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February 18, 1986

Mr. Ron Maines Operator Licensing Branch Division of Human Factors Technology U.S. Nuclear Regulatory Commission Washington, D.C. 20555

Dear Ron:

I am, of course, concerned and dismayed by the letter of complaint that you received from Toledo Edison's Davis Besse regarding the theory section (SRO section 5) that was administered to their candidates on the last written examination given on November 19, 1985. I have reviewed section 5 of that examination, and I feel adamant that it was appropriate. In fact, I consider this type of a theory section to be prototypic. I would welcome the opportunity to defend any or all of the questions contained in that section.

Sincerely,

J. C. Huenefeld Power Generation Engineering Concurrence

in

Leo'J. Defferding Program Manager

FEB 2 1 1986

/c

xc: B Boger J McMillen

B603110389 B60307 PDR ADUCK 050003

1.

Davis Besse 1 November 19, 1985

> Points Available

5.0 THEORY OF NUCLEAR POWER PLANT OPERATION, FLUIDS, AND THERMODYNAMICS

OUESTION 5.01

- Define shutdown margin. Include any assumptions about a. (2.0)axial power shaping rod or control rod positioning.
- During a plant heatup in accordance with the Plant Startup b. Procedure, PP 1102.02, the reactor must be shutdown by 21% Δk/k. If Group 1 rods are withdrawn, does their worth (1.0)count as part of that $1\% \Delta k/k?$

OUESTION 5.02

While drawing a bubble in the pressurizer, the vapor space is vented to the quench tank. Describe how conditions in the quench tank can be used for determining when a steam bubble exists in the pressurizer.

(2.0)

QUESTION 5.03

During a reactor plant startup with three reactor coolant pumps running, will Quadrant Power Tilt (QPT) be more limiting at (2.0)low power or high power? Explain.

- (25.0)

Davis Besse 1 November 19, 1985

> Points Available

QUESTION 5.04

Curve "A" on the trace below is a logarithmic plot of total neutron power versus time after a reactor trip. Curve "B" is a plot of the neutron power due to delayed neutrons alone versus time for the same trip. <u>Explain</u> why total neutron power (i.e., curve A) does not drop all the way down to the delayed neutron level (i.e., to curve B). (2.0)



OUESTION 5.05

The reactor is critical at 10⁻⁸ amps. A stable 1 DPM startup rate is achieved. If rods are inserted continuously until startup rate drops to zero, and then the rod insertion is immediately stopped, will the reactor be critical, supercritical, or sub-critical? Explain.

(2.0)

Davis Besse 1 November 19, 1985

> Points Available

OUESTION 5.06

The figure below shows neutron population response to reactivity insertion. Label each of the three (3) curves as supercritical, exactly critical, or subcritical. (Assume below the point of feed-back effects.) (1.0)



-Section 5 Continued on Next Page-

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Davis Besse 1 November 19, 1985

Points Available

QUESTION 5.07

<u>Given</u> a large vented tank 30 ft. in diameter and 60 ft. high with a centrifugal pump taking a suction from its base. The pump is located at a vertical elevation corresponding to the bottom of the tank. The tank is entirely full of water and is maintained at 60°F by heaters. <u>Assume</u> the vent becomes totally clogged while the pump is in operation. Atmospheric pressure is 14.7 psia. <u>Answer</u> the following questions:

a.	What is	the	maximum differen			1	pressure 1		that	could or	ccur			
	between	the	inside	and	outside	of	the	tank	? E	xplain.		(1.5)		

 Explain why the pump may begin to cavitate at a higher tank level than with the vent open. (1.0)

QUESTION 5.08

When conducting a rapid plant shutdown at 25 MW per minute (Abnormal Procedure AB 1203.07), why is the operator required to add boric acid to the makeup tank as unit load decreases? (2.0)

QUESTION 5.09

Assume that the condenser is not available and the operator is manually controlling steam generator pressure at 995 psig using the atmospheric vent valves. Estimate how many gallons of water would be required to cooldown the RCS from 582°F to 546°F. Show assumptions. (2.0)

- a. 350 gallons
- b. 3500 gallons
- c. 35,000 gallons
- d. 73,000 gallons

Davis Besse 1 November 19, 1985

> Points Available

QUESTION 5.10

Consider the system shown below (an 80 ft high loop of 3 ft diameter steel pipe and a pressurizer). Initially the pressurizer is saturated at 640 F and the loop is subcooled at 546 F. Assume that the entire system, including the pressurizer is allowed cooldown. The thermal contraction of the entire system due to this cooldown is 600 ft. Will the pressurizer be empty? Explain. (1.5)



Davis Besse 1 November 19, 1985

> Points Available

QUESTION 5.11

The reactor is at 100% FP equilibrium xenon conditions when a reactor trip occurs. Three (3) hours later the reactor is restarted.

a. When at 10^{-8} amps, which direction will rods have to go to hold power constant? Explain. (1.0)

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 <u>Sketch</u> the xenon concentration through to equilibrium assuming the reactor is raised to 92% power within 1 hour (4 hours after the trip). (1.5)

QUESTION 5.12

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When borating from a lower to a higher boron concentration, why will the final boron concentration value always be 3 to 4% lower than anticipated?

(1.0)

QUESTION 5.13

Why are SFRCS tripped and AFW actuated immediately following a loss of NNI X DC power, rather than waiting for the plant transient to initiate an SFRCS actuation? (1.5)

-End Section 5-

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Jun 1/19/15

POWER PLANT EXAMINATION RESULTS SUMMARY

FACILITY	Davis Bessel
DATE OF WRIT	TEN November 19, 1985
DATE OF ORAL	s November 20-21, 1985
DATE OF SIMU	LATOR
EXAMINERS	J.C. Huenefeld / B.F. Gore
TYPE OF EXAM	A (COLDI(HOT))

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	10101				
Overall Results	No.	No.	%	No.	%
Senior Operator	8	4	50	4	50
Reactor Operator	1	0	0	1	100

Total Passed

Failed

- 1. Reactor Operator
- Reactor Operator
 Senior Reactor Operator Instant
 Senior Reactor Operator Upgrade
 Reactor Operator Retake

- 5. Senior Reactor Operator Retake
- 6. Instructor Certification
- 7. Senior Reactor Operator Fuel Handling

TYPE OF EXAM ICOLD	(HOTI)												Exa	ninati esults	on	Ex	amini Initial	BT'S S
												TOTAL		RO			SRO	
NAME	DOCKET NO.	TYPE	1	2	3	4	TOTAL	5	6	-	•	TUTAL	W PA	Ê	$\frac{s}{\nabla}$	w	0	-
Michael G. Parker	55-30880	1	79.1	77.2	92.6	75.2	81.07				_		au	1	4	4	4	K
										-	2, 0	969	M	1	1	2	9/	ť
Dan L. Hughes	55-30952	2			-	-		80.4	47.6	88.0	16.0	\$2.0	17	7	7	10/	10/	ľ
Anthony R. Stallard	55-30451	2		-	-	-		56.8	97.2	88.0	82.2	88.59	6	6	6	17	1	ť
		-	-	+	+-	+	-	717	940	67.2	81.6	68.8)	Z	V	1	E	1/20	
Calvin E. Hoffer	55-5648	3		+	+-	+	-	100 6	aci	84 4	1924	1977		V	V	VZ	1/su	l
Lawrence G. Keller	55-30630	3		+	-	+	-	62.5	15.0	101.0	0	6.0	17	17	1	E	12	1
Steven L. Laeng	55-30224	3			-		-	58.3	92.9	84.0	78.4	108.0	K	t	t	XE)	TP/	Ť
Arthur J. Lewis	55-7854	3			-	-	-	62.2	96.8	79.0	70.0	(7.3)	K	Ł	Ł	K	1	1
Anthony R. Statland	55-3045	5	-	-	+	-	-	93.5	102	7/2/4	212	83.4	K	t	t	P	P	1
Dan T. Staudt	55-3022	5 3	-	+	-	+	-	The second	13.0	- 16.	0 830	82.9	15	t	t	E	12	1
Kim A Stiger	55-3022	6 3					-	63.7	17/1	100.	100.0	1		-	-			

EXAMINATION RESULTS

EXAMINER'S INITIALS

Only initials of examiner who actually administered the examination

- F = Failed
- W = Waived