05
step no. =	42	time =	9.1800e+04	mass check =	4.5375e-05
step no. =	43	time =	9.5400e+04	mass check =	4.5587e-05
step no. =	44	time =	9.9000e+04	mass check =	4.5619e-05
step no. =	45	time =	1.0260e+05	mass check =	4.5690e-05
step no. =	46	time =	1.0620e+05	mass check =	4.5870e-05
step no. =	47	time =	1.0980e+05	mass check =	4.5813e-05
step no. =	48	time =	1.1340e+05	mass check =	4.5813e-05
step no. =	49	time =	1.1700e+05	mass check =	4.5813e-05
step no. =	50	time =	1.2060e+05	mass check =	4.5813e-05
step no. =	51	time =	1.2240e+05	mass check =	4.5814e-05

---

The main output file, OUT

```

.....
*****
step no. = 0   time = 0.0000e+00   mass check = 0.0000e+00
*****

Mass budget...
air-borne   flor dep.   wall dep.   clng dep.   source   leaked
0.0000e+00  0.0000e+00  0.0000e+00  0.0000e+00  0.0000e+00  0.0000e+00
Airborne aerosol moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
0.0000e+00  0.0000e+00  0.0000e+00  0.0000e+00  0.0000e+00  0.0000e+00
Source moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
2.0000e+00  5.0000e-07  3.0884e-06  1.8292e+10  1.9419e-17  1.4661e-15
Airborne mass distribution...
m-distr   m-distr   m-distr   m-distr   m-distr   m-distr
1 0.0000e+00  2 0.0000e+00  3 0.0000e+00  4 0.0000e+00  5 0.0000e+00
6 0.0000e+00  7 0.0000e+00  8 0.0000e+00  9 0.0000e+00  10 0.0000e+00
11 0.0000e+00  12 0.0000e+00  13 0.0000e+00
Airborne number distribution...
n-distr   n-distr   n-distr   n-distr   n-distr   n-distr
1 0.0000e+00  2 0.0000e+00  3 0.0000e+00  4 0.0000e+00  5 0.0000e+00
6 0.0000e+00  7 0.0000e+00  8 0.0000e+00  9 0.0000e+00  10 0.0000e+00
11 0.0000e+00  12 0.0000e+00  13 0.0000e+00
Source mass distribution...
m-distr   m-distr   m-distr   m-distr   m-distr   m-distr
1 3.3845e-15  2 1.6832e-12  3 2.4563e-10  4 1.0518e-08  5 1.3215e-07
6 4.8719e-07  7 5.2702e-07  8 1.6728e-07  9 1.5580e-08  10 4.2580e-10
11 3.4145e-12  12 8.0341e-15  13 5.5459e-18
Source number distribution...
n-distr   n-distr   n-distr   n-distr   n-distr   n-distr
1 8.4611e-05  2 4.2080e+07  3 6.1407e+08  4 2.6294e+09  5 3.3037e+09
6 1.2180e+09  7 1.3178e+08  8 4.1821e+06  9 3.8951e+04  10 1.0645e+02
11 8.5361e-02  12 2.0085e-05  13 1.3867e-09
Collocation information...
nelement  ncoll      hwidth\      spacing      range
2          13         1.0000e+00  1.0000e+01  1.0000e+12
Indexing for production coefficients...
jbar   kbarmin  kbarmax  nkbar   index   jbar   kbarmin  kbarmax  nkbar   index
0      0         12       13      1       1       0         12       13      14
2      0         1        2       27      3       0         1        2       29
4      0         1        2       31      5       0         1        2       33
6      0         1        2       35      7       0         1        2       37
8      0         1        2       39      9       0         1        2       41
10     0         1        2       43     11     0         1        2       45
12     0         1        2       47
Production coefficients in indexing order...
pijk   pijk   pijk   pijk   pijk   pijk   pijk
2.9905e-01  1.8370e-01  1.5547e-02  1.5304e-03  1.5280e-04  1.5278e-05
1.5278e-06  1.5278e-07  1.5278e-08  1.5278e-09  1.5278e-10  1.5278e-11
1.5278e-12  9.1753e-01  8.2254e-02  2.1534e-04  2.0208e-06  2.0084e-08
2.0072e-10  2.0071e-12  2.0071e-14  2.0071e-16  2.0071e-18  2.0071e-20
2.0071e-22  2.0071e-24  9.9326e-01  6.7385e-03  9.9934e-01  6.6450e-04
9.9993e-01  6.6350e-05  9.9999e-01  6.6351e-06  1.0000e+00  6.6350e-07
1.0000e+00  6.6350e-08  1.0000e+00  6.6350e-09  1.0000e+00  6.6350e-10
1.0000e+00  6.6350e-11  1.0000e+00  6.6350e-12  1.0000e+00  6.6350e-13
Normalization factors...
nj      nj      nj      nj      nj      nj
1 8.9159e-01  2 9.3955e-01  3 9.9461e-01  4 9.9947e-01  5 9.9995e-01
6 9.9999e-01  7 1.0000e+00  8 1.0000e+00  9 1.0000e+00  10 1.0000e+00
11 1.0000e+00  12 1.0000e+00  13 1.0000e+00
1 9.3955e-01  2 8.9159e-01  3 9.9955e-01  4 9.9461e-01  5 9.9947e-01
6 9.9995e-01  7 9.9999e-01  8 1.0000e+00  9 1.0000e+00  10 1.0000e+00
11 1.0000e+00  12 1.0000e+00  13 1.0000e+00

```

1	9.9481e-01	2	9.3955e-01	3	8.9159e-01	4	9.3955e-01	5	9.9481e-01
6	9.9947e-01	7	9.9995e-01	8	9.9999e-01	9	1.0000e+00	10	1.0000e+00
11	1.0000e+00	12	1.0000e+00	13	1.0000e+00				
1	9.9947e-01	2	9.9481e-01	3	9.3955e-01	4	8.9159e-01	5	9.3955e-01
6	9.9481e-01	7	9.9947e-01	8	9.9995e-01	9	9.9999e-01	10	1.0000e+00
11	1.0000e+00	12	1.0000e+00	13	1.0000e+00				
1	9.9995e-01	2	9.9947e-01	3	9.9481e-01	4	9.3955e-01	5	8.9159e-01
6	9.3955e-01	7	9.9481e-01	8	9.9947e-01	9	9.9995e-01	10	9.9999e-01
11	1.0000e+00	12	1.0000e+00	13	1.0000e+00				
1	9.9999e-01	2	9.9995e-01	3	9.9947e-01	4	9.9481e-01	5	9.3955e-01
6	8.9159e-01	7	9.3955e-01	8	9.9481e-01	9	9.9947e-01	10	9.9995e-01
11	9.9999e-01	12	1.0000e+00	13	1.0000e+00				
1	1.0000e+00	2	9.9999e-01	3	9.9995e-01	4	9.9947e-01	5	9.9481e-01
6	9.3955e-01	7	8.9159e-01	8	9.3955e-01	9	9.9481e-01	10	9.9947e-01
11	9.9995e-01	12	9.9999e-01	13	1.0000e+00				
1	1.0000e+00	2	1.0000e+00	3	9.9999e-01	4	9.9995e-01	5	9.9947e-01
6	9.9481e-01	7	9.3955e-01	8	8.9159e-01	9	9.3955e-01	10	9.9481e-01
11	9.9947e-01	12	9.9995e-01	13	1.0000e+00				
1	1.0000e+00	2	1.0000e+00	3	1.0000e+00	4	9.9999e-01	5	9.9995e-01
6	9.9947e-01	7	9.9481e-01	8	9.3955e-01	9	8.9159e-01	10	9.3955e-01
11	9.9481e-01	12	9.9947e-01	13	1.0000e+00				
1	1.0000e+00	2	1.0000e+00	3	1.0000e+00	4	1.0000e+00	5	9.9999e-01
6	9.9995e-01	7	9.9947e-01	8	9.9481e-01	9	9.3955e-01	10	8.9159e-01
11	9.3955e-01	12	9.9481e-01	13	1.0000e+00				
1	1.0000e+00	2	1.0000e+00	3	1.0000e+00	4	1.0000e+00	5	1.0000e+00
6	9.9999e-01	7	9.9995e-01	8	9.9947e-01	9	9.9481e-01	10	9.3955e-01
11	8.9159e-01	12	9.3955e-01	13	1.0012e+00				
1	1.0000e+00	2	1.0000e+00	3	1.0000e+00	4	1.0000e+00	5	1.0000e+00
6	1.0000e+00	7	9.9999e-01	8	9.9995e-01	9	9.9947e-01	10	9.9481e-01
11	9.3955e-01	12	8.9159e-01	13	9.9888e-01				
1	1.0000e+00	2	1.0000e+00	3	1.0000e+00	4	1.0000e+00	5	1.0000e+00
6	1.0000e+00	7	1.0000e+00	8	1.0000e+00	9	1.0000e+00	10	1.0000e+00
11	1.0012e+00	12	9.9888e-01	13	3.3439e+00				

Collocation points...

	mass		mass		mass		mass		mass
1	4.0000e-21	2	4.0000e-20	3	4.0000e-19	4	4.0000e-18	5	4.0000e-17
6	4.0000e-16	7	4.0000e-15	8	4.0000e-14	9	4.0000e-13	10	4.0000e-12
11	4.0000e-11	12	4.0000e-10	13	4.0000e-09				

Radii at the collocation points...

	radius		radius		radius		radius		radius
1	6.9867e-09	2	1.5052e-08	3	3.2429e-08	4	6.9867e-08	5	1.5052e-07
6	3.2429e-07	7	6.9867e-07	8	1.5052e-06	9	3.2429e-05	10	6.9867e-05
11	1.5052e-05	12	3.2429e-05	13	6.9867e-05				

Tolerance information...

	eps	ets	zeta	maxcalls	maxtrys
	1.0000e-06	0.0000e+00	5.0000e-01	30	10

Aerosol physics data...

cshepfctr =	1.5000e+00	dshpfctr =	1.5000e+00	stickeff =	1.0000e+00
aknudweb =	1.3700e+00	qknudweb =	4.0000e-01	bknudweb =	1.1000e+00
pdensity =	2.8000e+03	pthrwall =	6.3750e-01		
kbrock =	1.0000e+00	cmbrock =	1.3700e+00	ctbrock =	1.0000e+00

Cell data...

volume =	1.8000e+05	leakrate =	1.1574e-07		
hyrdiam =	0.0000e+00	eqvrough =	4.5000e-05		
areacng =	0.0000e+00	areawall =	2.0000e+04	areaflo =	2.8000e+03
tempcng =	3.6315e+02	tempwall =	3.6315e+02	tempflo =	3.6315e+02

Gas data...

temp =	3.7315e+02	press =	1.0000e+05	velocity =	0.0000e+00
gdensity =	9.3345e-01	dynvisc =	2.1688e-05	mfpath =	8.8969e-08
solwt =	2.8980e+01	gthracon =	2.8500e-02		
solwtv =	1.8015e+01	diffusv =	3.9159e-05		
vmfrclng =	0.0000e+00	vmfrwall =	0.0000e+00	vmfrflo =	0.0000e+00
vcgrclng =	0.0000e+00	vcgrwall =	0.0000e+00	vcgrflo =	0.0000e+00
vconclng =	0.0000e+00	vconwall =	0.0000e+00	vconflo =	0.0000e+00

Flow data...

eddydiss =	0.0000e+00	ustar =	0.0000e+00	vbthick =	1.0000e-03
------------	------------	---------	------------	-----------	------------

Diffusion boundary layer thickness...

	dblthick		dblthick		dblthick		dblthick		dblthick
1	1.0000e-04	2	1.0000e-04	3	1.0000e-04	4	1.0000e-04	5	1.0000e-04

8	1.0000e-04	7	1.0000e-04	8	1.0000e-04	9	1.0000e-04	10	1.0000e-04
11	1.0000e-04	12	1.0000e-04	13	1.0000e-04				
Mobilities at the collocation points...									
	mobility		mobility		mobility		mobility		mobility
1	5.3955e+12	2	1.1983e+12	3	2.7624e+11	4	6.9072e+10	5	2.0005e+10
8	5.9286e+09	7	2.7413e+09	8	1.1711e+09	9	5.2176e+08	10	2.3748e+08
11	1.0021e+08	12	5.0475e+07	13	2.3381e+07				
Rate of deposition onto floors...									
	dep.rate		dep.rate		dep.rate		dep.rate		dep.rate
1	2.2801e-06	2	2.0180e-06	3	1.8672e-06	4	1.7106e-06	5	1.6780e-06
8	1.6339e-06	7	2.6097e-06	8	7.8452e-08	9	3.2385e-05	10	1.4540e-04
11	6.8705e-04	12	3.0814e-03	13	1.4272e-02				
Rate of deposition onto walls...									
	dep.rate		dep.rate		dep.rate		dep.rate		dep.rate
1	1.6263e-05	2	1.4362e-05	3	1.3217e-05	4	1.1917e-05	5	1.0399e-05
8	8.6500e-06	7	6.8885e-06	8	4.9772e-06	9	3.8335e-06	10	3.1910e-06
11	2.8632e-06	12	2.7041e-06	13	2.6286e-06				
Rate of deposition onto ceilings...									
	dep.rate		dep.rate		dep.rate		dep.rate		dep.rate
1	0.0000e+00	2	0.0000e+00	3	0.0000e+00	4	0.0000e+00	5	0.0000e+00
8	0.0000e+00	7	0.0000e+00	8	0.0000e+00	9	0.0000e+00	10	0.0000e+00
11	0.0000e+00	12	0.0000e+00	13	0.0000e+00				
Agglomeration kernel...									
	agg.rate		agg.rate		agg.rate		agg.rate		agg.rate
1	8.2218e-15	2	1.2023e-14	3	2.3269e-14	4	4.5735e-14	5	9.0165e-14
8	1.8255e-13	7	3.7960e-13	8	8.0311e-13	9	1.7150e-12	10	3.6791e-12
11	7.9097e-12	12	1.7022e-11	13	3.6651e-11				
1	1.2023e-14	2	6.8148e-15	3	7.2192e-15	4	1.1199e-14	5	2.0530e-14
8	4.0800e-14	7	8.4476e-14	8	1.7854e-13	9	3.8115e-13	10	8.1750e-13
11	1.7573e-12	12	3.7815e-12	13	8.1423e-12				
1	2.3269e-14	2	7.2192e-15	3	3.6009e-15	4	3.5472e-15	5	5.3991e-15
8	9.9687e-15	7	2.0005e-14	8	4.1693e-14	9	8.8434e-14	10	1.8913e-13
11	4.0617e-13	12	8.7450e-13	13	1.8875e-12				
1	4.5735e-14	2	1.1199e-14	3	3.5472e-15	4	1.9052e-15	5	1.9339e-15
8	2.9442e-15	7	5.4100e-15	8	1.0832e-14	9	2.2591e-14	10	4.8124e-14
11	1.0403e-13	12	2.2874e-13	13	5.1725e-13				
1	9.0165e-14	2	2.0530e-14	3	5.3991e-15	4	1.9339e-15	5	1.1781e-15
8	1.2555e-15	7	1.9127e-15	8	3.5323e-15	9	7.2827e-15	10	1.6310e-14
11	4.0054e-14	12	1.1113e-13	13	3.5673e-13				
1	1.8255e-13	2	4.0800e-14	3	9.9687e-15	4	2.9442e-15	5	1.2555e-15
8	8.7596e-16	7	1.0543e-15	8	1.9276e-15	9	4.8434e-15	10	1.5463e-14
11	5.8208e-14	12	2.4305e-13	13	1.0705e-12				
1	3.7960e-13	2	8.4476e-14	3	2.0005e-14	4	5.4100e-15	5	1.9127e-15
8	1.0543e-15	7	7.4551e-16	8	2.6613e-15	9	1.1293e-14	10	4.9902e-14
11	2.2562e-13	12	1.0335e-12	13	4.7670e-12				
1	8.0311e-13	2	1.7854e-13	3	4.1693e-14	4	1.0832e-14	5	3.5323e-15
8	1.9276e-15	7	2.6613e-15	8	6.8561e-16	9	3.8927e-14	10	2.1399e-13
11	1.0206e-12	12	4.7511e-12	13	2.2038e-11				
1	1.7150e-12	2	8.8116e-13	3	8.8434e-14	4	2.2591e-14	5	7.2827e-15
8	4.8434e-15	7	1.1293e-14	8	3.8927e-14	9	6.5779e-16	10	8.1155e-13
11	4.5515e-12	12	2.1859e-11	13	7.0208e-10				
1	3.6791e-12	2	8.1750e-13	3	1.8913e-13	4	4.8124e-14	5	1.6310e-14
8	1.5463e-14	7	4.9902e-14	8	2.1399e-13	9	8.1155e-13	10	6.4483e-16
11	1.7358e-11	12	9.7689e-11	13	4.7004e-10				
1	7.9097e-12	2	1.7573e-12	3	4.0617e-13	4	1.0403e-13	5	4.0054e-14
8	5.8288e-14	7	2.2562e-13	8	1.0206e-12	9	4.5515e-12	10	1.7258e-11
11	6.3878e-16	12	3.7286e-10	13	2.1011e-09				
1	1.7022e-11	2	3.7815e-12	3	8.7450e-13	4	2.2874e-13	5	1.1113e-13
8	2.4305e-13	7	1.0335e-12	8	4.7511e-12	9	2.1859e-11	10	9.7689e-11
11	3.7286e-10	12	6.3595e-16	13	8.0220e-09				
1	3.6651e-11	2	8.1423e-12	3	1.8875e-12	4	5.1725e-13	5	3.5673e-13
8	1.0705e-12	7	4.7670e-12	8	2.2038e-11	9	1.0206e-10	10	4.7004e-10
11	2.1011e-09	12	8.0220e-09	13	6.3462e-16				

\*\*\*\*\*  
 step no. = 1 time = 3.0000e+02 mass check = -6.3442e-08  
 \*\*\*\*\*

```

Mass budget...
air-borne   flor dep.   wall dep.   clng dep.   source      leaked
1.8640e+02  8.0880e-02  1.8715e-01  0.0000e+00  1.8667e+02  2.8904e-03
Airborne aerosol moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
1.8640e+00  5.2914e-07  9.2442e-04  3.6018e+12  4.0855e-17  1.7378e-15
Source moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
2.0000e+00  5.0000e-07  3.0864e-06  1.8292e+10  1.9419e-17  1.4661e-15

```

```

.....
step no. = 2   time = 8.0000e+02   mass check = -7.1820e-08
.....

```

```

Mass budget...
air-borne   flor dep.   wall dep.   clng dep.   source      leaked
3.3225e+02  3.3359e-01  7.3329e-01  0.0000e+00  3.3333e+02  1.1549e-02
Airborne aerosol moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
1.8661e+00  5.9020e-07  1.8459e-03  4.3885e+12  7.5102e-17  2.4113e-15
Source moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
2.0000e+00  5.0000e-07  3.0864e-06  1.8292e+10  1.9419e-17  1.4661e-15

```

```

.....
step no. = 3   time = 9.0000e+02   mass check = -3.5321e-07
.....

```

```

Mass budget...
air-borne   flor dep.   wall dep.   clng dep.   source      leaked
4.9757e+02  7.8986e-01  6.113e-00  0.0000e+00  5.0000e+02  2.5957e-02
Airborne aerosol moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
1.9089e+00  6.5451e-07  2.7643e-03  4.5489e+12  1.0506e-16  3.2884e-15
Source moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
2.0000e+00  5.0000e-07  3.0864e-06  1.8292e+10  1.9419e-17  1.4661e-15
Airborne mass distribution...
m-distr      m-distr      m-distr      m-distr      m-distr
1  5.1273e-15  2  1.1346e-11  3  6.6519e-09  4  9.3500e-07  5  3.1827e-05
6  3.0701e-04  7  6.2499e-04  8  2.1562e-04  9  1.9452e-05  10  6.6626e-07
11  7.2226e-09  12  1.8851e-11  13  8.3635e-15
Airborne number distribution...
n-distr      n-distr      n-distr      n-distr      n-distr
1  1.2818e+08  2  2.8368e+08  3  1.6630e+10  4  2.3375e+11  5  7.9567e+11
6  7.6753e+11  7  1.5625e+11  8  5.3905e+09  9  4.8631e+07  10  1.6656e+05
11  1.8056e+02  12  4.7127e-02  13  2.0909e-06

```

```

.....
step no. = 4   time = 1.2000e+03   mass check = -3.5668e-07
.....

```

```

Mass budget...
air-borne   flor dep.   wall dep.   clng dep.   source      leaked
6.6232e+02  1.4992e+00  2.7971e+00  0.0000e+00  6.6667e+02  4.6096e-02
Airborne aerosol moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
1.9535e+00  7.1154e-07  3.6796e-03  4.5703e+12  1.2822e-16  4.2251e-15
Source moments...
sigma      rad50      mdensity   ndensity   geommean   mass50
2.0000e+00  5.0000e-07  3.0864e-06  1.8292e+10  1.9419e-17  1.4661e-15

```

.....  
.....  
step no. = 5 time = 1.5000e+03 mass check = -3.5546e-07  
.....

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
8.2646e-02	2.5319e+00	4.2708e-00	0.0000e+00	8.3333e+02	7.1945e-02
Airborne aerosol moments...					
sigma	rad50	mdensity	ndensity	geommean	mass50
1.9988e-00	7.6952e-07	4.5914e-03	4.5540e+12	1.4571e-16	5.3445e-15
Source moments...					
sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e-00	5.0000e-07	3.0864e-06	1.8292e+10	1.9419e-17	1.4661e-15

.....  
.....  
step no. = 6 time = 1.8000e+03 mass check = -3.7419e-07  
.....

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
9.8990e-02	3.9848e+00	6.0153e-00	0.0000e+00	1.0000e+03	1.0348e-01
Airborne aerosol moments...					
sigma	rad50	mdensity	ndensity	geommean	mass50
2.0343e-00	8.3527e-07	5.4994e-03	4.5289e+12	1.5884e-16	6.8347e-15
Source moments...					
sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e-00	5.0000e-07	3.0864e-06	1.8292e+10	1.9419e-17	1.4661e-15
Airborne mass distribution...					
m-distr	m-distr	m-distr	m-distr	m-distr	m-distr
1 3.8118e-15	2 9.6511e-12	3 5.7070e-09	4 8.1363e-07	5 2.7037e-05	6 3.0151e-04
7 1.1954e-03	8 7.5284e-04	9 9.3264e-05	10 6.3285e-06	11 1.7402e-07	12 1.3540e-09
13 1.9548e-12	Airborne number distribution...				
n-distr	n-distr	n-distr	n-distr	n-distr	n-distr
1 9.5289e-05	2 2.4128e-08	3 1.4267e-10	4 2.0341e-11	5 6.7592e-11	6 7.5378e-11
7 2.9910e-11	8 1.9071e-10	9 2.3316e-08	10 1.5821e-06	11 4.3504e-03	12 3.3851e-00
13 4.8870e-04					

.....  
.....  
step no. = 7 time = 2.1000e+03 mass check = -3.2025e-07  
.....

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
1.1525e-03	5.9927e+00	8.0150e-00	0.0000e+00	1.1667e-03	1.4088e-01
Airborne aerosol moments...					
sigma	rad50	mdensity	ndensity	geommean	mass50
2.0655e-00	9.1087e-07	6.4029e-03	4.4977e+12	1.6848e-16	8.8639e-15
Source moments...					
sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e-00	5.0000e-07	3.0864e-06	1.8292e+10	1.9419e-17	1.4661e-15

.....  
.....  
step no. = 8 time = 2.4000e+03 mass check = -1.1730e-07  
.....

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
1.3141e-03	8.7487e+00	1.0285e-01	0.0000e+00	1.3333e+03	1.8351e-01
Airborne aerosol moments...					
sigma	rad50	mdensity	ndensity	geommean	mass50



```

2.0910e+00  9.9484e-07  7.3008e-03  4.4696e-12  1.7523e-16  1.1548e-14
Source moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.0000e+00  5.0000e-07  3.0864e-06  1.8292e-10  1.9419e-17  1.4551e-15

```

```

.....
step no. = 9   time = 2.7000e+03   mass check = 3.8089e-06
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  cing dep.  source  leaked
1.4745e+03  1.2539e+01  1.2723e+01  0.0000e+00  1.5000e+03  2.3192e+01
Airborne aerosol moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.1113e+00  1.0831e-06  8.1917e-03  4.4438e-12  1.7960e-16  1.4902e-14
Source moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.0000e+00  5.0000e-07  3.0864e-06  1.8292e-10  1.9419e-17  1.4661e-15
Airborne mass distribution...
  m-distr          m-distr          m-distr          m-distr          m-distr
1 3.9987e-15  2 9.1927e-12  3 5.4551e-09  4 7.8430e-07  5 2.6150e-05
6 2.7587e-04  7 1.3492e-03  8 1.5376e-03  9 3.1734e-04  10 4.7160e-05
11 3.3584e-06  12 7.4937e-08  13 3.1724e-10
Airborne number distribution...
  n-distr          n-distr          n-distr          n-distr          n-distr
1 9.9918e-05  2 2.2982e-08  3 1.3638e-10  4 1.9608e+11  5 6.5376e+11
6 6.8986e-11  7 3.3731e-11  8 3.8441e-10  9 7.9335e+08  10 1.1790e+07
11 8.3959e-04  12 1.8734e-02  13 7.9309e-02

```

```

.....
step no. = 10   time = 3.0000e+03   mass check = -3.6441e-06
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  cing dep.  source  leaked
1.6332e+03  1.7802e+01  1.5404e+01  0.0000e+00  1.6667e+03  2.8588e+01
Airborne aerosol moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.1271e+00  1.1716e-06  9.0732e-03  4.4708e-12  1.8205e-16  1.7961e-14
Source moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.0000e+00  5.0000e-07  3.0864e-06  1.8292e+10  1.9419e-17  1.4661e-15

```

```

.....
step no. = 11   time = 3.3000e+03   mass check = -3.8971e-06
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  cing dep.  source  leaked
1.7895e+03  2.5216e+01  1.8236e+01  0.0000e+00  1.8333e+03  3.4531e+01
Airborne aerosol moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.1390e+00  1.2583e-06  9.9416e-03  4.4010e-12  1.8299e-16  2.3369e-14
Source moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.0000e+00  5.0000e-07  3.0864e-06  1.8292e-10  1.9419e-17  1.4661e-15

```

```

.....
step no. = 12   time = 3.6000e+03   mass check = -3.8432e-06
.....

```

```

Mass budget...
  air-borne   flor dep.   wall dep.   clog dep.   source      leaked
1.9424e+03   3.5838e-01   2.1354e+01   0.0000e+00   2.0000e+03   4.1011e-01
Airborne aerosol moments...
  sigma      rad50      mdensity    ndensity    geommean    mass50
2.1473e+00   1.3438e-08   1.0791e-02   4.3845e+12   1.8276e-16   2.8451e-14
Source moments...
  sigma      rad50      mdensity    ndensity    geommean    mass50
2.0000e+00   5.0000e-07   3.0864e-06   1.8292e+10   1.9419e-17   1.4661e-15
Airborne mass distribution...
  m-distr    m-distr    m-distr    m-distr    m-distr
1  6.8464e-15  2  9.0981e-12  3  5.4043e-09  4  7.7890e-07  5  2.6041e-05
6  2.8713e-04  7  1.2857e-03  8  2.1426e-03  9  7.2295e-04  10 2.0860e-04
11 3.2863e-05  12 1.9091e-06  13 2.3576e-08
Airborne number distribution...
  n-distr    n-distr    n-distr    n-distr    n-distr
1  1.7116e+08  2  2.2745e+08  3  1.3511e+10  4  1.9472e+11  5  6.5103e+11
6  6.6782e-11  7  3.2142e+11  8  5.3561e+10  9  1.8074e+09  10 5.1849e+07
11 8.2158e-05  12 4.7728e+03  13 5.8941e+00

```

```

.....
step no. = 13   time = 7.2000e+03   mass check = -3.1102e-05
.....

```

```

Mass budget...
  air-borne   flor dep.   wall dep.   clog dep.   source      leaked
2.5552e+03   1.3783e+03   6.5045e+01   0.0000e+00   4.0000e+03   1.4441e+00
Airborne aerosol moments...
  sigma      rad50      mdensity    ndensity    geommean    mass50
2.1272e+00   1.9890e-08   1.4196e-02   4.3777e+12   1.7032e-16   8.9533e-14
Source moments...
  sigma      rad50      mdensity    ndensity    geommean    mass50
2.0000e+00   5.0000e-07   3.0864e-06   1.8292e+10   1.9419e-17   1.4661e-15

```

```

.....
step no. = 14   time = 1.0800e+04   mass check = 5.0609e-05
.....

```

```

Mass budget...
  air-borne   flor dep.   wall dep.   clog dep.   source      leaked
2.5168e+03   3.3722e+03   1.0845e+02   0.0000e+00   8.0000e+03   2.4908e+00
Airborne aerosol moments...
  sigma      rad50      mdensity    ndensity    geommean    mass50
2.1305e+00   1.8995e-08   1.3982e-02   4.3757e+12   1.7167e-16   8.0385e-14
Source moments...
  sigma      rad50      mdensity    ndensity    geommean    mass50
2.0000e+00   5.0000e-07   3.0864e-06   1.8292e+10   1.9419e-17   1.4661e-15

```

```

.....
step no. = 15   time = 1.4400e+04   mass check = 4.7371e-05
.....

```

```

Mass budget...
  air-borne   flor dep.   wall dep.   clog dep.   source      leaked
2.5167e+03   5.3278e+03   1.5197e+02   0.0000e+00   8.0000e+03   3.5397e+00
Airborne aerosol moments...
  sigma      rad50      mdensity    ndensity    geommean    mass50
2.1303e+00   1.9043e-08   1.3981e-02   4.3762e+12   1.7159e-16   8.0989e-14
Source moments...
  sigma      rad50      mdensity    ndensity    geommean    mass50
2.0000e+00   5.0000e-07   3.0864e-06   1.8292e+10   1.9419e-17   1.4661e-15
Airborne mass distribution...
  m-distr    m-distr    m-distr    m-distr    m-distr

```

1	4.1983e-15	2	9.3044e-12	3	5.5188e-09	4	7.9266e-07	5	2.6447e-05
6	2.7280e-04	7	1.1694e-03	8	1.9934e-03	9	1.1238e-03	10	7.2144e-04
11	5.7546e-04	12	1.7187e-04	13	1.6656e-05				

Airborne number distribution...

	n-distr		n-distr		n-distr		n-distr		n-distr
1	1.0498e+06	2	2.3261e+08	3	1.3797e+10	4	1.9816e+11	5	6.6118e+11
6	6.8199e+11	7	2.9235e+11	8	4.9835e+10	9	2.8096e+09	10	1.8036e+08
11	1.4388e+07	12	4.2967e+05	13	4.1640e+03				

step no. = 16 time = 1.8000e+04 mass check = 4.8542e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.5164e+03	7.2835e+03	1.9547e+02	0.0000e+00	1.0000e+04	4.6883e+00

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.1303e+00	1.9040e-06	1.3980e-02	4.3782e+12	1.7160e-16	8.0957e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	3.0884e-05	1.8292e+10	1.9419e-17	1.4361e-15

step no. = 17 time = 2.1600e+04 mass check = 4.5610e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.5164e+03	9.2390e+03	2.3897e+02	0.0000e+00	1.2000e+04	5.6368e+00

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.1303e+00	1.9040e-06	1.3980e-02	4.3782e+12	1.7160e-16	8.0958e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	3.0884e-05	1.8292e+10	1.9419e-17	1.4661e-15

step no. = 18 time = 2.5200e+04 mass check = 4.5708e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.5164e+03	1.1194e+04	2.8246e+02	0.0000e+00	1.4000e+04	6.8853e+00

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.1303e+00	1.9040e-06	1.3980e-02	4.3782e+12	1.7160e-16	8.0957e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	3.0884e-05	1.8292e+10	1.9419e-17	1.4661e-15

Airborne mass distribution...

	m-distr		m-distr		m-distr		m-distr		m-distr
1	4.1982e-15	2	9.3042e-12	3	5.5187e-09	4	7.9265e-07	5	2.6447e-05
6	2.7278e-04	7	1.1696e-03	8	1.9932e-03	9	1.1239e-03	10	7.2132e-04
11	5.7521e-04	12	1.7170e-04	13	1.6630e-05				

Airborne number distribution...

	n-distr		n-distr		n-distr		n-distr		n-distr
1	1.0495e+06	2	2.3260e+08	3	1.3797e+10	4	1.9816e+11	5	6.6117e+11
6	6.8198e+11	7	2.9240e+11	8	4.9829e+10	9	2.8097e+09	10	1.8033e+08
11	1.4380e+07	12	4.2924e+05	13	4.1576e+03				

```

.....
step no. = 19   time = 2.8800e+04   mass check = 4.7011e-05
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  cing dep.  source  leaked
2.5184e+03  1.3150e+04  3.2596e+02  0.0000e+00  1.8000e+04  7.7338e+00
Airborne aerosol moments...
  sigma      rad50      mdensity  ndensity  geommean  mass50
2.1303e+00  1.9040e-06  1.3980e-02  4.3762e+12  1.7160e-16  8.0957e-14
Source moments...
  sigma      rad50      mdensity  ndensity  geommean  mass50
2.0000e+00  5.0000e-07  3.0864e-08  1.8292e+10  1.9419e-17  1.4661e-15

```

```

.....
step no. = 20   time = 3.2400e+04   mass check = 4.7252e-05
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  cing dep.  source  leaked
2.5184e+03  1.5105e+04  3.8940e+02  0.0000e+00  1.8000e+04  8.7823e+00
Airborne aerosol moments...
  sigma      rad50      mdensity  ndensity  geommean  mass50
2.1303e+00  1.9040e-06  1.3980e-02  4.3762e+12  1.7160e-16  8.0957e-14
Source moments...
  sigma      rad50      mdensity  ndensity  geommean  mass50
2.0000e+00  5.0000e-07  3.0864e-08  1.8292e+10  1.9419e-17  1.4661e-15

```

```

.....
step no. = 21   time = 3.6000e+04   mass check = 4.6498e-05
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  cing dep.  source  leaked
2.5184e+03  1.7081e+04  4.1295e+02  0.0000e+00  2.0000e+04  9.8308e+00
Airborne aerosol moments...
  sigma      rad50      mdensity  ndensity  geommean  mass50
2.1303e+00  1.9040e-06  1.3980e-02  4.3762e+12  1.7160e-16  8.0957e-14
Source moments...
  sigma      rad50      mdensity  ndensity  geommean  mass50
2.0000e+00  5.0000e-07  3.0864e-08  1.8292e+10  1.9419e-17  1.4661e-15
Airborne mass distribution...
  m-distr      m-distr      m-distr      m-distr      e-distr
1 4.1983e-15  2 9.3042e-12  3 5.5187e-09  4 7.9265e-07  5 2.6447e-05
6 2.7178e-04  7 1.1698e-03  8 1.9932e-03  9 1.1239e-03  10 7.2132e-04
11 5.7823e-04  12 1.7170e-04  13 1.8630e-05
Airborne number distribution...
  n-distr      n-distr      n-distr      n-distr      n-distr
1 1.0495e-06  2 2.3260e-08  3 1.3797e-10  4 1.9816e+11  5 6.0717e+11
6 6.8198e-11  7 2.9240e-11  8 4.9829e+10  9 2.8097e+09  10 1.8033e+03
11 1.4380e+07  12 4.2924e-05  13 4.1570e+03

```

```

.....
step no. = 22   time = 3.6300e+04   mass check = 4.1648e-05
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  cing dep.  source  leaked
2.3503e+03  1.7223e+04  4.1640e+02  0.0000e+00  2.0000e+04  9.9153e+00
Airborne aerosol moments...
  sigma      rad50      mdensity  ndensity  geommean  mass50
1.9358e+00  2.0510e-06  1.3057e-02  2.1450e+12  5.5522e-16  1.0119e-13
Source moments...

```

sigma	rad50	mdensit	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

step no. = 23 time = 3.6600e+04 mass check = 4.1020e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.1866e+03	1.7384e+04	4.1954e+02	0.0000e+00	2.0000e+04	9.9941e+00

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.8922e+00	2.1800e-06	1.2148e-02	1.4572e+12	8.8039e-16	1.2151e-13

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

step no. = 24 time = 3.6900e+04 mass check = 4.0848e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.0281e+03	1.7539e+04	4.2239e+02	0.0000e+00	2.0000e+04	1.0067e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.8683e+00	2.2903e-06	1.1267e-02	1.0997e+12	1.1661e-15	1.4091e-13

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

Airborne mass distribution...

m-distr	m-distr	m-distr	m-distr	m-distr	m-distr
1 -5.1780e-23	2 -4.2209e-20	3 1.0480e-18	4 7.9735e-10	5 1.9142e-08	
6 8.2878e-05	7 7.1373e-04	8 1.8685e-03	9 1.0224e-03	10 8.7864e-04	
11 5.5185e-04	12 1.6084e-04	13 1.4939e-05			

Airborne number distribution...

n-distr	n-distr	n-distr	n-distr	n-distr	n-distr
1 -1.2940e-02	2 -1.0552e+00	3 2.6199e+00	4 1.9034e+08	5 9.7854e+10	
6 2.0670e+11	7 1.7843e+11	8 4.1664e+10	9 2.5561e+09	10 1.6786e-09	
11 1.3798e+07	12 4.0159e+05	13 3.7348e+03			

step no. = 25 time = 3.7200e+04 mass check = 4.1042e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
1.8776e+03	1.7887e+04	4.2500e+02	0.0000e+00	2.0000e+04	1.0135e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.8517e+00	2.3817e-06	1.0431e-02	8.7799e+11	1.4164e-15	1.5846e-13

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

step no. = 26 time = 3.7500e+04 mass check = 4.1395e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
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```

1.7372e+03 1.7825e+04 4.2739e+02 0.0000e+00 2.0000e+04 1.01f3e+01
Airborne aerosol moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
1.8395e+00 2.4552e-08 9.8513e-03 7.2683e+11 1.6347e-15 1.7359e-13
Source moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.0000e+00 5.0000e-07 0.0000e+00 0.0000e+00 1.9419e-17 1.4661e-15

```

```

.....
step no. = 27   time = 3.7800e+04   mass check = 4.2587e-05
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  clng dep.  source  leaked
1.6080e+03 1.7952e+04 4.2959e+02 0.0000e+00 2.0000e+04 1.0256e+01
Airborne aerosol moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
1.8303e+00 2.5128e-08 8.9335e-03 8.1730e+11 1.8253e-15 1.8610e-13
Source moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.0000e+00 5.0000e-07 0.0000e+00 0.0000e+00 1.9419e-17 1.4661e-15
Airborne mass distribution...
  m-distr      m-distr      m-distr      m-distr      m-distr
1 -3.4222e-24 2 3.4494e-23 3 2.8243e-21 4 2.2042e-11 5 5.1163e-07
6 4.1328e-05 7 4.8751e-04 8 1.3118e-03 9 8.5784e-04 10 5.8347e-04
11 4.8218e-04 12 1.2524e-04 13 1.0070e-05
Airborne number distribution...
  n-distr      n-distr      n-distr      n-distr      n-distr
1 -8.5555e-04 2 8.7336e-04 3 7.0808e-03 4 8.5106e+08 5 1.2791e+10
6 1.0332e+11 7 1.1609e+11 8 3.2795e+10 9 2.1441e+09 10 1.4587e+08
11 1.2055e+07 12 3.1310e+05 13 2.5178e+03

```

```

.....
step no. = 28   time = 4.1400e+04   mass check = 4.5807e-05
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  clng dep.  source  leaked
7.4924e+02 1.8794e+04 4.4654e+02 0.0000e+00 2.0000e+04 1.0712e+01
Airborne aerosol moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
1.7984e+00 2.8488e-08 4.1625e-03 2.0080e+11 2.9991e-15 2.1749e-13
Source moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.0000e+00 5.0000e-07 0.0000e+00 0.0000e+00 1.9419e-17 1.4661e-15

```

```

.....
step no. = 29   time = 4.5000e+04   mass check = 4.5840e-05
.....

```

```

Mass budget...
  air-borne  flor dep.  wall dep.  clng dep.  source  leaked
4.5430e+02 1.9079e+04 4.5551e+02 0.0000e+00 2.0000e+04 1.0954e+01
Airborne aerosol moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
1.7886e+00 2.8873e-08 2.5239e-03 1.1307e+11 3.4472e-15 2.0313e-13
Source moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.0000e+00 5.0000e-07 0.0000e+00 0.0000e+00 1.9419e-17 1.4661e-15

```

step no. = 30 time = 4.8600e+04 mass check = 4.5914e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
3.1588e+02	1.9212e+04	4.8139e+02	0.0000e+00	2.0000e+04	1.1111e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7848e+00	2.5272e-08	1.7549e-03	7.8737e+10	3.6880e-15	1.8931e-13

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4881e-15

Airborne mass distribution...

m-distr		m-distr		m-distr		m-distr		m-distr	
1	1.3458e-23	2	-1.7186e-24	3	-1.1105e-25	4	1.2102e-18	5	6.2822e-09
6	3.5897e-08	7	8.8789e-05	8	2.7712e-04	9	2.1144e-04	10	1.6397e-04
11	3.7088e-05	12	2.1145e-08	13	2.0952e-08				

Airborne number distribution...

n-distr		n-distr		n-distr		n-distr		n-distr	
1	3.3840e-03	2	-4.2961e-05	3	-2.7782e-07	4	3.0255e+01	5	1.5858e+08
6	8.9741e+09	7	1.6897e+10	8	8.9280e+09	9	5.2860e+08	10	4.0992e+07
11	9.2715e+05	12	5.2863e+03	13	5.2381e+00				

step no. = 31 time = 5.2200e+04 mass check = 4.8001e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.3584e+02	1.9287e+04	4.8585e+02	0.0000e+00	2.0000e+04	1.1225e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7815e+00	2.4498e-08	1.3102e-03	5.7285e+10	3.8448e-15	1.7245e-13

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4881e-15

step no. = 32 time = 5.5800e+04 mass check = 4.5983e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
1.5408e+02	1.9238e+04	4.8994e+02	0.0000e+00	2.0000e+04	1.1311e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7788e+00	2.3601e-08	1.0225e-03	4.5253e+10	3.9823e-15	1.5419e-13

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4881e-15

step no. = 33 time = 5.9400e+04 mass check = 4.5983e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
1.4838e+02	1.9389e+04	4.7157e+02	0.0000e+00	2.0000e+04	1.1380e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7782e+00	3.2717e-08	8.2438e-04	3.7150e+10	4.0598e-15	1.3750e-13

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
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```

2.0000e+00 5.0000e-07 0.0000e+00 0.0000e+00 1.9419e-17 1.4661e-15
Airborne mass distribution...
  m-distr          m-distr          m-distr          m-distr
  1 2.1814e-21    2 9.6148e-23    3 1.7230e-25    4 2.4821e-18    5 1.5792e-09
  6 1.6108e-08    7 3.2682e-05    8 1.4450e-04    9 1.0968e-04   10 6.3448e-05
 11 5.9710e-08   12 1.3989e-07   13 4.4123e-10
Airborne number distribution...
  n-distr          n-distr          n-distr          n-distr          n-distr
  1 5.4535e-01    2 2.4037e-03    3 4.3075e-07    4 6.2052e-01    5 3.9479e+07
  6 4.0284e+09    7 8.1654e+09    8 3.6125e+09    9 2.7420e+08   10 1.5862e+07
 11 1.4928e+05   12 3.4923e+02   13 1.1031e-01

```

```

*****
step no. = 34   time = 6.3000e+04   mass check = 4.5646e-05
*****

```

```

Mass budget...
air-borne  flor dep.  wall dep.  cing dep.  source  leaked
1.2276e+02 1.9392e+04 4.7374e+02 0.0000e+00 2.0000e+04 1.1436e+01
Airborne aerosol moments...
sigma      rad50      mdensity  ndensity  geommean  mass50
1.7742e+00 2.1933e-06 6.8199e-04 3.1329e+10 4.1442e-15 1.2374e-13
Source moments...
sigma      rad50      mdensity  ndensity  geommean  mass50
2.0000e+00 5.0000e-07 0.0000e+00 0.0000e+00 1.9419e-17 1.4661e-15

```

```

*****
step no. = 35   time = 6.6600e+04   mass check = 4.6273e-05
*****

```

```

Mass budget...
air-borne  flor dep.  wall dep.  cing dep.  source  leaked
1.0372e+02 1.9409e+04 4.7657e+02 0.0000e+00 2.0000e+04 1.1483e+01
Airborne aerosol moments...
sigma      rad50      mdensity  ndensity  geommean  mass50
1.7724e+00 2.1273e-06 5.7824e-04 2.8950e+10 4.2192e-15 1.1292e-13
Source moments...
sigma      rad50      mdensity  ndensity  geommean  mass50
2.0000e+00 5.0000e-07 0.0000e+00 0.0000e+00 1.9419e-17 1.4661e-15

```

```

*****
step no. = 38   time = 7.0200e+04   mass check = 4.6034e-05
*****

```

```

Mass budget...
air-borne  flor dep.  wall dep.  cing dep.  source  leaked
8.9185e+01 1.0422e+04 4.7714e+02 0.0000e+00 2.0000e+04 1.1523e+01
Airborne aerosol moments...
sigma      rad50      mdensity  ndensity  geommean  mass50
1.7709e+00 2.0732e-06 4.9536e-04 2.3538e+10 4.2860e-15 1.0451e-13
Source moments...
sigma      rad50      mdensity  ndensity  geommean  mass50
2.0000e+00 5.0000e-07 0.0000e+00 0.0000e+00 1.9419e-17 1.4661e-15
Airborne mass distribution...
  m-distr          m-distr          m-distr          m-distr          m-distr
  1 3.6072e-20    2 1.0056e-22    3 4.0920e-26    4 2.7196e-19    5 6.8296e-10
  6 9.7388e-07    7 2.0752e-05    8 9.5830e-05    9 7.2320e-05   10 2.3869e-05
 11 1.3728e-06   12 1.5245e-08   13 -3.8987e-10
Airborne number distribution...
  n-distr          n-distr          n-distr          n-distr          n-distr
  1 9.0180e+00    2 2.5145e-03    3 1.0230e-07    4 6.7990e-02    5 1.7074e+07
  6 2.4347e+09    7 5.1880e+09    8 2.3957e+09    9 1.8080e+08   10 5.9671e+06
 11 3.4321e+04   12 3.8111e+01   13 -9.7468e-02

```



step no. = 37 time = 7.3800e+04 mass check = 4.5486e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
7.7731e+01	1.9432e+04	4.7852e+02	0.0000e+00	2.0000e+04	1.1558e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7893e+00	2.0286e-08	4.3184e-04	2.0805e+10	4.3453e-15	9.7912e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4681e-15

step no. = 38 time = 7.7400e+04 mass check = 4.5340e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
6.8530e+01	1.9440e+04	4.7973e+02	0.0000e+00	2.0000e+04	1.1589e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7878e+00	1.9912e-08	3.8072e-04	1.8568e+10	4.3979e-15	9.2802e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4681e-15

step no. = 39 time = 8.1000e+04 mass check = 4.5453e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
6.0966e+01	1.9447e+04	4.8080e+02	0.0000e+00	2.0000e+04	1.1616e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7881e+00	1.9590e-08	3.3870e-04	1.6705e+10	4.4442e-15	8.8179e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4681e-15

Airborne mass distribution...

m-distr	m-distr	m-distr	m-distr	m-distr	m-distr
1 -2.6528e-20	2 2.9815e-23	3 -9.5324e-28	4 6.9910e-20	5 3.7088e-10	6 6.6798e-07
7 1.4755e-05	8 7.0241e-05	9 5.1397e-05	10 9.8505e-06	11 3.8124e-07	12 2.3619e-09
13 2.0986e-12					

Airborne number distribution...

n-distr	n-distr	n-distr	n-distr	n-distr	n-distr
1 -6.6318e+00	2 7.4538e-04	3 -2.3831e-09	4 1.4978e-02	5 9.2720e+06	6 1.6700e+09
7 3.6888e+09	8 1.7560e+08	9 1.2849e+08	10 2.4126e+06	11 9.5309e+03	12 5.9048e+00
13 5.2466e-04					

step no. = 40 time = 8.4600e+04 mass check = 4.5437e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
5.4631e+01	1.9452e+04	4.8177e+02	0.0000e+00	2.0000e+04	1.1640e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7642e+00	1.9303e-06	3.0351e-04	1.5130e+10	4.4848e-15	8.4355e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

step no. = 41 time = 8.8200e+04 mass check = 4.5415e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
4.9243e+01	1.9456e+04	4.8264e+02	0.0000e+00	2.0000e+04	1.1681e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7622e+00	1.9038e-06	2.7357e-04	1.3783e+10	4.5203e-15	8.0935e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

step no. = 42 time = 9.1800e+04 mass check = 4.5376e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
4.4600e+01	1.9460e+04	4.8344e+02	0.0000e+00	2.0000e+04	1.1681e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7601e+00	1.8789e-06	2.4778e-04	1.2618e+10	4.5512e-15	7.7792e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

Airborne mass distribution...

m-distr	m-distr	n-distr	m-distr	m-distr
1 -3.5820e-20	2 -1.0489e-23	3 -1.4901e-28	4 1.8478e-20	5 2.2854e-10
6 4.9135e-07	7 1.1174e-05	8 3.4326e-05	9 3.7118e-05	10 4.3750e-08
11 1.2350e-07	12 4.8239e-10	13 9.3030e-11		

Airborne number distribution...

n-distr	n-distr	n-distr	n-distr	n-distr
1 -8.9051e+00	2 -2.8223e-04	3 -3.7002e-10	4 4.8195e-03	5 5.7138e+08
6 1.2284e+09	7 2.7928e+09	8 1.3581e+09	9 9.2794e+07	10 1.0938e+08
11 3.0875e+03	12 1.2060e+00	13 1.5757e-02		

step no. = 43 time = 9.6400e+04 mass check = 4.5587e-05

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
4.0557e+01	1.9464e+04	4.8416e+02	0.0000e+00	2.0000e+04	1.1698e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7578e+00	1.8549e-06	2.2532e-04	1.1601e+10	4.5781e-15	7.4847e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

step no. = 44 time = 9.9000e+04 mass check = 4.5619e-05

```

Mass budget...
  air-borne   flor dep.   wall dep.   clng dep.   source       leaked
  3.7007e+01  1.9488e+04  4.8482e+02  0.0000e+00  2.0000e+04  1.1715e+01
Airborne aerosol moments...
  sigma      rad50      mdensity   ndensity   geommean    mass50
  1.7554e+00  1.8315e-06  2.0559e-04  1.0707e+10  4.8018e-15  7.2055e-14
Source moments...
  sigma      rad50      mdensity   ndensity   geommean    mass50
  2.0000e+00  5.0000e-07  0.0000e+00  0.0000e+00  1.9419e-17  1.4881e-15

```

```

.....
step no. = 45   time = 1.0280e+05   mass check = 4.5890e-05
.....

```

```

Mass budget...
  air-borne   flor dep.   wall dep.   clng dep.   source       leaked
  3.3887e+01  1.9489e+04  4.8542e+02  0.0000e+00  2.0000e+04  1.1729e+01
Airborne aerosol moments...
  sigma      rad50      mdensity   ndensity   geommean    mass50
  1.7529e+00  1.8086e-06  1.8815e-04  9.9181e+09  4.8220e-15  5.9391e-14
Source moments...
  sigma      rad50      mdensity   ndensity   geommean    mass50
  2.0000e+00  5.0000e-07  0.0000e+00  0.0000e+00  1.9419e-17  1.4881e-15
Airborne mass distribution...
  m-distr          m-distr          m-distr          m-distr          m-distr
  1  3.1743e-20    2 -2.3109e-23    3  1.7541e-29    4  7.2626e-21    5  1.5264e-10
  6  3.7787e-07    7  8.8140e-08    8  4.3480e-05    9  2.8792e-05   10  2.2040e-06
 11  4.5370e-08   12  1.2082e-10   13 -1.8089e-10
Airborne number distribution...
  n-distr          n-distr          n-distr          n-distr          n-distr
  1  7.9357e+00    2 -5.7772e-04    3  4.3853e-11    4  1.8157e-03    5  3.8159e+06
  6  9.4487e+08    7  2.2035e+09    8  1.0870e+09    9  8.8980e+07   10  5.5100e+05
 11  1.1342e+03   12  3.0208e-01   13 -4.0172e-02

```

```

.....
step no. = 46   time = 1.0620e+05   mass check = 4.5870e-05
.....

```

```

Mass budget...
  air-borne   flor dep.   wall dep.   clng dep.   source       leaked
  3.1075e+01  1.9471e+04  4.8598e+02  0.0000e+00  2.0000e+04  1.1743e+01
Airborne aerosol moments...
  sigma      rad50      mdensity   ndensity   geommean    mass50
  1.7503e+00  1.8863e-06  1.7264e-04  9.2111e+09  4.8397e-15  6.8849e-14
Source moments...
  sigma      rad50      mdensity   ndensity   geommean    mass50
  2.0000e+00  5.0000e-07  0.0000e+00  0.0000e+00  1.9419e-17  1.4881e-15

```

```

.....
step no. = 47   time = 1.0980e+05   mass check = 4.5813e-05
.....

```

```

Mass budget...
  air-borne   flor dep.   wall dep.   clng dep.   source       leaked
  2.8581e+01  1.9473e+04  4.8649e+02  0.0000e+00  2.0000e+04  1.1755e+01
Airborne aerosol moments...
  sigma      rad50      mdensity   ndensity   geommean    mass50
  1.7478e+00  1.7844e-06  1.5878e-04  8.5794e+09  4.8552e-15  6.4423e-14
Source moments...
  sigma      rad50      mdensity   ndensity   geommean    mass50
  2.0000e+00  5.0000e-07  0.0000e+00  0.0000e+00  1.9419e-17  1.4881e-15

```

.....  
.....  
step no. = 48 time = 1.1340e+05 mass check = 4.5813e-05  
.....

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.8343e+01	1.9475e+04	4.8696e+02	0.0000e+00	2.0000e+04	1.1767e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7449e+00	1.7431e-06	1.4635e-04	8.0106e+09	4.8686e-15	6.2118e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

Airborne mass distribution...

m-distr	m-distr	m-distr	m-distr	m-distr
1 -8.9422e-22	2 -6.4798e-25	3 1.3112e-30	4 3.3463e-21	5 1.0775e-10
6 2.9983e-07	7 7.1518e-06	8 3.5831e-05	9 1.9261e-05	10 1.1959e-06
11 1.8224e-08	12 3.4217e-11	13 -1.4100e-13		

Airborne number distribution...

n-distr	n-distr	n-distr	n-distr	n-distr
1 -2.2355e-01	2 -1.8199e-05	3 3.2781e-12	4 8.3658e-04	5 2.6937e+06
6 7.4908e+08	7 1.7879e+09	8 8.9079e+08	9 4.8154e+07	10 2.9897e+05
11 4.5580e+02	12 8.5544e-02	13 -3.5250e-05		

.....  
.....  
step no. = 49 time = 1.1700e+05 mass check = 4.5813e-05  
.....

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.4329e+01	1.9476e+04	4.8740e+02	0.0000e+00	2.0000e+04	1.1777e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7422e+00	1.7224e-06	1.3516e-04	7.4980e+09	4.8802e-15	5.9934e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

.....  
.....  
step no. = 50 time = 1.2090e+05 mass check = 4.5813e-05  
.....

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.2511e+01	1.9478e+04	4.8761e+02	0.0000e+00	2.0000e+04	1.1787e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
1.7394e+00	1.7025e-06	1.2506e-04	7.0286e-09	4.8903e-15	5.7873e-14

Source moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
2.0000e+00	5.0000e-07	0.0000e+00	0.0000e+00	1.9419e-17	1.4661e-15

.....  
.....  
step no. = 51 time = 1.2240e+05 mass check = 4.5814e-05  
.....

Mass budget...

air-borne	flor dep.	wall dep.	clng dep.	source	leaked
2.1867e+01	1.9479e+04	4.8800e+02	0.0000e+00	2.0000e+04	1.1792e+01

Airborne aerosol moments...

sigma	rad50	mdensity	ndensity	geommean	mass50
-------	-------	----------	----------	----------	--------

```

1.7381e+00 1.6928e-06 1.2037e-04 6.8107e+09 4.6948e-15 5.6890e-14
Source moments...
  sigma      rad50      mdensity      ndensity      geommean      mass50
2.0000e+00 5.0000e-07 0.0000e+00 0.0000e+00 1.9419e-17 1.4881e-15
Airborne mass distribution...
  m-distr      m-distr      m-distr      m-distr      m-distr
1 9.4432e-23 2 -9.3458e-27 3 2.3197e-31 4 1.9197e-21 5 8.3180e-11
8 2.5126e-07 7 8.1057e-08 8 3.0582e-05 9 1.4585e-05 10 7.4486e-07
11 8.9202e-09 12 1.2785e-11 13 2.0536e-15
Airborne number distribution...
  n-distr      n-distr      n-distr      n-distr      n-distr
1 2.3608e-02 2 -2.3384e-07 3 5.7991e-13 4 4.7993e-04 5 2.0790e+06
8 6.2814e+08 7 1.5284e+09 8 7.6454e+08 9 3.6464e+07 10 1.8621e+05
11 2.2301e+02 12 3.1982e-02 13 5.1340e-07

```

.....

## APPENDIX B - SUBROUTINE DESCRIPTION

We will summarize here the purpose of each subroutine in order of its appearance in the figure in Appendix C, reading left to right then top to bottom. Generally, this will only be a statement of what each subroutine does, since details can be obtained from the source listing in Appendix D. However, a more detailed description will be given when it is thought that some aspects of operation of a subroutine may not be immediately apparent.

### CHARM

This is the main program. It organizes the sequence in which the other subroutines are called, the aim being to make sure that the common block variables are updated in the right order as the calculation progresses.

The values the time dependent variables take, when they are not updated continuously, correspond to the mid-point of the current time and the next time they are to be updated. ITHHY is a counter which determines which set of interpolation formulae are to be used.

The ODE solver is allowed to integrate beyond the value of TIME and interpolate backwards as needed. Therefore, the subroutines CHARMUTH to CHARMSLN could have been called by CHARMRHS at a time not equal to TIME when the time dependent variables are updated continuously and so, in this circumstance, they are called again immediately prior to calling CHARMOUT.

When the argument to CHARMDIP equals RESET it tells the ODE solver to reinitialize its variables. This is done whenever the time dependent variables or their derivatives may change discontinuously and ensures that the solver is not required to integrate across a discontinuity.

### CHARMBLO

This is a block data subroutine which sets default values for all input variables, assigns values to  $\mu$ ,  $g$ ,  $k$  and  $R$ , and defines the Fortran unit numbers of the input and output streams.

### CHARMIN

This subroutine reads the input data file.

### CHARMCOL

This subroutine calculates  $m_i$  for  $i = 1, \dots, n$ ,  $h$ ,  $e^h$  and  $\log_e(m_1 e^{-h})$ .

### CHARMIND

This subroutine calculates the indexing which is later used to determine when  $P_{jk}^i$  for given  $i$ ,  $j$  and  $k$  is non-zero and where it is stored.

### CHARMFUN

This function subroutine calculates the function  $\log_e(1-e^{-x})$ . Series expansions and compiler directives to switch-off vectorization during addition of the terms in the series are used to reduce rounding errors.

### CHARMCOE

This subroutine calculates all non-zero values of  $P_{jk}^i$ . A change of variable has been made in Eq. (56)  $y' = y - j$  to avoid adding the result obtained from CHARMFUN, which can be small compared to unity, to  $j$ . Gauss-Legendre integration does not work when the integrand is non-smooth and so the integration range is divided into sub-ranges over which the integrand is smooth and the integral is calculated as the sum of the integrals over the sub-ranges.

### SSORT

This subroutine sorts the contents of an array into ascending order. Refer to the CLAMS compendium (Ford, 1984) for instructions on how to get an abstract, documentation and a compiler listing for this subroutine.

### GAUS8

This subroutine calculates the definite integral of the supplied function using Gauss-Legendre integration. Refer to the CLAMS compendium (Ford, 1984) for instructions on how to get an abstract, documentation and a compiler listing for this subroutine.

### CHARMPJK

This function subroutine calculates the integrand of the production coefficient integral. The addition is done in double precision to avoid rounding errors in CHARMPJK when CHARMFE is small compared to unity.

### CHARMFE

This function subroutine calculates the basic finite element. The calculations are done in double precision to avoid rounding errors in CHARMFE when it is small compared to unity.

### CHARMNOR

This subroutine calculates  $n_{jk}$  for  $j, k = 1, \dots, n$ .

### CHARMRAD

This subroutine calculates  $r_i$  for  $i = 1, \dots, n$ .

### CHARMZLN

This subroutine calculates the initial values of  $Y_i$  for  $i = 1, \dots, n$  assuming the initial aerosol number distribution to be log-normal. The discretized distribution is renormalized so the airborne mass exactly equals that specified.

### CHARMITH

This subroutine sets-up (Initializes) the interpolation formulae for the time dependent variables. It first calculates the time up to which each formula applies and the number of formulae and then calculates the interpolation formulae coefficients for all the time dependent variables.

### CHARMETH

This subroutine calculates a set of interpolation formulae coefficients for a given table of data values.

### CHARMUTH

This subroutine calculates (Updates) the time dependent variables at the specified time using the interpolation formulae previously calculated.

### CHARMGAS

This subroutine calculates  $\rho_g$ ,  $\eta_g$ ,  $l$ ,  $D_v$ ,  $c_c$ ,  $c_w$  and  $c_f$ . Correlations are used for  $\eta_g$  and  $D_v$  assuming the gas in the bulk of the cell to be pure air and the vapor in gas mixture adjacent to surfaces to be steam in air.

### CHARMMOB



This subroutine calculates  $B_i$  for  $i = 1, \dots, n$ .

#### CHARMFLO

This subroutine calculates  $u_w$ ,  $\epsilon_w$ ,  $\delta_w$  and  $\delta_{Di}$  for  $i = 1, \dots, n$ . The Fanning friction factor, which enters the equation for  $u_w$ , is determined by a transcendental equation which is solved with COSWHE.

#### COSWHE

This subroutine finds a root of the supplied function within the specified range.

#### CHARMFAN

The zero of this function determines the Fanning friction factor in a cylindrical pipe of any roughness at any Reynolds number. Pipes of other cross-sectional shape are dealt-with by defining a hydraulic diameter equal to the diameter of the equivalent cylindrical pipe.

#### CHARMAGG

This subroutine calculates  $K_{jk}$  for  $j, k = 1, \dots, n$ .

#### CHARMDEP

This subroutine calculates  $\lambda_{ci}$ ,  $\lambda_{wi}$  and  $\lambda_{fi}$  for  $i = 1, \dots, n$ .

#### CHARMSLN

This subroutine calculates  $m_i S_i$  for  $i = 1, \dots, n$ . The number distribution of the source is assumed to be log-normal. The  $m_i S_i$  are renormalized so that the mass generation rate of the discretized distribution exactly equals that specified.

#### CHARMDIF

This subroutine sets-up the input required by DEBDF, calls DEBDF to integrate the governing equations to the specified time and checks whether the call was successful.

### DEBDF

This subroutine integrates a set of coupled non-linear ODE's using the variable order backward differentiation method due to Hindmarsh (Shampine and Watts, 1979). Refer to the CLAMS compendium (Ford, 1984) for instructions on how to get an abstract, documentation and a compiler listing for this subroutine.

### CHARMRHS

This subroutine calculates the time derivatives of:  $Y_i$  for  $i = 1, \dots$ , the mass deposited on the floor, wall and ceiling, the mass released from the source and the leaked mass.

### CHARMMOM

This subroutine calculates the moments  $\sigma$ ,  $r_{50}$ ,  $\rho$ ,  $N$ ,  $m_g$  and  $m_{50}$  of the discretized distribution using the trapezium rule.  $m_{50}$  is determined by a transcendental equation whose root is found with COSWHE.

### CHARMM50

This function subroutine calculates  $\int_0^m mY(m,t) d\log_e m - \rho/2$ . The trapezium rule is used to estimate the integral. The zero of CHARMM50 is the natural logarithm of  $m_{50}$ .

### CHARMFEO

This function subroutine calculates  $\int_0^m g_i(\log_e m) d\log_e m$  for arbitrary  $m$ . Analytic formulae are used.

### CHARMOUT

This subroutine writes results on the two output files.

## APPENDIX C - SUBROUTINE HIERARCHY AND CALLING SEQUENCE

The overall organization of the computations in CHARM is discussed here to assist those who would like to modify CHARM to suit their own purposes.

CHARM is modular in the sense that the calculations are broken down into a sequence of tasks and each task is dealt-with within a subroutine devoted to that task only and nowhere else. The purpose of each subroutine has been described in the previous section. Here, we describe how the subroutines fit together.

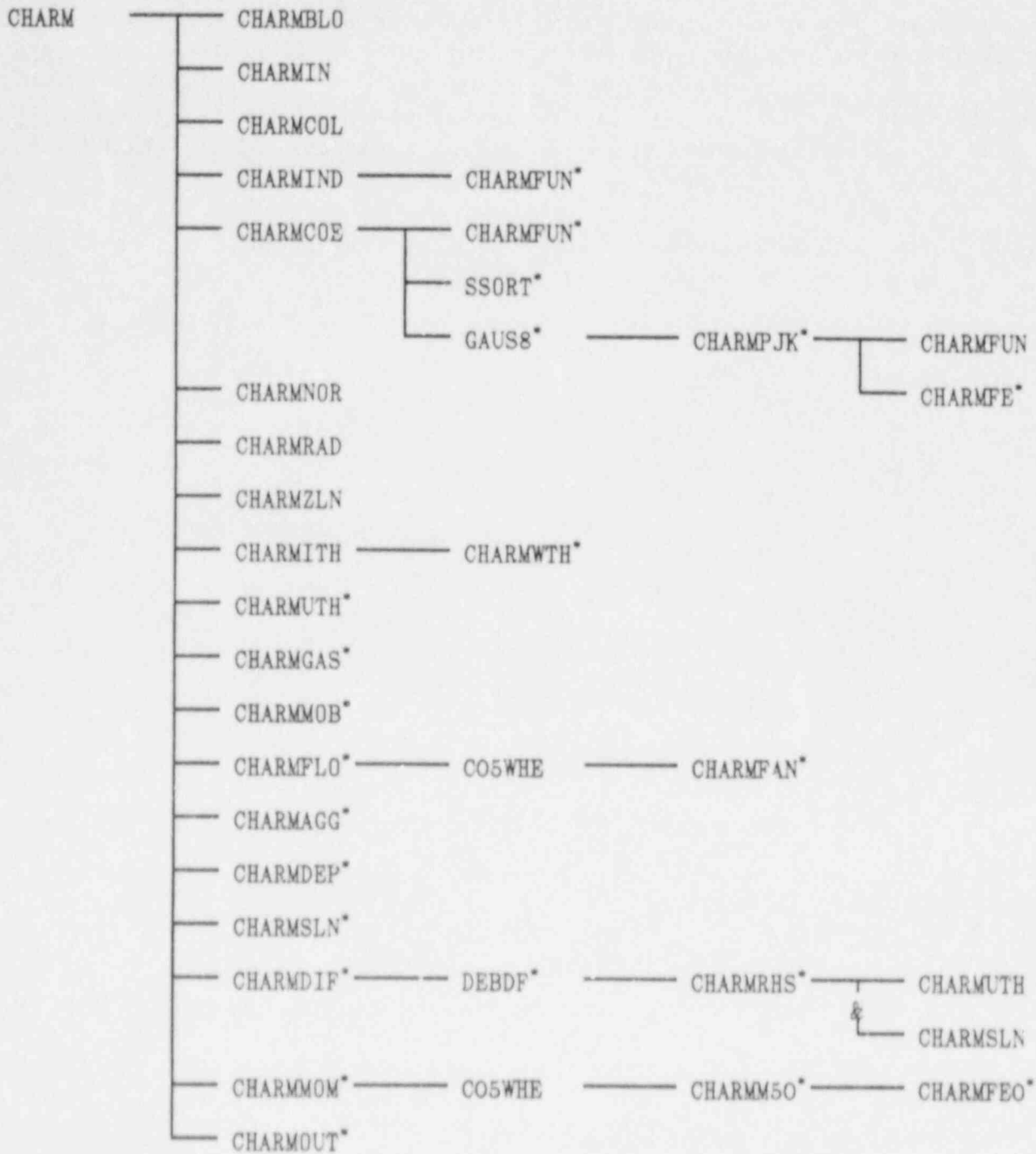
This is illustrated in the figure on the next page which shows what calls a subroutine makes to others and in what order. The logic for when and how often specific calls are made is outlined below (we indicate on the figure with an asterisk adjacent to a subroutine when it can be called more than once by its caller - the reader is referred to the source listing in Appendix D for exact details of when a subroutine is called). The callees for CHARMCOE and CHARMPJK are shown in order of their first encounter in the sequence of calls made by the callers.

Data is communicated largely by means of named common blocks; in some cases it is communicated through subroutine arguments when this is convenient or dictated by externally supplied subroutines. Each common block is designed to hold data for particular purposes so that subroutines as far as possible do not have long lists of common block variables.

Referring now to the sequence of calls shown in the figure, CHARMBLO is a block data subroutine and is shown on the sequence for completeness.

The subroutines CHARMIN to CHARMITH are called once only to calculate variables associated with the discretized form of the governing equations, the initial density distribution and coefficients in the interpolation formulae for the time dependent data.

The subroutines CHARMUTH to CHARMSLN calculate the source distribution and the agglomeration and deposition rates. These calculations depend on the external time dependent variables and therefore have to be repeated according to the specifications chosen by the user. If the user requires these quantities to be updated continuously with time then they are recalculated by CHARMRHS each time it is called. Otherwise they are recalculated by CHARM whenever the current time exceeds the previous time these variables were updated by a specified time period or equals a time when a new set of interpolation formulae for the time dependent variables apply, whichever occurs first.



\* The subroutine is called more than once by the caller.

& The sequence here is the same as that between CHARMUTH and CHARMSLN called from CHARM.

### The subroutine hierarchy and calling sequence

CHARMDIF is called to integrate the governing equations to the next time output is required or the next time the time dependent variables have to be updated

(when they are not updated continuously) or the next time a new set of interpolation formulae apply, whichever occurs first.

CHARMMOM is called initially (i.e. at time equals zero) and following every call to CHARMDIF, since some moments are used in the succeeding call to CHARMDIF to set tolerances.

CHARMOUT is called initially and whenever the governing equations have been integrated to a time when output is desired.

## APPENDIX D - SOURCE LISTING

The subroutines are listed in order of appearance in the calling sequence shown in the figure in Appendix C, reading left to right then top to bottom.

```

program charm(charmdat,tape4=charmdat, tty,tape5=TTY
+
, out,tape6=out)
c
c This program solves the aerosol equation taking account of
c agglomeration, deposition and leakage of the aerosol.
c Collocation is used to discretize the equation.
c The agglomeration kernel is calculated on a 2D mesh only
c so it can be updated as the thermal hydraulic conditions
c change with time without undue computational labor.
c The agglomeration and deposition rate formulae are based on those
c in MAEROS but have been extended to treat diffusiophoresis
c and turbulent deposition.
c
common /timings/ time,istep,thystep
+
,itime,ntime,timestep(20),timeend(20)
+
,ithhy,nthhy,timethhy(20)
+
,idata,ndata,timedata(20)
c
logical reset,noreset,flag
data reset,noreset/.true.,.false./
external charmblo
c
c Calculate time-independent variables
c *****
c
call charmin
call charmcol
call charmind
call charmcoe
call charmnor
call charmrtd
call charmzln
c
c Initialize the time dependent data
c *****
c
call charmith
ithhy=1
timemean=min(thystep,timethhy(ithhy))/2.e0
call charmuth(timemean)
call charmgas
call charmmob
call charmflo
call charmagg
call charmdep
call charmsln
c
c Calculate initial moments and print initial values
c *****
c
call charmmom
istep=0
time=0.e0
call charmout
istep=istep+1
c
c Calculate upper bound for number of calls to CHARMDIF
c *****
c
icalls=ntime+nthhy+timeend(1)/timestep(1)
if(thystep.ne.0.e0)then
icalls=icalls+timeend(ntime)/thystep
endif
if(ntime.gt.1)then
do 5 itime=2,ntime
icalls=icalls+(timeend(itime)-timeend(itime-1))/timestep(itime)
5 continue
endif
ncalls=icalls

```

c		charm 68
c	Loop over calls to CHARMDIF	charm 69
c	*****	charm 70
c		charm 71
	itime=1	charm 72
	flag=reset	charm 73
	do 10 icalls=1,ncalls	charm 74
c		charm 75
c	Find the next time to which the equations are to be integrated	charm 76
c	*****	charm 77
c		charm 78
	if(time.lt.timeend(ntime))then	charm 79
c		charm 80
c	Print results at this time	charm 81
c	*****	charm 82
c		charm 83
	if(itime.eq.1)then	charm 84
	timelow=0.e0	charm 85
	else	charm 86
	timelow=timeend(itime-1)	charm 87
	endif	charm 88
	timel=timelow	charm 89
	+ + (irt((time-timelow)/timestep(itime))+1)*timestep(itime)	charm 90
	if(timel.le.time)timel=timel+timestep(itime)	charm 91
	if(timel.gt.timeend(itime))timel=timeend(itime)	charm 92
c		charm 93
c	Update the variables at this time	charm 94
c	*****	charm 95
c		charm 96
	if(thhystep.ne.0.e0)then	charm 97
	if(ithhy.eq.1)then	charm 98
	timelow=0.e0	charm 99
	else	charm100
	timelow=timethhy(ithhy-1)	charm101
	endif	charm102
	time2=timelow+(int((time-timelow)/thhystep)+1)*thhystep	charm103
	if(time2.le.time)time2=time2+thhystep	charm104
	if(time2.gt.timethhy(ithhy))time2=timethhy(ithhy)	charm105
	else	charm106
	time2=timethhy(ithhy)	charm107
	endif	charm108
c		charm109
c	Integrate the equations to the new time	charm110
c	*****	charm111
c		charm112
c	CHARMMOM is always called after CHARMDIF because the following	charm113
c	call to CHARMDIF needs the moments to set tolerances.	charm114
c		charm115
	time=min(timel,time2)	charm116
	call charmdif(flag)	charm117
	call charmmom	charm118
c		charm119
c	Print results	charm120
c	*****	charm121
c		charm122
	if(time.eq.timeend(itime))itime=min(itime+1,ntime)	charm123
	if(time.eq.timel)then	charm124
c		charm125
c	Make sure time dependent variables	charm126
c	are evaluated at the current time.	charm127
c	*****	charm128
c		charm129
	if(thhystep.eq.0.e0)then	charm130
	call charmuth(time)	charm131
	call charmgas	charm132
	call charmsob	charm133
	call charmflo	charm134
	call charmagg	charm135
	call charmdep	charm136



```

        call charmsln
        endif
    call charmout
    istep=istep+1
    endif
c
c      Update the time dependent data if necessary
c      *****
c
    if(time.eq.timethhy(ithhy))ithhy=min(ithhy+1,nthhy)
        if( time.eq.time2
+ .and. thhystep.ne.0.e0
+ .and. time.lt.timeend(ntime) )then
            timemean=time+min(thhystep,timethhy(ithhy)-time)/2.e0
            call charmuth(timemean)
            call charmgas
            call charzmob
            call charmflo
            call charmagg
            call charmdep
            call charmsln
        endif
c
c      Reset the ODE solver when the variables are continuously
c      *****
c
        if(time.eq.time2)then
            flag=reset
        else
            flag=noreset
        endif
10  endif
    continue
    stop
    end

```

```

charm137
charm138
charm139
charm140
charm141
charm142
charm143
charm144
charm145
charm146
charm147
charm148
charm149
charm150
charm151
charm152
charm153
charm154
charm155
charm156
charm157
charm158
charm159
charm160
charm161
charm162
charm163
charm164
charm165
charm166
charm167
charm168
charm169
charm170
charm171

```

```

c      block data charmblo
c
c      This subroutine sets-up default data values. Phenological
c      constants are those used in MAEROS. The data values can be
c      altered by CHARMIN.
c
c      common /collpts/  ncoll,mlower,mupper,spacing,dlogem,logem0
+                       ,radius(100),mass(100),mobility(100)
c      real
+                       logem0,mass,mobility,mlower,mupper
c
c      common /aerslcon/ cshpfctr,dshpfctr,stickeff
+                       ,aknudweb,qknudweb,bknudweb
+                       ,pdensity,pthrcon
+                       ,kbrock,cmbrock,ctbrock
c      real
+                       kbrock
c
c      common /gasprops/ temp,press,gdensity,dynvisc,molwt,mnfrpath
+                       ,gthrcon,velocity,molwtv,diffusv
+                       ,vmfrclng,vmfrwall,vmfrflor
+                       ,vcgrclng,vcgrwall,vcgrflor
+                       ,vconclng,vconwall,vconflor
c      real
+                       molwt,mnfrpath,molwtv
c
c      common /fundcon/  pi,boltzmnn,gravitat,gasconst
c
c      common /indexcoe/ nelement,hwidth,jbarmin,index(-2:100)
+                       ,kbarmin(-2:100),kbarmax(-2:100),nkbar(-2:100)
c
c      common /lognormz/ sigmazln,rad50zln,mdenzln
+                       ,ndenzln,geomzln,mas50zln
c      real
+                       mdenzln,ndenzln,mas50zln
c
c      common /thrshydr/ tgasao(20),tgasal(20),tgasdata(20)
+                       ,pgasao(20),pgasal(20),pgasdata(20)
+                       ,vgasao(20),vgasal(20),vgasdata(20)
+                       ,tclgaO(20),tclgal(20),tclgdata(20)
+                       ,twalaO(20),twalal(20),twaldata(20)
+                       ,tflraO(20),tflral(20),tflrdata(20)
+                       ,sigasO(20),sigasal(20),sigasdata(20)
+                       ,radsaO(20),radsal(20),radsdata(20)
+                       ,mdesaO(20),mdesal(20),mdesdata(20)
c      real
+                       mdesaO,mdesal,mdesdata
c
c      common /timings/  time,istep,thhystep
+                       ,itime,ntime,timestep(20),timeend(20)
+                       ,ithhy,nthhy,timethhy(20)
+                       ,idata,ndata,timedata(20)
c
c      common /toleranc/ eps,eta,sets,maxcalls,maxtrys
c
c      common /ioflags/  iondis,iozrom,ioccoef,ionorm
+                       ,iodepo,iomase,ioradi,iomobi
+                       ,ioaggl,iomdis,iosdis,iombal
+                       ,ioindx,iosmom,iocell,iogasp
+                       ,iotole,ioacon,iowflow
c
c      common /iotapes/  columns,ntape4,ntape5,ntape6
c      integer
+                       columns
c
c      common /cell/
+                       areaclng,areawall,areafloor
+                       ,tempclng,tespwall,tespflor
+                       ,volume,leakrate
+                       ,hydrdiam,eqvrrough
c      real
+                       leakrate
c
c      common /flow/
+                       blflag,vblthick,dblthick(100)
+                       ,eddydiss,ustar,reynolds
c      integer
+                       blflag
c

```

```

chmblo 2
chmblo 3
chmblo 4
chmblo 5
chmblo 6
chmblo 7
collpts2
collpts3
collpts4
chmblo 9
aerslco2
aerslco3
aerslco4
aerslco5
aerslco6
chmblo11
gasprop2
gasprop3
gasprop4
gasprop5
gasprop6
gasprop7
chmblo13
fundcon2
chmblo15
indexco2
indexco3
chmblo17
lognorm2
lognorm3
lognorm4
chmblo19
thrshyd2
thrshyd3
thrshyd4
thrshyd5
thrshyd6
thrshyd7
thrshyd8
thrshyd9
thrshy10
thrshy11
chmblo21
timings2
timings3
timings4
timings5
chmblo23
toleran2
chmblo25
ioflags2
ioflags3
ioflags4
ioflags5
ioflags6
chmblo27
iotapes2
iotapes3
chmblo29
cell 2
cell 3
cell 4
cell 5
cell 6
chmblo31
flow 2
flow 3
flow 4
chmblo33

```

```

c
c
data mlower,mupper,spacing/4.e-21,4.e-9,10.e0/
data nelement,ncoll/2,0/
c
data cshpfctr,dshpfctr,wtickeff/1.e0,1.e0,1.e0/
data aknudweb,qknudweb,bknudweb/1.37e0,0.4e0,1.1e0/
data pdensity,pthrmcon/2.8e3,.8375e0/
data kbrock,cmbrock,ctbrock/1.e0,1.37e0,1.e0/
c
data molwt,gthrmcon,molwtv
+ /28.98e0,.0255e0,18.015e0/
data tgasdata,pgasdata,vgasdata
+ /293.15e0,19*-1.e0,1.01325e5,19*-1.e0,0.e0,19*-1.e0/
data vmfrclng,vmfrwall,vmfrflor/0.e0,0.e0,0.e0/
data vcgrclng,vcgrwall,vcgrglor/0.e0,0.e0,0.e0/
c
data blflag,vblthick,dblthick/0,0.e0,100*0.e0/
c
data pi,boltzmn,gravitat,gasconst
+ /3.141592653e0,1.38054e-23,9.81e0,8.3143e0/
c
data sigmazln,rad5Ozln,mdenzln/2.e0,5.e-7,0.e-2/
c
data sigsdata,radsdata,mdesdata
+ /2.e0,19*-1.e0,5.e-7,19*-1.e0,0.e0,19*-1.e0/
c
data ntime,timestep(1),timeend(1)/1,10.e0,10.e0/
c
data eps,eta,zeta,maxcalls,maxtrys
+ /1.e-8,0.e0,0.5e0,30,10/
c
data iocell,iogasp,ioacon/1,1,1/
data iocsmom,iocdis,iocflow/1,0,1/
data iocmass,iocradi,iocobi/1,1,0/
data iodepo,iocaggl/0,0/
data iocindx,ioccoef,iocnorm/0,0,0/
data iocbal,ioccle/1,0/
data iocsmom,iocdis,iocdis/1,0,0/
c
data columns/80/
data ntape4,ntape5,ntape6/4,8,0/
c
data volume,leakrate/1.e5,0.e0/
data hydridiaz,eqvrrough/0.e0,4.5e-5/
data areacng,areawall,areafloor/0.e0,0.e0,0.e0/
data tclgdata,twaldata,tflrdata
+ /293.15e0,19*-1.e0,293.15e0,19*-1.e0,293.15e0,19*-1.e0/
c
data ndata/1/
data timesdata/20*0.e0/
c
data thhystep/1.e10/
c
end

```

```

chmblo34
chmblo35
chmblo36
chmblo37
chmblo38
chmblo39
chmblo40
chmblo41
chmblo42
chmblo43
chmblo44
chmblo45
chmblo46
chmblo47
chmblo48
chmblo49
chmblo50
chmblo51
chmblo52
chmblo53
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chmblo58
chmblo59
chmblo60
chmblo61
chmblo62
chmblo63
chmblo64
chmblo65
chmblo66
chmblo67
chmblo68
chmblo69
chmblo70
chmblo71
chmblo72
chmblo73
chmblo74
chmblo75
chmblo76
chmblo77
chmblo78
chmblo79
chmblo80
chmblo81
chmblo82
chmblo83
chmblo84
chmblo85
chmblo86
chmblo87
chmblo88

```

```

subroutine charmin
c
c This subroutine reads in data from the file CHARMDAT.
c List directed read is used so data items can be in free format.
c Since character variables are not in the input lists, a character
c placed in a line will cause it to be read as a comment card.
c The back slash can be used to skip reading a line so that
c default values are used. Otherwise, values read-in will
c over-ride values preset in the blockdata subroutine CHARMBLO.
c
common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ ,radius(100),mass(100),mobility(100)
real
logem0,mass,mobility,mlower,mupper
c
common /aerslcon/ cshpfctr,dshpfctr,stickeff
+ ,aknudweb,qknudweb,bknudweb
+ ,pdensity,pthracon
+ ,kbrock,cmbrock,ctbrock
real
kbrock
c
common /gasprops/ temp,press,gdensity,dynvisc,molwt,mnfrpath
+ ,gthracon,velocity,molwtv,diffusv
+ ,vmfrclng,vmfrwall,vmfrflor
+ ,vcgrclng,vcgrwall,vcgrflor
+ ,vconclng,vconwall,vconflor
real
molwt,mnfrpath,molwtv
c
common /indexcoe/ nelement,hwidth,jbarmin,index(-2:100)
+ ,kbarmin(-2:100),kbarmax(-2:100),nkbar(-2:100)
c
common /timings/ time,istep,thhystep
+ ,itime,ntime,timestep(20),timeend(20)
+ ,ithhy,nthhy,timethhy(20)
+ ,idata,ndata,timedata(20)
c
common /toleranc/ eps,eta,zeta,maxcalls,maxtrys
c
common /lognorms/ sigmazln,rad50zln,mdenzln
+ ,ndenzln,geomzln,mas50zln
real
mdenzln,ndenzln,mas50zln
c
common /thrahydr/ tgas0(20),tgas1(20),tgasdat(20)
+ ,pgasa0(20),pgasa1(20),pgasdata(20)
+ ,vgasa0(20),vgasa1(20),vgasdata(20)
+ ,tclga0(20),tclga1(20),tclgdata(20)
+ ,twala0(20),twala1(20),twaldata(20)
+ ,tflra0(20),tflra1(20),tflrdata(20)
+ ,sigsa0(20),sigsa1(20),sigdata(20)
+ ,rades0(20),rades1(20),radesdata(20)
+ ,mdeea0(20),mdeea1(20),mdeedata(20)
real
mdeea0,mdeea1,mdeedata
c
common /ioflags/ iendis,iomom,iocosf,ionorm
+ ,iodepo,iomass,ioradi,iomobi
+ ,ioaggl,iomdis,iosdis,iombal
+ ,ioindx,iomom,iocell,iogasp
+ ,iotole,ioacon,ioflow
c
common /iotapes/ columns,ntape4,ntape5,ntape6
integer
columns
c
common /cell/ areaclng,areawall,areafloor
+ ,tempclng,tempwall,tempflor
+ ,volume,leakrate
+ ,hydrdiam,eqvrrough
real
leakrate
c
common /flow/ blflag,vblthick,dblthick(100)
+ ,eddydiss,ustar,reynolds

```

```

chmin 2
chmin 3
chmin 4
chmin 5
chmin 6
chmin 7
chmin 8
chmin 9
chmin 10
chmin 11
collpts2
collpts3
collpts4
chmin 13
aerslco2
aerslco3
aerslco4
aerslco5
aerslco6
chmin 15
gasprop2
gasprop3
gasprop4
gasprop5
gasprop6
gasprop7
chmin 17
indexco2
indexco3
chmin 19
timings2
timings3
timings4
timings5
chmin 21
toleran2
chmin 27
lognorm2
lognorm3
lognorm4
chmin 28
thrahyd2
thrahyd3
thrahyd4
thrahyd5
thrahyd6
thrahyd7
thrahyd8
thrahyd9
thrahyd10
thrahyd11
chmin 27
ioflags2
ioflags3
ioflags4
ioflags5
ioflags6
chmin 29
iotapes2
iotapes3
chmin 31
cell 2
cell 3
cell 4
cell 5
cell 6
chmin 33
flow 2
flow 3

```

```

integer          blflag                                flow  4
c                                                        chmin 35
character*1 input(72)                                chmin 36
c                                                        chmin 37
c Write input file to tapes NTAPE5 & NTAPE6          chmin 38
c *****                                              chmin 39
c                                                        chmin 40
c Tape5 is the terminal and tape6 is the output file.  c  r'n 41
c                                                        'n 42
50 read(ntape4,1000,end=80)(input(i),i=1,72)          c  ' 43
write(ntape5,1000)(input(i),i=1,72)                  chm... 44
write(ntape6,2000)(input(i),i=1,72)                  chmin 45
1000 format(72a1)                                     chmin 46
2000 format(4x,72a1)                                  chmin 47
goto 50                                                chmin 48
60 rewind(ntape4)                                     chmin 49
c                                                        chmin 50
c Read output flags                                    chmin 51
c *****                                              chmin 52
c                                                        chmin 53
c A zero value for a flag means no info. is printed.  chmin 54
c A non-zero value for a flag means print the information. chmin 55
c It will be printed every 10flag times (defined by ISTEP) chmin 56
c when the requested quantity is time dependent.      chmin 57
c                                                        hmin 58
1 read(ntape4,*,err= 1,end=100)iocell,ioga_p,ioacon  chmin 59
2 read(ntape4,*,err= 2,end=100)iosmom,iosdis,ioflow  chmin 60
3 read(ntape4,*,err= 3,end=100)iomass,ioradi,iomobi  chmin 61
23 read(ntape4,*,err=23,end=100)iodepo,ioaggl       chmin 62
4 read(ntape4,*,err= 4,end=100)ioindx,ioccoef,ionorm chmin 63
5 read(ntape4,*,err= 5,end=100)iombal,iotole       chmin 64
6 read(ntape4,*,err= 6,end=100)iozmom,iondis,iomdis  'sin 65
c                                                        cnmin 66
c Read step information.                               chmin 67
c *****                                              chmin 68
c                                                        chmin 69
c This defines the time steps at which information is printed chmin 70
c on the output file. This allows info. to be printed more chmin 71
c frequently when things get interesting.             chmin 72
c                                                        chmin 73
7 read(ntape4,*,err= 7,end=100)ntime                 chmin 74
  if(ntime.gt.20 .or. ntime.le.0)then                 chmin 75
    write(ntape5,2001)                                  chmin 76
    write(ntape6,2001)                                  chmin 77
    stop                                                 chm'n 78
2001 format(4x,'*** CHARMIN fails: NTIME is le 0 or gt 20 ***') chmin 79
    endif                                               chmin 80
8 read(ntape4,*,err= 8,end=100)                       chmin 81
  (timestep(itime),timeend(itime),itime=1,ntime)      chmin 82
c                                                        chmin 83
c Number of columns on output file.                   chmin 34
c *****                                              chmin 85
c                                                        chmin 86
9 read(ntape4,*,err= 9,end=100)columns               chmin 87
  if(columns.ne.80)columns=132                         chmin 88
c                                                        chmin 89
c Read times at which thermal-hydraulic data is provided. chmin 90
c *****                                              chmin 91
c                                                        chmin 92
10 read(ntape4,*,err=10,end=100)ndata                 chmin 93
  if(ndata.gt.20 .or. ndata.le.0)then                 chmin 94
    write(ntape6,2002)                                  chmin 95
    write(ntape6,2002)                                  chmin 96
    stop                                                 chmin 97
2002 format(4x,'*** CHARMIN fails: NDATA is le 0 or gt 20 ***') chmin 98
    endif                                               chmin 99
11 read(ntape4,*,err=11,end=100)                     chmin100
  + (timedata(idata),idata=1,ndata)                   chmin101
c                                                        chmin102

```

```

c      Read how often the thermal hydraulic variables are to be updated. chmin103
c      ***** chmin104
c      chmin105
c      If THHYSTEP = 0 then the thermal-hydraulic variables are updated chmin106
c      during the integration of the ODE's. Otherwise they are updated chmin107
c      every TRHYSTEP seconds. chmin108
c      chmin109
24     read(ntape4,*,err=24,end=100)thhystep chmin110
c      if(thhystep.lt.0.e0)thhystep=0.e0 chmin111
c      chmin112
c      Read cell information. chmin113
c      ***** chmin114
c      chmin115
12     read(ntape4,*,err=12,end=100)areaclng,areawall,areafloor chmin116
13     read(ntape4,*,err=13,end=100) chmin117
+      (tclgdata(idata),twalldata(idata),tflrdata(idata),idata=1,ndata) chmin118
14     read(ntape4,*,err=14,end=100)volume,leakrate chmin119
33     read(ntape4,*,err=33,end=100)hydrdiam,eqvrrough chmin120
c      chmin121
c      Read information about the gas. chmin122
c      ***** chmin123
c      chmin124
15     read(ntape4,*,err=15,end=100) chmin125
+      (tgasdata(idata),pgasdata(idata),vgasdata(idata),idata=1,ndata) chmin126
16     read(ntape4,*,err=16,end=100)molwt,gthrmcon,molwtv chmin127
31     read(ntape4,*,err=31,end=100)vmfrclng,vmfrwall,vmfrflor chmin128
32     read(ntape4,*,err=32,end=100)vcgrclng,vcgrwall,vcgrflor chmin129
c      chmin130
c      Read information about the boundary layer thicknesses chmin131
c      ***** chmin132
c      chmin133
30     read(ntape4,*,err=30,end=100)blflag,vblthick,dblthick(1) chmin134
c      chmin135
c      Read information about the initial aerosol. chmin136
c      ***** chmin137
c      chmin138
c      It is assumed to be log-normal in C(m,t)... chmin139
c      chmin140
25     read(ntape4,*,err=25,end=100)sigmazln,radsozln,mdenzln chmin141
c      chmin142
c      Read information about the aerosol source. chmin143
c      ***** chmin144
c      chmin145
c      This is treated in the same way as the thermal-hydraulic data. chmin146
c      chmin147
17     read(ntape4,*,err=17,end=100) chmin148
+      (sigdata(idata),radsozdata(idata),mdesdata(idata),idata=1,ndata) chmin149
c      chmin150
c      Read information about the collocation points. chmin151
c      ***** chmin152
c      chmin153
c      If NCOLL is zero then it is calculated from SPACING etc. chmin154
c      otherwise the input value of SPACING is ignored. chmin155
c      chmin156
18     read(ntape4,*,err=18,end=100)ncoll,spacing chrmin157
19     read(ntape4,*,err=19,end=100)mlower,mupper chmin158
20     read(ntape4,*,err=20,end=100)nelement chmin159
c      chmin160
c      Read tolerance information. chmin161
c      ***** chmin162
c      chmin163
21     read(ntape4,*,err=21,end=100)eps,maxcalls,maxtrys chmin164
22     read(ntape4,*,err=22,end=100)eta,zeta chmin165
c      chmin166
c      Read new aerosol physics data. chmin167
c      ***** chmin168
c      chmin169
26     read(ntape4,*,err=26,end=100)pdensity,pthrmcon chmin170
27     read(ntape4,*,err=27,end=100)cshepfctr,dshpfctr,stickcoeff chmin171

```

28	read(ntape4,*,err=28,end=100)aknudweb,qknudweb,bknudweb	chmin172
29	read(ntape4,*,err=29,end=100)kbrock,cmbrock,ctbrock	chmin173
	return	chmin174
c		chmin175
c	End of file read - give a warning and carry on	chmin176
c	*****	chmin177
c		chmin178
100	write(ntape5,2003)	chmin179
	write(ntape6,2003)	chmin180
2003	format(4x,'*** CHARMIN warning: end-of-file read - could be'	chmin181
	+, ' an error in the data ***')	chmin182
	return	chmin183
	end	chmin184

```

subroutine charmcol
c
c This subroutine calculates the aerosol particle masses which
c will serve as collocation points in the subsequent calculations.
c
common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ ,radius(100),mass(100),mobility(100)
real
logem0,mass,mobility,mlower,mupper
c
c Set-up parameters which define the collocation points
c *****
c
if(ncoll.eq.0)then
dummy=log(mupper/mlower)/log(spacing)+1.e0
ncoll=int(dummy)
if(float(ncoll).lt.dummy)ncoll=ncoll+1
if(ncoll.gt.100)ncoll=100
else
if(ncoll.gt.100)ncoll=100
spacing=(mupper/mlower)**(1.e0/float(ncoll-1))
endif
mass(1)=mlower
dlogem = log( spacing )
logem0 = log( mass(1) ) - dlogem
c
c Calculate the collocation points
c *****
c
do 100 icoll=2,ncoll
mass(icoll)=mass(icoll-1)*spacing
continue
100 mupper=mass(ncoll)
return
end

```

```

chmcol 2
chmcol 3
chmcol 4
chmcol 5
chmcol 6
collpts2
collpts3
collpts4
chmcol 8
chmcol 9
chmcol10
chmcol11
chmcol12
chmcol13
chmcol14
chmcol15
chmcol16
chmcol17
chmcol18
chmcol19
chmcol20
chmcol21
chmcol22
chmcol23
chmcol24
chmcol25
chmcol26
chmcol27
chmcol28
chmcol29
chmcol30
chmcol31
chmcol32
chmcol33

```



```

subroutine charmind
c
c This subroutine sets-up the indexing to the terms on the rhs.
c For given i and j with 1 <= i <= ncoll and 1 <= j <= i then
c values of k are found such that  $g_k(m_i - m) = g_j(m)$  for  $0 < m < m_i$ 
c is non-zero.
c  $g_j$  and  $g_k$  are the j-th and k-th finite elements and  $m_i$  is the
c mass at the i-th collocation point.
c
c Note that the indexing depends only on i-j (jbar) and i-k (kbar).
c
common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ ,radius(100),mass(100),mobility(100)
real
logem0,mass,mobility,mlower,mupper
c
common /indexco/ nelement,hwidth,jbarmin,index(-2:100)
+ ,kbarmin(-2:100),kbarmax(-2:100),nkbar(-2:100)
c
common /iotapes/ columns,ntape4,ntape5,ntape6
integer
columns
c
c Calculate the element half-width
c *****
c
if(nelement.eq.1)hwidth=0.5e0
if(nelement.eq.2)hwidth=1.e0
if(nelement.eq.3 .or. nelement.eq.4)hwidth=2.e0
if(nelement.eq.5 .or. nelement.eq.6)hwidth=3.e0
c
c Calculate the minimum value of jbar
c *****
c
jbarmin = -int(hwidth)
if(float(jbarmin) .le. -hwidth)jbarmin=jbarmin+1
c
c Calculate indexing for i=ncoll
c *****
c
if(jbarmin.le.ncoll-1)then
do 100 jbar=jbarmin,ncoll-1
sjbar=charfun((jbar+hwidth)*dlogem)/dlogem
kbarmin(jbar) = - int(sjbar+hwidth)
if( kbarmin(jbar)+hwidth .le. -sjbar )
+ kbarmin(jbar) = kbarmin(jbar) + 1
if(kbarmin(jbar).lt.jbarmin)kbarmin(jbar)=jbarmin
if(float(jbar).le.hwidth)then
kbarmax(jbar)=ncoll-1
else
sjbar=charfun((jbar-hwidth)*dlogem)/dlogem
kbarmax(jbar) = - int(sjbar-hwidth)
if( kbarmax(jbar)-hwidth .ge. -sjbar )
+ kbarmax(jbar) = kbarmax(jbar) - 1
if(kbarmax(jbar).gt.ncoll-1)kbarmax(jbar)=ncoll-1
endif
nkbar(jbar) = kbarmax(jbar) - kbarmin(jbar) + 1
if(nkbar(jbar).lt.0)nkbar(jbar)=0
if(jbar.eq.jbarmin)index(jbar)=1
if(jbar.gt.jbarmin)index(jbar)=index(jbar-1) + nkbar(jbar-1)
100 continue
c
c Check number of non-zero values
c *****
c
nonzero = index(ncoll-1) + nkbar(ncoll-1) - 1
index(ncoll)=nonzero
if(nonzero.gt.300)then
write(ntape5,1000)nonzero
write(ntape6,1000)nonzero
1000 format(4x,'*** CHARMIND fails: NONZERO is ',i3,' ***')
c
chmind 2
chmind 3
chmind 4
chmind 5
chmind 6
chmind 7
chmind 8
chmind 9
chmind10
chmind11
chmind12
collpts2
collpts3
collpts4
chmind14
indexco2
indexco3
chmind16
iotapes2
iotapes3
chmind18
chmind19
chmind20
chmind21
chmind22
chmind23
chmind24
chmind25
chmind26
chmind27
chmind28
chmind29
chmind30
chmind31
chmind32
chmind33
chmind34
chmind35
chmind36
chmind37
chmind38
chmind39
chmind40
chmind41
chmind42
chmind43
chmind44
chmind45
chmind46
chmind47
chmind48
chmind49
chmind50
chmind51
chmind52
chmind53
chmind54
chmind55
chmind56
chmind57
chmind58
chmind59
chmind60
chmind61
chmind62
chmind63
chmind64
chmind65
chmind66

```

```

        stop
        endif
c
c Translate index with respect to kbarmin
c *****
c
do 110 jbar=jbarmin,ncoll-1
index(jbar)=index(jbar)-kbarmin(jbar)
110 continue
endif
return
end

```

```

chmind67
chmind68
chmind69
chmind70
chmind71
chmind72
chmind73
chmind74
chmind75
chmind76
chmind77
chmind78

```

```

function charmfun(x)
c
c This function subroutine calculates the function alog(1.-exp(-x)).
c A series expansion is used when x is >= alog(10.) or x <= .1
c to avoid rounding errors.
c
c dimension term(14)
c data cutoff/0.1e0/
c
c Switch-off vectorization and expand the exponential if x is < .1
c .....
c
c$dir novector
if(x.lt.cutoff)then
  term(1)=x
  do 30 i=2,14
  term(i)=-term(i-1)*x/float(i)
30 continue
  sum=0.e0
  do 40 i=14,1,-1
  sum=sum+term(i)
40 continue
  charmfun=alog(sum)
else
c
c Expand the logarithm if x is large enough ie if y = exp(-x) < .1
c .....
c
  y=exp(-x)
  if(.gt.cutoff)then
    term(1)=y
    do 10 i=2,14
    term(i)=term(i-1)*y
10 continue
    sum=0.e0
    do 20 i=14,1,-1
    sum=sum+term(i)/float(i)
20 continue
    charmfun=-sum
  else
c
c Use standard functions and switch-on vectorization
c .....
c
    charmfun=alog(1.e0-y)
  endif
endif
c$dir vector
return
end

```

```

charmfun 2
charmfun 3
charmfun 4
charmfun 5
charmfun 6
charmfun 7
charmfun 8
charmfun 9
charmfun10
charmfun11
charmfun12
charmfun13
charmfun14
charmfun15
charmfun16
charmfun17
charmfun18
charmfun19
charmfun20
charmfun21
charmfun22
charmfun23
charmfun24
charmfun25
charmfun26
charmfun27
charmfun28
charmfun29
charmfun30
charmfun31
charmfun32
charmfun33
charmfun34
charmfun35
charmfun36
charmfun37
charmfun38
charmfun39
charmfun40
charmfun41
charmfun42
charmfun43
charmfun44
charmfun45
charmfun46
charmfun47
charmfun48
charmfun49
charmfun50
charmfun51

```

```

c      subroutine charmcoe                                     chmcoe 2
c      This subroutine calculates all non-zero values of the integral of gk(mi-m) * gj(m) w.r.t. loge(m) for the range 0 < m < mi. chmcoe 3
c      These depend only on i-j and i-k and are stored using the indexing developed in charmind. chmcoe 4
c      chmcoe 5
c      chmcoe 6
c      chmcoe 7
c      chmcoe 8
c      common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0 collpts2
+      radius(100),mass(100),mobility(100) collpts3
c      *er.l logem0,mass,mobility,mlower,mupper collpts4
c      chmcoe10
c      common /indexcoe/ nelement,hwidth,jbarmin,index(-2:100) indexco2
+      ,kbarmin(-2:100),kbarmax(-2:100),nkbar(-2:100) indexco3
c      chmcoe12
c      common /coef/ pijk(300),njk(100,100) coef 2
c      real njk coef 3
c      chmcoe14
c      common /toleranc/ eps,eta,zeta,maxcalls,maxtrys toleran2
c      chmcoe16
c      common /jandkbar/ jbar,kbar jandkba2
c      chmcoe18
c      common /iotapes/ columns,ntape4,ntape5,ntape6 iotapes2
c      integer columns iotapes3
c      chmcoe20
c      dimension xlimit(14),dummy(14) chmcoe21
c      external charmpjk chmcoe22
c      Set all pijk to zero chmcoe23
c      ***** chmcoe24
c      chmcoe25
c      chmcoe26
c      do 150 ind=1,300 chmcoe27
c      pijk(ind)=0.e0 chmcoe28
150 continue chmcoe29
c      chmcoe30
c      Calculate all non-zero values of pijk chmcoe31
c      ***** chmcoe32
c      chmcoe33
c      i=ncoll chmcoe34
c      if(i-jbarmin.ge.1)then chmcoe35
c      do 210 j=1,-jbarmin chmcoe36
c      jbar=i-j chmcoe37
c      if(nkbar(jbar).ne.0)then chmcoe38
c      do 220 kbar=kbarmin(jbar),kbarmax(jbar) chmcoe39
c      k=i-kbar chmcoe40
c      chmcoe41
c      Find integration range chmcoe42
c      ***** chmcoe43
c      chmcoe44
c      if(kbar-hwidth.le.0.e0)then chmcoe45
c      ylower=-hwidth-jbar chmcoe46
c      else chmcoe47
c      ylower=max(-hwidth-jbar, charmfun((kbar-hwidth)*dlogem)/dlogem) chmcoe48
c      endif chmcoe49
c      yupper=min( hwidth-jbar, charmfun((kbar+hwidth)*dlogem)/dlogem chmcoe50
+      ,0.e0 ) chmcoe51
c      if(ylower.ge.yupper)then chmcoe52
c      write(ntape5,1000) chmcoe53
c      write(ntape5,1000) chmcoe54
1000 format(4x,'*** CHARMCOE fails: YLOWER is ge YUPPER ***') chmcoe55
c      stop chmcoe56
c      endif chmcoe57
c      chmcoe58
c      No need for sub-ranges if NELEMENT = 1 chmcoe59
c      ***** chmcoe60
c      chmcoe61
c      if(nelement.eq.1)then chmcoe62
c      call gaus8(charmpjk,ylower,yupper,eps,answer,ierror) chmcoe63
c      if(ierror.ne.1)then chmcoe64
c      write(ntape5,1010)ierror chmcoe65

```

```

        write(ntape6,1010)ierror
1010    format(4x,'*** CHARMCGE warning: IERROR is ',i2,' ***')
        endif
        pijk(index(jbar)+kbar)=answer
        else
c
c      Split integration range into sub-ranges
c      *****
c
        nlimit=2*int(hwidth)+1
        do 50 klimit=1,nlimit
        ylimit=-hwidth+float(klimit-1)
        xlimit(nlimit+klimit)=ylimit-jbar
        if(kbar+ylimit.gt.C.e0)then
            xlimit(klimit)=charmfun((kbar+ylimit)*dlogem)/dlogem
        else
            xlimit(klimit)=-hwidth-jbar
        endif
50    continue
        call sort(xlimit,dummy,2*nlimit,1)
c
c      Integrate between successive limits
c      *****
c
        sum=0.e0
        do 100 klimit=1,2*nlimit-1
        xlower=xlimit(klimit)
        xupper=xlimit(klimit+1)
        if(
+      xlower.lt.xupper
+      .and. xlower.ge.ylower
+      .and. xupper.le.yupper )then
            call gauss8(charmpjk,xlower,xupper,eps,answer,ierror)
            if(ierror.ne.1)then
                write(ntape6,1010)ierror
                write(ntape6,1010)ierror
            endif
            sum = sum + answer
        endif
100    continue
        pijk(index(jbar)+kbar)=sum
        endif
220    continue
        endif
210    continue
        endif
        return
        end

```

```

chmcoe86
chmcoe87
chmcoe88
chmcoe89
chmcoe70
chmcoe71
chmcoe72
chmcoe73
chmcoe74
chmcoe75
chmcoe76
chmcoe77
chmcoe78
chmcoe79
chmcoe80
chmcoe81
chmcoe82
chmcoe83
chmcoe84
chmcoe85
chmcoe86
chmcoe87
chmcoe88
chmcoe89
chmcoe90
chmcoe91
chmcoe92
chmcoe93
chmcoe94
chmcoe95
chmcoe96
chmcoe97
chmcoe98
chmcoe99
chmco100
chmco101
chmco102
chmco103
chmco104
chmco105
chmco106
chmco107
chmco108
chmco109
chmco110
chmco111
chmco112

```

c	function charmpjk(arg)	chmpjk 2
c	This function subroutine calculates the integrand in the	chmpjk 3
c	integral required for the production coefficient.	chmpjk 4
c		chmpjk 5
	common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0	chmpjk 6
	+ ,radius(100),mass(100),mobility(100)	collpts2
	real logem0,mass,mobility,mlower,mupper	collpts3
c		collpts4
	common /jandkbar/ jbar,kbar	chmpjk 8
c		jandkba2
	charmpjk = charmfe(dble(arg)+jbar,0)	chmpjk10
	+ charmfe(dble(charmfun(-arg*dlogem)/dlogem)+kbar,0)	chmpjk11
	return	chmpjk12
	end	chmpjk13
		chmpjk14

```

function charmfe(arg,k)
c
c This function subroutine calculates the value of one from a
c choice of several finite elements at ARG. The elements
c herein calculated are centered with respect to ARG=0, are
c symmetric and have unit spacing. ARG is therefore scaled
c by the collocation interval (the points are equally spaced)
c and translated, assuming the argument to be mass.
c i.e. for the k-th element the following transformation is
c performed: x = (loge(m) - loge(m0))/dlogem - k.
c The transformation is not done when k = 0.
c
c The choice of element is determined by NELEMENT
c
c double precision arg,x,y,z
c
c common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ ,radius(100),mass(100),mobility(100)
c real logem0,mass,mobility,mlower,mupper
c
c common /indexcoe/ nelement,hwidth,jbarmin,index(-2:100)
+ ,kbarmin(-2:100),kbarmax(-2:100),nkbar(-2:100)
c
c Transform the argument and select an element
c *****
c
c charmfe = 0.e0
c if(k.eq.0) x = abs( arg )
c if(k.ne.0) x = abs( (log(arg) - logem0)/dlogem - k )
c goto(1,2,3,4,5,6)nelement
c
c First order element
c *****
c
c continue
c 1 if(x.le.0.5d0)charmfe=1.e0
c return
c
c Second order element
c *****
c
c 2 continue
c if(x.lt.1.d0)charmfe=1.d0-x
c return
c
c Third order element
c *****
c
c 3 continue
c y=2.d0-x
c if(x.lt.2.d0 .and. x.gt.1.d0)
+ charmfe=(1.d0-x)*y+y/2.d0
c if(x.lt.1.d0)
+ charmfe=(2.d0-5.d0*x+x+3.d0*x*x*x)/2.d0
c return
c
c Fourth order element
c *****
c
c 4 continue
c y=2.d0-x
c if(x.lt.2.d0 .and. x.gt.1.d0)
+ charmfe=-(1.d0-x)*y+y*y+(1.d0-2.d0*x)/2.d0
c if(x.lt.1.d0)
+ charmfe=(1.d0-x)*(1.d0+x-4.5e0*x*x*x+3.d0*x*x*x*x)
c return
c
c Fifth order element
c *****
c

```

```

charmfe 2
charmfe 3
charmfe 4
charmfe 5
charmfe 6
charmfe 7
charmfe 8
charmfe 9
charmfe 10
charmfe 11
charmfe 12
charmfe 13
charmfe 14
charmfe 15
charmfe 16
charmfe 17
collpts2
collpts3
collpts4
charmfe 19
indexco2
indexco3
charmfe 21
charmfe 22
charmfe 23
charmfe 24
charmfe 25
charmfe 26
charmfe 27
charmfe 28
charmfe 29
charmfe 30
charmfe 31
charmfe 32
charmfe 33
charmfe 34
charmfe 35
charmfe 36
charmfe 37
charmfe 38
charmfe 39
charmfe 40
charmfe 41
charmfe 42
charmfe 43
charmfe 44
charmfe 45
charmfe 46
charmfe 47
charmfe 48
charmfe 49
charmfe 50
charmfe 51
charmfe 52
charmfe 53
charmfe 54
charmfe 55
charmfe 56
charmfe 57
charmfe 58
charmfe 59
charmfe 60
charmfe 61
charmfe 62
charmfe 63
charmfe 64
charmfe 65
charmfe 66
charmfe 67

```

c		chmfe 68
5	continue	chmfe 69
	y=2.d0-x	chmfe 70
	z=3.d0-x	chmfe 71
	if(x.lt.3.d0 .and. x.gt.2.d0)	chmfe 72
+	charmfe=y*y*y*z*z*z/12.d0	chmfe 73
	if(x.lt.2.d0 .and. x.gt.1.d0)	chmfe 74
+	charmfe=-y*y*y*(1.d0-x)	chmfe 75
+	*(1.d0-61.d0*y+89.d0*y*y-35.d0*y*y*y)/12.d0	chmfe 76
	if(x.lt.1.d0)	chmfe 77
+	charmfe=1.d0-x*x-91.d0*x*x*x/8.d0	chmfe 78
+	+38.d0*x*x*x*x-32.d0*x*x*x*x*x+55.d0*x*x*x*x*x*x/6.d0	chmfe 79
	return	chmfe 80
c		chmfe 81
c	Sixth order element	chmfe 82
c	*****	chmfe 83
c		chmfe 84
6	continue	chmfe 85
	y=2.d0-x	chmfe 86
	z=3.d0-x	chmfe 87
	if(x.lt.3.d0 .and. x.gt.2.d0)	chmfe 88
+	charmfe=-z*z*z*z*z*y*y*y*(18.d0-9.d0*x)/24.d0	chmfe 89
	if(x.lt.2.d0 .and. x.gt.1.d0)	chmfe 90
+	charmfe=-y*y*y*(1.d0-x)*(2.d0+3.d0*y-432.d0*y*y	chmfe 91
+	+1010.d0*y*y*y-830.d0*y*y*y*y+235.d0*y*y*y*y*y)/24.d0	chmfe 92
	if(x.lt.1.d0)	chmfe 93
+	charmfe=(12.d0-12.d0*x*x+3.d0*x*x*x*x-659.d0*x*x*x*x*x	chmfe 94
+	+2226.d0*x*x*x*x*x*x-2880.d0*x*x*x*x*x*x*x	chmfe 95
+	+1685.d0*x*x*x*x*x*x*x*x-375.d0*x*x*x*x*x*x*x*x*x)/12.d0	chmfe 96
	return	chmfe 97
	end	chmfe 98



```

subroutine charnor                                     charnor 2
c                                                     charnor 3
c This subroutine calculates a normalization for the agglomeration charnor 4
c terms which guarantees mass conservation.          charnor 5
c The production term must be multiplied by the normalization if charnor 6
c it is non-zero, otherwise the corresponding destruction term charnor 7
c must be set to zero.                               charnor 8
c                                                     charnor 9
c common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0 charnor10
+ ,radius(100),mass(100),mobility(100)             collpts2
c real                                               collpts3
+ logem0,mass,mobility,mlower,mupper              collpts4
c                                                     charnor11
c common /indexcoe/ nelement,hwidth,jbarmin,index(-2:100) charnor12
+ ,kbarmin(-2:100),kbarmax(-2:100),nkbar(-2:100)  indexco2
c                                                     charnor13
c common /coef/ pijk(300),njc(100,100)             coef 2
c real                                               coef 3
+ njk                                             charnor15
c                                                     charnor16
c Loop over j and k: the normalization is symmetric so k <= j. charnor17
c .....                                           charnor18
c                                                     charnor19
c do 100 j=1,ncoll                                  charnor20
c do 200 k=1,j                                      charnor21
c sum=0.e0                                         charnor22
c do 300 i=1,ncoll                                  charnor23
c jbar=i-j                                         charnor24
c kbar=i-k                                         charnor25
c                                                     charnor26
c Extract Pijk                                     charnor27
c .....                                           charnor28
c                                                     charnor29
c cijk=0.e0                                        charnor30
c   if(jbar.ge.jbarmin)then                        charnor31
c     if(kbar.ge.kbarmin(jbar) .and. kbar.le.kbarmax(jbar)) charnor32
+   cijk=pijk(index(jbar)+kbar)                   charnor33
c   endif                                          charnor34
c                                                     charnor35
c Extract Pijk                                     charnor36
c .....                                           charnor37
c                                                     charnor38
c cikj=0.e0                                        charnor39
c   if(kbar.ge.jbarmin)then                        charnor40
c     if(jbar.ge.kbarmin(kbar) .and. jbar.le.kbarmax(kbar)) charnor41
+   cikj=pijk(index(kbar)+jbar)                   charnor42
c   endif                                          charnor43
c                                                     charnor44
c Add to the normalization sum                     charnor45
c .....                                           charnor46
c                                                     charnor47
c sum = sum + mass(i) * ( cijk + cikj )           charnor48
300 continue                                       charnor49
c                                                     charnor50
c Calculate the normalization                      charnor51
c .....                                           charnor52
c                                                     charnor53
c if(sum.eq.0.e0)njc(j,k)=0.e0                    charnor54
c if(sum.ne.0.e0)njc(j,k)=(mass(j)+mass(k))/sum   charnor55
c njc(k,j)=njc(j,k)                               charnor56
200 continue                                       charnor57
100 continue                                       charnor58
c return                                           charnor59
c end

```

```

subroutine charmrad
c
c This subroutine calculates particle radii at the collocation
c points.
c
common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ ,radius(100),mass(100),mobility(100)
real logem0,mass,mobility,mlower,mupper
c
common /aerslcon/ cshpfctr,dshpfctr,stickeff
+ ,aknudweb,qknudweb,bknudweb
+ ,pdensity,pthrmcon
+ ,kbrock,cmbrock,etbrock
real kbrock
c
common /fundcon/ pi,boltzmn,gravitat,gasconst
c
c The radius defined here is an equivalent radius, which is the
c radius of a spherical particle of equal mass. Non-sphericity is
c taken into account via correction factors (called shape factors).
c
factor = 4.e0 * pi * pdensity / 3.e0
do 100 icoll=1,ncoll
radius(icoll) = ( mass(icoll) / factor )**(1.e0/3.e0)
100 continue
return
end

```

```

chrad 2
chrad 3
chrad 4
chrad 5
chrad 6
collpts2
collpts3
collpts4
chrad 8
aerslco2
aerslco3
aerslco4
aerslco5
aerslco6
chrad10
fundcon2
chrad12
chrad13
chrad14
chrad15
chrad16
chrad17
chrad18
chrad19
chrad20
chrad21
chrad22

```



end

line63

```

subroutine charmith
c
c This subroutine translates the data for the time dependent
c variables into a form which can be used by CHARMUTH.
c It is assumed that the times for the data points are in
c non-decreasing order. Consecutive times can be equal to allow the
c variables to change discontinuously.
c The interpolation formulae are of the form: a0 + a1 * time.
c a1 is zero (i.e. constant extrapolation is used) when TIME lies
c outside the range of the times of the data.
c
common /timings/ time,istep,thhystep
+ ,itime,ntime,timestep(20),timeend(20)
+ ,ithhy,nthhy,timethhy(20)
+ ,idata,ndata,timedata(20)
c
common /thrmhydr/ tgasao(20),tgasal(20),tgasdata(20)
+ ,pgasao(20),pgasal(20),pgasdata(20)
+ ,vgasao(20),vgasal(20),vgasdata(20)
+ ,tclgao(20),tclgal(20),tclgdata(20)
+ ,twalao(20),twalal(20),twaldata(20)
+ ,tflrao(20),tflral(20),tflrdata(20)
+ ,sigasao(20),sigasal(20),sigasdata(20)
+ ,radasao(20),radasal(20),radasdata(20)
+ ,mdesao(20),mdesal(20),mdesdata(20)
real
mdesao,mdesal,mdesdata
c
c Find the end-point times for each set of formulae
c .....
c
ithhy=0
do 10 idata=1,ndata
  if( ithhy.ne.0
+ .and. timedata(idata).gt.timethhy(ithhy)
+ .and. timethhy(ithhy).lt.timeend(ntime)) then
    ithhy=ithhy+1
    timethhy(ithhy)=timedata(idata)
  endif
  if(ithhy.eq.0 .and. timedata(idata).gt.0.e0) then
    ithhy=1
    timethhy(1)=timedata(idata)
  endif
10 continue
  if(ithhy.eq.0 .or. ndata.eq.1) then
    nthhy=1
    timethhy(1)=timeend(ntime)
  else
    if(timethhy(ithhy).ge.timeend(ntime)) then
      nthhy=ithhy
    else
      nthhy=ithhy+1
      timethhy(nthhy)=timeend(ntime)
    endif
  endif
c
c Calculate a0 and a1 for the time dependent variables
c .....
c
call charmwith(tgasao,tgasal,tgasdata)
call charmwith(pgasao,pgasal,pgasdata)
call charmwith(vgasao,vgasal,vgasdata)
call charmwith(tclgao,tclgal,tclgdata)
call charmwith(twalao,twalal,twaldata)
call charmwith(tflrao,tflral,tflrdata)
call charmwith(sigasao,sigasal,sigasdata)
call charmwith(radasao,radasal,radasdata)
call charmwith(mdesao,mdesal,mdesdata)
return
end

```

```

subroutine charmwth(a0,a1,xdata)
c
c This subroutine calculates the interpolation coefficients
c a0 and a1 from the data table XDATA.
c
common /timings/  time,istep,thhystep
+                ,itime,ntime,timestep(20),timeend(20)
+                ,ithhy,nthhy,timethhy(20)
+                ,idata,ndata,timedata(20)
c
dimension a0(100),a1(100),xdata(100)
c
Special case when NDATA = 1
*****
c
if(ndata.eq.1)then
a0(1)=xdata(1)
a1(1)=0.e0
return
endif
c
Copy data points when insufficient supplied
*****
c
if(ndata.gt.1)then
do 5 idata=2,ndata
if(xdata(idata).lt.0.e0)xdata(idata)=xdata(idata-1)
continue
5
endif
c
Set-up interpolation formulae when NDATA > 1
*****
c
ithhy=1
do 10 idata=1,ndata
if(ithhy.le.nthhy)then
if(timedata(idata).eq.timethhy(ithhy))then
if(idata.eq.1)then
a0(1)=xdata(1)
a1(1)=0.e0
else
a0(ithhy)=( xdata(idata-1)*timedata(idata)
+          - xdata(idata)*timedata(idata-1) )
+          / ( timedata(idata) - timedata(idata-1) )
a1(ithhy)=( xdata(idata) - xdata(idata-1) )
+          / ( timedata(idata) - timedata(idata-1) )
endif
ithhy=ithhy+1
endif
endif
10
continue
if(timedata(ndata).lt.timethhy(nthhy))then
a0(nthhy)=xdata(ndata)
a1(nthhy)=0.e0
endif
return
end

```

```

chmwth 2
chmwth 3
chmwth 4
chmwth 5
chmwth 6
timings2
timings3
timings4
timings5
chmwth 8
chmwth 9
chmwth10
chmwth11
chmwth12
chmwth13
chmwth14
chmwth15
chmwth16
chmwth17
chmwth18
chmwth19
chmwth20
chmwth21
chmwth22
chmwth23
chmwth24
chmwth25
chmwth26
chmwth27
chmwth28
chmwth29
chmwth30
chmwth31
chmwth32
chmwth33
chmwth34
chmwth35
chmwth36
chmwth37
chmwth38
chmwth39
chmwth40
chmwth41
chmwth42
chmwth43
chmwth44
chmwth45
chmwth46
chmwth47
chmwth48
chmwth49
chmwth50
chmwth51
chmwth52
chmwth53
chmwth54
chmwth55

```

```

subroutine charmuth(timemean)
c
c This subroutine updates the thermal-hydraulic data at time
c TIMEMEAN using the interpolation formulae calculated previously.
c
common /timings/ time,istep,thhystep
+ ,itime,ntime,timestep(20),timeend(20)
+ ,ithhy,nthhy,timethhy(20)
+ ,idata,ndata,timedata(20)
c
common /thrmhydr/ tgasao(20),tgasal(20),tgasdata(20)
+ ,pgasao(20),pgasal(20),pgasdata(20)
+ ,vgasao(20),vgasal(20),vgasdata(20)
+ ,tclgaO(20),tclgal(20),tclgdata(20)
+ ,twalaO(20),twalal(20),twaldata(20)
+ ,tflraO(20),tflral(20),tflrdata(20)
+ ,sigasO(20),sigasal(20),sigasdata(20)
+ ,radesaO(20),radesal(20),radesdata(20)
+ ,mdesaO(20),mdesal(20),mdesdata(20)
real
mdesaO,mdesal,mdesdata
c
common /gasprops/ temp,press,gdensity,dynvisc,molwt,mnfrpath
+ ,gthrmcon,velocity,molwtv,diffusv
+ ,vmfrclng,vmfrwall,vmfrflor
+ ,vcgrclng,vcgrwall,vcgrflor
+ ,vconclng,vconwall,vconflor
real
molwt,mnfrpath,molwtv
c
common /cell/ areaclng,areawall,areaflor
+ ,tempclng,tempwall,tempflor
+ ,volume,leakrate
+ ,hydrdiam,eqvrrough
real
leakrate
c
common /lognorms/ sigmasln,rad50sln,mdensln
+ ,ndensln,geomsln,mas50sln
real
mdensln,ndensln,mas50sln
c
temp = tgasao(ithhy) + tgasal(ithhy) * timemean
press = pgasao(ithhy) + pgasal(ithhy) * timemean
velocity = vgasao(ithhy) + vgasal(ithhy) * timemean
tempclng = tclgaO(ithhy) + tclgal(ithhy) * timemean
tempwall = twalaO(ithhy) + twalal(ithhy) * timemean
tempflor = tflraO(ithhy) + tflral(ithhy) * timemean
sigmasln = sigasO(ithhy) + sigasal(ithhy) * timemean
rad50sln = radesaO(ithhy) + radesal(ithhy) * timemean
mdensln = mdesaO(ithhy) + mdesal(ithhy) * timemean
return
end

```

```

chmuth 2
chmuth 3
chmuth 4
chmuth 5
chmuth 6
timings2
timings3
timings4
timings5
chmuth 8
thrmhyd2
thrmhyd3
thrmhyd4
thrmhyd5
thrmhyd6
thrmhyd7
thrmhyd8
thrmhyd9
thrmhyd10
thrmhyd11
gasprop2
gasprop3
gasprop4
gasprop5
gasprop6
gasprop7
chmuth12
cell 2
cell 3
cell 4
cell 5
cell 6
chmuth14
lognorm2
lognorm3
lognorm4
chmuth16
chmuth17
chmuth18
chmuth19
chmuth20
chmuth21
chmuth22
chmuth23
chmuth24
chmuth25
chmuth26
chmuth27

```

```

subroutine charngas
c
c This subroutine calculates properties of the gas from its
c temperature, pressure and molecular weight.
c The formulae are those used in MAEROS.
c
common /gasprops/ temp,press,gdensity,dynvisc,molwt,mnfrpath
+ ,gthrmcon,velocity,molwtv,diffusv
+ ,vmfrclng,vmfrwall,vmfrflor
+ ,vcgrclng,vcgrwall,vcgrflor
+ ,vconclng,vconwall,vconflor
real
molwt,mnfrpath,molwtv
c
common /cell/ areaclng,areawall,areaflor
+ ,tempclng,tempwall,tempflor
+ ,volume,leakrate
+ ,hydrdiam,eqvrrough
real
leakrate
c
common /fundcon/ pi,boltzmnn,gravitat,gasconst
c
data dynviscr,temp1/15.85e-6,114.e0/
data diffusvr,temp2,pressr/2.11e-5,273.15e0,1.01325e5/
c
Density: the molecular weight has units = kgm/kmol.
*****
c
gdensity = press * molwt / ( 1.e3 * gasconst * temp )
c
Dynamic viscosity
*****
c
dynvisc = dynviscr * (temp/temp1)**1.5e0 *1.e0/(1.e0+temp/temp1)
c
Mean free path
*****
c
mnfrpath = dynvisc * sqrt(pi/(2.e0*press*gdensity))
c
Diffusivity of water vapor in air
*****
c
diffusv = diffusvr * (pressr/press) * (temp/temp2)**1.94
c
Vapor density near surfaces
*****
c
The molecular weight has units = kgm/kmol.
c
vconclng = press*molwtv*vmfrclng / ( 1.e3*gasconst*tempclng )
vconwall = press*molwtv*vmfrwall / ( 1.e3*gasconst*tempwall )
vconflor = press*molwtv*vmfrflor / ( 1.e3*gasconst*tempflor )
return
end

```

```

chngas 2
chngas 3
chngas 4
chngas 5
chngas 6
chngas 7
gasprop2
gasprop3
gasprop4
gasprop5
gasprop6
gasprop7
chngas 9
cell 2
cell 3
cell 4
cell 5
cell 6
chngas11
fundcon2
chngas13
chngas14
chngas15
chngas16
chngas17
chngas18
chngas19
chngas20
chngas21
chngas22
chngas23
chngas24
chngas26
chngas27
chngas28
chngas29
chngas30
chngas31
chngas32
chngas33
chngas34
chngas35
chngas36
chngas37
chngas38
chngas39
chngas40
chngas41
chngas42
chngas43
chngas44
chngas45
chngas46

```



```

c      subroutine charmmob                                chmmob 2
c      This subroutine calculates particle mobilities at the collocation points using the MAEROS formula.  chmmob 3
c      chmmob 4
c      chmmob 5
c      chmmob 6
c      common /collpts/  ncoll,mlower,mupper,spacing,dlogen,logem0 collpts2
+      ,radius(100),mass(100),mobility(100) collpts3
c      real      logem0,mass,mobility,mlower,mupper collpts4
c      chmmob 8
c      common /aerslcon/  cshpfctr,dshpfctr,stickcoeff aerslco2
+      ,aknudweb,qknudweb,bknudweb aerslco3
+      ,pdensity,pthrmcon aerslco4
+      ,kbrock,cmbrock,ctbrock aerslco5
c      real      kbrock aerslco6
c      chmmob10
c      common /gasprop/  temp,press,gdensity,dynvisc,molwt,mnfrpath gasprop2
+      ,gthrmcon,velocity,molwtv,diffusv gasprop3
+      ,vmfrclng,vmfrwall,vmfrflor gasprop4
+      ,vcgrclng,vcgrwall,vcgrflor gasprop5
+      ,vconclng,vconwall,vconflor gasprop6
c      real      molwt,mnfrpath,molwtv gasprop7
c      chmmob12
c      common /fundcon/  pi,boltzmann,gravitat,gasconst fundcon2
c      chmmob14
c      chmmob15
c      chmmob16
c      do 100 icoll=1,ncoll chmmob17
c      Stoke's law mobility chmmob18
c      ***** chmmob19
c      stokes = 1.e0/(8.e0*pi*dshpfctr*dynvisc*radius(icoll)) chmmob20
c      chmmob21
c      Cunningham slip correction chmmob22
c      ***** chmmob23
c      chmmob24
c      r1 = radius(icoll)/mnfrpath chmmob25
c      cunning = 1.e0 + aknudweb/r1 chmmob26
+      + qknudweb/r1*exp(-min(bknudweb*r1,100.e0)) chmmob27
c      chmmob28
c      chmmob29
c      chmmob30
c      Combine the two factors chmmob31
c      ***** chmmob32
c      chmmob33
c      mobility(icoll) = stokes * cunning chmmob34
100 continue chmmob35
c      return chmmob36
c      end chmmob37

```

```

subroutine charmflo
c
c This subroutine calculates flow properties which are needed
c for the calculation of deposition velocities and
c agglomeration rates.
c
common /gasprops/ temp,press,gdensity,dynvisc,molwt,mnfrpath
+ ,gthrmcon,velocity,molwtv,diffusv
+ ,vmfrclng,vmfrwall,vmfrflor
+ ,vcgrclng,vcgrwall,vcgrflor
+ ,vconclng,vconwall,vconflor
real
molwt,mnfrpath,molwtv
c
common /fundcon/ pi,boltzmnn,gravitat,gasconst
c
common /collpts/ ncoll,mlower,supper,spacing,dlogen,logem0
+ ,radius(100),mass(100),mobility(100)
real
logem0,mass,mobility,mlower,supper
c
common /cell/ areaclng,areawall,areaflor
+ ,tempclng,tempwall,tempflor
+ ,volume,leakrate
+ ,hydrdiam,eqvrrough
real
leakrate
c
common /flow/ blflag,vblthick,dblthick(100)
+ ,eddydiss,ustar,reynolds
integer
blflag
c
common /toleranc/ eps,eta,zeta,maxcalls,maxtrys
c
common /iotapes/ columns,ntape4,ntape5,ntape6
integer
columns
c
real kt
real kinvisc
logical firstgo
data firstgo/.true./
data reyncut/2300.e0/
external charmfan
c
kt = boltzmnn*temp
c
Friction velocity
c
*****
c
The formulae are from Schlichting. They are for a pipe of any
c roughness - the roughness required by the correlation is the
c equivalent sand roughness as first used by Nikuradse. The
c hydraulic diameter is 4 * the flow area / the wetted perimeter.
c This equals the pipe diameter for cylindrical pipes but enables
c the correlation to be used for other cross-sectional shapes.
c
kinvisc=dynvisc/gdensity
reynolds=velocity*hydrdiam/kinvisc
if(reynolds.lt.reyncut)then
ustar=0.e0
else
ifail = 1
flower = 1.e-10
fupper = 1.e0
rtol = eps
stol = eta
stol = zeta
ncalls = maxcalls
call cOSwhe
+ (flower,fupper,rtol,stol,charmfan,ncalls,stol,fanning,ifail)
if(ifail.ne.0)then
write(ntape5,1000)ifail

```

```

chmflo 2
chmflo 3
chmflo 4
chmflo 5
chmflo 6
chmflo 7
gasprop2
gasprop3
gasprop4
gaspro
gaspro
gasprop7
chmflo 9
fundcon2
chmflo11
collpts2
collpts3
collpts4
chmflo13
cell 2
cell 3
cell 4
cell 5
cell 6
chmflo15
flow 2
flow 3
flow 4
chmflo17
toleran2
chmflo19
iotapes2
iotapes3
chmflo21
chmflo22
chmflo23
chmflo24
chmflo25
chmflo26
chmflo27
chmflo28
chmflo29
chmflo30
chmflo31
chmflo32
chmflo33
chmflo34
chmflo35
chmflo36
chmflo37
chmflo38
chmflo39
chmflo40
chmflo41
chmflo42
chmflo43
chmflo44
chmflo45
chmflo46
chmflo47
chmflo48
chmflo49
chmflo50
chmflo51
chmflo52
chmflo53
chmflo54
chmflo55
chmflo56

```

```

1000      write(ntape8,1000)ifail
        format(4x,'*** CHARMFLO fails: IFAIL is ',i2,' ***')
        stop
        endif
        ustar = velocity * sqrt(fanning/2.e0)
        endif
c
c      Eddy dissipation rate
c      *****
c
c      The eddy dissipation rate is calculated by assuming all the energy
c      consumed by shear stresses at the walls is dissipated by turbulence
c
c      if(hydrdiam.eq.0.e0)then
        eddydiss=0.e0
      else
        eddydiss=4.e0*velocity*ustar*ustar/hydrdiam
      endif
c
c      Viscous boundary layer thickness
c      *****
c
c      if(blflag.eq.0)then
        if(ustar.eq.0.e0)then
          vblthick=0.e0
        else
          vblthick=kinvisc/ustar
        endif
      endif
c
c      Diffusion boundary layer thickness
c      *****
c
c      The diffusion boundary layer thickness is an input data item
c      or else defaults to 1.e-5 in MAEROS.
c
c      Here it is calculated from the viscous boundary layer
c      thickness using the Keller (1973) formula.
c
c      if(blflag.eq.0)then
        do 10 icoll=1,ncoll
          schmidt = kinvisc/(kt*sobility(icoll))
          dblthick(icoll) = vblthick / schmidt**(1.e0/3.e0)
        continue
      10  else
        if(firstgo)then
          firstgo = .false.
          do 20 icoll=1,ncoll
            dblthick(icoll)=dblthick(1)
          continue
        20  endif
      endif
      return
      end

```

```

chmflo57
chmflo58
chmflo59
chmflo60
chmflo61
chmflo62
chmflo63
chmflo64
chmflo65
chmflo66
chmflo67
chmflo68
chmflo69
chmflo70
chmflo71
chmflo72
chmflo73
chmflo74
chmflo75
chmflo76
chmflo76
chmflo77
chmflo78
chmflo79
chmflo80
chmflo81
chmflo82
chmflo83
chmflo84
chmflo85
chmflo86
chmflo87
chmflo88
chmflo89
chmflo90
chmflo91
chmflo92
chmflo93
chmflo94
chmflo95
chmflo96
chmflo97
chmflo98
chmflo99
chmf1100
chmf1101
chmf1102
chmf1103
chmf1104
chmf1105
chmf1106
chmf1107
chmf1108
chmf1109
chmf1110

```

```

subroutine c05whe(xl,xu,eps,eta,func,maxcalls,zeta,x,ifail)
c
c This subroutine locates zeros of a function of one variable. The
c method employs inverse quadratic interpolation and bisection.
c
c ifail = 1 on entry: soft fail.      ifail = 0 on entry: hard fail.
c ifail = 0 on return: success.      ifail = 1 on return: no zero.
c ifail = 2 on return: maxcalls reached.
c
c written by C.J.Wheatley October 1985.
c
c common /iotapes/  columns,ntape4,ntape5,ntape6
c integer          columns
c
c eps=amax1(1.e-14,eps)
c eta=amax1(0.e0,eta)
c zeta=amax1(0.5e0,zeta)
c maxcalls=max0(3,maxcalls)
c
c check if zero present and start iteration.
c *****
c
c x1=xl
c x3=xu
c y1 = func(x1)
c y3 = func(x3)
c icalls=2
c if(y1*y3.ge.0.e0)goto 1000
c x2=(x1+x3)/2.e0
c
c      start of iteration loop.
c      *****
c
c 100   y2 = func(x2)
c       icalls=icalls+1
c
c       test for last iteration step.
c       *****
c
c       if(abs(y2).le.eta)goto 500
c       if((y1*y2.lt.0.e0).and.(abs(x2-x1).le.eps))goto 800
c       if((y2*y3.le.0.e0).and.(abs(x3-x2).le.eps))goto 700
c       if(icalls.eq.maxcalls)goto 3000
c
c       test for inverse quadratic interpolation step.
c       *****
c
c       denom=x1*(y2-y3)+x2*(y3-y1)+x3*(y1-y2)
c       if(denom.eq.0.e0)goto 200
c       dy=0.5e0*(y1-y2)*(y2-y3)*(x3-x1)/denom
c       if(abs(dy).ge.zeta*abs(y3-y1))goto 200
c
c       interpolate.
c       *****
c
c       if(y1*y2.lt.0.e0)x=0.5e0*(x1+x2)
c       if(y2*y3.lt.0.e0)x=0.5e0*(x2+x3)
c       goto 300
c 200   x=x2-y2*(y3-((x2-x1)/(y2-y1))-y1+((x2-x3)/(y2-y3)))/(y3-y1)
c
c       revise range.
c       *****
c
c 300   if(y1*y2.lt.0.e0)goto 310
c       x1=x2
c       y1=y2
c       goto 400
c 310   x3=x2
c       y3=y2

```

```

c05whe 2
c05whe 3
c05whe 4
c05whe 5
c05whe 6
c05whe 7
c05whe 8
c05whe 9
c05whe10
c05whe11
c05whe12
iotapes2
iotapes3
c05whe14
c05whe15
c05whe16
c05whe17
c05whe18
c05whe19
c05whe20
c05whe21
c05whe22
c05whe23
c05whe24
c05whe25
c05whe26
c05whe27
c05whe28
c05whe29
c05whe30
c05whe31
c05whe32
c05whe33
c05whe34
c05whe35
c05whe36
c05whe37
c05whe38
c05whe39
c05whe40
c05whe41
c05whe42
c05whe43
c05whe44
c05whe45
c05whe46
c05whe47
c05whe48
c05whe49
c05whe50
c05whe51
c05whe52
c05whe53
c05whe54
c05whe55
c05whe56
c05whe57
c05whe58
c05whe59
c05whe60
c05whe61
c05whe62
c05whe63
c05whe64
c05whe65
c05whe66
c05whe67
c05whe68
c05whe69

```

```

c
c      revise intermediate point.
c      *****
c
c
400      x2=x
         if(abs(x3-x1).le.2.e0+eps)x2=0.5e0*(x1+x3)
         if(abs(x3-x1).le.2.e0+eps)goto 100
         if(abs(x2-x1).lt.eps)x2=x1+sign(eps,x3-x1)
         if(abs(x3-x2).lt.eps)x2=x3-sign(eps,x3-x1)
         goto 100
c
c      end of iteration loop.
c      *****
c
c
500      x=x2
         goto 710
600      x=x2
         if(abs(y1).lt.abs(y2))x=x1
         goto 710
700      x=x2
         if(abs(y3).lt.abs(y2))x=x3
710      ifail=0
         return
c
c      no zero found.
c      *****
c
c
1000     if(ifail.eq.1)return
         write(ntape5,9000)
         write(ntape5,9001)x1,y1,x3,y3
         write(ntape6,9000)
         write(ntape6,9001)x1,y1,x3,y3
         stop
c
c      maxcalls reached.
c      *****
c
c
2000     if(ifail.eq.1)ifail=2
         if(ifail.eq.2)return
         write(ntape5,9002)maxcalls
         write(ntape5,9001)x1,y1,x3,y3
         write(ntape6,9002)maxcalls
         write(ntape6,9001)x1,y1,x3,y3
         stop
9000     format(
+4x,'*** c05whe fails: interval does not contain a zero ***')
9001     format(
+4x,'***          x1          y1          x3          y3          ***',/
+4x,'***',1p4e12.4,' ***')
9002     format(
+4x,'*** c05whe fails: zero not found after ',i3,' steps ***')
         end

```

```

c05whe70
c05whe71
c05whe72
c05whe73
c05whe74
c05whe75
c05whe76
c05whe77
c05whe78
c05whe79
c05whe80
c05whe81
c05whe82
c05whe83
c05whe84
c05whe85
c05whe86
c05whe87
c05whe88
c05whe89
c05whe90
c05whe91
c05whe92
c05whe93
c05whe94
c05whe95
c05whe96
c05whe97
c05whe98
c05whe99
c05wh100
c05wh101
c05wh102
c05wh103
c05wh104
c05wh105
c05wh106
c05wh107
c05wh108
c05wh109
c05wh110
c05wh111
c05wh112
c05wh113
c05wh114
c05wh115
c05wh116
c05wh117
c05wh118
c05wh119
c05wh120
c05wh121

```



```

subroutine charmagg                                     chmagg 2
c                                                       chmagg 3
c This subroutine calculates the agglomeration rates of the chmagg 4
c particles at all combinations of the collocation points. This chmagg 5
c is done in a nested DO loop which could be written as a single chmagg 6
c loop to enable full vectorization if this program unit turns-out chmagg 7
c to be computationally costly. The agglomeration rates are chmagg 8
c identical to those used in MAEROS to facilitate comparisons. The chmagg 9
c particle radius, mass and mobility at the collocation points are chmagg10
c assumed to have been previously calculated. chmagg11
c chmagg12
c common /collpts/ ncoll,mlower,mupper,spacing,dlogen,logem0
+ ,radius(100),mass(100),mobility(100)
c real logem0,mass,mobility,mlower,mupper
c chmagg14
c common /aerslcon/ cshpfctr,dshpfctr,stickeff
+ ,aknudweb,qknudweb,bknudweb
+ ,pdensity,pthrmcon
+ ,kbrock,cmbrock,ctbrock
c real kbrock
c chmagg16
c common /gasprop/ temp,press,gdensity,dynvisc,molwt,mnfrpath
+ ,gthrmcon,velocity,molwtv,diffusv
+ ,vmfrclng,vmfrwall,vmfrflor
+ ,vcgrclng,vcgrwall,vcgrflor
+ ,vconclng,vconwall,vconflor
c real molwt,mnfrpath,molwtv
c chmagg18
c common /fundcon/ pi,boltzmann,gravitat,gasconst
c chmagg20
c common /agglom/ agglomrt(100,100),deposrtf(100)
+ ,deposrtw(100),deposrtc(100)
c chmagg22
c real ma1,ma2,mol,mo2,kt
c kt = boltzmann*temp
c chmagg23
c chmagg24
c chmagg25
c chmagg26
c chmagg27
c chmagg28
c chmagg29
c chmagg30
c chmagg31
c chmagg32
c chmagg33
c chmagg34
c chmagg35
c chmagg36
c chmagg37
c chmagg38
c chmagg39
c chmagg40
c chmagg41
c chmagg42
c chmagg43
c chmagg44
c chmagg45
c chmagg46
c chmagg47
c chmagg48
c chmagg49
c chmagg50
c chmagg51
c chmagg52
c chmagg53
c chmagg54
c chmagg55
c chmagg56
c chmagg57
c chmagg58

do 100 icoll1=1,ncoll
do 200 icoll2=1,icoll1
r1 = radius(icoll1)
r2 = radius(icoll2)
ma1 = mass(icoll1)
ma2 = mass(icoll2)
mol = mobility(icoll1)
mo2 = mobility(icoll2)
cr1=r1*cshpfctr
cr2=r2*cshpfctr

Brownian agglomeration
*****

vbar = sqrt( 8.e0*kt*(1.e0/ma1 + 1.e0/ma2)/pi )
fuchel = kt*(mol + mo2) / (stickeff*vbar*(r1 + r2))

a1 = mol*sqrt( 2.e0*kt*ma1/pi )
a2 = mo2*sqrt( 2.e0*kt*ma2/pi )
g1 = ((r1-a1)**3-(r1+r1-a1*a1)**1.5e0)/(3.e0*r1*a1) - r1
g2 = ((r2-a2)**3-(r2+r2-a2*a2)**1.5e0)/(3.e0*r2*a2) - r2
gbar = sqrt( g1*g1 + g2*g2 )
fuchs2 = 1.e0 / (1.e0 + 2.e0*gbar/(r1 + r2))

Note that there is no sticking efficiency factor.
FUCHS2 equals unity in Dunbar et al., EUR 9172.

fuchscor = 1.e0 / (fuchel + fuchs2)
aggb = 4.e0 * pi * kt * (mol + mo2) * (cr1 + cr2) * fuchscor

```

```

c      Gravitational aggloueration                                chmagg59
c      *****                                                    chmagg60
c      The Fuchs collision efficiency...                            chmagg61
c      colleff = 1.5e0 * ( min(r1,r2)/(r1+r2) )**2                chmagg62
c      Dunbar et al. has pdensity - gdensity / pdensity here...  chmagg63
c      relvel = gravitat * ( ma1*mo1 - ma2*mo2 )                   chmagg64
c      aggg = colleff * stickeff * abs(relvel) * pi * (cr1+cr2)**2 chmagg65
c      Turbulent agglomeration                                     chmagg66
c      *****                                                    chmagg67
c      tfactor = 8.e0*pi*gdensity*eddydiss/(15.e0*dynvisc)        chmagg68
c      aggte = stickeff * (cr1+cr2)**3 * sqrt( tfactor )          chmagg69
c      aggti = stickeff * (cr1+cr2)**2 * sqrt( 8.e0*pi*eddydiss ) chmagg70
c      * ( tfactor )**.25e0 * abs(relvel) / gravitat              chmagg71
c      Add the shear and inertial contributions in quadrature - note chmagg72
c      the collision efficiency factor is missing from both terms. chmagg73
c      aggt = sqrt(aggte*aggte + aggti*aggti)                       chmagg74
c      Combine the agglomeration contributions                     chmagg75
c      *****                                                    chmagg76
c      agglomrt(icoll1,icoll2) = aggb + aggg + aggt               chmagg77
c      agglomrt(icoll2,icoll1) = agglomrt(icoll1,icoll2)          chmagg78
200  continue                                                       chmagg79
100  continue                                                       chmagg80
      return                                                         chmagg81
      end                                                            chmagg82
                                                                    chmagg83
                                                                    chmagg84
                                                                    chmagg85
                                                                    chmagg86
                                                                    chmagg87
                                                                    chmagg88
                                                                    chmagg89
                                                                    chmagg90
                                                                    chmagg91
                                                                    chmagg92
                                                                    chmagg93
                                                                    chmagg94

```



```

subroutine charzdep
c
c This subroutine calculates the particle deposition rates
c at the collocation points. The deposition rates for
c gravitation, Brownian diffusion and thermophoresis are
c identical to those used in MAEROS to facilitate comparisons.
c Deposition due to turbulent diffusion, turbulent impaction and
c diffusio-phoresis have also been included. The diffusio-phoresis
c formula is taken from a later version of MAEROS which includes
c this mechanism. It was an input data item in early versions.
c
c The particle radius, mass and mobility at the collocation points
c are assumed to have been previously calculated.
c
c Deposition rates onto floors, walls and ceilings are kept
c separate to enable the deposited mass onto the three
c surfaces to be separately integrated.
c
c common /collpts/ ncoll,slower,mupper,spacing,dlogen,logen0
+ radius(100),mass(100),mobility(100)
real logen0,mass,mobility,slower,mupper
c
c common /aerelcon/ cshpfctr,dshpfctr,stickeff
+ ,aknudweb,qknudweb,bknudweb
+ ,pdensity,pthracon
+ ,kbrock,cmbrock,ctbrock
real kbrock
c
c common /gasprops/ temp,press,gdensity,dynvisc,molwt,mnfrpath
+ ,gthracon,velocity,molwtv,diffusv
+ ,vmfrclng,vmfrwall,vmfrflor
+ ,vcgrclng,vcgrwall,vcgrflor
+ ,vconclng,vconwall,vconflor
real molwt,mnfrpath,molwtv
c
c common /fundcon/ pi,boltzmn,gravitat,gasconst
c
c common /agglom/ agglomrt(100,100),depoartf(100)
+ ,depoartw(100),depoartc(100)
c
c common /cell/ areacing,areawall,areaflo
+ ,tempclng,tempwall,tempflor
+ ,volume,leakrate
+ ,hydrdiam,eqvrough
real leakrate
c
c common /flow/ blflag,vblthick,dblthick(100)
+ ,eddydiss,ustar,reynolds
integer blflag
c
c real kt,mo
c
c In MAEROS, ratioscon defaults to 0.05.
c
c kt = boltzmn*temp
c ratioscon = gthracon/pthracon
c deltcng = 1.e0 - tempcng/temp
c deltwall = 1.e0 - tempwall/temp
c deltflor = 1.e0 - tempflor/temp
c
c DO loop to calculate deposition rates
c *****
c
c do 100 icoll=1,ncoll
c r = radius(icoll)
c rl = r/mnfrpath
c mo = mobility(icoll)
c
c Gravitational deposition velocity

```

```

chmdep 2
chmdep 3
chmdep 4
chmdep 5
chmdep 6
chmdep 7
chmdep 8
chmdep 9
chmdep10
chmdep11
chmdep12
c' edep13
chmdep14
chmdep15
chmdep16
chmdep17
chmdep18
chmdep19
collpts3
collpts3
collpts4
chmdep21
aerelco2
aerelco3
aerelco4
aerelco5
aerelco6
chmdep23
gasprop2
gasprop3
gasprop4
gasprop5
gasprop6
gasprop7
chmdep25
fundcon2
chmdep27
agglom 2
agglom 3
chmdep29
cell 2
cell 3
cell 4
cell 5
cell 6
chmdep31
flow 2
flow 3
flow 4
chmdep33
chmdep34
chmdep35
chmdep36
chmdep37
chmdep38
chmdep39
chmdep40
chmdep41
chmdep42
chmdep43
chmdep44
chmdep45
chmdep46
chmdep47
chmdep48
chmdep49
chmdep50
chmdep51
chmdep52

```

```

c *****
c Dunbar et al. have pdensity - gdensity / pdensity here...
c vgravity = gravitat*mass(icoll)*mo
c Brownian diffusion deposition velocity
c *****
c if(dblthick(icoll).eq.0.e0)then
c   vbrown = 0.e0
c   else
c   vbrown = 0.0594e0 * kt*mo/dblthick(icoll)
c   endif
c
c Turbulence deposition velocity
c /*****
c
c The correlation used here is derived from the Liu and Agarwal
c data for dimensionless deposition velocity vs dimensionless
c particle relaxation time. The correlation is unverified for
c dimensionless relaxation time lt .1 and gt 100.
c
c relaxtim = mass(icoll)*mo
c dimrelax = relaxtim * ustar * ustar * gdensity / dynvisc
c if(dimrelax.eq.0.e0)then
c   dimvturb=0.e0
c   else
c     dimvtur1 = 8.e-4 * dimrelax * dimrelax
c     dimvtur2 = 2.13e-1 * dimrelax**(-0.125e0)
c     dimvturb = 1.e0 /
+   sqrt( 1.e0/(dimvtur1*dimvtur1) + 1.e0/(dimvtur2*dimvtur2) )
c   endif
c   vturb = dimvturb * ustar
c
c Thermophoresis deposition velocity
c *****
c
c The gdensity*vbthick term is missing in early versions of MAEROS.
c
c brockfac = kbrock / (1.e0 + 3.e0-cmbrock/rl)
+ / (2.e0 + 1.e0/(ratiocon+ctbrock/rl))
c if(vbthick.eq.0.e0)then
c   vthermo = 0.e0
c   else
c   vthermo = 9.e0*pi*dynvisc*dynvisc
+   *r*mo*brockfac/ gdensity*vbthick)
c   endif
c
c Diffusiophoresis deposition velocity
c *****
c
c This is taken from a later version of MAEROS.
c
c if(vconclng.eq.0.e0)then
c   vdfoclng=0.e0
c   else
c   vdfoclng = diffusv * vcgrclng / vconclng
+   * vmfrclng / ( vmfrclng + (1.e0-vmfrclng)*sqrt(molwt/molwtv) )
c   endif
c
c if(vconwall.eq.0.e0)then
c   vdfowall=0.e0
c   else
c   vdfowall = diffusv * vcgrwall / vconwall
+   * vmfrwall / ( vmfrwall + (1.e0-vmfrwall)*sqrt(molwt/molwtv) )
c   endif
c
c if(vconflor.eq.0.e0)then

```

```

chmdep53
chmdep54
chmdep55
chmdep56
chmdep57
chmdep58
chmdep59
chmdep60
chmdep61
chmdep62
chmdep63
chmdep64
chmdep65
chmdep66
chmdep67
chmdep68
chmdep69
chmdep70
chmdep71
chmdep72
chmdep73
chmdep74
chmdep75
chmdep76
chmdep77
chmdep78
chmdep79
chmdep80
chmdep81
chmdep82
chmdep83
chmdep84
chmdep85
chmdep86
chmdep87
chmdep88
chmdep89
chmdep90
chmdep91
chmdep92
chmdep93
chmdep94
chmdep95
chmdep96
chmdep97
chmdep98
chmdep99
chmde100
chmde101
chmde102
chmde103
chmde104
chmde105
chmde106
chmde107
chmde108
chmde109
chmde110
chmde111
chmde112
chmde113
chmde114
chmde115
chmde116
chmde117
chmde118
chmde119
chmde120
chmde121

```

```

vdfoflor=0.e0
else
vdfoflor = diffusv * vcgrflor / vconflor
+   * vmfrflor / ( vmfrflor + (1.e0-vmfrflor)*sqrt(molwt/molwtv) )
endif
c
c Net deposition velocity onto ceiling, walls and floor
c *****
c Note the thermo- and diffusiophoresis terms could be negative...
c
vclng = max(0.e0,vbrown+vturb+deltclng*vthermo+vdfoclng-vgravity)
vwall = max(0.e0,vbrown+vturb+deltwall*vthermo+vdfowall)
vflor = max(0.e0,vbrown+vturb+deltflor*vthermo+vdfoflor+vgravity)
c
c Store deposition rates for ceiling, walls and floor
c *****
c
deposrtf(icoll) = areaflor*vflor/volume
deposrtw(icoll) = areawall*vwall/volume
deposrtc(icoll) = areaclng*vclng/volume
100 continue
return
end

```

chmde122  
chmde123  
chmde124  
chmde125  
chmde126  
chmde127  
chmde128  
chmde129  
chmde130  
chmde131  
chmde132  
chmde133  
chmde134  
chmde135  
chmde136  
chmde137  
chmde138  
chmde139  
chmde140  
chmde141  
chmde142  
chmde143  
chmde144  
chmde145

```

subroutine charmsln
c
c This subroutine sets-up the source number density distribution.
c
c It takes the source distribution to be log-normal. The three
c input parameters are the cube root of the geometric mass
c standard deviation (in keeping with the normal convention),
c sigmasln (no units), the mass median radius, rad50sln (m),
c and the mass density generation rate, mdensln (kg m-3 s-1).
c
c mdensln = the mass generation rate divided by the cell volume.
c
c The three parameters of the log-normal distribution are the
c number density generation rate, ndensln (m-3 s-1), the
c geometric mean mass, geomsln (kg), and the logarithm of the
c geometric mass standard deviation, logsigma (no units).
c
c The discretized distribution is stored as the number density
c generation rate times mass, since this is the most convenient
c variable for the aerosol equation.
c
c common /fundcon/ pi,boltzmnn,gravitat,gasconst
c
c common /aerslcon/ cshpfctr,dsh.pfctr,stickeff
+ ,aknudweb,qknudweb,bknudweb
+ ,pdensity,pthrmcon
+ ,kbrock,cmbrock,ctbrock
c real
c
c common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ ,radius(100),mass(100),mobility(100)
c real
c
c common /lognorms/ sigmasln,rad50sln,mdensln
+ ,ndensln,geomsln,mass50sln
c real
c
c common /source/ sourcert(100)
c
c real logsigma,mdensity
c
c Convert the input parameters to the log-normal parameters
c *****
c
c logsigma = 3.e0*log( sigmasln )
c mass50sln=4.e0*pi*pdensity*rad50sln*rad50sln*rad50sln/3.e0
c geomsln=mass50sln*exp(-logsigma*logsigma)
c ndensln=mdensln*exp(-logsigma*logsigma/2.e0)/geomsln
c
c Calculate the distribution at the collocation points and the
c mass density generation rate of the discretized distribution
c *****
c
c mdensity=0.e0
c const=ndensln/( sqrt(2.e0*pi) * logsigma )
c do 100 icoll=1,ncoll
c exponent=log( mass(icoll)/geomsln ) / logsigma
c sourcert(icoll)=const*exp(-exponent*exponent/2.e0)
c mdensity=mdensity+dlogem*sourcert(icoll)*mass(icoll)
c continue
100
c
c Renormalize so that no mass is lost
c *****
c
c if(mdensity.ne.0.e0)then
c renorm=mdensln/mdensity
c do 200 icoll=1,ncoll
c sourcert(icoll)=sourcert(icoll)*renorm
200
c continue

```

```

chmsln 2
chmsln 3
chmsln 4
chmsln 5
chmsln 6
chmsln 7
chmsln 8
chmsln 9
chmsln10
chmsln11
chmsln12
chmsln13
chmsln14
chmsln15
chmsln16
chmsln17
chmsln18
chmsln19
chmsln20
chmsln21
chmsln22
fundcon2
chmsln24
aerslco2
aerslco3
aerslco4
aerslco5
aerslco6
chmsln26
collpts2
collpts3
collpts4
chmsln28
lognorm2
lognorm3
lognorm4
chmsln30
source 2
chmsln32
chmsln33
chmsln34
chmsln35
chmsln36
chmsln37
chmsln38
chmsln39
chmsln40
chmsln41
chmsln42
chmsln43
chmsln44
chmsln45
chmsln46
chmsln47
chmsln48
chmsln49
chmsln50
chmsln51
chmsln52
chmsln53
chmsln54
chmsln55
chmsln56
chmsln57
chmsln58
chmsln59
chmsln60
chmsln61
chmsln62

```

```
endif  
return  
end
```

```
chmsln63  
chmsln64  
chmsln65
```

```

subroutine charmdif(reset)
c
c This subroutine sets-up the input for the CLAMS ODE solver
c DEBDF, calls DEBDF for one time step and checks that the
c integration was done correctly.
c
common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ ,radius(100),mass(100),mobility(100)
real logem0,mass,mobility,mlower,mupper
c
common /distrib/ zstore(105)
c
common /timings/ time,istep,thhystep
+ ,itime,ntime,timestep(20),timeend(20)
+ ,ithhy,nthhy,timethhy(20)
+ ,idata,ndata,timedata(20)
c
common /toleranc/ eps,eta,zvca,maxcalls,maxtrys
c
common /moments/ sigma,r,d50,rdensity,ndensity,geommean,mass50
real mdensity,ndensity,mass50
c
common /lognormz/ sigmazln,rad50zln,mdenzln
+ ,ndenzln,geomzln,mass50zln
real mdenzln,ndenzln,mass50zln
c
common /lognorms/ sigmasln,rad50sln,mdensln
+ ,ndensln,geomsln,mass50sln
real mdensln,ndensln,mass50sln
c
common /iotapes/ columns,ntape4,ntape5,ntape6
integer columns
c
dimension z(105)
dimension rwork(12325),iwork(160)
dimension info(15)
dimension rtol(100),atol(100)
logical reset,firstgo
data firstgo/.true./
external charmrhs
c
c Set-up input for DEBDF
c *****
c
if(firstgo)then
timein=0.e0
else
if(reset)timein=timeout
endif
timeout=time
c
c Initial number density distribution and deposited mass
c *****
c
z(ncoll+1) holds the integrated mass deposited on floors
c
z(ncoll+2) holds the integrated mass deposited on walls
c
z(ncoll+3) holds the integrated mass deposited on ceilings
c
z(ncoll+4) holds the integrated source mass
c
z(ncoll+5) holds the integrated leaked mass
c
if(firstgo)then
do 100 icoll=1,ncoll
z(icoll)=zstore(icoll)
continue
100
c
neqns=ncoll+5
do 105 ieqns=ncoll+1,neqns
z(ieqns) = 0.e0
105
continue

```

```

endif
c
c Information for DEBDF
c *****
c
c Flag first/reset call or subsequent call
c Reset is set whenever the independent variables change
c discontinuously so that derivatives are calculated afresh on
c passing the discontinuity.
c
c if(firstgo .or. reset)then
c info(1)=0
c else
c info(1)=1
c endif
c
c Both tolerances are vector
c
c if(firstgo)then
c info(2)=1
c
c The solution is not required at intermediate times
c
c info(3)=0
c
c The integration can be done without restriction on t
c
c info(4)=0
c
c Partial derivatives should be calculated by differencing
c
c info(5)=0
c
c The Jacobian is dense
c
c info(6)=0
c endif
c
c info(7) to info(15) are not used by DEBDF
c
c Set-up relative and absolute tolerances
c *****
c
c atol is chosen to obtain accuracy in both the number density
c and mass density distributions. rtol is used as a trap in
c case ndensity or mdensity decrease by large amounts during
c the time step.
c
c do 150 icoll=1,ncoll
c rtol(icoll)=eps
c if(mdensity.eq.0.e0)then
c atol(icoll)=min( mdensln*(timeout-timein)/mass(icoll)
c + ,ndensln*(timeout-timein) )*eps/dlogem
c else
c atol(icoll)=min(mdensity/mass(icoll),ndensity)*eps/dlogem
c endif
150 continue
c
c do 155 icqns=ncoll+1,neqns
c rtol(icqns)=eps
c if(mdensity.eq.0.e0)then
c atol(icqns)=mdensln*(timeout-timein)*eps
c else
c atol(icqns)=mdensity*eps
c endif
155 continue
c
c Dimensions of rwork and iwork arrays.
c *****

```

```

chmdif80
chmdif81
chmdif82
chmdif83
chmdif84
chmdif85
chmdif86
chmdif87
chmdif88
chmdif89
chmdif90
chmdif91
chmdif92
chmdif93
chmdif94
chmdif95
chmdif96
chmdif97
chmdif98
chmdif99
chmdi100
chmdi101
chmdi102
chmdi103
chmdi104
chmdi105
chmdi106
chmdi107
chmdi108
chmdi109
chmdi110
chmdi111
chmdi112
chmdi113
chmdi114
chmdi115
chmdi116
chmdi117
chmdi118
chmdi119
chmdi120
chmdi121
chmdi122
chmdi123
chmdi124
chmdi125
chmdi126
chmdi127
chmdi128

```

```

c
if(firstgo)then
lrwork=12325
liwork=160
  if( (250 + 10*neqns + neqns*neqns) .gt. lrwork)then
  write(ntape5,2000)
  write(ntape6,2000)
2000  format(4x,'*** CHARMDIF fails: LRWORK is too small ***')
  stop
  end'f
  if( (55 + neqns) .gt. liwork)then
  write(ntape5,2001)
  write(ntape6,2001)
2001  format(4x,'*** CHARMDIF fails: LIWORK is too small ***')
  stop
  endif
endif

c
c Call DEBDF and check that the call was O.K.
c *****
c
icall=0
180  call debdf(chararhs,neqns,timein,z,timeout,info,rtol,atol
+      ,idid,rwork,lrwork,iwork,liwork,rpar,ipar,jac)
icall=icall+1
  if(idid.eq.-1 .and. icall.lt.maxtrys)then
  info(1)=1
  goto 180
  endif
  if(idid.lt.2)then
  write(ntape5,1000)idid
  write(ntape6,1000)idid
1000  format(4x,'*** CHARMDIF fails: IDID is ',i3,' ***')
  stop
  endif

c
c Store the answer
c *****
c
do 200 icoll=1,neqns
zstore(icoll)=z(icoll)
200  continue

c
c Kill the flag which signals first call to DEBDF
c *****
c
firstgo=.false.
return
end

```

```

chmdi129
chmdi130
chmdi131
chmdi132
chmdi133
chmdi134
chmdi135
chmdi136
chmdi137
chmdi138
chmdi139
chmdi140
chmdi141
chmdi142
chmdi143
chmdi144
chmdi145
chmdi146
chmdi147
chmdi148
chmdi149
chmdi150
chmdi151
chmdi152
chmdi153
chmdi154
chmdi155
chmdi156
chmdi157
chmdi158
chmdi159
chmdi160
chmdi161
chmdi162
chmdi163
chmdi164
chmdi165
chmdi166
chmdi167
chmdi168
chmdi169
chmdi170
chmdi171
chmdi172
chmdi173
chmdi174
chmdi175
chmdi176
chmdi177

```





```

c      Loop over the collocation points
c      *****
c
c      do 100 i=1,ncoll
c      dzdt(i)=0.
c
c      The production terms
c      *****
c
c      if(i-jbarmin.ge.1)then
c      do 10 j=1,min(i-jbarmin,ncoll)
c      jbar=i-j
c      prod=0.e0
c      if(nkbar(jbar).ne.0.e0)then
c      do 20 kbar=kbarmin(jbar),kbarmax(jbar)
c      k=i-kbar
c      if(k.ge.1 .and. k.le.ncoll)then
c      prod=prod+agglomrt(j,k)*njk(j,k)*z(k)
c      +      *pijk(index(jbar)+kbar)
c      endif
c      20  continue
c      prod=prod*z(j)*dlogem
c      endif
c      dzdt(i)=dzdt(i)+prod
c      10  continue
c      endif
c      100 continue
c
c      The destruction terms
c      *****
c
c      do 200 i=1,ncoll
c      dest=0.e0
c      do 30 j=1,ncoll
c      if(njk(i,j).ne.0.e0)dest=dest+agglomrt(i,j)*z(j)
c      30  continue
c      dest=dest*z(i)*dlogem
c      dzdt(i)=dzdt(i)-dest
c
c      Sources and sinks
c      *****
c
c      dzdt(i)=dzdt(i)-z(i)*deposrtf(i)
c      dzdt(i)=dzdt(i)-z(i)*deposrtw(i)
c      dzdt(i)=dzdt(i)-z(i)*deposrtc(i)
c      dzdt(i)=dzdt(i)+sourcert(i)
c      dzdt(i)=dzdt(i)-z(i)*leakrate
c
c      Update mass counters
c      *****
c
c      factor = dlogem*volume*mass(i)
c      dzdt(ncoll+1)=dzdt(ncoll+1)+z(i)*deposrtf(i)*factor
c      dzdt(ncoll+2)=dzdt(ncoll+2)+z(i)*deposrtw(i)*factor
c      dzdt(ncoll+3)=dzdt(ncoll+3)+z(i)*deposrtc(i)*factor
c      dzdt(ncoll+4)=dzdt(ncoll+4)+sourcert(i)*factor
c      dzdt(ncoll+5)=dzdt(ncoll+5)+z(i)*leakrate*factor
c      200 continue
c      return
c      end

```

```

chmrh57
chmrh58
chmrh59
chmrh80
chmrh61
chmrh62
chmrh63
chmrh64
chmrh65
chmrh66
chmrh67
chmrh68
chmrh69
chmrh70
chmrh71
chmrh72
chmrh73
chmrh74
chmrh75
chmrh76
chmrh77
chmrh78
chmrh79
chmrh80
chmrh81
chmrh82
chmrh83
chmrh84
chmrh85
chmrh86
chmrh87
chmrh88
chmrh89
chmrh90
chmrh91
chmrh92
chmrh93
chmrh94
chmrh95
chmrh96
chmrh97
chmrh98
chmrh99
chmrh100
chmrh101
chmrh102
chmrh103
chmrh104
chmrh105
chmrh106
chmrh107
chmrh108
chmrh109
chmrh110
chmrh111
chmrh112
chmrh113
chmrh114
chmrh115
chmrh116

```

```

subroutine charmmom
c
c This subroutine calculates moments of the discretized number
c density distribution using the trapezium rule.
c
common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ ,radius(100),mass(100),mobility(100)
real
logem0,mass,mobility,mlower,mupper
c
common /aerslcon/ cshpfctr,dshpfctr,stickeff
+ ,aknudweb,qknudweb,bknudweb
+ ,pdensity,pthrmcon
+ ,kbrock,cmbrock,ctbrock
real
kbrock
c
common /fundcon/ pi,boltzmnr,gravitat,gasconst
c
common /toleranc/ eps,eta,zeta,maxcalls,maxtrys
c
common /distrib/ zstore(105)
c
common /moments/ sigma,rad50,mdensity,ndensity,geommean,mass50
real
mdensity,ndensity,mass50
c
common /indexcoe/ nelement,hwidth,jbarmin,index(-2:100)
+ ,kbarmin(-2:100),kbarmax(-2:100),nkbar(-2:100)
c
common /iotapes/ columns,ntape4,ntape5,ntape6
integer
columns
c
external charmm50
c
c Calculate sums - x is loge(mass)
c *****
c
sum1 = 0.e0
sum2 = 0.e0
sum3 = 0.e0
sum4 = 0.e0
do 10 i=1,ncoll
x = logem0 + i*dlogem
sum1 = sum1 + zstore(i)*mass(i)
sum2 = sum2 + zstore(i)
sum3 = sum3 + zstore(i)*x
sum4 = sum4 + zstore(i)*x*x
10 continue
c
c Calculate moments from these sums
c *****
c
if(sum2.eq.0.e0)then
sigma=0.e0
rad50=0.e0
mdensity=0.e0
ndensity=0.e0
geommean=0.e0
mass50=0.e0
return
endif
mdensity = dlogem * sum1
ndensity = dlogem * sum2
dummy1 = dlogem * sum3
geommean = exp( dummy1/ndensity )
dummy2 = dlogem * sum4
dummy3 = (dummy2 - dummy1*dummy1/ndensity) /ndensity
if(dummy3.lt.0.e0)dummy3=0.e0
sigma = exp( sqrt( dummy3 )/3.e0 )
c
c Calculate mass median mass
c

```

```

chmmom 2
chmmom 3
chmmom 4
chmmom 5
chmmom 6
collpts2
collpts3
collpts4
chmmom 8
aerslco2
aerslco3
aerslco4
aerslco5
aerslco6
chmmom10
fundcon2
chmmom12
toleranc2
chmmom14
distrib2
chmmom16
moments2
moments3
chmmom18
indexco2
indexco3
chmmom20
iotapes2
iotapes3
chmmom22
chmmom23
chmmom24
chmmom25
chmmom26
chmmom27
chmmom28
chmmom29
chmmom30
chmmom31
chmmom32
chmmom33
chmmom34
chmmom35
chmmom36
chmmom37
chmmom38
chmmom39
chmmom40
chmmom41
chmmom42
chmmom43
chmmom44
chmmom45
chmmom46
chmmom47
chmmom48
chmmom49
chmmom50
chmmom51
chmmom52
chmmom53
chmmom54
chmmom55
chmmom56
chmmom57
chmmom58
chmmom59
chmmom60
chmmom61

```

c	*****	chmmom62
c		chmmom63
c	set-up input for c05whe - ifail = 1 is the soft fail option	chmmom64
c		chmmom65
	ifail = 1	chmmom66
	xlower = logem0 + dlogem	chmmom67
	xupper = logem0 + dlogem*ncoll	chmmom68
	rtol = eps	chmmom69
	atol = eta	chmmom70
	ztol = zeta	chmmom71
	ncalls = maxcalls	chmmom72
	call c05whe	chmmom73
+	(xlower,xupper,rtol,atol,charmm50,ncalls,ztol,x50,ifail)	chmmom74
	if(ifail.ne.0)then	chmmom75
	write(ntape5,1000)ifail	chmmom76
	write(ntape8,1000)ifail	chmmom77
1000	format(4x,'*** CHARMMOM fails: IFAIL is ',i2,' ***')	chmmom78
	stop	chmmom79
	endif	chmmom80
	mass50 = exp( x50 )	chmmom81
	rad50 = (3.e0*mass50/(4.e0*pi*pdensity))**(1.e0/3.e0)	chmmom82
	return	chmmom83
	end	chmmom84

```

function charmm50(x)
c
c This function subroutine calculates the mass density of the
c discretised distribution up to x and subtracts
c half the total mass density. The result is zero when
c x is x50: x is loge(mass).
c
common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ real          ,radius(100),mass(100),mobility(100)
real          logem0,mass,mobility,mlower,mupper
c
common /moments/ sigma,rad50,mdensity,ndensity,geommean,mass50
real          mdensity,ndensity,mass50
c
common /distrib/ zstore(105)
c
sum = 0.e0
do 10 i=1,ncoll
sum = sum + zstore(i)*mass(i)*charmfe0(x,i)
10 continue
charmm50 = dlogem*sum - 0.5e0*mdensity
return
end

```

```

chmm50 2
chmm50 3
chmm50 4
chmm50 5
chmm50 6
chmm50 7
chmm50 8
collpts2
collpts3
collpts4
chmm5010
moments2
moments3
chmm5012
distrib2
chmm5014
chmm5015
chmm5016
chmm5017
chmm5018
chmm5019
chmm5020
chmm5021

```

```

function charmfe0(arg,k)
c
c This function subroutine calculates the integral of the k-th
c finite element up to ARG, where ARG is loge(mass). As for
c CHARMFE, ARG is scaled by the collocation interval and
c translated so that the element is centred about zero.
c
c The elements are symmetric and have total integral unity
c so only the integral from zero up to the absolute value
c of the scaled argument is calculated.
c
c These integrals are calculated from analytic formulae since
c they may be done many times. They are used in the calculation
c of the mass median mass of the discretized distribution.
c
c The choice of element is determined by NELEMENT
c
common /collpts/ ncoll,mlower,mupper,spacing,dlogem,logem0
+ ,radius(100),mass(100),mobility(100)
real logem0,mass,mobility,mlower,mupper
c
common /indexcoe/ nelement,hwidth,jbarmin,index(-2:100)
+ ,kbarmin(-2:100),kbarmax(-2:100),nkbar(-2:100)
c
real integral
c
c Transform the argument and select an element
c *****
c
if(k.ne.0) x = (arg - logem0)/dlogem - k
if(k.eq.0) x = arg
if(x.le.-hwidth)then
  charmfe0 = 0.e0
  return
endif
if(x.ge.hwidth)then
  charmfe0 = 1.e0
  return
endif
y = abs(x)
goto(1,2,3,4,5,6)nelement
c
c First order element
c *****
c
1 continue
charmfe0 = 0.5e0 + x
return
c
c Second order element
c *****
c
2 continue
integral = y - y*y/2.e0
charmfe0 = 0.5e0 + sign(integral,x)
return
c
c Third order element
c *****
c
3 continue
z = y - 1.e0
if(y.lt.2.e0 .and. y.ge.1.e0)
+ integral=13.e0/24.e0-z*z*z/6.e0+z*z*z*z/8.e0
if(y.lt.1.e0)
+ integral=y-5.e0*y*y*y/6.e0+3.e0*y*y*y*y/8.e0
charmfe0 = 0.5e0 + sign(integral,x)
return
c

```

```

chmfe0 2
chmfe0 3
chmfe0 4
chmfe0 5
chmfe0 6
chmfe0 7
chmfe0 8
chmfe0 9
chmfe010
chmfe011
chmfe012
chmfe013
chmfe014
chmfe015
chmfe016
chmfe017
chmfe018
collpts2
collpts3
collpts4
chmfe020
indexco2
indexco3
chmfe022
chmfe023
chmfe024
chmfe025
chmfe026
chmfe027
chmfe028
chmfe029
chmfe030
chmfe031
chmfe032
chmfe033
chmfe034
chmfe035
chmfe036
chmfe037
chmfe038
chmfe039
chmfe040
chmfe041
chmfe042
chmfe043
chmfe044
chmfe045
chmfe046
chmfe047
chmfe048
chmfe049
chmfe050
chmfe051
chmfe052
chmfe053
chmfe054
chmfe055
chmfe056
chmfe057
chmfe058
chmfe059
chmfe060
chmfe061
chmfe062
chmfe063
chmfe064
chmfe065
chmfe066
chmfe067

```

```

c      Fourth order element
c      *****
c
c      4
c      continue
z = y - 1.e0
if(y.lt.2.e0 .and. y.ge.1.e0)
+   integral=13.e0/24.e0-3.e0*z*z*z*z/8.e0+z*z*z*z*z/2.e0
+   -z*z*z*z*z/8.e0
if(y.lt.1.e0)
+   integral=y-y*y*y/3.e0-9.e0*y*y*y*y/8.e0+3.e0*y*y*y*y*y/2.e0
+   -y*y*y*y*y/2.e0
charmfe0 = 0.5e0 + sign(integral,x)
return

c
c      Fifth order element
c      *****
c
c      5
c      continue
z = y - 1.e0
u = y - 2.e0
if(y.lt.3.e0 .and. y.ge.2.e0)
+   integral=1681.e0/3360.e0-u*u*u*u/u/80.e0+u*u*u*u*u/24.e0
+   -u*u*u*u*u/28.e0+u*u*u*u*u/96.e0
if(y.lt.2.e0 .and. y.ge.1.e0)
+   integral=303.e0/560.e0+z*z*z*z/48.e0-31.e0*z*z*z*z/z/30.e0
+   +25.e0*z*z*z*z/z/12.e0-31.e0*z*z*z*z*z/21.e0
+   +35.e0*z*z*z*z*z/96.e0
if(y.lt.1.e0)
+   integral=y-y*y*y/3.e0-91.e0*y*y*y*y*y/30.e0
+   +19.e0*y*y*y*y*y/3.e0-32.e0*y*y*y*y*y*y/7.e0
+   +65.e0*y*y*y*y*y*y/48.e0
charmfe0 = 0.5e0 + sign(integral,x)
return

c
c      Sixth order element
c      *****
c
c      6
c      continue
z = y - 1.e0
u = y - 2.e0
if(y.lt.3.e0 .and. y.ge.2.e0)
+   integral=1081.e0/2160.e0-11.e0*u*u*u*u/u/144.e0
+   +u*u*u*u/u/4.e0-5.e0*u*u*u*u/u/16.e0
+   +19.e0*u*u*u*u/u/108.e0
+   -3.e0*u*u*u*u/u/80.e0
if(y.lt.2.e0 .and. y.ge.1.e0)
+   integral=73.e0/135.e0+z*z*z*z/48.e0+z*z*z*z/z/120.e0
+   -145.e0*z*z*z*z/z/48.e0+103.e0*z*z*z*z/z/12.e0
+   -115.e0*z*z*z*z/z/12.e0+355.e0*z*z*z*z/z/72.e0
+   -47.e0*z*z*z*z*z/48.e0
if(y.lt.1.e0)
+   integral=y-y*y*y/3.e0+y*y*y*y/y/20.e0
+   -659.e0*y*y*y*y/y/72.e0+371.e0*y*y*y*y*y/y/14.e0
+   -30.e0*y*y*y*y*y/y+1665.e0*y*y*y*y*y/y/108.e0
+   -25.e0*y*y*y*y*y*y/y/24.e0
charmfe0 = 0.5e0 + sign(integral,x)
return
end

```

```

chmfe068
chmfe069
chmfe070
chmfe071
chmfe072
chmfe073
chmfe074
chmfe075
chmfe076
chmfe077
chmfe078
chmfe079
chmfe080
chmfe081
chmfe082
chmfe083
chmfe084
chmfe085
chmfe086
chmfe087
chmfe088
chmfe089
chmfe090
chmfe091
chmfe092
chmfe093
chmfe094
chmfe095
chmfe096
chmfe097
chmfe098
chmfe099
chmfe100
chmfe101
chmfe102
chmfe103
chmfe104
chmfe105
chmfe106
chmfe107
chmfe108
chmfe109
chmfe110
chmfe111
chmfe112
chmfe113
chmfe114
chmfe115
chmfe116
chmfe117
chmfe118
chmfe119
chmfe120
chmfe121
chmfe122
chmfe123
chmfe124
chmfe125

```

```

c      subroutine charmout
c
c      This subroutine writes to tapes 5 & 6 (tty & output file resp.).
c      No form control characters are printed.
c
c      common /collpts/  ncoll,mlower,mupper,spacing,dlogem,logem0
+      ,radius(100),mass(100),mobility(100)
c      real              logem0,mass,mobility,mlower,mupper
c
c      common /aerslcon/ cshpfctr,dshpfctr,stickoff
+      ,aknudweb,qknudweb,bknudweb
+      ,pdensity,pthrmcon
+      ,kbrock,cmbrock,ctbrock
c      real              kbrock
c
c      common /gasprops/ temp,press,gdensity,dynvisc,molwt,mnfrpath
+      ,gthrmcon,velocity,molwtv,diffusv
+      ,vmfrclng,vmfrwall,vmfrflor
+      ,vcgrclng,vcgrwall,vcgrflor
+      ,vconclng,vconwall,vconflor
c      real              molwt,mnfrpath,molwtv
c
c      common /agglom/   agglomrt(100,100),deposrtf(100)
+      ,deposrtw(100),deposrtc(100)
c
c      common /indexcoe/ nelement,hwidth,jbarmin,index(-2:100)
+      ,kbarmin(-2:100),kbarmax(-2:100),nkbar(-2:100)
c
c      common /coef/     pijk(300),njk(100,100)
c      real              njk
c
c      common /distrib/  zstore(105)
c
c      common /lognorms/ sigmasln,rad50sln,mdensln
+      ,ndensln,geomsln,mas50sln
c      real              mdensln,ndensln,mas50sln
c
c      common /source/   sourcert(100)
c
c      common /timings/  time,istep,thhystep
+      ,itime,ntime,timestep(20),timeend(20)
+      ,ithhy,nthhy,timethhy(20)
+      ,idata,ndata,timedata(20)
c
c      common /toleranc/ eps,eta,zeta,maxcalls,maxtrys
c
c      common /moments/  sigma,rad50,mdensity,ndensity,geommean,mas50
c      real              mdensity,ndensity,mas50
c
c      common /fundcon/  pi,boltzmnn,gravitat,gasconst
c
c      common /ioflags/  iondis,iomom,iocoef,iocnorm
+      ,iodepo,iomass,ioradi,iomobi
+      ,ioaggl,iomdis,iosdis,iombal
+      ,ioindx,iowmom,iocell,iogasp
+      ,iotole,ioacon,ioflow
c
c      common /iotapes/  columns,ntape4,ntape5,ntape6
c      integer          columns
c
c      common /cell/     areaclng,areawall,areaflor
+      ,tempclng,tempwall,tempflor
+      ,volume,leakrate
+      ,hydrdiam,eqvrrough
c      real              leakrate
c
c      common /flow/     blflag,vblthick,dblthick(100)
+      ,eddydiss,ustar,reynolds
c      integer          blflag

```

```

chmout 2
chmout 3
chmout 4
chmout 5
chmout 6
collpts2
collpts3
collpts4
chmout 8
aerslco2
aerslco3
aerslco4
aerslco5
aerslco6
chmout10
gasprop2
gasprop3
gasprop4
gasprop5
gasprop6
gasprop7
chmout12
agglom 2
agglom 3
chmout14
indexco2
indexco3
chmout16
coef 2
coef 3
chmout18
distrib2
chmout20
lognorm2
lognorm3
lognorm4
chmout22
source 2
chmout24
timings2
timings3
timings4
timings5
chmout26
toleran2
chmout28
moments2
moments3
chmout30
fundcon2
chmout32
ioflags2
ioflags3
ioflags4
ioflags5
ioflags6
chmout34
iotapes2
iotapes3
chmout36
cell 2
cell 3
cell 4
cell 5
cell 6
chmout38
flow 2
flow 3
flow 4

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c	logical firstgo	chmout40
	data firstgo/.true./	chmout41
c		chmout42
c	Rule-off page first time round	chmout43
c	*****	chmout44
c		chmout45
	if(firstgo)then	chmout46
	if(columns.eq. 80)write(ntape8,9999)	chmout47
	if(columns.eq.132)write(ntape8,8999)	chmout48
	endif	chmout49
c		chmout50
c	Current time and mass balance	chmout51
c	*****	chmout52
c		chmout53
	if(firstgo)balance0 = mdensity*volume	chmout54
	balance = mdensity*volume	chmout55
	+        + zstore(ncoll+1)	chmout56
	+        + zstore(ncoll+2)	chmout57
	+        + zstore(ncoll+3)	chmout58
	+        - zstore(ncoll+4)	chmout59
	+        + zstore(ncoll+5)	chmout60
	+        - balance0	chmout61
	write(ntape8,9009)istep,time,balance	chmout62
	write(ntape8,9038)istep,time,balance	chmout63
c		chmout64
c	Mass balances	chmout65
c	*****	chmout66
c		chmout67
	if(iombal.ne.0)then	chmout68
	if(mod(istep,iombal).eq.0)then	chmout69
	write(ntape8,9010)	chmout70
	write(ntape8,9001)mdensity*volume,zstore(ncoll+1)	chmout71
	+                                ,zstore(ncoll+2),zstore(ncoll+3)	chmout72
	+                                ,zstore(ncoll+4),zstore(ncoll+5)	chmout73
	endif	chmout74
	endif	chmout75
c		chmout76
c	Sound alarm if too much mass at end collocation points	chmout77
c	*****	chmout78
c		chmout79
	if(mdensity.ne.0.e0)then	chmout80
	fraction = zstore(ncoll)*mass(ncoll)*dlogem/mdensity	chmout81
	if(fraction.gt.1.e-1)then	chmout82
	write(ntape8,9015)fraction	chmout83
	write(ntape8,9015)fraction	chmout84
	endif	chmout85
	fraction = zstore(1)*mass(1)*dlogem/mdensity	chmout86
	if(fraction.gt.1.e-1)then	chmout87
	write(ntape8,9053)fraction	chmout88
	write(ntape8,9053)fraction	chmout89
	endif	chmout90
	endif	chmout91
c		chmout92
c	Sound alarm if too many particles at end collocation points	chmout93
c	*****	chmout94
c		chmout95
	if(ndensity.ne.0.e0)then	chmout96
	fraction = zstore(ncoll)*dlogem/ndensity	chmout97
	if(fraction.gt.1.e-1)then	chmout98
	write(ntape8,9054)fraction	chmout99
	write(ntape8,9054)fraction	chmout100
	endif	chmout101
	fraction = zstore(1)*dlogem/ndensity	chmout102
	if(fraction.gt.1.e-1)then	chmout103
	write(ntape8,9055)fraction	chmout104
	write(ntape8,9055)fraction	chmout105
	endif	chmout106
	endif	chmout107
		chmout108

```

c
c      Moments
c      *****
c
c      if(iozmom.ne.0)then
c      if(mod(istep,iozmom).eq.0)then
c      write(ntape8,9002)
c      write(ntape8,9001)sigma,rad50,mdensity,ndensity,geommean,mass50
c      endif
c      endif
c
c      Source moments
c      *****
c
c      if(iosmom.ne.0)then
c      if(mod(istep,iosmom).eq.0)then
c      write(ntape8,9021)
c      write(ntape8,9001)
c      +   sigmasln,rad50sln,mdensln,ndensln,geomsln,mass50sln
c      endif
c      endif
c
c      Mass density distribution
c      *****
c
c      if(iomdis.ne.0)then
c      if(mod(istep,iomdis).eq.0)then
c      write(ntape8,9044)
c      if(columns.eq.80)write(ntape8,9018)
c      if(columns.eq.132)write(ntape8,8018)
c      if(columns.eq.80)
c      +   write(ntape8,9003)(i,zstore(i)*mass(i),i=1,ncoll)
c      if(columns.eq.132)
c      +   write(ntape8,8003)(i,zstore(i)*mass(i),i=1,ncoll)
c      endif
c      endif
c
c      Number density distribution
c      *****
c
c      if(iondis.ne.0)then
c      if(mod(istep,iondis).eq.0)then
c      write(ntape8,9045)
c      if(columns.eq.80)write(ntape8,9017)
c      if(columns.eq.132)write(ntape8,8017)
c      if(columns.eq.80)write(ntape8,9003)(i,zstore(i),i=1,ncoll)
c      if(columns.eq.132)write(ntape8,8003)(i,zstore(i),i=1,ncoll)
c      endif
c      endif
c
c      Source mass and number density distributions
c      *****
c
c      if(iosdis.ne.0)then
c      if(mod(istep,iosdis).eq.0)then
c      write(ntape8,9022)
c      if(columns.eq.80)write(ntape8,9018)
c      if(columns.eq.132)write(ntape8,8018)
c      if(columns.eq.80)
c      +   write(ntape8,9003)(i,sourcert(i)*mass(i),i=1,ncoll)
c      if(columns.eq.132)
c      +   write(ntape8,8003)(i,sourcert(i)*mass(i),i=1,ncoll)
c      write(ntape8,9039)
c      if(columns.eq.80)write(ntape8,9017)
c      if(columns.eq.132)write(ntape8,8017)
c      if(columns.eq.80)write(ntape8,9003)(i,sourcert(i),i=1,ncoll)
c      if(columns.eq.132)write(ntape8,8003)(i,sourcert(i),i=1,ncoll)
c      endif
c      endif

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c
c Element, number of collocation points etc.
c *****
c
c if(firstgo)then
c range = mupper/mlower
c write(ntape6,9004)
c write(ntape6,9005)nelement,ncoll,hwidth,spacing,range
c endif
c
c Indexing for production coefficients
c *****
c
c if(firstgo .and. ioindx.ne.0)then
c write(ntape6,9023)
c write(ntape6,9024) (jbar,kbarmin(jbar),kbarmax(jbar),nkbar(jbar)
+ ,index(jbar),jbar=jbarmin,ncoll-1)
c endif
c
c Production coefficients
c *****
c
c if(firstgo .and. iocoef.ne.0)then
c if(columns.eq. 80)write(ntape6,9007)
c if(columns.eq.132)write(ntape6,8007)
c if(columns.eq. 80)write(ntape6,9001) (pijk(ind),ind=1,index(ncoll))
c if(columns.eq.132)write(ntape6,8001) (pijk(ind),ind=1,index(ncoll))
c endif
c
c Normalization
c *****
c
c if(firstgo .and. ionorm.ne.0)then
c if(columns.eq. 80)write(ntape6,9008)
c if(columns.eq.132)write(ntape6,8008)
c do 10 j=1,ncoll
c if(columns.eq. 80)write(ntape6,9003) (k,njk(j,k),k=1,ncoll)
c if(columns.eq.132)write(ntape6,8003) (k,njk(j,k),k=1,ncoll)
10 continue
c endif
c
c Collocation points
c *****
c
c if(firstgo .and. iomass.ne.0)then
c if(columns.eq. 80)write(ntape6,9006)
c if(columns.eq.132)write(ntape6,8006)
c if(columns.eq. 80)write(ntape6,9003) (i,mass(i),i=1,ncoll)
c if(columns.eq.132)write(ntape6,8003) (i,mass(i),i=1,ncoll)
c endif
c
c Radii at the collocation points
c *****
c
c if(firstgo .and. ioradi.ne.0)then
c if(columns.eq. 80)write(ntape6,9011)
c if(columns.eq.132)write(ntape6,8011)
c if(columns.eq. 80)write(ntape6,9003) (i,radius(i),i=1,ncoll)
c if(columns.eq.132)write(ntape6,8003) (i,radius(i),i=1,ncoll)
c endif
c
c Tolerances
c *****
c
c if(firstgo .and. iotole.ne.0)then
c write(ntape6,9025)
c write(ntape6,9025)eps,eta,zeta,maxcalls,maxtrys
c endif
c
c

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c      Aerosol physics data
c      *****
c
c      if(firstgo .and. ioacon.ne.0)then
c      write(ntape6,9040)
c      write(ntape6,9041) cshpfctr,dshpfctr,stickeff
c      write(ntape6,9027) aknudweb,qknudweb,bknudweb
c      write(ntape6,9028) pdensity,pthrmcon
c      write(ntape6,9029) kbrock,cmbrock,ctbrock
c      endif
c
c      Ce'l data
c      *****
c
c      if(iocell.ne.0)then
c      if(mod(istep,iocell).eq.0)then
c      write(ntape6,9042)
c      endif
c      endif
c      if(firstgo .and. iocell.ne.0)then
c      write(ntape6,9030) volume,leak .te
c      write(ntape6,9048) hydrdiam,eqvrrough
c      write(ntape6,9031) areaclng,areawall,areafloor
c      endif
c      if(iocell.ne.0)then
c      if(mod(istep,iocell).eq.0)then
c      write(ntape6,9032) tempclng,tempwall,tempfloor
c      endif
c      endif
c
c      Gas data
c      *****
c
c      if(iogasp.ne.0)then
c      if(mod(istep,iogasp).eq.0)then
c      write(ntape6,9043)
c      write(ntape6,9033) temp,press,velocity
c      write(ntape6,9034) gdensity,dynvisc,mnfrpath
c      if(firstgo)then
c      write(ntape6,9038) molwt,gthrmcon
c      write(ntape6,9051) molwtv,diffusv
c      write(ntape6,9049) vmfrclng,vmfrwall,vmfrflor
c      write(ntape6,9050) vcgrclng,vcgrwall,vcgrflor
c      write(ntape6,9052) vconclng,vconwall,vconflor
c      endif
c      endif
c      endif
c
c      Flow data
c      *****
c
c      if(ioflow.ne.0)then
c      if(mod(istep,ioflow).eq.0)then
c      write(ntape6,9046)
c      write(ntape6,9035) eddydiss,ustar,vblthick
c      write(ntape6,9047)
c      if(columns.eq. 80) write(ntape6,9003) (i,dblthick(i),i=1,ncoll)
c      if(columns.eq.132) write(ntape6,8003) (i,dblthick(i),i=1,ncoll)
c      endif
c      endif
c
c      Mobilities at the collocation points
c      *****
c
c      if(iomobi.ne.0)then
c      if(mod(istep,iomobi).eq.0)then
c      if(columns.eq. 80) write(ntape6,9012)
c      if(columns.eq.132) write(ntape6,8012)
c      if(columns.eq. 80) write(ntape6,9003) (i,mobility(i),i=1,ncoll)

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        if(columns.eq.132)write(ntape6,8003)(i,mobility(i),i=1,ncoll)
        endif
        endif
c
c      Deposition rates at the collocation points
c      *****
c
        if(iodepo.ne.0)then
        if(mod(istep,iodepo).eq.0)then
        write(ntape6,9018)
        if(columns.eq.80)write(ntape6,9013)
        if(columns.eq.132)write(ntape6,8013)
        if(columns.eq.80)write(ntape6,9003)(i,deposrtf(i),i=1,ncoll)
        if(columns.eq.132)write(ntape6,8003)(i,deposrtf(i),i=1,ncoll)
        write(ntape6,9019)
        if(columns.eq.80)write(ntape6,9013)
        if(columns.eq.132)write(ntape6,8013)
        if(columns.eq.80)write(ntape6,9003)(i,deposrtw(i),i=1,ncoll)
        if(columns.eq.132)write(ntape6,8003)(i,deposrtw(i),i=1,ncoll)
        write(ntape6,9020)
        if(columns.eq.80)write(ntape6,9013)
        if(columns.eq.132)write(ntape6,8013)
        if(columns.eq.80)write(ntape6,9003)(i,deposrtc(i),i=1,ncoll)
        if(columns.eq.132)write(ntape6,8003)(i,deposrtc(i),i=1,ncoll)
        endif
        endif
c
c      Agglomeration rates at the collocation points
c      *****
c
        if(ioaggl.ne.0)then
        if(mod(istep,ioaggl).eq.0)then:
        if(columns.eq.80)write(ntape6,9014)
        if(columns.eq.132)write(ntape6,8014)
        do 20 j=1,ncoll
        if(columns.eq.80)write(ntape6,9003)(k,agglomrt(j,k),k=1,ncoll)
        if(columns.eq.132)write(ntape6,8003)(k,agglomrt(j,k),k=1,ncoll)
20      continue
        endif
        endif
c
c      Kill FIRSTGO flag & rule-off page
c      *****
c
        firstgo=.false.
        if(columns.eq.80)write(ntape6,9999)
        if(columns.eq.132)write(ntape6,8999)
        return
c
c      Format statements
c      *****
c
9001  format(1p6e12.4)
9002  format('Airborne aerosol moments...',/
+ '      sigma      ',
+ '      rad50     ',
+ '      mdensity   ',
+ '      ndensity   ',
+ '      geommean   ',
+ '      mass50     ')
9003  format(5(i4,1p1e12.4))
9004  format('Collocation information...',/
+ '  nelement  ',
+ '  ncoll     ',
+ '  hwidth    ',4x,
+ '  spacing   ',4x,
+ '  range     ')
9005  format(2(i6,4x),3(1p1e12.4,4x))
9006  format('Collocation points...',/

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9007	+5(4x,' mass '))	chmou385
	format(+	chmou386
	'Production coefficients in indexing order...',/	chmou387
	+8(' pijk '))	chmou388
9008	format('Normalization factors...',/	chmou389
	+5(4x,' njk '))	chmou390
9009	format(+	chmou391
	'step no. = ',i3,' time = ',lple12.4,' mass check = ',lple12.4)	chmou392
9010	format('Mass budget...',/	chmou393
	+ ' air-borne',	chmou394
	+ ' flor dep.',	chmou395
	+ ' wall dep.',	chmou396
	+ ' clng dep.',	chmou397
	+ ' source',	chmou398
	+ ' leaked ')	chmou399
9011	format('Radii at the collocation points...',/	chmou400
	+5(4x,' radius '))	chmou401
9012	format('Mobilities at the collocation points...',/	chmou402
	+5(4x,' mobility '))	chmou403
9013	format(5(4x,' dep.rate '))	chmou404
9014	format('Agglomeration kernel...',/	chmou405
	+5(4x,' agg.rate '))	chmou406
9015	format(4x,'*** CHARMOU warning: the mass fraction in the',	chmou407
	+ ' top bin is ',lple12.4,' ***')	chmou408
9016	format(5(4x,' m-distr '))	chmou409
9017	format(5(4x,' n-distr '))	chmou410
9018	format('Rate of deposition onto floors...')	chmou411
9019	format('Rate of deposition onto walls...')	chmou412
9020	format('Rate of deposition onto ceilings...')	chmou413
9021	format('Source moments...',/	chmou414
	+ ' sigma',	chmou415
	+ ' rad50',	chmou416
	+ ' wdensity',	chmou417
	+ ' ndensity',	chmou418
	+ ' geommean',	chmou419
	+ ' mass50 ')	chmou420
9022	format('Source mass distribution...')	chmou421
9023	format('Indexing for production coefficients...',/	chmou422
	+ ' jbar',	chmou423
	+ ' kbarmin',	chmou424
	+ ' kbarmax',	chmou425
	+ ' nkbar',	chmou426
	+ ' index',	chmou427
	+ ' jbar',	chmou428
	+ ' kbarmin',	chmou429
	+ ' kbarmax',	chmou430
	+ ' nkbar',	chmou431
	+ ' index ')	chmou432
9024	format(i8,i8)	chmou433
9025	format('Tolerance information...',/	chmou434
	+ ' eps',	chmou435
	+ ' eta',	chmou436
	+ ' zeta',	chmou437
	+ ' maxcalls',	chmou438
	+ ' maxtrys ')	chmou439
9026	format(lp3e12.4,i8,i12)	chmou440
9027	format(+	chmou441
	' aknudweb = ',lple12.4,	chmou442
	+ ' qknudweb = ',lple12.4,	chmou443
	+ ' bknudweb = ',lple12.4)	chmou444
9028	format(+	chmou445
	' pdensity = ',lple12.4,	chmou446
	+ ' pthrmcon = ',lple12.4)	chmou447
9029	format(+	chmou448
	' kbrock = ',lple12.4,	chmou449
	+ ' cmbrock = ',lple12.4,	chmou450
	+ ' ctbrock = ',lple12.4)	chmou451
9030	format(+	chmou452
	' volume = ',lple12.4,	chmou453

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+ ' leakrate = ',1pl12.4)
9031 format(
+ ' areacng = ',1pl12.4,
+ ' areawall = ',1pl12.4,
+ ' areaflor = ',1pl12.4)
9032 format(
+ ' tempcng = ',1pl12.4,
+ ' tempwall = ',1pl12.4,
+ ' tempflor = ',1pl12.4)
9033 format(
+ ' temp = ',1pl12.4,
+ ' press = ',1pl12.4,
+ ' velocity = ',1pl12.4)
9034 format(
+ ' gdensity = ',1pl12.4,
+ ' dynvisc = ',1pl12.4,
+ ' mnfrpath = ',1pl12.4)
9035 format(
+ ' eddydiss = ',1pl12.4,
+ ' ustar = ',1pl12.4,
+ ' vblthick = ',1pl12.4)
9036 format(
+ ' molwt = ',1pl12.4,
+ ' gthrmcon = ',1pl12.4)
9038 format(
+82('*'),/
+ 'step no. = ',i3, ' time = ',1pl12.4, ' mass check = ',1pl12.4,/
+82('*'))/
9039 format('Source number distribution...')
9040 format('Aerosol physics data...')
9041 format(
+ ' cshpfctr = ',1pl12.4,
+ ' dshpfctr = ',1pl12.4,
+ ' stickeff = ',1pl12.4)
9042 format('Cell data...')
9043 format('Gas data...')
9044 format('Airborne mass distribution...')
9045 format('Airborne number distribution...')
9046 format('Flow data...')
9047 format('Diffusion boundary layer thickness...',/
+5(4x, ' dblthick '))
9048 format(
+ ' hydrdiam = ',1pl12.4,
+ ' eqvrrough = ',1pl12.4)
9049 format(
+ ' vmfrclng = ',1pl12.4,
+ ' vmfrwall = ',1pl12.4,
+ ' vmfrflor = ',1pl12.4)
9050 format(
+ ' vgrclng = ',1pl12.4,
+ ' vgrwall = ',1pl12.4,
+ ' vgrflor = ',1pl12.4)
9051 format(
+ ' molwtv = ',1pl12.4,
+ ' diffusv = ',1pl12.4)
9052 format(
+ ' vconclng = ',1pl12.4,
+ ' vconwall = ',1pl12.4,
+ ' vconflor = ',1pl12.4)
9053 format(4x, '*** CHARMOUT warning: the mass fraction in the',
+ ' bottom bin is ',1pl12.4, ' ***')
9054 format(4x, '*** CHARMOUT warning: the number fraction in the',
+ ' top bin is ',1pl12.4, ' ***')
9055 format(4x, '*** CHARMOUT warning: the number fraction in the',
+ ' bottom bin is ',1pl12.4, ' ***')
9999 format(/,80('*'),/)
8001 format(1pl12.4)
8003 format(8(i4,1pl12.4))
8006 format('Collocation points...',/

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	+8(4x, ' mass '))	chmou523
8007	format(	chmou524
	+ 'Production coefficients in indexing order... ', /	chmou525
	+11(' pijk '))	chmou526
8008	format('Normalization factors... ', /	chmou527
	+8(4x, ' njk '))	chmou528
8011	format('Radii at the collocation points... ', /	chmou529
	+8(4x, ' radius '))	chmou530
8012	format('Mobilities at the collocation points... ', /	chmou531
	+8(4x, ' mobility '))	chmou532
8013	format(8(4x, ' dep.rate '))	chmou533
8014	format('Agglomeration kernel... ', /	chmou534
	+8(4x, ' agg.rate '))	chmou535
8016	format(8(4x, ' m-distr '))	chmou536
8017	format(8(4x, ' n-distr '))	chmou537
8047	format('Diffusion boundary layer thickness... ', /	chmou538
	+8(4x, ' dblthick '))	chmou539
8999	format(/,132('='), /)	chmou540
	end	chmou541



## APPENDIX E - NOMENCLATURE

$a, \bar{a}, \bar{a}_j, \bar{a}_k$	Parameters in Sitariski and Seinfeld's correction to the Brownian agglomeration rate.
A	The cell cross-sectional area perpendicular to the flow.
$A_c, A_w, A_f, A_s$	The area exposed to aerosol of , respectively, the ceiling, wall, floor and any one of these surfaces.
$b_k, b_m, b_t$	Dimensionless constants appearing in the Brock factor, Br, in the expression for the thermophoresis deposition velocity.
$B, B_i, B_j, B_k$	The mobility of particles of any mass and those of mass $m_i, m_j$ and $m_k$ respectively.
Br	The Brock factor in the expression for the thermophoretic deposition velocity.
$B_{St}$	The particle mobility according to Stoke's law.
$c_c, c_w, c_f, c_s$	The vapor concentration adjacent to, respectively, the ceiling, wall, floor and any one of the surfaces.
$\frac{dc_c}{dx}, \frac{dc_w}{dx}, \frac{dc_f}{dx}, \frac{dc_s}{dx}$	The vapor concentration gradient adjacent to, respectively, the ceiling, wall, floor and any one of these surfaces.
$C(m, t)$	The number density distribution.
Cu	The Cunningham correction factor in the expression for the particle mobility.
$d_b$	The hydraulic diameter of the flow path - see Eq. 9.
$D_j^i$	The integral which appears in the destruction term in the discretized aerosol equation.
$D_r$	The diffusivity of steam in air at $T_{r1}$ and $P_r$ .
$D_v$	The vapor diffusivity in the gas.
$f_s$	The Fanning friction factor.
$f_c, f_w, f_f, f_s$	The molar fraction of vapor in the gas/vapor mixture adjacent to, respectively, the ceiling, wall, floor and any one of these surfaces.
Fu	Fuchs' correction factor to the Brownian agglomeration rate.
$Fu_1, Fu_2$	The terms due to Fuchs, and Sitariski and Seinfeld which appear in Fu.
g	The acceleration due to gravity.
$g(y)$	The basic finite element.
$g_i, g_j, g_k$	The $i^{th}, j^{th}$ and $k^{th}$ finite elements based on $g(y)$ . e.g. $g_1(x) = g((x-x_1)/h)$ .
h	The logarithmic spacing between successive collocation points.
i, j, k	Indices with values in the range 1 to n. See under subscripts below.
$\bar{j}, \bar{k}$	$\bar{j} = i - j$ and similarly for $\bar{k}$ .
k	Boltzmann's constant.

$k_a, k_b, k_c$	Dimensionless constants in the Cunningham correction factor, $C_u$ .
$K(\mu, m, t), K_{jk}$	The agglomeration kernel. $K_{jk}$ is $K(m_j, m_k, t)$ .
$Kn$	The particle Knudsen number based on the radius of the equivalent spherical particle.
$l$	The mean free path of gas molecules in the bulk gas.
$m, m_i, m_j, m_k$	The particle mass in general and at the $i^{th}$ , $j^{th}$ and $k^{th}$ collocation points respectively.
$m_{50}$	The mass median mass of the airborne and source distributions.
$m_g$	The geometric mean mass of the airborne and source number distributions.
$n$	The number of collocation points.
$n_{jk}$	The normalization factor appearing in the production term of the discretized aerosol equation.
$N$	The number density of the airborne distribution.
$\frac{dN}{dt}$	The number release rate of source particles per unit cell volume.
$p$	The "wetted" perimeter of the cell perpendicular to the flow field.
$P$	The mean pressure in the cell.
$P_{jk}^i$	The integral which appears in the production term of the discretized aerosol equation.
$P_r$	A reference pressure which appears in the correlation for the diffusivity of steam in air.
$r, r_i, r_j, r_k$	The radius of the equivalent spherical particle in general and at the $i^{th}$ , $j^{th}$ and $k^{th}$ collocation points respectively.
$r_{50}$	The mass median particle radius of the airborne and source distributions.
$r, s$	Indices with values in the range 1 to $n$ .
$R$	The universal gas constant.
$R(m, t), R_i, R_j$	The removal rate of particles of mass $m$ per unit cell volume. $R_i$ is $R(m_i, t)$ and similarly for $j$ .
$Re$	The Reynolds number based on the hydrodynamic diameter and the mean flow speed.
$S(m, t), S_i, S_j$	The source number distribution. $S_i$ is $S(m_i, t)$ and similarly for $j$ .
$Sc$	The particle Schmidt number.
$t$	Time.
$T$	The mean gas temperature in the cell.
$T_c, T_w, T_f, T_s$	The mean gas temperature adjacent to, respectively, the ceiling, wall, floor and any one of these surfaces.

$T_{r1}, T_{r2}$	Reference temperatures appearing in correlations for the dynamic viscosity of air and the diffusivity of steam in air respectively.
$U$	The mean flow speed in the cell.
$u_*$	The friction velocity.
$u_G$	The particle gravitational terminal velocity.
$v_*$	The deposition velocity due to turbulence.
$\bar{v}_*, \bar{v}_{*1}, \bar{v}_{*2}$	Non-dimensional turbulent deposition velocities appearing in the correlation based on the Lui and Agarwal data.
$v_c, v_w, v_f, v_s$	Net deposition velocities to, respectively, the ceiling, floor, wall and any one of these surfaces.
$v_B$	The deposition velocity due to Brownian diffusion across the laminar sublayer in a turbulent flow.
$v_{Dc}, v_{Dw}, v_{Df}, v_{Ds}$	Diffusiophoresis deposition velocities to, respectively, the ceiling, wall, floor and any one of these surfaces.
$v_G$	The gravitational deposition velocity.
$v_{Tc}, v_{Tw}, v_{Tf}, v_{Ts}$	Thermophoresis deposition velocities to, respectively, the ceiling, wall, floor and any one of these surfaces.
$V$	The cell volume.
$W_g, W_v$	The average molecular weight of the gas in the bulk of the cell and the molecular weight of the vapor promoting diffusiophoresis.
$x, x_i$	$x$ is $\log_e(m)$ and $x_i$ is $\log_e(m_i)$ .
$y$	The independent variable in the simplified integral for $P_{jk}^i$ (Eq. (56)).
$Y(m,t), Y_i, Y_j, Y_k$	The density distribution of the airborne aerosol. It is occasionally referred to as the mass distribution. $Y_i$ is $Y(m_i,t)$ and similarly for $j$ and $k$ .
$z_s$	The equivalent sand roughness of surfaces in the cell.
$a_g, a_p$	The thermal conductivities of the gas and the particle material respectively.
$\chi_c, \chi_d$	The collision and dynamic shape factors.
$\chi_{Fu}, \chi_s$	The Fuchs collision efficiency and the particle-particle sticking efficiency.
$\delta_*$	The viscous boundary layer thickness.
$\delta_{ij}$	The Kronecker delta.
$\delta_D, \delta_{Di}$	The particle diffusion boundary layer thickness. $\delta_{Di}$ is $\delta_D$ evaluated for particles of mass $m_i$ .
$\epsilon$	The relative tolerance parameter.
$\epsilon_*$	The average energy dissipation rate per unit mass due to turbulence in the bulk gas.
$\phi_I, \phi_S, \phi_B, \phi_G$	Agglomeration rates due to: particle inertia in a turbulent flow, turbulent shear, Brownian motion and gravitational settling respectively.

$\eta$	An absolute tolerance parameter required by the method for finding zeros of functions.
$\eta_g$	The dynamic viscosity of the bulk gas.
$\eta_r$	The dynamic viscosity of air at $T_{r1}$ .
$\lambda_l$	The removal rate due to leakage.
$\lambda_c, \lambda_w, \lambda_f, \lambda_s$	The removal rates due to deposition to, respectively, the ceiling, wall, floor and any one of these surfaces.
$\lambda_{ci}, \lambda_{wi}, \lambda_{fi}, \lambda_{si}$	As above evaluated at $m_i$ .
$\mu, \nu$	Particle masses.
$\pi$	Pi.
$\rho$	The density of the airborne aerosol.
$\frac{d\rho}{dt}$	The mass generation rate of the source per unit cell volume.
$\rho_g, \rho_p$	The density of the bulk gas and the particle material respectively.
$\sigma$	The cube root of the geometric standard deviation with respect to mass of the airborne and source number concentration distributions. It is also called the geometric standard deviation.
$\tau$	The particle relaxation time.
$\bar{\tau}$	The dimensionless particle relaxation time.
$\zeta$	A parameter required by the method for finding zeros of functions.

#### Subscripts

*	Denotes associated with turbulence.
c, w, f, s	Denotes, respectively, the ceiling, wall, floor and any one of these surfaces.
g, p	Denotes the bulk gas (except when used in $m_g$ ) and particles respectively.
i, j, k	Indices with values in the range 1 to n. They denote that the associated variable is to be evaluated at the corresponding collocation point.
r	Denotes a reference value. It is used for parameters appearing in correlations of physical properties.

APPENDIX F - INDEX OF SUBROUTINE AND FILE NAMES

CO5WHE	39,46,48,83 <sup>d</sup> ,84,117 <sup>1</sup>	CHARM50	48,84 <sup>d</sup> ,133 <sup>1</sup>
CHARM	40-47,80 <sup>d</sup> ,85,89 <sup>1</sup>	CHARMMOB	83 <sup>d</sup> ,114 <sup>1</sup>
CHARMAGG	83 <sup>d</sup> ,120 <sup>1</sup>	CHARMMOM	48,84 <sup>d</sup> ,87,131 <sup>1</sup>
CHARMBLO	54,80 <sup>d</sup> ,85,92 <sup>1</sup>	CHARMNOR	82 <sup>d</sup> ,107 <sup>1</sup>
CHARMCOE	18,45-46,54,81 <sup>d</sup> ,85,102 <sup>1</sup>	CHARMOPL	41,51
CHARMCOL	81 <sup>d</sup> ,98 <sup>1</sup>	CHARMOUT	48,51,80,84 <sup>d</sup> ,87,136 <sup>1</sup>
CHARMCFT	41-42,51	CHARMPJK	81 <sup>d</sup> ,85,104 <sup>1</sup>
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CHARMDIF	46-47,80,83 <sup>d</sup> ,86-87,126 <sup>1</sup>	CHARMSLN	54,80,83 <sup>d</sup> ,85,125 <sup>1</sup>
CHARMFAN	46,83 <sup>d</sup> ,119 <sup>1</sup>	CHARMUTH	54,80,82 <sup>d</sup> ,85,112 <sup>1</sup>
CHARMFE	81,82 <sup>d</sup> ,105 <sup>1</sup>	CHARMWTH	54,82 <sup>d</sup> ,111 <sup>1</sup>
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<sup>d</sup> subroutine description

<sup>1</sup> subroutine listing

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13. ABSTRACT (200 words or less)

CHARM is a computer model for the behavior of a one component aerosol in a single region with time-varying external conditions. It treats particle agglomeration due to Brownian motion, gravity and turbulence, and particle deposition due to Brownian motion, gravity, turbulence, thermophoresis and diffusiophoresis. Turbulence properties are estimated for flow through a region of arbitrary cross-sectional shape, with aerodynamically rough or smooth walls at any Reynolds number. The gas can be of any composition. The time-varying external conditions allowed for are: the temperature, pressure and velocity of the gas, wall temperatures, and the rate, mass median radius and geometric standard deviation of the source. The model is simple, modified to enable this list to be extended if needed. A new method of solving the governing equations, based on the finite element collocation method, enables the time-varying conditions to be treated accurately and economically. We describe in detail: the models, the numerical methods, the execution of the computer code (including how to write the input data file and interpret results), and how to make simple modifications to the model. We discuss how the model could be implemented as a sub-model of a larger one and what further work needs to be done to enable it to efficiently treat multicomponent aerosols, and condensation onto and evaporation from particles.

14. DOCUMENT ANALYSIS -- a. KEYWORDS/DESCRIPTORS

CHARM, aerosol computer model, aerosol coupling to thermal-hydraulics,  
finite-element method, collocation, CHARM user's manual

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15. AVAILABILITY STATEMENT

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