Docket Nos. 50-325 and 50-324 DISTRIBUTION: See next page

LICENSEE:

Carolina Power & Light Company (C'bl)

FACILITY:

Brunswick Steam Electric Plant, Units 1 and 2

SUBJECT:

SUMMARY OF MEETING HELD ON JULY 14, 1988 - HPCI/RCIC

VALVE OPERABILITY AND SAFETY SYSTEM RELIABILITY (TAC

NO. 68674)

Background

A meeting was held in Rockville, Maryland on Thursday, July 14, 1988, to discuss the specifics of CP&L's recently submitted Justification for Continued Operation (JCO) with respect to Brunswick Steam Electric Plant, Units 1 and 2. The meeting also was to address safety system reliability in light of a recent trend involving an increased number of reportable even 3. Participants in the meeting included representatives of the NRC and CP&L. The list of attendees is provided as Enclosure 1.

The specific events which focused attention on Brunswick's HPCI system were:

- A turbine steam supply valve (FOO1) failed to open and the HPCI system was declared inoperable on June 30, putting Unit 1 in a 14 day LCO.
- On July 5, upon determining that an undersized motor operator was used in the design for valve FOO6 (MOV injection valve). Unit 2 entered a 14 day LCO.

The licensee developed a JCO to support operation until the next refueling outages without making any physical changes to the injection valves. Subsequently. CP&L decided to shut down Unit 1 to replace the deficient motor operator on injection valve FOO6. Then, after Unit 1 was restarted and reached 60%. Unit 2 would be shut down for similar repair work. The NRC had concerns about the JCO and safety system reliability, which the meeting was organized to address. The agenda communicated to the licensee in a teleconference is shown in Enclosure 2.

Summary

In response to the questions reflected in the agenda, the licensee made a slide presentation addressing NRC concerns on technical issues, and discussing failure modes, corrective actions and the bases for projected future performance. The slides presented and clarifying information are provided in Enclosure 3.

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At the close of the meeting, CP&L summarized the following action items:

- ° Complete short term repairs.
 - 1. Remove starting resistors on FO13 valves.
 - Investigate whether removal of starting resistors from other similar valves is appropriate.
 - 3. Reverify findings of INPO SOER 84-7.
 - 4. Evaluate temperature effects (motor heater and shunt field.
- Long term program to be developed o include the complete analysis of safety related valves with respect to design basis requirements.

Schedule

08/15/88 - Prepare a plan and schedule that will establish milestones and completion dates for the analysis phase.

12/31/88 - Complete the design analysis of safety related valves.

02/28/89 - Complete development of a corrective action implementation plan to address problems identified.

Along with these CP&L proposals, the NRC requested intermediate briefings on the progress relative to the above-mentioned actions.

The licensee was instructed to prepare a confirmation of corrective actions letter specifically addressing the very near term actions to support restart. Also, a commitment was made by CP&L to obtain NRC approval prior to restarting Unit 1 after the valve repair outage.

A followup letter is expected in a couple of weeks after this meeting focusing on near term and long term actions. It is expected that the licensee's program will be somewhat evolutionary.

15/

Brenda Mozafari, Project Engineer Project Directorate II-1 Division of Reactor Projects I/II

Enclosuret: As stated

cc w/encls: See next page

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							 THE RESERVE THE PERSON NAMED IN

DISTRIBUTION FOR MEETING SUMMARY DATED: September 12, 1988

facility: Brunswick Steam Electric Plant, Units 1 and 2

Docket File

NRC PDR

Local PDR

PDII-1 Reading

E. Adensam

P. Anderson

B. Mozafari

B. Buckley

OGC

E. Jordan (MNBB 3302)

B. Grimes (9A2)

ACRS (10)

B. Troskoski (17D19)

cc: Licensee/Applicant Service List

ARC Participants

B. Buckley

N. Grace, RII

L. Reyes, RII

J. Sniezek (12618)

G. Lainas

T. Marguires (12020)

F. Rosa (8D20)

E. Brown (EWS 207)
O. Rothberg (NS 217A)
T. Martin (12G18)

S. Long (10A2)

R. Barrett (10A2)

K. Eccleston (14H3)

W. Ruland, RII

B. Troskoski RII

E. Adensam

B. Mozafari

J. Huang (9H3)

F. Miraglia (12G18) A. Thadani (7E4) D. Tondi (8D20)

P. Kang (8D20)

T. Collins (8E23)

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cc:

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Executive Director
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JULY 14, 1986

	Name	Organization
В.	Buckley	NRC
N.	Grace	NRC
L.	Reyes	NRC
J.	Sniezek	NRC
G.	Lainas	NRC
E.	Utley	CP&L
P.	Howe	CP&L
C.	Dietz	CP8L
R.	He lme	CP&L
J.	O'Sullivan	CP&L
T.	Marguiles	NRC
J.	Boone	CP&L
R.	Richey	CP&L
F.	Rosa	NRC
ε.	Brown	NRC
C.	Rothberg	NRC
Τ.	Martin	NRC
S.	Long	NRC
	Barrett	NRC
Κ.	Eccleston	NRC
	Ruland	NRC SRI
	Troskoski	NRC
Ε.	Adensam	NRC
8.	Mozafari	NRC
J.	Huang	NRC
F.	Miraglia	NRC
Α.	Thadani	NRC
D.	Tondi	NRC
P.		NRC
T.	Collins	NRC

AGENDA

JULY 14, 1988

1. Specifics on JCO

- A. Define problems with each valve.
- B. Identify changes proposed or implemented to resolve the defined problems.
- C. Basis for determining that the problems will be solved by the changes and not introduce new problems.
- D. Describe the testing proposed to demonstrate that the changes have resolved the identified problem.
- E. Previous operating history for each valve.
- F. Testing experience with MOVATS-type program for these valves.
- G. Discuss differences between units on torque requirements for sister valves.
- II. Address Safety System Reliability at Brunswick.

JULY 14, 1988

O OBJECTIVES

- O TO REVIEW SPECIFIC TECHNICAL ISSUES THAT IMPACT THE BASES OF BNP'S JUSTIFICATION FOR CONTINUED OPERATION FOR THE UNIT 1 AND UNIT 2 HIGH PRESSURE COOLANT INJECTION SYSTEMS, JULY 10, 1988.
- TO REVIEW BNP SAFETY SYSTEM RELIABILITY, SPECIFICALLY FOCUSED TO THE HIGH PRESSURE COOLANT INJECTION SYSTEMS. PRESENTATION IS STRUCTURED TO DISCUSS FAILURE MODES, CORRECTIVE ACTIONS, AND THE BASES FOR PROJECTED FUTURE PERFORMANCE.

JULY 14, 1988

0	SAFETY SYSTEM RELIABILITY	R. E. HELME
	o HISTORICAL PERFORMANCE	
	o FAILURE RESPONSE	
	o CORRECTIVE ACTIONS	
	o RESULTS OF CORRECTIVE ACTIONS	
	O CURRENT FAILURE HISTORY	
	o SEQUENCE AND TYPE	
0	CONCLUSIONS	C. R. DIFT

JULY 14, 1988

AGENDA

0	JUST	IFICATION FOR CONTINUED OPERATION RESPONSE	J.	S.	BOONE
	0	PROBLEMS IDENTIFIED PER VALVE			
	0	INDIVIDUAL MODIFICATIONS PER VALVE			
	,	ACCEPTABILITY OF CORRECTIVE ACTIONS			
	0	ACCEPTANCE TESTING			
0	HPCI	VALVE PERFORMANCE	J.	0'	SULLIVAN
	0	MECHANICAL ANALYSIS CHARACTERIZATION (MAC)			
	0	TORQUE SETTING VARIANCE			
	0	CORRECTIVE ACTIONS			

o INTERIM

O LONG TERM

JULY 14, 1988

- O CONCLUSIONS
 - o PREVIOUS CORRECTIVE ACTIONS
 - o NARROWLY FOCUSED
 - o FAILURE TO CHALLENGE DESIGN/AS-INSTALLED VERSUS THE DESIGN BASES/CRITERIA
 - CURRENT AND PROJECTED CORRECTIVE ACTIONS
 - O CONFIDENT IN THE RESULTS. . . . PROVE IT!!
 - O ASSESSING SELECTIVE DECREASES IN SURVEILLANCE
 INTERVALS OR INCREASED FREQUENCY OF TESTING
 FOR HISTORICAL POOR PERFORMANCE
 - O CONFIDENT IN THE RESULTS. . . . WHY IMPROVE?
 - O PLANT MODIFICATIONS ARE DEVELOPED TO IMPROVE
 OPERATING MARGINS COMPARED TO THE ENTIRE
 SPECTRUM OF DESIGN BASES REQUIREMENTS
 - O ROOT CAUSE DETERMINATIONS WILL ENABLE
 ELIMINATION OF CHRONIC FAILURE CONTRIBUTORS
 - O VOLTAGE SURGE PROTECTION

JULY 14, 1988

IMPROVE (?). . . (CONTINUED)

- o ELIMINATION OF STARTING RESISTORS
- O VALVE APPLICATIONS TO ELIMINATE THERMAL BINDING
 - O VALVE RELOCATION TO IMPROVE OPERATING ENVIRONMENT/TEMPERATURE IMPACT ON MOTOR CAPACITY
 - O EFFECT OF THE ABOVE ACTIONS IS NOT YET QUANTIFIABLE
 - O OTHER FAILURES SUCH AS THE HIGH STEAM FLOW ISOLATION SETPOINTS ARE CONSIDERED TO BE ISOLATED OCCURRENCES

PROBLEMS

- O SUMMARY
 - O THERMAL BINDING
 - O CHANGES IN VALVE TEMPERATURE INCREASE TORQUE REQUIREMENTS
 - o NO ALLOWANCE IN ORIGINAL MOTOR SIZING BY VENDOR
 - O CAUSED BY CLOSING HOT; OPENING COLD
 - VALVE BODY CONTRACTION EXCEEDS DISK CONTRACTION
 - o MOTOR TORQUE DEFICIENCY
 - o MOTOR UNABLE TO DEVELOP REQUIRED TORQUE IN SOME CONDITIONS
 - O STARTING RESISTOR
 - o REDUCED STARTING VOLTAGE FOR 1-2 SECONDS
 - o FOR OPENING,
 - MAXIMUM TORQUE NEEDED TO UNSEAT
 - o MOTOR MAY STALL AND NOT RESTART EVEN WITH FULL VOLTAGE

- o FOR CLOSING,
 - O MINIMAL TORQUE NEEDED TO START
 - O NO IMPACT
- O PRESENCE OF STARTING RESISTORS NOT CONSIDERED IN MOTOR SIZING BY VENDOR

o CABLE SIZING

- O UNABLE TO SUPPLY SUFFICIENT CURRENT TO
 DEVELOP ASSUMED TORQUE FOR ALL CONDITIONS
- ACTUAL MOTOR AND CABLE TEMPERATURES REDUCE
 ASSUMED CURRENT CAPABILITY
- O CABLE NOT SIZED FOR FULL LOAD REQUIRED TO UNSEAT OR TORQUE SEAT VALVE
- o TORQUE SWITCH SETTING
 - o MOTOR SIZED FOR MAXIMUM DESIGN LOAD
 - O TORQUE SWITCH SET ABOVE MAXIMUM DESIGN LOAD

- O UNIT 1 HPCI STEAM SUPPLY VALVE (1-E41-F001)
 - O THERMAL BINDING
 - O EXISTS UP TO APPROXIMATELY (WO HOURS AFTER HPCI STEAM LINE PRESSURIZED
 - O OCCURS ONLY AFTER STEAM LINE ISOLATED FOR MAINTENANCE OR TESTING
 - O DISAPPEARS AFTER RETURN TO NORMAL TEMPERATURE
 - o MOTOR TORQUE DEFICIENCY
 - INSUFFICIENT TORQUE TO OPEN VALVE
 - O RESULTS FROM A LOSS OF OFF-SITE POWER WHICH CAUSES MINIMUM BUS VOLTAGE
 - ADEQUATE VOLTAGE IN 10 SECONDS
- O UNIT 1 AND 2 HPCI INJECTION VALVES (E41-F006)
 - MOTOR TORQUE DEFICIENCY
 - O INSUFFICIENT TORQUE TO OPEN VALVE
 - O INSUFFICIENT TORQUE TO TORQUE SEAT VALVE CLOSED
 - OCCURS ONLY DURING A MAIN STEAM LINE BREAK ACCIDENT IN THE MSIV PIT
- O UNIT 1 AND 2 RCIC INJECTION VALVE (E51-F013)
 - O NO PROBLEMS FOUND

RESOLUTIONS

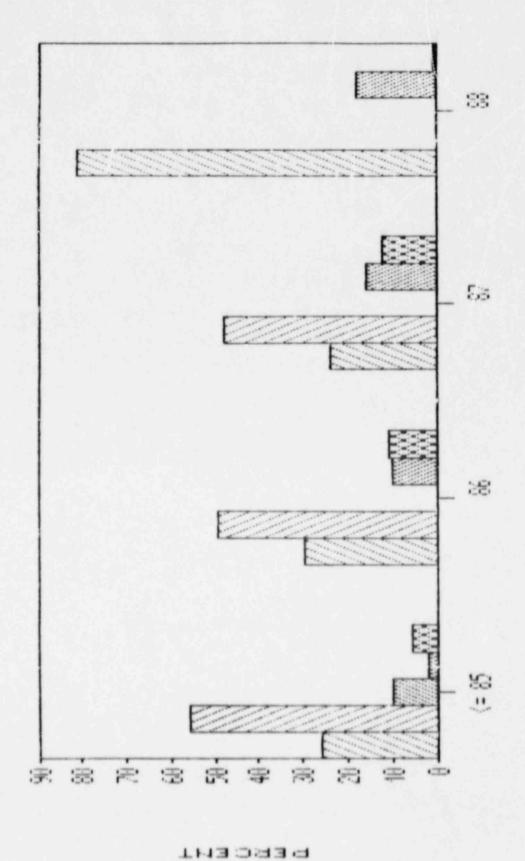
- O THERMAL BINDING
 - o E41-F001 (UNIT 1 AND UNIT 2)
 - O EXTENDED HPCI STEAM LINE PRESSURIZATION/WARM-UP TIME TO FOUR HOURS AFTER UNISOLATING
 - O HPCI CONTINUES TO BE CONSIDERED INOPERABLE DURING THIS PERIOD
 - O NO CREDIT TAKEN FOR HPC1 DURING PERIOD THERMAL BINDING COULD EXIST
 - o ACCEPTABILITY
 - O HPCI NOT CONSIDERED OPERABLE WHEN POTENTIAL FOR THERMAL BINDING EXISTS
 - O SUSCEPTIBLE CONDITION EXISTS ONLY APPROXIMATELY
 TWO HOURS AFTER HPCI STEAM LINE IS PRESSURIZED
 FOLLOWING MAINTENANCE OR TESTING
- O MOTOR TORQUE DEFICIENCY
 - o E41-F001 (UNIT 1)
 - O ELIMINATED REDUCED VOLTAGE STARTING
 - o INCREASED POWER CABLE SIZE
 - O CHANGED OPERATOR GEAR RATIO TO INCREASE TORQUE

- o E41-F006 (UNIT 1)
 - ELIMINATED REDUCED VOLTAGE STARTING
 - O OUTAGE BEGUN TO INSTALL LARGER MOTOR
 - o E41-F006 (UNIT 2)
 - O ELIMINATED REDUCED VOLTAGE STARTING
 - O OUTAGE PLANNED TO BEGIN ABOUT JULY 17 TO INSTALL LARGER MOTOR
 - o E51-F013 (UNIT 1 AND UNIT 2)
 - O ELIMINATING REDUCED VOLTAGE STARTING
 - SUFFICIENT MOTOR TORQUE AVAILABLE
 - CHANGE PERFORMED TO ACHIEVE ADDED MARGIN
 - o ACCEPTABILITY
 - o ADEQUATE TORQUE CAPABILITY RESTORED FOR DESIGN CONDITIONS
 - O CHANGES REVIEWED WITH VENDORS
 - O OTHER DESIGN REQUIREMENTS SATISFIED
 - O DC LOAD STUDY
 - O CABLE SIZING
 - O MCC/BREAKER/STARTER CAPACITY

ACCEPTANCE TESTING

- 0 E41-F001 VALVE
 - O MAC TEST AT 0# AND 1000#
 - O STROKE TIME
 - O CURRENT TRACE
 - o TORQUE
 - O HPCI OPERABILITY SURVEILLANCE
 - o TECHNICAL SPECIFICATION FUNCTIONAL TEST
 - o ISI PERFORMANCE PESTS ON SYSTEM AND FOO1 AND FOO6 VALVES
- 0 E41-F006
 - O STROKE TIME
 - O CURRENT TRACE
 - o MAC TEST (PLANNED)
 - o STROKE TIME
 - O CURRENT TRACE
 - o TORQUE

- O HPCI OPERABILITY SURVEILLANCE (PLANNED)
 - O TECHNICAL SPECIFICATION FUNCTIONAL TEST
 - O ISI PERFORMANCE TESTS ON SYSTEM AND FOO1 AND FOO6 VALVES
- 0 E51-F013
 - O STROKE TIME
 - O CURRENT TRACE



TO NOTE TO THE POSTUTIONS OF PRINCING OF THE CONTROLS

VALVE MOTOR FAILURE HISTORY

1-E41-F001 (4 FAILURES)

10/08/86

12/31/87

05/28/87

07/01/88

2-E41-F001 (0 FAILURES)

1-E41-F006 (0 FAILURES)

2-E41-F006 (FAILURE)

01/05/87

1-E51-F013 (0 FAILURES)

2-E51-F013 (0 FAILURES)

VALVE TEST DATA

(MOTOR ACTUATOR CHARACTERIZER)

		TORQUE (FT LBS)	CURRENT (AMPS)	т.с
1-E41-F001		XT CD3	1/1/15/	I.S.
5/17/87	CLOSING OPENING	584.5 245.9	26.25 11.11	2 1/4
7/10/88	CLOSING OPENING	569.0 379.1	45.66 18.8	2 1/8
2-E41-F001				
1/15/88	CLOSING OPENING	606.3 305.1	33.43A 10.13A	2 3/8
7/12/88(1)	CLOSING OPENING	601.9 257.5	31.77A 12.72A	2 3/8
1-E41-F006				
5/31/87	CLOSING OPENING	1,771.3	64.2 35.8	1.5
7/10/88(1,2	CLOSING OPENING	NA NA	66.18 82.78	NA
2-E41-F006				
3/31/88	CLOSING OPENING	1,871.3 1,211.1	61.78 28.08	1 3/4
7/11/88(1,2	OPENING	NA NA	78.39A 55.92A	NA

NOTE: (1) WITHOUT STARTING RESISTORS.

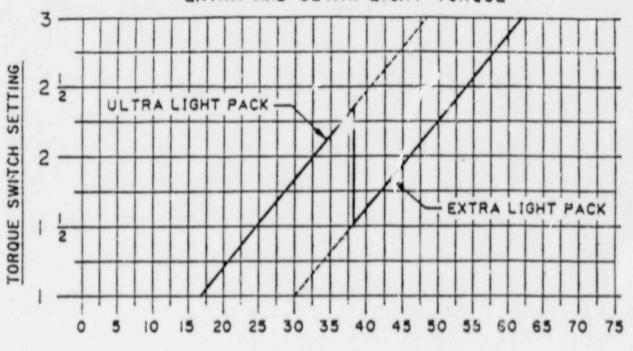
⁽²⁾ AT 1000 PSI DIFFERENTIAL PRESSURE-CURRENT TRACE ONLY.

VALVE TEST DATA

(MOTOR ACTUATOR CHARACTERIZER) (CONT'D)

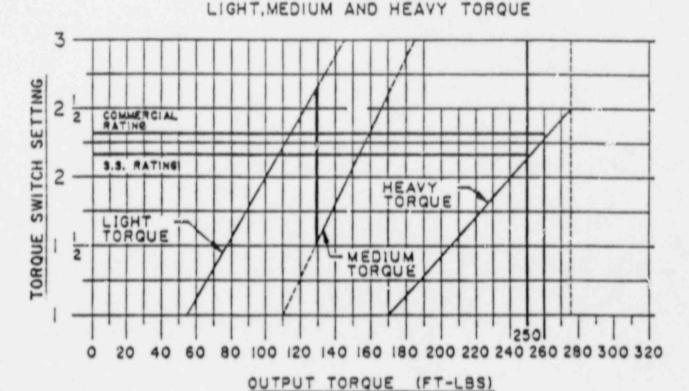
		TORQUE (FT LBS)	CURRENT (AMPS)	<u>I.S.</u>
1-E51-F013				
5/24/87	CLOSING OPENING	3.2 35.4	7.55 3.88	1.5
2-E51-F013				
3/2/88	CLOSING OPENING	76.2 56.5	4.4	1

TECHNICAL DETAILS SMB-00 TORQUE SWITCH SETTING CHART EXTRA AND ULTRA LIGHT TORQUE

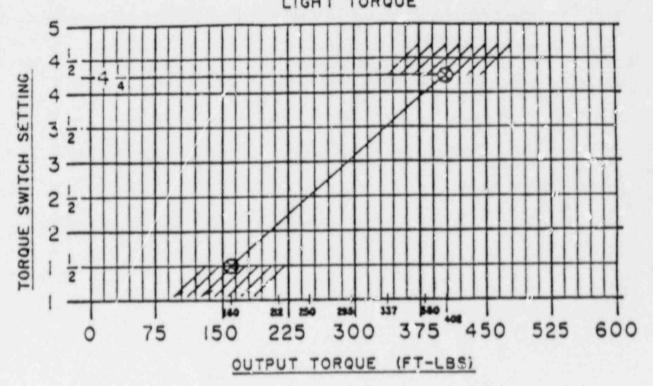


TECHNICAL DETAILS
SMB-00 TORQUE SWITCH SETTING CHART

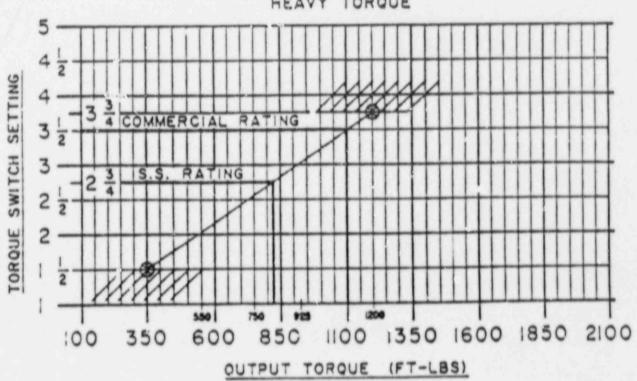
OUTPUT TORQUE (FT-LBS)

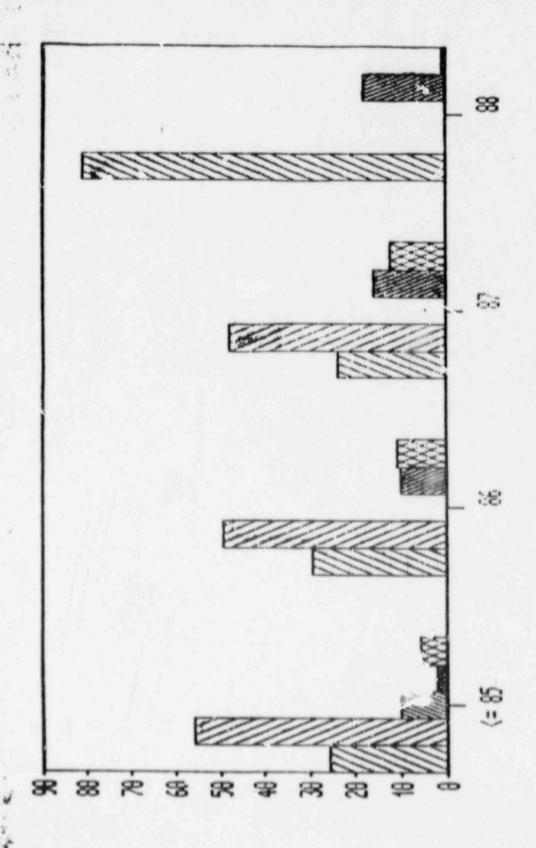


TECHNICAL DETAILS SMB-1 TORQUE SWITCH SETTING CHART LIGHT TORQUE



TECHNICAL DETAILS SMB-1 TORQUE SWITCH SETTING CHART HEAVY TORQUE



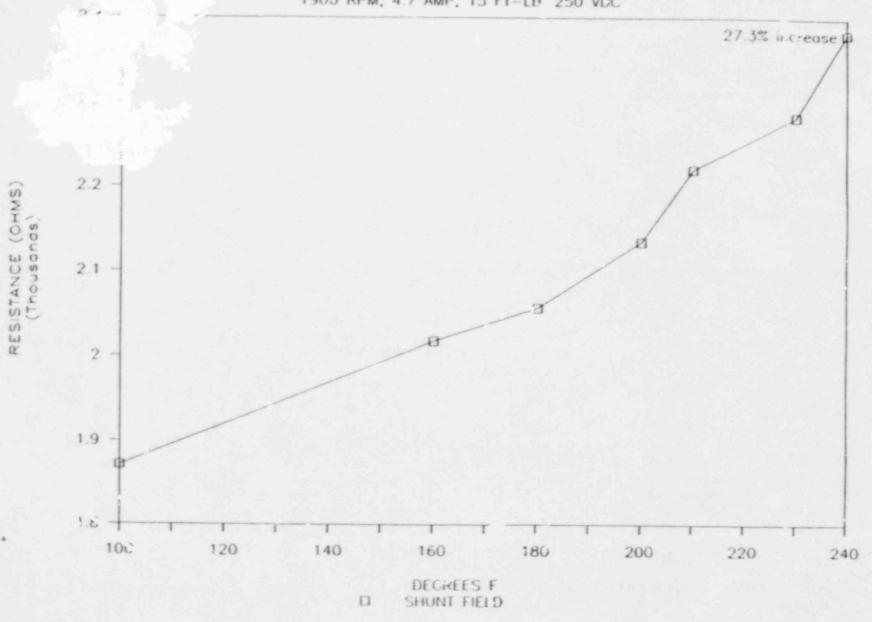


PERCENT

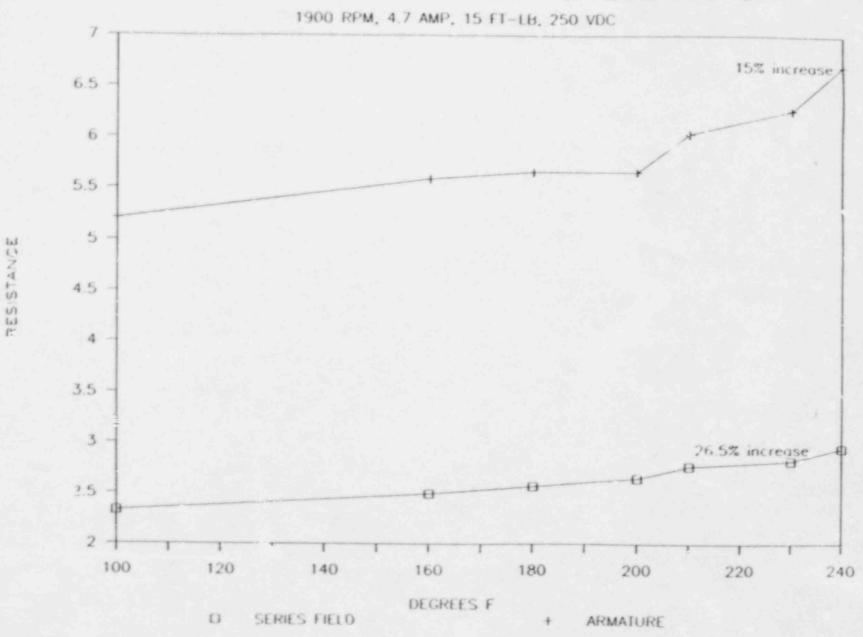
ZI MOY INTURB/DOTHTKOLS INTO PARKING IN PAR IN DOTHER

TEMP vs OHMS FOR A LIMITORQUE MOTOR

1900 RPM, 4.7 AMP, 15 FT-LB 250 VLC



TEMP vs OHMS FOR A LIMITORQUE MOTOR

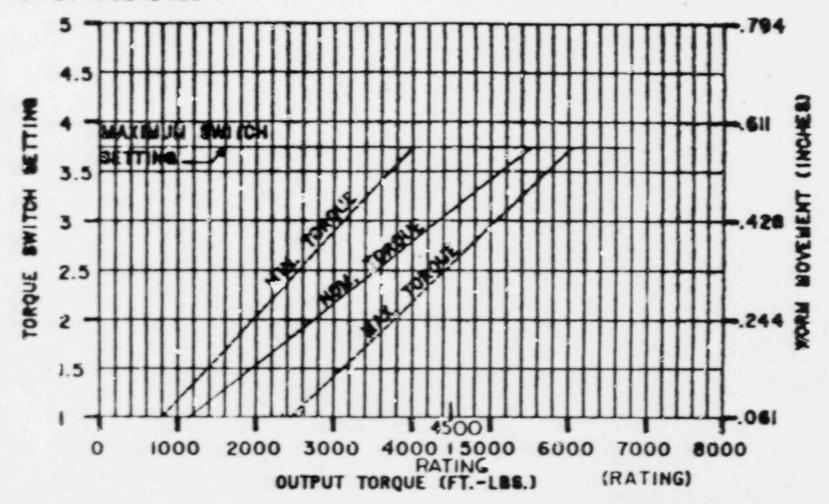


SMB/HMB-3 TURQUE SWITCH SETTING CHART

10 SPRINGS - .124" PRELOAD DWG. NO. 60-600-0079-1

NO 60-682-0405-1

CALIBRATION NAMEPLATE MAXIMUM TORQUE SWITCH SETTING - 3 3/4



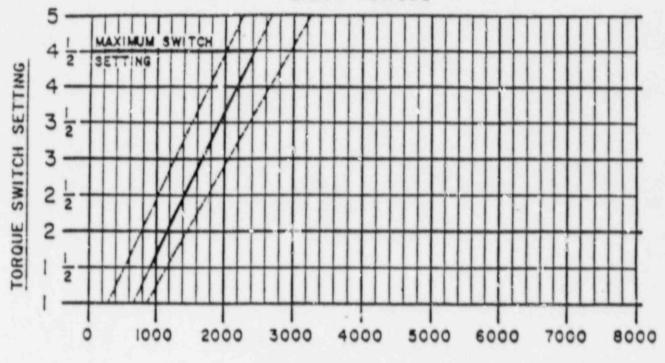
B/M NO. 1106-1-2

DRN. R.GLOVER DATE

REV.

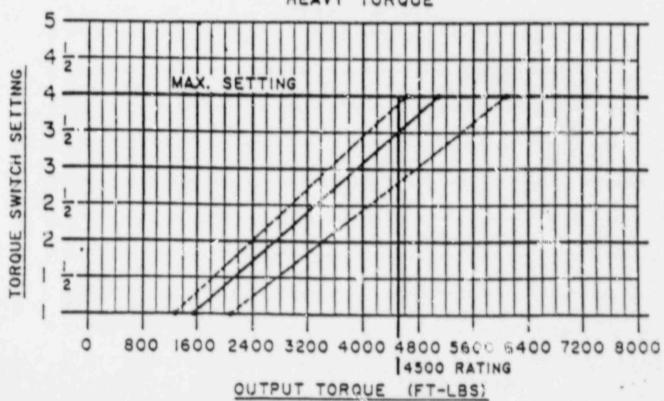
TECHNICAL DETAILS SMB-3 TORQUE SWITCH SETTING CHART

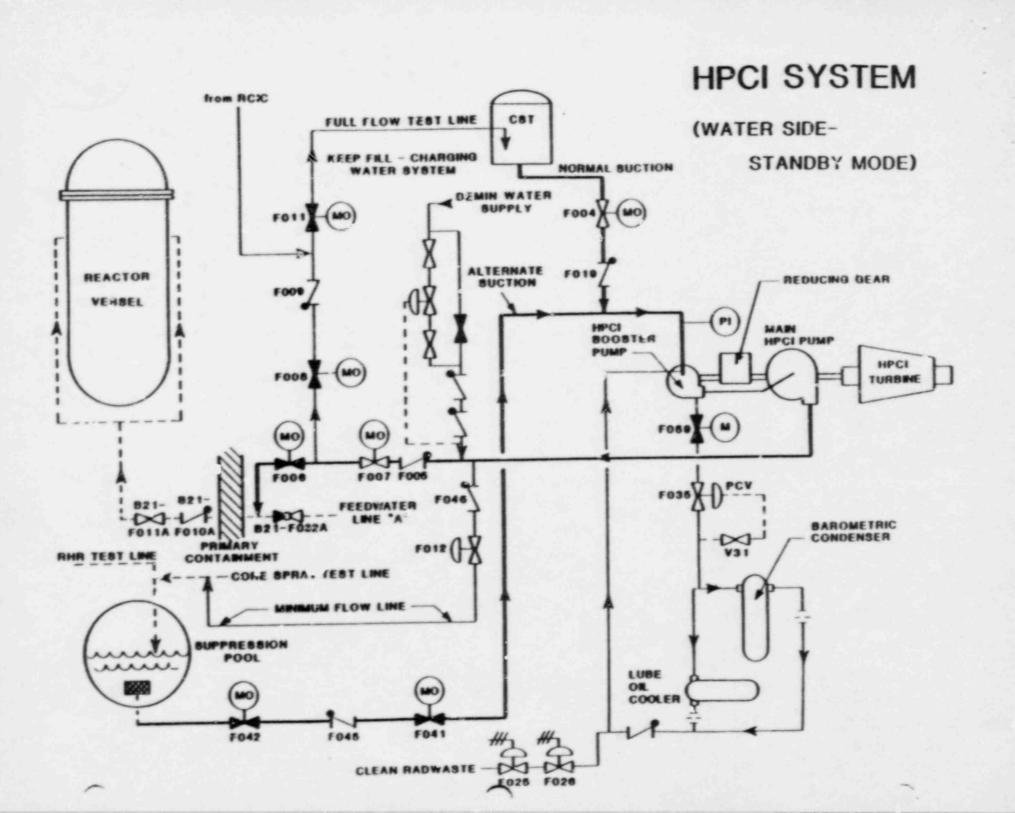
LIGHT TORQUE

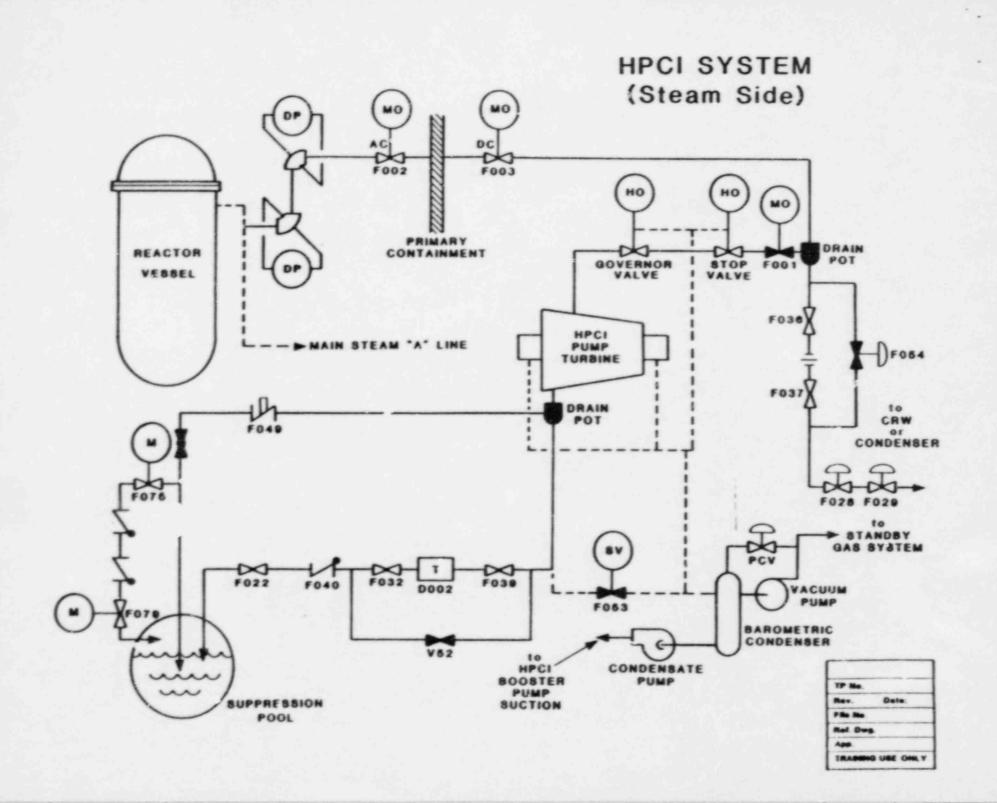


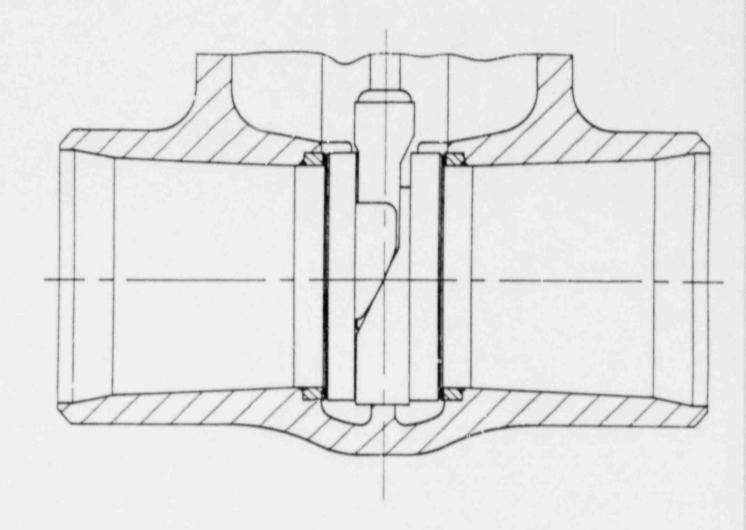
OUTPUT TORQUE (FT-LBS)

TECHNICAL DETAILS
SMB-3 TORQUE SWITCH SETTING CHART
HEAVY TORQUE

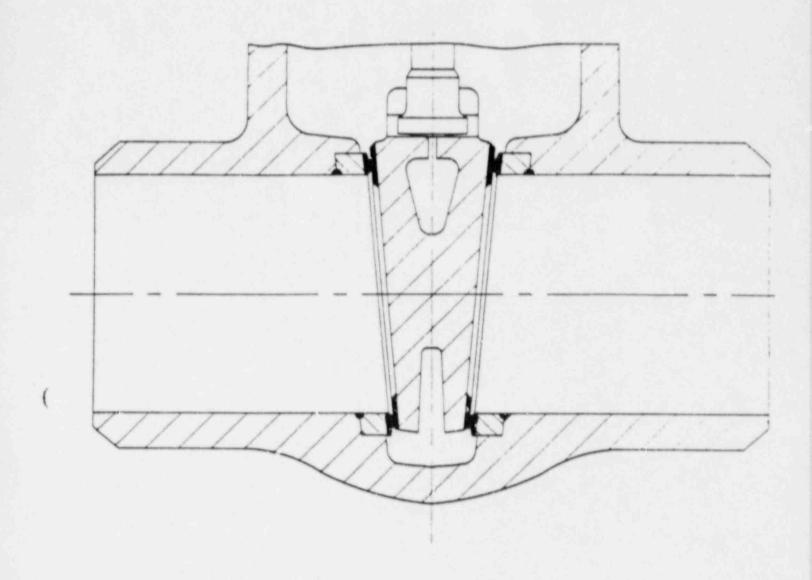






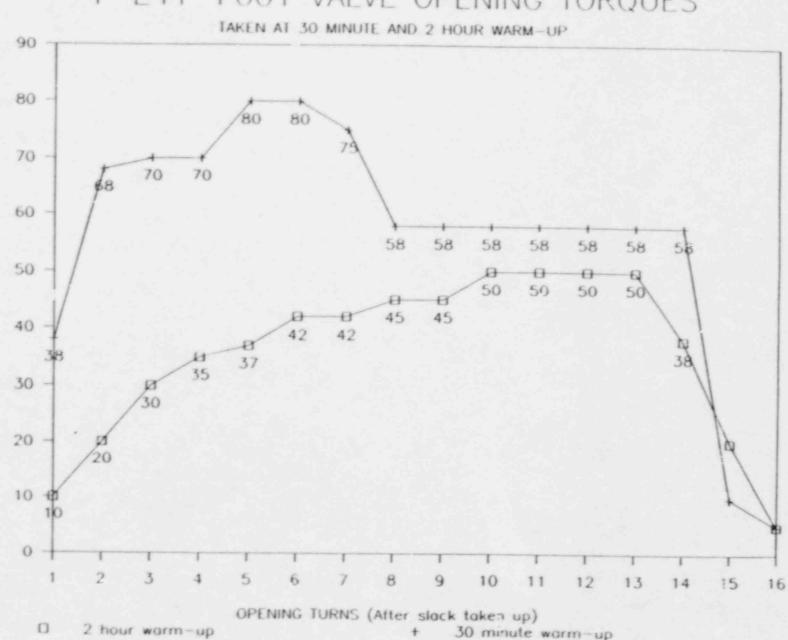


DOUBLE DISC PARALLEL SEAT GATE VALVE



FLEX WEDGE GATE VALVE

1-E41-F001 VALVE OPENING TORQUES



OPENING TOROUE

VALVE MOTOR OPERATOR DATA

E41-F001:

SIZE: SMB-1 (60'#) MCTOR: 1900
DIFF PRESS: 1118 PSI MOTOR HP: 4.35
STROKE TIME: 20 SEC FULL LOAD AMPS: 17
POWER SUPPLY: DC LOCKED ROTOR AMPS: 105
VOLTAGE: 240

E41-F006:

SIZE: DIFF PRESS:	SMB-3 (100'#) 1550 ps:	MOTOR: MOTOR HP:	1900
STROKE TIME:	20 SEC	FULL LOAD AMPS	30
POWER SUPPLY: VOLTAGE:	DC 240	LOCKED ROTCE AMPS:	146

NEAR TERM ENHANCEMENTS

1-E51-F013 2-E51-F013	REMOVE STARTING RESISTORS TO INCREASE OPERATING MARGINS.
1-E41-F012 1-E41-F041 1-E41-F042 1-E41-F059	REMOVE STARTING RESISTORS.
1-E51-F019 1-E51-F029 1-E51-F031	REMOVE STARTING RESISTORS.

REVERIFY INPO SOER 84-7 FINDINGS.

EVALUATE THE EFFECTS OF TEMPERATURE CONTRIBUTED BY MOTOR HEATERS AND SHUNT FIELD.

MISSION STATEMENT

THROUGH SYSTEMATIC ANALYSIS DETERMINE THAT THE BRUNSWICK PLANT'S
SAFETY RELATED MOTOR-OPERATED VALVES WILL FUNCTION PROPERLY
WHEN SUBJECTED TO DESIGN BASIS OPERATING, ENVIRONMENTAL AND
DEGRADED VOLTAGE SCENARIOS. VALVES AND OPERATORS WHOSE DESIGN
OR APPLICATION DOES NOT OFFER ADEQUATE DESIGN OPERATING MARGIN
WILL BE IDENTIFIED FOR REPLACEMENT OR MODIFICATION AS APPROPRIATE.

VALVE ANALYSIS OVERVIEW

- * CONSISTENT WITH DEVELOPED PRA TECHNIQUES, ESTABLISH A PRIORITIZATION SCHEME DESIGNED TO SELECT VALVES FOR EXAMINATION BASED ON THE FOLLOWING:
 - CRITICALITY OF SERVICE
 - OPERATING HISTORY IN-PLANT
 - INDUSTRY OPERATING HISTORY
- ESTABLISH EFFECTIVE LIAISON WITH VALVE AND OPERATOR VENDORS.
- * OBTAIN UPDATED VALVE AND OPERATOR DATA FROM VENDORS.
- DEVELOP CRITERIA FOR EVALUATING EXISTING VALVE INSTALLATIONS TO UPDATED DESIGN INFORMATION.
- DEVELOP A PROJECT PLAN AND SCHEDULE TO IDENTIFY NEAR-TERM AND LONG-"FRM OBJECTIVES BASED ON PRIORITIZATION SCHEME.

SCHEDULE

August 15, 1988: PROMULGATE A PLAN AND SCHEDULE THAT WILL ESTABLISH MILESTONES AND COMPLETION DATES FOR THE ANALYSIS PHASE.

DECEMBER 31, 1988: COMPLETE THE DESIGN ANALYSIS OF SAFETY RELATED VALVES.

FEBRUARY 28, 1989: COMPLETE DEVELOPMENT OF A CORRECTIVE ACTION IMPLEMENTATION PLAN TO ADDRESS PROBLEMS IDENTIFIED.