Carolina Power & Light Company

P. O. Box 1551 * Raleigh, N. C. 27602

SERIAL: NLS-88-093

257

023

LYNN W. EURY Senior Vice President Operations Support

MAY 2 5 1988

Dr. J. Nelson Grace, Regional Administrator United States Nuclear Regulatory Commission 101 Marietta Street, NW Atlanta, GA 30303

BRUNSWICK STEAM ELECTRIC PLANT, UNIT NOS. 1 AND 2 DOCKET NOS. 50-325 & 50-324/LICENSE NOS. DPR-71 & DPR-62 IE BULLETIN NO. 85-03 "MOTOR-OPERATED VALVE COMMON MODE FAILURES DURING PLANT TRANSIENTS DUE TO IMPROPER SWITCH SETTINGS"

Reference:

- (1) CP&L letter from Mr. A. B. Cutter to Dr. J. Nelson Grace (NRC-Region II) dated October 2, 1986, Serial No. NLS-86-300
- (2) CP&L letter from Mr. L. W. Eury to Dr. J. Nelson Grace (NRC-Region II) dated March 4, 1988, Serial No. NLS-88-037
- (3) BWR Owners' Group Report on the Operational Design Basis of Safety-Related Motor-Operated Valves, dated September 2, 1986
- (4) BWROG letter from Mr. R. F. Janecek to Mr. J. H. Sniezek (NRC) dated March 28, 1988, Serial No. BWROG-8815/OTRI
- (5) Request for Additional Information Concerning Brunswick Units I and 2 Response to IEB 85-03, dated April 18, 1988

Dear Dr. Grace:

Carolina Power & Light Company (CP&L) hereby submits information requested by IE Bulletin No. 85-03, "Motor-Operated Valve Common Mode Failures During Plant Transients Due to Improper Switch Settings," dated November 15, 1985 and Reference 5. The subject Bulletin required that a design basis review be performed and a program be developed and implemented to ensure that switch settings for certain safety-related, motor-operated valves (MOV) are properly selected, tested under simulated conditions, and correctly maintained. Results of the design basis review were submitted by Reference 1.

8806020044 880525 ADOCK 05000324 Attachment I to this submittal comprises a report detailing CP&L's completion of the IEB 85-03 program. The report provides a verification of completion of the requested program, a summary of the findings as to valve operability prior to any adjustment resulting from the subject Bulletin, and a summary of data as suggested by Table 2 of the Bulletin. This report provides the information required by Action f of the Bulletin. Attachment 2 specifically provides that information requested by Reference 5. Where appropriate, this information is also contained in Attachment I. This letter is submitted within the time frame as discussed with Mr. E. D. Sylvester on May 16, 1988.

Please note that as stated in Reference 4, the BWROG is re-evaluating valve differential pressures on the nine NRC selected MOVs, considering inadvertent valve operation. This BWROG re-evaluation is being undertaken with the understanding that assumptions are required that are outside the existing BWR ECCS design basis. CP&L will address changes to the valve differential pressures for the five NRC selected MOVs applicable to BSEP, upon completion of the BWROG re-evaluation. A report providing the results of the above design basis evaluation per Action (a) of NRC Bulletin 85-03, Supplement 1 and a schedule for implementing Actions (b) through (d) will be submitted within 30 days of our receipt of the BWROG re-evaluation.

Should you have any questions regarding this topic, please contact Mr. Arnold Schmich at (919) 836-8759.

Yours very truly,

L. W. Eury

Notary (Seal)

LWE/AWS/lah (5406AWS)

Attachments

cc: Mr. W.

Mr. W. H. Ruland Mr. E. D. Sylvester

NRC Document Control Desk

L. W. Eury, having been first duly sworn, did depose and say that the information contained herein is true and correct to the best of his information, knowledge and belief; and the sources of his information are officers, employees, contractors, and agents of Carolina Power & Light Company.

My commission expires:



ATTACHMENT I

Final Response to NRC IE Bulletin No. 85-03

Final Response to NRC IE Bulletin 85-03

The following sections provide specific detail on each of the IEB 85-03 action items. References 1, 2, 3, 4, and 5 refer to the references listed in the cover letter.

A. Design Basis Information

Action (a) requires that CP&L review and document the design basis for the operation of the MOVs in the High Pressure Coolant Injection (HPCI) and Reactor Core Isolation Cooling (RCIC) Systems required to be tested for operational readiness in accordance with 10CFR50.55a(g). This documentation should include the maximum expected differential pressure during both opening and closing of the valve.

The Boiling Water Reactor Owners' Group (BWROG), of which CP&L is a member, developed a program to address Action (a) of the Bulletin on a generic basis. Reference 3 provided this generic methodology. The valves analyzed as requiring calculation of the differential pressures in the BWROG Report are listed in Tables 1 and 2 of Reference 1 and Tables 1 and 2 of this response, along with the maximum expected differential pressure in the direction of opening and/or closing. It should be noted that Tables 1 and 2 (of this response) contain additional valves and/or pressures not contained in the initial BSEP response (Reference 1). These additional valves/pressures were added in response to

Calculations of the maximum expected differential pressures provided in Reference I were based on the BWROG generic methodology and contained several very conservative assumptions. Due to the excessively conservative assumptions contained in the BWROG generic methodology, the calculated differential pressure for several MOVs was listed as greater than the actual value. For those valves affected, the revised data and the basis for deviation from the generic methodology was presented in Reference 2.

The valves analyzed as requiring calculation of the differential pressures in the BWROG report are listed in Tables 1 and 2, along with the maximum expected differential pressure in the direction of opening and/or closing. A discussion of the valve function, design basis, and differential pressure location (upstream or downstream) are provided in the BWROG report. As indicated in Reference 4, the BWROG is re-evaluating valve differential pressures on the nine NRC selected MOVs, considering inadvertent valve operation. The BWROG re-evaluation is being undertaken with the understanding that such as sessment requires assumptions outside the existing BWR Emergency Core Cooling System design basis. CP&L will address any changes to the valve differential pressures for the five NRC selected MOVs which are applicable to BSEP, upon completion of the BWROG re-evaluation. This information will be provided in accordance with the requirements of IE Bulletin 85-03, Supplement 1.

For the valves in Tables 1 and 2 added by this response, the methodology utilized to calculate the maximum expected differential pressures is presented below:

MOV E41-F008

MOV E41-F008 is the HPCI pump CST Test return line isolation valve, and discharges to the CST. As discussed in the BWROG Report, this valve has no safety function. The valve is normally closed, and is only opened for testing or reactor pressure control.

Since the valve is a globe valve, flow will assist in opening the valve. With the opening torque switch jumpered out, ful! motor torque can be applied to opening the valve. Maximum pressure is expected upstream of the valve and, therefore, assists in opening the valve. For these reasons, the valve opening differential pressure is of no concern. For conservatism however, the existing valve design differential pressure of 1140 psid has been utilized for this response.

BSEP procedures call for closing this valve under various conditions. These include closure after turbine shutdown, closure at a turbine speed of 3300 rpm (920 psi pump discharge pressure), and closure upon transfer of flow paths following an automatic initiation. In this final case, the injection valve is open before this valve reaches the full closed position. Line pressure is then only slightly (approximately 40 psi) above reactor pressure. The differential pressure resulting from valve closure, the "water hammer" term, does not apply. This term accounts for the deceleration of the fluid during closure and uses the pressure wave movement through the pipe. Since this valve is not closed until another flow path is available, the pressure wave is eliminated by the flow path. The actual closing differential pressure is, therefore, 1140 psid.

MOV E41-F011

MOV E41-F011 is the redundant CST Test return isolation valve for both HPCI and RCIC, and discharges to the CST. As discussed in the BWROG Report, this valve has no safety function. The valve is normally closed and is only opened for testing or reactor pressure control. The opening torque switch is jumpered out; therefore, full motor torque can be applied to opening the valve. Maximum pressure is expected upstream of the valve.

BSEP procedures call for opening this valve under conditions of negligible differential pressure. This valve is opened prior to the opening of the E41-F008 or E51-F022 valves which isolate it from each system and, therefore, from high upstream pressures. For conservatism, the pressures obtained for the E41-F008 valve have been used for this valve also.

This valve is closed under conditions ranging from no differential pressure, to that seen upon transfer of flow paths following an automatic initiation. The same rationale utilized for the E41-F008 valve applies to this valve. Therefore, the same closing differential pressure also applies (1140 psid).

MOV E51-F022

MOV E51-F022 is the RCIC pump CST Test return line isolation valve, and discharges to the CST. As discussed in the BWROG Report, this valve has no safety function. The valve is normally closed, and is only opened for testing or reactor pressure control.

Since the valve is a globe valve, flow will assist in opening the valve. With the opening torque switch jumpered out, full motor torque can be applied to opening the valve. Maximum pressure is expected upstream of the valve and, therefore, assists in opening the valve. For these reasons, the valve opening differential pressure is of no concern. For conservatism, however, the existing valve design differential pressure of 1140 psid have been utilized for this response.

BSEP procedures call for closing this valve under various conditions. These include closure after turbine shutdown, closure at a turbine speed of 2300 rpm (340 psi pump discharge pressure), and closure upon transfer of flow paths following an automatic initiation. In this final case, the injection valve is open before this valve reaches the full closed position. In the pressure is then only slightly (approximately 110 psi) above reactor pressure. The differential pressure resulting from valve closure, the "water hammer" term, does not apply. This term accounts for the deceleration of the fluid during closure and uses the pressure wave movement through the pipe. Since this valve is not closed until another flow path is available, the pressure wave is eliminated by the flow path. The actual closing differential pressure is, therefore, 1140 psid.

B. Switch Settings

Action (b) requires that the correct switch settings be established for the differential pressures calculated in Action (a) above. It also requires the establishment of a program to review and revise, as necessary, the methods for selecting and setting all switches (i.e., torque, torque bypass, limit, and overload).

The procedures used to set torque switch bypass and position limit switches at BSEP have been reviewed and found to be acceptable. Switches are set four-percent from the full-opened and full-closed positions unless otherwise evaluated. The four-percent positions are determined by the total number of handwheel turns for the valves (listed on the data sheet). The problem encountered at Davis-Besse 1, as a result of counting handwheel turns, is not considered applicable to BSEP since for those valves governed by this Bulletin that are required to open against a differential pressure, the open torque switches are jumpered out for the full stroke of the valve. For those valves required to close, the limit switch is jumpered out to allow for torque seating of the valve.

The methodology used to determine overload protection setpoints has been reviewed and found to be acceptable. This methodology (coordination verification and component selection for safety-related valves) has been established using the guidance of Regulatory Guide 1.106 in that the uncertainties with respect to coordination are resolved in favor of the valve performing its design function.

A majority of the valves in this response (see Table 1 and 2) were tested against the calculated differential pressure, or a larger value, by the valve vendor prior to shipment. The actuator design torque values supplied by the valve vendor have, therefore, been previously verified and will be used as the minimum allowable torque value. The same philosophy applies to those valves that are "type tested". The required torque settings for these valves are listed in Tables 1 and 2.

For those valves that do not fall into the above grouping, the actuator torque required for proper operation against the calculated differential pressure was determined based on the valve vendor input, the actuator vendor input, and, as required, the results of differential testing. The methodology for determining the required torque settings for the valves in this grouping are detailed in Section C below. The required torque settings for these valves are listed in Table 1 and 2.

The Unit I valve actuators that are subject to the requirements of the Bulletin were completely rebuilt prior to stroke testing and therefore the "as-found" operability cannot be directly determined. There were no significant problems noted during the rebuilding or stroke testing of the Unit I actuators that would have been expected to result in valve inoperability. No valves tested as a result of this Bulletin were determined to be inoperable.

C. Valve Testing

Action (c) requires that valve torque switch settings shall be changed, as appropriate, to those determined in Action (b) above. This item also requires valve testing at the differential pressure calculated in Action (a) above, except where that differential pressure is the result of a line break.

The initial response to IEB 85-03 (Reference 1) specified that for valves for which differential pressure test data at the calculated differential pressure could not be found, or for which a "type test" valve could not be found, a test would be performed. Two such tests were required.

The first test was for the HPCI and RCIC turbine exhaust line vacuum breaker Isolation Valves 1-E41-F075, 1-E41-F079, 1-E51-F062, and 1-E51-F066, respectively. These valve/actuator assemblies are identical, and so meet the criteria for "type testing". The 1-E51-F062 was chosen for the test.

Special Procedure 87-022 was written to control and document the testing. The testing was done at the 27 psid value calculated for the valve, and the valve opened and closed properly at this differential pressure. Prior to the differential pressure test, the valve was verified to torque out at 34 ft-lbs. This torque value will therefore be the minimum setting allowable for the four valves mentioned above.

The second test was for the HPCI pump Condensate Storage Tank Suction. Valve 1-E41-F004. Special Procedure 87-028 was written to control and document the testing. The testing was done at a 38 psi differential. The only available test connection upstream of the valve is a 3/4-inch vons line. Sufficient flow could not be maintained to keep the downstream open using this 3/4-inch connection. The valve therefore closed differential pressure. The above result was a concern during the

phase, therefore, Anchor Darling (the valve vendor) was requested to evaluate the valve/actuator assembly at a differential pressure of 43 psid. The vendor responded that the valve/actuator assembly was acceptable at the higher differential pressure, and no adjustments were necessary. Based on the Anchor Darling response, no additional pressure testing was performed. This testing would have required disassembly of the downstream check valve for an adequate test.

The valves governed by this Bulletin were stroke tested in both the open and closed direction with the actuator output torque, spring-pack deflection, spring force, and motor current monitored for each valve. The as-found and as-left actuator output torque for each valve is listed in Tables I and 2.

D. Control of Switch Settings

Action (d) requires that procedures be prepared or revised to ensure that the correct switch settings are determined and maintained throughout the life of the plant.

The initial response to IEB 85-03 (Reference 1) specified that a procedure would be initiated to control the limit and torque switch settings for the valves of concern. The necessary requirements for changing a setting were also to be given. Engineering Procedure ENP-43, "Motor-Operated Valve Switch Settings," was therefore written to satisfy this requirement.

ENP-43 was originally written to specify HPCI and RCIC MOV torque and limit switch settings. This procedure has since been expanded to cover safety-related MOVs in general. Additionally, ENP-43 was revised to specify actuator torque requirements instead of torque switch settings, since torque switch settings alone may not guarantee that the actuator will develop adequate torque/thrust. Torque switch settings are no longer used as the sole acceptance criteria for setting up actuators since the actuator torque/thrust can vary depending on the "stiffness" (spring constant and force preload) of the spring-pack.

ENP-43 identifies the responsibilities of the various personnel involved in the control and adjustment of limit switches and actuator torque, and provides the guidelines necessary to ensure this control is maintained. It provides for informing the responsible System Engineer of all changes, and covers the methodology to be used to evaluate changes for settings outside the approved range.

I&C and mechanical technicians have been trained to set limit and torque switches and in general MOV maintenance by INPO accredited Craft and Technical Development training (C&TD). C&TD training is both formal and documented. In addition, the technicians receive on-the-job training on installed equipment in the plant. Technicians set the switches in accordance with detailed, approved maintenance procedures. Selected technicians, mechanics, and maintenance engineers have received specialized training from Limitorque on diagnostic testing and evaluation of diagnostic test results. Additionally, selected I&C and mechanical technicians have received detailed, specialized training from Power Safety on the maintenance of Limitorque valve operators.

E & F. Schedule and Report

References 1 and 2 provided a written report of the results of Action (a) and contained the program to accomplish Actions (b) through (d), including the schedule for completion.

This submittal provides a written report regarding the implementation and completion (except as noted in Reference 4) of the IE Bulletin 85-03 program at BSEP. The valves tested as a result of this Bulletin were determined to be operable, and a data summary is included in Tables 1 and 2.

TABLE I OF ATTACHMENT I

TER TYPE	
VALVE	FUNCTION

MANY NOTULY . X

TURBINE STEAM SUPPLY ANCHOL DARLING

VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (* CLASS)
GATE	1278-3	10	600#

ACTUATOR MANUFACTURER	OPERATOR MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
* ************************************	***********		==========
LIMITORQUE	SMB-1	1900.00	62.38

DESIGN		TEST CASE DIFFERENTIAL
OPEN	CLOSE	PRESSURE (PSID)
1105	N/A	1118

TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	584	561	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

* ACTUATOR WAS REBUILT PRIOR TO TESTING.

2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

	E FUNCTION		MANUFACTURER
STEAM SUPPLY	INBOARD I	SOLATION	ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1215-3	10	600#
ACTUATOR MANUFACTURER	OPERATOR MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-1	3400.00	46.95

DESIGN DIFFERENTIAL	BASIS PRESSURE	TEST CASE DIFFERENTIAL
OPEN	CLOSE	PRESSURE (PSID)
1105	1105	1118

TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
	627	561	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

		FUNCTION		MANUFACTURER
STEAM	SUPPLY	OUTBOARD	****	ANCHOR-DARLING

VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1217-3	10	600#

ACTUATOR MANUFACTURER	OPERATOR MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
TTVTTTTTTT	**********		
LIMITORQUE	SMB-1	1900.00	24.60

DESIGN DIFFERENTIAL	BASIS PRESSURE	TEST CASE DIFFERENTIAL
OPEN	CLOSE	PRESSURE (PSID)
1105	1105	1118

TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	651	568	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

- * ACTUATOR WAS REBUILT PRIOR TO TESTING.
- 1) OPENING TORQUE SWITCH IS JUMPERED OUT.
- 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

VA	LVE FUNCTION		MANUFACTURER
	CST SUCTION		ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1241-3	16	150#
ACTUATOR MANUFACTURE	OPERATOR R MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	49.22
DESIG DIFFERENTIA	N BASIS L PRESSURE		RENTIAL
OPEN	CLOSE		SSURE SID)
N/A	43	3	10
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	HAG BOWER
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	106	92	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve could not be tested at calculated differential pressure. Accepted based on vendor information.

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT. 2) OPENING TORQUE SWITCH IS JUMPERED OUT.

VAL	VE FUNCTION		MANUFACTURER
	INJECTION		ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1226-3	14	900#
ACTUATOR MANUFACTURES	OPERATOR MODEL	PPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-3	1900.00	35.38
DESIGN DIFFERENTIAL	BASIS PRESSURE		CASE RENTIAL SSURE
OPEN	CLOSE	(PS	SID)
1260	1368		50
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	1792	1615	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

MANUFACTURER

CST TEST RETURN

ANCHOR-DARLING

VALVE PRESSURE VALVE VALVE SIZE HATING MODEL (INCHES) (# CLASS) TYPE GLOBE 1727-3 10 900#

UNIT QUTPUT ACTUATOR OPERATOR MOTOR SPEED ANUFACTURER MODEL RPM (RPM) MANUFACTURER LIMITORQUE SMB-3 1900.00 10.99

DESIGN BASIS DIFFERENTIAL PRESSURE

TEST CASE DIFFERENTIAL PRESSURE

OPEN CLOSE (PSID)

1140 1140 1140

TORQUE TORQUE PRIOR TO AFTER DESIGN ADJUSTMENT ADJUSTMENT TORQUE

"AS-FOUND" (FT-LB) (FT-LB) (FT-LB) OPERABILITY 2691 2660 OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

- * ACTUATOR WAS REBUILT PRIOR TO TESTING.
- 1) OPENING TORQUE SWITCH IS JUMPERED OUT.
- 2) GLOSING LIMIT SWITCH IS JUMPERED OUT.

1-E41-F011

VALVE FUNCTION

MANUFACTURER

CST TEST RETURN

ANCHOR-DARLING

VALVE VE , 'NEL

VALVE PRESSURE SIZE

RATING

(INCHES) (# CLASS)

GATE 1728-3

10

900#

ACTUATOR OPERATOR MOTOR MANUFACTURER MODEL RPM

UNIT OUTPUT SPEED (RPM)

LIMITORQUE SMB-0 1900.00 30.82

DESIGN BASIS DIFFERENTIAL PRESSURE

TEST CASE DIFFERENTIAL PRESSURE

OPEN CLOSE

(PSID)

1140

1140

TORQUE TORQUE PRIOR TO AFTER

DESIGN

ADJUSTMENT ADJUSTMENT TORQUE

(FT-LB)

"AS-FOUND" (FT-LB) (FT-LB) OPERABILITY

520

488

OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

- 1) OPENING TORQUE SWITCH IS JUMPERED OUT.
- 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

V'A)	MANUFACTURER				
MINT	MUM FLOW BYPA	ss	SS ANCHOR-DARLING		
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)		
GLOBE	1725-3	4	600#		
ACTUATOR MANUFACTURE	CPERATOR R MODEL	RPM	UNIT OUTPUT SPEED (RPM)		
LIMITORQUE		1900.00			
DESIG DIFFERENTIA	N BASIS L PRESSURE	DIFFE	CASE RENTIAL		
OPEN	CLOSE	(PS	SSURE SID)		
950	1140		140		
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE			
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY		
*	250				

TEST METHOD, DESCRIPTION AND JUSTIFICATION

250

Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

252

OPERABLE

- * ACTUATOR WAS REBUILT PRIOR TO TESTING.
- 1) OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.
- 3) ACTUAL TORQUE IS SLIGHTLY LOWER THAN DESIGN, BUT IS ACCEPTABLE BASED ON CALCULATIONS OF REQUIRED TORQUE.

	MANUFACTURER		
SUPPRES	SION POOL SU	CTION	ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	RATING (# CLASS)
GATE	1242-3	16	150#
MANUFACTUR	OPERATOR ER MODEL	RPM	UNII OUTPUT SPEED (RPM)
LIMITORQUI		1900.00	24.68
DESIG DIFFERENTIA	GN BASIS AL PRESSURE	DIFFE	CASE RENTIAL
OPEN	CLOSE		SSURE SID)
97	30		00
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	176	172	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated ifferential pressure by vendor and requires no further testing.

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VA	MANUFACTURER			
			ANCHOR-DARLING	
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)	
GATE	1211-3	16	150#	
ACTUATOR MANUFACTURE	OPERATOR ER MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)	
LIMITORQUI	SMB-00	1900.00	24.68	
DESIG	ON BASIS	DIFFE	CASE RENTIAL	
OPEN	CLOSE		SSURE SID)	
97	30	1(00	
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE		
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY	
*	224	172.5	OPERABLE	

TEST METHOD, DESCRIPTION AND JUSTIFICATION ************************* Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VAI	LVE FUNCTION	========	MANUFACTURER
COOLIN	IG WATER SUF	PLY	VELAN
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	RATING (# CLASS)
GLOBE W	8-274B-2TS	2	500 #
ACTUATOR MANUFACTURE	R MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-000	1900.00	27.94
DESIGN DIFFERENTIAL	BASIS PRESSURE		ENTIAL
OPEN	CLOSE	/ DC	SURE ID)
30	33	46	0
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
	38	17.5	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

V	ALVE FUNCTIO	N	MANUFACTURER
TURBINE E	XHAUST VACUU	M BREAKER	VELAN
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GLOBE W	08-2074X-02T	S 2	600 #
ACTUATOR MANUFACTUR	ER MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQU	E SMB-000	1800.00	16.14
DESIGN DIFFERENTIA	GN BASIS AL PRESSURE	TEST DIFFER	CASE RENTIAL
OPEN	CLOSE		SEURE SID)
N/A	27	2	8
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	35	34	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve identical to one previously tested against calculated differential pressure and, therefore, by "type testing" required no further testing.

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ CLOSING LIMIT SWITCH JUMPERED OUT.

	=======	VALVE F	UNCTION		MANUFACTURER
	TURBINE	EXHAUST	VACUUM	BREAKER	VELAN
	VALVE TYPE		LVE	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
	GLOBE	W08-207	74X-02TS	2	600 #
	ACTUATO	URER	PERATOR MODEL	RPM	UNIT OUTPUT SPEED (RPM)
	LIMITOR	QUE S	MB-000	1800.00	16.14
	DES	SIGN BAS	IS SSURE		RENTIAL
	OPEN		CLOSE		SSURE SID)
	N/A		27	2	8
	TORQUE PRIOR TO ADJUSTMEN	AFT	RQUE TER STMENT	DESIGN TORQUE	
-	(FT-LB)	(FT-	LB)	(FT-LB)	"AS-FOUND" OPERABILITY
	*	3	8	34	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve identical to one previously tested against calculated differential pressure and, therefore, by "type testing" required no further testing.

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ CLOSING LIMIT SWITCH JUMPERED OUT.

VAL	VE FUNCTION		MANUFACTURER
STEAM SUPPL	Y INBOARD I	SOLATION	ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1220-3	4	600#
ACTUATOR MANUFACTURES	MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1800.00	52.79
DESIGN DIFFERENTIAL	BASIS PRESSURE	DIFFE	CASE RENTIAL
OPEN	CLOSE		SSURE SID)
1105	1105	1)	38
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	39	38	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

	VALVE	FUNCTION	4	MANUFACTURER
======		=======		===========
STEAM	SUPPLY	OUTBOARD	ISOLATION	ANCHOR-DARLING

VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1723-3	3	600#

ACTUATOR MANUFACTURER	OPERATOR MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	49.22

DESIGN DIFFERENTIAL	BASIS PRESSURE	TEST CASE DIFFERENTIAL
OPEN	CLOSE	PRESSURE (PSID)
		=============
1105	1105	1135

TORQUE PRIOR TO	TORQUE AFTER	DESIGN	
ADJUSTMENT	ADJUSTMENT	TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	69	37.9	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

-========	LVE FUNCTION		MANUFACTURER
	CST SUCTION		ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1243-3	6	150#
ACTUATOR MANUFACTUR	OPERATOR ER MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQU	E SMB-00	1900.00	49.22
DESIG	ON BASIS	DIFFER	CASE RENTIAL
OPEN	CLOSE		SSURE SID)
N/A	30	3	30
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	41	22.8	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

* ACTUATOR WAS REBUILT PRIOR TO TESTING.

1) CLOSING LIMIT SWITCH JUMPERED OUT.

²⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

VA	LVE FUNCTION		MANUFACTURER		
	INJECTION	ANCHOR-DARLING			
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)		
GATE	1227-3	4	900#		
ACTUATOR MANUFACTURE	R MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)		
LIMITORQUE		1900.00	67.38		
DESIG DIFFERENTIA	N BASIS L PRESSURE	DIFFE	CASE RENTIAL		
OPEN	CLOSE	PRESSURE (PSID)			
1140	440	1:	140		
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE			
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY		
*	93	64	OPERABLE		

TEST METHOD, DESCRIPTION AND JUSTIFICATION

Valve tested against calculated differential pressure by vendor and requires no further testing.

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VAL	VE FUNCTION		MANUFACTURER
MINIM	UM FLOW BYPA		VELAN
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	RATING (# CLASS)
GLOBE WE	3-274B-2TS	2	600 #
ACTUATOR MANUFACTURER	OPERATOR MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-000	1900.00	27.94
DESIGN DIFFERENTIAL OPEN	BASIS PRESSURE CLOSE	PRES	CASE RENTIAL SURE
1124	1280		30
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	

TEST METHOD, DESCRIPTION AND JUSTIFICATION -----Valve tested against calculated differential pressur by vendor and requires no further testing.

46

(FT-LB) (FT-LB) (FT-LB) OPERABILITY

"AS-FOUND"

OPERABLE

GENERAL COMMENTS

35.6

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

1-E51-F022

VALVE FUNCTION MANUFACTURER

CST TEST RETURN

ANCHOR-DARLING

VALVE TYPE

VALVE MODEL VALVE PRESSURE

(INCHES) (# CLASS)

GLOBE 1721-3 4

900#

ACTUATOR MANUFACTURER

OPERATOR MOTOR MODEL

RPM

UNIT QUTPUT SPEED (RPM)

LIMITORQUE SMB-0 1900.00 19.75

DESIGN BASIS DIFFERENTIAL PRESSURE

TEST CASE DIFFERENTIAL PRESSURE

OPEN

CLOSE

(PSID)

1140

1140

1140

PRIOR TO

TORQUE TORQUE PRIOR TO AFTER

DESIGN

ADJUSTMENT ADJUSTMENT TORQUE

"AS-FOUND" (FT-LB) (FT-LB) (FT-LB) OPERABILITY

214 214

OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressur by vendor and requires no further testing.

GENERAL COMMENTS

- 1) OPENING TORQUE SWITCH IS JUMPERED OUT.
- 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

VAL	VE FUNCTION		MANUFACTURER
SUPPRESS	ON POOL SUC	CTION	ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1243-3	6	150#
ACTUATOR MANUFACTURER		RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	49.22
DESIGN DIFFERENTIAL	BASIS PRESSURE	DIFFE	CASE RENTIAL
OPEN	CLOSE		SSURE SID)
97	30	10	
TORQUE PRIOR TO ADJUSTMENT A	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY

TEST METHOD, DESCRIPTION AND JUSTIFICATION

VALVE IS IDENTICAL TO ONE PREVIOUSLY TESTED

AGAINST CALCULATED DIFFERENTIAL PRESSURE AND,

THEREFORE, BY "TYPE TESTING". NO FURTHER

TESTING IS REQUIRED.

GENERAL COMMENTS

44 22.8 OPERABLE

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

VAL	VE FUNCTION		MANUFACTURER
SUPPRESSION POOL SUCTION			ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1213-3	6	150#
ACTUATOR MANUFACTURER	MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	49.22
DESIGN DIFFERENTIAL	BASIS PRESSURE	DIFFE	CASE RENTIAL
OPEN	CLOSE		
97	30	10	00
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	52	29	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

1-E51-F045

VALVE FUNCTION MANUFACTURER TURBINE STEAM SUPPLY ANCHOR-DARLING

VALVE PRESSURE VALVE VALVE SIZE RATING MODEL (INCHES) (# CLASS) TYPE GATE 1283-3 3 600 #

UNIT OUTPUT ACTUATOR OPERATOR MOTOR SPEED MANUFACTURER MODEL RPM (RPM) LIMITORQUE SMB-00 1900.00 43.58

DESIGN BASIS TEST CASE DIFFERENTIAL PRESSURE DIFFERENTIAL PRESSURE OPEN CLOSE (PSID) 1105

TORQUE TORQUE PRIOR TO AFTER DESIGN ADJUSTMENT ADJUSTMENT TORQUE

"AS-FOUND" (FT-LB) (FT-LB) (FT-LB) OPERABILITY 185.1 124 OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION -------This valve was previously tested against calculated differential pressure and requires no further testing.

GENERAL COMMENTS

- * ACTUATOR WAS REBUILT PRIOR TO TESTING.
- 1) OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

VAL	VE FUNCTION		MANUFACTURER
COOLING	WATER SUP	PLY	VELAN
VALVE TYPE	VALVE MODEL	SIZE (INCHES)	
	-274B-2TS	2	600 #
ACTUATOR MANUFACTURER	OPERATOR MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE			27.94
DESIGN DIFFERENTIAL OPEN	PRESSURE	PRES	CASE RENTIAL SSURE
1328	33	13	30
TORQUE PRIOR TO ADJUSTMENT A	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	HAG POWER
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY

TLST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential press re by vendor and requires no further testing.

41

GENERAL COMMENTS

35.6

OPERABLE

- * ACTUATOR WAS REBUILT PRIOR TO TESTING.
- 1) OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

	VALVE FU	UNCTION		MANUFACTURER
TURBINE I	EXHAUST	VACUUM	BREAKER	VELAN
VALVE TYPE	VAI	VE	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GLOBE	WO8-207	4X-02TS	2	600 #
ACTUATO MANUFACTU	and the same of th	PERATOR MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQ	UE S	MB-000	1800.00	16.14
DES DIFFERENT	IGN BAS	IS SSURE	DIFFE	CASE RENTIAL
OPEN		CLOSE	(P	SSURE SID)
N/A		27		====== 28
TORQUE PRIOR TO ADJUSTMENT	AFT	RQUE TER STMENT	DESIGN TORQUE	
(FT-LB)	(FT-	LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	3	4	34	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve was tested against the calculated differental pressure under Special Procedure 87-022

GENERAL COMMENTS

¹⁾ CLOSING LIMIT SWITCH JUMPERED OUT.

=======	VALVE F			MANUFACTURER
TURBINE	EXHAUST	VACUUM	BREAKER	VELAN
VALVE TYPE	VAI MOI	LVE	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GLOBE	W08-207	4X-02TS	2	600 #
ACTUAT	OR O	PERATOR MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITOR	QUE S	MB-000	1800.00	16.14
DES	SIGN BAS	IS SSURE	DIFFER	CASE
OPEN		CLOSE		SSURE SID)
N/A		27	2	8
TORQUE PRIOR TO ADJUSTMEN	AFT	RQUE TER STMENT	DESIGN TORQUE	
(FT-LB)	(FT-	LB)	(FT-LB)	"AS-FOUND" OPERABILITY
*	4	6	34	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION
Valve identical to one previously tested
against calculated differential pressure
and, therefore, by "type testing" required
no further testing

^{*} ACTUATOR WAS REBUILT PRIOR TO TESTING.

¹⁾ CLOSING LIMIT SWITCH JUMPERED OUT.

TABLE 2 OF ATTACHMENT 1

VALV	E FUNCTION	.=======	MANUFACTURER
TURBINE	STEAM SUPE	PLY	ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1278-3	10	600#
ACTUATOR MANUFACTURER	OPERATOR MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-1	1900.00	62.38
DESIGN DIFFERENTIAL	BASIS PRESSURE		RENTIAL
OPEN	CLOSE	(PS	SSURE SID)
1105	N/A		18
TORQUE PRIOR TO ADJUSTMENT A	TORQUE AFTER DJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
632	606	561	OPERABLE

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

V)	LVE FUNCTION		MANUFACTURER
STEAM SUPE	PLY INBOARD I	SOLATION	ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1215-3	10	600#
ACTUATOR MANUFACTUR	OPERATO: ER MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUI	E SMB-1	3400.00	46.95
DESIG DIFFERENTIA	SN BASIS AL PRESSURE	DIFFER	CASE RENTIAL
OPEN	CLOSE	(FSID)	
1105	1105		.68
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	UNG POWER
(FT-LB)	(FT-LE)	(FT-LB)	"AS-FOUND" OPERABILITY
587	587	561	OPERABLE

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

VAL	VE FUNCTION		MANUFACTURER
STEAM SUPPLY		ISOLATION	ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1217-3	10	600#
ACTUATOR MANUFACTURER	OPERATOR MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-1	1900.00	24.60
DESIGN DIFFERENTIAL	BASIS PRESSURE	DIFFE	CASE RENTIAL
OPEN	CLOSE	PRESSURE (PSID)	
1105	1105	1	118
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
613	613	568	OPERABLE

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VA	LVE FUNCTION		MANUFACTURER
	CST SUCTION		ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1241-3	16	150#
ACTUATOR MANUFACTURE	R MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	49.22
DESIG DIFFERENTIA	N BASIS L PRESSURE	DIFFE	CASE RENTIAL
OPEN	CLOSE	(1910)	
N/A	43	3	30
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
130	130	92	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION -----Valve could not be tested at calculated diffential pressure. Accepted based on vendor information.

GENERAL COMMENTS

1) CLOSING LIMIT SWITCH IS JUMPERED OUT.

²⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

VA:	LVE FUNCTION	========	MANUFACTURER
	INJECTION		ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1226-3	14	900#
ACTUATOR MANUFACTURE	OPERATOR R MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-3	1900.00	35.38
DIFFERENTIA	N BASIS L PRESSURE		CASE RENTIAL SURE
OPEN	CLOSE	(PSID)	
1260	1368	15	50
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
2381	1871	1615	OPERABLE

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

VALVE FUNCTION

MANUFACTURER

CST TEST RETURN ANCHOR-DARLING

VALVE TYPE

VALVE

SIZE

VALVE PRESSURE RATING MODEL (INCHES) (# CLASS)

GLOBE 1727-3

10

900#

ACTUATOR MANUFACTURER

OPERATOR MODEL

MOTOR RPM

UNIT OUTPUT SPEED (RPM)

LIMITORQUE SMB-3 1900.00 10.99

DESIGN BASIS DIFFERENTIAL PRESSURE

TEST CASE DIFFERENTIAL PRESSURE

OPEN

CLOSE

1140

1140

1140

TORQUE FORQUE

PRIOR TO ADJUSTMENT ADJUSTMENT TORQUE

AFTER

"AS-FOUND" (FT-LB) (FT-LB) (FT-LB) OPERABILITY

2835

2835 2660

OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

VALVE FUNCTION

MANUFACTURER

CST TEST RETURN

ANCHOR-DARLING

VALVE TYPE

VALVE

VALVE PRESSURE SIZE

RATING

MODEL

(INCHES) (# CLASS)

GATE

1728-3 10

900#

ACTUATOR OPERATOR MOTOR MANUFACTURER MODEL RPM

UNIT OUTPUT SPEED (RPM)

LIMITORQUE SMB-0 1900.00 30.82

DESIGN BASIS DIFFERENTIAL PRESSURE

TEST CASE DIFFERENTIAL PRESSURE

OPEN CLOSE

(PSID)

1140

1140

1140

TORQUE TORQUE PRIOR TO AFTER

DESIGN

ADJUSTMENT ADJUSTMENT TORQUE

(FT-LB)

"AS-FOUND" (FT-LB) (FT-LB) OPERABILITY

500

495

488 OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

VA	LVE FUNCTION		MANUFACTURER
MTNT	MUM FLOW BYF		
	MOM FLOW BYF	ASS	ANCHOR-DARLING
		VALVE	
VALVE	VALVE	SIZE	PRESSURE
TYPE	MODEL	(INCHES)	RATING
	==========	=========	(# CLASS)
GLOBE	1725-3	4	600#
10771170			UNIT OUTPUT
ACTUATOR	OPERATO	R MOTOR	SPEED
MANUFACTUR		RPM	(RPM)
LIMITORQUI			=======================================
ZIMITORQUI	E SMB-0	1900.10	48.59
DESIGN DIFFERENTIA	GN BASIS AL PRESSURE		CASE
	L PRESSURE		RENTIAL
OPEN	CLOSE	PRESSURE (PSID)	
950	1140		140
TORQUE	TORQUE		
PRIOR TO	AFTER	DESIGN	
ADJUSTMENT	ADJUSTMENT	TORQUE	
(FT-L3)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
443	274	252	OPERABLE

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.
2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

2-E51-F022

VALVE FUNCTION _______

MANUFACTURER

CST TEST RETURN ANCHOR-DARLING

VALVE TYPE

VALVE MODEL

VALVE PRESSURE SIZE (INCHES) (# CLASS)

RATING

GLOBE 1721-3

ACTUATOR OPERATOR MOTOR MANUFACTURER MODEL

RPM

UNIT OUTPUT SPEED (RPM)

_______ LIMITORQUE SMB-0 1900.00 19.75

DESIGN BASIS DIFFERENTIAL PRESSURE

TEST CASE DIFFERENTIAL PRESSURE

OPEN CLOSE

(PSID)

1140

1140

TORQUE TORQUE PRIOR TO AFTER AFTER

ADJUSTMENT ADJUSTMENT TORQUE

DESIGN

"AS-FOUND" (FT-LB) (FT-LB) (FT-LB) OPERABILITY

284

214

OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve tested against calculated differential pressur by vendor and requires no further testing.

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

2) CLOSING LIMIT SWITCH IS JUMPERED DUT.

	LVE FUNCTION	=======	MANUFACTURER
SUPPRES	SION POOL SU	CTION	ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1242-3	16	150#
ACTUATOR MANUFACTURE		RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	24.68
DESIG DIFFERENTIA	N BASIS L PRESSURE		RENTIAL
OPEN	CLOSE	PRESSURE (PSID)	
97	30	10	0
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
237	223	172	OPERABLE

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VA:	MANUFACTURER		
	SION POOL SUC		ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1211-3	16	150#
ACTUATOR MANUFACTURE		RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	24.68
DESIG DIFFERENTIA	N BASIS L PRESSURE	DIFFE	CASE RENTIAL
OPEN	CLOSE	PRESSURE (PSID)	
97	30	10	00
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
212	198	172.5	OPERABLE

GENERAL COMMENTS

1) OPEWING TORQUE SWITCH IS JUMPERED OUT.
2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

2-E51-F045

VALVE FUNCTION MANUFACTURER TURBINE STEAM SUPPLY ANCHOR-DARLING

VALVE PRESSURE VALVE VALVE RATING MODEL (INCHES) (# CLASS) TYPE GLOBE 1283-3 3.00 600 #

UNIT OUTPUT ACTUATOR OPERATOR MOTOR SPEED MANUFACTURER MODEL RPM (RPM) LIMITORQUE SMB-00 1900.00 43.58

DESIGN BASIS TEST CASE DIFFERENTIAL PRESSURE DIFFERENTIAL PRESSURE OPEN CLOSE (PSID) 1105 1105

TORQUE TORQUE PRIOR TO AFTER PRIOR TO DESIGN ADJUSTMENT ADJUSTMENT TORQUE

"AS-FOUND" (FT-LB) (FT-LB) (FT-LB) OPERABILITY 114 155 124 OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve previously tested against calculated differential pressure and requires no further testing.

GENERAL COMMENTS

- 1) OPENING TORQUE SWITCH IS JUMPERED OUT.
- 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.
- 3) VALVE AS-FOUND TORQUE IS SLIGHTLY LOWER THAN DESIGN, BUT WAS ACCEPTABLE BASED ON CALCULATION OF REQUIRED TORQUE.

V	LVE FUNCTION		MANUFACTURER
COULT	NG WATER SUP	PLY	VELAN
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GLOBE	W8-274B-2TS	2	600 #
ACTUATOR MANUFACTUR	ER MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQU	E SMB-000	1900.00	27.94
DESIO DIFFERENTIA	GN BASIS AL PRESSURE		RENTIAL
OPEN	CLOSE		SURE
30	33	46	0
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
32	32	17.5	OPERABLE

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VALVE FUNCTION

4========	ALVE F	JNCTION		MANUFACTURER
TURBINE E	XHAUST	VACUUM	BREAKER	VELAN
VALVE TYPE	VAI		VALVE SIZE (INCHES)	RATING (# CLASS)
GATE	W8-254		2	600 #
ACTUATO: MANUFACTU	RER	MODEL	RPM	(RPM)
LIMITORQ		MB-000	1800.00	
DESI	IGN BAS	IS SSURE	DIFFE	CASE CRENTIAL
OPEN		CLOSE	(F	SSURE PSID)
N/A		27	6	00
TORQUE PRIOR TO ADJUSTMENT	AFT		DESIGN TORQUE	
(FT-LB)	(FT-		(FT-LB)	"AS-FOUND" OPERABILITY
36	3	6	10.8	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve is identical to one previously tested against calculated differential pressure and, therefore, by "type testing", so no further testing is required.

¹⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VA	LVE FUNCTIO		MANUFACTURER	
TURBINE EX	HAUST VACUU	M BREAKER	VELAN	
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	RATING	
GATE	W8-254B-2TS	2	600 #	
ACTUATOR MANUFACTURE	OPERATO ER MODEL	RPM	UNIT OUTPUT SPEED (RPM)	
LIMITORQUI	E SMB-000	1800.00	41.14	
DESIGN DIFFERENTIA	GN BASIS AL PRESSURE	DIFFE	CASE RENTIAL	
OPEN	CLOSE	(P	PRESSURE (PSID)	
N/A	27		00	
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE		
(FT-LB)	(FT-Lb)	(FT-LB)	"AS-FOUND" OPERABILITY	
31	31	10.8	OPERABLE	

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve is identical to one previously tested against calculated differential pressure and, therefore, by "type testing", so no further testing is required.

¹⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VA	MANUFACTURER		
STEAM SUPP	LY INBOARD I	SOLATION	ANCHOR
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1220-3	4	600#
ACTUATOR MANUFACTURE		RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1800.00	52.79
DESIG DIFFERENTIA	N BASIS L PRESSURE		RENTIAL
OPEN	CLOSE	(PS	SURE SID)
1105	1105		38
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
78	58	38	OPERABLE

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT. 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

		E FUNCTION	MANUFACTURER
STEAM	SUPPLY	OUTBOARD	 ANCHOR-DARLING

VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
C1.TT			
GATE	1723-3	3.00	600#

ACTUATOR MANUFACTURER	OPERATOR MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	49.22

DESIGN DIFFERENTIAL		TEST CASE DIFFERENTIAL
OPEN	CLOSE	PRESSURE (PSID)
1105	1105	1135

TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
54	54	37.9	OPERABLE

¹⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VALV	VE FUNCTION	MANUFACTURER	
CST SUCTION			ANCHOR
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1243-3	6	150#
ACTUATOR MANUFACTURER	OPERATOR MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	49.22
DESIGN DIFFERENTIAL OPEN	PRESSURE	PRES	ENTIAL SURE
OPEN	CLOSE	(PS	ID)
N/A	30	3	0
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
62	52	22.8	OPERABLE

¹⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

²⁾ OPENING TORQUE SWITCH IS JUMPERED OUT.

VA	LVE FUNCTION		MANUFACTURER
	INJECTION		ANCHOR-DARLING
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1227-3	4.00	900 #
ACTUATOR MANUFACTURE	R MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	67.38
DESIGN DIFFERENTIA:	N BASIS L PRESSURE		RENTIAL
OPEN	CLOSE		SSURE SID)
1140	440	11	40
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
127	76	64	OPEPABLE

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VALVE FUNCTION

==========	PATA LONGITON		MANUFACTURER
MIN	MUM FLOW BYP	ASS	VELAN
VALVE TYPE	VALVE MODEL	SIZE (INCHES)	(# CLASS)
GLOBE	W8-274B-2TS	2.00	600 #
ACTUATOR MANUFACTUR	OPERATOR ER MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQU			25.33
DESI DIFFERENTI	GN BASIS AL PRESSURE	DIFFER	CASE RENTIAL
OPEN	CLOSE	(PS	SSURE SID)
1124	1280		30
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
31	54	36	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve was tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

³⁾ AS-FOUND TORQUE WAS SLIGHTLY LOWER THAN DESIGN, BUT WAS ACCEPTABLE BASED ON CALCULATION OF REQUIRED TORQUE.

V2	LVE FUNCTION		MANUFACTURER
SUPPRES	SION POOL SU	CTION	ANCHOR
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	RATING (# CLASS)
GATE	1243-3	6	150#
ACTUATOR MANUFACTUR	ER MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQU	2 SMB-00	1900.00	49.22
DESIGN DIFFERENTIA	GN BASIS AL PRESSURE		RENTIAL
OPEN	CLOSE		SURE ID)
97	30	10	0
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
87	43	22.8	OPERABLE

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve is identical to one previously tested against calculated differential pressure and, therefore, by "type testing", so no further testing is required.

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

VA	MANUFACTURER		
SUPPRESSION POOL SUCTION		ANCHOR	
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GATE	1213-3	6	150#
ACTUATOR MANUFACTURE	OPERATOR R MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQUE	SMB-00	1900.00	49.22
DESIG DIFFERENTIA	N BASIS L PRESSURE		RENTIAL
OPEN	CLOSE		SSURE SID)
97	30	10	00
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE	
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY
53	53	29	OPERABLE

- 1) OPENING TORQUE SWITCH IS JUMPERED OUT.
- 2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

ANUFACTURER
CHOR-DARLING
CHOR-

VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)
GLOBE	1283-3	3.00	600 #

ACTUATOR MANUFACTURER	OPERATOR MODEL	MOTOR RPM	UNIT OUTPUT SPEED (RPM)
TTWEMODALL			
LIMITORQUE	SMB-00	1900.00	43.58

DESIGN DIFFERENTIAL	BASIS PRESSURE	TEST CASE DIFFERENTIAL
OPEN	CLOSE	PRESSURE (PSID)
1105	N/A	1135

TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE		
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY	
114	155	124	OPERABLE	

TEST METHOD, DESCRIPTION AND JUSTIFICATION ************************* Valve previously tested against calculated differential pressure and requires no further testing.

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

2) CLOSING LIMIT SWITCH IS JUMPERED OUT.

³⁾ VALVE AS-FOUND TORQUE IS SLIGHTLY LOWER THAN DESIGN, BUT WAS ACCEPTABLE BASED ON CALCULATION OF REQUIRED TORQUE.

VA	LVE FUNCTION		MANUFACTURER	
COOLI	NG WATER SUP	PLY	VELAN	
VALVE TYPE	VALVE MODEL	VALVE SIZE (INCHES)	PRESSURE RATING (# CLASS)	
GLOBE	W8-274B-2TS	2	600 #	
ACTUATOR MANUFACTURE	ER MODEL	RPM	UNI': OUTPUT SPEED (RPM)	
LIMITORQUI	SMB-000	1900.00	25.33	
DESIG	N BASIS		RENTIAL	
OPEN CLOSE		PRESSURE (PSID)		
1328	33	13	30	
TORQUE PRIOR TO ADJUSTMENT	TORQUE AFTER ADJUSTMENT	DESIGN TORQUE		
(FT-LB)	(FT-LB)	(FT-LB)	"AS-FOUND" OPERABILITY	
150	38	36	OPERABLE	

TEST METHOD, DESCRIPTION AND JUSTIFICATION Valve was tested against calculated differential pressure by vendor and requires no further testing.

GENERAL COMMENTS

1) OPENING TORQUE SWITCH IS JUMPERED OUT.

²⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

	VALVE FU	NCTION		MANUFACTURE	ER
TURBINE	EXHAUST	VACUUM	BREAKER	VELAN	
VALVE TYPE	VALV MODE		VALVE SIZE (INCHES)	RATING	
GATE	W8-274E	3-2TS	2	600 #	==
ACTUATO MANUFACTU	RER M	ERATOR	RPM	(RPM)	
LIMITORQ	UE SM	B-000	1800.0	0 45.00	-
DES DIFFERENT	IGN BASI	S SURE	DIFF	T CASE ERENTIAL	
OPEN CLOSE		PRESSURE (PSID)			
N/A		27		500	
TORQUE PRIOR TO ADJUSTMENT	AFTE	CR	DESIGN TORQUE		
(FT-LB)	(FT-L		(FT-LB)	"AS-FOUND" OPERABILITY	
28	23		10.8	OPERABLE	

TEST METHOD, DESCRIPTION AND JUSTIFICATION ******************************* Valve was tested against calculated differential pressure by vendor and requires no further testing.

¹⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

V	ALVE FU			MANUFACTURER
TURBINE E	XHAUST	VACUUM	BREAKER	VELAN
VALVE TYPE	VAL MOD	VE EL	VALVE SIZE (INCHES)	RATING
GATE	GATE W8-274B-2TS		2	600 #
ACTUATOR MANUFACTUR	RER 1	PERATOR MODEL	RPM	UNIT OUTPUT SPEED (RPM)
LIMITORQU	E SI	1B-000	1800.00	45.00
DESI DIFFERENTI	GN BASI AL PRES	SURE	DIFFE	CASE RENTIAL
OPEN		CLOSE	PRESSURE (PSID)	
N/A		27	6	00
TORQUE PRIOR TO ADJUSTMENT	TOR AFT ADJUS		DESIGN TORQUE	
(FT-LB)	(FT-	LB)	(FT-LB)	"AS-FOUND" OPERABILITY
47	2	4	10.8	OPERABLE

¹⁾ CLOSING LIMIT SWITCH IS JUMPERED OUT.

ATTACHMENT 2

Response to NRC Request for Additional Information

Response to NRC Request for Additional Information Concerning the Initial BSEP Response to IE Bulletin 85-03

NRC REQUEST:

- Revise Tables 1 and 2 of the response dated October 2, 1986
 to include the following MOVs, or justify their exclusion. As
 required by Action Item a of the Bulletin, assume inadvertent
 equipment operations:
 - (a) HPCI MOV F007 is shown normally open in Zone B-6 of Drawing D-25023, Sheet 1, Revision 28 (Unit 1), and as MOV 8 on page 68 of BWROG Report NEDC-31322 dated September 1986. How would injection to the reactor vessel be ensured if this valve were to be:

 (a) actuated inadvertently to the closed position upon intended initiation of the system, or (b) left closed inadvertently?
 - (b) RCIC MOV F012 is shown normally open in Zone B-6 of Drawing D-25029, Sheet 1, Revision 31 (Unit 1), and as MOV 8 on page 72 of the BWROG Report. The question in Item 1(a) above applies here also.
 - (c) RCIC MOV V8 is shown normally open in Zone C-2 of Drawing D-25029, Sheet 1, Revision 31 (Unit 1), and as MOV X on page 74 of the BWROG Report. How would steam supply to the RCIC Turbine be ensured if this valve were to be operated inadvertently as described in Item 1(a) above?

CP&L RESPONSE

In accordance with the agreement between the BWROG and the NRC (Reference 4), the BWROG is re-evaluating the differential pressures of the subject valves while taking into account inadvertent operation. Upon completion of that analysis, CP&L will provide the requested response in accordance with IEB 85-03, Supplement 1. This position is addressed in Attachment 1 Action (a), "Design Basis Information."

NRC REQUEST

- 2. Revise Tables I and 2 of the response dated October 2, 1986 to include the following MOVs, or justify their exclusion. According to pages 55 and 59 of the BWROG Report, these valves have no safety actions; however, utilities are expected to report differential pressures for testing, per Note o on page 66 of that report.
 - (a) HPCI MOVs F008 and F011 are shown normally closed in Zones C-5 and F-3 of Drawing D-25023, Sheet 1, Revision 28 (Unit 1), and as MOVs 5 and 6 on page 68 of the BWROG Report.
 - (b) RCIC MOV F022 is shown normally closed in Zone D-5 of Drawing D-25029, Sheet 1, Revision 31 (Unit 1), and is MOV 5 on page 72 of the BWROG Report.

CP&L RESPONSE

The requested information has been incorporated into the response accompanying this additional information. Tables 1 and 2 of the initial response (Reference 1) have not been revised since the data sheets provided in this response have incorporated the required changes. The methodology utilized to obtain the differential pressures for the valves added is provided in Attachment 1, Action (a), "Design Basis Information."

NRC REQUEST

3. Revise Tables 1 and 2 of the response dated October 2, 1986 to include values of differential pressure for opening MOVs F004 and F010, or justify exclusion of these pressures. These valves are shown normally open as HPCI MOV 3 on page 68 and as RCIC MOV 3 on page 72 of the BWROG Report. How would suction from the CST be ensured if these MOVs were to be operated inadvertently as described in Item 1(a) above?

CP&L RESPONSE

Refer to our response to Request No. 1.

NRC REQUEST

4. Revise Table 2 of the response dated October 2, 1986 to replace "N/A" with a value of differential pressure for closing RCIC Turbine Steam Supply MOV F045, or justify its exclusion. This normally closed valve is shown in Zone D-2 of Drawing D-25029, Sheet 1, Revision 31, is shown as MOV I on page 74 of the BWROG Report, and is given a safety action for closing on page 61 of that report.

CP&L RESPONSE

Refer to our response to Request No. 2.

NRC REQUEST

5. The method of handwheel turns described in Item B of the response dated October 2, 1986 is not recommended. For the reason, refer to the description of the Davis-Besse event on pages 1 and 2 of IEB 85-03. If this method is indeed planned for use, additional justification is required.

CP&L RESPONSE

The justification for the BSEP position is provided in Attachment I, Action (b), "Switch Settings."

NRC REQUEST

- 6. The proposed program for Action Items b, c, and d of the Bulletin is incomplete. Provide the following details as a minimum:
 - (a) commitment to a training program for setting switches and maintaining valve operators,
 - (b) commitment to justify continued operation of a valve determined to be inoperable,

- (c) description of a method possibly needed to extrapolate valve stem thrust determined by testing at less than maximum differential pressure,
- (d) justification of a possible alternative to testing at maximum differential pressure at the plant,
- (e) consideration of pipe break conditions as required by the bulletin,
- (f) stroke testing when necessary to meet Bulletin requirements, and
- (g) consideration of applicable industry recommendations in the preparation of procedures to ensure maintenance of correct switch settings.

CP&L RESPONSE

- (a) A description of the training provided to maintenance personnel who work with limitorque actuators is provided in Attachment I, Action (d), "Control of Switch Settings."
- (b) A commitment to justify continued operation with inoperable valves is not required. This is inherent in existing plant operations methodology. If a motor-operated valve is inoperable, system operability is dispositioned in accordance with the Technical Specifications for that system. If an LCO was generated as a result of the condition, the LCO cannot be canceled unless the condition is corrected or evaluated as acceptable by an engineering evaluation in accordance with ENP-12. The engineering evaluation is the required justification for continued operation.
- (c) This item does not apply to BSEP. Valve testing was performed at the required differential pressures, or justification provided for not testing the valve. BSEP does not intend to test valves at less than the maximum differential pressure. The statement in question was included in the initial response since test methods had not been finalized at that time.
- (d) Same as (c) above.
- (e) IE Bulletin 85-03 requires consideration of pipe break conditions in the determination of valve differential pressures, when a line break is part of the design basis for that valve. It also requires that the resulting switch settings should be verified, to the extent practical, by the same methods that would be used to verify other settings that are not tested at the maximum differential pressure.

BSEP participated in the BWROG program that addressed the subject Bulletin on a generic basis. The report prepared by the BWROG (Reference 3) took into account line breaks as required by the Bulletin when determining valve differential

pressures. As for verification of the associated switch settings, the differential pressures obtained for the subject valves were less than the existing design differential pressures of the valves. Therefore, as discussed in the initial response for BSEP (Reference 1), the settings have been previously verified to be acceptable and additional testing is not required.

(f) IE Bulletin 85-03 requires that each valve be stroke tested, to the extent practical, to verify that the settings defined in Action (b) of the bulletin have been properly implemented. This testing is required even if testing with differential pressure cannot be performed.

As detailed in Attachment 1, Action (c), "Valve Testing," the valves contained in the response were stroked in both the open and closed directions. Actuator output torque was measured during this testing, with the as-found and as-left torque values provided. No further action is required.

(g) Attachment I, Action (d), "Control of Switch Settings," provides details on the procedure developed to ensure that switch settings are properly maintained. The torque requirements referred to in the response are the minimum and maximum values for each valve. The minimum value is that required to ensure proper operation at the specified differential pressure, while the maximum is that which will not exceed the rating of the spring-pack, the actuator, the motor, or the valve itself. Criteria more restrictive than that used by the actuator manufacturer was utilized.