NRC FORM 366 U.S. NUCLEAR REGULATORY COMMISSION (4-95) LICENSEE EVENT REPORT (LER)	APPROVED OMD NO. EXFIRES: 0.4. ESTIMATED BURDEN PER RESPONSE INFORMATION COLLECTION REQUEST COMMENTS REGARDING BURDEN ESTI INFORMATION AND RECORDS MANAGE 7/14), U.S. NUCLEAR REGULATORY MASHINGTON, DC 20555-0001, AND REDUCTION PROJECT (3150-0304), AND BUDGET, WASHINGTCH, DC 205	(30/98) TO COMPLY WITH THIS : 50.0 HRS. FORWARD MATE TO THE MENT BRANCH (MNBB COMMISSION, TO THE FAPERWORK OFFICE OF MANAGEMENT
FACILITY NAME (1)	DOCKET NUMBER (2)	PAGE (3)
Catawba Nuclear Station Unit 2	05000414	1 of 12
TITLE (4)		
Error During Tagout Causes De-Energization of Vita.	l Bus and Actuat	ion of Low
Temperature Overpressure Protection		
EVENT DATE (5) LER NUMBER (6) REPORT DATE (7) MONTH DAT YEAR YEAR SEQUENTIAL SEQUENTIAL MONTH DAY YEAR FACT	OTHER FACILITIES IN	DOCKET NUMBER (S)
NUMBER NUMBER		DOCKET HUNDER (2)
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OPERATING THIS REPORT IS SUBMITTED PURSUANT TO THE REQUIREMENTS OF 10 CFR		
MODE (9) 5 20,402(b) 20,405(c)	X 50.73(a)(2)(1v)	73.71(b)
POWER 20.405(a)(1)(1) 50.36(c)(1)	50.73(a)(2)(v)	73.71(c)
LEVEL (10) 000 20.405 (a) (1) (11) 50.36 (c) (2)	50.73(a)(2)(vii)	X OTHER (Specify in
20.405(a) (1) (iii) 50.73(a) (2) (i) 20.405(a) (1) (iv) 50.73(a) (2) (ii)	50.73(a)(2)(viii)(A) 50.73(a)(2)(viii)(B)	Abstract below and
20.405 (a) (1) (v) 50.73 (a) (2) (11)	50.73(a) (2) (V111) (B)	in Text, NRC Form 366A) Special
LICENSEE CONTACT FOR THIS LER (12	2)	Report
NAME	TELEPH	ONE NUMBER
	AREA CODE (803)	
M. H. Chernoff, Regulatory Compliance Specialist		831-3414
COMPLETE ONE LINE FOR EACH COMPONENT FAILURE DESCRIBE	ED IN THIS REPORT (13)
CAUGE SYSTEM COMPONENT MANUFACTURER REPORTABL CAUSE SYSTEM	COMPONENT MANUFACTURER	REPORTABLE
TO EPIX		TO EPIX
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SUPPLEMENTAL REPORT EXPECTED (14)	EXPECTED	MONTH DAY YEAR
YES (if yes, complete EXPECTED SUBMISSION DATE) X NO	SUBMISSION DATE (15)	
ABSTRACT (Limit to 1400 spaces, i.e. approximately fifteen sing On September 6, 1998, at 1405 hours, during tagon the wrong potential transformer was isolated, sat undervoltage on 4160 VAC Essential Bus 2ETB. The relays performed a load shed on Bus 2ETB and oper The "B" Diesel Generator had been removed from se All engineered safety features equipment responde Centrifugal Charging Pump (CCP) Discharge Valve w position, maximizing charging and seal injection swapped to the Refueling Water Storage Tank. Pre cooldown rate limits were exceeded, and an evalua integrity of the pressurizer was done which confi operability. One Pressurizer Power Operated Reli Temperature Overpressure Protection mode to maint pressure. This Report also satisfies the Technic requirement for a Special Report for this occurre At 1435 hours, power was restored to Bus 2ETB. The attributed to inadequate work practices, in that verification was not performed to determine the operated to the performed to determine the operated to be approximate.	at of Diesel Gen disfying the log e Black Out Load hed the feeder b ervice and did n ed properly. Th went to the full flow. Suction essurizer heatup ation of the str irmed its contin hef Valve cycled cain Reactor Coo cal Specificatio ence. The event has be the appropriate correct componen	erator "B", ic for Sequencer reaker. ot start. e open of the CCPs and uctural ued in Low lant System ns
tagged when labeling discrepancies were encounter expectations regarding actions to be taken in the iterated to appropriate personnel. NRC FORM 366	-	e been re-
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		ESTIMATED BURDEN PER RESPONSE TO COMPLY WITH THIS INFORMATION COLLECTION REQUEST 50.0 HRS. FORWARD COMMENTS REGARDING BURDEN ESTIMATE TO THE INFORMATION AND RECORDS MANAGEMENT BRANCH (MNBB 7714), U.S. NUCLEAR REGULATORY COMMISSION, WASHINGTON, DC 20555-0001, AND TO THE PAPERWORK REDUCTION PROJECT (3150-0104), OFFICE OF MANAGEMENT AND BUDGET, WASHINGTON, DC 20503					
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Background

This report describes an event in which an error was made during tagout of a Diesel Generator [EIIS:DG], which ultimately caused de-energization of the "B" train Class 1E 4160 VAC Essential Auxiliary Power Bus [EIIS:BUS]. This event is reportable pursuant to 10 CFR 50.73 (a)(2)(iv) as an actuation of Engineered Safety Features equipment. During the ensuing transient, a Power Operated Relief Valve [EIIS:PCV] operated to maintain Reactor Coolant System [EIIS:AB] pressure at its Low Temperature Overpressure Protection setpoint. Technical Specification 3.4.9.3 requires submittal of a Special Report for this occurrence. This Licensee Event Report also serves as that Special Report.

The 4160 VAC Essential Auxiliary Power System [EIIS:EB] supplies power to those Class 1E loads required to safely shut down the unit following a design basis accident. The system is divided into two completely redundant and independent trains designated A and B, each consisting of one 4160 volt switchgear assembly [EIIS:SWGR], three 6900/4160 volt transformers [EIIS :XFMR], two 600 volt load centers [EIIS:MCC], and associated loads.

Normally, each Class 1E 4160 volt switchgear is powered from its associated non-Class 1E train of the 6900VAC Normal Auxiliary Power System [EIIS:EB]. Each train has an alternate source of power from the 6900 volt system via two separate and independent 6900/4160 volt transformers. These transformers are shared between units.

Each train of the 4160 VAC Essential Auxiliary Power System is also provided with a separate and independent diesel generator to supply the Class 1E loads required to safely shut down the unit following a design basis accident. Each diesel generator is also capable of supplying its associated 4160 volt blackout switchgear through a connection with the 4160 volt essential switchgear.

Each of the redundant 4160 volt essential buses is provided with two levels of undervoltage protection to monitor bus voltage. Each level is provided with a separate set of three undervoltage relays [EIIS:RLY] which are utilized in a two-out-of-three logic scheme. The first level of undervoltage relays detect a loss of voltage on the 4160VAC essential bus and has a ten cycle time delay. The second level provides degraded voltage protection and actuates in the existence of a prolonged degraded voltage condition.

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		INFORMATION REGARDING B MANAGEMENT COMMISSION, REDUCTION P	JRDEN PER RESPOI COLLECTION REQU URDEN ESTIMATE T BRANCH (MNBB 77 WASHINGTON, DC 20 ROJECT (3150-0104) HINGTON, DC 20503	UEST 50.0 HRS. FOI TO THE INFORMATIC 14), U.S. NUCLEAR 20555-0001, AND TO), OFFICE OF MANA	RWARD COMMENTS ON AND RECORDS REGULATORY) THE PAPERWORK		
NRC FORM 366A U.S. NUCLEAR REGULATORY COMMISSION(6- 89)		6- APPROVED OMB NO. 3150-0104 EXPIRES:5/31/95					

If the undervoltage relays are actuated, the diesel generator starts, and if the undervoltage condition does not clear in 8.5 seconds, the Class 1E switchgear incoming breaker [EIIS:BKR] is tripped and the bus is load shed. At 1J seconds, the diesel generator breaker [EIIS:BKR] closes, thus aligning the diesel generator to the essential bus, and the necessary automatic load sequencing begins. The loads sequenced onto the bus are dependent on whether a blackout and/or Loss of Coolant Accident (as evidenced by a Safety Injection Actuation Signal) exists.

The "Diesel Generator 2B PT Fuse Drawer" is located in the Diesel Generator 2B Control Panel. The "2ETB Bus PT" and "Diesel Gen 2B Source PT" drawers are located in the Turbine Building in cubicle 2ETB 19.

Technical Specification 3.4.9.3, Overpressure Protection Systems, applicable for Mode 5 operations, provides requirements for operability of the Overpressure Protection Systems. Action d of this Technical Specification requires in the event the Power Operated Relief Valves (PORVs) or the Reactor Coolant System vent(s) [EIIS:RV] are used to mitigate a Reactor Coolant System pressure transient, a Special Report shall be prepared and submitted to the Commission pursuant to Specification 6.9.2 within 30 days. The report shall describe the circumstances initiating the transient, the effect of the PORVs or Reactor Coolant System vent(s) on the transient, and any corrective action necessary to prevent recurrence.

Technical Specification 3.4.9.2, Pressurizer [EIIS:PZR], specifies that the pressurizer temperature shall be limited to a maximum heatup of 100 degrees Fahrenheit in any one-hour period, and a maximum cooldown of 200 degrees Fahrenheit in any one-hour period. The associated Action states that with the pressurizer temperature limits in excess of any of these limits, restore the temperature to within the limits within 30 minutes, perform an engineering evaluation to determine the effects of the out-of-limit condition on the structural integrity of the pressurizer, and determine that the pressurizer remains acceptable for continued operation or be in at least Hot Standby within the next 6 hours and reduce the pressurizer pressure to less than 500 psig within the following 30 hours.

Event Description

September 6, 1998

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	an na anns an san ann an an an ann an ann an		Handland Andrew Constant and the second constants	National Advances of the State of States and States		
was approximately 180 degree Reactor Coolant Pumps A and preparations were in progres Emergency Diesel Generator 2 planned to remove it from se Senior Reactor Operator and performing the Removal and R 1221 hours	B [EIIS:P] we s to perform B had been ru rvice. A pre two non-licen	re in a a crud n for : -job b: sed op:	operation, burst. 24 hours a rief was h	and and it wheld bet	was tween the	
Emergency Diesel Generator 2	B was removed	from a	service.			
1358 hours						
Diesel Generator Output Brea	ker 2ETB-18 w	as racl	ked out ar	nd tagge	ed.	
The next step directed on th tag "Diesel Generator 2B PT position. Following that st 2ETB 19 were to be removed a proceeded to cubicle 2ETB 19 operators, it was erroneousl Bus PT" was the same drawer	Fuse Drawer" ep, the "D/G nd tagged. T . After some y concluded t	[EIIS: 2B Southe non- discut hat the	FU] in th rce PT Fus -licensed ssion betw e drawer 1	ne open ses" in operato ween the abeled	Cubicle ors 2 "2ETB	

1405 hours

The 2ETB Bus PT fuse drawer was opened. This caused the circuitry to sense an undervoltage condition on 2ETB. The 2ETB undervoltage relays actuated and 8.5 seconds later the feeder breaker was tripped, isolating the bus from off-site power sources. The Train B blackout sequencer was actuated which shed the loads on 2ETB.

The blackout sequencer sent a start signal to Diesel Generator 2B, but the Diesel Generator had been removed from service and did not start. The sequencer also sent a start signal to the "B" train Blackout Class 1E loads. The "B" train Pressurizing Filter Train Fan of the Control Room Area Ventilation System was in standby and aligned to receive power from Catawba Unit 1 prior to the event. It automatically started. The steam supply valves to the Turbine Driven Auxiliary Feedwater Pump

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	an a substant and the state about a state of the state of t		e Millel Cherning in order at the constrained states between	C. Martine Construction of Construction		
[EIIS:P] opened, but the Pump The remainder of the Class 1E energized.	did not sta loads did n	rt beca ot star	use there t because	was no 2ETB w	steam. as not	
Valve 2NV-294, Centrifugal Cha [EIIS:FCV], went to the full of causing maximum charging flow.	open positio	Dischar n upon	ge Flow C loss of "	ontrol B" trai	Valve n power,	
Operators entered AP/2/A/5500, to loss of power to ETB.	/07, Loss of	Power	To An Ess	ential	Bus, due	
1409 hours						
Centrifugal Charging Pump suct Water Storage Tank [EIIS:TK] ([EIIS:TK] Outlet valves closed	opened, and					
1411 hours						
Operators increased pressurize System pressure increase.	er spray flo	w to re	duce the	Reactor	Coolant	
1414 hours						
Due to increased charging flow increased, and Power Operated to control Reactor Coolant Sys 2NC-32B was set at its Low Ter of 400 psig.	Relief Valv stem pressur	e 2NC-3 e. Pow	2B lifted er Operat	numero ed Reli	us times ef Valve	
1425 hours						
Throttling of charging line fl procedure AP/2/A/5500/07.	low was perf	ormed i	n accorda	nce wit	h	
1435 hours						
Voltage was restored to 2ETB. time.	The Pressu	rizer P	ORV lifte	d for t	he last	
1447 hours						
Volume Control Tank Outlet Val	lves were re	opened				

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1501 nours

Centrifugal Charging Pump Discharge Flow Control Valve was returned to its throttled position. Plant conditions were stabilized.

Conclusion

This event occurred as a result of an inappropriate action by non-licensed operators who inadvertently de-energized 2ETB 4160 volt essential bus by isolating the 2ETB bus side potential transformer rather than the 2B Diesel Generator side potential transformer when tagging out the 2B Diesel Generator. The Diesel Generator had been previously removed from service, and the Diesel Generator Output Breaker had been racked out. The next action in the Removal and Restoration Tagout Sheet and the applicable procedure specified opening the Diesel Generator 2B PT Fuse Drawer. Following this action, the fuses were to be removed in 2ETB 19, the D/G 2B Source PT Fuses. One of the non-licensed operators noted that the 2ETB 19 cubicle was referenced in the Tagout Sheet and procedure and recalled that there were two potential transformer fuse drawers located in the 2ETB 19 cubicle. However, the fuse drawers were labeled 2ETB Bus PT and Diesel Gen 2B Source PT. The two non-licensed operators discussed the fact that the label 2ETB Bus PT was not identical to the nomenclature on the Tagout Sheet and procedure. Concluding that this was a poor labeling issue, and believing that the 2ETB 19 cubicle was the correct location for both PT's, the operator opened the 2ETB Bus PT fuse drawer, actuating the loss of voltage and degraded bus sensing circuit. This action, a rule based error involving misjudgment, was not consistent with expected work practices at Catawba. When there is uncertainty regarding the correct component, personnel are expected to verify information from an independent source prior to taking action. Therefore, the root cause of this event is inadequate work practices due to lack of information verification.

During review of this event, two contributing factors were identified. During this event, the process of independent verification was not executed as intended. When safety-related components are removed from service, independent verification is required. It is intended that one operator perform the component manipulations and a second operator independently verify the action is correct. During this event, the two operators discussed the difference in nomenclature and together determined that the drawer was the correct one, rather than independently reaching a conclusion.

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Additionally, the Removal and Restoration Tagout Sheet package contained incomplete and misleading information, even though the tagout was a computerized, pre-planned tagout. The Sheet did not specify the correct location of the DG2B Fuse Drawer. The tag stub, which was attached to the tag to be placed, indicated that the component was in the rear of the Diesel Generator Control Panel, but stated that this was located in the Turbine Building, rather than the Diesel Generator Room. There were additional discrepancies in the supporting documentation in the package. While these discrepancies did not contribute directly to this event, the existence of other discrepancies may have contributed to acceptance of the component nomenclature discrepancy.

An engineering review of plant response to this event was conducted. The review concluded that all equipment responded as designed to the transient. The major plant effects included valve 2Nv. .94, Centrifugal Charging Pump Discharge Flow Control Valve, failing open upon loss of power to the "B" train. The valve went as designed to the full open position to ensure an abundance of charging upon loss of air or power. Approximately 4 minutes later, low level in the Volume Control Tank was reached, and suction of the Centrifugal Charging Pump automatically swapped to the Refueling Water Storage Tank. The increased charging header pressure, coupled with increasing backpressure due to the Volume Control Tank being isolated caused an overall decrease in differential pressure across the Reactor Coolant Pumps Number One Seal. The increase in charging also caused a cooldown in the pressurizer, along with an increase in level. Pressurizer PORV NC32B cycled numerous times at its setpoint of 400 psig to control Reactor Coolant System pressure.

Indication of charging flow and seal injection flow was lost during this event. Based on a flow balance using best available data, it was determined that flow exceeded the manufacturer's recommended flow through the Regenerative Heat Exchanger [EIIS:HX]. The effects of this transient on the Regenerative Heat Exchanger have been evaluated and found acceptable.

When power was lost to 2ETB, valve 2NV-294 went to the full open position and 2NV-309, Seal Water Injection Flow valve, also went to the full open position, causing increased seal injection flow. Indication of total seal injection flow was lost and the instruments indicating seal injection flow to individual pumps were pegged high. Based on a review of the data, it was concluded that a positive flow from the pump seal cavity into the Reactor Coolant System was maintained.

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When suction of the Centrifugal Charging Pumps swapped to the Refueling Water Storage Tank, the Volume Control Tank outlet isolation valve closed. Volume Control Tank pressure began increasing, creating a higher backpressure to the Reactor Coolant Pumps Number One seal, and causing a decrease in seal leakoff flow. Since the occurrence of a seal face plate rub cannot be conclusively ruled out, a seal inspection on the 2A Reactor Coolant Pump was planned. However, the seal was damaged during removal and has been replaced. Replacement of the seal on the other Reactor Coolant Pump operating during this event, the 2B Reactor Coolant Pump, was already planned for this outage and has been completed. The seal was inspected and there was evidence of rubbing, although the indications found on the seal cannot be positively attributed to this event. The other two Reactor Coolant Pumps were not in operation and were not affected by this event.

The insurge of cooler water caused by the increase in charging caused a temperature decrease in the Pressurizer. Prior to this transient, the pressurizer water temperature was approximately 416 degrees Fahrenheit and the surge line temperature was approximately 418 degrees Fahrenheit. Ten minutes after the loss of power, indicated temperature of the water reached a minimum of 234 degrees Fahrenheit and the surge line reached a minimum of 188 degrees Fahrenheit. Within a few minutes, indicated temperatures had increased to 399 degrees for Pressurizer Water temperature and 392 degrees for surge line temperature. The temperature changes in the pressurizer were caused by the movement of the relatively stagnant mass of water in the pressurizer. As this mass of water was displaced upward by the insurge due to increased charging flow, the temperature decreased at the location monitored by the Resistance Temperature Detectors. When spray was initiated, the mass of water was displaced downward, causing an increase in temperature at the location monitored by the Detectors. During this event, the station was in noncompliance with the cooldown and heatup limits of Technical Specification 3.4.9.2. In accordance with the Action of Technical Specification 3.4.9.2, an engineering evaluation was performed to determine the effects of the out-of-limit condition on the structural integrity of the pressurizer. This evaluation concluded that this transient did not adversely affect the structural integrity of the pressurizer and that the pressurizer continued to be operable.

The increase in charging caused the pressurizer to go water solid. Approximately 8 minutes after the interruption of power, Pressurizer PORV 2NC32B began cycling at its low temperature overpressure setpoint of 400 psig. The valve cycled numerous times over a 22 minute period, relieving to the Pressurizer Relief Tank [EIIS:TK]. The maximum pressure reached in the Pressurizer Relief Tank was 95 psig. The high pressure setpoint for

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System pressure during the trans Wide Range Reactor Coolant System adverse effects on the valve inc inability of the valve to meet s event, the valve remained closed seat leakage. Stroke time testi for all three PORVs was already Corrective actions to prevent re actuation of the valve in Low Tem provided in the Corrective Actio Operated Relief Valve which was	m Hot Leg Pro lude the pote troke time re for several ng and limit planned to be currence of mperature Ove	essure ential equirem days w switch e perfo the cir erpress	Transmitt for seat ents. Fo ithout ar indicati rmed duri cumstance ure Prote	er. Po leakage blowing by indic on veri on veri on this es requi	tential and this ation o ficatio outage

There are no EPIX reportable equipment failures associated with this event.

Corrective Actions

Immediate

 Power was restored to 2ETB in accordance with plant procedure AP/2/A/5500/07, Loss of Power To An Essential Bus, and plant systems were stabilized.

Subsequent

- 1. The individuals involved were counseled regarding this error.
- Before resuming the 2B D/G tagout, the Senior Reactor Operator on shift reviewed the tagout with the Non-Licensed Operators and determined the critical portion of it. Based on that determination, he and the Non-Licensed Operators performed a walk through of the tagout before

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actually performing it. During the Senior Reactor Operator.	the tagout,	, there	was dired	ct over	sight by
 Operations management conducte personnel to discuss this even reduce human performance error performance. 	t and to re:	inforce	the prope	er ways	to
4. A "Human Performance" time-out this event and stress how prop techniques could have prevente	er use of hu	uman per	on person formance	nnel to improv	discuss ement
5. The Removal and Restoration ta correct location of the potent	gout databa: ial transfo:	se was r rmer.	evised to	o refle	ct the
 A tag was placed on Units 1 an cabinets warning personnel tha or ETB. 	d 2 ETA and t opening th	ETB Pot he drawe	ential Tr r will de	ransfor e-energ	mer ize ETA
 A process was established to r identify "critical" tagouts th oversight. This type of tagou restoration, and any tagout in transformers. This process wi outage. 	at need dire t includes I volving man:	ect Seni Diesel G ipulatio	or Reacto enerator n of pote	or Oper tagout ential	ator s and
8. A team was established to asse occurrence, or common practice identified. This review concl communication was distributed management's expectations for	when a comp uded that th to station p	ponent l his was personne	abeling r an isolat l which r	nismatc. ted cas	e. A
9. Management expectations for ma distributed to station personn Station personnel were instruc troubleshoot when performing a verification, but rather to br perform the second check if th independence of the verifier.	el via Stat: ted to be ca n activity : ing the supe	ion Divi areful n involvin ervisor	sion Tear ot to col g indeper into the	n Notes llabora ndent activi	te or ty to

10. The seal on the 2A Reactor Coolant Pump was removed for inspection. The seal was damaged during removal and has been replaced. The seal on the 2B Reactor Coolant Pump has been replaced. The removed seal was

 Catawba Nuclear Station Unit 2 Catawba Nuclear Station Unit 2 O5000414 inspected. Indications of rubbing were ide However, these indications cannot be posit: event. As previously scheduled for this Refueling implemented to provide backup power to Cent Discharge Flow Control Valve 2NV-294 and Se 309, and other similar valves on Unit 2. To implemented on Unit 1 during its End of Cyc 	ively attributed to this
<pre>inspected. Indications of rubbing were ide However, these indications cannot be posit: event. 11.As previously scheduled for this Refueling implemented to provide backup power to Cent Discharge Flow Control Valve 2NV-294 and Se 309, and other similar valves on Unit 2. 10</pre>	1998 004 00 11 of : Mentified on the seal. Lively attributed to this
<pre>inspected. Indications of rubbing were ide However, these indications cannot be posit: event. 11.As previously scheduled for this Refueling implemented to provide backup power to Cent Discharge Flow Control Valve 2NV-294 and Se 309, and other similar valves on Unit 2. 10</pre>	lentified on the seal. lively attributed to this
 12.The effects of this transient on the Regen been evaluated and found to be acceptable. 13.In accordance with the Action of Technical engineering evaluation was performed to det out-of-limit condition on the structural in The evaluation concluded that this transier the structural integrity of the pressurizer continued to be operable. Planned 	trifugal Charging Pumps Geal Injection Flow Valve 2NV- This modification was vole 10 Refueling Outage. Merative Heat Exchanger have I Specification 3.4.9.2, an etermine the effects of the integrity of the pressurizer. ent did not adversely affect

2. As a long term project, the Equipment Database nomenclature used by the computerized pre-planned tagouts is being validated and revised for consistency with plant labels and drawings.

transformers will be evaluated for needed enhancements.

3. Stroke time testing and limit switch indication verification for all three PORVs will be conducted. This activity was already planned to be performed during this outage.

Safety Analysis

All equipment responded as designed to the initiating event. "A" Train equipment was not affected by this event and continued to function normally. Normal residual heat removal utilizing the train "A" Residual Heat Removal Pump was in service prior to de-energization of 2ETB. Normal residual heat removal was not interrupted by this event, and no setpoints or limits associated with this function were exceeded. The "B" crain essential loads had already been removed from service in preparation for the Emergency Diesel Generator outage. The Pressurizer PORV successfully

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LICENSEE EVENT REPORT (LER) TEXT CONTINUATION		ESTIMATED BURDEN PER RESPONSE TO COMPLY WI INFORMATION COLLECTION REQUEST: 50.0 HRS. FOR REGARDING BURDEN ESTIMATE TO THE INFORMATIC MANAGEMENT BRANCH (MNBB 7714), U.S. NUCLEAR COMMISSION, WASHINGTON, DC 20555-0001, AND TO REDUCTION PROJECT (3150-0104), OFFICE OF MANA BUDGET, WASHINGTON, DC 20503			RWARD COMMENTS ON AND RECORDS REGULATORY THE PAPERWORK	
FACILITY NAME (1)	DOCKET NUMBER (LER NUMBER (6)			PAGE (3)	
		YEAR	SEQUENTIAL NUMBER	REVISION NUMBER		
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terminated the pressurization of the Reactor Coolant System due to this mass injection event and the allowable combinations of peak pressure and minimum temperature remained below and to the right of the limit lines shown in Table 3.4-3, Reactor Coolant System Cooldown Limitations.

At no time during this event was the health or safety of onsite personnel or the public jeopardized.