

E 2.30.1.5 RR 2 P-2-85-02

February 13, 1986

Mr. James G. Keppler Regional Director, Region III Office of Inspection & Enforcement U. S. Nuclear Regulatory Commission 799 Roosevelt Road Glen Ellyn, Illinois 60137

Subject: Effluent and Waste Disposal Semiannual Report for the Period From July 1, 1985 through December 31, 1985 Davis-Besse Nuclear Power Station Unit 1.

Dear Mr. Keppler:

Enclosed find two (2) copies of the Effluent and Waste Disposal Semiannual Report for Davis-Besse Nuclear Power Station covering the third and fourth quarters of 1985. Included as attachments are the revised versions of the Offsite Dose Calculation Manual (ODCM) and the Process Control Program (PCP) per Davis-Besse's Technical Specifications Appendix A, Section 6.9.1.11.

The applicable portions of Regulatory Guides 1.109, 1.111, and 1.113 have been used along with NUREG-0133 for dose calculations and meteorological modeling methodology to demonstrate compliance with Appendix I to 10 CFR Part 50.

Sincerely.

Louis F. Storz Plant Manager

Davis-Besse Nuclear Power Station

LFS/JB

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Enclosures

Mr. James M. Taylor

Office of Inspection & Enforcement

Encl.: 25 copies

Ohio Environmental Protection Agency

Northwest District Office

Services

Encl:

1 copy

Health Program Director Ohio Department of Health

Encl: 1 copy

Mr. James Greer

Ottawa County Disaster

Encl:

1 copy

THE TOLEDO EDISON COMPANY EDISON PLAZA

300 MADISON AVENUE TOLEDO, OHIO 43652

NRC Resident Inspector

Encl: 1 copy

SEMIANNUAL REPORT

DAVIS-BESSE NUCLEAR POWER STATION

UNIT 1

For the Period From

JULY 1, 1985 - DECEMBER 31, 1985

Docket No. 50-346 License No. NPF-3

TOLEDO EDISON COMPANY 300 MADIFON AVENUE TOLEDO, OHIO 43652

FEBRUARY, 1986

EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT

DAVIS-BESSE NUCLEAR POWER STATION

UNIT 1

JULY 1, 1985 - DECEMBER 31, 1985

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Facility: Licensee:

Davis-Besse Nuclear Power Station, Unit 1

The Toledo Edison Company

Reporting Period:

July 1, 1985 - December 31, 1985

Supplemental Information:

1. Regulatory Limits

Liquid and Gaseous Radioactive Effluent Limits

	LIQUID	G.	AS
ANNUAL DOSE COMMITMENT FROM URANIUM FUEL CYCLE SOURCES (40 CFR 190)		nrems total body or any	organ .
DOSE LIMIT		Noble Gas	I-131, Tritium & Particulates**
Calendar quarter	<pre><1.5 mrem total body <5 mrem to any organ</pre>	<pre><5 mrad /qtr.* <10 mrad /qtr.*</pre>	<7.5 mrems/qtr. any organ
lendar year	<pre><3 mrem total body <10 mrem to any</pre>	<pre><10 mrad /yr* <20 mrad /yr*</pre>	<15 mrems/yr any organ
DOSE RATE LIMIT		<pre><500 mrems/yr total</pre>	<1500 mrems/yr any organ
MICROCURIES PER MILLIMETER LIMIT	10 CFR 20 Part 20.106		
MICROCURIES PER MILLIMETER LIMIT FOR DISSOLVED OR ENTRAINED NOBLE GASES	2x10 ⁻⁴ microcuries/ml		

^{**}With half-lifes greater than 8 days

^{2.} Maximum Permissible Concentrations - Limits used are specified in 10 CFR 20, Appendix B, Table II, Column 2.

4. Measurements and Approximations of Total Radioactivity



- These sases, excluding tritium, are collected in a Marinelli type beaker, specially modified for sas sampling, steel bombs, or slass vials and counted on a sermanium detector for principal samma emitters.
- Tritium sas is collected using a bubbler apparatus and counted by liquid scintillation.
- b. Iodines are collected on a charcoal or zeolite cartridge filter, and counted on a sermanium detector.
- c. Particulates are collected on filter paper and counted on a sermanium detector.
- d. Liquid Effluents are counted in a bottle or Marinelli beaker on a sermanium detector.

Batch Releases

a. Liquid

1.	Number of ba	tch releases:	35	
2.	Total time s	eriod for batch releases:	5.31E+01	Hours
3.	Maximum time	period for a batch release:	1.80E+02	Minute
4.	Average time	period for batch releases:	9.11E+01	Minute
5.	Minimum time	period for a batch release:	7,50E+01	Minute

b. Gaseous

1.	Number of batch releases:	5	
2.	Number of containment purses:	3	
3.	Number of waste sas decay tank releases:	2	
4.	Total time period for batch releases:	1.15E+02	Hours
5.	Maximum time period for a batch release:	2.22E+03	Minutes
6.	Average time period for batch releases:	1.38E+03	Minutes
7.	Minimum time period for a batch release:	8.80E+01	Minutes

6. Abnormal Releases

None

7. Radiological Effluent Technical Specifications (RETS) Percent of Limits

Specification	Limit	Percent
a. Quarterly: Gaseous		
Third quarter, 1985		
Noble dases (damea)	5 mRad/atr	7.46E-03
Noble dases (beta)	10 mRad/atr	1.10E-02
I-131, tritium, and radionuclide in particulate form with half-		
lives greater than 8 days	7.5 mRem/atr	2.76E-03
b. Quarterly: Gaseous		
Fourth quarter, 1985		
Noble sases (samma)	5 mRad/atr	4.14E-06
Noble sases (beta)	10 mRad/atr	2.34E-04
I-131, tritium, and radionuclide in particulate form with half-		
lives sreater than 8 days	7.5 mRem/atr	1.83E-03
c. Calendar year: Gaseous		
Noble dases (damma)	10 mRad/yr	3.73E-03*
Noble dases (beta)	20 mRad/yr	5.64E-03*
I-131, tritium, and radionuclide in particulate form with half-	5	
lives greater than 8 days	15 mRem/sr	2.29E-03
d. Quarterly: Liquid		
Third quarter, 1985		
Total body	1.5 mRem/atr	9.99E+00
Any organ (LIVER)	5 mRem/atr	4.27E+00
e. Quarterly, Liquid		
Fourth auarter, 1985		
Total body	1.5 mRem/atr	9.89E-01
Any orsan (LIVER)	5 mRem/atr	4.19E-01
f. Calendar year:		
Total body	3 mRem/yr	5.49E+00*
Any organ (LIVER)	10 mRem/yr	2.34E+00*

^{*} Value represents the percent of annual limit for the third and fourth quarters of 1985 since Davis-Besse's RETS went into effect during the second half of 1985.

8. Dose Assessment

The following is a list of the sources of input data:

- a. Water usage source:
 Appendix I analysis, NRC Docket 50-346, Evaluation of Compliance with Appendix I to 10CFR50, June 4, 1976, Davis-Besse Nuclear Power Station Unit No. 1.
- b. 0-50 mile meat, milk, vesetable production, and population data source: 1982 Annual Environmental Operating Report, report entitled, "Evaluation of Compliance With Appendix I to 10CFR50: Updated Population, Asricultural, Meat-Animal, and Milk Production Data Tables for 1982. This evaluation was based on the 1980 Census; the Asricultural Ministry of Ontario 1980 report entitled, "Asricultural Statistics and Livestock Marketing Account, 1980; the Asricultural Ministry of Ontario 1980 report entitled "Asricultural Statistics for Ontario - 1980 Publication 21, 1980; the Michigan Department of Asriculture, July, 1981 report entitled "Michigan Asricultural Statistics, 1981; the Ohio Crop Reporting Service, 1981 report entitled "Ohio Asricultural Statistics, 1981"
- c. Gaseous and liquid source terms sources: Tables 1A, 1C, 2A and 2B.
- d. Location of the nearest individuals and pathways by sector out to 5 miles - source: 1985 Annual Environmental Operating Report, report entitled, "Land Use Census".

Tables 1 and 3 present the maximum doses computed from the noble sas effluents for each quarter. Tables 2 and 4 present doses resulting from saseous iodine, and particulate effluents. Doses resulting from liquid releases are presented in Tables 5 and 6.

9. Inoperable RETS Equipment

The following are explanations as to why certain monitoring equipment required under Davis-Besse's Radiological Effluent Technical Specifications were inoperable for more than 30 days.

- a. Waste Gas System Effluent Flow Rate Measuring Device's FT1821 and FT1821A were declared inoperable on 10/30/85 at 0000 hours. These meters were found to be malfunctioning during calibration and were sent to a vendor for repair. The vendor has informed us that replacement parts are no longer available. New monitors have been ordered and we are currently awaiting shipment.
- b. Waste Gas System Oxygen Monitor AE5828B was declared inoperable on 11/8/85 at 0825 hours. Due to engineering difficulties this meter is still inoperable.
- c. Station Vent Stack Radiation Monitor Sample Flow Device FT4598AA was declared inoperable on 10/30/85 at 0000 hours. The meter was returned to an operable state on 2/12/86 at 0200 hours. The delay in getting the meter back to an operable state was due to the implementation of newly acquired test equipment. The total days of inoperability was 105 days.
- d. Station Vent Stack Radiation Monitor Sample Flow Device FT4598BA was declared inoperable on 10/30/85 at 0000 hours. The meter was declared operable on 12/6/85 at 1650 hours. The delay was caused by the implementation of newly acquired test equipment. The total days of inoperability was 36 days.

TABLE 1A

| EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1985) | GASEOUS EFFLUENTS - SUMMATION OF ALL RELEASES |

		UNIT	3RD QUARTER		EST. TOTAL ERROR, %
Α.	FISSION & ACTIVATION GASES				
	1. TOTAL RELEASE 2. AVERAGE RELEASE RATE	CI	1.81E+01	2.07E-01	2.00E+01
	FOR PERIOD 3. PERCENT OF TECHNICAL	UCI/SEC	2.27E+00	2.61E-02	
	SPEC. LIMIT (RETS)	See Sect	7, Supp I	nformation	
В.	I-131, TRITIUM, PARTICULATES,	and ALPH	4		
	1. I-131, TRITIUM, AND PARTICULATES WITH HALF-				
	LIVES > 8 DAYS 2. AVERAGE RELEASE RATE	CI	3.06E+00	2.76E+00	2.00E+01
	FOR PERIOD 3. PERCENT OF TECHNICAL	UCI/SEC	3.84E-01	3.48E-01	
	SPEC. LIMIT (RETS) 4. GROSS ALPHA RADIO-	See Sect	7. Supp I	nformation	
	ACTIVITY	CI	1.36E-05	7.99E-06	

EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (85-2)

GASEOUS EFFLUENTS- ELEVATED RELEASE *

The state of the same of the s	-			-	-
Muclides Released	Unit	Quar-	Quar-	Quarter	Quar-

1. Fission gases

krypton-85	Cí	E		E	E	E
krypton-85m	Ci	E		E	E	E
krypton-87	Ci	E		E	E	E
krypton-88	Ci	E		E	E	E
xenon-133	Ci	E		E	E	E
xenon-135	Ci	E	٥	E	E	E
xenon-135m	C1	E		E	E	E
xenon-138	C1	E		E	E	E
Others (specify)	C1	E		E	E	E
	Ci	E		E	E	E
	C1	E		E	E	E
unidentified	Ci	E		E	E	E
Total for period	Ci	E		E	E	E

2. Iodines

iodine-131	Ci	1.	E	E	E	E
iodine-133	Ci		E	E	E	E
iodine-135	Ci		E	E	E	E
Total for period	Ci		E	E	E	E

3. Particulates

strontium-89	Ci	1.	E	E	E	E
strontium-90	Ci		E	E	E	E
cesium-134	Ci		E	E	E	E
cesium-137	Ci		E	E	E	E
barium-lanthanum-140	Ci		E	E	E	E
Others (specify)	Ci		E	E	E	E
	Ci		E	E	E	E
	Ci		E	E	E	E
unidentified	Ci		E	E	E	E

^{*} Not applicable; all releases are classified as mixed mode releases.

TABLE 1C

| EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1985) | GASEOUS EFFLUENTS MIXED MODE RELEASES

		CONTINUOU	S MODE	BATCH	MODE
NUCLIDES RELEASED	UNIT		4TH QUARTER	3RD QUARTER	
1. FISSION GASES					
KR-85	CI	0.00E-01	0.00E-01	6.92E-03	2.07E-01
XE131H	CI	0.00E-01		7.85E-05	
XE133M	CI	0.00E-01		7.09E-02	
XE-133	CI	0.00E-01		1.79E+01	The second secon
XE-135	CI	0.00E-01	0.00E-01	3.70E-02	0.00E-01
TOTAL FOR PERIOD	CI	0.00E-01	0.00E-01	1.81E+01	2.07E-01
2. IODINES					
I-131	CI	2.55E-06	0.00E-01	0.00E-01	0.00E-01
TOTAL FOR PERIOD	CI	2.55E-06	0.00E-01	0.00E-01	0.00E-01
3. PARTICULATES					
H-3	CI	2.91E+00	2.76E+00	1.47E-01	5.80E-04
TOTAL FOR PERIOD	CI	2.91E+00	2.76E+00	1.47E-01	5.80E-04

TABLE 2A

| EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1985) | | LIQUID EFFLUENTS - SUMMATION OF ALL RELEASES |

			QUARTER	QUARTER	EST. TOTAL ERROR, %
Α.	FISSION & ACTIVATION PRODUCTS				
	1. TOTAL RELEASE (WITHOUT TRITIUM, GASES, ALPHA)	CI	1.72F-02	8.535-03	2.00F±01
	2. AVERAGE DILUTED CONCEN- TRATION DURING PERIOD			1.41E-09	
	3. PERCENT OF TECHNICAL SPEC. LIMIT, (RETS) 4. PERCENT OF 10 CFR 20	See See	ct 7, Supp	Informatio	on
	LIMIT	χ	1.28E-02	2.87E-03	
в.	TRITIUM				
	1. TOTAL RELEASE 2. AVERAGE DILUTED CONCEN-	CI	5.88E+00	2.02E÷01	2.00E+01
	TRATION DURING PERIOD 3. PERCENT OF 10 CFR 20		9.01E-07	3.34E-06	
	LIMIT	×.	3.00E-02	1.11E-01	
С.	DISSOLVED & ENTRAINED GASES				
	1. TOTAL RELEASE 2. AVERAGE DILUTED CONCEN-	CI	0.00E-01	0.00E-01	2.00E+01
	TRATION DURING PERIOD 3. PERCENT OF 2 E-4	UCI/ML	0.00E-01	0.00E-01	
	UCI/CC LIMIT	%	0.00E-01	0.00E-01	
D.	GROSS ALPHA RADIDACTIVITY				
	1. TOTAL RELEASE	CI	0.00E-01	0.00E-01	2.00E+01
ε.	VOLUME OF WASTE RELEASED				
	(PRIOR TO DILUTION)	LITERS	3.33E+05	6.85E+05	2.00E+01
F.	VOLUME OF DILUTION WATER	1.5			
	1. TOTAL RELEASE	LITERS	6.53E+09	6.04E+09	2.00E+01

1.72E-02 8.53E-03

TABLE 2B

| EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1985) |

NUCLIDES RELEASED UNIT	3RD QUARTER	4TH QUARTER	3RD QUARTER	4TH QUARTER
E-55 CI			0.00E-01	2.12E-05
			2.59E-03	4.73E-03
FE-59 CI			7.03E-06	5.35E-06
CO-58 CI			1.66E-03	4.82E-04
CO-60 CI			3.29E-04	1.33E-03
AG110M CI			4.17E-05	4.80E-05
SB-125 CI			6.10E-05	8.70E-05
CS-134 CI			2.85E-03	3.85E-04
CS-137 CI			9.66E-03	1.44E-03
CE-141 CI			0.00E-01	9.06E-07

TOTAL FOR PERIOD ABOVE CI

^{*} NOT APPLICABLE; ALL RADIOACTIVE LIQUID EFFLUENTS ARE RELEASED BY BATCH MODE.

EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (85-2) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS

A. SOLID WASTE SHIPPED OFFSITE FOR BURIAL OR DISPOSAL. (Not irradiated fuel)

1. Type of waste	Unit		Est. Total
a.Spent resins, filter sludges, evaporator bottoms, etc.	3 M Ci	3.50 E+1 3.76 E+0	1 1.0 E+1
b.Dry compressible waste, contaminated equip, etc.	3 M Ci	5.00 E+1 5.70 E-1	1.0 E+1
c.Irradiated components, control rods, etc.	3 M Ci	· E	
d.Other (describe) Dewatered Primary system cartridge filters	3 M Ci	4.19 E+0 5.20 E+1	

2 Estimate of major nuclide composition (by type of waste)

а,	Co-58	1 %	1 3.90 E+1 1
	Co-60	! ! %	2.10 E+1
	Ni-63	1 %	2.10 E+1
ь.	Cs-137	1 %	1 4.60 E+1
	Co-60	1 %	1 1.60 E+1
	Cs-134		1 1.80 E+1
c.	N/A		. E !
d.	Ni-63	1 %	6.40 E+1
	Co-60	1 %	1 3.20 E+1
	Cs-137	1 %	1.00 E+0

3. Solid Waste Disposition

Barnwell, S.C. 29812

B. IRRADIATED FUEL SHIPMENTS (Disposition)

Number of Shipments	Mode of Transportation	Destination
None	N/A	N/A

Table 1 Page 12

SEMIANNUAL MAXIMUM INDIVIDUAL DOSE TABLE (GASEOUS)

JULY 1, 1985 THROUGH DEC. 31,1985

DOSE DUE TO RELEASE OF NOBLE GAS

WHOLE BODY DOSE (MREM)

	SECTOR	CRITICAL DISTANCE	CRITICAL	ORGAN	CRITICAL DOSE
THIRD QUARTER	N	980.(M)	NA	W BODY	6.55E-07
FOURTH QUARTER	N	0.(M)	NA	W BODY	0.00E-01
SEMIANNUAL TOTAL	N	980.(M)	NA	W BODY	6.55E-07

SKIN DOSES (MREM)

	CRITICAL SECTOR	CRITICAL DISTANCE	CRITICAL AGE	CRITICAL ORGAN	CRITICAL DOSE
THIRD QUARTER	N	980.(M)	NA	SKIN	1.84E-06
FOURTH QUARTER	N	0.(M)	NA	SKIN	0.00E-01
SEMIANNUAL TOTAL	N	980.(H)	NA	SKIN	1.84E-06

SEMIANNUAL MAXIMUM INDIVIDUAL DOSE TABLE (GASEOUS) JULY 1, 1985 THROUGH DEC. 31,1985

DOSE DUE TO I-131, H-3, AND PARTICULATES WITH HALFLIVES > 8 DAYS

WHOLE BODY DOSE (MREM)

	CRITICAL SECTOR	CRITICAL DISTANCE	CRITICAL AGE	CRITICAL ORGAN	CRITICAL DOSE
THIRD QUARTER	NNE	990.(M)	CHILD	W BODY	1.17E-03
FOURTH QUARTER	NNE	990.(H)	CHILD	W BODY	9.50E-04
SEMIANNUAL TOTAL	NNE	990.(H)	CHILD	W BODY	2.12E-03

SIGNIFICANT ORGAN DOSES (MREM)

	CRITICAL SECTOR	CRITICAL DISTANCE	CRITICAL AGE	CRITICAL ORGAN	CRITICAL DOSE
THIRD QUARTER	NNE	990.(M)	CHILD	THYROID	1.54E-03
FOURTH QUARTER	NNE	990.(M)	CHILD	THYROID	9.50E-04
SEMIANNUAL TOTAL	NNE	990.(M)	CHILD	THYROID	2.49E-03

SEMIANNUAL POPULATION DOSE TABLE (GASEOUS) JULY 1, 1985 THROUGH DEC. 31,1985

DOSE DUE TO RELEASE OF NOBLE GAS

	TOTAL IN EGRATED POPULATION DOSE (MANREM)	AVERAGE DOSE TO INDIVIDUALS IN POPULATION (MREM)
	WHOLE BODY	MHOLE BODY
THIRD QUARTER	6.53E-04	2.93E-07
FOURTH QUARTER	6.36E-08	2.86E-11
SEMIANNUAL TOTAL	6.53E-04	2.93E-07

3.61E-07

SEMIANNUAL POPULATION DOSE TABLE (GASEOUS)

JULY 1, 1985 THROUGH DEC. 31,1985

DOSE DUE TO I-131, H-3, AND PARTICULATES WITH HALFLIVES > 8 DAYS

TOTAL INTEGRATED	AVERAGE DOSE TO INDIVIDUALS
POPULATION DOSE (MANREM)	IN POPULATION (MREM)
WHOLE BODY	WHOLE BODY
9.86E-04	4.43E-07

SEMIANNUAL TOTAL 1.79E-03 8.04E-07

8.04E-04

THIRD QUARTER

FOURTH QUARTER

Table 5 Page 16

SEMIANNUAL POPULATION DOSE TABLE (LIQUID)

JULY 1, 1985 THROUGH DEC. 31,1985



	TOTAL INTEGRATED	AUFRACE POCE TO TURNING
	POPULATION DOSE (MANREM)	AVERAGE DOSE TO INDIVIDUALS IN POPULATION (MREM)
	WHOLE BODY	WHOLE BODY
THIRD QUARTER	5.05E-01	2.27E-04
FOURTH QUARTER	1.30E-01	5.84E-05
SEMIANNUAL TOTAL	6.35E-01	2.85E-04

SEMIANNUAL MAXIMUM INDIVIDUAL DOSE TABLE (LIQUID) JULY 1, 1985 THROUGH DEC. 31,1985

CRITICAL RECEPTOR : 0.6 MILES NW OF DISCHARGE

	WHOLE BODY	DOSES (MREM)	SIGNIFICAN	T ORGAN DO	SES (MREM)
	CRITICAL AGE	CRITICAL DOSE	CRITICAL AGE	CRITICAL ORGAN	CRITICAL DOSE
THIRD QUARTER	ADULT	1.50E-01	TEEN	LIVER	2.20E-01
FOURTH QUARTER	ADULT	1.48E-02	TEEN	LIVER	2.14E-02
SEMIANNUAL TOTAL	ADULT	1.65E-01	TEEN	LIVER	2.42E-01

Table 7

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

WIND SPEED (MPH)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: A ELEVATION: 35 FEET WIND DIRECTION 0.7- 3.5-3.4 7.4 N

7.5- 12.5- 18.5-12.4 18.4 24.4 >24.4 TOTAL NNE NE ENE E ESE SE SSE S SSW SW WSW WNW NW HHH VARIABLE TOTAL

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS

35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT) PERIOD OF RECORD: 7/01/85 TO 9/30/85 STABILITY CLASS: B ELEVATION: 35 FEET

WIND	33 1 21		HTND	COFED (ADU.		
DIRECTION	0.7- 3.4	3.5- 7.4	7.5- 12.4	12.5- 18.4	18.5-	>24.4	TOTAL
N	0	4	0	0	0	0	4
NNE	0	0	0	0	0	0	0
NE	0	0	0	1	0	0	1
ENE	0	0	7	1	0	0	8
Ε	0	0	9	0	0	0	9
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	1	0	0	0	1
SSW	0	0	3	1	0	0	4
SW	0	0	1	1	0	0	2
WSW	0	0	1	1	0	0	2
u	0	0	0	0	0	0	0
MMM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	4	22	5	0	0	31

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: C ELEVATION: 35 FEET

WIND DIRECTION	0.7-	3.5-	7.5-	SPEED (M 12.5- 18.4	18.5- 24.4	>24.4	TOTAL
N	0	0	1	2	0	0	3
NNE	0	3	3	0	0	0	6
NE	0	2	5	6	0	0	13
ENE	0	2	20	0	0	0	22
Ε	0	10	6	1	0	0	17
ESE	0	1	0	0	0	0	1
SE	0	0	0	0	0	0	0
SSE	0	1	0	0	0	0	1
S	0	3	3	0	0	0	6
SSW	0	3	17	1	0	0	21
SW	0	2	13	2	0	0	17
WSW	0	2	7	6	0	0	15
u	0	0	0	1	0	0	1
WNW	0	0	1	0	0	0	1
NW	0	1	0	0	0	0	1
NNW	0	1	4	1	0	0	6
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	31	80	20	0	0	131

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIODS OF CALM (HOURS): 0

TOTAL

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: E ELEVATION: 35 FEET

WIND DIRECTION	0.7-	3.5-		SPEED (M	PH) 18.5-		
DIRECTION	3.4	7.4	12.4		24.4	>24.4	TOTAL
N	8	0	0	0	0	0	8
NNE	1	2	0	2	0	0	5
NE	1	2	1	0	0	0	4
ENE	1	5	17	1	0	0	24
Ε	3	11	8	2	0	0	24
ESE	1	14	8	2	0	0	25
SE	8	39	5	0	0	0	52
SSE	12	39	1	0	0	0	52
S	16	37	6	0	0	0	59
SSW	4	66	42	4	0	0	116
SW	5	53	26	5	0	0	89
WSW	2	27	20	2	3	0	54
ч	4	34	22	0	0	0	60
MNM	1	5	14	0	0	0	20
NW	0	5	5	0	0	0	10
NNW	1	6	4	1	0	0	12
VARIABLE	0	0	0	0	0	0	0
TOTAL	68	345	179	19	3	0	614

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: G ELEVATION: 35 FEET

WIND DIRECTION	0.7-		WIND 7.5- 12.4	SPEED (M 12.5- 18.4	PH) 18.5- 24.4	>24.4	TOTAL
N	1	0	0				
				0	0	0	1
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	1	0	0	0	1
Ε	0	0	1	0	0	0	1
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	4	3	0	0	0	0	7
S	8	17	0	0	0	0	25
SSW	1	31	2	0	1	0	35
SW	3	7	3	4	0	0	17
wsw	3	7	1	0	0	0	11
W	1	6	1	0	0	0	8
MNM	0	3	0	0	0	0	3
NW	0	0	0	0	0	0	0
NNW	0	0	2	0	0	0	2
VARIABLE	0	0	0	0	0	0	0
TOTAL	21	74	11	4	1	0	111

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: TOTAL ELEVATION: 35 FEET

WIND				SPEED (M			
DIRECTION	0.7-	3.5-	7.5-	12.5-	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	13	23	38	14	0	0	88
NNE	3	31	41	34	4	0	113
NE	1	24	57	75	10	0	167
ENE	1	37	94	8	0	0	140
Ε	5	59	50	5	0	0	119
ESE	3	43	16	5	0	0	67
SE	11	52	11	0	0	0	74
SSE	31	89	9	1	0	0	130
S	53	110	30	1	0	0	194
SSW	18	176	125	12	1	0	332
SW	17	142	112	32	0	0	303
wsw	12	60	88	36	5	0	201
W	10	60	44	20	0	0	134
WNW	1	18	24	3	0	0	46
NW	1	15	14	3	0	0	33
NNW	1	16	30	5	0	0	52
VARIABLE	0	0	0	٥	٥	0	0
TOTAL	181	955	783	254	20	0	2193

PERIODS OF CALM (HOURS): 0

HOURS OF MISSING DATA: 15

Table 8

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: A ELEVATION: 250 FEET

WIND	200 1 20		HTND	SPEED (M	DUS		
DIRECTION	0.7-	3.5-	7.5-	12.5-	18.5-		
DIRECTION	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	1	0	1
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
w	0	0	0	0	0	0	0
MMM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	٥	0
TOTAL	0	0	0	0	1	0	1

DAVIS - BESSE

WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85 STABILITY CLASS: B ELEVATION: 250 FEET

PERIODS OF CALM (HOURS): 0

HIND

DIRECTION	0.7-	3.5-7.4	7.5- 12.4	SPEED (M 12.5- 18.4	PH) 18.5- 24.4	>24.4	TOTAL
N	0	4	0	0	0	0	4
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	1	4	0	0	5
Ε	0	0	6	7	0	0	13
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	1	0	0	
SSW	0	0	3	0	1	0	
SW	0	0	0	1	0	0	1
WSW	0	0	0	3	0	0	3
W	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	4	10	16	1	0	31
							O 1

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: C ELEVATION: 250 FEET

WIND			MIND	SPEED (M	PH)		
DIRECTION			7.5-	12.5-	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	0	0	3	0	0	3
NNE	0	2	3	0	0	0	5
NE	0	3	2	3	2	0	10
ENE	0	2	14	9	0	0	25
Ε	0	5	11	1	0	0	17
ESE	0	2	0	0	0	0	2
SE	0	0	0	0	0	0	0
SSE	0	1	0	0	0	0	1
S	0	0	1	1	1	2	5
SSW	0		2	14	2	0	22
SW	0	0	10	5	1	0	16
wsw	0	0	4	8	1	0	13
w	0	0	1	2	2	0	5
WNW	0	1	0	0	0	0	1
NW	0	1	0	0	0	0	1
NNW	0	0	4	1	0	0	5
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	21	52	47	9	2	131

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85 STABILITY CLASS: D

STABILITY CLASS: D ELEVATION: 250 FEET

UTHD.	250 FE						
DIRECTION	0.7-	3.5-	7.5-	SPEED (M	18.5-		
D11120112011	3.4	7.4				>24.4	TOTAL
N	0	13	29	30	1	0	73
NNE	2	20	32	24	13	. 0	91
NE	0	21	35	40	44	3	143
ENE	0	12	48	29	9	1	99
ε	1	17	20	16	4	0	58
ESE	1	17	23	6	1	2	50
SE	1	5	7	5	0	0	18
SSE	1	5	9	6	1	0	22
S	1	3	21	23	9	2	59
SSW	1	8	32	33	19	0	93
SW	0	11	24	49	18	0	102
wsw	2	6	34	51	23	2	118
w	1	4	12	20	12	0	49
WNW	0	3	6	7	5	0	21
NW	0	8	10	9	0	0	27
NNW	1	3	13	7	1	0	25
VARIABLE	0	0	0	0	0	0	0
TOTAL	12	156	355	355	160	10	1048
	The second second						

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: E ELEVATION: 250 FEET

DIRECTION	0.7-	3.5-	7.5- 12.4	SPEED (M 12.5- 18.4	PH) 18.5- 24.4	>24.4	TOTAL
N	0	4	4	0	1	0	9
NNE	0	3	0	1	1	0	5
NE	1	3	2	2	0	0	8
ENE	1	1	3	16	1	0	22
Ε	0	6	7	6	0	2	21
ESE	2	5	15	18	1	1	42
SE	0	8	17	24	0	0	49
SSE	0	8	9	13	0	0	30
S	0	1	15	36	15	1	68
SSW	0	1	13	53	12	4	83
SW	0	3	17	55	18	0	93
WSW	0	8	21	36	2	3	70
w	0	3	16	30	3	0	52
WNW	1	3	11	14	7	0	36
NW	0	2	5	8	1	0	16
NNW	0	1	3	5	0	0	9
VARIABLE	1	0	0	0	0	0	1
TOTAL	6	60	158	317	62	11	614

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: F ELEVATION: 250 FEET

WIND	250 FEE	1	MIND	SPEED (M	PH)		
DIRECTION		3.5-	7.5-	12.5-	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	1	1	1	0	0	0	3
NNE	0	0	0	0	0	0	0
NE	0	1	0	0	0	0	1
ENE	0	0	1	0	0	0	1
Ε	0	1	1	0	0	0	2
ESE	0	3	2	0	0	0	5
SE	2	10	5	0	0	0	17
SSE	0	2	11	10	2	0	25
S	0	4	4	29	14	0	51
SSW	0	2	5	27	6	0	40
SW	0	2	4	25	2	0	33
WSW	2	2	7	22	0	0	33
u	0	1	7	12	0	0	20
WNW	0	2	2	6	2	0	12
NW	0	2	3	4	0	0	9
NNW	0	1	1	0	0	0	2
VARIABLE	1	0	0	0	0	0	1
TOTAL	6	34	54	135	26	0	255

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: G ELEVATION: 250 FEET

WIND	250 FE		WIND	SPEED (M	IPH)		
DIRECTION			7.5-	12.5-	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	1	1	0	0	0	2
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	1	0	0	0	1
Ε	0	0	0	1	0	0	1
ESE	0	0	0	0	0	0	0
SE	0	4	3	0	0	0	7
SSE	0	3	0	5	0	0	8
S	0	1	2	6	0	0	9
SSW	0	0	2	21	8	0	31
SW	0	0	1	18	3	1	23
WSW	0	0	1	5	0	0	6
u	0	0	1	2	1	0	4
MNM	0	3	1	1	0	0	5
NW	0	5	1	4	0	0	10
NNW	0	0	4	0	0	0	4
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	17	18	63	12	1	111

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STALLLITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/01/85 TO 9/30/85

STABILITY CLASS: TOTAL ELEVATION: 250 FEET

DAIM				SPEED (M			
DIRECTION	3.4	7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	1	23	35	33	2	0	94
NNE	2	25	35	25	14	0	101
NE	1	28	39	45	46	3	162
ENE	1	15	68	58	10	1	153
Ε	1	29	45	31	4	2	112
ESE	3	27	40	24	2	3	99
SE	3	27	32	29	0	0	91
SSE	1	19	29	34	3	0	36
S	1	9	43	96	39	5	193
SSW	1	15	57	148	49	4	274
SW	0	16	56	153	42	1	268
wsw	4	16	67	125	26	5	243
W	1	8	37	66	18	0	130
WNU	1	12	20	28	14	0	75
NW	0	18	19	25	1	0	63
NNW	1	5	25	13	1	0	45
VARIABLE	2	0	0	0	0	0	2
TOTAL	24	292	647	933	271	24	2191

PERIODS OF CALM (HOURS): 0

HOURS OF MISSING DATA: 17

Table 9

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85 STABILITY CLASS: A ELEVATION: 35 FEET

WIND.	33 FE	- 1	HTHD	SPEED (M	(PH)		
DIRECTION	0.7-	3.5- 7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
W	0	0	0	٥	0	0	0
MNM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: B ELEVATION: 35 FEET

WIND DIRECTION	0.7-	3.5-	WIND 7.5- 12.4	SPEED (M 12.5- 18.4	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	2	0	0	2
ENE	0	0	0	0	0	0	0
Ε	0	0	1	0	0	0	1
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
w	0	0	0	0	0	0	0
WNW	0	0	0	0	1	0	1
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	1	2	1	0	4

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECURD: 10/01/85 TO 12/31/85 STABILITY CLASS: C ELEVATION: 35 FEET

WIND DIRECTION	0.7-	3.5-	7.5- 12.4	SPEED (M 12.5- 18.4	18.5- 24.4	>24.4	TOTAL
N	0	0	1	0	0	0	1
NNE	0	1	1	0	0	0	2
NE	0	0	0	3	0	0	3
ENE	0	1	3	0	0	0	4
Ε	0	0	3	2	0	0	5
ESE	0	0	1	0	0	0	1
SE	0	0	0	0	0	0	0
SSE	0	1	0	0	0	0	1
S	0	0	0	0	0	0	0
SSW	0	0	3	4	0	0	7
SW	0	0	0	1	0	0	1
WSW	0	0	6	3	2	1	12
w	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	1	0	0	0	0	1
NNW	0	0	2	0	0	0	2
VARIABLE	c	0	0	0	0	0	0
TOTAL	0	4	20	13	2	1	40

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: D ELEVATION: 35 FEET

FFEAMITON	. 35 12						
MIND				SPEED (M			
DIRECTION		3.5-	7.5-	12.5-	18.5-		
	3 . 4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	1	3	17	11	12	7	51
NNE	1	10	15	31	10	0	67
NE	1	11	37	60	27	1	137
ENE	0	14	12	35	16	0	77
Ε	1	13	34	39	5	0	92
ESE	4	18	26	14	0	0	62
SE	6	15	7	7	1	1	37
SSE	10	17	1	1	0	0	29
S	4	14	8	15	0	0	41
SSW	6	14	48	40	3	0	111
SW	2	13	45	80	37	12	189
wsw	0	17	74	67	48	18	224
W	0	19	35	23	7	0	84
WNW	1	11	16	27	2	0	57
NW	3	5	37	14	2	0	61
NNW	2	8	36	20	6	0	72
VARIABLE	0	0	0	0	0	0	0
TOTAL	42	202	448	484	176	39	1391

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: E ELEVATION: 35 FEET

LLETHIT DILL	00 1 1						
DIRECTION	0.7-	3.5- 7.4	7.5-	12.5- 18.4	18.5- 24.4	>24.4	TOTAL
N	0	4	2	0	0	0	6
NNE	0	1	0	0	0	0	1
NE	1	0	1	0	0	0	2
ENE	0	5	4	0	0	0	9
Ε	3	20	7	8	0	0	38
ESE	4	17	12	14	0	0	47
SE	6	15	6	0	0	0	27
SSE	9	21	5	0	0	0	35
S	4	23	13	9	1	0	50
SSW	8	36	50	11	5	0	110
SW	2	29	53	10	3	0	97
WSW	5	23	44	8	1	0	81
W	0	6	18	3	1	0	28
MNM	1	4	4	0	0	0	9
NW	1	2	5	1	0	0	9
NNW	0	5	4	0	0	0	9
VARIABLE	0	0	0	0	0	0	0
TOTAL	44	211	228	64	11	0	358

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85 STABILITY CLASS: F ELEVATION: 35 FEET

WIND DIRECTION	0.7-	3.5-	7.5-	SPEED (M	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	2	1	0	0	0	0	3
ESE	3	2	0	0	0	0	5
SE	4	8	2	0	1	0	15
SSE	10	14	0	0	0	0	24
S	7	13	1	0	0	0	21
SSW	1	20	1	0	0	0	22
SW	0	14	4	0	0	0	18
WSW	1	5	0	0	0	0	6
W	0	6	3	0	0	0	9
MNM	0	0	2	0	0	0	2
NW	1	0	1	0	0	0	2
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	٥	0
TOTAL	29	83	14	0	1	0	127

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: G ELEVATION: 35 FEET

WIND	33 121		HTND	SPEED (M	DHI		
DIRECTION	0.7-	3.5-	7.5-	12.5-	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	1	0	0	0	0	0	1
ESE	0	1	0	0	0	0	1
SE	0	0	0	0	0	0	0
SSE	1	2	1	0	0	0	4
S	0	0	0	0	0	0	0
SSW	0	11	0	0	0	0	11
SW	0	4	0	0	0	0	4
wsw	0	0	0	0	0	0	0
u	0	1	0	0	0	0	1
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	٥	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	2	19	1	0	0	0	22

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: TOTAL ELEVATION: 35 FEET

WIND	^ 7	7.0		SPEED (M				
DIRECTION	3.4	3.5- 7.4	7.5-	12.5-	18.5-	>24.4	TOTAL	
N	1	7	20	11	12	7	58	
NNE	1	12	16	31	10	0	70	
NE	2	11	38	65	27	1	144	
ENE	0	20	19	35	16	0	90	
E	7	34	45	49	5	0	140	
ESE	11	38	39	28	0	Ü	116	
SE	16	38	15	7	2	1	79	
SSE	30	55	7	1	0	0	93	
S	15	50	22	24	1	0	112	
SSW	15	81	102	55	8	0	261	
3 W	4	60	102	91	40	12	309	
WSW	6	45	124	78	51	19	323	
w	0	32	56	26	8	0	122	
WNW	2	15	22	27	3	0	69	
NW	5	8	43	15	2	0	73	
NNW	2	13	42	20	6	٥	83	
VARIABLE	0	0	0	0	0	0	0	
TOTAL	117	519	712	563	191	40	2142	

PERIODS OF CALM (HOURS): 0

HOURS OF MISSING DATA: 66

Table 10

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: A ELEVATION: 250 FEET

WIND			MIND	SPEED (M	PHI		
	0.7-	3.5- 7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
wsw	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
MNM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	٥

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: B ELEVATION: 250 FEET

WIND			WIND	SPEED (M			
DIRECTION	3.4	7.4	7.5-	12.5-	18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	1	1	0	2
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	1	0	0	0	1
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
wsw	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	1	1
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	1	1	1	1	4

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85 STABILITY CLASS: C

ELEVATIOM: 250 FEET

WIND	230 FE		HIND	SPEED (F	(PH)		
DIRECTION	0.7-	3.5-			18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	0	1	0	0	0	1
NNE	0	1	1	0	0	0	2
NE	0	0	0	0	2	0	2
ENE	0	0	3	2	0	0	5
Ε	0	0	2	0	2	0	4
ESE	0	0	2	0	0	0	2
SE	0	0	0	0	0	0	0
SSE	0	0	1	0	0	0	1
S	0	0	0	0	0	0	0
SSW	0	0	0	3	3	0	6
SW	0	0	0	2	0	0	2
WSW	0	0	0	6	1	1	8
w	0	0	0	1	2	1	4
WNW	0	٥	0	0	0	0	0
NW	0	1	0	0	0	0	1
NNW	0	0	2	0	0	0	2
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	2	12	14	10	2	40

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85 STABILITY CLASS: 5

ELEVATION: 250 FEET

HTHD			HERME	COFFO (M	DUN		
DIRECTION	0.7-	3.5-	7.5-	SPEED (M	18.5-		
DIRECTION	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	1	4	12	9	10	23	59
NNE	1	6	8	21	10	7	53
NE	2	8	27	50	42	5	134
ENE	0	6	11	15	33	21	86
Ε	2	7	10	15	37	22	93
ESE	1	5	13	25	21	3	68
SE	3	13	6	5	9	0	36
SSE	5	4	14	1	1	1	26
S	3	7	9	9	8	9	45
SSW	0	5	12	25	23	14	79
SW	0	7	6	53	38	23	127
WSW	1	5	17	71	81	80	255
W	1	8	17	43	28	17	114
WNW	1	4	27	21	18	5	76
NW	1	2	19	18	11	3	54
NNW	1	5	18	37	16	1	78
VARIABLE	0	0	0	0	0	0	0
TOTAL	23	96	226	418	386	234	1383

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: E ELEVATION: 250 FEET

WIND	230 FE		HTHE	CREED /	(DU)		
DIRECTION	0.7-	3.5-	7.5- 12.4	12.5- 18.4	18.5-	>24.4	TOTAL
N	0	0	3	4	1	0	8
NNE	0	0	1	0	0	0	1
NE	0	1	1	0	0	0	2
ENE	0	1	1	2	0	0	4
E	0	3	15	6	3	4	31
ESE	1	3	13	9	8	13	47
SE	1	6	6	8	2	1	24
SSE	1	1	10	9	2	0	23
S	1	2	7	23	14	6	53
SSW	1	5	9	29	31	14	89
SW	1	2	13	43	27	4	90
WSW	0	4	16	50	17	3	90
W	0	2	8	27	6	1	44
WNW	0	2	6	13	3	0	24
NU	0	1	2	6	3	0	12
NNW	0	1	2	5	0	0	8
VARIABLE	0	0	0	0	0	0	0
TOTAL	6	34	113	234	117	46	550

DAVIS - BESSE

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: F ELEVATION: 250 FEET

MIND			WIND	SPEED (M	IPH)		
DIRECTION	0.7-	3.5-	7.5-	12.5-	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	1	1	0	0	0	2
ENE	0	1	0	0	0	0	1
Ε	0	1	0	0	0	0	1
ESE	0	1	2	1	0	0	4
SE	0	1	5	5	1	1	13
SSE	0	0	2	7	2	0	11
S	0	1	2	14	4	1	22
SSW	1	1	5	9	3	0	19
SW	0	1	2	12	11	0	26
WSW	0	0	0	2	4	0	6
W	0	٥	2	5	0	0	7
WNW	0	0	2	5	0	0	7
NW	0	1	0	6	0	0	7
NNW	0	0	0	1	0	0	1
VARIABLE	0	0	0	0	0	0	0
TOTAL	1	9	23	67	25	2	127

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: G ELEVATION: 250 FEET

DIRECTION	0.7-	3.5-	WIND 7.5- 12.4	SPEED (% 12.5- 18.4	PH) 18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	1	0	1
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	1	0	0	0	0	1
ESE	0	0	0	0	0	0	0
SE	0	0	0	1	0	0	1
SSE	0	0	0	0	0	0	0
S	0	0	1	0	0	c	1
SSW	0	0	1	4	2	0	7
SW	0	0	0	5	0	0	5
WSW	0	0	0	1	1	0	2
u	0	0	2	1	0	0	3
WNW	0	0	0	0	0	0	0
NW	0	0	0	1	0	0	1
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	1	4	13	4	0	22

DAVIS - BESSE UNIT 1

JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/01/85 TO 12/31/85

STABILITY CLASS: TOTAL ELEVATION: 250 FEET

WIND DIRECTION	0.7-	3.5-	WIND 7.5- 12.4	SPEED (M 12.5- 18.4	PH) 18.5- 24.4	>24.4	TOTAL
N	1		16	13	11	23	68
NNE	1	7	10	21	11	7	57
NE	2	10	29	51	45	5	142
ENE	0	8	15	19	33	21	96
Ε	2	12	27	21	42	26	130
ESE	2	9	31	35	29	16	122
SE	4	20	17	19	12	2	74
SSE	6	5	27	17	5	1	61
S	4	10	19	46	26	16	121
SSW	2	11	27	70	62	28	200
SW	1	10	21	115	76	27	250
WSW	1	9	33	130	104	84	361
W	1	10	29	77	36	19	172
WNW	1	6	35	39	21	5	107
NW	1	5	21	31	14	4	76
NNW	1	6	22	43	16	1	89
VARIABLE	0	0	0	0	0	0	0
TOTAL	30	142	379	747	543	285	2126

PERIODS OF CALM (HOURS): 0

HOURS OF MISSING DATA: 82

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: A ELEVATION: 35 FEET

DIRECTION	0.7-	3.5-	7.5- 12.4		18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	1	0	0	0	1
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
ины	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	1	0	0	٥	1

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: B ELEVATION: 35 FEET

WIND			WIND	SPEED (M	PH)		
DIRECTION	0.7- 3.4	3.5- 7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
MMM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 vo 9/30/85

STABILITY CLASS: C ELEVATION: 35 FEET

WIND.	33 FE		HTMD				
DIRECTION	0.7-	3.5- 7.4	7.5-		18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	9	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SS'4	0	0	1	0	0	0	1
SW	0	0	0	1	0	0	1
WSW	0	0	0	0	0	٥	0
W	0	0	0	0	0	0	0
MNM	0	0	0	0	0	0	0
NW	0	1	0	0	0	0	1
NNW	0	0	0	0	٥	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	1	1	1	0	٥	3

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: D ELEVATION: 35 FEET

WIND DIRECTION	0.7-	3.5-	7.5- 12.4	SPEED (M 12.5- 18.4	18.5-	>24.4	TOTAL
N	0	1	0	0	0	0	1
NNE	0	3	0	0	0	0	3
NE	0	1	3	0	0	0	4
ENE	0	1	2	0	0	0	3
Ε	0	1	0	0	0	0	1
ESE	0	0	0	0	0	0	0
SE	0	2	0	0	0	0	2
SSE	0	1	1	0	0	0	2
S	0	0	0	0	0	0	0
SSW	0	3	9	1	0	0	13
SW	0	1	3	1	0	0	5
wsw	0	0	0	0	0	0	0
W	0	0	1	0	0	0	1
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
WNW	0	2	0	0	0	0	2
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	16	19	2	0	0	37

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: E ELEVATION: 35 FEET

ELEVALION.	33 FE	- 1	HTMD		DUL		
DIRECTION	0.7- 3.4	3.5- 7.4	7.5- 12.4	SPEED (M 12.5- 18.4	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	1	0	1	0	0	0	2
E	0	0	0	0	0	0	0
ESE	1	0	0	٥	0	0	1
SE	0	1	0	0	0	0	1
SSE	0	0	0	0	0	0	0
S	1	5	0	0	0	0	6
SSW	0	6	8	0	0	0	14
SW	0	1	3	0	0	0	4
WSW	0	0	0	0	0	0	0
w	1	1	0	0	0	0	2
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	4	14	12	0	0	0	30

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: F ELEVATION: 35 FEET

WIND			WIND	SPEED (M			
DIRECTION	3.4	7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	٥	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	1	0	0	0	0	1
SW	0	0	1	0	0	0	1
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	٥	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	1	1	0	0	0	2

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: G ELEVATION: 35 FEET

WIND	. 33		WIND	SPEED (M	(PH)		
DIRECTION	0.7-	3.5- 7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	1	2	0	1	0	4
SW	0	0	3	4	0	0	7
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	1	5	4	1	0	11

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: TOTAL ELEVATION: 35 FEET

MIND				SPEED (M			
DIRECTION	3.4	7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
						/24.4	TOTAL
N	0	1	0	0	0	0	1
NNE	0	3	0	0	0	0	3
NE	0	1	3	0	0	0	4
ENE	1	1	3	0	0	0	5
Ε	0	1	0	0	0	0	1
ESE	1	0	0	0	0	0	1
SE	0	3	0	0	0	0	3
SSE	٥	1	1	0	0	0	2
S	1	5	0	0	0	0	6
SSW	0	11	21	1	1	0	34
SW	0	2	10	6	0	0	18
wsw	0	0	0	0	0	0	0
W	1	1	1	0	0	0	3
UNU	0	0	0	0	0	0	0
NW	0	1	0	0	0	0	1
NNW	0	2	0	0	0	0	2
VARIABLE	0	0	0	0	0	0	0
TOTAL	. 4	33	39	7	1	0	84

PERIODS OF CALM (HOURS): 0

HOURS OF MISSING DATA: 3

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: A ELEVATION: 250 FEET

KIND.	230 FE		HIND	SPEED (M	PHI		
DIRECTION	3.4	3.5-7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
E	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	1	0	1
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
MMM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	1	0	1

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: B ELEVATION: 250 FEFT

WIND	. 250 12		HTM				
DIRECTION	0.7- 3.4	3.5- 7.4	7.5- 12.4	SPEED (M 12.5- 18.4		>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	٥	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	٥	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	٥	0	0	0

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: C ELEVATION: 250 FEET

WIND DIRECTION	^ 7		WIND	SPEED (M	PH)		
DIRECTION	3.4	7.4	7.5-	12.5-	18.5-		
			12.4	18.4	24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	1	0	1
SW	0	0	0	0	1	0	1
WSW	0	٥	0	0	0	0	0
W	0	0	0	0	0	0	0
MMM	0	0	0	0	0	0	0
NW	0	1	0	0	0	0	1
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	
TOTAL	0	1	0	0	2	0	0
					-	V	3

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: D ELEVATION: 250 FEET

WIND DIRECTION	0.7-	3.5-	WIND 7.5-	SPEED (H	PH) 18.5-		
DIRECTION	3.4	7.4	12.4		24.4	>24.4	TOTAL
N	0	1	0	0	0	0	1
NNE	0	1	0	0	0	0	1
NE	0	2	1	0	0	0	3
ENE	0	0	2	4	0	0	6
E	0	0	0	0	0	0	0
ESE	0	0	1	0	0	0	1
SE	0	1	1	0	0	0	2
SSE	0	0	1	1	0	0	2
S	0	0	0	0	1	0	1
SSW	0	0	1	7	2	0	10
SW	0	0	2	4	1	0	7
WSW	0	0	0	0	0	0	0
W	0	0	0	1	0	0	1
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	2	0	0	0	0	2
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	7	9	17	4	0	37

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: E ELEVATION: 250 FEET

WIND	200 121						
DIRECTION	0.7-	3.5- 7.4	7.5- 12.4	SPEED (M 12.5- 18.4	18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	٥	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	1	0	0	1
Ε	0	1	0	0	0	0	1
ESE	0	1	0	0	0	0	1
SE	0	2	0	0	0	0	2
SSE	0	0	0	0	0	0	0
S	0	0	0	1	0	0	1
SSW	0	0	2	10	4	0	16
SW	0	0	2	3	1	0	6
WSW	0	0	0	0	0	0	0
W	0	1	1	0	0	0	2
MMM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
HNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	٥	0
TOTAL	0	5	5	15	5	0	30

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85 STABILITY CLASS: F ELEVATION: 250 FEET

DIRECTION	0.7-	3.5-7.4	7.5- 12.4	SPEED (M 12.5- 18.4	PH) 18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
E	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	1	0	0	0	1
SW	0	0	0	0	1	0	1
WSW	0	0	0	0	0	0	0
u	0	0	0	c	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	1	0	1	0	. 2

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: G ELEVATION: 250 FEET

WIND DIRECTION	0.7-	3.5-	7.5-	SPEED (M	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	c	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	1	1	1	0	3
SW	0	0	1	3	3	1	8
wsw	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	2	4	4	1	11

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 7/1/85 to 9/30/85

STABILITY CLASS: TOTAL ELEVATION: 250 FEET

WIND DIRECTION	0.7-	3.5-	7.5- 12.4	SPEED (M 12.5- 18.4	PH) 18.5- 24.4	>24.4	TOTAL
N	0	1	0	0	0	0	1
NNE	0	1	0	0	0	0	1
NE	0	2	1	0	0	0	3
ENE	0	0	2	5	0	0	7
Ε	0	1	0	0	0	0	1
ESE	0	1	1	0	0	0	2
SE	0	3	1	0	0	0	4
SSE	0	С	1	1	0	0	2
S	0	0	0	1	1	0	2
SSW	0	0	5	18	9	0	32
SW	0	0	5	10	7	1	23
WSW	0	0	0	0	0	0	0
W	0	1	1	1	0	0	3
MNM	0	0	0	0	0	0	0
NW	0	1	0	0	0	0	1
иим	0	2	0	0	0	0	2
VARIABLE	0	o	0	0	0	0	0
TOTAL	0	13	17	36	17	1	84

PERIODS OF CALM (HOURS): 0

HOURS OF MISSING DATA: 3

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85 STABILITY CLASS: A ELEVATION: 35 FEET

WIND	35 FE	:1	HIND	SPEED (M	PH)		
DIRECTION	0.7-	3.5- 7.4	7.5-		18.5-	>24.4	TOTAL
N	0	٥	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
MMM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: B ELEVATION: 35 FEET

WIND			WIND	SPEED (M			
DIRECTION	3.4	7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
ш	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
мм	0	0	0	0	0	0	0
иим	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85 STABILITY CLASS: C

ELEVATION: 35 FEET

MIND	. 33 FE		HTME				
DIRECTION	0.7- 3.4	3.5- 7.4	7.5- 12.4	SPEED (M 12.5- 18.4	18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	٥	0	0

DAVIS - BESSE UNIT 1

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: D ELEVATION: 35 FEET

WIND				SPEED (M	PH)		
DIRECTION	3.4	3.5-	7.5-	12.5-	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	4	6	2	0	12
SW	0	0	3	11	0	0	14
WSW	0	0	2	5	0	0	7
W	0	0	1	0	0	0	1
MNM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
ини	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	10	22	2	0	34

DAVIS - BESSE UNIT 1

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: E ELEVATION: 35 FEET

WIND DIRECTION	0.7-	3.5-	7.5- 12.4	SPEED (M 12.5- 18.4	18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	c	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	2	1	0	0	3
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	٥	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	2	1	0	0	3

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: F ELEVATION: 35 FEET

WIND	. 35 FE	- 1	WIND	SPEED (M	PH)		
DIRECTION			7.5-	12.5-	18.5-		
	3.4	7.4	12.4	18.4	24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
E	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0

DAVIS - BESSE UNIT 1

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: G ELEVATION: 35 FEET

DIRECTION	0.7-	3.5-	7.5- 12.4	SPEED (M 12.5- 18.4	PH) 18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
E	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
MNM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 35-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85 STABILITY CLASS: TOTAL

ELEVATION: 35 FEET

. 55 FE		WIND	SPEED (M	(PH)		
0.7- 3.4	3.5- 7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	4	6	2	0	12
0	0	5	12	0	0	17
0	0	2	5	0	0	7
0	0	1	0	0	0	1
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	12	23	2	0	37
	0.7-3.4	0.7- 3.4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.7- 3.5- 7.5- 7.5- 3.4 7.4 12.4 0	WIND SPEED (N 7.5- 12.5- 12.5- 12.4	WIND SPEED (MPH) 7.5- 12.5- 18.5- 3.4 7.4 12.4 18.4 24.4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WIND SPEED (MPH) 7.5- 12.5- 18.5- 12.4 18.4 24.4 >24.4 >24.4

PERIODS OF CALM (HOURS): 0

HOURS OF MISSING DATA: 0

DAVIS - BESSE UNIT 1

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: A ELEVATION: 250 FEET

WIND DIRECTION	0.7-	3.5-		SPEED (M 12.5- 18.4	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
E	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
s	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
wsw	0	0	0	0	0	0	0
u	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	c
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85 STABILITY CLASS: B

ELEVATION: 250 FEET HIND

DIRECTION	0.7-	3.5-	7.5- 12.4	SPEED (M 12.5- 18.4	18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0		
ENE	0	0	0	0	0	0	0
E	0	0	0	0	0	0	0
ESE	0	0	0	0	0		0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0		0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0		0	0	0
WSW	0	0		0	0	0	0
W			0	0	0	0	0
	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	
TOTAL	0	0	0	0	0	0	0
PERTONS OF S				7	*	0	0

DAVIS - BESSE UNIT 1

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: C ELEVATION: 250 FEET

WIND	230 FEE		MIND	SPEED (M	PH)		
DIRECTION	0.7- 3.4	3.5- 7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
E	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
wsw	0	0	0	0	0	0	0
W	0	0	0	0	0	0	0
MNM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: D ELEVATION: 250 FEET

WIND				SPEED (M			
DIRECTION	3.4	7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	3	4	7
SW	0	0	0	4	4	3	11
WSW	0	0	0	5	7	0	12
W	0	0	0	2	2	0	4
MMM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
иим	0	0	0	0		0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	c	0	11	16	7	34

DAVIS - BESSE UNIT:

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85 STABILITY CLASS: E

ELEVATION: 250 FEET

	. 200 121	- '					
DIRECTION	0.7- 3.4	3.5- 7.4	7.5- 12.4	SPEED (M 12.5- 18.4	18.5- 24.4	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
wsw	0	0	0	0	3	0	3
u	0	0	0	0	0	0	0
MMM	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
ним	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	3	0	3

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/21/85 STABILITY CLASS: F

ELEVATION: 250 FEET

		WIND	SPEED (M	PH)		
0.7- 3.4	3.5- 7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
0	0	0	0	0	. 0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	0	0	0
0	0	0	0	٥	0	0
0	0	0	0	0	0	0
	0.7-3.4	3.4 7.4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.7- 3.5- 7.5- 7.5- 3.4 7.4 12.4 0	WIND SPEED (N 7.5- 12.5- 12.4 18.4 0	WIND SPEED (MPH) 7.5- 12.5- 18.5- 12.4 18.4 24.4	WIND SPEED (MPH) 7.5- 12.5- 18.5- 12.4 18.4 24.4 >24.4 >24.4

DAVIS - BESSE UNIT 1

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: G ELEVATION: 250 FEET

WIND	230 FE	• •	WIND	SPEED (M	IPH)		
DIRECTION	0.7-	3.5- 7.4	7.5-	12.5-		>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	0	0	0
SW	0	0	0	0	0	0	0
WSW	0	0	0	0	0	0	0
u	0	0	0	0	0	0	0
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0

DAVIS - BESSE

BATCH RELEASE JOINT FREQUENCY DISTRIBUTION WIND SPEED AND DIRECTION BY ATMOSPHERIC STABILITY CLASS 250-FT WINDS AND DELTA TEMPERATURE (250FT-35FT)

PERIOD OF RECORD: 10/1/85 to 12/31/85

STABILITY CLASS: TOTAL ELEVATION: 250 FEET

WIND	250 FE	E1	MIND	SPEED (M	IPH)		
DIRECTION	0.7- 3.4	3.5- 7.4	7.5-	12.5-	18.5-	>24.4	TOTAL
N	0	0	0	0	0	0	0
NNE	0	0	0	0	0	0	0
NE	0	0	0	0	0	0	0
ENE	0	0	0	0	0	0	0
Ε	0	0	0	0	0	0	0
ESE	0	0	0	0	0	0	0
SE	0	0	0	0	0	0	0
SSE	0	0	0	0	0	0	0
S	0	0	0	0	0	0	0
SSW	0	0	0	0	3	4	7
SW	0	0	0	4	4	3	11
WSW	0	0	0	5	10	0	15
W	0	0	0	2	2	0	4
WNW	0	0	0	0	0	0	0
NW	0	0	0	0	0	0	0
NNW	0	0	0	0	0	0	0
VARIABLE	0	0	0	0	0	0	0
TOTAL	0	0	0	11	19	7	37

PERIODS OF CALM (HOURS): 0

HOURS OF MISSING DATA: 0

TABLE 15 HOURLY METEOROLOGICAL DATA DURING BATCH RELEASES DAVIS-BESSE NUCLEAR POWER STATION

JULY 1, 1985 - SEPTEMBER 30, 1985

YR	HONTH	DAY	HOUR	35' WIND SPD	35' WIND DIRECTION	T 250'-35'
85	7	1	1	10.7	69	-0.6
85	7	1	2	10.9	64	-0.7
85	7	1	3	9.6	59	-0.7
85	7	1	4	9.1	51	-0.8
85	7	1	5	8.2	54	-0.7
85	7	1	6	7.4	58	-0.8
85	7	1	7	7.1	51	-1.1
85	7	1	8	8.0	36	-1.3
85	7	1	9	6.0	33	-1.3
85	7	1	10	6.2	31	-1.3
85	7	1	11	4.0	17	-1.1
85	7	1	12	5.5	340	-1.3
85	7	1	13	4.9	326	-1.4
85	7	1	14	4.8	314	-1.9
85	7	1	15	6.5	353	-1.8
35	7	1	16	6.7	94	-1.
85	7	1	17	5.9	140	-0.
85	7	1	18	4.3	129	-0.3
85	7	1	19	3.6	114	-0.4
85	7	1	20	1.8	75	. 2
85	7	1	21	4.4	133	-0.8
85	7	1	22	2.6	179	0.3
85	7	4	10	6.9	202	-1.7
85	7	4	11	8.6	219	-1.4
85	7	4	12	11.7	221	0.5
85	7	4	13	13.5	229	1.5
85	7	4	14	12.4	227	2.4
85	7	4	15	11.6	203	1.3
85	7	4	16	13.6	216	-0.3
85	7	4	17	13.9	214	3.2
85	7	4	18	13.6	216	2.3
85	7	4	19	10.5	204	0.2
85	7	4	20	10.4	200	-0.4
85	7	4	21	8.3 7.7	197	0.3
85	7	4	22	7.7	198	0.4
85	7	4	23	6.4	195	0.6
85	7 7 7 7 7 7 7	4	24	6.4	181	0.6
85	7	5		8.0	193	0.2
85	7	5	1 2 3	9.5	201 194	-0.4
85	7	5	3	7.6	194	-0.2
85	7	5	4	8.6	195	-0.1
85	7	555555	5	10.5	204	-0.0
85	7	5	6	10.4	224	-0.

TABLE 15 Continued

HOURLY METEOROLOGICAL DATA DURING BATCH RELEASES

DAVIS-BESSE NUCLEAR POWER STATION

JULY 1, 1985 - SEPTEMBER 30, 1985

YR	MONTH	DAY	HOUR	35' WIND SPD	35' WIND DIRECTION	T 250' - 35'
85	7	5	7	3.6	269	-0.2
85	7	5	8	4.0	198	-0.6
85	7	5	9	6.6	143	-1.4
85	7	5	10	8.9	162	-1.5
85	7	5	11	10.9	194	-1.7
85	7	5	12	15.1	212	-1.6
85	7	5	13	16.7	216	-1.8
85	7	5	14	****	***	****
85	7	5	15	****	***	****
85	7	5	16	8.9	318	-1.3
85	7	5	17	19.4	39	****
85	7	5	18	****	***	****
85	7	5	19	****	***	****
85	7	5	20	****	***	****
85	7	5	21	10.6	203	-2.5
85	7	5	22	10.5	207	-0.8
85	7	5	23	9.1	210	-1.0
85	7	5	24	7.1	200	-0.7
85	7	6	1	6.3	215	-0.7
85	8	6	9	11.8	197	-1.4
85	8	6	10	13.9	198	-1.7
85	8	6	11	12.9	200	-1.8
85	8	6	12	11.6	204	-1.3
85	8	6	13	9.8	206	-1.0
85	8	6	14	9.9	206	-1.2
85	8	6	15	11.2	210	-1.3
85	8	6	16	9.7	213	-1.3
85	8	6	17	7.2	212	-1.2
85	8	6	18	7.8	209	-1.1
85	8	6	19	7.8	216	-0.6
85	8	6	20	11.8	220	-0.3
85	8	6	21	8.4	216	2.0
85	8	6	22	6.1	196	0.9
85	8	6	23	4.0	185	0.1
85		6	24	4.0	186	1.5
85	8	6 7	1	4.8	187	1.6
85	8	7	2	5.4	198	0.8
85	8	7	3	7.2	201	-0.1
85	8	7	4	6.0	222	0.0
85	8	7	5	5.6	202	-0.1
85	8 8 8 8 8 8 8	7	6	6.8	262	-0.1
85	9	28	17	10.1	249	-1.3
85	9	28	18	8.6	240	-0.7
85	9	28	19	6.5	236	0.6

*** Indicates unavailable data

TABLE 16

HOURLY METEOROLOGICAL DATA DURING BATCH RELEASES

DAVIS-BESSE NUCLEAR POWER STATION

OCTOBER 1, 1985 - DECEMBER 31, 1985

YR	MONTH	DAY	HOUR	35' WIND SPD	35' WIND	T 250'-35'
				(MPH)	DIRECTION	(F)
85	12	21	15	15.4	229	-1.4
85	12	21	16	15.4	232	-1.2
85	12	21	17	12.7	227	-0.9
85	12	21	18	11.6	225	-0.6
85	12	21	19	12.6	226	-0.5
85	12	21	20	12.3	224	-0.1
85	12	21	21	10.8	225	0.1
85	12	21	22	10.5	224	-0.7
85	12	21	23	12.6	226	-0.8
85	12	21	24	13.2	228	-0.8
85	12	22	1	12.1	218	-1.1
85	12	22	2	11.6	210	-1.0
85	12	22	3	12.3	209	
85	12	22	4	12.2		-1.1
85	12	22	5	12.4	208 198	-1.1
85	12	22	6	13.4		-1.1
85	12	22	7		195	-1.
85	12	22	8	14.0	192	-1
85	12	22	9	15.2	196	-1.0
85	12		10	16.1	193	-1.0
85	12	22		18.0	194	-1.0
		22	11	17.8	203	-1.0
85	12	22	12	20.0	210	-1.0
85	12	22	13	19.0	213	-1.0
85	12	22	14	17.7	217	-0.9
85	12	22	15	17.8	224	-0.9
85	12	22	16	16.6	226	-0.9
85	12	22	17	17.8	231	-0.9
85	12	22	18	15.4	226	-0.9
85	12	22	19	16.4	229	-0.8
85	12	22	20	17.2	237	-0.7
85	12	22	21	17.9	248	-0.8
85	12	22	22	13.5	253	-0.8
85	12	22	23	11.4	249	-0.8
85	12	22	24	11.9	252	-0.8
85	12	23	1	13.3	248	-0.8
85	12	23	2	13.6	252	-0.8
85	12	23	3	11.1	260	-0.8

THE TOLEDO EDISON COMPANY DAVIS-BESSE NUCLEAR POWER STATION OFFSITE DOSE CALCULATIONS MANUAL

Revision No.	Station Review Board	Date
0	Stepren m Jeanney	2/21/34
1	D. W. Briden	8/29/85

OFFSITE DOSE CALCULATION MANUAL
FOR
DAVIS-BESSE NUCLEAR POWER STATION
March 1984

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INTRODUCTION

This OFFSITE DOSE CALCULATION MANUAL (ODCM) describes the methodology and parameters to be used in the calculation of offsite doses due to radioactive liquid and gaseous effluents and in the calculation of liquid and gaseous effluent monitoring instrumentation alarm/trip setpoints. The ODCM also contains a list and graphic description of the specific sample locations for the radiological environmental monitoring program.

The ODCM will be maintained at the Station for use as a reference guide and training document of accepted methodologies and calculations. Changes in the calculational methods or parameters will be incorporated into the ODCM in order to assure that the ODCM represents the present methodology in all applicable areas.

The methodology stated in this manual is acceptable for use in demonstrating compliance with 10 CFR Part 20.106, 10 CFR Part 50 Appendix I, and 40 CFR Part 190. Only the dose attributable to the Davis-Besse Nuclear Power Station is considered in demonstrating compliance with 40 CFR Part 190.

More conservative calculation methods and/or conditions (e.g., location and/or exposure pathways expected to yield higher computed doses) than appropriate for the maximally exposed person may be assumed in the dose evaluations.

For the calculation of individual doses from gaseous effluents, the receptor is selected on the basis of applicable exposure pathways identified in the land use census. Methodologies and pathways considered in NUREG-0133 are consistent with those in the ODCM.

For liquid releases, doses are evaluated for the drinking water and freshwater fish pathways. In the Great Lakes region, invertebrates do not constitute a direct ingestion pathway to man.

1.0 LIQUID EFFLUENTS

1.1 Liquid Effluent Monitor Setpoints

1.1.1 Liquid Radwaste Effluent Line Monitors

Liquid Radwaste Effluent Line Monitors provide alarm and automatic termination of release prior to exceeding the concentration limits specified in 10 CFR Part 20, Appendix B, Table II, Column 2 at the release point to the unrestricted area. To meet this specification, the alarm/trip setpoints for liquid effluent monitors and flow measurement devices are set to assure that the following equation is satisfied:

$$\frac{\text{cf}}{\text{F+f}} \leq C,$$
 (1-1)

where:

- C = the effluent concentration limit (RETS, section 3.11.1) implementing 10 CFR Part 20.106 for the site, in µCi/ml
- c = the setpoint, in μCi/ml, of the radioactivity monitor measuring the radioactivity concentration in the effluent line prior to dilution and subsequent release; the setpoint, which is proportional to the volumetric flow of the effluent line and inversely proportional to the volumetric flow of the dilution stream plus the effluent stream, represents a value which, if exceeded, would result in concentrations exceeding the limits of 10 CFR Part 20.106 in the unrestricted area
- f = the flow setpoint as measured at the radiation monitor location, in volume per unit time, but in the same units as F, below

F = the dilution water flow setpoint as measured prior to the release point in volume per unit time.

At Davis-Besse Unit 1, the available dilution water flow (F) is constant for a given release, and the waste tank flow (f) and monitor setpoint (c) are set to meet the condition of Equation 1-1 for a given effluent concentration, C. The method by which this is accomplished is as follows:

The isotopic concentration for a waste tank to be released is determined by the analyses required in RETS Table 4.11-1. The ratio of the concentration to the unrestricted area MPC (10 CFR Part 20, Appendix B, Table II, Column 2) is calculated with the equation:

$$FMPC = \sum_{i}^{C} \frac{g_{i}}{MPC_{i}}$$
 (1-2)

where:

FMPC = fraction of the unrestricted area MPC

Cg = concentration of each radionuclide i measured
in each tank prior to release (µCi/ml)

MPC₁ = unrestricted area MPC for each radionuclide i from 10 CFR Part 20, Appendix B, Table II, Column 2. For dissolved and entrained noble gases a value of 2 x 10⁻⁴ μCi/ml shall be used. The total or gross beta or gamma activity alone may be used to conservatively determine the MPC fraction by the equation:

$$FMPC = \frac{C_{t}}{1 \times 10^{-7}}$$
 (1-3)

Where:

Ct = the total or gross beta or gamma activity

- The MPC fraction (FMPC) as determined for each batch used to calculate a Dilution Factor, D.F., which is the ratio of total dilution flow rate to tank flow rate required to assure that the limiting concentration of 10 CFR Part 20, Appendix B, Table II, Column 2 are met at the point of discharge.

$$D.F. = \frac{FMPC}{S.F.} \tag{1-4}$$

where:

- D.F. = dilution factor
- S.F. = an administrative safety factor normally applied at Davis-Besse which causes the calculated Dilution Factor to be 3.33 times larger than the dilution factor required for compliance with 10 CFR Part 20 limits.

3) The maximum permissible waste tank flow rate, f_d, is calculated based on a fixed dilution flow rate, F_d:

$$f_d = \frac{F_d + f_d}{D.F.} \cong \frac{F_d}{D.F.}$$
 for $f_d >> f_d$ (1-5)

where:

F_d = 0.9 x (dilution flow rate), as readout in control room

f = maximum permissible waste tank flow rate

D.F. = Dilution Factor from Step 2.

NOTE that the equation is valid only for D.F. >1; for D.F. \leq 1, the waste tank concentration meets the limits of 10 CFR Part 20 without dilution, and f_d may take on any desired value.

4) The minimum dilution flow (F), and waste tank maximum flow rate setpoint (f) are calculated as follows:

 $F = F_d = 0.9 \times \text{actual dilution flow rate as observed}$ from the control room readout,

 $f = 0.9 \times f_d = 0.9$ calculated maximum waste tank flow rate for the stated release conditions.

A control room alarm occurs if the dilution flow rate falls below the preset flow rate, or if the tank flow rate exceeds 0.9 of the preset flow rate, and the release is terminated.

The monitor setpoint may now be specified based on the values of F, and f which were specified to assure that releases are maintained below the concentrations of 10 CFR Part 20, Appendix B, Table II, Column 2. The monitor setpoint in counts per minute (cpm) is taken from the monitor calibration graph (e.g., Figure 1) to correspond to three times the concentration in the batch.

S.P. = the monitor setpoint obtained from the calibration curve for the monitor (cpm)

A = total radioactivity concentration in the batch

$$A = \sum_{i} C_{g_{i}}$$

or, if based on gross or total beta or gamma analysis,

$$A = C_t$$

Normally, only one liquid release is conducted at a time. If more than one release of radioactive effluents is conducted simultaneously, the setpoints for the individual radiation monitors for the combined releases will be set to prevent exceeding the concentrations of 10 CFR Part 20, Appendix B, Table II, Column 2 in the environment.

NOTE that the setpoint contains a factor of conservatism, even if the calculated setpoint tank flow rate is attained, since the calculated rate contains the factors as shown:

In practice, the actual tank flow rate normally is many times less than the calculated tank flow rate, thus providing an additional safety factor during a release.

1.1.2 Turbine Building (Floor Drains) Sump Effluent Line (Applicable upon completion of modification)

The purpose of the monitor for the turbine building sump effluent line (or Unit Storm Sewer Outlet) is to detect abnormal radionuclide concentrations in the sump effluent system. Because the only sources to the sump effluent system are from the secondary steam system, activity is expected in the turbine building sump effluent system only if a significant primary-to-secondary leak is present. If a primary-to-secondary leak is present, the activity in the sump effluent system would be comprised of only those radionuclides found in the secondary system, but with reduced activity from decay and dilution.

Until activity is measured in the secondary system, it will not be practical to select radionuclides on which to calculate the setpoint of the inline monitor. The monitor is, therefore, operated normally as a gross gamma detector at the lowest practical activity level to prevent false alarms. The lowest practical level has been determined to be three times the background count rate of the monitor when filled with clean water.

When activity above the level specified in RETS Table 4.11-1 is detected in the secondary system, the principal nuclide or nuclides comprising a major fraction of the activity in the secondary system condensate will be identified by gamma ray spectroscopy in the laboratory. The monitor setpoint will then be determined as follows:

The isotopic concentration for the turbine building sump effluent is determined by the sampling and analytical requirements per RETS Table 4.11-1 (only required when secondary system concentration exceeds 10⁻⁵ μCi/ml). The ratio of the concentration to the unrestricted area MPC is calculated with the equation:

$$FMPC = \sum_{i}^{C} \frac{g_{i}}{MPC_{i}}$$
 (1-7)

Where:

FMPC = fraction of the unrestricted area MPC

Gg = concentration of each radionuclide i measured
in each grab sample

MPC_i = unrestricted area MPC for each radionuclide i from 10 CFR Part 20, Appendix B, Table II, Column 2. For dissolved and entrained gases, a value of 2x10⁻⁴ μCi/ml shall be used.

If based on gross or total beta or gamma analysis, the unrestricted area MPC fraction is simply:

$$FMPC = \frac{C_{t}}{1 \times 10^{-7}}$$
 (1-8)

Ct = the total or gross beta or gamma activity

- 1x10⁻⁷ = MFC value for an unidentified mixture of radionuclides (from footnote 3.b to 10 CFR Part 20,-Appendix B).
- 2) The actual dilution factor from fixed flow rates of the turbine building sump effluent flow rate and dilution flow rate is as follows:

actual dilution factor =
$$\frac{f + F}{f}$$

where:

F = dilution flow rate (gpm)

3) The concentration in the turbine building sump which corresponds to an unrestricted area MPC value after dilution is calculated from the previously defined quantities, and is:

$$c = \frac{A}{FMPC} * \frac{f + F}{f}$$
 (1-9)

where:

- c = concentration corresponding to the unrestricted area MPC value after dilution
- A = total radioactivity concentration (μCi/ml)

$$A = \sum_{i} C_{g_{i}}$$

or, if based on total or gross beta or gamma analysis,

The calibration curve for the monitor (e.g., Figure 1) is then used to determine the count rate (cpm) corresponding to the radionuclide concentration (c). The monitor setpoint is the sum of the calculated count rate plus the observed background count rate of the monitor.

To simplify the determination of setpoint or in the event that the concentration of radioactive material in the sample from the turbine building sump is below measurable levels (<u>i.e.</u>, less than 5 x 10^{-7} μ Ci/ml for principal gamma emitters), the value of 1 x 10^{-7} μ Ci/ml may be substituted for the factor $\frac{A}{FMPC}$ (<u>i.e.</u>, $\frac{A}{FMPC}$ = 1 x 10^{-7}).

It may conservatively be assumed that the radionuclide concentrations in the secondary system are identical to those in the turbine building sump. Therefore, the results of the sampling and analysis of the secondary system may be used in conservatively determining the values of FMPC and c, above.

1.2 Dose Calculation for Liquid Effluents

Technical Specification 4.11.1.2.1 requires that an assessment be performed at least once every 31 days in any quarter in which radio-active effluent is discharged to determine whether the dose or dose commitment to a person offsite due to radioactive material released in liquid effluent calculated on a cumulative basis exceeds Specification 3.11.1.2. The requirement is satisfied by computing the accumulated dose commitment to the most exposed organ and to the total body of a hypothetical person exposed by eating fish and drinking water taken from Lake Erie.

The dose contribution from all radionuclides identified in liquid effluents released to unrestricted areas is calculated using the following expressions:

$$D_{\tau} = \sum_{i} A_{i\tau} \begin{vmatrix} m \\ \sum_{\ell=1}^{m} \Delta t_{\ell} & C_{i\ell} & F_{\ell} \end{vmatrix}$$

where:

D_T = dose or dose commitment to organ t, including total body (mrem).

 $A_{i\tau} = K_{o} \begin{bmatrix} \frac{U_{w}}{D_{w}} + U_{F} & BF_{i} \end{bmatrix}$ DF_i, the site-related ingestion does commitment factor from radionuclide i $(\frac{mrem/hr}{\mu Ci/ml})$ (from Table 3 of Appendix B).

 Δt_{ℓ} = length of the ℓ^{th} time period over which $C_{i\ell}$ and F_{ℓ} are averaged for all liquid releases, in hours.

 $^{\text{C}}$ i2 = average concentration of radionuclide i observed in undiluted liquid effluent during time period Δt_{χ} from any liquid release, in $\mu\text{Ci/ml}$. Concentrations are determined

primarily from a gamma isotopic analysis of a liquid effluent sample. For Fe-55, Sr-89, Sr-90, and H-3, the last measured value will be used in dose calculations.

- near-field average dilution factor for C during any liquid effluent release. Defined as the ratio of the average undiluted liquid waste flow during release to the product of the average flow from the site discharge structure to unrestricted receiving waters times the near-field dilution factor of 10 times the collection box factor of 1.0 (Ref. 2).
- F₂ = average undiluted liquid waste flow average flow from the site discharge x 10 x 1.0
- K = units conversion factor 1.14 x 103

$$(10^6 \frac{\text{oCi}}{\mu\text{Ci}} \times 10^3 \frac{\text{ml}}{\text{liter}} \div 8,760 \frac{\text{hr}}{\text{yr}})$$

- U = adult water consumption (730 licers/yr) (Ref. 3)
- D_w = dilution factor from the near-field area within one-quarter mile of the release point to the potable water intake for adult water consumption. D_w is (57/(10 x 1.0)) = 5.7, where 57 = lowest dilution factor corresponding to beach wells located approximately 966 m NW of the discharge point (Ref. 2). The near-field dilution factor of 10, represents the mixing effect of the discharge structure (Ref. 2).
- $U_{\overline{F}}$ = adult fish consumption (21 kg/yr) (Ref. 3).
- BF = bioaccumulation factor for nuclide, i, in fish, in pCi/kg per pCi/liter from Table 1 of Appendix B (taken from Reference 3, Table A-1).

DF_i = dose conversion factor for nuclide, i, for adults in preselected organ, t, in mrem/pCi, from Table 2 of Appendix B (taken from Reference 3, Table E-11).

1.3 Projected Personal Maximum Dose For Liquid Effluents

The dose commitment to a person offsite due to radioactive material released in liquid effluent may be projected by calculating the extrapolated total body and most exposed organ dose commitments to a hypothetical person exposed by eating fish and drinking water. The potential dose commitments to organs and to the total body are computed separately.

The dose commitment to a maximally exposed hypothetical person will be projected by calculating the doses accumulated during the most recent three months according to the method described in Section 1.2 and by assuming that the result represents the projected doses during the current month or quarter

Alternatively, the 31 day dose commitment may be projected by using the equation:

$$P_{\tau} = \frac{\tau}{X} D_{\tau} \tag{1-11}$$

where:

P_T = projected dose commitment (mrem) to organ t (including total body) for the current quarter

T = number of days in the projected time period (i.e. 31 days 91 days).

X = number of days to date in current quarter

D_T = accumulated personal dose to data during the current quarter via radioactive material in liquid effluent (mrem). 1

1.4 REFERENCES TO 1.0 LIQUID EFFLUENTS

- 1.4.1 J.S. Boegli, W.L. Britz, R.R. Bellamy, and R.L. Waterfield. 1978. "Preparation of Radiological Effluent Technical Specifications for Nuclear Power Plants," NUREG-0133, Office of Nuclear Reactor Regulation, U.S. Nuclear Regulatory Commission.
- 1.4.2 D.W. McDougall. 1980. "Aquatic Dilution Factors within 50 miles of the Davis-Besse Unit 1 Nuclear Power Plant."Stone & Webster Engineering Corporation.
- 1.4.3 United States Nuclear Regulatory Commission. 1977.

 "Calculation of Annual Dose to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10CFR50, Appendix I," Regulatory Guide 1.109, Revision 1.

2.0 GASEOUS EFFLUENTS

2.1 Gaseous Effluent Monitor Setpoints

.1.1 Station Vent Monitor

The station vent is the only normal radioactive gaseous release point.

For the purpose of implementation of section 3.3.3.10 ofthe RETS, the alarm setpoint level for the station vent noble gas monitor will be calculated as follows:

$$S_{v}$$
 = the lesser of 0.5 (R_{t}) 500 or (2-1) 0.5 (R_{s}) 3000

Where:

S_v = count rate of station vent noble gas monitor at alarm setpoint level (cpm)

0.5 = safety factor allowing 100% margin for cumulative uncertainties of measurements (dimensionless)

R_t = count rate per mrem/yr to the total body

R = count rate per mrem/yr to the skin.

The values of $\mathbf{R}_{\mathbf{t}}$ and $\mathbf{R}_{\mathbf{s}}$ are dependent on the radionuclide distribution and are derived by the equations:

$$R_{t} = C + \left[\overline{\chi/Q}_{NG} \sum_{i} K_{i} (\dot{Q}_{i}) \right] \qquad (2-2)$$

$$R_{s} = C \div [(\overline{\chi/Q}_{NG}) \Sigma (L_{i} + 1.1 M_{i}) \dot{Q}_{i}] \qquad (2-3)$$

where:

- C = count rate of the station vent monitor corresponding to grab sample radionuclide concentrations (cpm)
- χ/Q = highest sector annual average atmospheric dis-NG persion at the unrestricted area boundary
 - = $1.83 \times 10^{-6} \sec/m^3$ in the north-northeast sector
- K_i = total body dose factor due to gamma emissions from isotope i (mrem/yr per μCi/m³) from Table 4 of Appendix B
- Q
 i = rate of release of each noble gas radionuclide i
 identified by the sampling and analysis per RETS
 Table 4.11-2 (μCi/sec)
- L_i = skin dose factor due to beta emissions from isotope i 'mrem/yr per $\mu Ci/m^3$ ') from Table 4 of Appendix B
- 1.1 = mrem skin dose per mrad air dose
- M_i = air dose factor due to gamma emissions from isotope i (mrad/yr per μCi/m³) from Table 4 of Appendix B.

A more conservative setpoint may be calculated to minimize requirements for adjustment of the monitor by using the equations:

$$R'_{t} = C' \div \left[\left(\overline{\chi/Q}_{NG} \right) K \right] \tag{2-4}$$

$$R'_{\alpha} = C' \div [(\overline{\chi/Q}_{NG})(L + 1.1M)]$$
 (2-5)

where:

R'_t = conservative count rate per mrem/yr to the total body (Xe-133 detection, Kr-89 dose)

C' = count rate of station vent monitor for an effluent concentration of Xe-133 corresponding to 1.0 μCi/sec release rate of Xe-133 (cpm)

K = total body dose factor for Kr-89, from Table 4 of Appendix B

L = skin dose factor for Kr-89, from Table 4 of Appendix B

M = air dose factor for Kr-89, from Table 4 of Appendix B

2.1.2 Waste Gas Decay System and Containment Purge Monitors

The waste gas decay tank releases and containment purges, in addition to being monitored by the station vent monitor, are controlled individually to provide additional assurance that releases do not exceed the limits of Technical Specifications 3.11.2.1.

The setpoint level (S_d) for discharge through the waste gas decay system monitor will be calculated in a corresponding manner:

$$S_d =$$
 the lesser of $\begin{vmatrix} 0.5 & (r_t) & 500 \\ or & & & \\ 0.5 & (r_s) & 3000 \end{vmatrix}$ (2-6)

where:

S_d = count rate of waste gas decay system monitor at alarm setpoint level

r, = count rate per mrem/yr to the total body

r = count rate per mrem/yr to the skin

The values of $r_{\rm t}$ and $r_{\rm s}$ are dependent on the radionuclide distribution and are derived by the equations:

$$r_{t} = c + \left[\left(\overline{\chi/Q}_{NG} \right) \sum_{i} K_{i} \dot{q}_{i} \right] \qquad (2-7)$$

$$r_s = c + [(\overline{\chi/Q}_{NG})^{\Sigma}_{i} (L_{i} + 1.1M_{i})^{i}_{i}]$$
 (2-8)

where:

c = count rate of the waste gas decay system monitor for radionuclide concentrations to be discharged (cpm)

q
i = rate of release of noble gas radionuclide i
 (μCi/sec)

For a more conservative, simpler setpoint for the waste gas system monitor, the equations are:

$$\mathbf{r}'_{\mathsf{t}} = \mathbf{c}' \div \left[\left(\overline{\chi/Q} \right) \mathbf{K} \right] \tag{2-9}$$

$$r'_{s} = c' \div [(\overline{\chi/Q})(L + 1.1M)]$$
 (2-10)

where:

r't = conservative count rate per mrem to the total body (Xe-133 detection, Kr-89 dose)

r's conservative count rate per mrem to the skin (Xe-133 detection, Kr-89 dose)

c' = count rate of the waste gas decay system monitor for an effluent concentration corresponding to 1.0 µCi/sec release rate for Xe-133

The setpo - level for the containment purge noble gas monitor will be calculated using the same methodology as indicated for the waste gas decay system, utilizing the appropriate corresponding count and release rates.

The calculated setpoint values will be regarded as upper bounds for the actual setpoint adjustments (ie, setpoint adjustments are not required to be performed if the existing setpoint level corresponds to a lower count rate than the calculated value).

2.2 Gaseous Effluent Dose Rate and Dose Calculations

2.2.1 Unrestricted Area Boundary Dose Rate

a. Technical Specification 3.11.2.1a limits the dose rate in the unrestricted area due to noble gas releases from the station to <500 mrem/yr, total body and <3000 mrem/yr, skin. Radiation monitor alarm setpoints are established to assure that these release limits are not exceeded. In the event any gaseous releases from the station results in the alarm setpoints being exceeded, an evaluation of the unrestricted area dose rate resulting from the release shall be performed using the following equations:

$$D_{tb} = (\overline{\chi/Q}_{NG}) \sum_{i} K_{i} \dot{Q}_{i}$$
 (2-11)

$$D_{s} = (\overline{\chi/Q}_{NG}) \sum_{i} (L_{i} + 1.1M_{i}) \dot{Q}_{i} \qquad (2-12)$$

where:

D_{tb} = total body dose rate (mrem/yr)

D = skin dose rate (mrem/yr)

 $\overline{\chi/Q}$ = highest sector annual average atmospheric NG dispersion at the unrestricted area boundary

- = $1.83 \times 10^{-6} \text{ sec/m}^3$ in the north-northeast sector
- b. For I-131, tritium and particulates with half-lives greater than 8 days, Technical Specification 3.11.2.1.b limits the dose rate to ≤1500 mrem/yr to any organ. To demonstrate compliance with this limit, an evaluation is performed at a frequency corresponding to the

sampling and analysis time period (e.g., normally once per 7 days for I-131). The following equation may be used for evaluation:

$$D_{o} = (\overline{\chi/Q}) \sum_{i} (P_{i} \overline{Q}'_{i}) \qquad (2-13)$$

where:

D = average organ dose rate over the sampling time period (mrem/year)

 $\overline{\chi/Q}$ = controlling sector annual average atmospheric dispersion at the site boundary for the inhalation pathway.

- = 1.68 x 10⁻⁶ sec/m³ in the north-northeast sector.
- P_i = dose parameter for radionuclide i, (mrem/yr per μCi/m³) for inhalation pathway from Table 5 of Appendix B. Values for P_i are derived in accordance with the methods described in NUREG-0133.
- Q'_i = average release rate over the appropriate sampling period and analysis frequency for isotope i, I-131 or other radionuclide in particulate form with half-life greater than eight days (μCi/sec).

By substituting 1500 mrem/yr for D $_{\rm o}$ (equation 2-13) and solving for $\overline{\rm Q}_{\rm i}'$, an allowable release rate for I-131 can be determined. Based on the annual average meteorological dispersion (1.68 x 10⁻⁶ sec/m³) and the child inhalation pathway (P $_{\rm i}$ = 1.62 x 10⁷ mrem/yr per μ Ci/m³), the release rate for I-131 is 44.1 μ Ci/sec. An added conservatism

factor of 0.8 has been included in this calculation to account for any potential dose contribution from other radioactive particulate material. For a 7 day period which is the sampling and analysis frequency for I-131, the cumulative allowable release is 26.7 Ci. Therefore, as long as the I-131 releases in any 7 day period do not exceed 26.7 Ci, no additional analyses are needed to verify compliance with the Technical Specification 3.11.2.1.b limits on allowable release rate.

2.2.2 Unrestricted Area Dose to Individual

a. Technical specification 4.11.2.2 requires at least a monthly assessment of releases of noble gases to evaluate compliance with the quarterly dose limits of ≤5 mrad, gamma-air dose and ≤10 mrad, beta-air dose. The following equations may be used to calculate the gamma-air and beta-air doses:

$$D_{\gamma} = 3.17 \times 10^{-8} \sum_{i} M_{i} [(\overline{\chi/Q}_{NG})\tilde{Q}_{i}]$$
 (2-14)

$$D_{\beta} = 3.17 \times 10^{-8} \sum_{i} N_{i} [(\overline{\chi/Q}_{NG})\tilde{Q}_{i}]$$
 (2-15)

where:

Dy = air dose due to gamma emissions for noble gas radionuclide i (mrad)

 χ/Q a dispersion parameter for unrestricted areas NG = 1.83 x 10^{-6} sec/m³

 \widetilde{Q}_{i} = cumulative release of noble gas radionuclide i over the period of interest (μ Ci)

- D_β = air dose due to beta emissions from noble gas radionuclide i (mrad)
- N_i = air dose factor due to beta emissions from noble gas redionuclide i (mrad/yr per μCi/m³) from Table 4 of Appendix B.
- $3.17 \times 10^{-8} =$ conversion factor (yr/sec)
- b. Technical Specification 4.11.2.3 requires an assessment at least once per 31 days to evaluate compliance with the quarterly dose limit of ≤7.5 mrem to any organ. The following equation may be used to evaluate the maximum organ dose due to releases of I-131, tritium and particulates with half-lives greater than 8 days.

$$D_{p} = 3.17 \times 10^{-8} \sum_{i} \tilde{Q}'_{i} (R_{inh_{i}} \overline{\chi/Q'} + R_{veg_{i}} \overline{D/Q'})$$
 (2-16)

1

where:

- D_p = dose or dose commitment to organ p, including the total body, from I-131 and radionuclides in particulate form with half-life greater than eight days (mrem)
- χ/Q' = 1.19 x 10⁻⁶ sec/m³ for inhalation pathway and H-3 dose contribution via other pathways (from Table 7 of Appendix B)
- $\overline{D/Q}'$ = 1.39 x 10⁻⁸ m⁻² vegetation pathway (from Table 7 of Appendix B)

R_{inh} = inhalation dose factor for radionuclide i from Table 6 of Appendix B (mrem/year per µCi/m³). Values for the inhalation dose factor were derived in accordance with the methods described in NUREG-0133.

R_{veg} = vegetation pathways dose factor for radionuclide i from Table 6 of Appendix B (m² - mrem/year per µCi/sec). Values for vegetation pathway dose factor were derived in accordance with the methods described in NUREG-0133.

Q'_i = cumulative release of radionuclide i of I-131 or material in particulate form in long-term releases over the period of interest (μCi).

The location of exposure pathways and the maximum organ dose may be based on the available pathways in the surrounding environment of Davis-Besse as identified by the annual land-use census (Technical Specification 3.12.2). Table 7 of Appendix B will be supplemented yearly by including in the Semi-Annual Radioactive Effluent Report the applicable exposure pathways as identified by the census.

c. For the purpose of implementing RETS Technical Specification 3.11.3 on the EPA environmental radiation dose standard and 6.9.1.13 on reporting, dose calculations will be performed using the above equations with the substitution of average or actual meteor logical parameters for the period of interest and applicable pathways.

2.3 Projected Personel Maximum Dose from Gaseous Effluents

The dose commitment to a person offsite due to radioactive material released in gaseous effluent may be projected by calculating the air dose for gamma and beta radiation and the most exposed organ dose commitments to a hypothetical person.

The dose commitment to a maximally exposed hypothetical person will be projected by calculating the doses accumulated during the most recent three months according to the method described in Section 2.2.2 and by assuming that the result represents the projected doses during the current month or quarter.

Alternatively, the 31 day dose commitment may be projected by using the equation:

$$P_{t} = \underline{T} D_{t}$$

$$X \tag{1-11}$$

where:

Pt = projected air dose commitment (mrem) from or dose to organ t (including total body).

1

T = number of days in the projected time period (i.e. 31 days, 91 days).

X = number of days to date in current quarter

Dt = accumulated personal dose to date during the current quarter via radioactive material in gaseous effluent (mrem)

2.4 Total Dose

2.4.1 Compliance with 40CFR190

Compliance with 40CFR190 as prescribed by Specification 3.11.4 will be demonstrated when one or more of Specifications 3.11.1.2a, 3.11.1.2b, 3.11.2.2a, 3.11.2.2b, 3.11.2.3a, or 3.11.2.3b has been exceeded by a factor of 2. Once this occurs, the Company has 30 days to submit a report in accordance with Specification 6.9.2.

2.4.2 Calculations Evaluating Conformance with 40CFR190

To perform the calculation to evaluate conformance with 40CFR190, an effort will be made to develop doses that are realistic by removing assumptions that might lead to overestimates of dose to a member of the public. To accomplish this, the following general rules will apply:

- a. Environmental sampling data which demonstrates that no pathway exists may be used to delete a pathway to man.
- b. Locations used to calculate doses to a member of the public will only be at actual residences.
- c. When doses via direct radiation are added to doses via the inhalation pathway, they will be calculated for the same receptor location (i.e., the same distance in the same sector).

2.4.3 Calculation of the Total Body Dose

Estimates will be made for each of the following exposure pathways to the same location by age class. Only those age classes known to exist at a location are considered.

a. Direct Radiation

The component of dose to a Member of the Public due to direct radiation will be determined by first estimating the direct radiation dose at or near the site boundary, in each sector, using direct radiation measurements or radiation transport methodology. The dose at the calculational location is then determined by extrapolating the dose at the Site Boundary to the calculational location. The following method will be used.

$$D_{L,\theta} = D_{B,\theta} \frac{(X_{B,\theta})^2}{(X_{L,\theta})^2}$$

 $D_{B,\theta}$ = Direct radiation dose at the site boundary in sector θ .

 $D_{L,\theta}$ = Dose at calculational location in sector θ .

 $X_{L,\theta}$ = Distance to the calculational location in sector θ .

 $X_{B,\theta}$ = Distance to the site boundary (or TLD location) in sector θ in meters.

b. Inhalation Dose

The inhalation dose will be determined at the calculational locations for each age group according to the methods outlined in Sections 2.2 of this manual.

c. Ingestion Pathway

The dose via the ingestion pathway will be calculated at the consumer locations for the consumers at risk.

d. Other Uranium Fuel Cycle Sources

For purposes of the Special Report, it will be assumed that the contribution to the dose commitment from other Uranium fuel cycle sources is negligible.

2.4.4 Calculation of the Thyroid Dose

The dose to the thyroid will be calculated for each sector as the sum of the inhalation dose and the milk ingestion dose (if existing). The calculational methods will be those identified in Section 2.2 of this manual.

2.5 Meteorological Model

2.5.1 Long-Term Atmospheric Dispersion

Atmospheric dispersion for long-term releases is calculated using a mixed-mode, wake-split form of the straight-line flow Gaussian dispersion model, referenced in Regulatory Guide 1.111, Revision 1.

 χ/Q = atmospheric dispersion (sec/m³)

$$= \frac{2.03 \text{ k\delta}}{r} \left[\frac{1-E}{u\sigma_z} \exp \left[-\frac{h^2}{2\sigma_z^2} \right] + \frac{E}{u_g \Sigma} \right]$$
 (2-17)

1

where:

- k = open terrain recirculation factor at distance r from Figure 2 of Appendix A.
- δ = plume depletion factor at distance r for appropriate stability class and effective height from Figures 3-6 of Appendix A. (Note: This plume depletion factor applies only to releases of radioiodines. The depletion factor for noblegases is unity.)
- E = fraction considered as ground level

1.0 for
$$\frac{v}{u} \le 1.0$$

2.58-1.58 $\frac{v}{u}$ for $1.0 < \frac{v}{u} \le 1.5$

0.3-0.06 $\frac{v}{u}$ for $1.5 < \frac{v}{u} \le 5.0$

0 for $\frac{v}{u} > 5.0$

- v = station vent exit velocity (13.4 m/sec)
- u = wind speed at vent height from the 75-m level of
 the main meteorological tower (m/sec)
- u = wind speed at ground level from the 10-m level of the satellite meteorological tower (m/sec)
- σ_z = vertical standard deviation of the plume at distance r for effective height under stability category indicated by temperature lapse rate ΔT (°C/100m) from Figure 7 of Appendix A.

ΔT = temperature differential with vertical separation between the 10-m and 75-m levels of the main meteorological tower (°K/100m)

the lesser of
$$\begin{bmatrix} 1.44 & \frac{v}{u} & \frac{r}{d} & d \\ 0 & \frac{v}{d} & \frac{v}{d} \end{bmatrix} - c_v$$
or
$$3 & \frac{vd}{u}$$

subject to, for stable conditions ($\Delta T > -0.5$ °K/100m):

the lesser of
$$\begin{bmatrix} 4 & \frac{F_m}{S} \end{bmatrix}^{1/4}$$
 or
$$\begin{bmatrix} 1.5 & \frac{F_m}{u} \end{bmatrix}^{1/3} S^{-1/6}$$

- d = diameter of station vent
 - = 2.12 m
- c = correction for low vent exit velocity (m)

$$= \begin{bmatrix} 3 & 1.5 - \frac{v}{u} \end{bmatrix} d \text{ for } \frac{v}{u} < 1.5$$

$$= \begin{bmatrix} 0 & \text{for } \frac{v}{u} \ge 1.5 \end{bmatrix}$$

- $F_m = momentum flux parameter (m^4/sec^2)$ = $(\frac{vd}{2})^2$
- S = restoring acceleration per unit vertical displacement for adiabatic motion in the atmosphere

8.7 x
$$10^{-4} \text{ sec}^{-2}$$
 for $\Delta T \le 1.5$ (E)

1.75 x
$$10^{-3}$$
 sec⁻² for $\Delta T \le 4.0$ (F)

$$2.45 \times 10^{-3} \text{ sec}^{-2} \text{ for } \Delta T > 4.0 (G)$$

- h_t = height of terrain at distance r in sector of interest (m)
- r = downwind distance (m)

 Σ = vertical standard deviation of the plume with building wake correction (m)

- b = height of reactor building
 - = 73.5m

2.5.2 Long-Term Deposition

Relative deposition per unit area for long term releases is calculated for a mixed mode release.

D/Q = relative deposition per unit area (m^{-2})

$$= \frac{2.55k}{r} \left[(1-E) D_e + ED_g \right]$$
 (2-18)

where:

D_e = relative deposition rate for elevated releases from Figures 9 through 11 of Appendix A.

g = relative deposition rate for ground level releases from Figure 8 of Appendix A.

2.6 Definitions of Gaseous Effluents Parameters

b = height of reactor building (m) (Section 2.3.1)

- C = count rate of the station vent monitor corresponding to
 grab sample radionuclide concentrations (cpm)
 (Section 2.1.1)
- C' = count rate of station vent monitor corresponding to a 1.0 μCi/sec release rate of Xe-133 (cpm) (Section 2.1.1)
- c = count rate of the waste gas decay system monitor for radionuclide concentrations to be discharged (cpm) (Section 2.1.2)
- c' = count rate of the waste gas decay system monitor corresponding to a 1.0 μCi/sec release rate of Xe-133 (cpm) (Section 2.1.2)
- c_y = effective plume height correction for low vent exit velocity (m) (Section 2.3.1)
- D_e = relative deposition rate for elevated releases from Figure 6 of Appendix A (Section 2.3.2)
- D = relative deposition rate for ground level releases from Figure 7 of Appendix A (Section 2.3.2)
- D = average organ dose rate (mrem/year) (Section 2.2.1.b)
- D = dose or dose commitment to organ p, including the total body, from I-131 and radionuclides in particulate form, with half-life greater than eight days (mrem)

 (Section 2.2.2.b)
- D_s = average skin dose rate (mrem/year) (Section 2.2.1.a)
- D_{rh} = average total body dose rate (mrem/year) (Section 2.2.1.a)

- D_β = air dose due to beta emissions from noble gas radionuclide i (mrad) (Section 2.2.2.a)
- D_Y = air dose due to gamma emissions from noble gas radionuclide i (mrad) (Section 2.2.2.a)
- $\overline{D/Q}$ = relative deposition per unit area (m⁻²) (Section 2.3.2)
- d = diameter of station vent (m) (Section 2.3.1)
- δ = plume depletion factor at distance r for appropriate stability class and effective height from Figures 3 and 4 of Appendix A (dimensionless) (Section 2.3.1)
- E = fraction of release considered as ground level (dimensionless) (Section 2.3.1)
- $F_m = momentum flux parameter (m^4/sec^2) (Section 2.3.1)$
- h = effective height of release (m) (Section 2.3.1)
- $h_v = height of station vent (m) (Section 2.3.1)$
- K = total body dose factor for Kr-89, (mrem/yr per μ Ci/m³) from Table 4 of Appendix B (Section 2.1.1)
- K_i = total body dose factor due to gamma emissions from radionuclide (mrem/yr per μCi/m³) from Table 4 of Appendix B (Section 2.1.1)

- k = open terrain recirculation factor at distance r from Figure 2 of Appendix A (dimensionless) (Section 2.3.1)
- L = skin dose factor for Kr-89, the most restrictive radionuclide, from Table 4 of Appendix B (mrem/yr per µCi/m³) (Section 2.1.1)
- L_i = skin dose factor due to beta emissions from radionuclide i (mrem/yr per μCi/m³) from Table 4 of Appendix B (mrem/yr per μCi/m³) (Section 2.1.1)
- M = air dose factor for Kr-89, the most restrictive radionuclide, from Table 4 of Appendix B (mrad/yr per μCi/m³) (Section 2.1.1)
- M_i = air dose factor due to gamma emissions from radionuclide i (mrad/yr per μCi/m³) from Table 4 of Appendix B (Section 2.1.1)
- N_i = air dose factor due to beta emissions from noble gas radionuclide i (mrad/yr per µCi/m³) from Table 4 of Appendix B (Section 2.2.2.a)
- P_i = dose parameter for radionuclide i, (wrem/yr per μCi/m³) for inhalation from Table 5 of Appendix B (Section 2.2.1.b)
- \dot{Q}_{i} = rate of release of noble gas radionuclide i (μ Ci/sec) (Section 2.1.1)
- Q'_i = average release rate over appropriate sampling period of isotope i of I-131 or other radionuclide in particulate form, with half-life greater than eight (8) days (μCi/sec) (Section 2.2.1.b)
- \tilde{Q}_{i} = cumulative release of noble gas radionuclide i over the period of interest (μ Ci) (Section 2.2.2.a)

- \widetilde{Q}'_{i} = cumulative release of radionuclide i of I-131 or material in particulate form over the period of interest (μ Ci) (Section 2.2.2.b)
- q = rate of release of noble gas radionuclide i (μCi/sec) (Section 2.1.2)
- $R_{inh_{i}}$ = inhalation dose factor for radionuclide i from Table 6 of Appendix B (mrem/year per $\mu Ci/m^3$) (Section 2.2.2.b).
- R_{veg} = vegetation pathway dose factor for radionaclide i from Table 6 of Appendix B (m² mrem/year per μCi/sec) (Section 2.2.2.b).
- R_s = count rate per mrem/yr to the skin based on current isotope distribution (Section 2.1.1)
- R_t = count rate per mrem/yr to the total body based on current isotope distribution (Section 2.1.1)
- R's conservative count rate per mrem/yr to the skin (Xe-133 detection Kr-89 dose) (Section 2.1.1)
- R'_t = conservative count rate per mrem/yr to the total body (Xe-133 detection, Kr-89 dose) (Section 2.1.1)
- r = downwind distance (m)
- r_s = count rate per mrem/yr to the skin based on waste gas decay system isotope distribution (Section 2.1.2)
- rt = count rate per mrem/yr to the total body based on current waste gas decay system isotope distribution (Section 2.1.2)
- r's = conservative count rate per mrem to the skin for waste gas decay system only (Section 2.1.2)

- r't = conservative count rate per mrem to the total body for waste gas decay system only (Section 2.1.2)
- S = restoring acceleration per unit vertical displacement for adiabatic motion in the atmosphere (sec⁻²) (Section 2.3.1)
- S_d = count rate of waste gas decay system noble gas monitor at alarm setpoint level (Section 2.1.2)
- S_v = count rate of station vent noble gas monitor at alarm setpoint level (Section 2.1.1)
- Σ = vertical standard deviation of the plume with building wake correction (m) (Section 2.3.1)
- σ_z = vertical standard deviation of the plume at distance r for effective height under stability category indicated by ΔT from Figure 5 of Appendix A (m) (Section 2.3.1)
- ΔT = temperature differential with vertical separation (°K/100m) (Section 2.3.1)
- wind speed at vent height from the 75-m level of the main meteorological tower (m/sec) (Section 2.3.1)
- u = wind speed at ground level from the 10-m level of the satellite meteorological tower (m/sec) (Section 2.3.1)
- v = plant vent exit velocity (m/sec) (Section 2.3.1)
- χ/Q = atmospheric dispersion (sec/m³) (Section 2.3.1)
- $\overline{\chi/Q}$ = highest sector annual average atmospheric dispersion value at the unrestricted area boundary (sec/m³) (Section 2.1.1)

- $\overline{\chi/Q}_{I}$ = controlling sector annual average atmospheric dispersion at the site boundry for the inhalation pathway (Section 2.2.1.b)
- $\overline{\chi/Q}_{NG}$ = highest sector annual average atmospheric dispersion at the unrestricted area boundary (sec/m³) (Secton 2.2.2.a)

2.7 References to 2.0 Gaseous Effluents

- 2.7.1 J. S. Boegli, W. L. Britz, R. R. Belamy, and R. L. Waterfield. 1978. "Preparation of Radiological Effluent Technical Specifications for Nuclear Power Plants," NUREG-0133, Office of Nuclear Reactor Regulation, U.S. Nuclear Regulatory Commission.
- 2.7.2 United States Nuclear Regulatory Commission. 1977.

 "Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water-Cooled Reactors," Regulatory Guide 1.111, Revision 1.

3.0 RADIOLOGICAL ENVIRONMENTAL MONITORING

Sampling locations as required in Section 3/4.12.1 of the Radiological Effluent Technical Specifications are described in Table 8 of Appendix B and shown on maps in Appendix A, pages A-12 and A-16 through A-50.

3.1 Land Use Census

A land use census shall be conducted annually for the purpose-of identifying changes in the use of the offsite area surrounding Davis-Besse which may substantially affect the radiological dose assessment or which may indicate needed adjustments to the Program. This census satisfies the criteria of 10 CFR Part 50, Appendix I, Section IV.B.3.

The census will include land within 5 miles of Davis-Besse and will be conducted at least annually. It will be conducted by either a door-to-door survey, aerial survey, or by consulting local agricultural authorities or by a combination thereof.

The locations of: 1) the nearest milk animal, 2) the nearest vegetable garden greater than 500 square feet, and 3) the nearest resident, within 5 miles of Davis-Besse in each of 16 sectors in cardinal compass point directions from the plant, are to be identified in the census. If a milk animal is not identified in a sector within 5 miles, one may conservatively assume that one is located at the 5-mile distance for purposes of evaluating maximum potential organ dose and identifying the controlling pathway, except in those sectors over Lake Erie.

If the land use census identifies a location(s) at which the dose or dose commitment calculated at the time is greater than the maximum calculated dose associated with the like pathway(s) at a location where sampling is conducted as specified by the monitoring program, then the pathways having maximum exposure

lpotential at the newly identified location will be added to the program, if samples are reasonably obtainable at the new location. Like pathways monitored (sampled) at a location, excluding control station location(s), having a lower associated calculated personal dose may be deleted from the program at the time the new pathway(s) and location(s) are added.

3.2 Sample Analyses

Radioactivity in environmental samples described in Table 8 of Appendix B may be analyzed either at Davis-Besse or at an offsite laboratory. In order to provide a comparative check on the accuracy and precision of these analyses, the laboratory participates in the USEPA Interlaboratory Comparison Program by analyzing radioactive samples distributed for the purpose.

Tables 9 and 10 of Appendix B identify the type and frequency of environmental sample collection.

4.0 REGULATORY GUIDE 1.21 - EFFLUENT AND WASTE DISPOSAL SEMI-ANNUAL REPORT

4.1 Technical Specification Limits Used for Gaseous Effluents

Since the β-air dose is usually the most limiting for exposure to noble gases, this specification as shown in 3.11.2.2a will be used to determine the percent of limits reported in the Regulatory Guide 1.21 Report. The specification for the dose to a Member of the Public from I-131, tritium, and particulates with half-lives greater than 8-days is specified in 3.11.2.3.a for any organ.

4.2 Technical Specification Limits Used for Liquid Effluents

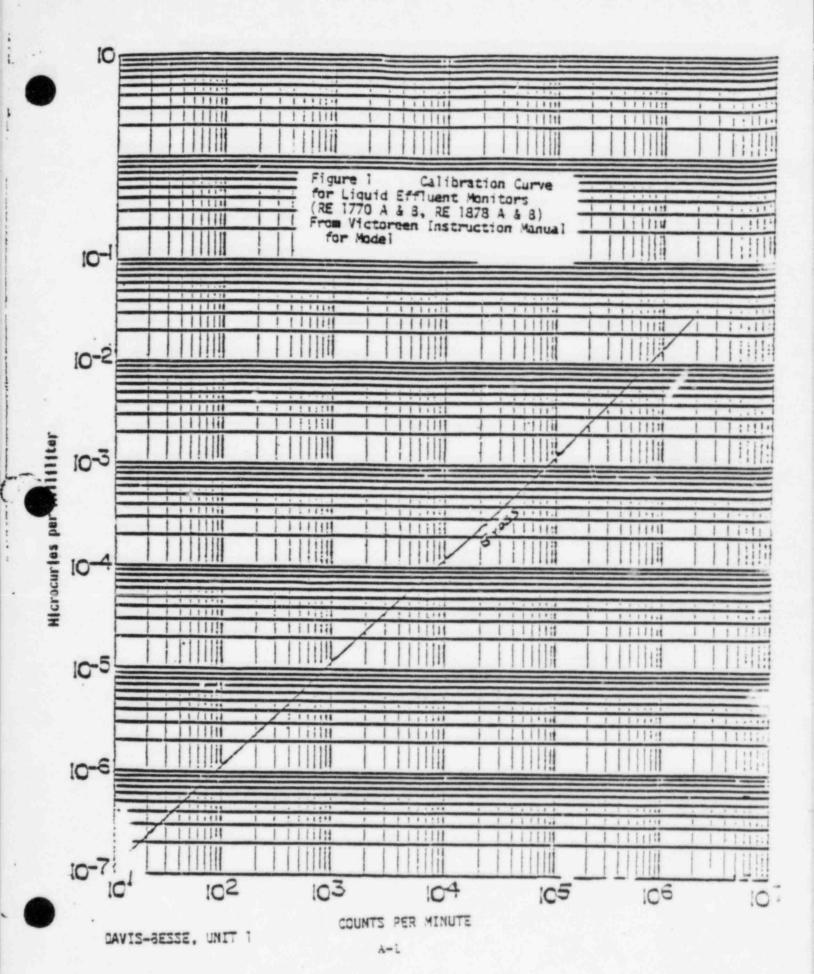
The specification for dose to a MEMBER OF THE PUBLIC used to determine the reported percent of limit from liquid effluents is shown in 3.11.1.2.a for the total body and to any organ.

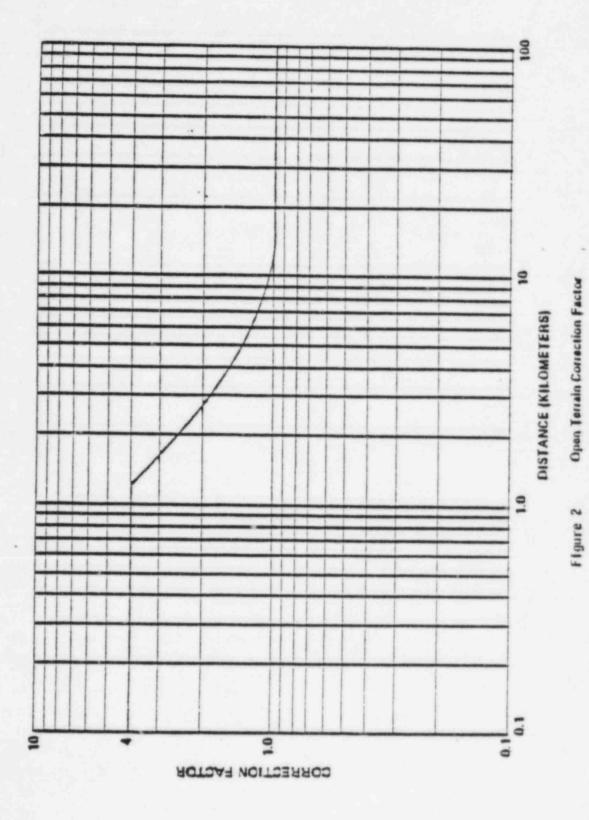
The limit for the concentration of radioactive material released to UNRESTRICTED AREAS from liquid effluents, other than dissolved or entrained noble gases, are those specified in 10CFR Part 20.106.

T. S. 3.11.1.1 specifies 2 X 10⁻⁴ microcuries/ml as the concentration limit for dissolved or entrained noble gases.

DBP 4306G

APPENDIX A Figures

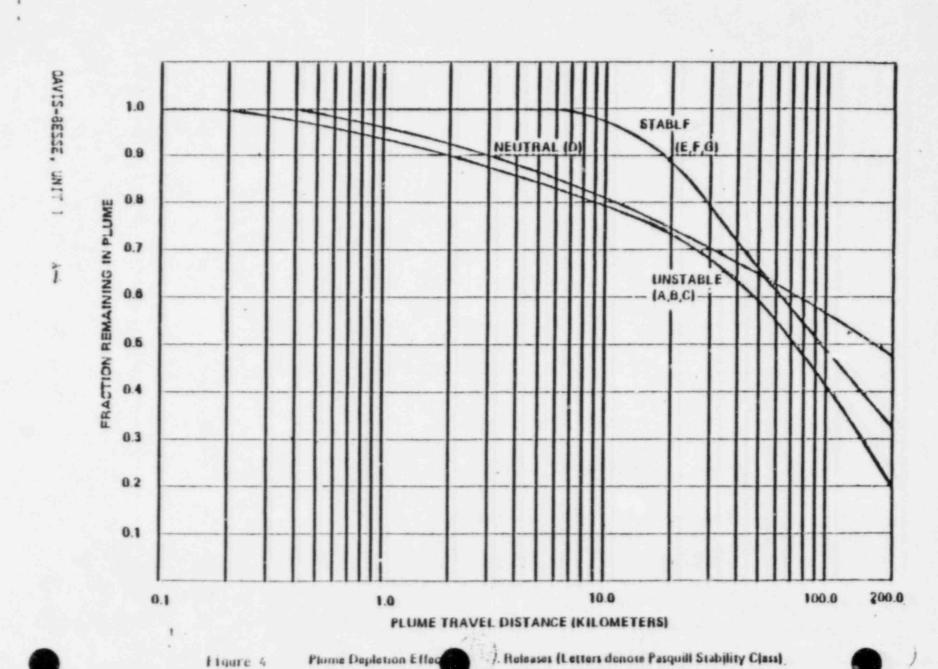


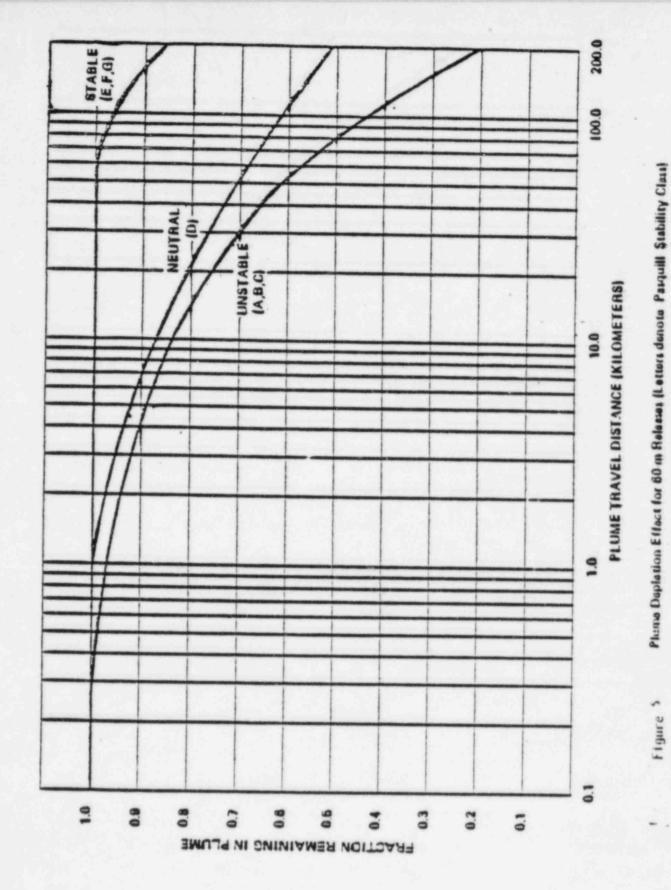


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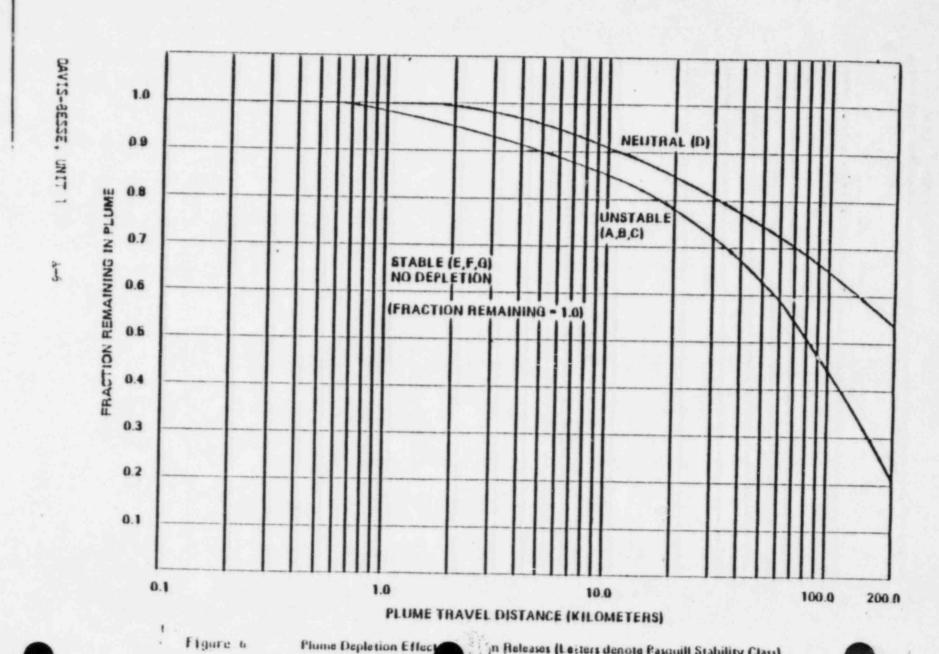
Pluma Depletion Effect for Ground Level Heleases (All Atmospheric Stability Classes) Figure 1

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in Releases (Leiters denote Pasquill Stability Class)

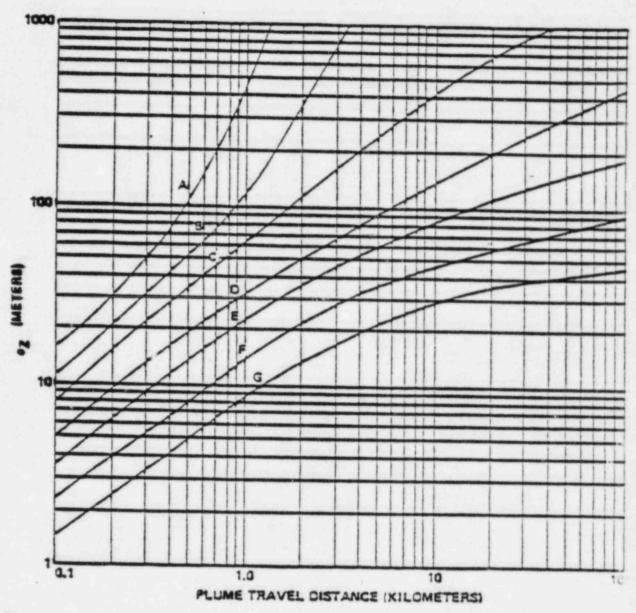


Fig. 7 Vertical Standard Deviation of Material in a Plume (Letters denote Pasquill Stability Class

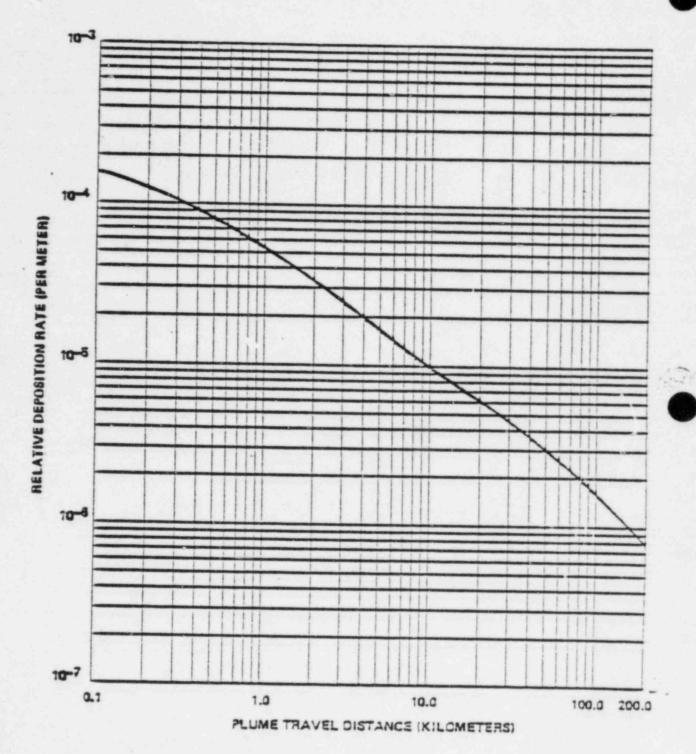


Figure 3 Relative Deposition for Ground-Lavel Releases (All Atmospheric Stability Classes)

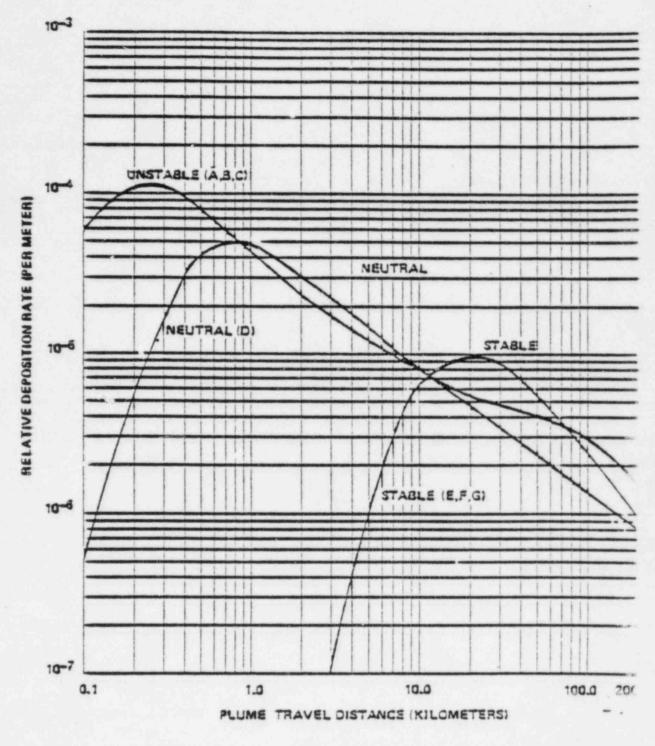


Figure 9 Relative Deposition for 30-m Releases (Letters denote Pasquill Stability Class)

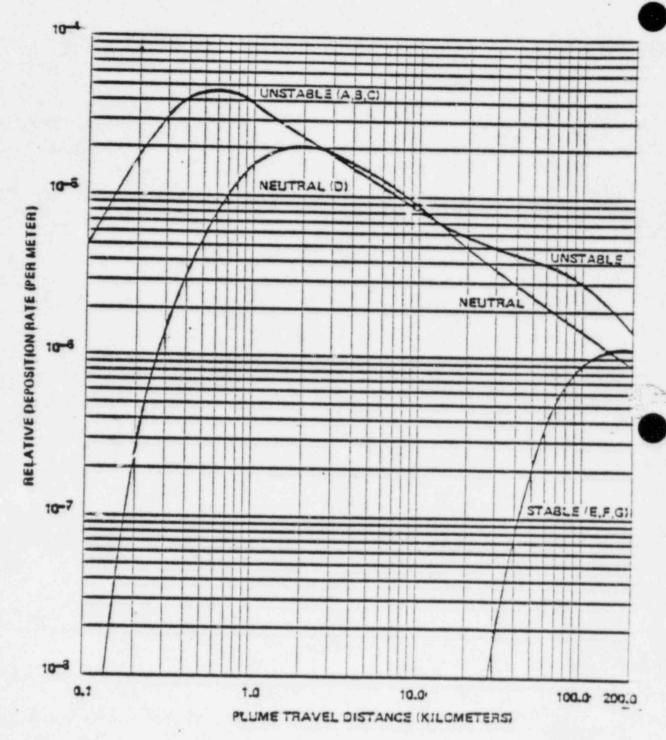


Figure 10 Relative Deposition for 60-m Releases (Latters denote Pasquill Stability Class)

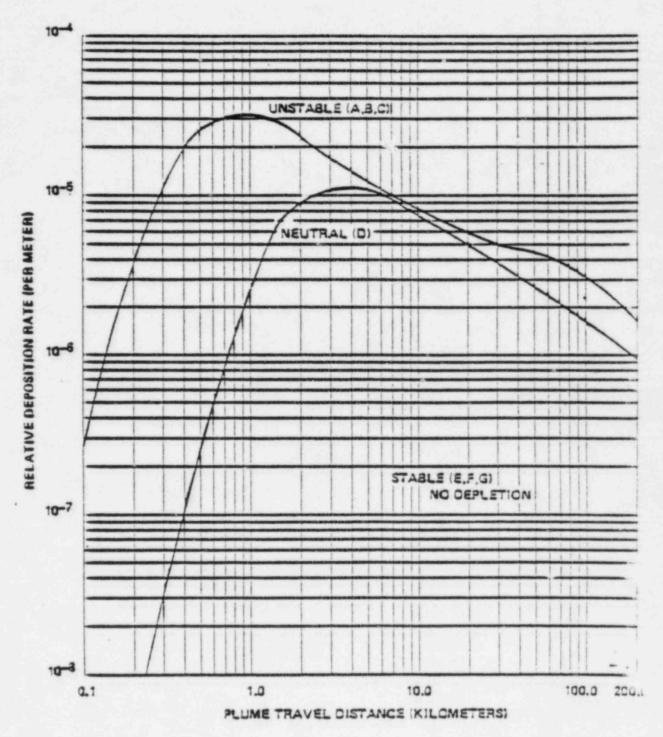
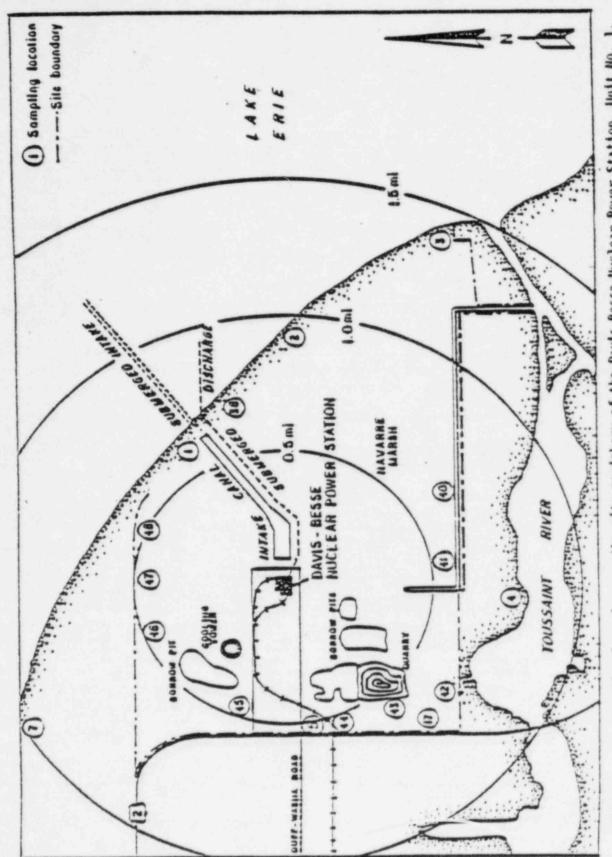
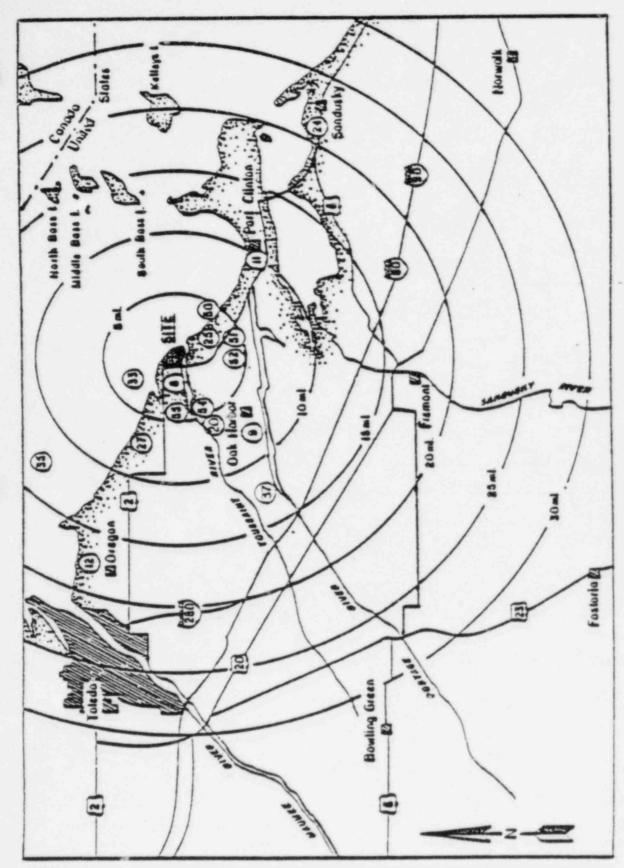


Figure 11 Relative Deposition for 100-m Releases (Latters denote Pasquill Stability Class)

CAVIS-BESSE, UNIT 1



Sampling locations on the site periphery of the Davis-Besse Huclear Power Station, Unit No. 1. Figure 12



Sampling locations (excepting those on the site periphery), Davis-Besse Nuclear Power Station, Unit No. 1. Flgure 13

FIGURE 14. DAVIS-BESSE GASEOUS DISCHARGE

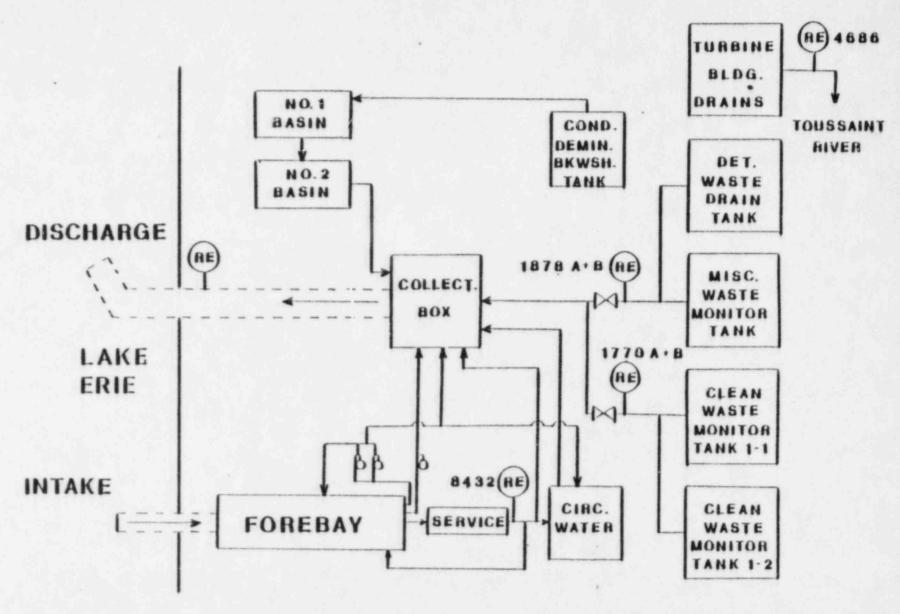
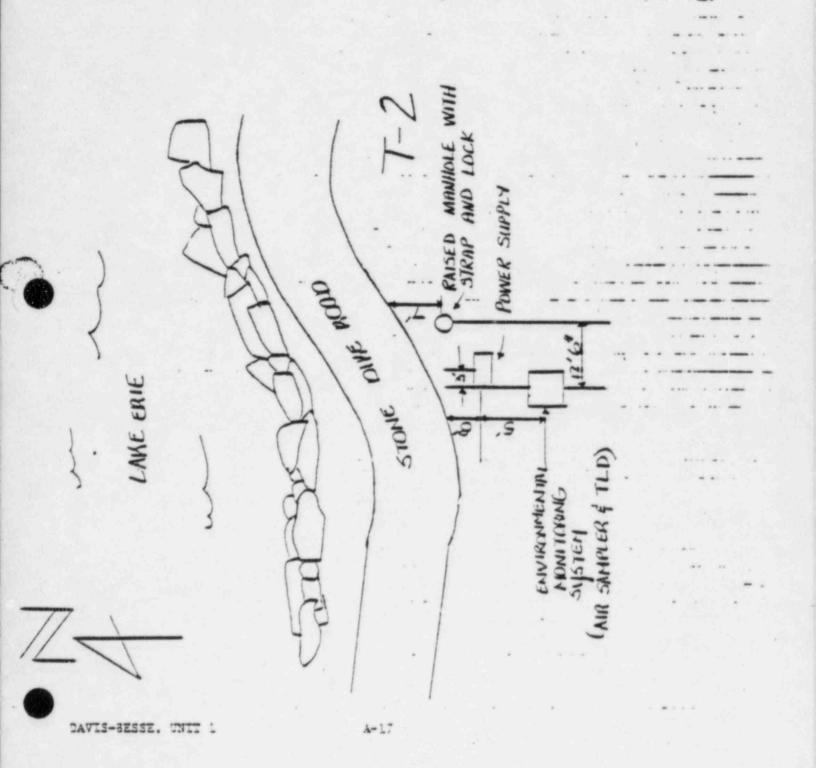
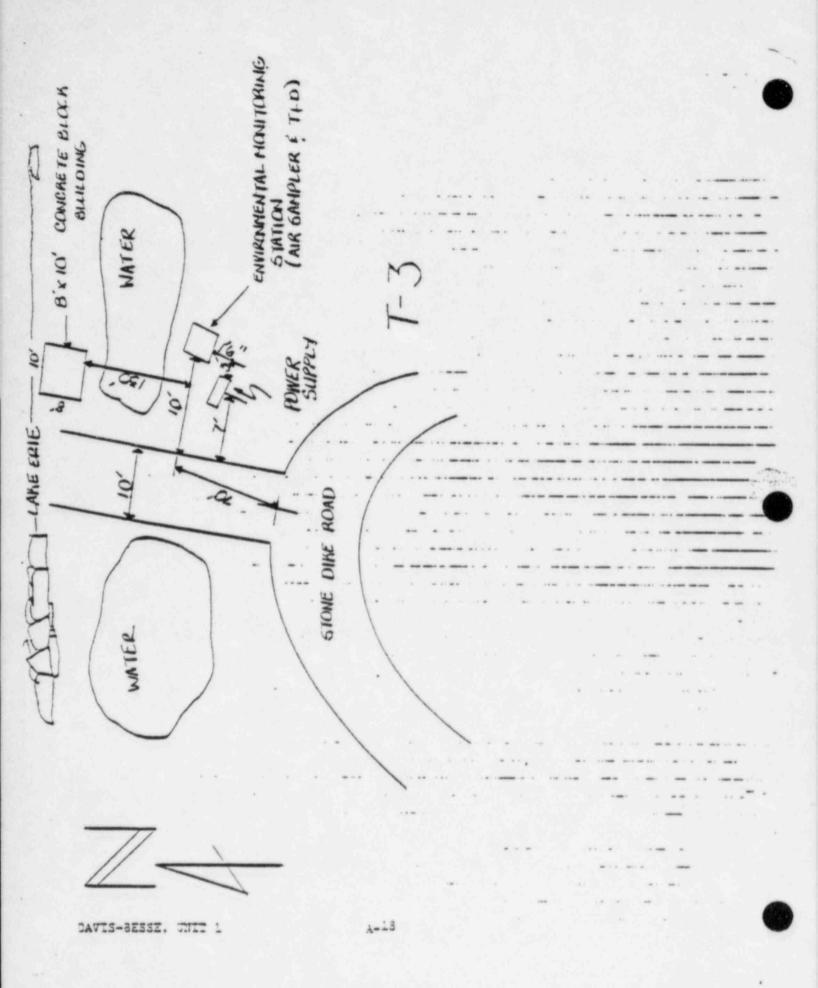
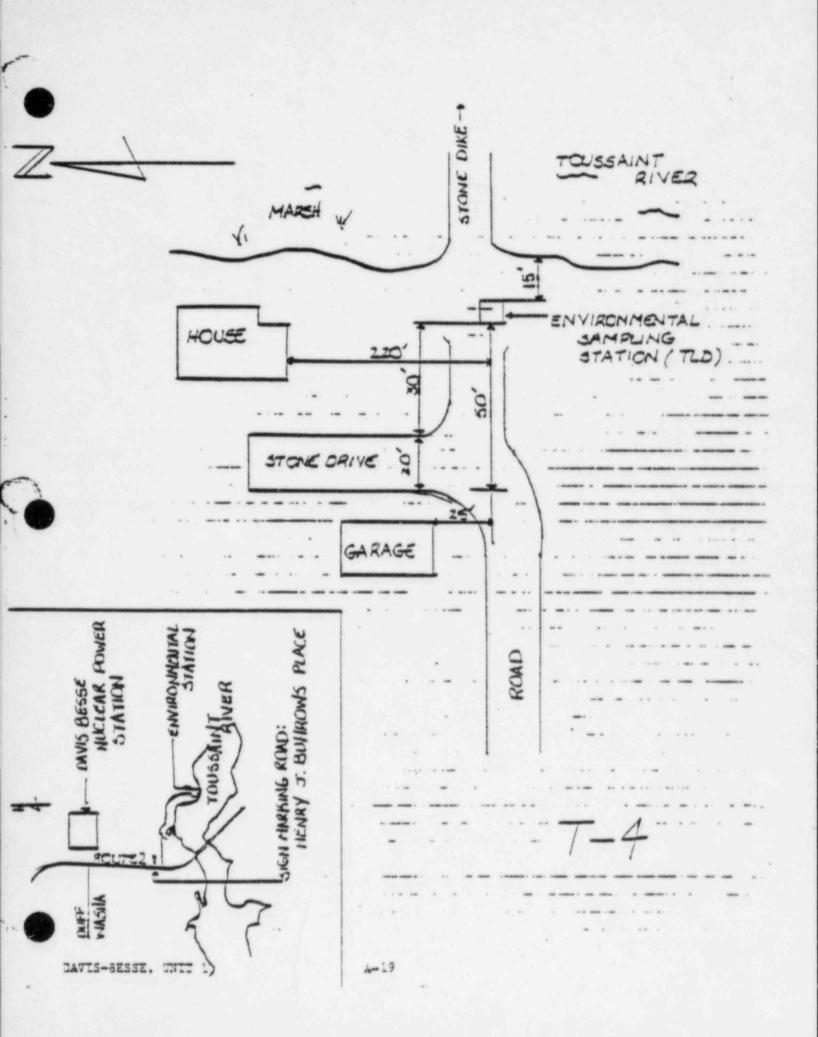


FIGURE 15. DAVIS - BESSE UNIT ONE LIQUID DISCHARGE

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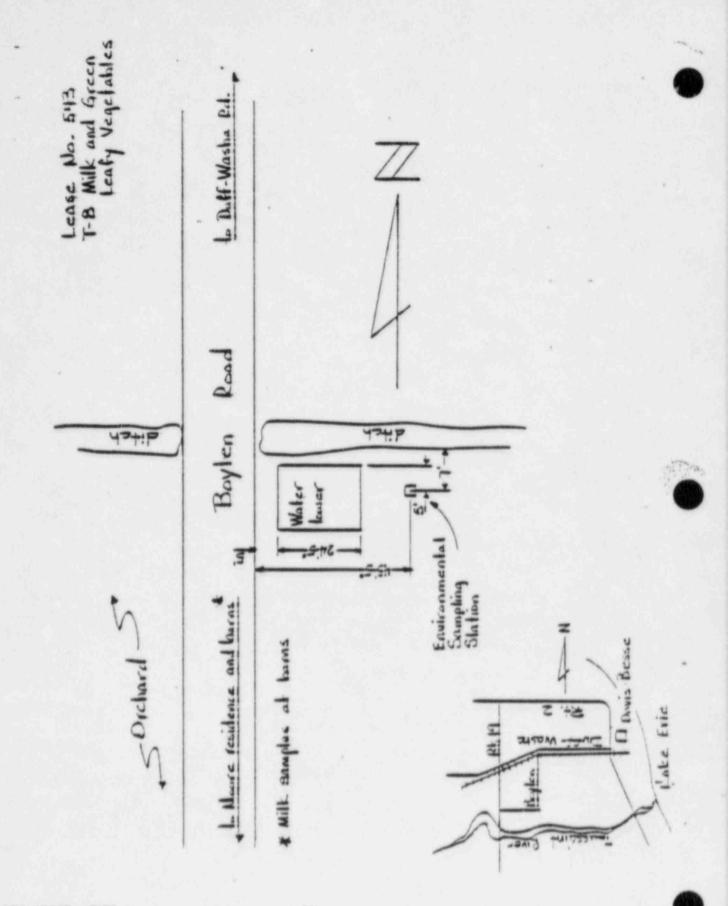


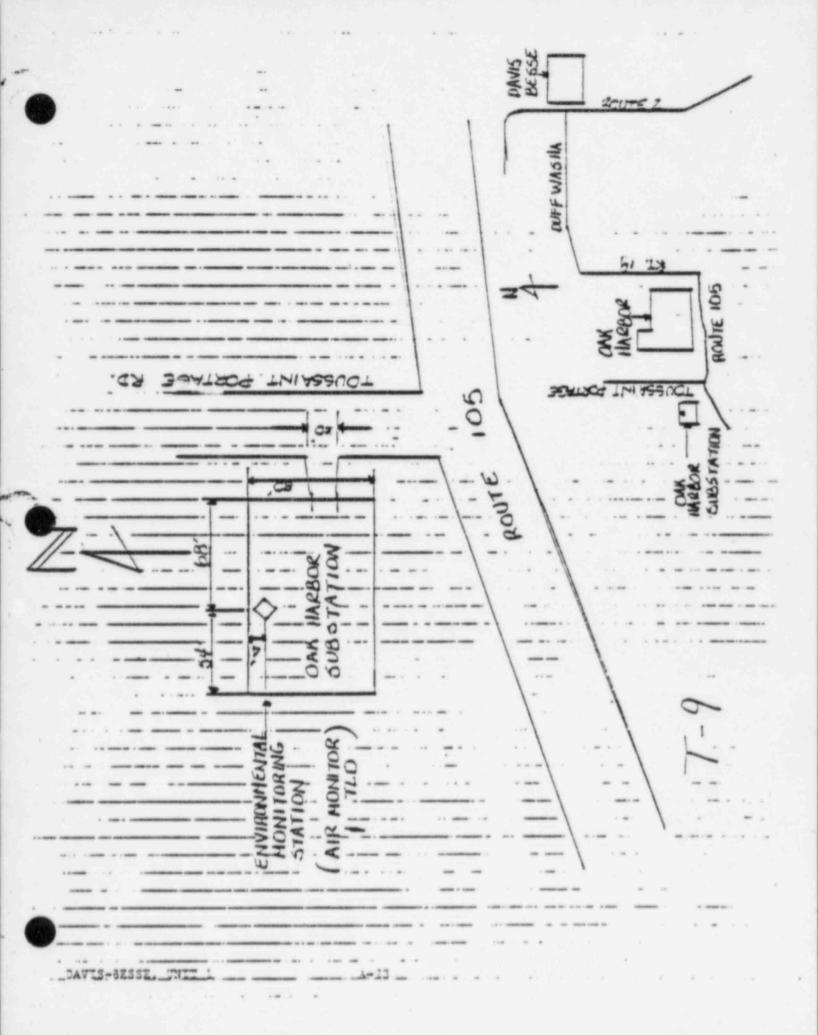


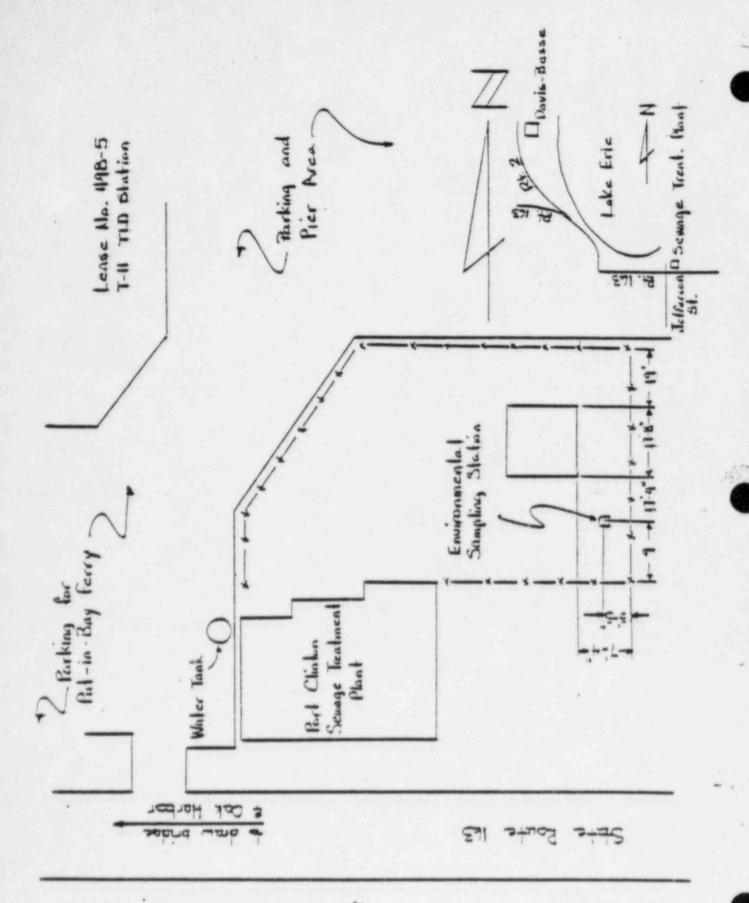
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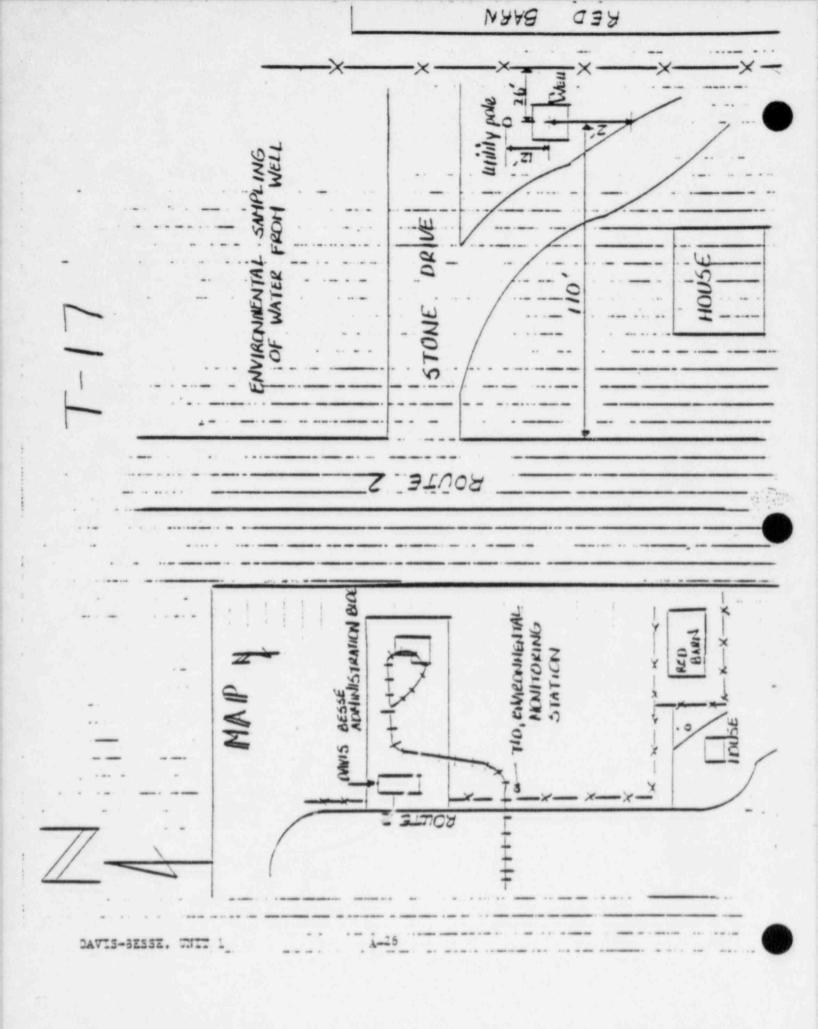
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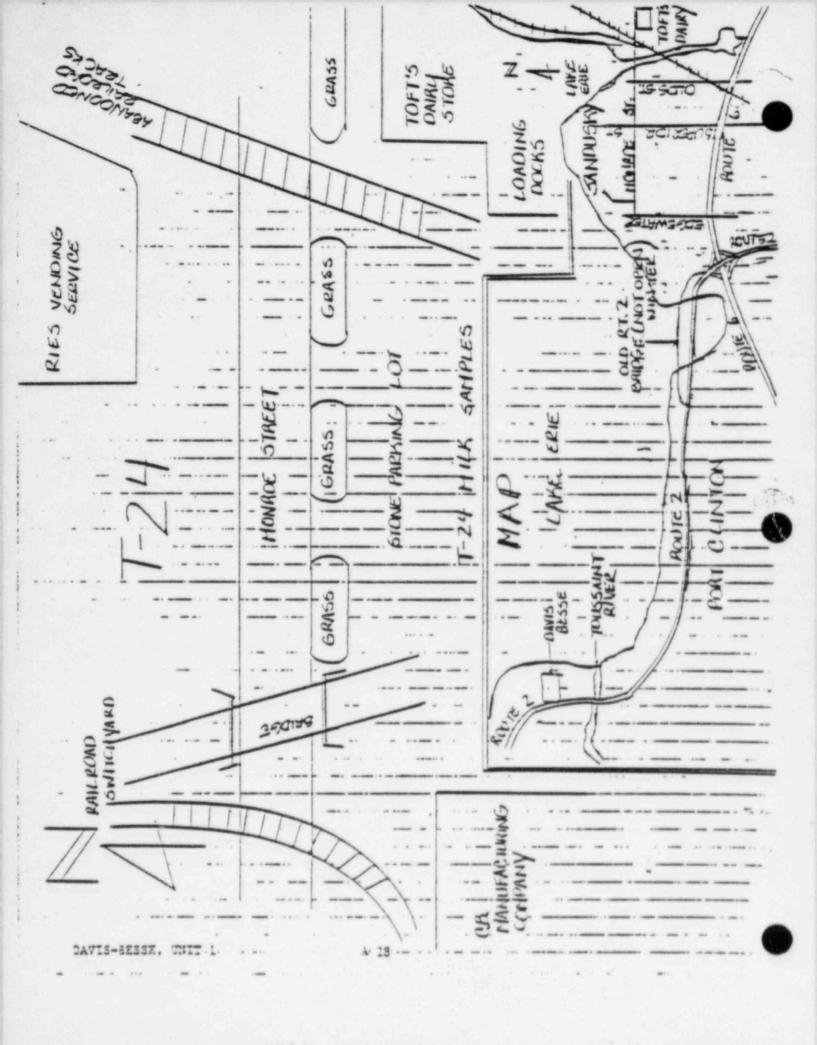


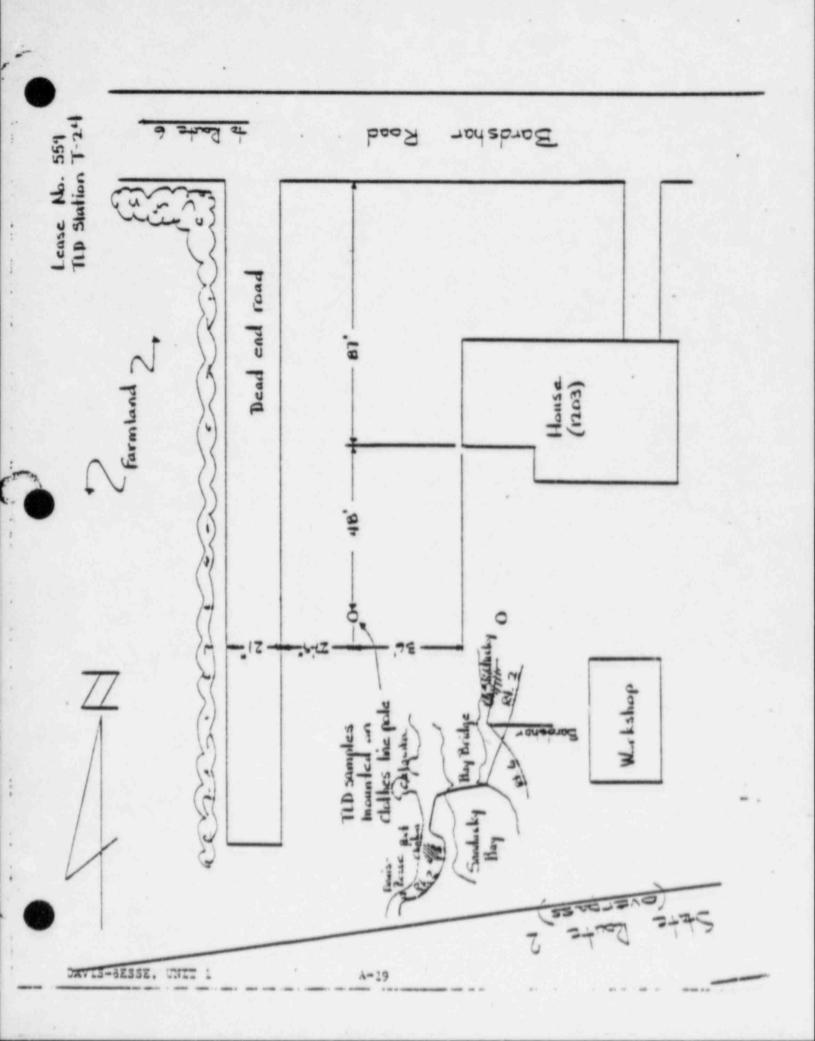


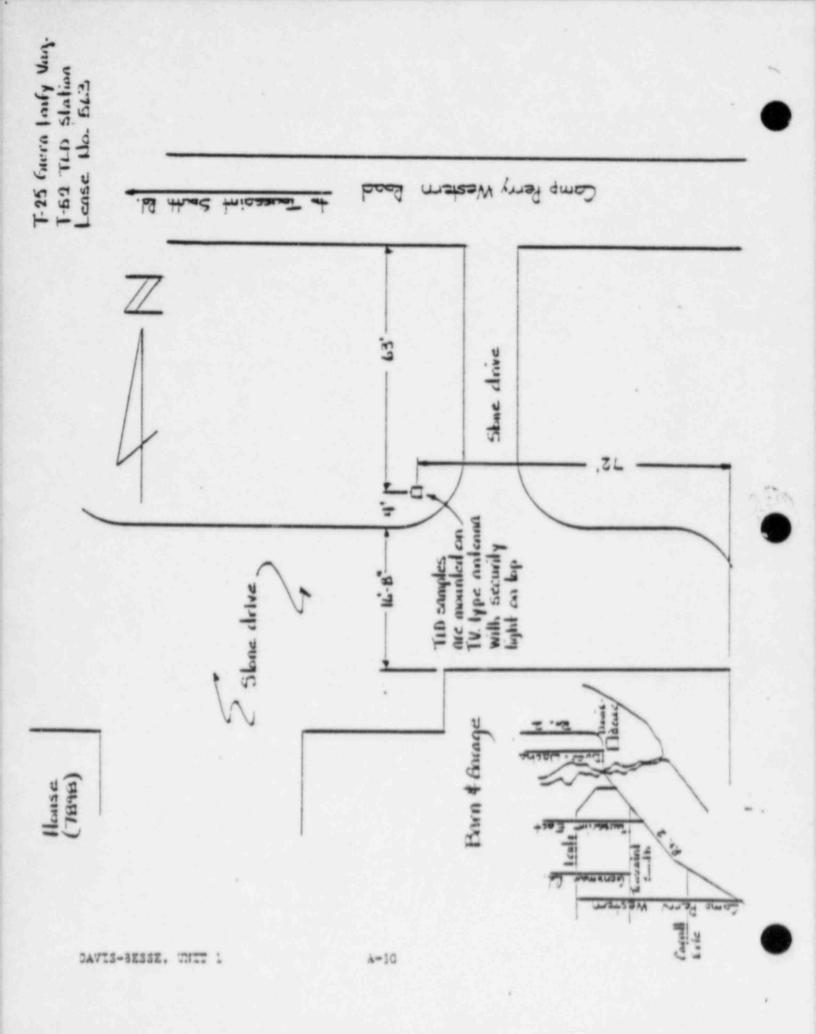


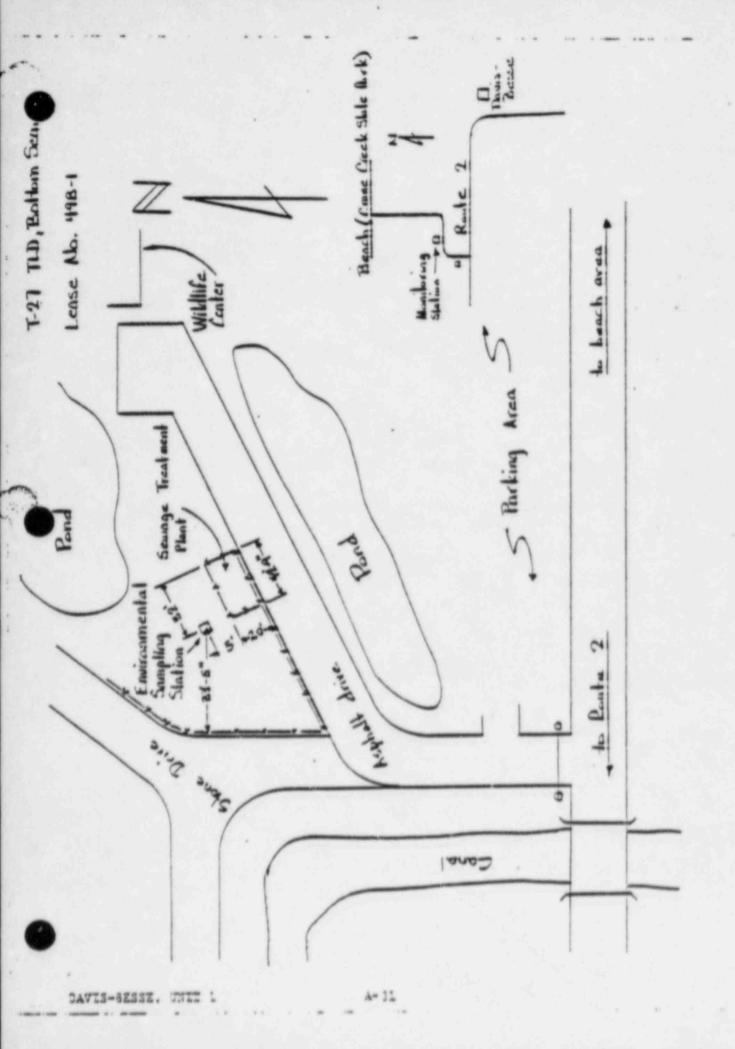
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T-28 Surface Water-Treated

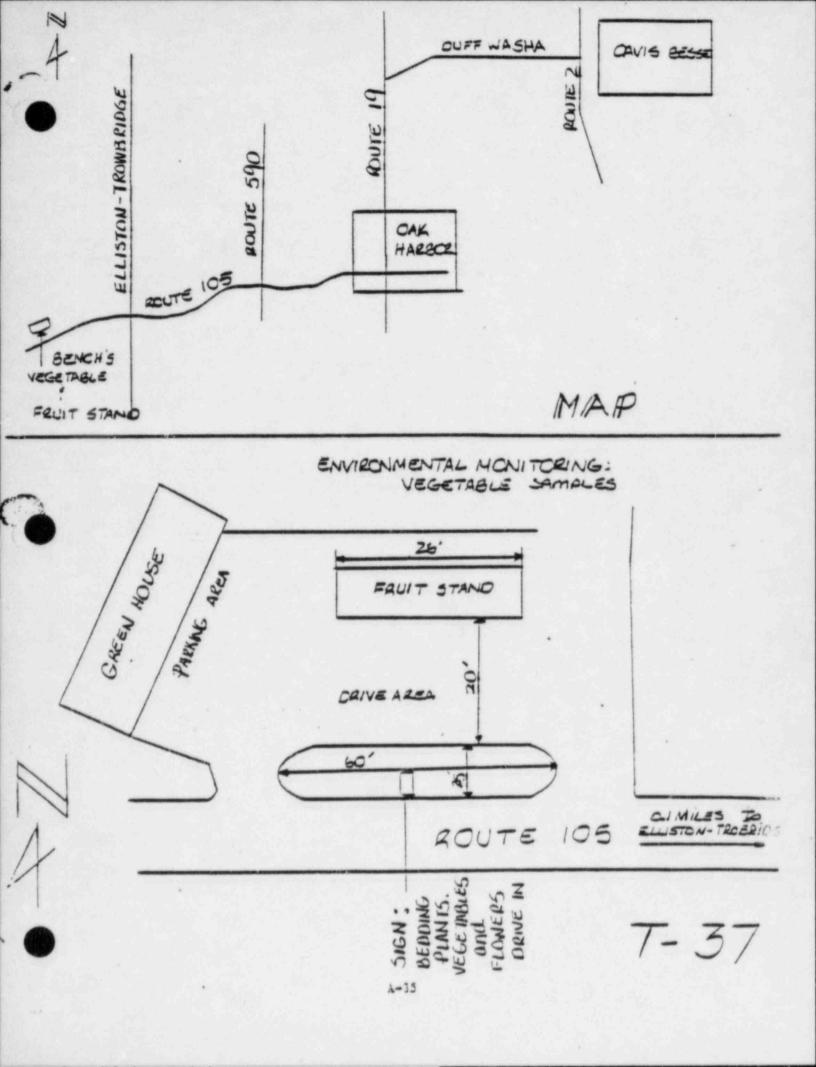
Station is located on-site in the Water Treatment Building.

The Water Treatment Suilding is located within the Protected Area of the Station.

T-33 Fish samples

T-33 is located in Lake Erie within an 8.0 km radius of the site.

T-35 is located in Lake Erie at a distance greater than a 16 km radius from the site.

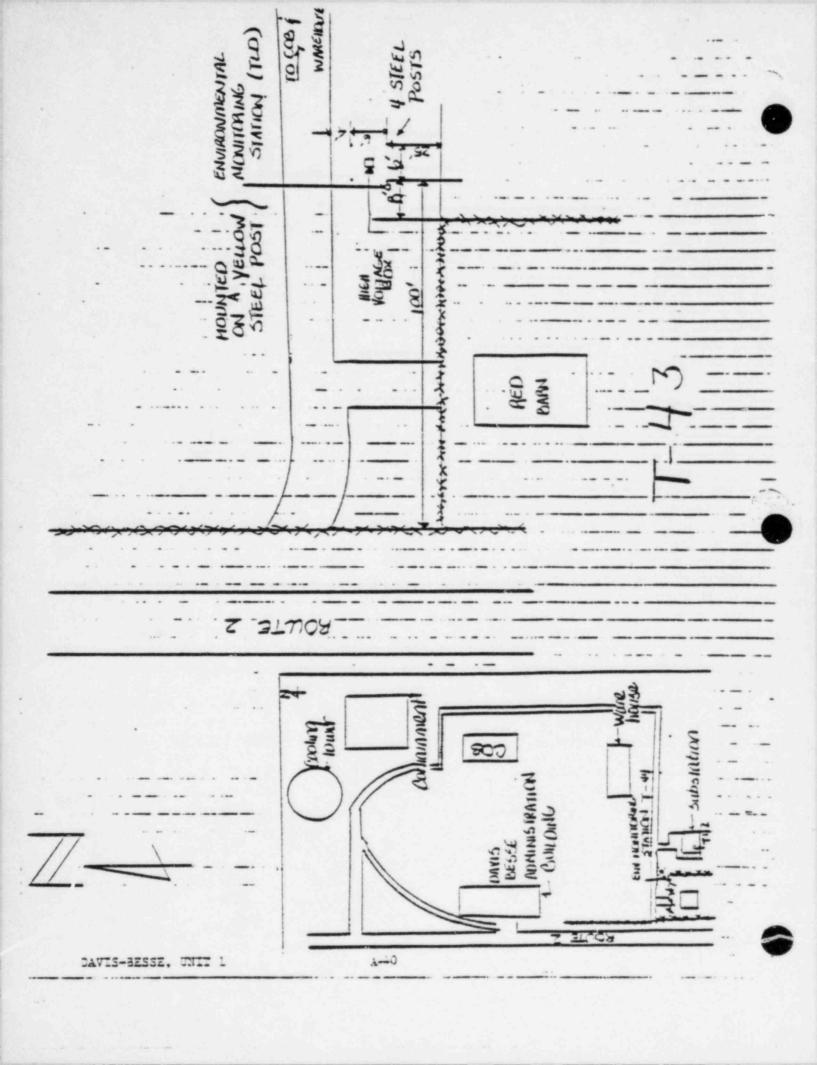


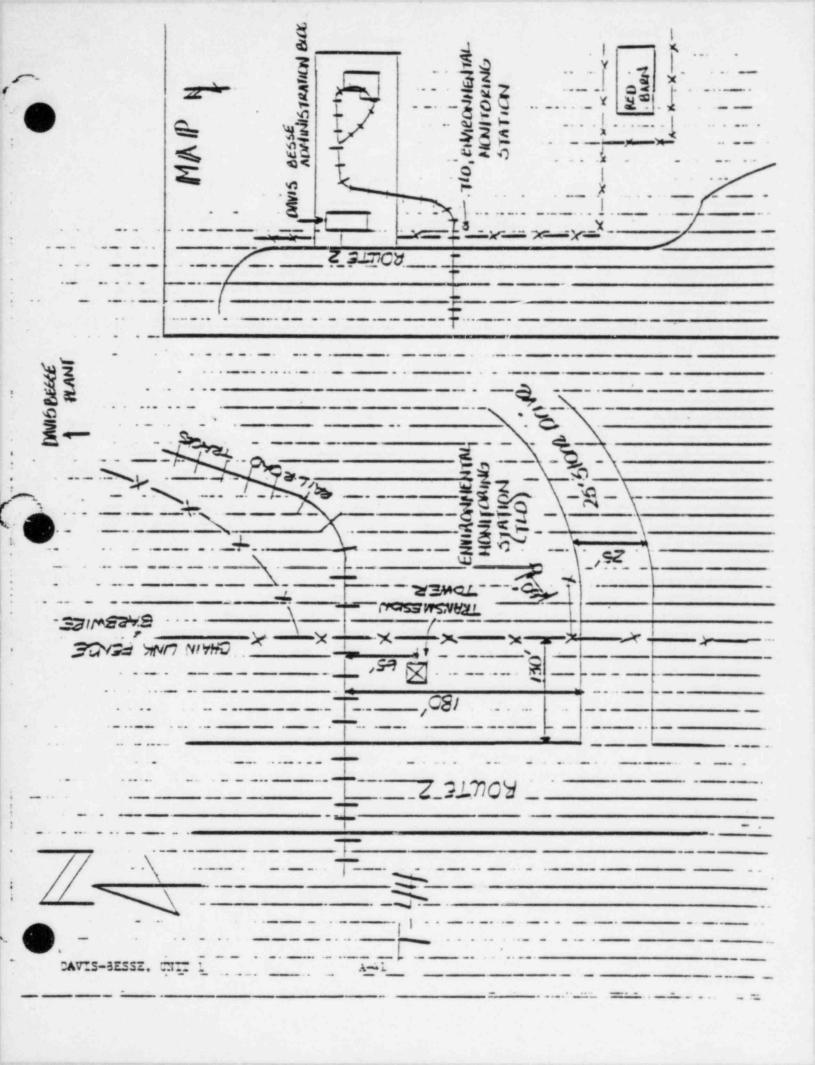
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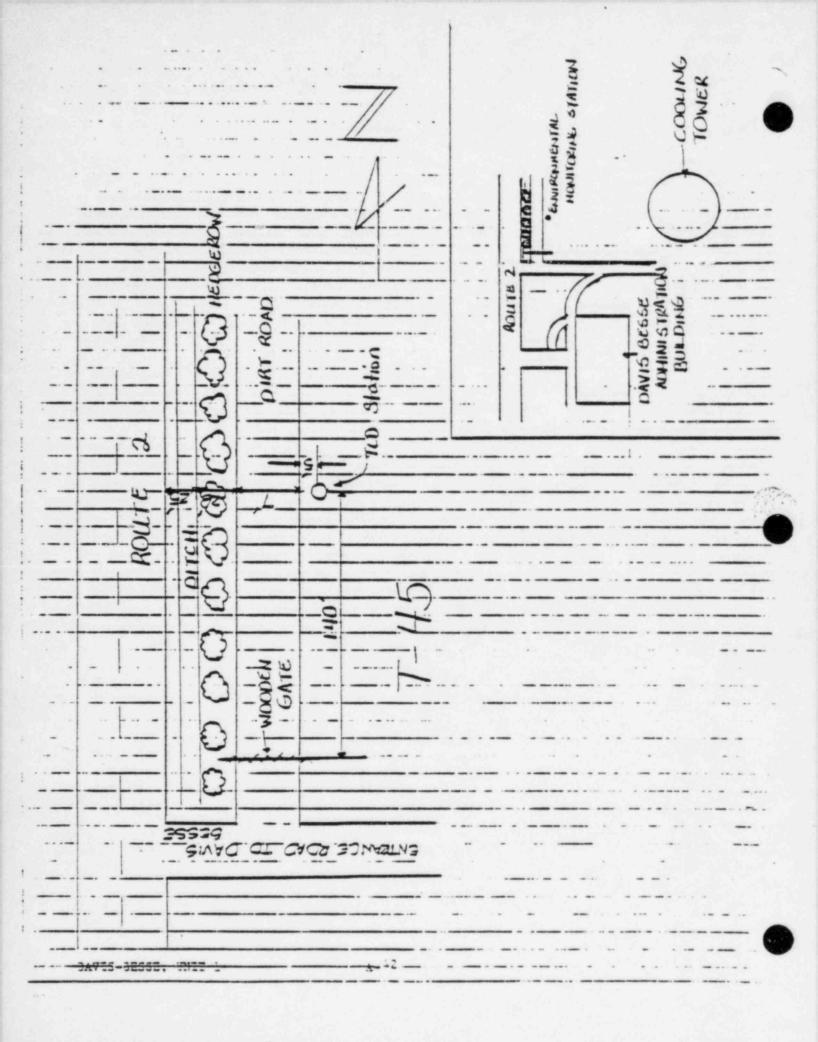
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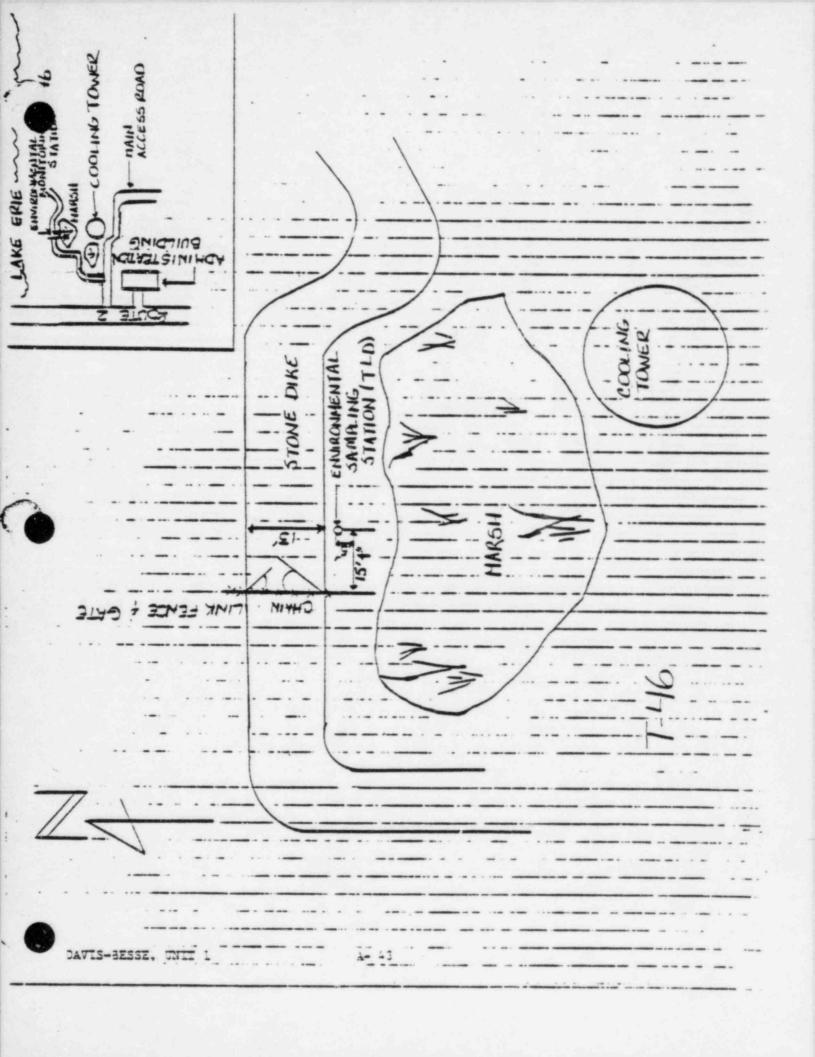
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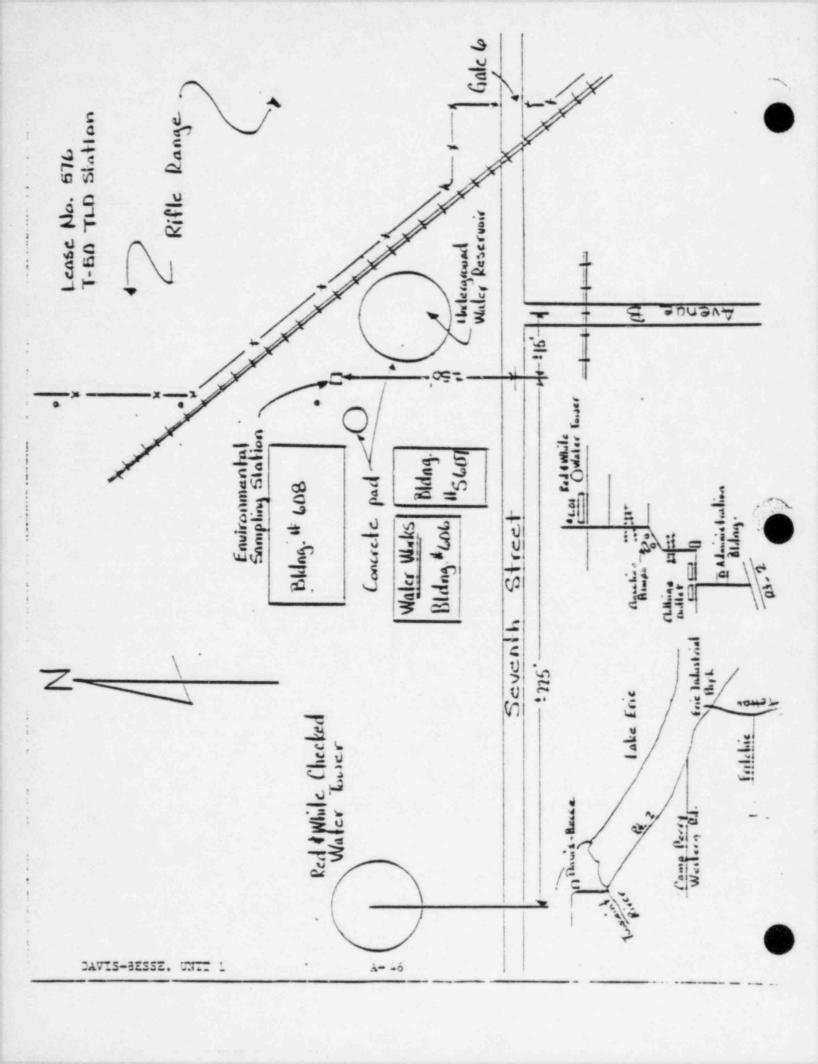


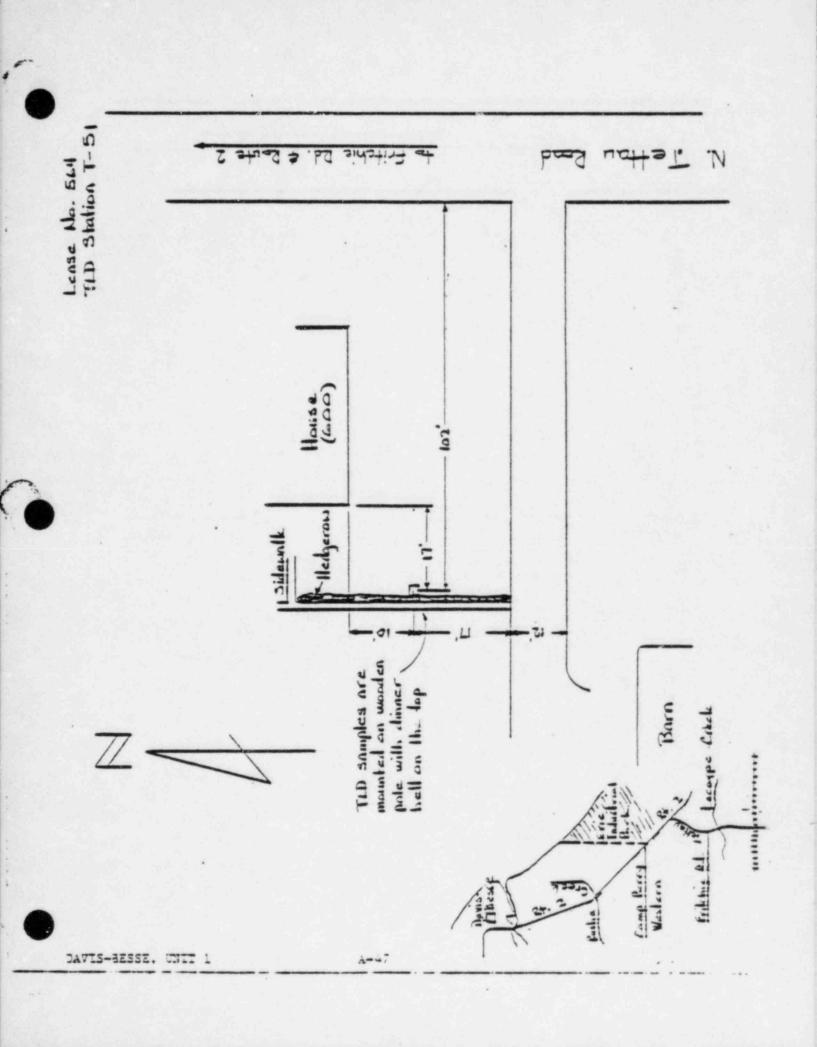
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DAVIS-BESSE, UNIT 1		
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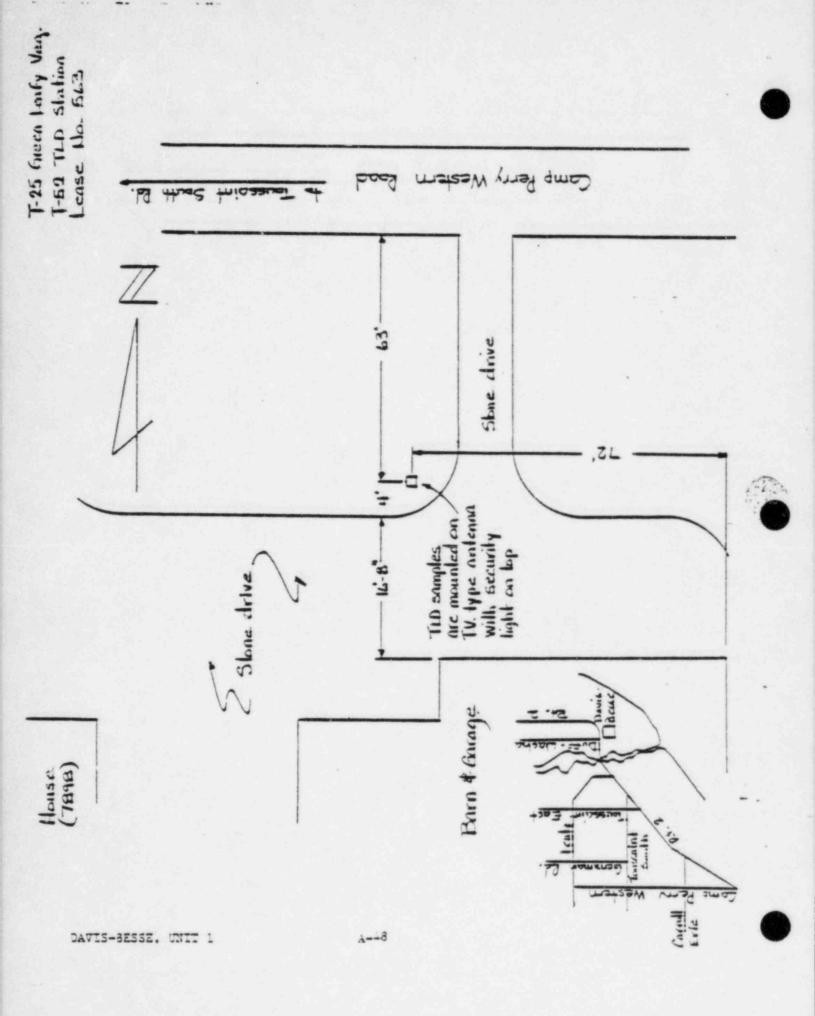
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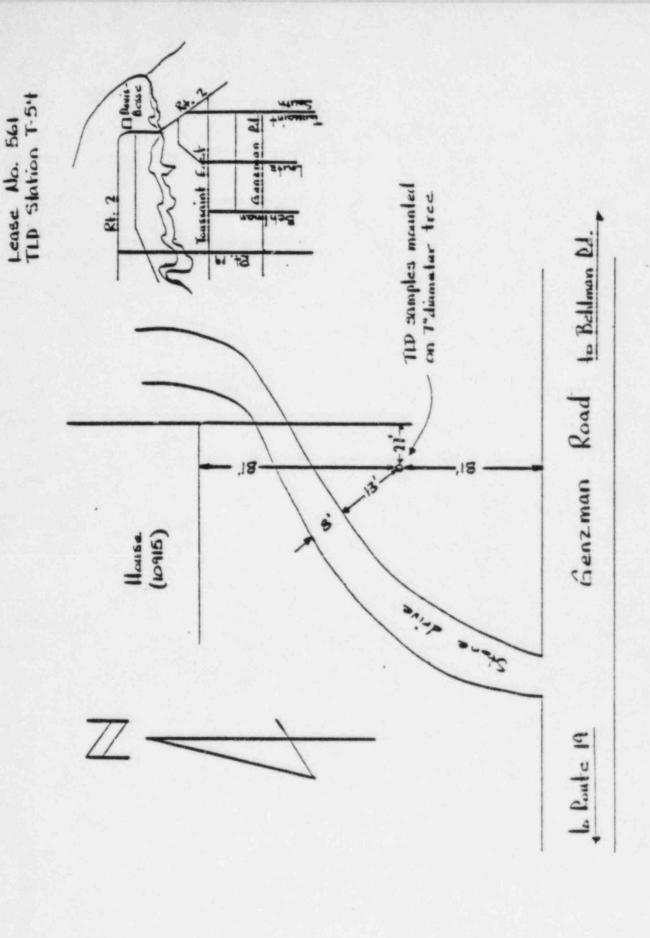
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APPENDIX B

Tables

TABLE 1
BIOACCUMULATION FACTORS
(pC1/kg per pC1/liter)

ELEMENT	FRESHWATER FISH
H	9.0E-01
C	4.6E+03
NA.	1.0E+02
2	3.0E+03
C3	2.0E+02
MIS	4.0E+02
FE	1.0E+02
CO	5.0E+01
NI	1.0E+02
CII	5.0E+01
ZN	2.0E+03
BR	4.2E+02
33	2.0E+03
SR	3.0E+01
T	2.5E+01
ZR	3.3E+00
NB	3.0E+04
350	1.0E+01
TC	1.5E+01
RU	1.0E+01
RH	1.0E+01
TE	4.0E+02
I	1.5E+01
CS	2.0E+03
BA	4.0E+00
LA	2.5E+G1
CE	1.0E+00
79.	2.5E+01
ND	2.5E+01
7	1.2E+03
ХP	1.0E+01

Values in this Table are taken from Regulatory Guide 1.109 except for Phosphorus which is taken from NUREG/CR-1336.

Table 2

Page 1 of 3

[MGESFION DUSE FACTORS FOR ADULES (MREM PER PCI (MGESFED)

TU C	LILE	BONE	LIVE*	F.AGET	DIDRYHIT	KIONEY	LUNG	GI-LLI
+	3	ATAD DM	1.35E-07	1.056-07	1.056-07	1.356-07	1.058-07	1.055-07
:	14	2.246-70	5.048-07	5-486-07	5.485-17	5.486-07	5-088-07	5.68E-07
44	24	1.708-06	1.708-04	1.705-34	1.705-04	1.708-00	1.70E-06	1.705-06
,	32	1.936-04	1.205-05	7.400-00	ATAC DE	NC GATA	NO DATA	2-175-05
23	51	AC CALT	40 0717	2.006-09	1.57E-09	5.306-10	3.538-09	6-69E-07
44	54	AC UATA	4.575-C4	1.725-07	ATAD DP	1.306-00	ATAC DM	1.408-05
	54	NO DATA	1.156-07	2.045-38	NO CATA	1.406-07	ATAC DE	3-675-06
LE		2.756-04	1. 70E-20	4.418-37	NG CATA	NG CATA	1.066-06	1.096-04
a E	59	4.346-Cb	1.625-05	3-915-04	ATAD DE	NG CATA	2.456-06	3.408-05
co	58	NO DATA	7.454-07	1.678-04	NO DATA	NO DATA	NG DATA	1.515-05
CC	00	AC DATE	2.145-00	4.725-06	MO SATA	ATAC DM	ATAD DM	4.02E-05
16	53	1.308-04	7.01E-06	+.36E-36	NO GATA	MG GATA	MG CATA	1.486-04
4 (9.5	5.236-07	9-346-08	3-136-38	NO DATA	NG DATA	MG CATA	1.746-06
cu	34	ATAC DE	8.335-08	3.915-38	HO CATA	2.10E-07	MO GATA	7-108-04
ZN	oż	4.34E-06	1.544-05	a. 706-76	NG GATA	1.036-05	MC GATA	9.706-04
ZN	59	1.036-08	1.975-08	1.375-04	NO DATA	1.286-72	NG GATA	2.966-09
SE	83	4G CATA	40 DATA	4.025-08	40 CATA	NG CATA	NC DATA	9.796-08
BR	34	ALTED DA	NG CATA	5.216-08	ATAC DE	NO DATA	40 DATA	4.096-13
38	35	NG DATA	HO CATA	2.146-39	NO DATA	NO DATA	NG DATA	LT E-24
28	100000	MO CATA	2.115-05	9.336-00	MO DATA	ATAC DM	YO CATA	4. LbE-06
28	18	4C DATA	6.355-08	1.215-08	NG DATA	ATAC DE	LIAC DE	8.366-19
29	39	NO GATA	4.318-08	2.825-38	ATAD DE	NG DATA	NO DATA	2.336-21
SR	39	3-386-04	MC CATA	8.346-36	TIAC DE	AZ CATA	NO DATA	4.946-0
SR	40	7.58E-03	ATAC DM	1.866-03	AD DATE	NO DATA	NO DATA	2.19€-04
SR	91	5.075-05	40 DATA	2.278-77	40 CATA	NG DATA	NO DATA	2.708-05
SR	72	2.156-06	YO GATA	9.305-38	NO DATA	NG GATA	AC CATA	4.20E-05
*	90	9.025-09	NG GATA	2.586-10	ATAD DE	MG CATA	NO DATA	1.025-04
*	91×	7.098-11	NG DATA	3-525-12	NG DATA	NO DATA	NO DATA	2.475-10
4	91	L. +LE-GT	4C CATA	3.775-09	NO CATA	NG DATA	MC CATA	7.766-05
*	92	8.458-10	MG CATA	2.475-11	NO CATA	ATAC DY	ATAE DM	1.446-01

Reference: Regulatory Guide. 1.109. Table E-11

TABLE 2, continued

Page 2 of 3

INGESTION ODSE FACTORS FOR ADULTS (MREM PER POL (1985/180))

AUCTIOE	BONE	LIVER	T.SCCY	THYPOIC	KIONEY	LUNG	GI-LLI
7 93 28 75 28 97	2.446-07 3.346-07	7.75E-09 3.39E-10	7.408-11	NG CATA NG CATA NG CATA	10 0ATA 1.536-08 5.128-10	ATAD DE ATAD DE ATAD DE	1.508-05 3.096-05 1.056-06
48 95	4-228-09	14E-09	1.362-09	ATAD DE	3.428-09	NG GATA	2.10E-05
40 34	NO DATA	4.31E-08	8.208-07		9.766-06	NG GATA	9.99E-06
FC 99#	2-478-10	6.78E-10	3.398-09		1.066-08	3.428-LG	4.13E-07
7C101 3U103 3U105	2.546-10 1.856-07 1.546-08	1-364-E 4740 DF 4740 UF	3.59E-09 7.97E-08 5.08E-07	ATAC DE ATAC DE	6.59E-09 7.06E-07 1.99E-07	NG GATA	1.108-21 2.106-05 9.428-06
10104 46110# 78125#	2.756-06 1.006-07 2.056-06	10 3ATA 1.44E-07 9.71E-07	3.448-07 8.798-08 3.578-07	TO CATA	5.31E-06 1.71E-07 1.09E-05	ATAD DM ATAD DM ATAD DM	1.788-04
78127m	6.778-46	2.42E-04	8.256-07	1.738-04	2.75E-05	ATAD DM	2.278-05
78127	1.128-47	3.95E-08	2.386-08	8.158-08	4.48E-07	ATAD DM	4.085-06
78129m	1.158-45	4.29E-0a	1.425-06	3.958-04	4.3GE-05	ATAD DM	5.796-05
78129	3-1-6-08	1.18E-28	7.45E-09	2.415-78	1.328-07	NO CATA	2.375-78
78131*	1-736-06	8.44E-07	7.05E-07	1.346-36	8.578-06	NO CATA	8.408-75
78131	1-976-08	1.23E-09	4.22E-09	1.425-08	3.638-08	NO CATA	2.795-09
T#132 1 130 1 131	2.525-06 7.566-07 4.166-06	1.03E-06 2.23E-06 5.75E-06	1.536-04 8.408-07 3.41E-04	1.405-06	1.57E-05 3.44E-06 1.32E-09	NG GATA	7.718-05 1.925-06 1.578-06
1 132	2.03E-07	5.+3E-07	1.90E-07	1.908-05	8-65E-07	NG CATA	1.02#-07
1 133	1.42E-08	2.+7E-06	7.53E-07	3.436-04	4-315-76	NG CATA	2.22#-06
1 134	1.08E-07	2.48E-07	1.03E-07	4.996-06	4-58E-07	NG CATA	2.51#-10
[135	4.438-07	1.10d-06	4.29E-37	7.05E-05	1.446-05	1.59E-05	1.31E-06
CS134	6.225-05	146-04	1.21E-34	NO DATA	4.796-05		2.59E-06
CS136	6.518-06	2.575-05	1.85E-35	NO DATA	1.436-05		2.92E-04
CS137	7.978-05	1.69E-04	7.14E-05	NO DATA	3.706-05	1.23E-05	2.11E-04
CS138	5.528-08	1.69E-07	5.40E-08		8.012-08	7.91E-09	4.45E-13
BAL39	9.708-08	6.71E-11	2.84E-09		046-11	1.92E-11	1.72E-03

TABLE 2, Continued

Page 3 of 3
[MGESTION DOSE FACTORS FOR AGULTS
[MGEX PER PC] [MGESTED]

WCLIUS	SONE	LIVER	r.accy	CHANGIO	KIONEY	LUNG	GI-LLI
1141 14141 14142	2.03E-05 4.715-08 2.136-08	2.555-08 3.566-11 2.196-11	1.336-04	ATAG DATA NG GATA NG GATA	8.676-09 3.318-(1 1.358-11	1.40E-08 2.0ZE-11 1.24E-11	4-15E-05 2-225-17 1-005-26
LA142 LA142	2.50E-09 1.28E-10 9.30E-09	1.252-09 5.829-11 5.38-09	3.33E-10 1.45E-11 7.13E-10	NG CATA NG CATA NG CATA	NC DATA NC DATA 2.946-09	ATAD DE ATAD DE ATAD DE	9.258-05 4.258-07 2.425-05
CE1+3 CE1+4 PR1+3	1.45E-C7 4.88E-07 9.20E-09	1.225-06 2.346-07 3.495-39	1.35E-LG 2.42E-08 4.50E-LG	ATAD DE	5.376-10 1.216-07 2.136-09	ATAC DE	4.56E-05 1.45E-04 4.03E-05
92144 10147 4 197	3.018-11 5.296-09 1.036-07	1.255-11 7.275-09 1.818-08	1.5:E-12 4.35E-10 3.01E-78	ATAD DH ATAD DH ATAD DH	7.05E-12 4.25E-09 40 DATA	ATAC DE ATAC DE ATAC DE	4.33E-13 3.49E-05 2.82E-05
##23?	1.176-07	1.170-10	0.45E-11	NG DATA	3.456-10	NO DATA	2.408-05

TABLE 3

SITE-RELATED INGESTION DOSE COMMITMENT FACTOR

ALT

(urem/hr per uCi/ml) Page 1 of 2

"UCLIDE	BUNE	LIVER	TEGDY	THYROTE	KIDHEY	LUNG	31-44
H-2	2.008-01	1.746+00	1.75€+00	1-746+00	1.755+00	1.748+00	1.745+00
C-14	3.13E+04	4.246+93	4-24E+03	4-246+03	1.246+03	4.252+03	1.246+03
44-24	4.322+02	4.322+02	4.322+02	4.325+02	4.325+02	4.322+02	*.322+02
08-51	0.00€-01	0.00€-01	1.312+00	7.856-01	2.896-01	1.775+00	1.10€+02
**-54	0.00€-01	4.44€+03	8.48€+02	0.00€-01	1.325+03	7.00€-01	1.346+04
HH-54	0.006-01	1.125+02	1.988+01	0.00€-01	1 . 42E+02	0.00€-01	3.57€+03
FE-53	5.798+02	4.33E+02	1-13E+02	0.00€-01	0.00€-01	2.49€+02	2.778+02
2E-20	1.106+03	2.59€+03	9.93E+02	0.008-01	0.00€-01	7.246402	9-446+03
00-68	0.00E-01	1.00€+02	2.24€+02	9.00€-91	2.00€-21	2.00#-01	2.038+03
00-40	0.00€-01	2.878+02	6.34€+02	9.00E-01	0.00E-01	0.008-01	5. 10€+03
HI-59	2.462+03	8.51E+02	4.146+02	0.00€-01	0.00E-01	0.00€-01	1.758+02
Ke-18	3.30E+04	2.29€+03	1.112+03	0.006-01	0.00€-01	1.00€-91	4.79€+02
HI-65	1.346+02	1.74€+01	7.952+00	0.00€-01	0.008-01	1.00E-11	4. 422+02
CU-64	0.006-01	1.122+01	5.25E+00	0.006-01	2.325+01	0.00€-01	*.54E+02
24-45	2.322+04	7.40€+0+	3.346+04	0.006-01	4.952+04	7.00€-01	4.446+04
9R-94	0.008-01	0.006-01	5.312+01	0.00€-01	0.00€-01	0.00€-01	4.178-04
29-48	0.00€-01	2. *1E+02	1.546+02	0.008-01	0.00€-01	0.00€-01	4.01E-99
28-49	0.008-01	1.932+02	1.338+02	0.00€-01	0.006-01	0.006-01	1-128-11
5R-39	2.446+04	0.006-01	7.446+02	9.00€-01	0.00€-01	0.00€-01	4.278+03
5R-#0	4.552+05	0.00€-01	1.415+05	1.008-11	0.00€-01	0.006-01	1.89€+04
14-45	4.908+02	0.008-01	1.996+01	0.00€-01	0.00€-01	0.00€-01	2.33E-03
98-42	1.846+02	0.008-01	8.04€+00	0.006-01	0.00€-01	0.00€-01	3.488+03
Y-49	7-146-01	0.008-01	1.925-02	0.00€-01	1.00€-01	0.00E-01	7.59€+03
791H	6.77E-03	0.008-01	2.425-04	0.00€-01	0.00€-01	0.008-01	1.000-02
7-45	1.052+01	0.00€-01	2.818-01	0.00€-01	7.00€-01	0.00€-01	5.79E+03
Y-42	6.298-02	0.00€-01	1.846-03	9.00€-01	0.00€-01	0.00€-01	1.106+93
79-45	5.34E-01	2.19€-01	1.498-01	0.008-01	1.44€-01	0.002-01	1.995+02
28-07	1.788-02	7.43E-03	1.496-01	0.00€-01	1.155-02	1.30€-01	2.246+03
48-05	4.478+02	2.495+02	1.34€+02	0.00E-01	2.446+02	7.09E-01	1.515+04
+8-47	0.008-01	0.00E-01	0.00E-01	0.00€-01	0.30€-01	0.008-01	2.475+07

Calculations made according to the methods specified in Section 1.2 of the Offsite Dose Calculation Manual

TABLE 3 (continued)

SITE-RELATED INGESTION DOSE COMMITMENT FACTOR

Alt (mrem/hr per uCi/ml) Page 2 of 2

HUCLIDE	304€	LIVER	LEGGA	THYRGID	KIDHEY	LUMG	SI-LLI	
HQ-44	0.006-01	1.446+02	1.14E+01	0.00€-01	3.77E+02	0.008-01	1.85E+02	
TC99H	1.258-02	1.538-02	4.498-01	0.00€-01	5.35E-01	1.738-02	2.098+01	
20-103	7.13E+00	0.00E-)1	3.07E+00	0.006-01	2.725+01	0.00€-11	3.322+02	
2U-104	1.006+02	3.00E-31	1.34€+01	0.006-01	2.05E+02	1.00€-01	5.34E+03	
46110H	1.222+00	2.986+00	1.775+00	0.00€-01	5.85E+00	1.00€-01	1.216+03	
CD115M	0.008-01	9.088+02	2.472+01	0.006-01	7.208+02	0.30€-01	1.825+04	
58-124	4.78E+01	3.50€-01	1.89€+01	9.00E-91	0.00€-01	3.70€+01	1.352+03	
TE-132	2.45E+03	1.586+03	1.496+03	1.752+03	1.53F+04	0.00€-01	7.506+04	
1-131	2.102+02	3.01E+02	1.725+02	*.85E+04	5.15E+02	7.008-01	7.93E+01	
1-132	1.03E+01	2.74€+01	*.40€+00	+.40E+02	4.375+01	0.00#-01	5.15E+00	
1-133	7.175+01	1.258+02	3.80€+01	1.83E+04	2.186+02	0.00€-01	1.121+02	
1-134	5.355+00	1.45E+01	5.20€+90	2.525+02	2.316+01	0.00€-01	1.278-02	
:-135	2.246+01	5.846+01	2.14E+01	1.848+03	4.395+01	0.00€-01	5.422+01	10
C3-134	2.99€+05	7.112+05	5.312+05	0.00€-01	2.30€+05	7.446+94	1.248+04	-
C3-134	3.13E+04	1.238+05	8.888+04	0.00€-01	4.378+0+	*. 41E+03	1.40€+04	1
03-137	3.83E+05	5.23E+05	3.43E+05	0.008-01	1.798+05	3.715+04	1.012004	
03-138	2.45E+02	5.238+02	2.59€+02	0.00€-01	1.852+02	3.80€+01	2.238-03	
03-139	1.446+02	3.40E+02	+.80E+01	0.008-01	1.925+02	0.00F-01	7.00E-01	
8A-139	2.35E+00	1-478-03	6.87E-02	0.00€-01	1.54E-03	7.48E-04	4.146+00	
3A-140	4.712+02	0-16E-01	1.222+01	0.00€-01	2.10#-01	1.538-01	1.018+03	
LA-140	1.24E-01	*.18E-02	2.48E-02	0.008-01	0.008-01	0.00€-01	6.89€+03	
CE-141	1.598-01	1.088-01	1.228-02	0.00E-01	5.008-02	1.00€-91	***115+02	
CE-143	2.30€-02	2.07E+01	2.294-03	0.00€-01	9.13E-03	0.30€-01	7.752+02	
GE-144	3.275+00	3.478+90	4.45E-01	0.008-01	2.04€+00	0.000-01	2.30€+03	
	2.246-03	9.31E-04	1-146-04	9.00€-91	5.22E-04	0.00€-01	3.221-10	
4-187	2.978+02	2.446+02	9.498+01	0.00€-01	9.008-01	0.008-01	9-146+04	
11-222	1.558+04	0.306-01	*.42E+02	7.008-01	1.438+03	1.00€-01	1.515+03 -	
11-238	1.498+04	7.008-01	1.822+02	0.00E-01	1.3*4+03	0.008-01	1.225+01	
49-239	4.596-02	4.51E-03	:.49E)I	2.008-01	1.416-02	0.00€-01	*.25E+02	
P-12	1.398+06	5.44€+04	5.378+04	0.008-01	1.008-01	0.00€-01	1.546+05	

TABLE 4

DOSE FACTORS FOR EXPOSURE TO A SEMI-INFINITE CLOUD OF NOBLE GASES

Nuc11de	y-Body ** (K)	s-Skin=*(L)	-Air*(M)	8-41r*(N)
Kr-85m	1.17E+03***	1.46E+03	1.23E+03	1.97E+03
Kr-85	1.675+01	1.34E+03	1.72E+01	1.95E+03
Kr-87	5.92E+03	9.73E+03	6.17E+03	1.03E+04
Kr-88	1.47E+04	2.37E+03	1.52E+04	2.93E+03
Kr-89	1.662+04	1.01E+04	1.73E+04	1.06E+04
Kr-90	1.56E+04	7.29E+03	1.63E+04	7.83E+03
Xe-131m	9.15E+01	4.76E+02	1.56E+02	1.11E+03
Xe-133m	2.57 E+02	9.948+02	3.27E+02	1.48E+03
Xe-133	2.948+02	3.06E+02	3.53E+02	1.05E+03
Xe-135m	3.12E+03	7.11E+02	3.36E+03	7.39E+02
Xe-135	1.815+03	1.86E+03	1.92E+03	2.46E+03
Xe-137	1.425+03	1.225+04	1.51E+03	1.27E+04
Xe-138	8.83E+03	4.13E+03	9.21E+03	4.75E+03
Ar-41	8.84E+03	2.69E+03	9.30E+03	3.28E+03

Reference: Regulatory Guide 1.109 Table 3-1 and Section 2.1.1 of the Offsite Dose Calculation Manual

^{*} mrad-m3

mem-m3

^{1.97}E+03 = 1.97 x 10³

TABLE 5

Page 1 of 12

(Por Section 2.2.1.b, units in mrom/year per pC1/m3).

EKIN CKITICAL	103	000E-01 W. E0b	-01 FOR	10-	ū	10	10	00 H - 01 11816		1 10	1 10	10	311 10	to	3	GOOD OF LINE	01		01 110	CCOL 61 LIVER	10-	10	10	1	T	10	000E-61 LINE	01 111	11 10 10 3000	
81-111 EX		104 0	440E101 0.	2.581E105 0.6	101 0.	104 0.	104 0.	6.64.3 403 0.0	16: 0	100 0.	10.1 0.	101 0.	164 6.	P.E. 164 U.	111 104 0.	0.0 101 E.2.1	010	0 10	1.554 101 6.6	07 0.	12 0,	100 0.	100 0.	102 0.	104 0.	103 0.	1.3.30 100 0.0	10: 0	7.35 ± 101 0.0	
01811	1.2546103	1.024E104	3000	0.000E-01	1.41CE 104	1.400E105	9.4406133	7.20mm 104		BALLE I	4.5401 101	-	-	TOTAL .	-	0.000E 31	0.666E-01	0.000E 01	0.60CE-01		x	-	-	3.6401.104	-	-	1.9201103	-	1.5501.104	7401.104
KIMEY	1.2446103	1.024E104	1.30	0.000E103		-	-	0.000		E	4. COOE - 01	Æ.		-	401376FT94	0.0006-01	T.	J.R	0.000E-01	1	1	0.0001-01	T.	T.	F	Æ.	T	1	0.000	- 4
LIVER	1.2546103	-	-	8.530E165	T	-		3.77.6104		15.3E1	1.1400.134	-	X :			0.000E 01	SOUF	6.000E-01	1.35.3E 105	-	-	T.	T.	T	Ŧ.	T.	Ī.	F.	0.000E 01	*
BONE	10-3000.0	1.0246104	1.3306104	-	T.	E		1.1745.104	3000	0.000E 01	-	-	-		3.2400.104	0.0001 01	0.000E 01	0.036E	0.000E-01			-	-	-	-	-			0.4405.00	
IIIYRIII	1,2546103	1.0246 164	0.COUF -01	L	5,953E101	0.0001-01	Ŧ.	0.000E 01	J	0.000E-01	0.00ct 01	3.	J.	T.	0.000.0	3.000E-01	0.0ccf 61	0.000l 61	C. 030E 01	1	I.	T.		I	Ŧ.	Ī.	Ε.	To 1	0.0004 01	
W. PORT	1.2541 '03	-	-	-	-	-		1.0546.104	-	1. 1113E 104	5.4121.103	-	т.	T :		2. 16:4 103	1.1 '0' 133	1. : HOE 161	5,8921 164	-	-	-	-	-	T	-	-	-	3.015t 01	
FATHMAY I FINIALAL	11-3	NA-24	F-32	14. 45	CK 51	Mil De	10 IN	1 20	E0 58	1.11 2.0	87 III	HI .3	H 25	+7 17	6.5 6.3	M: 63	fix nd												1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	

TABLE 5 (CONT)

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(For Section 2.2.1.b, units in mrem/year per pC1/m)

AGE I AME I FATHMAY I IMMA ATTOM

Ξ	=	3-01091 m	ż	PODA	HITKELLE	BUNE	LIVER	1 TONE Y	TIMO	177-10	BK IN	CKITICAL
3.5	111	6.42	4.30	10.1 3D	0.000E 01	1.40BE 104	7.815E103	7.735€103	5.0488 105	*	-	TUNG
37	215	16-13	2.0	18	å	2.2346-01	5.424E-02	4	2.400E 103	2.414F 102	0.000E-01	Linns
Jul	rtit	66-1	3.39	E	0.000E	0.000E-01	1.200E 102	1.2E	9.120E104	. *	0.00GE-01	01-111
3.7	-	1166-3	3.76	=	0.030E-01	1.033E 03	2.9131 03	4.414E-02	7.64JE102	4.140E103	0.000E-01	111-10
300	11	101-3	2.96	- 31	0.000E-01	30	4.016E-65	1.000E 03	. 993E 1	1.04mf. 11	Æ	Luni
41	N	101	4.50	11	0.000E 01	1,520£103	0.000E-01	5.U32E103	5.04BE105	1.1040105	0.000E-01	1.1916
4.2	124	501-1	3.11	10 11	0.000E-01	7.994E-01	0.000L-01	1.014E100	1.095E104	4.012E104	0.000E-01	111 19
4.5	2	701-1	11.7	30E 103	10-3000.0 1	4.913E104	0.000E-01	1.3321.105	9.350E105	-		1. (101/5)
+	3	HO11-	2.0	146 103	10.50cf.01	1.0604 104	1.000E 101	1.95UE 104	4.432E104	3.024£ 105	T	111111
4	7	MEII A	4.3.	E01 105	0.000E 01	0.000E-01	1.94th 105	1.584E105	1.400E105	3.840E 105	0.000E 01	Limit
4.4	III	b-124	1.3	101:104	7,553,8101	3.120E104	5.6huE 102	0.000F 01	2.400E 104	4.054£ 165	0.0001 91	1 111411
47	=	1-125M	4.5	11	1.014610.1	1 3.412E 103	1.584E103	1.2401 104	3.135E105	7.034E104	0.000E 01	1,11110
411	=	1.127H	-2	LIE 103	3.3cbt 103	1 1.24-16104	5.75HE 103	4.5748104	9.400E 105	1.475E 105	0.000E-01	1 (1110)
4.9	=	1.137	3.0	10 TO	1.3524 100	1.400E100	4.42 11 -01	5.092E 103	4.5131103	5.735E104		01-111
202	1	L-129M	1.5	14E 103	1 3.440E163	1 9.750E103	4.672E103	3.656E164	1.140E 104	3.632£ 105	0.000E-01	1.1116
77	=	1.129	1.3	101 02	3.87.E 02	1 4.975E-02	2.39.E 03	1.6735-01	1.9354 103	1.5400 103	0.000E-01	1.1910
	=	E-13116	2.9	101310	5.50 1E 101	1 4.972E101	÷	3. ubue 102	1.456E105	5 Jisot 105	T	111-111
3	=	1111	3.5	-	1 9.350E 03	30	12	4.35BE-02	1.392E103	1.840£101	0.000E-01	1111111
4.5	=	1.132	1.6	156 102	1.892E103	2.400E103	2,1531102	1. (55E 103	2.800E 105	\$.692E105	0.00GE-01	111-19
25.5	-	130	5.3	10E 103	1.1351105	4.5746103	1.344E104	2.000E 104	0.000E-01	7.40HE 103	0.000E-01	HITCHIE
47	-	121	2.0	1:11 104	1.1935107	7 2.530E104	3.574E 104	4.120E104	0.000E-01	4.200E101		HIYF01D
12.	-	133	1.1	50E 103	1 1.144E105	1.140E103	3.254E+03	5.1846103	0.0035-01	4.05-11:102	0.000E 01	UNKUID
9::	-	133	4.5	201 103	-	-	-	-	0.00CE-01	-	- 60	HYKBIP
5.5	-	134	5.1:	5.3E 102	2.901E 104	1 4.440E 102	-	2.753E103	0.000E-01	1.001# 100	T	HYKOH
0.0	-	1.35	1.5	LUE 103	4.44GE105	2.4HOE 103	3.981E103	1.113E 104	0.0006-01	5,2404 103	T	HYKUID
77	3	1-134	7.3	COF 105	\$ 0.000E-01	3.720E105	0,400E105	2.073£105	9.740E 104	1.0101.04	0.000E-01	1.17.14
4			1.1	61E 105	0.000E 0	1.904E104	1.454E105	0.5302104	1.2000.104	1.16 11:101	0.000£ 01	1 141
5.03			4,23	201.105	0.000E 0	4.784E105	6.200E 105	2.234£105	7.520E104	8.400£103	0.000E-01	LIVER
2.4			3,3	101.102	0.000E-01	1.312E102	A. 200E 102	4.1000E #	1.8551.101	1.051E 03	0.0006-01	LIVER
177		- 1	1.1	13E 103	0.000E 0	2.04fil 102	2.904E102	2,4406 103	2.373E101	0.000E 01	0.000E 01	LINER
44		4	2.7	15E 02	0.000E 0	19.350E-01	4.455E-04	4.224E 04	3.740£103	P.940E102	10-3000'0	Linn.
-			2.5	11	10.0001	-	4.904E101	-	1.272E104	3. 114E 105	1	Links
77	PA I	A-141	3.35	OF.	1 0.000E 01	130	7.52BE-05	7.000E	1.935E t03	1.140E 07	T	Lunis
4.5			7.1	37	10.000.01	T	2,7346 05	I	-	1	1	Linni
20			4.25	1111111	10.66UE 01	3.440E102	1.736E102	0.000E-01	1.350£ 105	4.584E105	0.000E-01	01-111

TABLE 5 (COUT) Page 3 of 12

(For Section 2.2.1.6, units in mrem/year per pict/m3).

FATHANY I INIVACITOR

COLLEGE	THE LANGE	Lind	Limb	01-111	1.1884.3	1.100%	LIMIG	LUMB	Linio				171-17
CAL WAS	the state of	7.720E-02	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.030E-01	0.0001-01	0.030E-01	0.000E-01	0,000E-01	0.0036-01	0.000E-01
		2.112E103	3.414E105 1.200E105	7.976E104 2.254E105	B.146E105	2.000E 105	2,153E - 0B	1.730E105	4.454E105 8.520E104 0.	2.904L104 1.552E105	3.920E100 3.073t 105	1.444E100 8.240E105	1.192E 105
	7	4.328E103 3.112E103 7.720E-02	3.416E105	7.976E104	7.776E104 1	2.808E105	1.015E103	2.200E105	4.455E105	2.9041.104	3.920E100	3.444E100	7.000E101 3.740E104 1.192E105 0.000E-01
V. T. Same V	V S PORT	0.000E-01	1.352E104 4.264E103	4.000E101	8.480£ 105	3.140E103	7.040E-03	3.550E 103	0.000E-01	0.0001 01	1.0735107	1.744E107	7.000E101
0.2002	LIVER	3.104E-01	1.352E104	1.374E102 4.000E101	1.432E104	9.340E103 3.752F103	1.2181-02	5.272E103 4.095E103	5.174E162	7.080£100	8.000E107 0.060E-01 1.U73E107	0.000E-01	2.254E 101
Trepret .		.0.121-01	.992E104	.84E102	3.432E 104	9.360E103	3.00BE-03	5.272E103	1.540E103 5.174E162 0.000E	0.480E100	4. U.S.E 105 0.000E-01 0.000E 107 0.000E-01	7.444E107	2.294E 102
THEOREM	1	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.00CE 01	0.000E-01	0.000E-01	6.000E-01	3.000E-01
A Linky		7.7:04-02	1.520E103	1.528 101 0.000E-01 1	1.01 40E 103	4.640E102	1,5300-03	3.4401.102	5, 4 101 101	2, 400£ 100	4. US. SE 105	4.5.32E 104	1013012.1
300000	The state of the s	A-143	E-141	73 08-143	E-144	14.143	141	110-147	201-1	7111-1	11 235	01:310	11. 259
		-	-	-	-	-	-	-	-	-	-	-	-

TABLE 5 (CONT) Page 4 of 12

(For Section 2.2.1.b, units in mrem/year per pCt/m3).

AUL I TEEN FATHBAY I IMBALATION

-	NO ISOTORE	u. pant	HYKOID	FONE	LIVER	KIMEY	LUNG	01-111	EN IN	CRITICAL	
-	-	1.2726103	1.272E103	0.000E-01	1.272£103	1.272E103	1.3735403	1.3725101	1.3736403	to forms	
	14	4.872E103	4.872E103	. 400E	872E		873E1		3028	- 4	
-	1-24	1.3756104	-		37/2	1.374F 104			2000	the English	
	32	7.140E104		-			. 1		1000	Four Dubi	
-	45	3. 40HE 105	Ŧ	-	540F		DOOR		1000	Denie.	
100	15-3	1.353£133	-	000E	- 4000		0015	2 6606 107	0.000	HALK	
700	4:24	B. 400E 103	· T	- 1				1007			
100	1-54	3.530£ 01	17	1	19767	• •	0013001		1	11111	
700	FE 25	5.5116103	- T	***		• 1	•	A. 1001 101	0.000E	1 1 1 1 1	
-	62.3	1.4131.104	0.000E 01	-	-	3				1100	
795	9 28	3.772E104		1	-	I	-			I town	
-	05.0	1.5.146.101	0.000E 01	0.000E-01	1.5126104	1	-	-	1	111111	
	67	5.4135.103	T	-	-	T.	-	-	T	Links	
	-2.5	1.974104		-	-	0.000E 01	3.072£105	1.41ct 164	1	FOLIE	
	00	1.37.1 01		-	- th.	0.000E-01	9.350E 103	3.472E104	T	111.19	
MR 1	1 24	8.4110E 61	T.	E	2.033£100	5.468E100	1.1135104	5.111E104	6.000E-01	177-19	
-	27.7	4.240E 104	1	-	-	-	-	4.6511104	T	Luni	
-		6. 135E 03	1	T.		I	-	-	8.	Time?	
- N	600	3. 440E 102	T.	T	T	Ī.	T	T	0.000E-01	W. folloy	
40.00	100	4.3.38.80.4		F.	1	J.	T.	Τ.	1		
- A	70	1.83.1.101		Ī.	4	I.	T	0.000E-01	0.000E-01	W. John	
-	400	B. 400E 104	L	T.	-	A.	0.030E-01	*	. 1	LIME	
-	000	2. / :: OE 10:	0.000.0		5.454E 102	Z.	1	2.920£ -05	0.00CE-01	LIVER	
-	200	201 1107	-	1 1	-	T	0.000E-01		0.000E-01	LIME	
-	200	101		-	F	*	-	3.713E 105	0.000E-01	LIBRO	
-	200	\$01 TOB3.9		-	I .	1	-	. 4411E 1	0.000E 01	DOME	
	1 2	3.51.3 100		1980	-	E	6.073E104	3.193E 105	0.0001-01	111 19	
-	7.4	1.024 01	T.	-	1	- 3000 ·	2.7441.104	1.1921.105	0.000E-01	61-111	
	20	10 000F 101		-	Ŧ	0.000t-01	2.92HE 105	5.573£105	0.000.0	111-19	
	210	1.415E 03	Ŧ.	AC.	0.00E-01	0.0001.01	3.200E103	3.012£101	0.000.0	LIME	
	7.1	1.7.411.104	т.	-	Ŧ	T.	2.9351.105	4.000 10:	0.000E-01	Links	
		4 01		-	I.	T	-	1.641111165	0.0000 . 61	11117	
- 4	7.7	1.7 of 100	Ę.,	-	E. 1		med.	5. 793E 165	0.000E-01	11119	
	25	1.15.1.104		-	-	-	-	1. 400E 105	0.000E-01	1 11111.	
-	14.	1. 2341.101	0.0001-01	1.374E 102	2.730E101	4.120£101	1.274E 105	4. 30 1E 10t.	0.000.0	111 111	

TABLE 5 (CONT) Page 5 of 12

(FOR Section 2.2.1.b, units in mrem/year per pC1/m3).

MIE I TEEN FATHMAY I TRHIM ALLON

1.000E+04 7.512E+05 9.480E+04 5.44E+03 LIMIG 5.544E-03 2.400E+03 3.412E+03 0.000E-01 LIMIG 4.112E+02 1.534E+05 2.48RE+05 0.000E-01 LIMIG 5.740E-03 1.153E+03 4.12E+03 0.000E-01 LIMIG 7.432E+03 7.832E+03 4.720E+03 0.000E-01 LIMIG 7.432E+03 7.832E+03 1.00RE+03 0.000E-01 LIMIG 7.504E+05 1.400E+05 1.00RE+05 0.000E-01 LIMIG 7.504E+05 1.400E+05 9.400E+03 0.000E-01 LIMIG 7.504E+05 1.400E+05 1.500E+03 0.000E-01 LIMIG 7.504E+05 1.400E+05 1.500E+03 0.000E-01 LIMIG 7.504E+05 1.400E+05 1.500E+03 0.000E-01 LIMIG 7.500E+01 1.200E+03 1.500E+03 0.000E-01 LIMIG 7.500E+01 1.200E+03 1.513E+03 0.000E-01 LIMIG 7.500E+01 1.200E+03 1.513E+03 0.000E-01 LIMIG 7.500E+03 0.000E-01 2.700E+03 0.000E-01 LIMIG 7.500E+03 0.000E-01 1.525E+03 0.000E-01 LIMIG 7.500E+03 0.000E-01 1.032E+03 0.000E-01 LIMIG 7.500E+03 0.000E-01 1.032E+03 0.000E-01 LIMIG 7.500E+03 0.000E-01 1.032E+03 0.000E-01 LIMIG 7.500E+03 0.000E-01 2.700E+03 0.000E-01 LIMIG 7.500E+03 0.000E-03 0.000E-01 0.000E-01 LIMIG 7.500E+03 0.000E-03 0.000E-03 0.000E-01 LIMIG 7.500E+03 0.000E-03 0.000E-0
000E 104 7.512E 105 9.480E 104 6.464E 1514E - 63 2.400E 103 3.412E 103 0.000E - 112E 102 1.534E 105 2.488E 105 0.000E - 112E 102 1.534E 105 3.412E 103 0.000E - 112E 103 4.122E 103 0.000E - 112E 103 1.688E 105 0.000E - 112E 103 1.888E 105 0.000E - 112E 103 0.000E
2446-63 2. 4006 103 2. 4146 102 0.0006 11. 126 102 1. 5346 105 2. 4146 105 0.0006 12. 4166 105 2. 4146 105 0.0006 12. 4126 105 0.0006 12. 4126 105 0.0006 13. 4126 105 0.0006 14. 4126 105 1. 4126 105
112E 102 1.534E 105 2.488E 105 0.000E 720E-03 1.153E 103 4.121E 103 0.000E 730E-03 4.122E 103 0.000E 730E-03 4.122E 103 0.000E 730E 103 7.812E 104 0.000E 700E 100 1.814E 104 9.046E 103 0.000E 700E 104 4.752E 104 3.721E 103 0.000E 700E 104 4.752E 104 3.721E 103 0.000E 700E 104 4.752E 104 3.721E 103 0.000E 700E 104 1.752E 104 3.721E 103 0.000E 700E 104 1.752E 104 1.572E 103 0.000E 700E 104 1.752E 104 1.712E 103 0.000E 700E 104 1.726E 104 1.712E 103 0.000E 700E 104 1.726E 104 1.712E 103 0.000E 700E 104 1.726E 104 1.712E 103 0.000E 700E 104 0.000E -01 4.132E 103 0.000E 700E 104 0.000E -01 4.132E 103 0.000E 700E 104 0.000E -01 1.722E 103 0.000E 700E 104 0.000E -01 1.722E 103 0.000E 700E 104 0.000E -01 1.032E 104 0.000E 700E 105 1.72E 101 1.000E 700E 103 0.000E -01 1.032E 104 0.000E 700E 103 0.000E -01 1.000E 103 0.000E
720E-03 1.153E 103 4.121E 163 0.060E-173E 163 1.011E 163 0.060E-173E 103 7.832E 103 8.720E-07 0.060E-173E 103 1.011E 103 0.060E-170E 103 1.011E 103 0.060E-170E 103 1.20E 104 0.060E-170E 103 1.20E 103 0.060E-170E 103 0.060E-170E-170E 103 0.060E-170E-170E 103 0.060E-170E-170E 103 0.060E-170E-170E-170E-170E-170E-170E-170E-17
43.20E-03 6.472E 102 8.720E-07 0.000E-13.E 103 7.832E 103 1.00HE 105 0.000E-106 1.00E 104 9.040E 103 0.000E-106 1.40E 103 1.40E 103 2.40CE 103 0.000E-106 1.40E 104 2.720E 105 0.000E-106 2.40E 105 2.20E 105 0.000E-106 2.40E 105 2.504E 101 0.030E-107 2.40E 105 2.504E 101 0.030E-107 2.40E 103 1.20E 103 0.000E-107 2.40E 103 1.20E 103 0.000E-107 2.32E 103 1.20E 103 0.000E-107 2.32E 103 1.20E 103 0.000E-107 2.32E 103 0.000E-107 2.3
432E 103 7.832E 105 1.000E 105 0.000E 400E 100 1.832E 105 1.000E 105 0.000E 105 0.400E 105 0.400E 105 0.400E 105 0.400E 105 0.400E 105 1.400E 105 3.200E 105 0.400E 105 0.400E 105 1.400E 105 3.200E 105 0.400E 105 1.400E 105 3.200E 105 0.000E 105 1.200E 105 1.500E 105 0.000E 105 1.200E 105 1.500E 105 0.000E 105 1.200E 105 1.200E 105 0.000E 105 1.200E 105 1.200E 105 0.000E 1
400E 100 1.014E 104 9.040E 101 0.000E 204E 105 1.400E 107 9.404E 105 0.000E 204E 105 2.720E 105 0.000E 204E 105 1.400E 104 4.024E 105 0.000E 2060E -01 2.400E 104 4.024E 105 0.000E -01 2.400E 104 4.024E 105 0.000E -01 2.400E 105 1.592E 105 0.000E -01 2.400E 105 1.592E 105 0.000E -01 1.20E 104 0.000E -01 2.32E 104 0.000E -01 2.32E 104 0.000E -01 2.22E 104 0.000E -01 2.22E 104 0.000E -01 2.22E 104 0.000E -01 2.22E 104 0.000E -01 1.032E 104 0.000E -01 2.040E 104 0.000E -01 1.032E 104 0.000E -01 1.032E 104 0.000E -01 2.22E 104 0.000E -01 0
904E 103 1.404E 107 9.404E 103 0.400E 504E 104 4.752E 103 3.724E 163 0.000E 0006-01 2.480E 104 4.04E 103 0.000E 0006-01 5.480E 104 7.04E 103 0.000E 0006-01 5.420E 103 7.804E 103 0.000E 2304E 104 1.974E 103 1.572E 104 0.000E 192E 104 1.974E 103 1.412E 103 0.000E 192E 104 1.974E 103 1.412E 103 0.000E 192E 104 1.974E 103 1.412E 103 0.000E 192E 104 1.974E 103 1.212E 103 0.000E 192E 104 0.000E -01 1.272E 104 0.000E 192E 104 0.000E -01 1.272E 104 0.000E 192E 104 0.000E -01 1.032E 104 0.000E 192E 105 0.000E -01 1.00E 103 0.000E
504E104 4.752E103 3.72HE163 0.000E- 584E105 1.40HE105 3.8140E165 0.000E- 000E-01 5.490E105 7.504E101 0.000E- 5336E104 1.754E105 7.504E101 0.000E- 534E104 1.974E105 4.04HE105 0.000E- 192E104 1.974E105 4.04HE105 0.000E- 254E-01 3.294E103 1.212E103 0.000E- 254E-01 3.294E103 1.212E103 0.000E- 254E103 0.000E-01 3.425E105 0.000E- 252E104 0.000E-01 4.435E105 0.000E- 252E104 0.000E-01 4.435E105 0.000E- 252E104 0.000E-01 4.435E104 0.000E- 252E104 0.000E-01 4.435E104 0.000E- 252E104 0.000E-01 4.035E104 0.000E- 252E104 0.000E-01 1.032E104 0.000E- 252E105 1.444E105 0.40E103 0.000E- 254E105 1.774E105 0.40E103 0.000E- 254E105 1.774E105 0.40E103 0.000E- 254E105 1.774E105 0.40E103 0.000E- 254E105 1.774E105 0.40E103 0.000E- 256E105 1.774E105 0.40E103 0.000E- 256E105 1.774E105 0.40E103 0.000E- 256E105 1.774E105 0.40E103 0.000E- 250E105 1.774E105 0.40E103 0.000E- 250E105 1.774E105 0.40E103 0.000E- 250E105 1.774E105 0.40E103 0.000E- 250E105 1.774E103 0.40E103 0.000E- 250E105 1.774E103 0.40E103 0.000E- 250E105 0.200E-01 0.000E-01 0.000E- 250E105 0.200E-01 0.000E-01 0.000E- 250E105 0.200E-01 0.000E-01 0.000E- 250E105 0.40E103 0.40E103 0.000E- 250E105 0.200E-01 0.000E-01 0.000E- 250E105 0.40E-02 0.200E-01 0.000E- 250E105 0.40E-03 0.40E103 0.000E- 250E105 0.40E-03 0.40E103 0.000E-01 0.000E-05 0.000E
584E 105 1.400E 104 3.840E 105 0.000E 000E-01 2.480E 102 4.024E 105 0.000E 534E 104 1.455E 105 1.592E 105 0.000E 280E 104 1.720E 103 1.592E 105 0.000E 192E 104 1.720E 103 1.414E 103 0.000E 192E 104 1.720E 103 1.414E 101 0.000E 172E -02 2.332E 103 1.513E 101 0.000E 172E -02 2.332E 103 1.513E 101 0.000E 172E -03 0.000E-01 1.372E 103 0.000E 172E 104 0.000E-01 1.032E 104 0.000E 252E 104 0.000E-01 1.032E 104 0.000E 172E 105 0.000E-01 1.032E 104 0.000E 172E 105 0.000E-01 1.032E 104 0.000E 172E 105 1.72E 104 1.000E 101 0.000E
0006-01 2.480E102 4.024E105 0.000E-000E-01 5.320E105 7.504E101 0.030E-230E104 1.255E105 7.504E101 0.030E-230E104 1.720E105 4.048E105 0.000E-19.255E104 1.920E105 1.920E105 1.920E105 1.920E105 1.920E105 0.000E-19.255E103 1.513E101 0.000E-19.253E103 1.513E101 0.000E-19.253E103 0.000E-19.272E103 0.000E-
000E-01 5.340E 05 7.504E 01 0.030E 053E 04 1.455E 04 1.592E 05 0.030E 053E 04 1.592E 05 0.030E 055E 04 1.976E 04 1.976E 04 1.976E 04 1.976E 05 1.976E 05 0.030E 053E 05 1.372E 04 1.372E 05 0.030E 052E 05 1.372E 05 0.030E 052E 05 0.030E 05 0.0
53.4E 0.4 1.45.5E 0.4 1.59.2E 0.5 0.000E 28.0E 0.0 1.12.0E 0.4 0.000E 19.2E 0.4 1.97.4E 10.4 1.61.5E 0.5 0.000E 25.4E 0.4 1.97.4E 10.4 1.61.5E 0.5 0.000E 25.2E 0.3 2.37.4E 0.3 1.51.5E 0.3 0.000E 25.2E 0.4 0.000E 0.4 2.00E 0.5 0.000E 25.2E 0.4 0.000E 0.4 2.00E 0.5 0.000E 25.2E 0.4 0.000E 0.4 2.00E 0.5 0.000E 25.2E 0.4 0.000E 0.4 2.25 0.4 0.000E 25.2E 0.4 0.000E 0.4 0.000E 25.2E 0.5 0.000E 0.4 0.000E 25.2E 0.5 0.000E 0.5 0.000E 25.2E 0.000E 25.2E
200E 100 1.120E 104 8.000E 104 0.000E 192E 104 1.976E 105 4.040E 105 0.000E 192E 103 1.212E 103 0.000E 192E 103 2.372E 103 1.212E 103 0.000E 172E 103 2.372E 103 1.513E 101 0.000E 172E 103 0.000E 172E 104 0.000E 172E 104 0.000E 172E 104 0.000E 105 0.000E
192E 104 1.97dE 103 4.044E 103 0.000E-254E 01 1.212E 103 0.000E-392E 102 1.212E 103 0.000E-392E 103 1.212E 103 0.000E-392E 103 4.48HE 103 4.23E 101 0.000E-392E 103 4.48HE 103 4.23E 103 0.000E-10 0.120E 103 0.000E-10 0.120E 103 0.000E-10 0.000E-10 0.120E 103 0.000E-10 0.000E-1
254E-01 3.294E103 1.214E103 0.000E 392E102 3.374E103 4.20BE103 0.000E 953E103 4.4BHE103 4.33E101 0.000E 953E103 4.4BHE103 4.33E103 0.000E 100E103 0.000E-01 0.120E103 0.000E 920E104 0.000E-01 1.272E103 0.000E 593E104 0.000E-01 1.032E104 0.000E 593E104 0.000E-01 1.032E104 0.000E 593E104 0.000E-01 1.032E104 0.000E 454E103 0.000E-01 1.032E104 0.000E 100E105 1.774E104 1.0BHE103 0.000E 446E103 7.672E101 0.000E-01 0.000E 446E103 2.272E101 0.000E-01 0.000E 446E103 2.272E101 0.000E-01 0.000E 1145E 03 3.29E103 3.20BE103 0.000E
392E102 3,374E105 6,208E105 0,030E-174E-02 2,334E103 1,513E101 0,000E-753E103 4,481E105 4,437E105 0,000E-7753E104 0,000E-01 9,120E103 0,000E-7753E104 0,000E-01 1,272E104 0,000E-7753E104 0,000E-1753E104 0,000E-7753E103 0,00
1746-02 2.3346403 1.5136101 0.0006- 7536103 4.4818105 4.4376105 0.0006- 7536103 0.0006-01 7.2726103 0.0006- 7536103 0.0006-01 1.2726103 0.0006- 55736103 0.0006-01 1.0326103 0.0006- 75346103 0.0006-01 2.0466101 0.0006- 7536103 1.446105 9.7206103 0.0006- 1046105 1.7746103 0.7046103 0.0006- 7546103 7.8726101 2.7046 01 0.0006- 7546103 7.8726101 2.7046 01 0.0006- 7546103 7.8726101 0.0006-01 0.0006- 7556103 2.2726101 0.0006-01 0.0006- 7556103 2.2726101 0.0006-01 0.0006- 7556103 2.2726101 0.0006-01 0.0006- 7556103 2.2726101 0.0006-01 0.0006- 7556103 2.2726103 0.0006-01 0.0006- 7556103 2.2726103 0.0006-01 0.0006- 7556103 2.2726103 0.0006-01 0.0006- 7556103 2.2726103 0.0006-01 0.0006-
75.2E 103 4.4811E 165 4.23.2E 165 0.00.0E 75.2E 104 0.000E -01 7.120E 103 0.000E -01 7.120E 103 0.000E -01 7.22E 103 0.000E -01 1.272E 103 0.000E -01 1.272E 103 0.000E -01 1.272E 103 0.000E -01 1.032E 103 0.000E -01 1.032E 103 0.000E -01 0.00
75.25 104 0.000E-01 9.120E103 0.000E-1040CE104 0.000E-1072E103 0.000E-1072E103 0.000E-1072E103 0.000E-1072E103 0.000E-1072E103 0.000E-1072E103 0.000E-1072E103 0.000E-1072E103 0.000E-1072E103 1.000E-1072E103 0.000E-104E103 1.000E-1072E103
100E 104 0.000E-01 0.372E 103 0.000E-0552E 103 0.000E-01 1.372E 103 0.000E-01 1.032E 103 0.000E-01 1.032E 103 0.000E-01 1.032E 103 0.000E-01 2.046E 101 0.600E-01 2.046E 101 0.600E-01 0.752E 103 0.000E-01 0.752E 103 0.000E-01 0.752E 103 0.000E-01 0.752E 103 0.000E-01
59.26 103 0.0006-01 1.2726103 0.0006-04 4.46 103 0.0006-01 1.0326104 0.0006-04 4.46 103 0.0006-01 0.0066-01 0.0066-01 0.0066-01 0.0066-01 0.0066-01 0.0066-01 0.0066-01 0.0006-01 0.0066-01 0.0006-0
592E 104 0.000E-01 1.032E 104 0.000E-434E 103 0.000E-01 2.046E101 0.600E-732E 103 0.000E-01 2.046E101 0.600E-752E 103 0.000E-752E 103 1.000E-103 0.000E-104E 103 1.000E 103 1.000E 103 1.000E 103 1.200E 103 1.000E 103 1.000E 103 1.000E 103 1.000E 103 1.000E-103 1.0000E-103 1.000E-103 1.000E-103 1.000E-103 1.000E-103 1.000E-103 1.0
400E104 0,000E-01 2,010E101 0,000E-01 2,010E101 0,000E-01 4,952E103 0,000E-01 4,952E103 0,000E-01 4,952E103 0,000E-01 4,952E103 0,000E-01 0,000E-03 1,201E103 0,000E-040E103 0,000E-01 0,0
753E 105 1,464E 105 9,720E 103 0,000E 104E 105 1,724E 104 1,00aE 104 0,000E 1040E 105 1,720E 103 0,000E 1040E 105 1,724E 104 1,00aE 104 0,000E 105 1,20aE 105 0,400E 103 0,224E 103 2,224E 103 2,204E 103 0,000E 103 0,234E 103 2,244E 103 4,446E 103 3,244E 103 3,244E 103 0,000E 1040E 105 3,244E 103 0,000E 1040E 105 1,912E 103 4,724E 10 0,000E 106 106 106 106 106 106 106 106 106 106
753E105 1,464E105 9,720E103 0,000E- 104E105 1,774E104 1,004E104 0,000E- 040E105 1,201E105 0,400E103 0,000E- 446E102 7,072E101 2,704E 61 0,000E- 440E103 2,272E101 0,000E-01 0,000E- 200E-04 4,44E103 4,440E103 0,000E- 040E-05 3,200E103 7,444E-04 0,000E- 040E-05 3,200E103 7,444E-04 0,000E-
105 1.774E 04 1.084E 04 0.050E 152 1.201E 05 8.4f00E 03 0.050E 102 7.072E 01 2.704E 01 0.050E 103 2.272E 01 0.000E 01 0.000E 01 2.072E 01 0.000E 01 2.072E 01 0.200E 02 3.286E 03 0.000E 05 3.286E 03 7.74E 04 0.000E 05 3.286E 03 7.74E 05 0.000E 05 3.286E 03 7.74E 05 0.000E 05 3.286E 03 7.74E 05 0.000E 05 3.286E 05 3.286E 05 0.000E 05 3.286E 05 3.286E
102 7,072E101 2,704E 01 0,055E-102 7,072E101 2,704E 01 0,000E-01 0,000E-01 0,000E-01 0,000E-01 0,000E-01 0,000E-01 0,203E101 0,206E103 0,000E-05 1,200E103 7,44E-04 0,000E-05 1,912E103 7,72E-10 0,000E-05
102 7,072E101 2,704E 61 0,000E- 103 2,272E101 0,000E-01 0,003E- -04 4,44E103 6,440E103 0,000E- 101 2,032E105 2,200E105 0,000E- 05 3,200E103 7,745E-0 0,000E- 05 1,912E103 4,745E-0 0,000E-
103 2,272E101 0,000E-01 0,000E- -04 4,44E103 4,44E103 0,000E- 101 2,032E105 2,280E105 0,000E- 05 3,280E103 7,44E-04 0,000E- 05 1,912E103 4,722E-10 0,000E-
101 2.0328103 6.4408103 0.0008- 101 2.0328105 2.2808105 0.0008- 05 3.2808103 7.4448-04 0.0008- 05 1.9128103 4.7928-10 0.0008-
101 2.012E105 2.280E105 0.000E-05 3.280E103 7.444E-04 0.000E-05 1.912E103 4.792E-10 0.000E-
05 1.9126 F03 4.7226 - 10 0.0006
-3000.0 01-3547.4 F03 3C19.1 60 33
.000E 01 2.144E105 4.873E165 0.060E-01

TABLE 5 (CONT) Page 6 of 12

(Por Section 2.2.1.b, units in mrem/year per HC1/m).

	EA	1		-	_			_	_	1.1		-	-
	CRITICAL										1.11116		
		0	10	10	10	10	10	2	10	10	0	0	10
	BKIN	1.05.4E	3000 · 0	0.000E	9000'0	9000 . O	0.000E	0.000E	9000 . O	0.000E	3000.0	9000 . 0	9000 . O
	01-171	1.200E 104	1.24 11 105	3.55.11.105	0.4401.105	2.134E 105	2.3528-04	1.024E105	0.550E131	1.7601 105	3.8721.105	0.240E105	1.320E 165
	tung	1.052E-01 0.000E-01 9.600E-01 4.248E-01 0.000E-01 1.052E104 1.200E104 1.054E-01	4.136E/05	1.304E105	1.334E107	4.832E105	1.752E103	3,720£105	4.456E105	4.734E101	1.920E 108	3.664E 100	4.4BUE 101
	KIPHEY	0.000E-01	6.800E103	0.440E101	1.20uf 105	3.04HE 103	1.00uE-03	5.034£103	0.003E-01	0.000E-01	1.8731.107	1.7445.107	1.000E103
	LIVER	4.248E-01	1.896E104	1.934E102	2.024E105	5.313E103	1.740E-02	0.540£ 103	5.174E103	9.75UE 100	0.000E-01	0.000E-01	3.192£101
	PONE	9.400E-01	2.840E104	2.454E102	4.000E104	1.334E104	4.296E-03	7.84E103	1.540E 103	1.200E101	0.000E 107	7.644E 107	3.384E102
	HICKOID	0.000E-01	0.000E-01	0.000E-01	0.0006-01	0.00GE-01	0.000E-01	0.000E-01	0.0006-01	0.000E-01	0.0005-01	0.000E-01	0.000E-01
T TURE	Arthri	10-375	£01307	40£ 101	24E 105	246103	74E-03	COL 103	14BE 101	13E100	1:2E 104	37E 105	101 779
HINLA	2	1.0	3.1	13.	2.6	4.3	::	i.	2.	3.	+	+	
GOE I BEEN FATHBAY I IMINLALIN	3401081 an	21 16-142	72 CE-141	73 CL - 143	74 CE-144	75 FK-141	75 FK-144	77 110-147	76 11-1165	79 11-11/2	110 11 235	01 10-238	B2 HF 239

TABLE 5 (CONT) Page 7 of 12 PATHMAY DODE FARAMETER FACTORS FOR INTLEMENTING TO CFR FAKE 20 (For Section 2.2.1.b, units in mrem/year per pC1/m³).

AGE I CHILD FATHWAY I THIM ATTON

J.	ATHUAY I THIM AT	IBIN ATION								
2	THO ISBIDINE	W. BODY	THYKOID	BONE	LIVER	KIMEY	LUMB	111-19	ENIM	CRITICAL
-	E-11	1.125E103	1.1256103	0.000E-01	1.125E 103	1.1256104	1.1256103	1.125E103	1.1356 103	W. DODY
cı	6-14		6.734E1	3.589E104	6.7346103		734E1	-	. 734E1	ā
m	110-24		-		-	410E		1310E	-3000	W. Milley
+	F-32	9.879E104	0.000E-	2.405£104	1.1436105	0.000E 01	- 1	4.21BE104	0.0000.0	BONE
:3	BC- 45		0.000E	19E	3.959E10S	. 700E 1	0.000E 01	1.19:4 105	0.000E-01	1.194.16
47	CK 51			0.000E-01	0.000E-01	2.4316101	1.69HE 104	1.08 11.103	0.00CE-01	t tieds
-	nii 54		0.000 01	0.000E-01	4.392E104	1.00.3E 104	-	2.2501 101	0.6062-01	1 1816
=	NH 5.5		3000°	- 300	-	1.472£100	-	33361	T.	61 11.1
0	11. 55		0.000E 01	4.7356104	2.516E101	0.000E-01	1.1106105	2.84ilf 103	0.000E-01	1 111113
	FE 59		6.0601 01	2.050E104	3.345E 104	0.000E-01	-		1	1.1881
	E.O. 5.8	_	0.000t 01	7	1.772E103	0.000.01	-	3.447.101	0.000E-01	1 11111
	07 03	2.24 11.104	0.000E-01	0.000E-01	1.3146101	0.000E-01	7.057E104	9.430E104	0.0001 01	LIMIG
	45 111		0.000E 01	-	403E1	T	. 0.344. 1	1117		LUIN
	111-53	2,7976104	0.000E-01	8.214E105	4.25E	0.000E-01	3.749E105	4.327E103	1	14 hrii
	111-55		1	2.990E100	3.954E 01	1	1177E1	0.399E104	- 3.	111-111
	FII-54		T		-	4.031E100	. 50 JE 1	3.5700.104	0.030E-01	61-11.1
	28-N2			4.255E 104	-	7.141E101	. 953£ 1	1.4.124.104	0.0001	1 tinti
	65 NZ		0.000E	4.497E-03	9.457E-02	5.845E-02	1.421E103	-	1	61-11.1
	PK B3		0.000E	0.000E-01	0.000E-31	0.000E-01	0.0006-01	0.0001: 01	0.000E-01	W. Bulli
	Mc -84		0.000E-01	0.000t -01	0.000E-01	0.600E 01	10000	0.000E 01		
	lak mis	2.5311 101	0.000E-01	0.000E 01	0.000E-01	0.000E-01	0.0001-01	0.000E-01	10 3000.0	
	ht: 115	1.14.16.105	9.00GE	0.000E-01	1.9113£105	0.000E-01	0.00GE 01	7.993£103	0.000E 01	11011
	Kb 00		0	-	. 423E i	Ŧ	. 600E	1.7216101	0.000E 01	LINER
	1:E 89	-	0.000E		3.452E103	0.0001 01	0.000E-01	1.091E100	0.000E-01	LIME
	5R 119		0.000 01	5.9941.105	0.000E-01	6, COOE -01	15/E1	1.47.1 105	0.000E-01	Linni
	SK 96		0.633E	1.0106 100	0.0306-01	0.000E 01	1.474E107	3, 1311 105	0.6001-01	HHH
	16-319	4.50m 100	0.000E 01	1.2146 102	0.0001	0.000E-01	5. J26E 104	1.747E 105	0.000E-01	11119
	Ek 92	5.25 M 91	0.630E	1.3, 3, 101	0.03CE-01	0.000E-01	2.401E104	2.4246105	0.000E-01	61-11.1
	2.50	1.1051103	6.00GE	4.16/1103	I	0.6008-01	. 41 54 1	2.4776 105		111-19
	1 -91H		0.0001-01	5.029E -01	0.0001-01	0.000E 01	2.812E103	1.717E103	6.000E-01	Linds
==	16 1	2,4301.104	0.030E-01	9.1396105	0.000E-01	0.0001-01	2.4371.105	1.8196105	0.00cE 01	1 11111
	1-93	5, G39E 01	-30000	2.03th 101	F	0.000E-01		2,390E105	0.000E-01	01-111
	1 93		0.00cE-01		0.000E 01	0.000E-01		3.805£105	0.000E-01	11119
	ZK-92		-3000	9111	-	5.9571104	.231E	4.105E101		1 118to
	78-97	1.590E101	0.000E-01	1.875E 102	2.715E101	3.005E101	1.132E105	3.511E165	6.000E-61	111119

TABLE 5 (CONT) Page 8 of 12

PATHHAY BOSE PARAMETER FACTORS FOR INFLEMENTING TO CFR PART 20

			(For Section	2.2.1	.b, units in	in arca/year	h 1	per µC1/m*).		
AGE	AGE 1 CHILD FATHUAY 1 IMIM	INIIAI ATTUN								
=	3.101051 OH	. u. buhr	HIVKOID	DONE	LIVER	N. I SPHEY	L-UMB	01-111	EN 310	CRITIC
3.5	26-98	4.5496103	0.0006-01	2.350E104	9.176E103	B. 621E103	4.142E105	3.700E104	6.549E103	T THE
37	116 97	9.473E	0.000E-01	1.029E-01	2.401E-02	3.02/E-03	. 110E #	-	-9000.	TIME
36	66 01	÷	0.000E-01		. 724E1	-	.354E+	1.245E 105	0.000E-01	111110
3.0	1C-99H	5.773E	0	- JOHZ .	3.4026-03		. 509E	-	T	17.19
40	101 31	1.077E	0	. 103E -		1	.844E1	-	T	TIME
7	Kil 103	-	·	38E1	- 3000 ·	-	. 423E 1	4.477E104	Ŧ	Luni
47	KH-165	5.550L	0.000E-01	300		-	-	-	0,0005-01	10
11	KH 103	1.49161	0.000E-01	-30	.030E	39E		-	Ŧ.	TIME
7 7	ALT-1108	9.13VE1	T.	-	-	-	-	1.0031105	I	THE
-	CB-1150	3.94361	8	1	10351	-	135	-	T.	LIMB
-1-4	124 424	5.73561	-	-	. 723E 1	T	-	-	1	11111
47	16 125	9.13961	-	-	.327E+	*	-	-	7	TIME
114	11 11/1	-		ci	.547E	-	-	-	0.000E-0	1
4.5	11:137	4.1054	-	2.77161	- 200c	.04761	1.003E104	-	Ŧ	11 10
20	16:11-11	3.011E	4.327E103	1.9206.104	4.645E103	-	1.751E104	-	0.0001-01	T THE
77	HE 129	2.30 %	T	9.748E 03	•		2.9346103	-	Ī.	-
7	131	5.049E	-	4.16.16	30E	3.995E 102		-	T	-
70	171	A. 500.E		2.17.15	4776	5 4	-			
	11. 13.	2.531E	3.1.04.102	4.BIOE		2 444 104	3.7.11.103	1775	0.000.0	
3 .	1 1 1 1 1	2.7356104	1.1.11.107	•	4. B10F104	-		2.0426103	0. GOOF - 01	
173	-133	1.8748.1	-	2.11484	-	25364		-		1100
77:	1 133	7.	3.01401.105	1.4	2.031E104		1	5.474E103		Inyled
7.7	1111	\$. 953E103	5.067E10	1.1736103	2.161E10J	3, 300E 10.1	0.000E-01	-	т	HIYES
30	1.15	4.1941.1	7	+	-	1.3396104		-	1	HILL
17	Ch 134	3.34511	0.000	-	1.014E105	3.304E1	-	-	0.000E 01	1 101
41	CS 135	1.1531.1	ò	4.5131104	. 70.JE I	9.542E	-	-	*	1.74
7.3	Cu-1.1/	1.204t b	0	-	8.251E105	2.0138 103	-	-	T	POHIE.
17	12 130	5.550E	1	-	B. 399E102	4.215E 102		-	6.0004 01	1361
77.77	62 1.19	5.1111	Ti.	2	. 34 1E 1	-		T	T	14
-7	171	5, 32:4	0.000E 0	-	176	4	-	-	0.0001	-
	110	4.1:91.16.3	0.0000	7.4006.104	4.475E101		71.16	011111	Tu:	LIBRE
3	14. 14.7	2 7006	0.000E	7	3 AGOF -02	3010	1. 44 16 10 1	2 7474 400	400000	
3	1 V 1 40	7.54061	0.0006	-	2.356E1	0.000E 01		B 498	0.000E-01	91 19
	-									-

TABLE 5 (CONT) Page 9 of 12

FAILMAY GOSE PARAMETER FACTORS FOR INPLEMENTING TO CFR PART 30

	FATHWAY I IMMALATION	110N								
no ISOTORE		FODY	HYKBIB	MODE	LIVER	KIDNEY	thut	177-10	BNIN	CKITICAL
71 1.0-142		91E-01	0.0006-01	291E-01 0.000E-01 1.295E100 4.107E-01 0.000E-01 8.495E101 7.5H5E104 1 2015-61	4.107E-01	0.000E-01	B. 495F 103	7.5.056 104	3000	
72 CE-141		9.1E103	0.000E-01	3.923E104	1.95-1E104	6.547E103	5.410F 105	F. 4.16 104	2000	1
73 CE 143		75E101	0.000E-01	3.459E103	1.987E402	8.3476101	1 15.45 108	3336104	2000	t three
74 CE- 144		15E 105	0.000E-01	6.771E106	2.114E165	1.1735 104	1056107	3 4056 164	2000	1
75 FK 144		171 102	0.0000.0	1.845E404	5.550£101	1.0011-101	4 3005 105	0 2315.00	2000.0	
74 I'K 144		E0 3/6	0.000E-01	5.95/E-03	1.84KF-32	0.7405.03	2013479	1010101	0.000E-01	1.1940
77 Hit 147		OHE 102	0.000E 01	1.080E104	8.732E103	4.010F103	3. 369E 40K	0 21 46 10 4	10 3000 O	
CH 1-1102		OF 101	0.0000.0	3.5.0E101 0.000E-01 7.215E102 2.494E163 0.000E-01 3.641E108 3 0541E108	2.4946163	0.000F-01	2.041F10S	1 05.1.10.5	0000	
79 H 107		398100	0.COOF -01	1.332E101	9.457E100	0.000E-01	4.1075 464	0 1013.010	30000	
89 0 335		: 36: 105	6.030E 01	3.700£ 107	0.000E-01	B. 450F 105	1 A 1 4 1 1 0 11	3015100	20000	
ut 11-230		9th 105	0.000E-01	3.545E 107	0.000E-01	B. 044F 104	1. 40 L. 100	2011111111	10 3000 0	
u2 m-239	3.3	50E 101	0.003E-01	4.45 F 102	3.3456101	9.7316101	S. 900F 104	A 40.16 10.1	0.000	1 IMM
									D. DOOL OF	11111

ASE I INFANT FATIBIAY I IMIALAI	FRIM AT 10H								
NO ENDTONE	u. 100y	DIVEGIE	FONE	LIVER	KIDNEY	Lisna	177-19	BKIN	CRITICAL
1.11.3	6.46BE 102	4. 46HE 102	0.000E-01	4.44BE 102	2.45ut 103	4.44BE 102	6.45HE 102	6.46HE 103	W. 1001
2 6-14	5.304E103		2.445E104		370E.	.305E	.305£	. 300E	FIGHE
3 His 24		1.055E104	1.055E 104	1.054E104	1.055E104	1.054E104	1.055E101	-3000°	u. billin
4 F-43	7.743E104	0.000E-01	2.030E104	1.124E105	0.000E-01	0.000E-01	1.6101104	0.00CE-01	HUME
5 BC 45	4.354E104	0.000E-01	-	1.4981.105	1.400E105	0.000E-01	-	0.000E-01	LIVER
CK-SI	10.945E101	5.754E101	0.000E-01	0.000E-01	1.323E101	1.204E104	-	0.000E-01	Lind
7 mm 54	4.9011103	0.000E 01	1	1.452E104	4.984E103	9.996E105	7.054.103	0.000E-01	1.1011
B NH 55	2.2128-01	0.000E-01	0.000E-01	1.5 10E 100	-	1.353£104	-	0.000E-01	177 10
9 11 55	3.311.103	0.0001-01	1.974E t04	1.175E104	1	8.694E104	1.09:31.10.1	1	£1000
10 1E- 59	9.47at 103	0.000E-01	1.357E104	-	3			1	t tirtis
	1.01305.103	0.000E-01	1		30	7.770E 105	-	1	4.11/413
12 00 -00	1.17./1.104	0.000E-01	0.000E-01	8.022E	1	4.508F 105	3.192E104	0.000E-01	1.1846
	9.4711.102	0.000E-01	5.484E 103	2.044E1		1.149E104	8.554£ 10.3	0.0001-01	1 111113
14 111 53	SIE	0.000E-01	-	ci	1	-	2.4: 11.03	7	DUNIE
	311	0.0006-01	2.3946100	3.8436	0.000E-01	-	5.01:E101	0.000E-01	11111
15 01 54	1.3E	1	Ŧ	-	-	-		0.000E-01	111111
	DILL 4	0.300E-01	-	4.35.0E b	-	-	-	1	
	3.16	0.000E 01	1	9.6746	1	11/01	-		-
	DINE .	0.000E-01	1	10000	7	.000F			
Ξ.	910	0.000E-01	T	3000.		T.		7	W. fulling
ž :	141	0.000F 01	3	0.0001	.000E				
=	100	Γ.	Ŧ.				-		47.1
7.2 KB 000	10 10 10 10 10 10 10 10 10 10 10 10 10 1	0.0000.01	0.0000	2013/2012	0.000	0.000E 01	A BINE 101	0.0000.0	2 1 1 1
40	=	0.000E-01	-		. 666£	-	3 7 111 1		1 111/11
Nil.	1 106	0.0001	- 100	- 9000.	OOOE	-	-	18/	1:1910
	1111	3000	-		3000.		7.334.101	0.000.0	11119
201 KK 92	3. COSE 01	0.000E 01	1.0504 101	0.000E-01	0.000E 01	2.300E104	1.4006 165	0.000L-01	111-17
	B.01.00.101	0.0006-01	3.290E103	0	0.000E-01	2.586E 105	1.0100105	1	Linn
30 Y 91H	1.3utf 02	0.600E 01		0.600£	3000		-	Æ	I LAMES
	1.5500104	0.000E 01	-	0.000E	Ŧ		7.03BE 104	T	Listili
	4.2021 01			0.0000	1	-	-	L	111 111
	7.11.1	0.0005-01		0.000		-	-	1	1111
34 ZK-95	2.0300104	0.0001	-	2.784E1	-	-	-	3 .	
	1.1704 191	0.000E-01	1 . 49th 102	2.5528 101	2.2900.101	1.1031 105	1.4001.105	0.0001-01	1111

TABLE 5 (CONT) Page 11 of 12

PATHUMY DOUE FARANCIER FACTORS FOR INFLEMENTING 10 CFR PART 20 (For Section 2.2.1.b, units in mrow/year per pC1/m3).

AGE 1 INFAMI PATISTAY 1 IMIALATION

3. 710E 103 0. 000E 01 1. 554E 104 4. 723E 103 4. 710E 104 4. 720E 105 4. 220E 103 0. 000E 01 3. 892E 02 9. 843E 03 1. 445E 02 4. 220E 102 4. 220E 13. 234E 101 0. 000E 01 0. 000E 01 1. 397E 03 2. 644E 102 1. 346E 103 0. 000E 01 2. 014E 103 0. 000E 01 2. 014E 103 0. 000E 01 2. 014E 103 0. 000E 01 1. 224E 103 0. 000E 01 1. 024E 103 1. 024E 103 1. 040E 104 0. 000E 01 1. 024E 103 0. 000E 01 1. 024E 103 1. 024E 103 1. 040E 104 0. 000E 01 1. 024E 103 1	1 0.000E-01 1.554E104 4.425E103 4.710E103 4.780E105 4.000E-01 3.892E-02 9.842E-03 1.445E 02 4.200E102 4.200E102 4.0.000E-01 1.397E-02 1.462E102 1.340E105 4.0.000E-01 1.397E-02 2.644E102 1.340E105 4.0.000E-01 1.397E-03 2.644E102 1.340E105 4.0.000E-01 1.224E100 0.000E-01 4.342E 04 1.554E102 1.340E102 4.0.000E-01 1.224E100 0.000E-01 1.090RE-01 1.554E102 1.554E102 4.0.000E-01 1.224E103 1.0.000E-01 1.090RE-01 1.554E102 1.554E102 1.0.000E-01 1.055E104 1.554E105 1.0.000E-01 1.000E-01 1.00	in thorogre u.	huby	HINKOID,	PAINE.	LIVER	1	t Studen		***	CKILLER
3, 5046-03 0,0006-01 3, 8926-03 1, 456-02 4, 2006 102 4, 2206 104 1, 5016-03 0,0006-01 0,0006-01 1, 4526 102 1, 4466 102 1, 4466 102 1, 4466 102 1, 4466 102 1, 4466 102 1, 4466 102 1, 4466 102 1, 4466 103 1, 44	3. (1) 11 12 10 10 0.000E - 01 3. 1972E - 03 1, 145E - 02 1, 340E 1 02		101.300	0 0000 0	5406.4	-	710E	780£	-	3.780E 103	Linin
3, 234E 01 0, 000E 01 1, 397E 03 2, 644E 02 1, 244E 102 1, 340E 103 6, 102E 104 1, 397E 03 2, 644E 03 1, 104E 02 0, 000E 01 1, 397E 03 2, 644E 03 1, 104E 02 0, 000E 01 1, 397E 03 0, 000E 01 1, 324E 103 0, 000E 01 1, 224E 103 0, 000E 01 1, 000E 01 1, 000E 10 1, 000E	1, 234E 101 0, 000E -01 1, 397E -03 3, 404E -04 5, 434E 102 1, 344E 101 0, 000E -01 1, 397E -03 2, 604E -04 5, 134E 102 6, 504E -04 0, 000E -01 1, 397E -03 2, 604E -04 5, 134E 102 6, 504E -04 6, 134E 102 6, 504E -04 6, 134E 102 6, 504E -04 1, 134E 102 6, 504E -04 1, 134E 103 7, 134E 103 6, 504E -04 1, 134E 103 7, 134E 103 6, 504E -04 1, 134E 103 7, 134		100		30.00	0 4476		200F	-		111111
3, 2344101 0, 6000E-01 1, 397E-03 3, 104E-04 5, 034E-04 5, 034E-102 1, 104E-04 5, 034E-103 1, 104E-04 5, 104E-04 5, 034E-103 1, 104E-04 5, 104E-04 5, 034E-104 1, 104E-104 1, 104E-	3, 214E 101 0, 0000E - 01 1, 397E - 03 2, 6144E - 03 1, 100E - 02 6, 100E - 01 1, 397E - 03 2, 6144E - 03 1, 100E - 02 6, 100E - 01 1, 397E - 03 9, 7046E - 04 6, 000E - 01 1, 2046E 1 03 0, 000E - 01 2, 0146E 1 03 0, 000E - 01 1, 2046E 1 03 1,	**	1141 03		11. C	3.01.0			1013000	-3000	
3,724E 02 0,606E-01 1,397E-03 2,8144E-04 3,001E-04 5,034E102 4,412E 103 1,204E-02 0,000E-01 4,510E-03 9,724E-03 5,514E102 1,412E-03 0,000E-01 1,524E103 0,500E-01 1,524E103 1,534E104 1,414E104 0,000E-01 1,224E103 0,000E-01 1,524E103 1,534E104 1,414E104 0,000E-01 1,224E103 0,000E-01 1,524E103 1,524E104 1,534E104 1,414E103 0,000E-01 1,524E103 1,524E103 1,524E104 1,524E103 1,52	3,724E-02 0.660E-01 1.397E-03 2.444E-03 4.100E-04 6.034E-102 6.796E-03 0.000E-01 1.397E-03 0.000E-01 4.342E-03 9.784E-04 6.000E-01 1.224E-100 0.000E-01 1.924E-103 1.092E-104 3.426E-105 1.534E-107 1.002E-01 0.000E-01 1.224E-100 0.000E-01 1.024E-103 1.092E-104 3.426E-105 1.534E-107 1.002E-01 0.000E-01 1.224E-103 0.000E-01 1.324E-103 1.092E-104 3.426E-103 1.092E-104 3.426E-105 1.534E-107 1.324E-103 0.000E-01 9.992E-103 7.224E-103 1.092E-104 3.424E-105 1.324E-103 1.224E-103 1.224E-10	7	141 101	7	1	-	BACK	1		1000	
6. 130E 04 0.000E 01 4.510E 05 8.23E 05 9.704E 04 5.030E 102 6.410E 14.102E 04 0.000E 01 1.024E 105 1.000E 01 1.024E 105 1.510E 104 4.102E 103 0.000E 01 1.024E 105 1.024E 105 1.524E 107 1.534E 104 1.000E 01 1.024E 105 1.	6. 120F -04 0.090E -01 2.014E 103 0.000E -01 4.242E 103 6.134E 105 4 4. 102E -03 0.000E -01 2.014E 103 0.000E -01 1.024E 103 1.154E 105 4 4. 102E -03 0.000E -01 2.014E 103 0.000E -01 1.024E 103 1.154E 107 4 4. 102E -03 0.000E -01 9.992E 103 7.224E 103 1.024E 105 1.154E 107 4 4. 991E 103 0.000E -01 0.000E -01 3.224E 103 1.092E 104 3.44E 105 4 5. 100E 103 1.323E 103 5.430E 103 1.036E 103 1.092E 104 2.773E 104 1.34E 105 5 5. 100E 103 1.534E 103 5.430E 103 1.036E 103 0.000E -01 4.346E 105 5 5. 100E 103 1.534E 103 1.424E 104 5.902E 103 3.752E 104 1.313E 105 5 5. 204E 103 1.034E 103 1.424E 104 5.902E 103 3.752E 104 1.313E 105 5 5. 204E 103 1.034E 103 1.734E 103 1.702E 103 3.752E 104 1.313E 105 5 5. 204E 103 1.034E 103 1.734E 103 1.735E 104 1.313E 105 1.754E 103 1.75	3.	246-02	F.	F.	T	100t	1036	0.306	€.,	
6. 790E 103 0. 000E - 01 2. 014E 103 0. 000E - 01 4. 342E 103 5. 514E 105 1. 1531E 104 4. 010E 1. 10.2E 101 0. 000E - 01 1. 254E 105 1. 1531E 104 4. 010E 104 0. 000E - 01 1. 254E 105 1. 1531E 104 4. 010E 104 0. 000E - 01 1. 254E 103 1. 054E 103 3. 3094 1. 1131E 103 6. 000E - 01 0. 000E - 01 3. 444E 103 4. 444E 103 4. 244E 103 6. 000E - 01 0. 000E - 01 3. 224E 103 1. 052E 104 3. 444E 103 4. 254E 103 1. 323E 103 1. 054E 103 1. 056E 103 2. 773E 104 4. 444E 103 4. 726E 103 1. 324E 103 1. 224E 103 1. 056E 103 1. 725E 104 1. 444E 103 5. 730E 103 1. 054E 103 1. 224E 103 1. 056E 103 1. 725E 104 1. 444E 103 5. 730E 103 1. 054E 103 1. 056E 103 1. 725E 104 1. 444E 103 1. 291E 103 1. 056E 103 1. 224E 103 1. 056E 103	4, 102E-31 0, 0000E-01 2, 014E103 0, 000E-01 4, 242E103 5, 514E105 1, 1, 024E105 1, 024E	8.1	30E 04	1	-301G	1	784E-	030F	14381	1	
4. 102E - 31 0.000E - 01 1.224E 100 0.000E - 01 1.021E 105 1.551E 104 4.011E 109 0.000E - 01 0.000E - 01 1.021E 103 1.021E 107 1.551E 107 1.551	4, 102E-31 0,000E-01 1,224E100 0,000E-01 1,024E105 1,554E107 1,000E107 0,000E-01 0,908E-01 1,024E105 1,554E107 1,994E103 6,909E-01 1,044E103 1,224E103 1,034E103 0,000E-01 1,444E103 2,722E104 1,323E107 1,323E103 1,334E103 1,034E103 0,000E-01 1,444E103 0,000E-01 1,323E103 1,324E103 1,244E103 0,000E-01 1,323E103 1,324E103 1,244E103 1,244	6.	190E 103	T.	-	0.000E	242F1	21 4E +	\$10E		
1. 0100E 104 0.000E -01 0.410E 104 0.000E -01 1.02:E105 1.153.E107 1.5340E 104 0.000E -01 9.991E 103 7.224E 103 1.025.E104 3.424E 105 3.426E 105 3.426E 105 1.373E 104 3.424E 105 1.373E 104 3.424E 105 5.730E 103 1.323E 103 1.434E 103 1.034E 103 1.030E 101 1.034E 103 1.034E 10	1. 0000E 104 0.000E -01 9.902E103 7.224E103 1.092E104 3.424E105 3.170E103 6.000E -01 9.902E103 7.224E103 1.092E104 3.444E105 3.272E104 2.444E105 5.170E103 1.092E104 1.332E103 1.030E-103 1.030E-103 0.000E -01 4.346E105 3.2.444E105 0.000E -01 4.346E105 3.2.444E105 0.000E -01 4.346E105 3.2.446E105 3.2.446E105 3.2.446E105 3.2.446E105 3.2.446E105 3.2.446E105 3.2.446E105 3.2.446E105 3.2.246E103 3.7.22E104 1.313E105 3.3.073E104 1.313E105 3.3.073E103 3.7.22E104 1.313E105 3.3.073E103 3.2.23E103 3.7.246E103 3.7.22E104 1.313E105 3.3.224E103 3.2.246E103 3.7.226 0.0 3.000E -01 3.946E103 3.2.246E103 3.7.246E103 3.7.246E103 3.2.246E103 3		02E-31	1	224E	0.000E	E	1,5500.104	-	0.000E.01	
4, 9911E 103 6, 0005E -01 9, 9102E 103 7, 224E 103 1, 092E 104 3, 424E 105 6, 720E 101 1, 1322E 101 5, 434E 103 1, 036E 102 0, 606E -01 4, 444E 105 6, 720E 103 1, 323E 101 5, 434E 103 1, 036E 102 0, 606E -01 4, 444E 105 7, 113E 103 0, 0000E -01 4, 444E 105 1, 291E 103 1, 253E 103 1, 253E 104 1, 313E 105 1, 291E 103 1, 253E 103 1, 253E 104 1, 313E 105 1, 291E 103 1, 254E 103 1, 244E 103 1, 242E 104 1, 313E 103 1, 254E 104 1, 313E 105 1, 291E 103 1, 254E 103 1, 244E 103 1	4. 9911E 103 6.000E-01 9.910E 103 7.224E 103 1.092E 104 3.424E 105 3.424E 105 1.323E 101 5.430E 103 1.036E 102 0.606E-01 4.346E 105 5.120E 103 1.323E 101 5.430E 103 1.036E 102 0.606E-01 4.346E 105 5.256E 103 1.323E 103 1.242E 104 1.242E 104 1.242E 104 1.313E 105 1.323E 103 1.242E 104 1.242E 104 1.252E 104 4.033E 104 1.313E 105 2.323E 104 4.033E 104 1.313E 105 1.323E 103 1.642E 103 1.242E 104 4.035E 104 1.313E 105 2.323E 104 4.033E 104 1.313E 105 2.323E 104 4.033E 104 1.313E 105 2.323E 104 1.313E 104 1.335E 104 1.313E 105 2.323E 104 1.325E 104 1.335E 104 1.335E 104 1.352E 104 1.342E 103 1.734E 104 1		101. 104	. 8	AlluE &	0.000E	17:50	154E	-	80	
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3, 170E 103 1, 333E 101 5, 435E 103 1, 910E 103 0, 606E -01 4, 445E 105 7, 1131 132 103 1, 256E 102 1, 634E 103 4, 756E 103 1, 910E 103 0, 0006E -01 4, 445E 105 1, 291E 13 0, 2073E 103 1, 1072E 103 1, 242E 104 6, 903E 103 3, 733E 104 1, 313E 105 3, 733E 1, 613 2, 174E 103 1, 616E 103 2, 274E 103 1, 616E 103 2, 764E 103 2, 764E 103 1, 764E 1	3, 170E 103 1, 333E 101 5, 430E 103 1, 910E 103 0, 600E - 01 4, 442E 105 1, 5,56E 103 1, 634E 103 4, 750E 103 1, 753E 104 1, 313E 105 1, 634E 103 1, 753E 104 1, 313E 105 1, 635E 104 1, 313E 105 1, 635E 103 1, 635E 103 1, 635E 104 1, 635E 103 1, 756E 103 1, 756E 103 1, 756E 103 1, 994E 103 2, 254E 103 1, 756E 103 1, 756E 103 1, 994E 103 1, 754E 103 1, 7		1 26. 10.7	-		-		44.4E	730F1	6.000E-01	1 11111
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7, 440E 104 0.000E -01 3.912E 105 7.020E 105 1.904E 105 7.914E 104 1.334E 104 1.324E 105 7.124E 104 1.722E 105 7.124E 104 1.334E 105 3.974E 105 0.000E 01 5.054E 102 7.012E 102 4.102E 102 4.324E 101 0.000E 01 3.504E 101 5.003E 101 4.370E 101 3.974E 100 0.000E 1.341E 101 5.000E 101 1.341E 101 1.370E 101 1.394E 103 5.094E 101 5.000E 101 1.341E 101 1.394E 103 4.74E 103 4.970E 03 0.000E 01 1.550E 01 1.070E 04 6.494E 05 2.950E 103 4.746E 103 4.740E 103 0.000E 01 3.974E -02 3.3304E 05 1.554E 103 4.740E 103 4.940E 103 4.940E 103 6.000E 01 3.974E -02 3.3304E 05 1.554E 103 4.940E 103 4.940E 103 6.000E 01 3.974E -02 3.3304E 05 1.554E 103 4.940E 103 4.9	7, 441E 104 0, 000E 01 3,923E 105 7,02ME 105 1,904E 105 7,945E 104 1,52,92E 104 0,000E 01 4,630E 104 1,344E 105 5,542E 104 1,172E 104 1,722E 105 7,125E 104 1,525E 104 1,525E 104 1,525E 104 1,525E 105 7,125E 104 1,525E 105 0,000E 01 5,054E 102 7,812E 102 4,102E 102 5,534E 101 1,945E 101 0,000E 01 1,544E 101 5,002E 101 4,270E 101 3,975E 101 5,500E 101 1,344E 101 1,594E 103 3,470E 01 0,000E 01 1,975E -01 1,074E -04 4,970E -03 0,000E 01 3,975E -02 3,062E 103 1,564E 103 4,570E -01 0,000E 01 3,975E -02 3,062E 102 3,000E -01 1,5440E 105 1,5440E 10		17.16.403	4.95allt 1	3.044	7.40311	0.47061	1	-	1	
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4 0.050c 01 5.40H 105 6.110E 105 1.723E 105 7.125E 104 1.334E 102 0.050E 01 5.054E 102 7.812E 102 4.102F 102 4.53HE 101 8.75HE 101 0.055E 01 3.544E 101 5.042E 101 4.270E 101 3.975E 100 0.000E 10 0.050E 01 1.484E 101 6.770E 101 3.975E 100 0.000E 103 0.050E 01 1.484E 104 5.750E 101 1.594E 105 3.835E 103 0.050E 01 1.554E 101 1.07HE 04 4.495E 05 2.954E 103 4.746E 103 0.050E 01 3.975E -02 3.304E 001 1.904E 05 1.554E 103 4.740E 103 0.050E 01 3.975E -02 3.304E 001 1.904E 05 1.554E 103 4.740E	14 0.050k 01 5.40HE 105 6.11HE 105 1.722E 105 7.125E 104 1. 15 0.000k 01 5.054E 102 7.812E 102 4.102E 102 5.53HE 101 H. 16 0.000k 01 3.504E 101 5.005E 101 4.270E 101 3.974E 100 0. 15 0.000k 01 1.404E 100 9.442k 04 5.922f 04 5.956E 103 5. 15 0.000k 01 1.554E 01 1.07HE 04 5.492E 05 2.954E 104 3.4. 16 0.000k 01 1.554E 01 3.304k 05 1.904E 05 1.554E 103 4.		1013.01		-	1.3454	5.54281		-	6.000E	HINE I
102 0.000E 01 5.054E102 7.812E102 4.102E102 4.53HE101 8.75HE101 0.000E 01 3.974E101 5.000E 101 4.270E101 3.974E100 0.000E 0.000E 01 1.484E101 5.000E 01 4.270E101 3.974E100 5.000E 103 0.000E 01 1.484E100 9.842E 04 5.925F 04 5.956E103 5.094E103 0.000E 01 1.550E 01 1.07HE 04 4.494E 05 2.944E103 4.746E1 03 0.000E 01 3.975E 02 3.304E 03 1.904E 05 1.554E103 4.930E	E 02 0.000E 01 5.054E 102 7.812E 102 4.102E 102 5.53HE 101 B. E 02 0.000E 01 3.5HE 101 5.0HE 101 4.270E 101 3.974E 100 0. E 03 0.000E 01 1.484E 100 9.843E 04 5.923E 04 5.936E 101 5.816 1 1.594E 103 5. E 03 0.000E 01 1.55HE 01 1.07HE 04 5.494E 05 2.944H 103 4. E 03 0.000E 01 1.55HE 02 3.004E 05 1.904E 05 1.554E 103 4.		20.64 164		-	6.11111.1	1.72361	7.135E1	-	0	11016
101 0.035 01 3.584E101 5.082E101 4.270E101 3.974E100 0.000E	101 0.0336 31 3.58448 101 5.0828 101 4.2708 101 3.9758 100 0.038					7.81%	4.10211	4.53HE 1	75111	0.000F-0	11110
NE 02 0.000E 01 1.484E100 9.442E 04 5.922F 04 5.956E103 5.095E NE 103 0.000E 01 5.200E104 5.200E101 1.343E101 1.592E105 3.633E NE 03 0.600E 01 1.550E 01 1.070E 04 6.492E 05 2.950E103 4.716E NE 03 0.600E 01 3.975E 02 3.304E 05 1.904E 05 1.504E103 4.716E	HE 92 0.000E 01 1.484E100 9.842E 04 5.922F-04 5.95GE101 5. H 103 0.000E 01 5.200E104 5.200E101 1.344E101 1.592E105 3. HE 03 0.000E 01 1.55UE 01 1.07H -04 5.492E-05 2.92UE103 4. M 03 0.000E 01 3.97AE 02 3.304E 05 1.904E-05 1.554E103 4.	· •				- 10	4.370E	975E1	1000	0.000E 0	1 1171K
H 103 0.0001 01 5.200E 104 5.200E 101 1.343L 101 1.592E 105 3.035L 105 01 0.600E 01 1.550E -01 1.070E -04 4.492E -05 2.950L 103 4.716E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304L 05 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304E 01 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304E 01 1.904E -05 1.554E 103 4.930E 101 0.000E 01 3.972E -02 3.304E 01 1.904E -05 1.554E 103 4.930E 101 0.000E 01 0.000E 01 3.972E -02 3.304E 01 1.904E -05 1.554E 103 4.930E 101 0.000E 01 0.000E	H 103 0.0001 01 5.200E 134 5.200E 101 1.343L 101 1.592E 135 3. HE 03 0.000E 01 1.550E 01 1.071E -04 5.492E -05 2.920E 103 4. M. 03 0.000E 01 3.972E -02 3.304E 05 1.904E -05 1.554E 103 4.					9.64.36	5.423		075E	0.0000.0	11111111111
01 6.600E 01 1.550E 01 1.070E 04 6.492E 05 2.950E 103 4.746E 01 0.000E 01 3.975E 02 3.304E 05 1.904E 05 1.554E 103 4.740E	03 0.000E 01 1.550E 01 1.070E 04 4.492E 05 2.950E 103 4.03 0.000E 01 3.974E 02 3.304E 05 1.904E 05 1.554E 103 4.01 0.000E 01 1.500E 103 0.000E 01 1.500E 103 0.000E			10 1000 0	2.00	5.400E	1.34511		0.351.1	10.000E 01	
01 0.000E 01 3.974E-02 3.304E 05 1.904E-05 1.554E103 4.930E	03 0.000E 01 3.974E-02 3.304E 05 1.904E 05 1.554E103 4.	1 4		6. GOOF 01	8.	1	4.494E	2.9444.4	-	0.1000.0	1 11 11 1
THE RESERVE TO STREET OF THE PERSON OF THE P	101 0.0001 01 5.054E102 2.062E102 0.000E-01 1.600E105 0.			0 000F 0	1	3.304	1.904L	1.55461	-	0 .0000. 0	1 1 11116
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, T			U		2.0031	0.000E-	100	0.404E 104	0 - 30000 0	1 1 111111

TABLE 5 (COUT)

Page 12 of 12

FAILUAY DUBE PARAMETER FACTORS FOR IMPLEMENTING TO CFR PART 20 (For Section 2.2.1.b, units in mrem/year per pCt/ms).

	CKITICAL	171-19	1 that	1 10016	1 1846	Linio	61.111	4 (15-16)	1111111	1111111	1 11941		1
	BKIN	9.044E-02	0.000E-01	0.000E-01	0.000E-01	0.000E-61	0	0.000E-01	0.000E-01	0.000F-01	0.000F-01	2000	2000
	177-19	5.950E 104	2.154E104	4.970E164	1.4016165	3.724E104	4.2846103	3.220E105 3.123E104 6	7.790E104 1.470E104	3.96:E104 3.5:45104 0.000F	4.77%E104	3 44.36 14.65	3.49.15 104
	t time	8.218E103	5.145E105	1.142E105	3.192E104 1.211E104 5.374E105 9.843E105 1.481E105	1.974E163 4.324E105	4.720E-03 1.610E103	3.320E105	7.79uE104	3.963£104	3.274E105 6.650E107 4.775E104 0.000F	4. 41 16 10.7	5. 95cF 10a
	KIDSEY	0.000E-01	5.350E103	5.443E101	5.374E103	1.974E163	4.720E-03	7.93UE 103 8.134E 103 3.150E 103	0.000E-01	0.000E-01	3.374E105	3.053E104	4.433F101
	LIVER	3.744E-01	1.355E 104	1.932E102	1.211E104	5.2356 103	1.840F 32	B. 134E103	9.03ist 101	9.013510.9	0.000E-01	0.000E-01	3.3166101
	DOME	9.044E-02 0.000E-01 1.030E100 3.744E-01 0.000E-01 8.218E103 5.950E104 9.044E-02	2.773£104	2.924E102 1.933E102 5.443E101 1.162E105 4.970E164 0.000E-01	3.192£104	1.400E 104 5.235F 103	4. 700E -02	7.93UE 103	2.730L162	1.3946101	1.400E107 0.000E-01 3.274E105	1.341E107 0.000E-01 3.053E104 4 41 9 107 1 41 9 05 0 000E 01	.0/25101 0.600E-01 3.710E103 3.310E101 4.432E101 5.950E104 2.4005 104 0.4006 A.
	THYKOID	0.000E 01	9011E 103 0.000E 01	0.000E-01	0.000E-01	0.000E 01	0.000E 01	994E 102 0.000E-01			10	9.3	0.600E-01
NOT DE PRI	W. BOLY	9.044E-03	1 . 9 HIR 103	2.2136101	1.7241.103	4.985E102 0.000E	2.40df 03	4.99aE102	9.534E 130 0.000E 01	3.123E103	U. 490E103 0.000E	7.93BE105	1.075E101
FARMAY I IMEGALION	no Isofort	71 IA-142	111	CF 143	1111	141.141	1K-144	111-147	100	187	1 245	11-230	rtt 239
33	=	7.	~	7	-	?	1	1	7.10	12	100	=	18.3

TABLE 6

Page 1 of 39

(For Section 2.2.2.b, units in mrem/year per pG1/m3).

AGE I ADIR T

105 7, 253E102 7, 529E102 7, 529E 105 7, 253E104 7, 253E104 7, 253E 104 2, 459E104 7, 253E104 7, 253E 105 1, 053E104 0, 050E-01 0, 050E 105 3, 517E105 3, 255E105 0, 050E 101 0, 050E-01 4, 300E105 0, 050E	1	0.000E 3.433E 3.459E	.6292462 0.
7.429E103 7.429E103 7.4 2.459E104 7.253E104 7.2 1.043E109 0.000E 01 0.0 3.517E102 3.255E103 0.0 0.00E-01 4.300E103 3.7	200	. 632E 1	-4292402 0.000E-
7,243E104 7,243E104 7,2 2,459E104 2,459E104 2,4 1,043E109 0,000E 01 0,0 3,517E102 3,254E102 0,0 0,000E-01 4,300E103 3,7 0,414E104 2,504E104 0,0	A 13 11	45964	
2,459E104 2,459E104 2,4 1,043E109 0,000E-01 0,0 3,517E102 3,256E102 0,0 0,000E-01 4,300E103 3,7 0,41E104 2,504E104 0,0	-	429E#	.243E104 3.432E1
1,50518 107 0,50008 -01 0, 3,5176 102 3,555 103 0, 0,0008 -01 5,5008 103 3,	١		104 2. 459E
0.000E-01 4.350E103 0.		-	. COOK 01 1./10E1
0.000E-01 6.300E103 3.	-	1.794E	.0001 01 1.7
B. 414E 104 2.504E 105 0.	7		. 799E 104 0.
	7	*	.030E-01 0.
4,129E-03 5,242E-03 0,	-	. *	010
1.735E107 0.000E-01 9.	=	2.511E	01 2.
4.978E 107 0.000E 01 1.	=	2.949E	-01 2.
4.724E104 0.000E-01 0.	4	*	0 10
107 0. CODE - 01 0.	7	0.000E	0
108 1.735E108 0.000E 01 0.000E	*	5.059E	0.000E 01 5.059E
09 4.654E10B 0.009E-01 0.		4.729E1	-01 4.729E
01 4.810E 02 0.000E 01 0.000E	*	3.702E	1 3.
2.351E104 5.553E104 6.	-	0.000E	01 0.00
9 4.343£169 2.910E109 0.	-	1.371E1	.000 0: 1.37
4.354£ -12 4.079E-12 0.	1	4.093E	. 0 30CC .
0.000E-01 0.000E-01 0.	7	3000.3	. COCE - 01 C.
0.000E-01 0.030E-01 0.	T	0.000E	.000E 01 0.
0.000E 01 0.00CE 01 0.	1	0.000	010
2.2711.107 0.000E 01 0.	F	0.000	.000E 01 0.
-61 6,000E -01 0,000E -01 0,	F.	0.000E	0.00 to 3000.
		1 45.06	0 0000 01 0 0000 0
110 0 000 0 10 0 000 0 0		4 Ailist	0.000
104 0.660F 01 0.000F 01 0.		3.69.5	0001-01
01 0.000£ 01 0.000E 01 0.	6 6	4.61361	-01 4
0.000E-01 0.000E 01 0.	-	7.091E	-61 7
01 0.0000 01 0.		4.41BE	.000E 01 4.41
0.000E-01 0.000E-01 0.	-	- 2	.0001 01 8.
0 0.000E 01 0.000E 01 0.	k. i.	5.5.56E	.000E 01 5.
0.606E 01 0.600E 01 0.		2.317E	01 2.
02 4.041E 102 4.774E 102 0.030E	100	9.403E	1 9.4
-01 U.724E 02 1.31HE 01 0.000E	766	4.324E-	. 32.4£

TABLE 6 (CONT) Page 2 of 39 (Nor Section 2.2.2.b, units in mrem/year per pct/m3).

GIR I AMN I FATHRIAY I COM NILK

CKITICAL	111-19	177-19	111.19	111-10	W. foliar	01 11.1	111-19	111-19	11119	111 19	11119	Klinth Y	KIBIRY	111119	111.19	KIMMI	1111	h listif. f	111119	HILL-LALE	und.nib	HIMMIN	Install	HEREBIE	HICKOID	LIVER	11911	11.71.16	11.71.1	H. Miller	11111	111119	-	u. bultt	111 19
ENIN	0.0006-01	-0000.	-3000°		X	.000E	0.000E-01	0.0006.01	- 9000 ·	0.000E 01	0.0000.0	0.000.0	0.000E-01	0.00GE 01	0,000E 01	0.0001-01	0.000E 01	0.000E-01	0.00E 01	0.00cc.01	0.0001 01	10 1000.0	0.000.01	0.000E 01	0.000.0	. 000E	0.000E 01	0.000E 01	0.000t-01	0.000E 01	0.0006-01	0.0001.01	0.000E-01	0.000E-01	0.000E-01
177-10	2. 7ilcE 100	1	.73351	5.4401.103	. 1000	*	5.3071 01	1.3:11 164	2,1791110	5.2401.107	7. 11 01 1611	4.507.167	1.5.84 100	5.25JH 104	3.0321 101	2.5 HE 10	1.7.3 107	0.0001 01	7.3171.107	1.0021 105	1.1101 100	7.54.4 02	4.0416105	4.44.91 15	3.711E101	-	1.172 108	1.95 11 160	0.734£ 29	0.0001 61	7.85.11 015	5.5.311.107	0.000E 01	0.000E 01	1.5746 105
t und	0.000E 01	J	3000 ·	4.577£100	- 3000 ·	T	0.000E 01	I	0.000E-01	0.000E-01	2.0014:007	16 3000.0	0.000E 01	0.0005-01	6.000E 01	0.000E-01	0.00CE-01	0.000E-01	0.000E-01	T	6.000E 01	0.000E-01	I	0.0001-01	0.000E-01	1.4456109	7.857E107	1.1351.109		0.000E 01	11.79:16 -11	1.9338104		0.000E-01	0.000E 01
K.1 DNEY	4.530E104		. 400E 1	1.450E102	0.000E-01	13768.	1.131E-03	3.949E104	1.059E138	9. BUILE 105	0.300E 01	4.429E107	1.850E 108	2.714E103	2.50UL 108	1.415E -05	-	1.913E 32	-	1.919E102	7.24E 10B	5.397E 01	1.177.1.107	8.155E-12	5,3111,104	-	5.739£ 100	3.427L109	1.5034 23	0.0006-01	2.95.31-11	1.1471.104	0.000E-01	0.0001-01	0.000E 01
LIVER	4.591E104		. 473E1	9.545£100	0.000E-01	. 0000.	0.000E-01	0.000E-01	5.300£ 10?	1.2 tak 105	4.6731.105	5.905E 103	1.4.35£107	2.39.3E 102	2.2426107	1.245E 10	1.744 105	0.000E-01	1.5476 104	1.347£104	4.237£10B	4.01tf-01	-	5.12dE 12	3.31.1.164	127	1.012109	1.007E110		10 30:0.0	3.15%E-11	3,3/46104	. 000E		2. 200f. 100
DONE	8.253E104	. BBGE -	0.000E-01	-	- 1	-	8.474E-04	2.040E104	5.u25E107	7	2.504E167	1.630£107	4.57IIE 107	3.443E102	4.009E107	3.35/E-10	-	0.000E 01	-	7BE 1	3.943E 108	1.501E 01	3.6776105	1.00/E-13	1.245E104	5361	2.51 JE 108	7. Juit 109	3	0.000E 01		2.485E137		300	4.523E100
HITKOID	.000E	0.000E-01	-3000°	-3000°	- 3000 ·	3000°	0.0001-01	0.00CE 01	3000.	0.000E-01	1013515.7	-	1.170E167	1.94/1102	2.04 11 107	2.504£-10	-	0.000E 01	1.70%E105	-	1.30%	1.405E101		0.605f-11	3.104L105	I	0.000.0	3000 ·	10000	10 Jeou. 0	3000°	1000.	10000	1000°	0.000E-01
W. BODY	2.44BE 104	5.419E-13	-	1.215E103		4.376E102	3. 4.mt 04	2,56.3,10.1	3. Book 107	3.9BH 104	1.0211107	2.16.11.105	5.577E 105	1.1124.102	9.5111.105	B. 36.3E-11	1.4704.105	0.000E 01	1.45.11.04	4.9001 165	2. 4244 106	1.405E 01	2.054E105	1.6341-12	1.22.3 104	-	7.4 E.E 100	2.2131109	1.01.11 23	1.000	-	=	1	-	5.035£ 01
nn ISDIOFE	NB 95	HB 97	NI 59	11C 99H	101-31	KII-103	105	103	11011		124	1.25m			-		-						1-133	1 134	1 133	1.5 1.14	751 53	Ch 1.17	1311	CE 139	lic. 1.59	Dr. 140	la 141	les 142	17, 140
1	*1	17	313		40	:	4.3	4.5	* *	4:5	*1	11	41.	45	200		****	MT	:	174	77.7	100	=	67	7.0	7	-1	7.3	+ 1	7.7	77	-	7.11		7.0

TABLE 6 (CONT)

(For Section 2.2.2.b, units in mrem/year per µC1/m3).

TATE I AND I

CRITICAL	171-19	111-19	111 19	111-10	11119	u. bling	111-19	177-10	111-19	FILLIE	Dinie	177-19
EKIN C												
01-111	9.141E-12 4.145E-12 0.000E-01 0.000E-01 3.042E-00 0.000E-91	1.252E107	1.150E104	1.2096100	4.914E105	0.0004 01	5.27.35 105	4.9875107	1.79 11:104	3.010E160	6.415£108	1.120E100 0,000E-01 7.15:4101 0.000E-
1-UNG	0.000E-01	0.000E-01	0.00 GE -01	0.00CE 01	0.000E-01	0.6005 01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0,000E-01
N. I INEY	10-3000.0	1.521E103	1.355E101	0.650E104	3.554E101	0.00CE -01	6. 459E 101	0.000E-01	10-3000.0	7.236E100	4.743E108	1.120E100
LIVER	4.165E-12	3.276E103	3.07BE 104	1.495E 105	4.331E101	0.000E-01	1.000E 103	4.315£105	5.474E103	0.000E-01	0.000E-01	3.591E-01 1.1
DONE	9.141E-12	4.84E103	4.143E 101	3.577E 105	1.57tiE 102	0.000E-01	9.412E101	1.29BE 104	4.551E103	3.099E 109	2.944E109	3.452E100
HITKOID	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.000E 91	0.000E-01	0.000E-01	0.000E-01	0.000E-01
M. BODY	1.0386-12	3.715E103	3.405E100	1.920E134	7.423E 100	0.000E-01	4.5091100	4.5.19E101	1.915E103	1.117.11E 1 GB	1.75HE 100	1.979E-01 0.000E-01 3.
no Isolar	14-143	CE - 141	CE-143	CE-144	FE-143	14 144	711-111	100 m	W 187	11-235	11 2.18	13. 239
=	-	73	13	*	127	2	1:1	7.00	12	011	117	83

TABLE 6 (CONT) Page 4 of 39

(Not Section 2.2.2.6, units in area/year ner hC/m).

					d jost	pect ton	7.7	4 . D.		111 111 111	mite in mentacat her her w			
P. I.	I J	AGE 1 TEEN FATHWAY I COU HI	2 2											
3	no tenfort	3.40	3	PODY	THYKOLD	9	MONE	-	LIVER	KIDIEY	FINE	01-111	EKIN	CKITICAL
***	7-11		9.930	£103	9.930E	102	0.000E-0		1000	9			.93uE 1	
cı	F-14		1.345	-		-	. 499Es	. 1 50	-	-	1.340E +0	. 3 16E	1.340E	
7	113 3		4.29	-	4.2946	-	. 294E 1	÷	-	9	4.294E10	4.294E1	-3000°0	
+	F-32		1,223	-	0.000E	1		0 1.	-	0	0.000E	45.56.	0.000E	
77	BC 4	4	1.307	-	0.000E	T		2 4.	-	4.202E102	•	. 1117£ 1	9.000E-	
7	CK S	-	4.994	-	2.775€	101	0.000E-0	1 0.	000E-01	9	7.131Et	1 8.393E102	- 3000° 0	
1	HIN S		2.77%	100	0.000€	1	-3000°	-	10261	4.101E105		11/11	0.000E	111-10
=	5 111	9	1.302		0.000E	7	7	01 7.	30EF	9.245E-03	0.000E-0	1 4.01BE-61	0.000L	
0	1	2	7.354	-	0.000E	0	4.454E10	m	-	0.000E 0	a	-	3.000E	
10	1 E 5.9	•	4.470	-	0.00CE	T	***	-	209E 168	- 3000°		1 1078.	0.000E	
=	2 03	13	1.833	-	0.000E	10-	- 2	1	95361	7	. 0000.	13760'	3000.0	
77	CII 5	0	4.34	-	0.000E	T	X	ci	130E	- 3000°	.000E	-	6.600E	
7	92 JH	*	1.069	1001 3	0.000E	J	-	ci	230E108	3000°	0.000E 0	-	0.00GE	
-	7 114	-	4.00.	-	0.000E	1	1.182611	0 8.	3 40E !	-	- 3000°	-	6.000	
-7	111	n	3.94	3	0.000E	T	777E		42.9E	T	. 000E	13567	0.000€	
5	CII 44		1.979	E104	0.000E	0	7	+	205E 1	9	0.00cE	377E	0.00CE	
17	2111 5	0	3.411	-	ė.	1	2.105E10	9 7.	312E 109	4. 490E 109	0	1 3.0%7E109	0.000E	=
=	711 5	5			ó	81	8	5	714E-11		1000.	35.71.	100	3
1.7	Die fo	7	1.079		ò	T	T.	0 .	3000		.000E		- 9000°	2
20	146. 8		2.53		ò	30	1	010	3000	T		3000	3000 ·	3
7	lik u	0	0.000		0	7	T	1 6.	-3000	- 30 0 0 ·	. 000E	BOOD.	3.000E	3
e!	6.44 13	-1	2.2176	£109	0	10	7	. 10	723E 109		T	1 4.989£ 100	6.000E	LIVER
7	6.6. 0	10	0.000		0	A.	-300	1 0.	10-3000	0.000. 41				i
7:	N.B. B	6	0.000		ó	Ð	0.000E-0		DOOF	. 600E	- 3000°	1000	0.000E	;
711	EK B	63	7.455	-	ò	æ	3.473110	9 0	3000	*	- 3000°	110161	0.000E	100
77	E.K. 9	0	1.43	11.110	0.000E		-68	0 0	10-3000	I	- 3000 ·	1750	\$000.0	2
-	Ek 9	-	2.0%	-	0.0000		5.274E10	0 1 0.	0000 -01	P	J		0.00CE	61
412.	14. 2	ÇI	1.1.		ò		T	1 0.	3000	J000.	. 000g.		-3000 ·	17
25	0 A		3.51.	0013	ò	5	-	9	3000	I		-	0.000F	1 19
30	1 91	=	4 . 47		ò		1.175.	19 0.	Œ	3000°	T.	1 5.5401 10	0.000E	3
7	16 1		4.2326	-	0		-	.0	10-3000	I	T.	75	- 3000°	=
-	77		2.97ak	L 05	o.		1.02% C	.0 +	3000	0.0000	0.000E-0	1 2.11:36 100	0.000E	3
77	1 93		1.17		ò		73E	0 10	0000	31	£			T
1.5	24.	in in	3.1.010	-	0.000	10	1117	03 15.	1E 1	4.02LE 105	0.000E 0	1 1.20uf 165	0.0001.01	4
37.5	24.7	1.	7.17.	T-03	0		- 1	.1 1.	5:57k - 01	2.341E-0	0.000E-0	1 4.2176104		177 19

TABLE 6 (CONT) Page 5 of 39

(For Section 2.2.2.5, units in mrem/year per (R.f.).

FATHWAY I COM MILK

He Part He He He He He He He H		EAL		-	===	H. Y	=	LUGY	1	-	-	100	-	-	-	LY	-	1.1	-	-	F 1	-	110	110	110	1111	1111	410	2		30		Miller				111
1801		CKIT			119	KIN	1 19		-	DI	1-10	1-10	1 10	1-19	119	KIMI		HI4	1-10	-	FIL	1 1	THERE	fill.t.bi	HILLSON	HEADI	HILLOI	HEROI	1101		11011	1191	3				3
Heart Hear				1	30	. 1	Ŧ		T	.1	- 3		.1	.10.	. A.	. 81	10	10	3	0	0	10	10	10	10	0	0	10	10	0	10	10	10	10		10	00
150110FE U. DRIFY HYKRDID BONE L.1VER KIDHEY LINNI DITOLOGO D. 1502E D. 1500E		EK IN		*		0.000	3000.0	0.000E	4.000E	0.600E	0.000				*	*				3000 · 0	0.000E	3000.0	\$0000 g	3000.0	0.000k	C.COOE	10000.0	0.000E	3000 · 0	0.000E	Joco . 0	3000 O			THE PARTY AND TH	- 3	0.00GE
15010PE U. DOINY DONE DONE LIVER KIDNEY LINKID LINKID LINKID LINKID DONE LINKID LIN		=		-	1	-	-		-	-	-	-	-	-	-	11 1:10	-	-		-	77	-	-	-	n	***	8	**	-	-	-		3	I		-	E 01
15010PE U. DANY HYKOLD DANE L. VER K. DAEY L. LANG HIP 95 4.97 E 104 0.000E - 01 1.407 E 103 7.607 E 104 7.567 E 104 0.000E - 01 7.507 E 104 7.567 E 104 0.000E - 01 0.000E - 01 4.44 E 107 1.023 E 108 0.000E - 01 0.000E		-		*		1.99	1.67	0.00	17:17	1.37	1.80			*	=	*	4.53	-	3.3%		0.00	6.27	1.67	1.40	3.03	9.000	1.17	2.4	2.073	1.409	2,111	1.43/	0.000	7.314		1.470	7.47ut
Harry Harr			4		F	8	100	0	0	0	0	0	0	107	3	0	0	10	0	0	10	0	0	0	0	0	0	5	00	=	60	*	01	=		10	00
Harring Harr		LIMB				0.000	4.070E	0.000E	0.000E	9.000E	0.000E	0.000	*		0.000	0.000	0.000	0.000	0.0001	0.000	0.000E	10000.0	0.0001	10000.0	0.000	0.000	10000.0	0.000E	1.00.1	*	*	3.09%E	3000 · 0	3.9/54	A SALLING M.	4.77% L	0.0000
15010FE W.		HE.Y	-		F 4	-	-		-	10	-	-	-	V.	T 4		-	-	6 4	-	1 4	-	•	-	-	-	1 4		-		-	1	-			-	-
150101FE W.		KID	7.54		77.9	*			4. 13	1.77	7		2/20	000.00	0000	*	*	4.07	200.2		3.470		7.7.7					- 7	*	*			*		3	5	3
15010FE			-	F	- 14		-	f	8	1	1 4	-	•	-		-	-				1 4		100			701								-	6.0		0
		1 1VE			4 44 45			*				1 46.76	3000			AL 777.4	1020	4.0.	7 .	* 4	3000	3/0/	Try Col	30000	3,100	400 1	3600		*	3000		1/17	3	1	. 7.		.00
			02	13			000	3 5	70										200	-		* Y	700			20				1 9		7 0			4		-
		DOME	. 407E	5683				*									3000	1001	*- 1		1000	7	13161		0806		34111			1 1111	7 4	3 4			*		
		_	10		_									14	. ^					9 1 6	7		-	-	0	0						• •					0 1
		HIYKDI				- 9000 ·	0000	0000	U	0000	COCF	. 1	-			B (45)			-		-		-	-	-		-	1	i T		7	1	13				0-3000
		>	-	-					040			0 40	07 8	0.5 8	07 3	32 8	37 3	10	35	0 10	36 3	15	38 2	31 3	3.5. 1	-	11	0 0	0 %	0 4	13 0	0	0	4			0
EST	1	=	77E1	-357	_	-		-		-	31.1	34.			-	_			-		-	- 40	_		-	0.16	-	-	_	-				-	è		0 1
		3	4.33	5.93	B	3.1	0.00	7.75	4.15	4.73	5.2.5	5.1.5	1.31	1.01	1.60	3.65	1.74	1.10	2.4.5	0.00	3.54	11.53	4.64	3.50	1.65	3.17	2.14	1.07	1.17	4.30	1.10	0.00	3. 3.4			O. Gelle	0.0001
	-	# =	52	11	**	19m	101	103	105	6.5	101	15.cd	24	35H	37H	33	H452	61	31111	11	1.1	2	-	-	*	-		11	3.5	1.1	113	14	1.7	10		2.5	= :
# #A##################################		200	All I	1111	IIII S	16.5	11:	113	111	111	1910	113									-	1.1	1.1	1.4	-	-	1.5	-				12	-				
	*****	=		-																	-	2	775	11	Tree 1	1.5	207	.1 6.	-	1.1							

TABLE 6 (CONT)

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FAILMAY MISE PANAMETER FACTORS FOR INFLEMENTING TO CFR PART 50

(For Section 2.2.2.b, units in mrem/year per µC1/m3). AGE I BEEN FARBANT I COM MILK

=	TEM FIRE	W. PODY		HIYKUIL	Billite	LIVER	KIDNEY	nun't	177-10	SKIN	CRITICA
							0 0000-01	10 3000 0	20.3456.62	0.000E-01	91-11
1.	1.4 14.1	1.0.01	17 0	. COOP - 01	1.6538-11	1.311E 14	0.000	10000		20.00	01-11
2	1111	3.811E1	0.3 0	.000E 01	B. 001E103	5.929E 103	2.791E 103	0.0000.0	1.4756 107	0.000	
7.8	11.143	4.217E	0 00	.000E-01	4.21/E100 0.000E-01 7.49/E101 5.55/E104 2.49/E101 0.000E-01 1.4/3E102 0.00/E-0	5.55tk 104	2.497E101	0.000E 01	1.4736105	0.00.0	
*	(1 111	3.537E	0 10	.000t-01	4.582E105	2.724£105	1.6371.105	0.000E-01	1 . 435E 1 VII	0.000	
1	A 11 11 11 11 11 11 11 11 11 11 11 11 11	1.1438101 6	91 0	10-3000°	1. 113E131 0.000E-01 2. V00E102 1.15UE103 6.730E101 0.000E-01 V.541E103 0.000E	1.15u£103	4.7405101	0.000E-01	9.541E103	0.000	
72	11: 111	0.033E	0 10	. Coot 01	0.000E-01	0.000E-01	0.0000	0.000E-01	0.0000	20000	
27.	110 147	1.100E	0 191	0.0000.	1.811E102	1.95%E102	1.15/1103	0.000E 01	1.1035.00	3000	
713	u iff	2.00.1	101 0	.000E-01	1.675E104	5.550E 103	6.000E 01	0.000	2 4 3 4E 10.	0.000	-
200	11 1187	3.423	161 0	1.000E-01	1.19BE 104	9.7474103	0.0001 01	0.0000	2 00 15 100	0 0000	FADINE
611	13 2.3%	2.423	0 801	0.0001	3.999E169	0.000E-01	V. 1.: 1E 10H	0.0000.0	3.67 6 100	0 0000	FULLIF
101	10 230	3676 6	0 1171	1.000E-01	3.0240109	0.000E-01	8.724 108	0.0000	B. 277E 100	0.000	111
13.1	III. 23%	3.451E	010	1.000E 01	4.94.96 100	4.57.18 01	2.0331.100	0.0008-0	2014/201	1000.0	

)

(CONT) TABLE 6

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FAILMAY GOSE PARAMETER FACIONS FOR FRIEDENTING TO CFR FART 50 (For Section 2.2.2.b, units in mrem/year µC1/m³).

					A STATE OF	Chair a	11170	Car Tan	Cheffich
no Esolute	W. DODY	HIYK016	PUNE	LIVER	N I MIE I	Lumb	1111	DAIN	Fullian
1 11 1	1.5/06103	1.570E103	0.000E-01	1.570£103	1.5701.103		.570E1	-	W. SOBY
2 5 14	1.2946105	394E	. 547E1	3.294E105	3.294£ 105	3.294E105	.33	294E1	-
1 MA . 34	8.93 15 105	8.737E105	124	-	8.932E144	- *	0.93.4 102	3000	u. bully
0 4	601 1046 1.	.000E	70161	3.441E109	0.000E 01	0.000E-01	. Inch !	-3000	D(114
× 100.44		6006	91061	4461	3.456E 102	T	1.404£ 104	T	61-11.6
	1.0196105	-	DOOF	OGOE	1.545E104	-	2.4031105	0.000E 01	01-111
7 800 54		.000	000E	0771.1	-	0.000E-01	-	J	LIVER
10 Mil 2.4	3.003.6-63	0.0006 01	0.000E 01	377	1.514E-02	Ŧ	-	0.3001-01	111119
	- 100		-	5.930E107	0.000E-01	3.354E 107	1.6701.107	T	PONE
10 11 29	-	1	-	-	0.000E-01	5.4375.107	-	1	111-19
: :	3.719E107	3000	0.1	215E1		J.	-	à.	01-111
-	-	1	-	4.310E107	I	0.000E 01	-		11119
-		3	-	1.847E100	0.0000.01	0.0001 01	1.00:1:107	3	DOM:
	1.0001 109	J	-	HZE I	- 3000	0.000E-01	1.043720.1	0.000E-01	HINE
15 111 25	9.10.1 03	0.000E 01	571.1	0 80	3000	0.0006-01	1.91116101	T.	111 19
	-	I	K.E	-	ZHSE 1	0.000E-01	3.4701.105	1	111-19
		- 3	-	1.101E110	4.9376109	0.000E-01	1.9:31.109	1	2
77		0.000E 01		3,2036-11	11.7416-11	I	8	0.0000.01	11119
Sed.	T	0.000E	0.000E-01	0.00 JE 01	Ŧ	Ŧ.		Ī.	W. Peliby
	5.74% - 23	0.60JE	0.000E 01	0.0000.01	3	0.0000.01	Z.	0.0000 01	E. Billie
144		0.00CE-01	0.000E 01	0.0006.01	0.000E OI	0.000. 01	0.0001	Ŧ.	H. Beller
- 100	-	0.0001-01	0.000F 01	G. / LOE 109	0.000F 01	0.0001-01	5.4.35£ 108		2
1.1		0.000E 01	0.000E-01	0.0001 01	0.000£ 01	1	6.000L 01		W. bullet
	- 7	T.	.000E	0,000E-01	0.00ck 01	1			u. miler
200	1.0701.108	0.000E 01	4.414E109	0.000	0.000E 01	10-1000.0	2.531E100	ī	DOM:
1	-	D. COUE	1.11/1/1111	0.000E	0.000.0	T.	1.505.169	0.000E 0	=
á	7	0.000	131.5	B.Oute	0.000E 01	0.0006 01	2, HSHE 105	Ŧ	1 1 1 1
d	-	J	2.1435160	0.000E	0.0001 01	0.000E-01	4.09 1E 101	J	11110
	3	0	-	10.0001 01	6.000 61	Т	9.11171.105	0.000	01 111
		0	31	0.000E 01	0.030£ 01	0.660E 01	5.4231-14	E	01 111
>	11. 1	0.0001.01	3.9041.104	10 1000.0 1	0.000E 01	0.000E 01	5.200E 102	I	11119
30		0	2.1334 04	9		0.000£ 01	9.5E I	0.000E-0	111 19
11 7 93	2.finit 02	ó	1.019E100	10.000E 01	b.000f 01	T	7	1	1111
	7.5 KW 103	0.0001 01	1.053£103	-	-	8	15.1		111119
35 78 97	-	0.000E 01	1.915E100	3.74/E 01	3.97:1-01	0.000E 01	4.191E104	0.000E 0	111 19

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TABLE 6 (CONT) Page 8 of 39 (For Section 2.2.2.b, units in mrem/year per pc1/m3).

CATHROY I COW HILK

CRITICAL.	111-10	111-19	KIMEY	111-19	W. Buffy	111-19	11-19	171-19	111-19	111-10	171-19	FORE .	A LIME Y	61 111	F. HAHLA	111-11	111-111	117 19	61 11 1	manne	HINTEDID.	HINEOTE	HIMMIN	Inchile	HITCHIEF.	1 101 1	1141	Бини	11011	D. feller	11119	Bettek	te. bullet	u. Bubi	91-111
	3	0	0	0	0	0	0	0	-	0	0	10	3	0	0	0	10	10	0	3	10	0	0	10	5	0	ä	0	10	3	10	10	7	0	0
ENIN	0.000	6.000t	0.000E	10000.0	0.000E	0.000E	0.000E	0.000	0.000E	0.000E	0.000E	0.000E	0.630E	0.000E	O. DOUE	0.000E	0.000£	0.000E	0.000E	0.000E	9000.0	3000.0	0.000E	0.000E	0.000E	0.000E	6.000L	0.000E	0.000E	0.000E	0.060E	3000 O	0.0000	0.000E	0.000E
01-111	2.288£168	5.U38L-09	4.719E167	1.497E104	0.000E 01	1.1101105	2.535£ 160	1.4326 102	1.67ut 110	5.5.08 107	7.70.4 100	7.1316167	1.2011 100	1.10/E10t	3.364 108	9.5254 00	2,213,167	1.6291 31	4.5474167	1.4434 104	1.14/4 100	1.34.4 100	8.2738 105	9.761E 13	7.29% 104	2.0031 100	9.359E 107	1.9324 1001	2,9141 23	10-1000.0	1.1636 05	5.930t 107	0.000E 01	0.0006 01	1.0754 105
94011	0.000E-01	0.000E-01	0.000E 01	1.330E101	0.000E 01	0.000E 01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	2.1346167	0.000E-01	0.000£ 01	0.000E 01	0.0001-01	0.000E-01	0.000E-01	0.000E-01	0.0CUE -01	0.000E-01	0.000E-01	0.000F-01	0.000E-01	0.000E-01	0.000E-01	4.1.111.109	2.1936100	1.41ul 109	4.79.14 -24	0.000E 01	4.325E-11	4.1136104	0.000E.01	0.000E 01	0.000E-01
KIMEY	1.153E105	1.0436-13	1.735£100	3.629£102	0.000E 01	1.001E104	3.400E 03	1.210£ 105	2.6375 100	1.0535 105	0.000E-01	0.000E 01	5.932E100	B. 541E 103	7.955E 108	4.475E 09	5. 351E 106	S. 923E 32	4.194E107	5.3131.104	2,1531,109	1.771E100	3.545E107	2,254€ 11	1.450t 105	1.1516110	1.470E 109	1.005£110	1.4544 .13	0.0306.01	9.3731-11	3.33HE 104	0.0006 01	0.0000.01	0.0001-01
LIVER	1.237£105	1.580E-12	8.123E107	2.435£101	0.00CE 01	0.000E 01	0.000E-01	0.000E-01	1.411E10B	1.324E 104	5.100E 165	2.000£107	5.401E107	Ø.190€103	7.545£107	4.25%E 10	5.528E 105	0.000E-01	4.517E105	3.554E 105	1.31.E 109	1.15/E160	2.13/E107	1.47:4-11	9.575E104		2.74GE1C9	3.005£ 110	6.331E 23	0.000E 01	1.075E-10	1.6256105	0.603E 01	0.000E-01	4.797E100
BONE	3.17UE 105	4.259E-12	0.000E-01	1.344E 101	0.000E-01	4.294E103	3.048E-03	9.240E104	2.009£ 100	0.000E-01	2.751E107	7.380E107	2. Guo£ 108	1.037£163	2.70%E 100	1.2.30E 09	1.59"E 104	1.959E-32	1.0216107	1.759E104	1.304E109	6.29th -01	1.720£107	7.943E-13	5.3176104	2.244 110	1.00 1E 109	3.2246 110	4.5548-23	0.000E-01	2.015t -07	1.1700.100	0.600E-01	0.000E-01	1.94CE 101
HIYKUID	0.0006.01	0.000E 01	0.0006.01	0.000E-01	0.000E-01	0.00CE 01	6.000E-01	0.300E-01	0.0000	0.600E-01	4.344E104	2.0/2E10/	4.97 1E 107	2,103:103	8.734E167	1.0916 07	1.1371103	1.4996-33	5.5/UL 104	3.9124 108	4.335E111	5.359E101	3.95.1 109	3.393E-10	B. 4811 103	0.000E-01	0.000E 01	0.00nt 01	0.000	0.0001 01	0.600E 01	6.000E 01	10 3000.0	0.000E 01	0.000E 01
W. Buby	8.44.35.104	5.750E-13	2.669E 107	4.357E102	0.00m 61	1.451E103	1, 10 11 03	1.15.11.104	1.1246 104	4.23/4104	1.683E 107	9.841E105	2.4591107	2.51 M. 102	4.30:E107	3.4.101-10	S.IIII II 103	0.0001-01	5. 45/1104	1.11111 102	7, 45.£ 15B	5, 1:11 01	B. 01.01 10.5	6.7H4F 12	4.5.27.104	7.835E109	1.784E 109	4.1.1.4 109	4.6116 23	0.0304 61	S. H.171, 69	2.11111.102	0.0004 01	0.600k 01	2,1191 100
no Isonart	56 400	Hs 97	10 99	11. 99B	101 31	KH 103	KH 105	KH 163	NO. 110H	LI-115H	121 131	if Lith	11 1278	1771 - 11	11 129M	67 1 11	11 131M	11 131	11-132	1 130	1 131	1.11.1	1 133	1.134	1 1.55	Ch 134	CE 135	CE 137	CS 138	CS 139	14 1 157 tot	b6. 140	EA 141	Dei 14.2	14 1 10
2	3.5	37	311	3.5	10	-	-	**	-	17	4.5	-	2	44	200	17.7	27.42		* 27	25.5	72.5	* 77	211.5	577	277	-	**	17	*	Silk.	-1	17.7	27	6.2	70%

TABLE 6 (CONT) Page 9 of 39

PATISMAY MUSE PAKAMETER FACTORS FOR INFLEMENTING 10 CFR PART 50

				1	(נים מכ		7.7.7 110	D, units	(For Section 4.4.2.0, units in micm/year per julian).	tat per	7	1/18).				
e =	ME I CHIED	11 E Sh	HILK													
-	O ISOIONE	4	W. 505Y	Ann	DIYKOLD		BONE	LIVER	KIDNEY	THING		111-10	BAIN	2	CRITICA	4
200	1 1A-142	-	1.984	E-12	3000.0	10	3.9938-11	11.3735-11	984E-12 0.000E-01 3.993E-11 1.373E-11 0.000E-01 0.000E-01 2.532E-04 0.000E-01	0.000E-	10	1.533E 04	0.0006-0		61-11	100
-	3 Ct -141		1.430	1.103	430E103 0.030E-01	10	2.107£104	1.0916104	2.187E104 1.091E104 4.731E103 0.000E-01 1.341E107 0.000E-0	0.000	10	.3416107	0.000E-0		111111	-
74	3 (E- 43	_	1.474	E101	474E101 0.000E-		1.877E102	1.01uE105	4.2706 101	0.000E	10	. 190F 104	0.000E		G F - 1 1	- 14
~	4 CE-144	_	3.4.0	\$10E 104	6.000E	10	1.4235104	1.423E104 5.087E105	2.815E105	0.000E	10	01 1.3226 108	0.000E-0		61-11	* ***
174	75 116-143		1.561	Elei	541E 101 0.000E-	10	7.177E102	2.155£102	7.177E102 2.155E102 1.147E102	0.000E	10	7.7441.105	0		61-11	- 100
-	2 16 144	,	3.000	10-3000	0.000E	10	0.000E-01	0.000E-01	0.000E-01 0.000E-01 0.000E-01	0.000E		0.000E 01	0.000F		71	1
	7 HP 147		2. 7:34	1013	-3000.0 101 300.	10	4.4416102	4.441E102 3.400E102	1.975E102	0.000E		5.7034 165	0.000E-0		11-19	
Phy.	2		1.65	101 1	013 104 0.000E 01		1.343£ 104	4.5946105	1.343E104 4.594E105 0.300E-01	0.000E-	10	30ilt 107	0.600E-0		01-11	-
74	7 to 107		7.715	1013	719E 101 0.000E-01		2.905E104	1.7:0E104	0.000E-01	0.000E-01	10	. 41 /E 102	0.300E-0	-	11 19	-
-	=		1.66.	E 1 CH	997E 1CB 0.000E-01	0.1	3.299E109	0.000E-01	3.299E109 0.060E-01 7.593E10d	0.0006-	10	1.2136 100	0.000E-0		bount	
a	1 11 2311		1.47	1100	0.000E	10	3.155E109	0.000E-01	7.199E10B	0.000E	10	.6:VE 163	0.000E		LIMB.	
22	2 HF 219		9.427	10 1	0.0006	10	1.715.6101	1.2326103	437k 01 0.060k-01 1.715k101 1.213k103 3.541k100 0.6005-01 9.115k104 0.050k-01	0.000	10		0.000E-0		11-19	200

	FAIL	(Por Seci	Section 2.2.2	(For Section 2.2.2,b, units of	Inflenenting in mrcm/year	ind to CFK FART car per pC1/m3	C1/m ³).		
ME I INFANT	N HILK								
IN TROTOFE	W. MILLY	HIYKO16	BONE	LIVER	KIDNEY	1.1818	01 111	BKIN	CKITIC/
1 11-3	2. 3036103	2.382E103	0.000E-01	2.3026103	2.382£103	2.3626103	2. 382£ 103	2.303£103	W. 1001
3 6-14	4.00BE 105	4.00BE 1	-				BBBB.	. munk 1	DONE
3 HA 24	1.555E107	-	-	1.553E107	1.555E 107	1.555E 107	1.555£107	0.000E-01	W. MIL
4 F 32	4.31EE109	0.000E	1.4035111	9.432E109	0.0001-01	0.0006-01	2.147E109	0.000E-01	
5 bC-45	1.0701.102	0	1.910E	-	-	- 11	1.804E105	1	01-11
15 NJ 7	1.514E 105	1.0536105	0.000E-01	0.000E-01	2.300E104	-	4.704E105	T.	11-10
7 mil 54	8.817E105	ö	0.000E-01	-	-	1	-	T	LIVER
	5. 3471 03	0		3.124E	7		-	E	-
4	2.3311107	ė	1.351E10B	B. 729E i	Ŧ.		-	T	PUH.
4	1.5411.104	0	-	3.91 tit. 1	Ŧ	-	-	1	1 1 VEK
6.6	4.03:1E 107	å	T.	3.430E1	I	Ê	-	*	
93	2.001£100	ė	0.000E-01	B.disk	E	1	-	100	61 111
Ξ	B.905E107	i	-	1.847E1	T	T	-	T	COME
77	1.312£109	ė	-	ci	E	Ŧ	_	T	44
57-IN 51	1.801E 01	0	3.500E 100	3.9716	0.000E-01	1	3.023E101	1	11 11
63	8.507E104	o.	T	B	-	1	-	T	11-19
7.11	B.777£109	ó	5.550E 109	1.903E110	-	8	-	T	11711
211	4.319E 12	å	4.717E-11	8.493E-11	1	1	T	0.0001-01	11 19
1	9.803E 01		8	10 3000 0	T	50	Ŧ.	H	H. Fell
26 56 04	1.10%-22	0	T	T	Ŧ.,	7	T.	1	H. 1
ž	10 3000.0	0.000E 01	E.	0.000E-01	0.000E 01	50		T	N. 1651
Ť.	-	0.000E 0	T	2.223E110	3	8	2.4674 100	T)	11711
Ę,	1	0.000E 0	7			n	1	T.	LINER
	0.0000.01	0.0006.0	0.000E 0	0.0001-01	7	3		1.	H. HOI
	3.50% 100	0.000E 0	1.250E110	10 3000.0	B	G.000E-01	-	T	Petrill.
	3.0741110	0.000.0	1.3146111	0	0.0004 01	6.000.01	-	T	THE PARTY
	9.75.7E10.5	0.0006.0	2.494E105	\$ 0.000E-01	0.0001-01	0.000E 01	3.1931 105	0.000E 01	11-19
	1.70/E 01	0.000F.0	4.57/E100	10.000F 01	0.0001 61	0.000E 01	4.95.54 101	0.000F-01	11 19
	1.01301101	0.000.0	4.023E102	0	I	0.000E 01	-	6.000E-01	11 19
	4.	o ·		0.0006-01	0.0006.01	0.0006-01	2.039E 15	3	11 19
16 1 15	1.952E103	0	7.32/E10	.0	0.0001-01	0.00GE OF	5.353£104	T	11 19
		ò	0 3.75.6	10.0000.01	0.000E 01	0.000E 01	-	1	11 19
	6.09 IE 0.3	ė.	2.237E100	1 0.000E 01	0.000E-01	0.0006-01	1.7471101	T	11-19
51 2K 95	1,103,103		4.041E10.	1 1.45/E103	1.7978103	3	8.30% I 05	7	11-19
717	3.1701-01	0.000£ 0	1 4.054E100	0 3.95th -01	7.013E 01	0.0001-01	4.4301.104	0.000E-01	11-19

TABLE 6 (CONT) Page 11 of 39

				FA	(For Sea	Sect Ion	OR 2.2.2.b.	FACTORY FOR	(For Section 2.2.2.b, units in mrem/year		10 CFR PART 50 per µC1/m³).			
100	3	INFANT NY 1 COM	11											
2	1501061	DFE.	i	Attibi	THYKOLD	2	BONE	LIVER	NIGHEY	1100	177-10	EKIN	CKITTE	3
-1		10	3 . 4	3F 105	0.000E-0	10	5.932E100	5 2.44E103	3 1.751E10	5 0.0000-0		- J000E-		-
37	116 97		2	E1-307.	0.000E	***			1.643E	- 000E	1 5.83UF	0.000	91	-
=		*	4.04	95107	0.000E-	10	0.000E-01	ci	-	0	1 4.841E1	0	K I GM	1
3	11: 51	254		4246103	0.000E-0	10	2.795E101	5.745E	4	3.01361	1 1.474E	- 6	1-19	-
2	16. 14	10		6	0.000E-0	10	0.000E-01	2.000E-	0.1	0.000E	1 0.00CE	*		ı
=	E11 10	0.3	2.9008	-	Ŧ	10	B. 494E 103	0.660E	13600	0.000E	1 1.05/51	C.000E-	16	E
4	1111	020	2.747E		0.063E-0	10	8.154E-03	0.000E-0	1 5.997E-0	0.000E	1 3.215.E.	0.000E-	1-10	=
7	Kit 10	50	2.3776		1	10	1.90 SE 103	0.000E-		0.030E-	1 1.14SE1	0	91-11	=
=	ali - la	1 Ori	1.115.45		1	10	-	ci	8 4.030E108	0 3000 C B	1.151E1	0.000E-0	1-10	=
7	1 177	HUH	4.337E	-		01	0.000E-01	1.32261	1.052E1	0.000E	1 5.5.31116	0.000E-01	1-19	-
+1	111	**	1.01151	-		**	2.751E107	5.1001	0.000E	1 2.134610	2 7.7u2£101	0.000E 01	1-19	-
-	11	SSM	3.639E	-	5.074E10	03	1.500E 100	1 5.0131.107	7 0.000E-0	0.000E G	1 3	0.000E-0	DOM	
417	- 1	374	5.09.4	101 1/	1.217E10	98	4.211E 10B	1 1.197E 1CB	0 1.037E109	9 0.000E 0	1 1.477108	0.00CE	Klim	H.
2	-	37	1 . 3005k 1	28 193	5.249E10	23	4.449E103	ci	1.57361	0.000E	-	0.000E 61	1-19	=
20	44	17.61	8.54	11107	-	00	-	1 . 900E.	1.391E	9 0.00E-0	1 3.321E10	1 6.000E-C	KIME	#
3	-	5.5	7.5:81	10		60	X .	1.11111	0.071E	3000°		0.000E 01	1 19	=
7	4	NIS:		21E 135	- mar	603	3.375E 105	-	4 9.347E104	0.000E	1 2	T.	- 19	=
7	-	10	-1	3.2	1 3			1.234		3000.0	1 1.57uf 30	T	1 13	=
2 4	1	77	7.7	11.103		10	2. 10 1 107	1.0411	-	0.000		E	A. 1 mile	-
25.5	1 0 51	0.51	7.7	1.410F109	1.054F11	30	3. 41 4E 105	3 3075 100	4 H. 735E 105	0.000E-0	1.70:E10:	30	HILL	= :
7.	1 1 1		4.41	10-1	1.244610	0.2		ci	3.9406	0.000	2.1496 106	3 0		
3	-	**	1.54	1013A	9.319E1d	40	3.23 11 107	si	4.21%	0.000		0.000E		=
**	1 11	-	1.300	N-11	7.B:2E-1	01	11-3/19:1	ř	m	0.000E-0		-	III	=
2.5	1 1	*	8.0	1 101	1.77.JE 10	~	1. such 105	ei	5 2.4531.165	5 0.000E 0	1 7,94110	0.000E-01	man	=
-	f 1.		2. Gall	-	I	10	3.6478 110	4		3 7.17HE 109	9 1.84at 10E	0.660E-01	LIVE	4
	7.7	WT .	17.17	-		10	180	5.74BE	ei	+	4 8,75% 10.	0.000.0	LIMER	×
	1.2.		1	-	0.000E-0	11	-	4	-	vi	9 1.13E 101	0.000E-01	11011	4
* 7	1.15	113	1.22.1		0.0001		L	-	2 7.709f 3.	1 1,2151-2	3 2. lenf .m	0.000E-01	11-19	-
	17.	7.5	d.oout		9.000.0	310		ó		1000.0	1 0.000E 01	6.000£-01		=
1	1.4	2.5	1 411		D. GOOF O			2,013	-	3 1.723E-10	0 2.71% OC	0.0000.0	1 19	=
	100	10	1.::::	-	0.0001		-	3.40H	5 5,71HE 16	-		0.000E-01	Direct	
100	1.4	-	6.000E		0.0001	9	8	0.000E B	0.0000 1	0 3000.0 I	10.0001 01	0,030E 01	H. I	HIE
7.	1 54	-	0.000		ī.	9 1 6	- 100	ж.	0 1000.0 1	Æ.	1 0.0001 01	J.	H. IN	HIII
7.0	1 11 11	90	1.123	1100	0.000E 0	0.1	4.04 1E 101	1.403£10	0.000 0	0.000E-0	1 1.0031.165	0.000E-01	1 19	-

TABLE 6 (CONT) Page 12 of 39

FARIMAY LOBE PARAMETER FACTORS FOR INFLEMENTING 10 CFR FAKE 50 (For Section 2.2.2.b, units in area/year per pC1/m3).

-	Artici	INTROID	9	FURIE	LIVER	A STANE Y	1 11816)		111-10	ENIM	CKINEAL
3	E - 13	0.000E		8.380E-11	8.380E-11 3.07HE-11 0.630E-01 0.56ME-01 8 334E-04 0 4/AE-01	10.3000.0	0.0001-0		30.316.	0.000	
-	E 103	3.112E103 0.000E-01		4.3356104	4. 335E+04 2. 444E104 8. 153E+03 0. 000E	B. 153F 103	0 000E	::	1 144E 107 C 0000	2000.0	
100	DE 101	0.000E	10	3.974E103	2.4376105	7. 680F tot	0 000E	: :	\$30E	2000	
100	3636 105	0.000	10	2.335 104		3.644E105	0.000		1116130		
14.7	Ct 101	0.0006	10	1.485£103		2.0546 102	0.000F		B 1-E 10-		
-	10 30		10	0.000E 01	0.000E-01	3.600£-01	0 000E -		0000	2000	1000
-	5.5131101		10	B.809£103	9.0402103	3. 400E 103	0.00CF		2116 10:	100 OC 10	
100	31104	3000.0	10	1.3H2E 104		0.000E-01	0.000F		TO 11 107	2000	111111111111111111111111111111111111111
100	1.439E104 0	-	10	4.1146.104	4.253E164	0.000E 01	0 000 t		45115 104	3000	
	9E 10H	4	10	3. 399£ 109	- 12	2.493£ ±08	3.000E		. 14 (6 4 011		1001
	B0135	11/3E100 0.000E	10	1.125E109	0.000E-01	7.199E10B	0.000E-0	7	A. B. 14 4 6411 6.	70000	1000
-	SE 100	111 100 0.000E	10	3. 634E 101	m	4.48 100	0.000F-0		1000 9 5013.61 0	20000	

TABLE 6 (CONT) Page 13 of 39 PATHURY DINE PARMETER FACTURE FOR INFLEMENTING 10 CFR FART 50 (For Section 2.2.2.b, waits in mrem/year per pcf./m3).

CATHERY I INDIA ATOM

CKITICAL.	W. Milby	Little .	F. Scott	PORR.	I I'VEN	Lunis	Luna	61-11.1	t their	1 1016	Linns.	i tillità	Limit	Linn	111 19	61-111	1 tires	1 settle	W. Dilly	B. bilbr	W. billing	LIVIE	LIVER	LIVER	L tittii.	Balling.	11119	111-17	61 11.1	t sunt	i tibiti	11119	111111	t thii.	111-19
SE IN C	1.3245103	3. 100E 103	0.000E-01	0.000E-01	10		10	X	10		T.	0.000E-01	T	0.000E-01	0.000E-01	0.000E-01	-	0.0008-01	0.00CE 01	0.300C.0	0.6001-01	0.600E 51	£	0.000E-01	0. 300t 01	0.000E-01	6.0008-61	0.0001 61	I	0.000E-01	0.000E-01	0.0000.01	T	0.000E-01	0.000E-01
111-10	1.3548 104	3, 40 103	1.024£101	. 4 40£ 104		3.300E103		2.021E104	\$.033E103	1.000 165	1.0441.105	2.840E 105	4.Buft 103	1.33af 101	1.2323.101	4.0931 104	5.3141.101	1,412.161	2, 320f 162	1.4401 63	0.000E-C1	1.2541.101	3.3411 .09	9.20of 12	3. 1928 165	-	1.9131 165	1.394.161	-	1.324 160	-	7. 35.34 164	-	1.30 H 103. I	5.333 105
1.1869	1,2648103	3.40UE :03	1.0246 104	1	0.0306 01	1.440E104	-	9.440E103	7.200E104	1.014E 104	-	2.948E 104	4.54HE 101	1.7011.103	5.400£103	4.7014103	198	9.20at 132	0.000E 01	0.000E-01	0. 000E-01	6.600E 01	T.	0.000E-01	1.4001.165	-	3.4401.164		1.0954 100	1.926t 103	-	1.55dE 101	-186	-108	7.8724 164
K I BHE Y	1.2541.103	1.40dE 163	1.024E104	0.000E-01	B.000E105	2.2BUE 101	9.010E103	1.304£190	0.0008-01	0.000E-01	I	0.000E-01	0.000E-01	0.000E-01	0.0000.01	4.1241100	4.6736 104	1.214£ 02	0.000E-01	0.0001 01	0.300E 01	0.000£ 01	T.	6.930E 01	6.000E 01	0.000E 01	0.0001 01	0.0036 01	0.000£ 01	0.COUE 01	I	0.3004 01	J.	5. 4121 104	2. 75BE 101
LIVER	1.3446103	3. 40dE 103	1.024E104	-	-	0.00CE-01		1.240E 100	1.4926104	2.774E104	-	1.1520104	1.1401 104	3.1446104	2.094E-01	1.45 1 100	1.0331105	4.5136 03	10	0.300E-01	0.035E-01	1 . 45 3E 105	-	2.540E 102	6.0001 61	0.000E 01	0.000E 01	T		0.30cf - 01	T.	0.0001 01	7	3.4 NE 101	1.950E 161
FORE	0.000E-01	-	1.024E104	1.320E104	4. 400E 105	0.000E-01	0.0006-01	0.000E-01	2.452E104	1.1745104	7	0.000E-01	3.2486104	4.330£ 105	1.535E 100	0.0001-01	3.240E104	3.304£ 02	0.000E-01	3.630E 01	6.000E 01	0.0001 01	T	0.000€ 01	3.040£103	-	4.1921.01	5.744E100	3.000E 163	3.40dk 01	4.4.14.100	1.0321.101	-	1.0724 105	9. cant 101
PINKOID	1,2445103	3.4001:103	1.0216164	T	4	5.9535101	0.300E-01	0.000E-01	10 3000.0	0.000E-01	0.000t 01	0.603E-01	0.0006 01	0.000E-01	0.600E-01	0. Got 01	0.030E 01	10 3000.0	0.000t 01	0.0006 01	0.00cm 01	0.000E 01	0.000E-01	0.000t 01	6.60at 01	0.000.0	0.0001 01	0.000E 01	9.000t 01	6.000f 01		3.0004 01	0.035£ 01	0.000E 61	0.0000 01
u. pant	1.3548 103	3. 40HE 103	1.0211.104	DOUE !	=	1.6366103	335E	1.03.% 01	18	1.0526.101	1 75	13	5.11.2.103	1.4441.164	9.120E 02	-	1.45.46.101	46	11	7	1 3	5.01.12.11.04	7	1.5924 143	-	5.0". £ 105	=	-	=	+	-	17	111	111	9.0 to 13c
NO ISOLORE	11.3	E 11	Ho 24	F 32	LC: 45	CK St	Rul 54	hut 5.5	14 SS		ED 5:0	65 83	1H -59	111 2.3							14. 45.	1.1: 13.5	kb a3	Lu 10.7	1.4s H2	2.55 7/4	24K 97E	14K 9.3	1 70	* 718	1 71	276 *	1 73	24 Vill	78 M7
2	***	61	7	-	1/3	1	*	3	5-	10	=	17	=	-	2	-1	-	111	1	N.	#;	100	* **	77	1117	*	1	25.00	P.	でい	2.0	**	41	47	3.5

	FAE	BUBE	VIE TEK	1000	INTLEMENTING	1000	PART 50		
		(For Section	lon 2.2.2.b.		units in area/year	car per pci/m")	1/11).		
ACE I ABUR I	Inna at ton								
no tentort	u. buby	HITKOIL	Bring	t.IVEK	N. I BOREY	Line	111-19	10 k I to	CKIIII
35 mp 73	4.20m to1	0.0000	1.40UE 104	7.8148103	7.7356103	3.04UE 105	1.0106 105	4.2006 103	1.11445
37 10 97	2.0481 02	0.0006 01	2.3348-01	5.424E-02	4.5446 -02	. *	2.412£ 103	0.300E-61	i tuni
-	2.2944 101	0.000E 01	0.000E-01	1.300E 102	3.913E102		2.400£ 105	0.0006-61	17-19
	3.764 03	0.000E 01	1.0326-03	2.913 03	4.4151 02	7.440E103	4.150£ 103	6.00CE-01	11 19
	5. yout 04	0.000E-01	4.174E-05	4.014E-05	1.0000 03	3.992E103	1.0806-11	0.0001-01	i until
	5.501E103	0.000E-01	1.52HE 103	0.000E-01	5.613.103	5.010E105	1.1011 105	0.000E-01	Links
12 kill 105	3,11.% 01	10.00ce 01	7.904E-01	0.000E-01	1.0141103	1.093E 164	4.815£ jest	0.000E-01	11 19
	8.2354 163	0.000E 01	***	0.0000.01	1.334E105	-	9,1201.100	0.000E-01	LIMBS
	5,944,103	0.000E-01	1.086£ 104	1.00CE 104	1 . 94ftt 104	4.432E105	3.024 1:45	0.000E-01	LIMIG
	3.3cot 103	0.000E 01	0.000E-01	1 . Potts 105	1.584£ 105	1.400E 104	3.8101.103	0.000 01	1.11116
	1.2 108 104	7.353,101	3.120E104	5. unit 102	0.0000.01		4.0542 103	0.0004-01	LIBRO
	4.473.103	1.040f 103	3.41.E 10.3	1.50 16 103	1.240£404	3.134£105	7.0246 104	0.000 -08	8. 8 to 263
10, 11, 12,711	1.5400.103	-	\$. 22.4£ 10.6	5.750£10.1	4.5/24 101	9.400E105	1.49.18 105	0.00Ct 31	.: : H 813
=	3.0.2E 01	1.0524 100	1.4006100	4.4248-01	5.092E 100	4.513E 103	5.74:4101	0.000E 01	61 11
-	1.5uff 103	3.410E 103	9.7406 103	1.47.4 163	3.555E 103	1.15GE 103	3.03.5 105	0.000E-01	1 THERE
=	1,2401.02	3.0-1E 03	4.972E 03	3.393E -03	1.117.34 .01	1.9351103	1 . U.S. 10.2	6. doof as	1 11216
10	2,7311.101	5.50 W 101	101 35 66.7	4.3204.101	3. other 102	8 . 45 3E 40E	S. 53.50 103	0.0001-01	61 12
=	3.59.2 03	9.35.0E .03	1.1138-62	5.95.1£ 03	4. 3:ta - 0.3	1.35 E 103	-	0.300E 01	1 181933
21 11 112	1.4124 103	1.075E103	2,4006103	2.1526103	1.1552 104	2.880£ 102	5.69.4 165	0.0304 01	61 13
-	5. 20at 104	1.1328102	4.574£ 103	1.3142.164	2. vidur 104	0.0006-01	-	0.030£ 01	fitter.
_	2.0 mf. 193	1.17.E10/	3.5366104	3.5746 104	4.138E 104	0.000E-01	4.200f 163	0.000E-01	BHILLIA
_	-	1.1446 105	-	-	5. 1846 103	0.000E-01	4.0248.102	0.0001 01	Berkel
_	\$ 30E B	2, 15,4 103	-	1. HRE 104	-	0.000E-01	**	\$6. 30000 a	HILLS
-	5,153,102	2. VB 1 10 1	4. 110E 102	1.720 103	2,7526101	0.000E 01	1.00HE 100	6.0301 61	SHIPE
-	2.55se 103	4. 4shit 105	2.440£ 103	4.984£163	1.113 104	0.000E-01	5.244E 103	0.00ct 01	THINKE
17.7	7.384 105	0.000E 01	3.7.3K 105	B. 10-36 10%	3.8 73 105	9.7.0E104	1.0401104	0.0008 -01	4 152.5
=	1.101.105	0.000€ 01	3.704£ 104	1.45 16 805	B.520E 104	1.200£ 104	1.1464 104	0.0001 01	LIVER
	4. 2llot 145	0.0000.01	4.784£165	4.2548.105	2,224 105	7.53ut.101	B. 400t 14.5	0.000E 01	1 Ives
-	3.2436.103	0.000 01	3, 31.26 10.3	4.3001.103	4.BOOK 103	4.835E 161	1.16541. 0.1	0.000,0	LIVER
-	1,112,102	0.0000	3.04HE 102	2.90 M 103	2.440£ 102	2.272£101	0.0001 61	0.0001 61	1 106 1
21 64 139	2,71.4 42	0.00.00	9.326t 01	4.41.4 01	4.234£ 04	3.7201.103	0.9566 103	0.0001 61	I IMM's
	2,3248 103	0.330£ 01	1.9046 104	4.90 IE 101	1.17.11.101	1.373 105	2.1844.145	0.0000.01	1 titles
-	3, 1:01 03	0.030E 01	1,000E 01	7.5.5H 05	7.000k 05	1.91-E103	1.150 07	0.0000	2 silles
	1.45.48 0.1	0.0004 01	3.61 E 03	2.76 tk 05	2.3unk - 05	1.17.36.103	1.55tH 14	0.0000.01	4 138H3
-	4.5846.101	0.000t 01	3.4406.102	1.7346 162	0.v00t-01	1.350£ 165	4.5848.162s	6.000 01	61 1.1

TABLE 6 (CONT) Fage 15 of 39

			(For Sect	(For Section 2.2.2.b, unite in mrem/wear nor acts/")	FACTORS FO.	fo mrem/v	I IMB 10 CF	FAKT 56		
3 2	F. P. ASSERT	Mini AT TON								
=	3,801051	u. basy	TH-COLD	BONE	LIVER	KIMEY	1.1940	171-10	SAIM	CRITICAL
17	1.4-142	7.730E-03	0.000E-01	4.835-01	T. SAME.O.		The state of the last			
K	Ct. 141	1.5346 103	0 000E 0	13HE 181 0 0006 At 1 0000 At 1 0000 At 1 0000 By 6. \$248 103 2. 1126 183 7,7206 -02	4.101E-01	0.0000.01	4 . 338E 103	2.1136103	7,7206-02	
2	CE 143	1.5286131	22HE 131 0.060F 01	OI 1 0/45103	1013:E104	1.30.E.104 6.254E.103 3.414E.103 1.300E.103 0.000E-01	3.414E105	1.300E 105	0.000E-01	
14	CE-144	8 - B + 36 + 655	0.0006	3 42 16 10 1		4.0801101	7.975E104	3.24E105	0.000E-01	177-19
2	fr. 143	4.540£103	D 0006 0	A1 0 1405 42 2 2625 42	1.43.E 103	B. 4806 105	7.774E106 B.150E105	8.140£ 105	0.000E-01	
27	FK-144	1.5386-03	0.000F-01	3 0.30E 0.3	1.727103	2. 140E 103	2.800E 105	2.000E 105 0	0.000E-01	
22	Mb-147	3.540E102	0.000E DI	101 102 0.0000 01	1 4 40 F 10 Z	7.040E-03	1.015E103	2.152£ 04	0.000E-01	t thite
#17	182	5.4406.101	0.000F-01	1.5.06.103	8.470E103	3.550t 103	2. 2048 105	1.72b£ 105	0.000E-01	
7,	W 187	2. 4dot 100	0.030E 01	B. 480F 100	7. Aune 100	0.000t 01	4. 454£ 165	B. 550t 104	0.000E-01	
Ho	11 235	4.052E 105	0.000F at	B 000E 103	A ACOF A.	10 3000 o	7. YOUE 104	1.22.4 103	0.000E-01	
112	0 230	4.53.4 105	0.000F-01	7.4446103	4 400E 01	1.47.4107	3. V.20t. 10B	3.07-1105	0.000E 01	
578	18-239	1.240£101	0.00M A	2 3045103	0. W. W. W.	1.711107	3.544.108	6.2 10F 105	0.000E 01	
				THE SERVICE	日本 日本の日本日本日	7.000E 101	3.740E 104	1 . 19 N. 1 del.	A GAME As	

TABLE 6 (CONT Page 16 of 39

FARMANY LOSE FARAMETER EACTORS FOR INTERENTING 10 CFR FART 50 (For Section 2.2.2.b, units in mrcm/year per µCI/m³).

PARMAY I INDIGATION

E .	The Hamiliers.		Milit	HITKOID	bine d		LIVER	KIDDEY	L UNUS	01-111	UNIN	CRITICAL
*	11-11			a Section .			- 0					
			1	W-7-1-	3000 o Fr	F-	-	-	1.2724103	1.272 161	1.27 E 103	W. boley
7.7		1.0	4	4.0/22.0	33 2.400E	-	4.073E103	4.87% 103	4.873E103	4.8735103	- 100	- 2
7	NA 28	1.1	SE 104	1.37.55 10	14 1.374E	E104	1.374E104	-	-	1 1745 104		The second
+	1 32	2.15	101 10	0.000E	3000 I 10	-	13750			0 3000 100		W. Billi
V3	EE 45	2.48	HE 105	0.000E	01 4.400	- 10		N 000F 108	20000	A	F.	Milit
4	(k 51	1.35	11.103	7.49.1E 11	000.000		0.0000.01	2 A 2 '15 1 A 2	0.0000	COL # 102	Τ.	LIME
N	BH 54	8.40	04 103	0.030E	000 000	16-01	4013619	2.07.4.101	2.073E104	1.0000.101	£ .	£ 410363
-	108 55	3.53	04 - 41	0.003E	0000 0 10	10 3	1015151	-	1.704.103	5.4854 104	Ð.	1.111165
2,4	22	A3.	16163	0.000E	3.344		3 364E 404	0 0000	1.0.00	5.74 14 101	6.000E 01	111 19
3.0	64. 14	1.43	36 104	0.000E	1 2 20		1 10.4	0.000E 01	1.2404.103	4.37.1.161	L	1 tiptics
2.3	En 58	3.23		O DOOF	0000		2 A 2 TO 1 TO 1	0.0000	1.0.38.103	1.78 11 145	Ŧ.	1.48943
-	CB 25	1.92	4E 104	0.000E	000 9 10	10.4	20175101	U.0000E-01	1.344.105	V.D.S.CE 101	.75	1 (14/2)
8.8	111 .29	5.41	1011	0.0005	2 2 240			20000	10. 7.50E 105	7.57 1 103		4 444740
	411 . 63		40.44	30.00			1.12th 101	0.0000	4 . Dalut 10 1	4.6am 103	ш	I tivit.
-	111			200000	10 OF 1	200	4.394E 104	0.0001-01	3.0731 103	1.4124 104	0.000.0	Betrief.
		D AUT		D.000E	7.10	200	2.7.10 - 01	0.0000	9.350t 103	3.47 1164		111 10
	724 477	10. 40		D. OLVOR	10000 T	T.	3.037£100	4. 100E 100	1.113.104	4.1116101	0.000E 01	111119
	200	-	1011	G.vool 6	37 83 7F 10	E 101	1.115E 100	6.44ct 101	1.2401 104	4.44 11.104		- 6
250	. H 27	4.45	11 03	0.0008	11 4.833E	£ 03	9.200E 02	4.624E 02	1.584£103	2.61.4.102		1 419403
10.00	11. 111	7.7	Of 102	B.COUL B	3000 P	E 01	0.00ce -01	0.000E-01	0.000£ 01	0.00ut 61		the feedback
7	lik ar	4.43	HE 102	ī	01 0.000E	10 3	0.000E-01	0.630E 01	0.600E GE	6.65of 61		
	64. 83	1.83	I lol	D. Doct 0	11 0.300E	10 3	0.000E-01	0.000E OF	0.063E 01	0.00.0		
1	ha ile	B. 16c	101 10	6. Dings -0	11 0.0006	E-01	1.904E 103	ı	0.0036.61	7:116		M. Colles
1	TP: 42	27.72	-	0. JOSE 0	11 0.0306	10 3	5. Cast 16.2	7	0.0006-01	43.40	1000	11111
	kile fry	2.53	M 193	D. Duvie D	10.0000	€ 01	3.530£ 102		0.000F 01	1 10 th A2	2000.0	41014
ď.	14 187	1.240	-	0.000£ 0	11 4.3446	£103	0.00vt 01	0.0006 01	3.4145.104			41011
4	2: 4:	4.013	14 102	0.3000.0	1 1. June	8013	U	0.6006.01	1 41/16 1.0.7			1 111111
1	12. 31	1.51	7	0.000.0	1 8.803£	E101		0.6464 01	5.074104		0 0000 01	DINIE.
375	打井 神江	4.05	11 01	0.500	1 9.5.30k	£ 100		0 0000 00				1111
ħ	1 24	4.600	-	3.05GE 0	3.9846			0 0000 01	2 6 145 101		1	1111
30	N SIM	1.41:	-	0.0000	1 3.7016	6.7	ш	A 305. At			E.	111 19
318	12. 1	B. 7.34	16 104	0.0004	4 5, 1008		IJ	4 0000			I.	1 1111.
17.8	* 75 *	4. 383		0.0000	27.4			מימחת מו	•	-	T	4 138363
107	2.5	3.7.5	-	3.003F G	1 100		4 0000 B	0.000E 01	-	-	0.000E 01	61 111
1 1	28 AZ	3.15	-	9.0536 0	1 1 45.15		4.000	0.000.01	H. 1:00 104	*	I	11119
No.	d						1.00 16 104	5.7358 101	4 dille 103	1 . 4talk 105	0.000E G1	I thus.
		Section 2	4 101	O. GOOD. C	1 1.3761	107	2.720t 101	4.130£101	1.396£105	4. 304E 105	Ā	11119

TABLE 6 (CONT) Page 17 of 39

FAHMANY PODE FARAMETER FACIUNE FOR INSTERNITING TO CER FARI CO (For Section 2.2.2.5, units in mem/year per pc1/m3).

AND I SEED FAILURE ATTOM

IN ISOHOFE IN MINY I	- Inthon	*	fuvkorts	A.Chart						
	tone.	THE PARKET	DATES		LIVER	V House Y	1.1980)	111119	14.14	CKITICAL
244E103 0.	25 1E 103 0.000E -01 1.	01 1.	1.854	0	1.0328 104	1.000E 104	7.5136105	9.4006.104	S ALAELAN	*******
3.04HE 02 0.000E 01 2.	3 40K 02 0.000E 01 2.	01 2.	2,234€-	3	00	K.E	- 100		- 000E	1 1040
3.114E101 0.000E 01 0.	114E 101 0.000E 01 0.	010	0.000E	7	1.490E 102	4.1136102	-	-	0.000F-01	
4. V. T. 0.3 0.000E 01 1.3	E 02 0.000E 01 1.3	01 1.3	1.3046-1	7	3.84E-03	5.7501 02	1.152£163	-		6.8
B 0. 10t 04 0.000t 01 5.9	01 0.0000 01 2.9	200	26 1	0	T.	3	4.4725 102	8.73UE 07	J	Linds
8.7.7.4 10.2 0.000E 01 2.1	102 0.0000 01 2.1			103	0.0004-01	-	7.832£105	1.00rlt 105	0.000E-01	1.1816
Transfer of Ground of I.	1 0 0.000 D		1.1.500	200	0.0001-01	-	1.815E104	9.41×164	0.000E-01	61 11.1
1	101 0.000E 01 4.	0 4	7.8408	-	30	1.904E105	1.4001107	9.400E 105	0.000E-01	
1 10 1000 0 000 01 I	E 103 0.000E 01 1.	. 10	1.3846	101	1.31.35 104	2.504£104	5.75% 104	2,7211 165	0.000E-01	Ltmiti
	101 0.000E 01 0.0	0.0	0.000		-	1.5846 105	-	3.40 Sel 3.	0.000E-01	I siellis
TO THE PARTY OF TH	101 101 101 101 101	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	3.1.50	-	-	0.0000 01	-	1.0:16 10:	0.000E-01	1.14113
3.1016101.1			1.000		-	0.000 01	-	7.50 H 104	T.	1.112.114
4. 11:15 - G1 1. 11:16 15:00 3	- 01 1 11 12 15 15 15 15 15 15 15 15 15 15 15 15 15	150 3	3 0000	-	0.14.26.10.3	3.2324101	-	1.27 1 103	I	1 1000
2. 246k 10 t 9. 5245 16 t 1	101 1 2245101 1	101	1 10.00		1. 3	7. Shot 160	1,120£ 101	B. C 101	I	111 17
1.725£ 02 5.181 03 7.00	- 02 S. 1814 - 02 7.00	00 7 00	7.001		1 17.5	3.174.101	-	1,0 ;: 2 165	I.	4 taries
4.00:4E101 7.240E101 9.	E101 7.240E101 9.	101	9.8406	101	A. 0636 +01	4 10 10 10 10 10 10 10 10 10 10 10 10 10	4.2721.103		L	1 41111
5.04uk 03 1.240k 62 1.	E 01 1.210E 62 1.	62 1.	1.574	6.50	6 T	4.17:E 02	***	1.01.11.10.1	0 6001 01	11111
2.17.2 10.2 2. 15.5£102 3.4	102 2.15% 102 3.4	102 3.4	3.500E	102	2.904£ 103	-	4. 48ak 105		I	111-19
	104 1 44 1 103 6 2	102 4 5.2		500	4	2.7526 164	0.600F 01	V.120£101	0.0004 01	fintento
1.5/401901.51905.1.50	101 1.51 4.65 1.5	105 1.5	1.5036	204	4 1745 141	B. 1004 104	0.000t	4. 4lint 0.5	I	HIGHID
A. 124E 103 2.920E 104 1.2	103 2.9306104 1.2	105 1.3	1.75.6	101	2.0406104	2 . 2 . 4 . 6 . 6 . 6 . 6	0.000	1.27 3 103	0.000 01	Inchie
3.463E132 3.953E104 8.8	143 1.95% 104 8.1	101 8.1	B. Huof	10.3	-	1.446131	0.003F 01	0.000	0.0000.01	- The same
	103 6.20HE105 3.6	105 3.4	3.4948	101	9.410E103	1. tillin 104	3.0006.01	A. 97. # 16.1	OCH OF	HILLER
5, true 105 0.000£ 51 5.03	100 0.000E OF 2.03	01 5.03	2.034	103	1.1206 105	3.7531.105	1.4:46:105		C COME OF	
1 . 52.18 10C 0.	100 0.000E 01 5.10	21 2.12	2. 875.3	101	1.933£ 165	1.104 1.05	1.7756104	1.041111111111	0.0006-01	1 100 5
	100 9.000 0 CO1	.2 10	4.70#	102	B. 480£ 103	3.0401 105	1.2648.105.1	B. 4000 104		
	10. 0.000 01 4.4	01 4.4	4.45.4	102	8.5506 103					* 1 A 1 K
1.11.1 102 0.6064 01 2.0	103 0.6064 01 2.0	01 2.0	2.0 4HE	0.2	4		* 4		Π.	1 1/1 1/1
3.6921 62 6.6551 61 1.3	0.2 0.6551 01 1.3	01 1.3	1.3358	001	ŧ.				Ε.	45
3.5.56 103 0.003t 01 5.4	101 0.0006 01 5.4	01 5.4	3.4/36	101	A. 704E 101	. 3			0.0000.0	1 1500
01 0.003E 01 1.43	01 0.003E 01 1.43	01 1.43	1.4346	0.1	37			2 44 11 04	E.	1 111112
	01 0.0000 01 1.2	01 3.4	3.492E	6.2	4.70 H 05	3. 1356 05	1.013610.1		1000000	Links
40 4.77.1 101 0.000F 01 4.79.3E	101 0.0000 01 4.7	01 4.7	4.793	102	2.3506102	10 3000.0	3.1446105	4.8728 165	0.0001-01	61

13

(CONT) TABLE 6 (1

(For Section 2.2.2.b, units in mrem/year per pol/m3).

	3	=		=						=			-
	CRITICAL	7-10	Lunio	7 19	LIMIL	1.11016	Lum	1.1816	LIBBS	7	Limit	I tatiff	61-13
		-	0	70	ā	10	0		10	0	7	7	10
	SFIR	1.054E	9.000E-	3000.0	9000 . O	3000 . O	9000.0	0.000E	0.000E	9000°0	0.000E	0.000E	0.000E
	111-10	1.2000104	1.24 NE 105	2.55.1 103	B.440f 10th	2.134 105 0.00CF	2,353, 04	1.02 M 105	8.540t 104	1.746£ 100	3.67.4 165	8.240L105	1.330t total
	11860	05.4 01 0.000E 01 9.400E-01 4.240E-01 0.000E-01 1.014E104 1.200E104 1.054E-01	4.1341.105	1.304E 103	1.332E107	4.833£105	1.753£ 103 2.353 04 0.000£-	3.720£ 165	4.455£ 105	4.735£104	3.9.30E 10th	4.5121104 0.000E-01 7.444107 0.000E-01 1.744E107 3.654E108 8.2401103 0.000E-01	2 24 10 100 1 3 0 0 0 0 1 1 18 4 5 10 3 1 19 3 5 10 1 1 6 0 0 5 1 3 2 4 4 8 10 5 16 4 1 1 3 0 1 10 3 0 0 0 0 0 5 10 10 10 10 10 10 10 10 10 10 10 10 10
	KIDHEY	0.0006-01	8.000E103	8.4 10E 101	1.3386104	3.060E 103	1,00BE-02	5.0246103	0.000E-01	0.000E-01	1.073E107	1.7446107	1.660E133
	LIVER	4.2406-01	1.89 SE 104	2.454E 103 1.934E 103 8.410E 101	4. BULE 104 2.024E 105 1.250E 104	1.335E104 5.31 E103 3.06HE103	4.294E-02 1.740E-03 1.00HE-02	B.550£103	5.175E103	4.740E 100	0.000E-01	0.000E-01	3.1934 101
	FONE	9.4006-01	3.640£104	2.454E 103	4. BURE 104	1.3356104	4.294E-02	7.864E103	1.540E 103	1.300E 101	8.000E107	7.644 107	1. 184F 103
	-	-	0.0	0.5	10	70	10	10	10	10	10	10	10
	HIVEOID	0.00CE	3000.0	3000.0	- 3000 · 0	0.000E	0.00JK	30.0.0	0.000E	0.000E	\$.000E	0.003E	D. GGOSE
11011	PERM	10 170	518 103	101 307	244 105	246193	75k 01 0.000K	5.120E 162 0	4th 101	13 100	101 375	Jit 104	A 550 W.D. B
ATE 1 IEEN ANDERS AND	3	1.0	2.1	13	2.5	-1-0	2.1	2.2	2.4	3.4	4.1	+	
DIE 4 HERN	Spint	7	-	17	**	17	**	43	2	11	2	=	200
- 1	150	4	-	-	-	-	4	100	2 82	11 1	4 3	77 9	
PARK FARE	-	711	# 17%	1.3 4	74 4	元	75. 2	111	718 1	127	11.5	BL B 23B	4 47.00
PIT													

Page 19 of 19

FATHBAY MISE PANAMETER PACHIKS FIRE INFLEMENTING TO CITE PAKE SO

		(For Section	on 2.2.2	b. unitta	in area/vear	100	100 1/4 31		
CAE I CHIEB	***************************************					į			
I viliality !	SHIPS OF LINE								
OF USBIGGE	H. billy	dirikini b	Dink	LIVER	L.HME Y	1.1800	111-18	EKIN	CKITICAL
1 11 3	1.124.103	1.1254.103	0.000E-01	1.1256103	1.1256103	1.1256103	1.1334 103	1.135£103	W. 1:011
11 3 2	4.73H 10.1	4.7345103	3.58%E 104	4.731E103	4.734E103	-	1 46 1	190	DOM
3 465 24	1.20% 101	1.407E104	1.50% 104	1.409E101	1.569E104	1.409E 131	11.0		W. Bunt
4 4 32	9.0791.194	0.000E-01	2.405£165	1.143£105	0.000E 01	0.0006 01	4.21th 164	1	
5 15E 45	1.1516.105	0.000E 01	2.0198.105	3.9591 105	3.700E 165	0.000E-01	1.15:4100	T	LIVIA
2 12 24	1.543.102	B.547E161	0.030E 01	0.000E 01	2.431E101	1.49tit 104	1.01.11.10.1	0.030E-01	Linic
7 100 54	9.50%E163	0.000£ 01	10	4.2926161	-	1.5736 103	2.1504 131	0.000E-01	i initi
5, 100 55	75	0.300E-01	T	1.6501.100	***	1.3131.101	1.21.1103	6.000k 01	01.11.1
5: 17 %	7.7764 103	0.000E 01	4.7355101	2.512E104		1.110£ 105	3.64.71103	0.030E-01	Linni
	1.5558.101	0. track 01	3.040£ 104	3.3154.101	6.000E 01	1.2491.105	7.01/1/104	6.000E 01	1 111115
11 431 54	3.14.14.133	0.6001-01	0.00ct -01	1.77% 103	30	1.134E 105	3.43.4401	0.000E 01	1.1043
E 68 29	2.2546 104	0.000E 01	0.000E 01	1.1138 04	T	7.057E105	9.4. c. 101	10 3000.0	\$ 137 NO
11 111 2.9	-	0.0001 01	*	3. 103E 103	0.000 . 01	3.0308 104	2.2411.101	-	LIBIE.
£ 111 : 2	-	C.30CE 01	0.214E10S	4.4.355 104	0.000E 01	2.7491.165	6.327F163	-	Tinn.
12 dl 23	1.1.1.1.01	0.5504 41	2.990E 100	3	0.000E 01	0.1775103	0.3" Tio1		11111
17 111 71		0.0001 01	0.0001 01	-	4.431E 100	-	-	T.	61 11.1
27 117 .1	-	T)	*	1.1111105	7.1111134	-	1.4.13 104	1	4 tunts
46 . II . 29	-	0.0000 01	4.497E 02		5.844£ 02	1315	1,017,101	-	1111
	-	3.0000.01	F	Ŧ.	Π.	AL.	I		*
	2.1.28102	0.0000.01	0.0000.01	0.0000.01		E.	T.	6.0000 01	W. Filler
		0 0000	2000.0		B. DOOR DE	3000			W. Dillin
		0.6066 01			0.0306 01	0.0004-01	1.7.11.101	0.000	1 114 1
	2.09-71.102	0.000E 01	0.0306.01		0.0000.01			J	1100
	1.7.2% 104	0.300E 61	5.9946105	0.0001 01	0.0006-01	1571	-	1	Links
	-	0.0001 01	-	Ŧ.	0.0001 01	1.4754 107	-	0.0000 01	1-1111
	-	0.000E 01	1.21 HE 162	Œ.	0.0001 31	5.330E 104	1.7394 105	I	61 11.1
	5, 35.48 91	6. wood 01	1.310£ 101	Æ	0.0001.01	2. 401E 104	2.421 165	0.00CE-01	111 19
	-	0.000 01	-	£	0.000t 01	2.2134 105	2.4.7E 165	0.000E-01	61-111
		0.000E 01	5.05% 01	70	0.0000. 01	2.8128.103	1.7171103	0.000E 01	LIBRE
	and the	0.0000 01	*	0.0001 01	0.000.01	-	1.4391.163	0.000E-01	1111111
A. S. W. S.	2.30% 91	0.0001 01	-	1	0.6mar 01	2.370£ 104	-		111
		0.00tt 01		0.0000.01	0.0000	7.4376104	3.Buth 105	0.030E 01	111 19
24 ch 70	3. Cold 10 1	0.000E GE		4.1016.104	10.707L104		A. 100 109		Limits
	111111111111111111111111111111111111111	0.0001 01	1.0/st 102	7.7128.101	S. Heart les	1.13.1105	3.511E 105	0.0000	111119

TABLE 6 Page 20 of 39

(For Section 2.2.2.b. units in mrem/year are uci/m3).

Statister t.	u. suby	HITEGIE	BUME	LIVER	KIMEY	1. tittle	111 10	DA IN	CKITICAL
	£613/45.7	0.0606-01	2.349E104	9.175E103	B. 421E 103	6.1426105	3.700€ 101	5.549E103	Linus
	1		.029E		3/5	100		- 3000°	Limited
	4. 355£ 101	0.000E 01		1.724E102	1994	1.3541.105	1.25:4 105	0.000E 01	Lund
	5.77.3 03	0.000E-01		3.483E-03	5.029E 02	9.50%E162	4.610t 103	\mathcal{K}	01 111
	1.6776 03	0.000E 01	0.103E 05	8.510E-05		-	- 5		Links
	1.0731 103	E	-	0.000E 01	-	4.423E 105	4.17/1.104		LIMIT
	5.550E 01	30	-	T	-	***	34.1	1	01 11.1
	1.4711101	0.000£ 01	-	0.660E 61	-	-	-	L	Limit.
	9.1371.101	0.000E 01	-	-	3.1346104	2.4751163	-	T.	1. 137.11
T Complete	2,9481 104	0.0001-01	0.000E 01	9.10 E 104	7. 134E 104	4.51 × 105	1.7.21.10t.	Ħ	4.16.04
	5.754 163	1.47.1.101	1.443£104	2. 234E 103	0.000E 01	1.1471.164	1.00 total	X	L tarns
- mail	9.13/1/102	1.9211.103	4.714 103	2.327E103	3000.0	4.7738.105	3. 3 'dt 104	0.0001.01	Links
	3.0271.103	£013070.7	2.465£104	B.517E133	5.34.46.104	1. 411Gt 105	7.1111101	0.0000.01	1 thins
	5.10:4 01	1.9411100	2.771E100	9.509E-01	7.047.100	-	5.4.11 tol	0.000.0	111119
12911	3.641E103	4.3276133	1.930£104	4.045£163	5.63:E104	-	1.017(105)	Ŧ.	Linns
55	2, 39 31 52	7.141E 03	9.750E 62	3.474k -03	2.54HE 01	2.9341.104	2.2198 101	0.000E-01	01 11.1
SIM	5.0296101	9.7261.101	***	5.920€101	3.295E102	3.057E165	3.0 CE 103	6.000E 01	61 11 1
11		1.47BL 02		7	8	-	1.323.103	T,	Linis
27	1000	1.175£103	4.010£103	2.733E103	1.77:E:03	3.77 1E 165	1.3/21 105	J	Links
*	-	177	-	1.5398164	-	0.0001 01	5.1651.103		HINKINI
	-	1.4.316107	4.810E104	4.810E104	7.BillE 104	0.000E 01	2,013,103	E	III IIII
*1	1.01.1:101	1.9304100	2.112£103	1.070E103	-	L	3.200t 103	70	unicoto
	-	3.11 HIE 105	1.454E 104	2.041E101	3.3/ut 101	I	5.4726 103	0.0001-01	HINKOIL
	9.9a H 162	2.02% 101	1.1731.103	2.121E103	-	0.0001 01	9.514E 103	0. COOF 01	Invent
.7	4.1111.103	7.91ut 165	4.921E103	H.732E103	1.11% 104	0.000t 01	1.4401.103	Æ.	HIGHDII
1.5	3.21.51165	0.0001 01	4.512£105	1.011/1.104	3.104 105	1.2100105	3.84th 163	0.000E 01	1171.6
3.5	1.153.133	0.000E 01	4.5131104	1.70% 105	9.5156104	1.454[101	4.11111.103	C. 000t 01	I IVE
37	1.24 H 105	0.0000 01	9.035£ 105	0.251E105	2.41.3E 105	1.0404 105	1.4171.104	0.0001-01	Petrit.
311	1 10	0.000.01	-	PAE I	2013112.9	2.00il.101	2.497E103	Z	71.11
3.5	5.11.16.151	0.0301 01	9.42.E 101	1.3136103	1.12b£103	1.6511.101	9.000E 01	0.000t 01	1124 K
475	5.355k 03	6.000t 01	1.8436 160	9.01E 04	0.0211 04	5.77.E 103	5.77.28 104	0.0001 01	11111
10	4. 5274 103	0.000E 01	7.430£ 104	4.4754.101	2.1134.101	-	1.0171.105	1	1 10 41
111	4. 1546 65	0.0001 01		1.071E	9.47.E 05	-	1900	T	1.111163
77	2.770€ 03	0.000E-01	CO 3566 *	1 4006 DM	74 G 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	S A A RE A A B	۰		A habert
				41.00		1.0135103	2.74.1100	0.0000.01	4 130 24 3

TABLE 6 (CONT)

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FAIRMAY DIDE FARAMETER FACTURE FOR INTERESTING TO CFR FART 50 (For Section 2.2.2.b, units in mem/year par pCl/m3).

CALL I COULD TO THE A FLORE

100												
CRITICAL	111-19	1.1916	11119	1 mil	LIMIG	Lillini	1 11116	Linis	9 11 19	£ thinks	Links	61-111
UNIN	1.291E-01	0.000E-01	0.000E-01	0.000E-01	0.000E-61	0.060E-01	0.000E 01	0.000E-01	J.000E-01	0.000E 01	0.600E 01	0.66CE-61
111-10	7. Suite 104	5.441E 104	1.3/3/165	3.0ur.4 105	9.7311104	1.94ta 162	0.21 :: 161	3.755E101	9.103 164	1.771E105	3.811E 135	4. 1011 10:
Trulo	11 1.295E100 4.107E-01 0.000E-01 8.695E103 7.585E104 1.291E-01	5.439E165	1.154E 105	1.1956107	4.329E105	1.545E163	3.2024 105	2.04116105	4.10/E161	1.01361001	1.4952168	5.80%E 104
KIGHE Y	0.000E-01	U.547E104	8.342E101	1.173£105	3.001F103	9.74BE -33	4.111GE 103	0.000E-01	0.000E-01	8.450£ 104	0.045E104	9.7316:01
LIVER	4.1076-01	1.954E104	1.987E102	2.114E105	5.550E103	1.8455-02	B.733E103	2.494£103	9.4576100	0.000E-01	0.000E-01	3.345£ 101
PUNE	1.295E100	3.923E104	3.459E103	4.773E106	1.844£104	5.95/E-02	1.000E104	7.315£ 103	1.432E101	3.760E107	3.545E107	4.452E103
THYKOIB	10-3000 0 10 31/	6.000E 01	0.000E-01	0.000E-01	0.000E 01	0.000E-01	C. 000E -01	0.0001-01	0.0006-01	0.000E-01	J. 0000E 01	0.0000
H. 5057	1.391E 01	3.097E163	2.075£101	3.615E105 0.000E-01 4.77E106 2.115E104 1.173E104 1.195E107 3.6151 105 0.000E-01	9.1154.462	3.997E 03	5.doin 132	3.5306191	4. 32%E100	2.344E 105	2. 07th 105	2.349£101
BOTORE				1111		i		183	147	2.455	2.50	2.19
=	1		\$7.	+.	**	7.5	**	7.11	1.0	217	191	11.1

TABLE 6 (CONT)
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	Hv.I	(Por Sec	(Por Section 2.2.2.b, units	ACTORS FOR		no Cr	TH POST 50		
ATHURY & CHIMA	HINA ALTON								
in isolore	u. Dilby	HIYKHIB	DONE	LIVER	KIDNEY	1. UNIO	111-10	ENIM	CRITICAL
	2. 4500 103	4. 440E 102	0.000E-01	4. 46HE 103	6.45BE 102	. 44111 1	4.45UE 103	5.46UE 102	W. FORM
	1	5. 304E 103	ri		5, 305E 103			1 300E	
1 NO 74	37	1.054E104	1.05561	13750	1.054F10-1	-	1.05.3E 104	P	W. 1:116
	36		-	1.1246165	0.000t-01	0.000E-01	1.4106101	*	binit
5 66 45	16.	. 1	-	1.49UE 10:5	1. 100E 105	- 1	-	0.000E 01	11016
5 CK-51	17	-	0.000E-01	0.00CE-01	-			7	
/ BH 54	4.9001:103	0.000E-01	1						1
6 Hill 54	2.2134-01	0.000E 01	0.000E 01	1.5 10E 100	-	_	-		
9 11 - 55	3.4324103	0.000E-01	1.574E104	1.175E104		-	-	T	1
10 11 59	9.47011.103	0.000	1.357E104	2,353£104	0.000E 01	-	-	6	-
82 111 11	-	0.0000	0.000E-01	1,219E103		776E 1		TO .	****
07 07 61	-	1000	0.000E-01	0.0325103	0.0001-01	-	3.17.3 104	1	111111
200	1 111/2	3000	-	2.01111.103	0.300E 01	1.11% 101	8.55 H 103	1	1 11111
17 111 11		000F	3. June 105	2.0141104	0.000E-01	-	-	0.0006-01	11111
57 111 51		J	2.374E100		0.000E-01	-	-	F	
15 (11 54	1.4	1	0.000E-01	1.8741.163	3.97:4 100	-	-		11-19
17 311 25	01:E 1	G. 9000. 0	1.9326104	-	-	-	-	F .	i tirili
92 HZ 81	11::E	0.000E-0	No.	1	T	1701	-		
12 10: 03	-	T	1	T.	7	1000	0.000	0.0000	
20 10: 164	0 11 1	T	1	F	0.0000	0.000	0.000 6		U. 1401
21 FR B5	-	1	0.0000.0	0.000E 01				3	-
22 KB 113	10.10.10.10	0.000				- 1	311:11	4000.0	
23 121 110		0.000		36.46	3000	3000.	-	0.000E	
	411	0.0004	-		0.000£ 01	2.030E105	-	0.000	
	406	0.000E		3000	0.000E-01	1.121E107		3000.0	
10 Min 11	11111	0.000€	-		0.0006 01	5,24E104		0.000E	
10 175 17	1.9	0.0001		0.003E-01	0.000t 01	2.300£ 104	-	9000.0	
00 X 60	1 107	0	1 3.2901101		J	-	1.010.1	0.000	
30 (910)	3711F	6.000E-0	1 4.074E-08	Ŧ	0.0001.01	-	2.35.4	0.000	
31 1 71	1.52111 104	0.600E G	3.000E 165	0.000k	I	-	-	0.000	
23 Y 42	1.4.40.11 01	0.000E 0	1.4301101			2.4500.104	177	0.000	
33 7 93		0	1 1.49UE 102	0	0.000.0		1.6224 103	0.000	1
81 . E. 95		0.3000.0	-	3.784	1. Total 104	1.7306.105			
JE 28 97	1.1700.101	0.000k-6	1 1.47UL 102	3.56.4.101	2.570t 101	1.1036 103		D.000	a.

TABLE 6 (COHT) Page 23 of 39 FAILURY GUSE FARAMETER FACTORY FUR INFLEMENTING 10 CFR FART SO (For Section 2.2.2.b, units in mrem/year per [101/m3],

DATE & INFANT

-3"									90			
CRITICAL	9991				9119					3 3 3		
	000	30	333	0000	000	30	000	000	33	555	333	0000
EN IN	3.780£ 0.000E	0.0000	0.000E	0.0000	0.000	0.000E	3.0000	0.0000	0.000	0.000	0.0000	6.000E 0.000E 0.000E
111-10	1.227E104 4.228E101	100			2. 730E 104 2. 435E 104 6. 902E 101			1.05.0E.10.1 1.90.0.10.1 2.15.0E.10.1	-	1.42am 163	0.724E102 0.040E 01 5.072E104	
1186	4.788E 105 4.200E 103	104E	260k		1.0156104			0.000E 01 0.000E 01	- 300	1.174E104	3.97.E100 5.950E103	
KIDHEY	4.718E103 1.145E-03	. 10HE 0	8.900E-01		1.752E 104 4.853E 104 3.178E 104		1	5.100E 104 3.940E 104 2.240E 104	-	5.2131104	4.3766101	** 1
LIVER	9.842E-03	.242E	0.000E-01		9.53 H-01		2.322E102 1.347E104	4.440E101 4.542E101	-		5.6013 162 5.603 161 9.813 01	5,400L 101 1,070E 04 3,30 H 05 2,603E 102
DUME	1.54BE 104 3.892E -02 0.000E -01	.397E-	1.224E100 B.480E104		2.324E 100	-		1.2946 104	9.21 3 102 3.85 1 103		5.054E 102 3.584E 101 1.48 H 100	
HIYKOTE	0.000E-01	0.000E 01	0.000E-01	0.000E 01	1.010E 100 5.471E 103	-	-	1.494E 105 1.494E 105 3.554E 104	4.452E104 6.95sE105	0.0000	0.000L 01 0.000L 01	0.000E 01 0.000E 01 0.000E 01 0.000E 01
H. 1001	3.780£103 3.504£-03 3.234£101				4.803E 01	1.072E-02 3,223E101	1.724 102 5.5/3E 103	1.2591.104	2,773 103	5.39.3E101	1.974 102 1.914 161	3.870E 03 1.970E 03 1.950E 03 5.153 161
a solosi on	12 HB 92 77 HB 97 10 HB 99	100	555		===	225	90 170 170 170 170		:			2222 2222 2332
	202			444	:				** ** *	9 79 17	-1 -1 -3	41.01.41.4

(CONT) TABLE

Page 24 of 39

FATHMAY THE FAKAHETER FACTORS FOR INTERESTING TO CFR PART 50 (For Section 2.2.2.b, units in mrem/year per pc1/m3).

2	FATHINY I THIN AL	1/11/101	1001								
2	NO ISOTOFE	3	Adod	THYROID	DONE	LIVER	KIMEY	1.11040	171-10	BKIN	CRITICAL
-	14-142	9.0	441-02	0.000E-01	1.030E100	3.764E-01	0.000E-01	14E-02 0.000E-01 1.030E100 3.764E-01 0.000E-01 8.218E103 5.950E104 9.044E-02	5. V50E 104	9.0441-0	111-10 5
CI	CE-141	-	DUE 10.3	0.000E-01	3.772E104	1.444E104	5.250£103	3.772E104 1.444E104 5.250E103 5.144E105 2.154E104 0.000E-01	2.1551104	0.000E-0	
	CE-143	CI	13E101	212E101 0.000E-01	2.926E103		5.42E101	1.932E102 5.442E101 1.152E103 4.970E101 0.000E-	4.970E101	0.000E-0	1 1111163
	CE -14¢	-	241.105	744E105 0.900E-01	3.192E104		1.211E104 5.375E105		9.042F164 1.404E105	0.000E-01	Lumi
2	FR-143		115E 102	0.000E-01	1 . 400E 104	5.236E103 1	1.974E103	4.326E105	3.724£104 0.000E-	0.000E-0	1 Lunis
5	11:-144		311E -03	2. 40HE -03 0.000E-01	4.700E-02	1.8 10E-02	4.730E 03	1.610E103	4.30 1E 10.1 0.000E-	0.000E-0	1 01-111
12	1111 147		90E 102	4.990E 102 0.000E-01	7.93uE103	7.93uE103 0.134E103 3.150E103	3.150£ 103	3.220E105	3.123£104 0.000E	0.000E-0	timin i
9,	U 1855	4.0	341.100	14E 100 0.00CE -01	2.730E102	2.730E102 9.05HE101 0.000E	0.000E-01	7.79uE104	7.79UE 104 1.49UE 104 0.000E-	0.000E-0	1 111116
1.1	187		235 100	3.123E 100 0.000E-01	1.294E101	1.294E101 9.014E100	0.000E 01	3.963E104	3.55.4 101 0.000E-	0.000E-0	1 111116
101	110 11 235		CO 1 111.	14.105 0.000E-01	1.400E107	1.400E107 0.000E 01	3.274E105		4.850E107 4.775E104 0.000E	0.000E-0	1 1.11165
==	01 230		311 105	7.93HE 105 0.000E-01	1.341E107	1.341E107 0.000E-01		1.052E106 5.412E107 1.412E105 0.000E-	1.4121.105	0.000E-0	1 1 111115
*	M. 239	Ī	75E101	0.000E-01	1.0/3E101 0.000E-01 3.710E102 3.310E101 4.523E101 5.950E104 2.493E101 0.600E-01	3.310E 101	4.523E101	5.950E 104	2.4936101	0.000E-0	

3

(CONT) TABLE 6 Fage 25 of 39

(For Section 2.2.2.b, units in mrem/year per pc1/m3).

	CKITICAL.	W. MODY		No. of the last	W. Bullet	200	22.00	20.74	u. hoby	BA IN	Sr. In	SKIN	W. BOBY	W. MILLY	EN IN	ENIN		H. Dillo?	EKIT	-	H. Ballet	121.111	El. 111	1141	=	n. min.	Dr. In	-	21.43	EN IS	ENER	1		20.00	LF. 111
	GR.IN L		0.0000.0	Tant.	. 4	-	2001			-	-	3.533F : 40	0. Su0E 01	-81			-	8	-	-		-	-	450E	:00/E		1700	43.77 ·	111	-	-	-	20111100	-	1. 4438 100
	01.11.1	.000		11/11/1	. 4		4.25th 195	7.7.	C. 0000 5	73.6	1111	15.36	1000	0.60ct -01	2.9701105	5.651t 105	7,4101 1011	6.0mt 31	-	-		-	-	150	-		1:1	-	-	1.0041.05	1.074	1.00.1	1.1117	# 10.7	2. YOU 102
	timit	-300C.	5 4	. I VIIE	1. 1	-	4. 5. UE 105	-	V. 030E 103	3.16.6	83.46	-	. OOOE	0.000E-01	2.9701105	5.051E 105	-	0.00CE -01	-	190	0.000E-01	8.923E105	-	-	-	,000t	-	-	-	-	1.0741	1.80 NE	1.04%	10.5	2. Yaut 105
	KIDNEY	-3000	0.000E-01	-	30.3	316	4. 15HE 105	-	-	2 22.6100	-		3000	1000	3.970E105	4.051E105	7. 110£ 100	0.000E 01	1,00 % 103	2,0231105	0.0004 01	-	-	-	-	.000r.	-	7.75.165	4. 197E 16.1	1.004	1.07 11.10.1	1 .Bo 4f 1	1.01.01	-	2.958 165
	1. IVER	3000.	0.000E 01	. 19aE 1	1	-	-	-	-	0.000 01			- 3000	3000.	. 970E	.051E1	41 GE 1	0.000	. Bul7t 1	2.0326135	0.0000.01	11.92 11 102	3,367 101	1,20% 105	2,1506104	1000	2.1 154 102	7.74.1.105	1.477.103	-	1.0711 134	1.00.1	1.84%	-	2, 95HE 105
	DONE	- 1	0.000E-31	-				BAE	-	0.000E 01	201327.7	3.635.100	0 000E-01		-	-	7.4101.108	0.000E-01	-	-		-	-	1.309E165	3.1501.104	0.000.01	2.14:4 105	7.753E165	1.17/E103	1,0045105	1.0746105	1.8011105	1.049E105	2.5136.100	2.950E 106
	HIGHOID	_	10 3000.0	. 19BE		-	-	304E	.03061	7 3		7. 11.11		OUGE	-				400	-	0.0000-01	-	-	-	3.1401.164	0.0001 01	201 124 107	7.7431.105	1.1971.10.1	-	1.0716164	1.0041.105	1.019E 105		2,95dE104
INID FLAME	H. 1000Y	-	10			-	-	1.3041.109	-	100	-	3.0138.00	2000	- 3	-				100	291 1		-	-	-	2.1501164	0.0001	2,11,11,135	7.753 105	4.49.7.13.1		1.0711.105	1.0011.105	1.047/1.155	2.51.31.1011	2.9500.105
MA 1 GLL. FATHUAY I GEORID	no teamer	1.11-3	3 6 14	3 113 24	4 1-32	5 EC-45	7 (18 51	2 mm 54	0 Int 5.5	9 1 8 55		3	-		::			07 17, 111	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			1	1	=	4.:		717	7			10 / 11	22.1.92	11 7 93	31 2K 75	Jr. 2k 97

TABLE 6 (CONT Page 26 of 39 (For Section 2.2.2.b, units in mrem/year per pCI/m3).

AGE 1 ALL. FATHERY 1 GROWIND PLANE

1. 1. 1. 1. 1. 1. 1. 1.	CRITICAL.	EKIN	BAIN	ENIN	BE. 181	BK IN	BK III	BAIN	61.111	EN LII	W. bub?	51.111	ENIN	LAIN	ENIE	GNIM	DK III	ENIN	EN IN	EN III	EKIN	Chili	BN 111	5k III	Sh in	21.12	11:11	Bt. 1H	ENIM	5KIN	EN IN	EN III	Ek.111	EN III	tik III	ENTH
1, 2010 1, 30.50 1, 20.50	BEIN	1.507E100	10%	13057	11561	-	-	-	-	-		-	-	-	-	-	-	-	_	-	2.735E 105		-	7113E	-	11016	77.E	-	-	11161	1117	1911	-	-	1 OF	BIE
44. Bully HYKHIID BONE LIDER KINGEY LINIO 1. 354E 101 1. 397E 103 1. 797E 103	111-10	-	797E	-	-	-	-	-	-	-	1000.	99111	Still 1	1 17.71.	-	11:76	-	-	-	3264 1	1321	7254	3.3mE	45.45	450E	-	-	-	-	3.597E105	-	1.057E165	-	-	-	-
4. PODLY HYKOLID DONE LIVER KIDNEY 1. 352E 100 1. 345E 104 1. 354E 109 1. 354E 100 1. 344E 1. 797E 165 1. 797E 165 1. 797E 105 1. 875E 105 1. 797E 106 1. 093E 108 1. 093E 1	01411	-	-	-	-	-	-	-	-	-	3	-	-			-	-	-	-	-		-	-	-	-	-	-	-	-	29 AE 1	-	-	-	-		
4. PRIDLY FIFTER BY 1.344E 108 1.344E 108 1.344E 101 1.344E 108 1.797E 105 1.797E 106 1.797E 107 1.	Klinter	-	-	-	-	-	-	-	-	-		-	SSSEI	-	991E1	95761	-	-	-	-	5371.1	-	1 10E	45.34.1	-	-	-	1911	1.030£170	1.478	1125	1 16:0	-	17961	10:11	-
4. PODLY THYKHID BONE 1. 345E 100 1. 345E 103 1. 345EE 1. 797E 165 1. 797E 165 1. 797E 3. 990E 105 3. 990E 105 3. 990E 1. 013E 105 1. 1945E 105 1. 949EE 1. 013E 105 1. 1945E 105 1. 949EE 1. 023E 100 1. 094E 100 1. 094EE 4. 239E 100 1. 094E 100 1. 094EE 5. 994E 100 1. 239E 100 1. 239EE 6. 0300E 01 0. 000E 01 0. 000E 5. 994E 100 1. 239E 100 1. 239EE 6. 030E 10 0. 000E 7. 927E 100 1. 555E 103 1. 239EE 7. 927E 103 1. 555E 104 1. 239EE 7. 927E 103 1. 555E 104 1. 230E 8. 023E 104 1. 555E 104 1. 230E 8. 023E 104 1. 230E 104 1. 230E 8. 023E 104 1. 230E 104 1. 230E 8. 023E 104 1. 230E 104 1. 230E 8. 023E 105 1. 230E 104 1. 230E 8. 023E 105 1. 230E 105 1. 230E 8. 023E 105 1. 230E 105 1. 035EE 8. 023E 106 1. 925E 107 1. 93EE 8. 023E 106 1. 93EE 106 3. 553EE 8. 023E 106 1. 93EE 106 3. 553EE 8. 023E 107 1. 230E 107 1. 93EE 8. 023E 107 1. 93EE 107 1. 93EE 8. 023E 107 1. 03EE 107 1. 93EE 8. 023E 107 1. 93EE 107 1. 93TE 8. 023E 107 1. 93EE 107 1. 93EE 8. 023E 107 1. 93EE 107 1. 93TE 8. 023E 107 1. 93TE 8. 023E 107 1. 93EE 107 1. 93TE 8. 023E 107 1. 93EE 107 1. 93TE 8. 023E 107 1. 93EE 107 1. 93TE 8. 023E	LIVER		797E	-	-	-	-	-	-	-	-		State 1	1 55E	991E1			033E1	1 3756	-	-	1.7236 107	1.23fac 105	2.45.41.105	17076	2.53ot 105		-	1.010110				-	-	-	Mic
4. PRIDLY FRYKING 1. 3454 100 1. 3454 1 1. 7978 165 1. 7978 1 3. 9906 105 3. 9966 1 1. 0136 105 1. 0436 1 1. 0136 105 1. 0436 1 1. 0136 105 1. 0436 1 1. 0139 100 1. 0536 1 2. 040 100 10. 0006 2 2. 040 100 1. 0536 1 1. 0536 105 1. 0436 1 2. 0536 105 1. 0536 1 2. 05	DONE	356E	797E1	13066	045E1	-	-	-	239E1		7											1.723E107			470E			-				35%E	-	17911	11::II	-
1. 3446 1. 7976 1. 7976 1. 7976 1. 7976 1. 7976 1. 7976 1. 7976 1. 7576 1. 757	HIYKBIB	1.3651.108	1.797E105	3.990E 104	1.845E 103	2.039E104	-	-	-	-		-				17/76	_						-	-	-			1.4911.100	1.0305110	3.5976 105	3.115£104	1.059E 105		4.1796104	4, 4025.104	1.72 N 107
	=	1.355E 10H	1.7971165		_	-	3	6.373E103	4.239£ 10B	3.4464 109		13166	Same 1	-	-	=	=	=	=	=	-	-	-	-	-	-	=	=	=	=	-	-	-	-	-	=
	un tentore			_	3	71	1.11	-	41 101 105	41 116M	1 113	12 50-124	47 ft 1258	=	=	=	=	=	-	=	-	-	-	-	-	_	21 (6 134	2.2 (1) 1.55	23 (5) 137	-	-	-	27 63 110	_	22 65 142	20 10 140

TABLE 6 (CONT)

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PARHHAY DUSE PARAHETER FACTORS FOR INFLEMENTING 10 CFR FART 50 (For Section 2.2.2.5. units in mccm/year per (CI/m3).

ABE 1 ALL. FRANK FLANK

7					11			7.1		20	2.5	
CRITICAL	BKIN	SKIN	5KIN	GKIN	U. In	DAIN	ENIN	U. BOI	BK III	W. BO	W. Full	ENIM
BKIN	8.830E105	1.5.39E107	2.430F.105	8.017E107	U. COUE - 01	2.1000.103	1.007E107	0.000E-01	2.739E105	3.000E-01	0.000E 01	1.972E105
111-10	7.35% 105	1.345E107	2.31 1F 104	4.9311.107	0.000E-01	1.01 11 11.1	8.31191.105	0.0001 01	2. 3511E 105	0 000r 01	0.000E-01	1.703E102
LUNG	7.359E105	1.341.E 107	2.314E104	4.934E107	0.000E-01	1.6331.103	0.389E 105	0.000E-01	30 . 3000 . 5	0.000E-01	0.000.01	1.703E105
KIDNEY	7.359£105	1.345E107	2.314E104	4.934E107	0.000E-01	1.6331.103	8.389E104	0.000E-01	2.350E105	0.6006-01	0.000E-01	1.703F 134
LIVER	7.3596105	1.345E107	2.314E105	4.9345107	0.000E-01	1.0336.103	8.389E 104	0.000E-01	2,350E104	0.000E-01	0.000E-01	1.703E105
POSIE	7.359E105	1.345€107	2.314E105	4.934E107	0.000E-01	1.833E103	0.307E106	0.000E-01	2.350E 106	0.000E-01	0.000E-01	1.703E104
THYROTO	7.359E 105	1.325E+07	2.314E105	4.934E107	0.000E-01	1.033E103	8.309E105	0.000E-01	2, 350E 134	0.90GE-01	0.030E-61	1.703E105
W. BODY	7.359E(05 7.359E(05 7.359E(05 7.359E(05 7.359E(05 7.359E(05 7.359E(05	1.355£ 107	2.314E104	4.934E107	0.000E-01	1.0138 103	8. 307£ 105	0.000E-01	2. Jule 104	0.000E-01	0.0000.0	1.703E104
m tentofe												
=	71.	73	7	71	R	2	~	711	6/	23	- 111	11.2

TABLE 6 (CONT) Page 28 of 39 (Nor Section 2.2.2.b, units in mrem/year per pC1/m3).

AGE I AMILT PATHMAY I VEGETALION

1.79 1.79		TEDIOFE	W. BODY	HIYKBIB	BONE	LIVER	KIMEY	LUNG	111-10	BK IN	CKITICAL	
1. 77.21 (0.5.1.79		3	2504.1	2.340£	- 9000.	.2401	. 340E	. 240E	250E	3075	W. BODY	
2. 473E 105 3.492E 105 3.492E 105 2.492E 105 2.492E 105 2.492E 105 2.492E 105 0.000E-01 1.402E 107 0.000E-01 1.625E 107 0.000E-01 1.625E 107 0.000E-01 1.625E 107 0.000E-01 1.600E-01 1.625E 107 0.000E-01 1.600E-01 1.625E 107 0.000E-01 1.600E-01 1.600E	7		-	-	944E	793E +	79.11.105	1.793E105	1.7936103	. 793E1	BOME	
5.434107 0.000E-01 1.002E 09 8.740E 107 0.000E-01 0.000E-01 1.500E 101 0.000E-01 1.002E-01 1.002E-01 1.002E-01 1.002E-01 1.000E-01 1.002E-01 1.000E-01 1.000		34	-	3.49361	. 492E1	492E	492E105	3.492E 105	1 35.69	- 1000.		
1.414(102.0) 0.000(6-01.0) 1.000(6-01.1.0024(104.1.17) (10.0) 0.000(6-01.0) 1.000(6-01.0) 0.000(6-01.0) 1.000(6-01.0) 0.000(6-01.0) 1.000(6-01.0) 0.000(6-01	1	12	-	0.000E-	. 404E	740E	.000E-01	0.000E-01		-3000	DONE	
4, 254 F104 0, 0006E -01 0, 0006E -01 1, 024E 04 4, 17BE 04 1, 17FE 02 0, 000E -01 01 0, 000E -01 0, 0000E -01 1, 172BE 08 9, 1395E 07 0, 0006E -01 0, 0000E -01 0, 0000E -01 1, 172BE 08 9, 1395E 07 0, 0006E -01 0, 0000E -01 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 172BE 08 0, 0000E -01 1, 172BE 08 0, 0000E -01 1, 172BE 08 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E -01 0, 0000E -01 1, 172BE 08 0, 0000E	1.5	13	-	0.000E	. 50%E 1	13014	-	1		-3000 ·	111-19	
\$4 \$7.92F 10 \$0.000E 01 \$0.000E 01 \$1.53FE 10 \$1.000E 01 \$1.	30	77	-	2.783E1	-3000·	-3000	-	. 170E1	171E1	1	111-19	
2. 2.734E 100 0.000E-01 1.037EE101 1.954E 101 0.000E-01 4.912E 102 0.000E-01 101 2. 3.734E 102 0.000E-01 2.094E 103 0.000E-01 0.077E107 9.0424E 107 0.000E-01 101 2. 3.734E 102 0.000E-01 1.240E 103 2.944E 103 0.000E-01 0.077E107 9.0424E 107 0.000E-01 101 2. 3.494E 107 0.000E-01 0.000E-01 3.094E 107 0.000E-01 0.000E-01 3.1324E 107 0.000E-01 101 2. 3.494E 107 0.000E-01 0.000E-01 3.094E 107 0.000E-01 0.000E-01 1.105.E 107 0.000E-01 101 2. 3.494E 101 0.000E-01 1.346E 102 2.484E 103 0.000E-01 1.554E 103 0.000E-01 101 2. 3.494E 101 0.000E-01 1.346E 102 2.484E 103 0.000E-01 1.755.E 102 0.000E-01 1.000E-01 1	-	24	-00	0.00GE-	-3000 ·	128E1	-	- 9000°	50.18	1	177-19	
3.3.24E 10.7 0.003E 01 2.094E 100 0.000E 01 0.077E 10.7 0.364E 101 0.600E 01 0.000E 01	7	2.5	-	0.000E	- 3000 ·	1.539E101	95.4E	1		1	111119	
2.9 1.1351108 0.0005 01 0.0005 01 1.0005 01 0.0005 01 0.0005 01 3.1375 109 0.0005 01 0	524	25	-	3000.0	-	1.44BE100	.000k	-	3646 1	I	Filtis.	
4.9397107 0.000E 01 0.000E-01 3.024E167 0.000E-01 0.000E-01 4.274E108 0.000E-01 0.000E-01 0.1.474E108 0.000E-01 0.000E-01 0.1.474E108 0.000E-01 0.000E-01 0.1.474E108 0.000E-01	200	5.5	-	0.000	-		. OCOE	-	17470		1.11-10	
23 3.2424 100 0.000E 01 0.000E 01 1.471E 100 0.000E 01 0.000E 01 3.137E 109 0.000E 01 1.000E 01 3.2421 109 0.000E 01 1.000E 01 1.5024 100 0.000E 01 1.000E 0	-		-	0.000E	-3000 ·	3.094E167	3000	-	274E1	1	171-19	
3. 4174 101 0.000E -01 7.830E 108 0.000E -01 0.000E -01 5.514E 107 0.000E -01 1011 0.000E -01 1.505E 108 0.000E -01 1.505E -01 -01 1.505	1		-	0.000E		. 471E1	.000		13851		01-111	
3. 41974 104 0.000E-01 1.34GE110 7.211E100 0.000E-01 0.000E-01 1.5GE10B 0.000E-01 1010 4.52474 104 0.000E-01 5.927E101 7.752E100 0.000E-01 1.924E102 0.000E-01 1.924E103 0.000E-01 0.000E-01 1.924E103 0.000E	-		1.302.10	3000	830E	. ABSE	or.	1		A.	DINIE	
4.55.7 [103 0.000E-01 5.927E101 7.75.2E100 0.000E-01 1.92.E10.2 0.000E-01 [104.25.7E10.3 0.000E-01 3.74.E10.3 0.000E-01 3.74.E10.3 0.000E-01 3.74.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 3.74.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 3.74.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 3.74.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 2.34.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 1.10.25.E10.3 0.000E-01 0.000E	-		-	0.000E	346E1	.211E	-3000	J.			FUH	
4.22/7103 0.000E-01 0.000E-01 9.090E103 2.293E104 0.000E-01 7.741E105 0.000E-01 11N 25 4.5531 10H 0.000E-01 7.819E-05 1.493E-05 0.000E-01 1.337E-05 0.000E-01 1.1N 25 1.0040E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.337E-05 0.000E-01 1.1N 25 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.377E-15 0.000E-01 1.1N 25 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 25 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 25 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 25 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 25 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 27 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 28 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 29 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 20 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 20 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 20 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1N 20 0.000E-01 0.000	-		-	0.000E	17/76	75.3E I	. 1	1	94.11	1	11119	
4.554.100 0.300E-01 3.120E100 1.000E169 4.74.E100 0.600E-01 4.3.4/100 0.000E 01 110 1.040E 04 0.600E-01 7.619E-04 1.493E-05 9.714E-04 0.600E-01 4.317E-04 0.600E 01 110 1.040E 04 0.600E-01 0.000E-01 0.000E-01 0.000E 01 4.444E103 0.000E-01 11. 1.040E 10 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.574E14 0.000E-01 10. 1.040E 10 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1574E14 0.000E-01 10.000E-01 0.000E-01 1.1574E14 0.000E-01 11.000E-01 0.000E-01 11.000E-01 10.000E-01 0.000E-01 1.1574E101 0.000E-01 0.000E-01 1.1574E101 0.000E-01 0.000E-01 1.1000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.1000E-01 0.000E-01 1.1000E-01 0.000E-01 0.000E-01 1.1000E-01 0.000E-01 0.000E-01 0.000E-01 1.1000E-01 0.000E-01 0.000E	-		-	30000.0	-3000.	1 3040	2928	. book	7.74:11:15		61-11.1	
1, 04-3E 0.5 0.600E-01 7.019E-0.5 1.49%E-0.5 9.712E-0.5 0.000E-01 3.317E-0.5 0.000E-01 1.040E 0.5 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.577E-1.5 0.000E-01 1.050E-01 1.577E-1.5 0.000E-01 1.050E-01 0.000E-01 0.000E	-		-	-3000.0	17071	BOLLE	74.E	1	001 Jours 77	I	LIVER	
3.00.7 100 0.000E-01 0.000E-01 0.000E-01 0.000E-01 1.577E-13 0.000E-01 0.000E-01 1.577E-13 0.000E-01 0.000E-01 0.000E-01 1.577E-13 0.000E-01 0.000E-01 0.000E-01 1.577E-13 0.000E-01 0.000	=			0.000	-361B	49:34	-371Z				LIVER	
2. 3031E 11 0. 3040E 01 0. 000E 01 0. 000E 01 0. 000E 01 1.57/E 15 0. 000E 01 W. 0. 0041 01 6. 000E 01 0. 000E 01 0. 000E 01 0. 000E 01 0. 606E 01 0. 606E 01 0. 000E 01 W. 1. 017/E 1010 0. 000E 01 11NO 9. 133 E 23 0. 000E 01 0. 0000E 01 0. 000E 01 11NO 0. 0001 01 0. 000E 01 0. 0000E 01 0. 000E 01 0. 000E 01 0. 000E 01 0. 000E 1. 411 H 111 0. 000E 01 4. 000E 01 0. 000E 01 0. 000E 01 1. 777F 110 0. 000E 01 11NO 1. 31.E 104 0. 000E 01 4. 123.E 102 0. 000E 01 0. 000E 01 1. 777F 110 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 130E 104 0. 000E 01 0. 000E 01 1. 777F 110 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 130E 104 0. 000E 01 0. 000E 01 1. 777F 110 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 130E 104 0. 000E 01 0. 000E 01 1. 777F 110 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 130E 104 0. 000E 01 0. 000E 01 1. 777F 110 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 130E 104 0. 000E 01 0. 000E 01 1. 777F 110 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 130E 104 0. 000E 01 0. 000E 01 1. 777F 110 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 777F 100 0. 000E 01 1. 777F 100 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 777F 100 0. 000E 01 1. 777F 100 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 777F 100 0. 000E 01 1. 777F 100 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 777F 100 0. 000E 01 1. 777F 100 0. 000E 01 11NO 1. 711 H 101 0. 000E 01 1. 777F 100 0. 000E 01 1. 777F 100 0. 000E 01 11NO 2. 771 H 102 0. 000E 01 1. 777F 101 0. 000E 01 1. 777F 100 0. 000E 01 11NO 2. 777 H 101 0. 000E 01 1. 777F 101 1. 000E 01 1. 000E 01 1. 777F 100 0. 000E 01 11NO 2. 777 H 101 0. 000E 01 1. 777F 101 1. 000E 01 1. 000E 01 1. 777F 101 0. 000E 01 1. 000E 01 1. 777F 101 0. 000E 01 1. 000E 01 1. 777F 101 0. 000E 01 1. 000E 01 1. 777F 101 0. 000E 01 1. 777F 101 0. 000E 01 1. 000E 0	Ë	11.1	-	0.000	- 1000	-3000	. 3000	E	1 171 1	I	111-19	
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9, BB.S. 23 0,000E 01 0,000E-01 1,023E 22 0,000E 01 0,000E 01 0,000E 01 0,000E-01 U. 0,000I 01 0,000E 01 0,000E-01 0,000E-01 0,000E 01 0,000E 01 0,000E-01 U. 3, B.S. 100 0,000E 01 9, 934E109 0,000E-01 0,000E-01 1,535E109 0,000E-01 U. 1,411 11 0,000E 01 4,000E-01 0,000E-01 0,000E-01 1,777 110 0,000E-01 UI. 1,711 101 0,000E 01 1,000E105 0,000E-01 0,000E-01 1,777 110 0,000E-01 UI. 3, E.S. 103 0,000E-01 1,130E104 0,000E-01 0,000E-01 0,000E-01 1,141 100 0,000E-01 UI. 1,500E-01 0,000E-01 0,000E-01 0,000E-01 0,000E-01 1,144 100 0,000E-01 UI. 1,500E-01 0,000E-01 0,000E-01 0,000E-01 0,000E-01 1,557 104 0,000E-01 UI. 2,513E-02 0,000E-01 1,721E102 0,000E-01 0,000E-01 1,557 104 0,000E-01 UI. 3,509E-03 0,000E-01 1,721E102 0,000E-01 0,000E-01 1,212E109 0,000E-01 UI.	3	7	-	1000.0	ī.	. 111/E1	JOE .		311E	1	11911	
0.0551 01 0.050E-01 0.050E-01 0.000E-01 0.050E 01 0.000E 01 0.005E 01 0.050E-01 IIII 3.157E 1031 0.050E 01 9.954E 109 0.050E-01 0.050E-01 1.5°5E 109 0.050E-01 IIIII 1.4B II II 0.050E 01 5.045E III 0.050E-01 0.050E-01 1.747E 110 0.550E-01 IIIII 1.7B II II 0.050E 01 1.059E 105 0.050E-01 0.050E-01 1.747E 110 0.550E-01 IIII 1.7B II II 0.050E 01 1.059E 105 0.050E-01 0.050E-01 0.050E-01 IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	ž	=		3000.0 8	Æ.	1177E	1000	1		L	LICER	
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1. 48 if 111 0.000F 01 4.045E111 0.000E 01 0.000E 01 1.747 110 0.000E 01 11.11 E104 0.000E 01 13.009E 01 0.000E 01 1.000E 01 11.11 E104 0.000E 01 13.009E 01 0.000E 01 1.431 102 0.000E 01 11.11 E104 0.000E 01 13.009E 01 0.000E 01 0.000E 01 1.431 102 0.000E 01 11.11 E104 0.000E 01 0.140E 101 0.000E 01 0.000	-	60	-	10000.0	954E1	. 3000°	. Odok .	1	135.45	1	Title II	
1.31.6 104 0.0056 01 3.009E105 0.000E-01 0.000E-01 0.000E-01 1.4316 102 0.000E-01 11.7116 101 0.0056 01 4.1336 102 0.000E-01 1.4106 101 0.000E-01 1.4106 101 0.000E-01 0.000E-01 0.000E-01 1.4106 101 0.000E-01 1.4236 101 0.000E-01 1.4106 101 0.000E-01 0.000E	3.0	0.6	-	1 0.000t	045E1	- 3000'	. 3000.	M.	11711		Little	
1.7011 101 0.000F 01 4.133E102 0.000E-01 0.000E-01 0.000E-01 0.000F-01 0.000F-01 0.000F-01 0.000E-01 1.310E103 0.000E-01 0.000E-01 0.000E-01 1.410E100 0.000E-01 0.000E-01 1.410E100 0.000E-01 0.000E-01 0.000E-01 1.410E100 0.000E-01 0.0000E-01 0.000E-01 0.00		1,4	-	4 0.00ct	13500	3000°	3000	A	1 1111		61 11.1	
3,554,163 0,000E 01 1,310E104 0,000E 01 0,000E 01 1,410E100 0,000E 01 1,1991 10 0,000E 01 4,930E 09 0,000E 01 0,500E 01 0,000E 01 1,440E 00 0,000E 01 1,340E105 0,000E 01 1,1440E 01 0,000E 01 0,340E 02 0,000E 01 1,114E105 0,000E 01 0,000	100	9.3	-	0.00CE	12:2E	-3000 ·	1000	J	17351		-	
1,9091 10 0,000E 01 4,930E 09 0.000E 01 0.500E 01 0.000E 01 1,444E 01 0.000E 01 61. 1,334E 105 0,000E 01 5,112E 105 0,000E 01 0.000E 01 0.000E 01 2,812E 109 0,000E 01 61. 2,513E 02 0,000E 01 1,944E 01 0,000E 01 0,000E 01 1,557E 104 0,000E 01 61. 4,751I 100 0,000E 01 1,721E 102 0,000E 01 0,000E 01 5,457E 104 0,000E 01 61. 2,594E 105 0,000E 01 1,194E 105 3,035E 105 6,000E 01 1,214E 107 0,000E 01 61. 3,091E 101 0,000E 01 3,354E 102 4,727E 101 1,023E 102 0,000E 01 2,094E 107 0,000E 01 61.		0%	1.5.L.	0.000E	3.10E	1000	-3000	A.	11011	. 000k		
1.334E105 0.000E 01 5.112E105 0.000E 01 0.000E 01 0.000E 01 2.812E109 6.000E 01 61 0.213E 02 0.000E 01 0.942E 01 0.000E 01 0.000E 01 1.357E104 0.000E 01 61 4.7511 103 0.000E 01 1.721E102 0.000E 01 0.000E 01 0.000E 01 1.721E102 0.000E 01 0.000E 01 0.000E 01 0.000E 01 0.000E 01 0.312E103 0.000E 01 0.312E103 0.000E 01 0.312E103 0.000E 01 0.312E103 0.000E 01 0.000E		7111	1306	3000 C	9.30E	-3000.	-300G		1111	1	. 1	
2.513E 02 0.000E 01 0.944E 01 0.600E 01 0.000E 01 0.600E 01 1.557E104 0.060E 01 61 4.7511 103 0.035E 01 1.721E102 0.000E 01 0.000E 01 0.000E 01 5.457E104 3.000E 01 61 5.594E105 0.605E 01 1.194E105 3.035E105 5.019E105 0.000E 01 1.214E107 3.000E 01 0.000E 01 3.354E102 6.727E101 1.023E102 0.000E 01 3.354E102 6.727E101 1.023E102 0.000E 01 2.094E107 3.003E 01 61 61 61 61 61 61 61 61 61 61 61 61 61		1.6	-	0.000E	11761	3000'	- 30co.	1	17718			
4,75H 103 6,035E-01 1,721E102 0,000E-01 0,000E-01 0,000E-01 5,457E192 3,000E-01 61-2,595E105 0,000E-01 1,212E107 3,000E-01 0,000E-01 3,354E102 2,727E101 1,023E102 0,000E-01 2,095E107 3,000E-01 61-2		9.3		0.000	- 371 6	- 3000 ·	1000	- 3000 ·				
3.091E101 0.000E 01 3.354E102 4.727E101 1.022E102 0.000E-01 2.092E107 0.000E-01 61-		63	-	6.000E	1.721E102	0.000E 01	.000E	- 3000 ·		- 3000 ·	*	
3.071E101 0.000E 01 3.354E102 4.767E101 1.023E102 0.000E-01 2.092E107 0.003E-01	2	7.2	-	0.00CE	1.192E105	3.035E 105	.019E1	-3000°	1.2126 109	3000	X.	
	10	16	-	1 0.000E	3.354E162	3/7/	-	.0000.	.09:E	- 9000	1.11-19	

TABLE 6 Page 29 of 39

FATHMAY MUSE PAKAMETER FACTORS FOR INFLEMENTING 10 CFR PAKT SO

A HARRY L. A. HARR	Secritor 2.2.2.b, unitib 1 Secritor 2.2.2.b, unitib 1 OE 01 1.423E105 7.914E104 OE 01 2.730E 04 4.809E 07 OE 01 3.093E100 8.710E104 OE 01 3.093E100 8.710E104 OE 01 1.929E100 0.000E 01 OE 01 1.934E105 1.77E110E105 OE 01 1.934E105 1.77E110E105 OE 01 1.934E105 1.77E110E105 OE 01 1.934E100 1.21E10E105
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TABLE 6 (CORT)
Page 30 of 39

(FOR Section 2.2.2.5, units in mrem/year per pict/m3).

AGE I ABURT PATERATION

CRITICAL												111-19
EKIN	10-3000 · 0	9.000E-01	0.000E-01	0.000E-01	0.000E-01	0.00CE -01	0.000E 01	0.000.01	0.000E-01	0.000E-01	0. GOOF -01	C. OCOE - 01
177-10	4.419L-01	5.094 100	2.754 107	1.1131.110	2.7151.100	0.000F 61	1.844£ 100 0.000E	4.4531 1601	1.017.167	4. 2.1.1.09	1.33cE110	2.84.36.10?
11010	0.000E-01	0.00CE-01	0.000E-01	0.000E-01	0.000E-31	0.000E-01	0.000E 01	0.000E-01	0.000E-01	0.000E-01	0.000E-01	0.000E-01
KIDNEY	0.000E-01	4. 1.1	3 12	E 5 JE 104	1.4481.104	0.00cE-01	2.350£104	0.0001-01	0.000E 01	1.499E110	1 4025110	4.35 1E 102
LIVER	4.051E-05	1.333E 105	7.349E105	1.375E107 E., 51E104 0.000E-	2.509E101	0.000E-01	3.849E104	5.754E105	3.101E164	0.000E-01	0.0000.01	1.394E102
POME	1.331E-04	1.970E105	9.964E103	3.260E107 1.375E107 E., 54E104 0.000E-01 1.113.110 0.000E-01	4.355E104	0.000E-01	3.330E104	1.7346107	3.803E104	4.427E110	4.1471.10	1.419E103
THYROTO				-	-	0.000E-01	0.000E-01	0.000E-01	0.000E 01	0.000E-01	0.000E-01	0.000E-01
W. 1000.	1.50HE-05	1.511E104 0.000E-01	0.154E101	1.745E104	3.161£103	0.000E-01	3.303L 103 0.000E-0	6.0454.103	1.112E104	3.6954 169	3.5451109	7.497E101 0.000E-01 1.419E103 1.394E103 4.354E102 0.000E-01 2.04.4E102 0.000E-01
no tsorore	=	7	3	CE 144	FK-143	111 141	110-147	n 105	1.01.11	11 235	01.2.10	111 - 339
3												00

(CONT) Page 31 of 39 TABLE 6

FAIRMAY BOSE FURGHETER FACTORS FOR IMPLEMENTING 10 GFR PART 50 (For Section 2.2.2.5, units in mrem/year per pg1/m3).

11. 3 2.500E103 3.500E 11. 3 2.907E105 3.90E 11. 32 4.317E107 0.000E 12. 32 4.317E107 0.000E 13. 34 5.317E107 0.000E 13. 51 5.105E101 3.437E 14. 51 5.105E101 3.437E 15. 51 5.105E101 3.000E 16. 53 5.30E100 0.000E 17. 54 5.30E100 0.000E 17. 55 5.40E100 0.000E 17. 55 5.40E100 0.000E 17. 50 5.40E100 0.000E 18. 50 5.60E100 0.000E		LIVER	KIMEY	1 11110	1.11.10	EKIN	CKITICAL
2.907E165 3. 5.379E165 3. 5.379E165 0. 6.105E104 3. 9.010E107 0. 1.419E104 0. 1.419E104 0. 1.419E104 0. 1.419E104 0. 5.597E104 0. 1.419E104 0. 5.597E104 0. 1.419E104 0. 2.419E106 0. 3.417E106 0. 3.417E106 0. 4.336E104 0. 6.606E 01 0. 4.336E104 0.	103 0.000E-	2.50BE	Subt 1	SBBE !	Sour !	2.58HE 103	ż
2. 3904 1055 2. 5. 317E 107 0. 1. 517E 107 0. 2. 145E 104 3. 2. 45E 100 0. 2. 45E 100 0. 1. 517E 100 0. 2. 557E 100 0. 3. 147E 100 0. 3. 147E 100 0. 3. 147E 100 0. 4. 340E 100 0.	105 1.	2.907E1	2.907E105	3.907£105	2.90.% 10D	.907E1	
5.21/E107 0. 1.51/E103 0. 5.105E104 3. 5.005E107 0. 2.45/E104 3. 5.55/E104 0. 5.55/E104 0. 5.55/E104 0. 5.55/E104 0. 5.55/E104 0. 5.74/E108 0. 3.47/E108 0. 3.47/E108 0. 5.48/E108 0. 3.47/E108 0. 5.48/E108 0. 6.606E 61 0. 4.346E104 0.	105 2.390€1	3.390E1	. 390E 1	. 390E	13005	€.	ż
6. 105F105 0. 6. 105F104 3. 7. 010F107 0. 2. 010F107 0. 1. 0116 100 0. 5. 557F100 0. 1. 012 100 0. 3. 0172F100 0. 1. 010F100 0. 3. 0172F100 0. 4. 3306F101 0. 4. 3306F101 0.	01 1.611E1	,	- 3000 ·	- 3000°	35 11 1	. 000E	NIN.
6. 103E 104 3. 9. 010E 107 0. 2. 112E 100 0. 1. 61 1E 100 0. 5. 597E 100 0. 1. 112 100 0. 5. 112 100 0. 3. 112 100 0. 5. 112 100 0. 4. 112 E 21 0. 6. 600E 61 0. 4. 113 E 100 0.	01 3.745£1	5.300E1	-	.000E	taval.	3000 ·	3
9.010E102 0. 2.4581100 0. 5.4581100 0. 1.5141108 0. 1.5141108 0. 1.5141108 0. 3.4541108 0. 3.4541108 0. 3.4541108 0. 3.4541108 0. 4.346108 0. 4.346108 0. 4.346108 0.	104 0.000E	0.000E	-	. B 32E 4	1.0401167	- 3000 ·	10
2. 454E 100 0. 5. 48HE 102 0. 1. 614E 100 0. 1. 614E 100 0. 5. 597E 100 0. 3. 444E 100 0. 3. 444E 100 0. 3. 444E 100 0. 3. 444E 100 0. 4. 444E 100 0. 6. 650E 61 0. 6. 650E 61 0. 4. 4346E 100 0. 4. 4346E 100 0.	10	4.543£1	-	(4)	. 31111	. 000E	19
5. Jane 102 0. 1. £15£100 0. 1. £15£100 0. 5. 527€100 0. 3. £15£100 0. 3. £15£100 0. 3. £15£100 0. 3. £172€100 0. 1. £17€11 0. 6. £30€10 0. 1. £136€10 0. 4. £36€10 0.	-3000°0 10	1. Julik 4	.757E1	- 900CE	1311	.000F	9
1. 2152 108 0. 1. 61 16 108 0. 5. 5976 108 0. 5. 1124 108 0. 3. 1174 108 0. 3. 1174 108 0. 3. 1174 108 0. 4. 1776 11 0. 6. 6506 61 0. 1. 1178 11 0. 6. 6506 61 0. 4. 3366 108 0.	01 3,259£1	2.310E	.000E	-	-	.000E	200
5. 597E 100 0. 5. 597E 100 0. 1. 4021 100 0. 3. 414E 100 0. 3. 417E 100 0. 3. 417E 100 0. 5. 417E 100 0. 7. 417E 100 0. 1. 6. 650E 61 0. 4. 330E 101 0. 4. 330E 101 0.	-01 1.793E1	4.101E		.3181	OHEA.	1000.	3
5.597E104 0. 1. 4021 104 0. 5. 4 1/2 104 0. 3. 4 1/2 104 0. 3. 4 1/2 104 0. 5. 74 0. 5. 74 0. 6. 600 0. 1. 200 1.0 6. 600 0. 7. 330 0.00 0. 4. 330 0.00 0.	01 0.000E	÷	.000		-	1000.	9
5. 11.2 100 0. 5. 11.2 100 0. 3. 12.4 100 0. 3. 12.4 100 0. 5. 11.2 100 0. 2. 11.2 10 0. 1. 11.2 10 0. 1. 21.0 10 0. 4. 33.0 10 0. 4. 33.0 10 0.	3000.0 10	-		3000	Baint !	3000°	19
5.11/L 10H 0. 3.21/L 10H 0. 3.11/L 10H 0. 5.11/L 10H 0. 9.71/L 0.0 1.11/L 11 0. 1.21/L 11 0. 4.330E10H 0.		3.04564	- 9000°	1000°	11/2	COCE.	2
3.232 100 0. 3.474 103 6. 5.1631 104 0. 9.744 07 0. 2.1874 100 0. 1.137 11 0. 6.650 61 0. 1.210 21 0. 0.606 01 0. 4.330 104 0.	01 1.	-	10 1000.0		-	.000E	Ξ
3.42.4E 103 6. 5.163 1E 1040 0. 9.72.4E 0.7 0. 2.49.2E 100 0. 1.41.7E 11 0. 6.650E 61 0. 9.173E 23 0. 9.173E 23 0. 4.330E 1040 0.	01 5.55 IE I	. 077E3	1000.	.000E	1.111	.000F	111.19
5.115.1E 10H 0. 9.724E 07 0. 2.197E 10 0. 1.117E 11 0. 6.650E 61 0. 1.210E 10H 0. 9.172E - 23 0. 0.606E 01 0. 4.330E 10H 0.	01 0.000E	0.23:Æ	. 00 11 1	3000.	. 311.16	1000 ·	3
9,74E 07 0. 2,892E100 0. 1,827E 11 0. 6,650E 61 0. 1,210E108 0. 9,172E 23 0. 0,606E 01 0. 4,340E108 0.	01 4.25IE	1.459E109	7.403E10B	1000	-		
2. 09.2E 100 0. 1. 0.27E 11 0. 6. 650E 61 0. 1. 200E 100 0. 9. 173E 23 0. 0. 606E 01 0. 4. 336E 00 0.	01 7.323E	1.395E-	1115E	.000E	10/9	1000	3
1.027E-11 0. 6.650E-61 0. 1.200E-100 0. 9.173E-23 0. 0.606E-01 0. 4.336E100 0.	-3000.0 10	0.000E	3000	. 000E	1000.	3000	3
6, 630E 61 0. 1, 210E 104 0. 9, 173E 23 0. 0, 606E 91 0. 4, 336E10H 0.	010	0.00CE	0.000E 01	3000°	0.0001 01	. OOOF	
1.200E100 0. 9.173E-23 0. 0.606E 01 0. 4.330E100 0.	01 0.000E	0.000E	. J000 *	. 600E	1000	SOOP.	i
9.173E-33 0. 0.606E 01 0. 4.330E10H 0.	3000'0 10	2.73561	.000E	1	0.111.1	3000 ·	=
0.606E 01 0.	01 0.000E-	1.721	0.0001 01	1000.		3000	-
4.330E10H 0.	-3000.0 10	0.000E	1000.	1000	1000 ·	- 1000 ·	i
1.053E111 0.	01 1.51261	0.000E	1000	1000	. 001E1	1000 ·	
	01 7.507E1	0.000L	ī		2.1071110	.000	DONE
1.11111101 0.	2.BIJE	0.000E-	3000	10000.	1777	10000	- 19
1.537.101 0.	3.840E	0.000E	0.0001 01	3	. 711.1	0.000E	11 11
3.347/102 0.	01 1.24	0.000E	300c.	3000°	1 7 0	0.00GE	11-19
1.755E 10 0.	01 4.591E	0.000E	- 0000°	. 000E	1171		1 19
2,104,105 0.	-01 7.01361	0	3000 ·	.000t	-	- 0000.	11-19
3,413, 63 6.	01 8.40	.000E	. 1000.	J.	1701.	0.0001	3
1.43 11 106 0.	01 1.514E	0.000E		1000 ·	11	- 3000 .	
1.00m 105 0.	01 1.755E1	5.5300	1001	0.000E 01	-	.000F	2
2.010E101 0.		1 6.1441.101	9.3141.101	0.000E 01	1.434E107	0.000E 01	1111

3

TABLE 6 (CONT)
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		FAII	(For Section	ton 2.2.2	(For Section 2.2.2.b, units	In mesm/year	HAD TO CFR PAR	C1/m).		
TATHMAY I VEGLTA	ILEN T I VE	DE TATION								
NO 15010FE	int.	H. BOBY	HIYKOID	FONE	LIVER	N. I EME Y	1.000	111-10	NI NI	CRITTEM
	2	5.0554.104	0.000F 01	1.921E105	1.045E105		3000	-	.000E	111-10
37 mm	11	1.5:11 0.		. 791E 0	. 531E-	.374E-		1		177-19
	66	111		1	5.431E104	.209E1	- 9000.	*	1000	KIMEY
	N44	1717	3000.	. 730E1	7.410E103	1.1340102	. 234E I	-	- 3000°	01-11
	101	. 30g	-3000.	T	0.000E-01	0.	T	3000 ·	-3000.	3
3	103	-	3000.	4.1191E105	- 000E-	. 439E1	. 000E	-	- 3000 ·	7
	105	13F 8	0.000E 01	-	- 3000°	. 347E 1	. 000E	. 99th 1	E	111-19
	105	0.31.6	Ŧ.	-	6	-	3000.	1.411.110	A	=
	HOTE	0.735E105		1.517E107	1.435E107	73%E1	T).	.03111	J	=
	HELL	1370	0.000E 01	0.000E 01	5.4011107	4.205E107	0.000E 01	2,2731 169	T.	7
	131	1.11.1	2.712£105	1.1.25 100	2.116E105		4.705E107	-	8.	
	HEE!	1121	4.150E107	1.405E 10B	. 35.2E i	3000°		-	- 4000°	177-10
=	113711	SYEL	-	-	1.934E10B	2.235E 109		-		KIMEY
11	127	5.31.1	-	5.350E 103	1.899E103		0.000E 01	4.1376165	0.000t-01	177-10
=	1.9H	3.4HPE 107	1.140E 10B	=	1.331E10B	1.504£109	Ŧ.	1.31-1.109	8	KILDERY
=	62.1	1101	5.235E 04			.070E	0.000E 01		1	01 111
11 ES	1318	1377	4.070E	8.415E1	. 035£ 10	. 26ut 10	0.000E	4.2491.107		11119
	131	916	4	1.278E-	37E-		0.000E	1.0176-15	- 9000°	F. I IABLE Y
	133	1/4	JIIE I	3.091E	3. 44 E	. 32.46 10	0.000E	-	1	111-10
	30	4.0741.105	20E I	3.537E	1.020E	-	0.000E	. B11E	- 3000 ·	THYKOLI
	31	11.16	3.141E110	7.489E107	1.073E 1	13	0.000	13%	1000	HYKOLE
	1.1	4. 4921.101	4.32164	+	1.35.41.10	. 97.1E 1			- 3000°	HIYKUII
	1.1	7111	1.572E	1.9334	3.37BE	14981	3000	-	3000°	HILL
	13	17:5	1.41.1	1.7.35	2.0381	E .	0.000E	1667	- 9000r	HIMEOTE
1 1 07	22	9.31.1	5.7154	-	H. BB 18 10	. 4031.10	0.0001	177.0	3000	IIIIKOII
	1.14	1707	0.000F	-	8 . 57.0E B	John I	.03/F1	-	1	3 5 7
	1.34	1.11	0.000E	4.269E107	1.400	-	. 4 mil.	-	- 9000°	LINER
	1.1.	4.27:4 107	0.0031 01	1.0136.110	1.3181.110	4.04 34 10V	1.703.139	1.9101 100	0.000E 01	LIVER
	1111	177	B		. 4 151.	4.7516 11		- 30E6.	F	LIVER
	1.17	0.000.01	0.000 01	0.000E 01	0.000E -01	T	-300	3000.	6.00GE-01	W. DOBE
	1.17	1.1	0.0001 01		1.791E	7	8.2346	2,374E 61	0.000E 01	1
	140	6.th: 1 105	£	-	1.489E1	5.7.7.101	1.132£1.1	13771	T.	111.19
211 lbs	les 141	4		1	T.	T	X.	. 10000.	0.000E-01	
	113	100	7		Ă.	1	I	F	1	u. 1:01)
	149	2, 54.31 102	0.000 01	1.0071.103	B. B76E 103	10-1000.0	0.000E-01	5.07ut 107	0.0000.01	11-19

TABLE 6 (CONT)
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(POE Section 2.2.2.b, units in mrem/year per pot/m3).

Anie 1 leen

CKITICAL DOM 3030000000 0.000E SK IN 5.395/ 108 2.037/ 108 2.037/ 108 2.037/ 108 2.301/ 108 2.301/ 108 7.323/ 108 7.097/ 109 1.509/ 110 1.11.10 33333333333 tun. 11.221E-04 5.424E-05 0.000E-01 0.000E-01 0.000E-01 0.315E|02 4.770E|05 3.040E|02 0.000E|01 0.305E|02 0.000E|01 0.305E|02 0.000E|01 0.000E-01 0.000 KILHEY LIVER 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 0.000E-01 HIVEOILE 2.1581E-05 2.158101 2.833E101 2.833E103 3.103E103 5.135E103 4.115E109 4.115E109 7.217E101 PUBLIX ; IN TEGINE ERREASERRESE

INTERNAT I VENETATION

TABLE 6 (CONT) Page 34 of 39

			(For Section	2.2.	2.b, units	in mrem/year	per	µC1/m³).		
TO THE	AGE I CHILD FATHWAY I VEUETO	UEINTION								
9	NO 15010FE	W. SOBY	HIYKOID	DONE	LIVER	KIMEY	Lung	111-19	BAIN	CRITICA
-	-	4.00BE 103	4.00UE 103	0.000E-01	4.00UE 103	4. COUE 103	4.00BE 163	4.00UE 103	1.00UE 103	u. 605
3 5	11	7.00ut.105	7.00BE 105	.504E1	-	-	-	-	-	DONE
3 11	0-24	-		3.732E105	3.732£105	3.732E105	3.732E105	3.733£105	0.000E-01	H. But
4 1	F 32	1.301E10B	0.000E-01	3.375£109	1.5796100	0.000E-01	0.000E 01		0.000E-01	DOME
25 25	1.45	1.2791.105	0.000E 01	2.195E165	4.302E105	_		-	0.000E-01	111-10
3 7	R 51	1.175E 105	4.522E104	- 3000 ·	8	, 7u3£ i	-	2331	T	111-19
7 11	HN 54	1.770€ 108	3000°	0.000E-01	4.545E10B	-	0.000E-01	5.57BE 10B	0.000E 01	LIVER
11 11	11 5.5	4.100E100	0.0006 01	0.000E 01	-	2.197E101	0.000E-01	-	0.0001-01	01-11-1
6	E - 15.5	1.317E100	0.000E-01	B.013E100	4.25GE 100	0.000E-01	2.404£108	7.873E 107	0.000E-01	BONE
	60. 3	3,2001.100	0.00ct -01	3.9701.100	4. 423E 10H	1	1.0525100	6. 2441 1011	0.000.01	61-11.1
	0 50	1.90/1.100	0.000E-01	0.000E-01	-	6.030E 01	0.000E-61	3,704,160	T	11111
	EB 50	-	0.000E 01	0.000E-01	3.70 JE 100	0.050E-01	0.000E-01	2.09:4 167	0.000E-01	177-19
	62 1	-	0.000E 01	7.103E10B	2.4531 108	0.COOE 01	0.000E-01	5.073£ 107	0.000E-01	BUHIE
14 11	1.2.1	-	7	3.949E110	2.11 IE 109	0.000E-01	0.000E-01	1.4211100	0.000E-01	DINH
	177	5.401E100	0.000E 01	1.019E102	9.5756103	0.000E-01	0.000E-01	1.1751 103	0.000E-01	01 111
		3.551E103	0.000E-01	0.000E-01	1.013E101	2.424E104	6.000E 01	5.09HB 165	0.000E-01	111-19
		1.3441.109	Ŧ.	B.112E10B	3.161E109	-	T	-	Ŧ	LIVER
		1.004E 05	0.0001 01	1.351E 05	-10	1	1	1.236t 03	T	-
		5.43 IE 106	0.0006 01	0.000E 01	×.	T	1	.000E	0.030E 01	
		3.1011	J	0.000E-01	0.000E 01		E	I.	T	H. 500
		0.000E 01	0.0001 01	-3000		0.0001 01	1		1	u. 505
		2,7478100	0.000E-01	0.000E-01	-	T.	T	-	ī	LIVER
		1.45.11 33	. 3000.	.000E	4	1			T	LIVER
		0.000E 31	0.0001 01	0.000E 01	0.000E-01		T		T	n. File
		1.0.151.09	0.0001 01	-	B.	1	1	-	7	Finite
		3.15.9.111	0.0001 01	1.21.11.11.2	0.0001 01	0.0001.01	T	-	T	HINN
		1.95.11.101	0.000L 01	5.1754 105	0.000E-01	0.0001 61	0.630E 01	1.1111104	1	61 111
		2.11211.101	0.000E 01	7.03ft 102	0.00CE 01	0.0001-01	0.000E-01	-	T	11119
		4.17.1.102	0.0001. 01	2.30H 104	Œ.			4.3701 107	I	
30 1	1 7111	3.05M 10	0.0001			1000.	T		7	
	1.6	4.9764 105	0.0001 01	1.06.36.107			k	2.41151.109	8	
	1 73	4, 4404, 02	9	1.5400 100		Ŧ.	0.000E 01	-		1119
	5.6	131	6.000E 01	2.97.3£ 102	0.0001. 01	8.	1	-	1	
	28 MZ	7.70.3 105	0.0004 61	-	-	#	J.	-	T	11119
. 4:4.	1. 97	4,0138,101	0.0001 01	5.459E 102	B. 1916 101	1.1758.102	0.0001-01	1.2411.107	0.000E-01	11-19

TABLE 6 (CONT)

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(For Section 2.2.2.b, units in mrem/year per pG1/m3).

FATHAY I VEGETATION

3	no morore	u. muy	HIYKOID	DONE	LIVER	KIDIEY	FINIE	111-19	BATH	CKITICAL
1	NB 95	1.1411.103	0.000E-01	4.101E105	1.597E105	1.500E 105	0.000E-01	2.9536 100	0.000E-01	111 10
-	offe 97		T	1.1095-04	2,799E-07	3.255E-07	1	1.033E 03	. 000E-	111-19
311	-	1.903E 104	1		7.593E105		*	4.352E104	3000	KIMEY
14	11. vvn	1.1.351 102	0.0006-01	4.595E 100	9.30EE 100	1.130£102	4.675E100	5.210F163	0.000E-01	111 19
10			T.	0.000E-01	0.000E-01	0.000E G1	0.000E . 01	0.000 01	1	W. folloy
=	4	5.959E134	0.000E-01	1.550E107	T	3.902E107	0.000E 01	1.06td 100	0.000E-01	177-10
+	-	3.3900.131	0.000E-01	9.070E101	0.000E-01	7.9731 103	0.000E 01	5.9304.101	0.000E 01	111-10
1.5	-	-	0.000E 01	7.459E10B	0.000E-61	1.0076 109	6.600E-61	1.120110	160	111-10
-	HC11-110	1.735E107	0.000E-01	3.216E107	2.1726107	4.012E107	0.000E 01	2.5t. u. 169	0.000E-01	111 19
12.	Ch. 115d	-	0.000E 01	0.0001-01	4.351E107	3.3731107	0.60UE 01	1.7md 167	0.0000-01	11119
-	ER 134	3.524E1	2.155E105	0.931E107		3	5.921E167	2.5.1 H 147	0.000k 01	177 19
1	H . L 35.M	4.503E1	9.659E107		9.5::0E 10.	0.0361 01	10 1000.0	3. :: 17E 1 5E	0.COCE-01	Dinit
=	11. 13./h	1.15251.1	3.151E 10B			-	10	1.070E 1G9	6.00CE 61	KINGET
4.	11 127	2.136	4.84.3E 103		-	2.8131.161	0.000E-01	3.114.2E 555	3	111-19
3	11. 129H		2.493E100	B.354E100	2.133E100	2. 45.3E 109	0.000E-01	1.01%167	0.000E 01	KIIGH: (
.7	47 1 31		9.54111-01	1.355E-03	3.701E-01	3.9431-63	0.000E-01	8. 111E 52	0.000E-01	01 41.1
1	11 - 13111	5.4500 105	1.09.3E10.1	1.5372105	5.314E105	5.115E105	л	2.15.4.167	X.	
7.			1.800E 15	2,353E-15	7.1716 14	7,1176-15	0.0000.01	1. 1346	0.000E 01	111 19
-:		3.7.374.105	4. 19 1E 105	4.973E104	3.004£ 104	2.0456.107	0.030E-01	3.1026 107	0.000E-01	111 19
.7		6.41.1E1	1.37HE 10B	4	1.351E105	1.05%104	0.000E 01	2.BEC4 105	0.000E-01	THYROLD
-7	1 131		4.75/1110	1.1306108	1.139£ 100	2,3526100	0.000E-01	1.201E162	0.000E 01	HIMMIN
12	1 133		7.245E103	8.478E 101	1.542E102	2,390E102	0.000E-G1	1.03fa 103	C.000E-01	HIVEOID
7:	1-133	1.419E104	U. 07 4E 109	3.523E105	4.355E 101	7.241E104	0.000E 01	1.752E 104	0.00CE-01	HIGHIR
:	1-131	1.1716 04	5.95 NE 03	1.3738 04	2.5496 01	3.890E 04	0.600E 01	1. 290E -04	C.000E-01	HIVEOUR
3,	1.13:	D. 1261 164	9.774E105	4.130E104	1.104.165	1.49.1E 105	0.000E-01	10.407.101	0.000E-61	HINKOID
-7	CE 1.54	201 361 37. 199	T.	1.5031.110	111	0.15:4109	-	1. HIR 108	T	LIVER
-1	CB 135	1.4146 130	0.0000.01	0.0435.407	2.314E 103	1 . 1 iiof. 10ii	1.750L107	7.74.1.106	6.060E 01	LINER
17	(8 137	3. 3Hot 109	0.0001 01	3.393£110	2.3906110	7.14.34.169	2.4056 109	1.1141 106	0.000E 01	Petral.
77	CB 130	5, 3, 54, 11	0.000E-01	1		1	1	T	T	LISTE
-1	_		0.03CE 01	0.000E 01	0.000E-01	0.0001-01	0.6306-01	0.000E 31	0.0006 01	u. pour
-	11 11 N	1.3596-03	T.	. 69 JE	2.505E-05	2.1111E 05	1.474E -05	2.76% 100	6,030E-01	1711-19
1	P. 140	1.5111.107	0.300E 01	-	-	-	-	1.3971 100	T	FORM
7.8	161 141		0.000E 01		di.				T	HOME
-1	ba- 142	0.0008 61	Ž.	OJE	1	8	T	0.0001 01	0.000E-01	W. BIBLY
20	14 140	3.5356.103	0.000E 01	3.245E103	1.134E163	0.000E-01	0.000E-01	3.152£107	0.000E-01	61-111

TABLE 6 (CONT)

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(For Section 2.2.2.b, units in mrem/year per pol/m3).

CATHERY I SUGERSTON

CKILICAL	111-10	111-10	61-11.1	01-111	111 10	111-19	177-19	111-19	111-10	EGriff	BOHE	1.11-13
	-	10	0.1	10	10	10	0	10	10	10	10	10
ENIN	C.000E	C.000E	0.000E	0.000E	0.000	0.000E	4.000E	4.000E	0.000E	0.000E-	9000'0	0.000E
1.11-10	1.39:NE 101	4.07CE.108	1.323.107	1.0331 116	1.5391100	2.4.1.1	9.1211 107	5.40% tou	5.35vi 105	5.7411.169	1.2361110	E-01 1.3524107 0.000E-01 GI
	10	10	10	10	10	10	10	10	10	10	10	10
1 11110	0.000E	3000.0	0.000E-	0.000E	0.000E	0.000E	10000.0	10000.0	0.000	0.000E	3.000£	0.000E
	0	03	03	07		10	60	13	5	9	10	03
A Butter	0.000	1.43381	3.903E	2,3056.4	2:345E	3000.0	3.171E	0.000E	0.000E	1.375£1	1.3864	5.2836
LIVER	7.054E-05	3.249E 105	9.300E 105	3.982E107	4.357E104	0.000E-01	5. 703E134	5.019E104	3.013E104	0.030E-01	0.000.01	1.037£102
FUHE	3.309E 05 0.000E 01 3.313E-04 7.054E-05 0.000E-01 0.000E-01 1.39HE101 6.000E-	4.555£105	1.715E103	1.270E100	1.454E105	0.000E-01	7.11GE104	1.50%E107	4. 117E104	5.09%E110	5.430E110	2.544E103
2	3	10	10	10	10	10	10	10	0	10	0	10
HYKUID	9.000E	0.000E	1000.0	0.000E	0.000	0.000E	0.000E	C.000E	0.0001	10000.0	1000.0	0.000E
W. Fulfi	00 360	34E104	17:103	10E 105	141103	10 TOT	/it 103	201 167	111.161	.W 10%	451.109	BIL 102
3	2.3	4.1	1	7.7	7.3	0.0	1.3	5.3		M.:	3.3	1.3
III I:OHAT												
=	7.17	-		7 7	-	-1	-	11 11	-	0	-	2
-	-	-	^	~	-	-		100	-	=	***	2

TABLE 6 (CONT) Page 37 of 39

FAIRMAY DOSE FARAMETER FACTORS FOR INTERESTING TO CFR PART SO (For Section 2.2.2.b, units in mrem/year per pc1/m3).

TABLE INFARI

CRITICAL	Fully	Fillity	LOBER	Philips	Lalley	Pully	Filler	Linky	Fills	Filling	Little	Link	Hillir	I district	Junit.	Lilly	Pollin.	MILLY	Julio !	Filling.	LIIIIY	Littley	111111	Links	Billit	MINITA	Lunx	HOLY	Bulliy	Filler	Piliting.	Politics.	Link	Lillity	POLY
CKI	3	2	3	3	n.	=	ż	3	i	3	:	i	3	3	3	i	3	=	=	3	i	i	=	i	i	3	i	ż	3	i	i	;	3	i	ż
	10	10	10-	19	10-	10	10	10	0	0	10	10	10	10	3	0	10	10	0	10	0	10	10	10	10	10	10	10	50	01	10	10	0	10-	10
ENER	0.000E				0.000E					0.000E	6.00GE	0.000E	0.000t	0.000E	4000 O	0.000E	3000.0	0.000E	C. 660E	0.000	0.000E	3000.0	0.000E	3000 °	0.000E	0.000E		\$.000E	0.000E	0.00GE	0.000E	0.000E		3000.0	3000E
	10	10	0	10	10	10	10	10	-	7	70	70	10	10	10	70	7	10	10	10	10	1)1	10	10	10	10	10	10	10	10	10	10	10	10	10
01-111	0.000	- 19			0.000E				3000.0	0.00cl	D. Sent	6.00ut	6.0.04	1000.0	0.000	D.00.0		0.000£	0.0000	O. COCE	0.0001	0.000	0.0001	1000.0	0.00vt	0.00 d	0.63W	10000.0	10000.0		0.000		0.00GE	3000.0	9.000E
	10	0.1	10	10	10	10	0.1	10	10	5	10	0	3	10	10	10	70	10	10	10	10	10	10	10	10	10	10	0	10	10	10	10	10.	10	10
DMI11	0.000			0.000E						6.000£	0.00GE	0.030E	3000.0	0.000E	\$000.9	0.000		3.0001	0.0001	C.000E	0.000E	0.000E	0.00CE	6.00GE	0.000E	0.000E	9.000E	6.00at	0.000€	0.000E	0.0001	0.000E	0.000E	0.000E	0.000E
_	10	10	10	0	10	10	10	10	0	10	10	0	10	0	10	10	0	0	.0	10	0	10	10	10	3	3		0	10	0	10	10	0	10	10
KIMEY	0.06GE	3.600E		O.COUE	0.000E	0.000E	0.00GE	0.000E		0.000E	O.tuGE	0.000E	9000.0	O.COOF	0.00uE	0.00CE	3000 O	0.000E	0.000E	0.09CE	0.000E	9000.0	0.000E	0.000E	3000°C	0.000	0.000	1000.0	0.00CE	0.000E	0.000E	0.000E	0.300E	10000.0	0.000E
	10	10	10	10	10	10	10	10	10	10	10	10	7	10	0	10	10	0	0.1	10	10	0.1	10	0	16	0	0.0	10	10	5	10	10	10	10	10
LIVER	0.000	0.000E	0.000E	- **			0.000	0.00.0k		-3000° 0	-3000°0		10000.0	3000 · 0		0.000E		0.000E	0.900E		3000.0			0.000E	3000°0	10000.0	0.000E	0.000E	. 3000 . 0	0.000E	0.000	0.00GE	.3000 ° 0		0.000E
	10	10	10	10	10	10	10	10	10	10	10	7	10	10	10	10	10	10	00	10	10	10	10	10	10	5	10	10	10	10	10	10	10	10	10
BUNE		-3000 · 0				-300C.0	. *			0,000E		3000.0	145	0.000E		0.000E	0.000E-	0.000E	*		0.000E					*	0.000E	0.000k	0.000E		0.000E	3000 . O			0.000
-	10	10	0.1	10	10	10	10	10	10	5	10	10	10	10	10	7	10	10	7	10	01	ě	10	10	63	10	10	70	-	0	10	0.1	10	10	10
THYKOID	*			0.000E-		0.000E	9.000E	3.000E		3000.0	*	0.000E	1000.0		3000.0	0.000E	0.0000	0.000	*	4000.0		J000 ' 0		0.000E	3000.0	*	3000 · 5	3.000		0,00GE		0.000E		0.0001	0.000E
>	10	10	0.1	10	10	10	0.1	10	10	7	70	10	10	10	10	0	10	0	10	3	91	0	10	01	0	7	10	10	0	01	10	70	10	63	0
u. bully	0.000	3000.0	0.00GE	3000.0	10:0:0	0.00ct	0.000F	10000.0	0.00ct	0.000L	1000.0	9.000t	0.000	0.000F	0.0001	0.000F	0.00CE	0.000E	0.000F	0.000E	0.000F	1000.0	0.0000	9000.0	0.000r	0.000	0.6.)OF	0.0004	6.00ol	0.0001	0.0001	6.0004	0.000E	O. OOOE	0.0005
NO HOUSE		-14	17.74	177	1-45	10 3	11 54	_	E 25		97: 0	07 0	57	1.3	57 11	17 11	9:7 11	67 11	K 0.3	11 111	K 055	11 115	1111	411	F 113	24 3	16 M	к 72	22	2111	7.1	9.5	9.3	K 955	K 97
-	=	2	T	-	4	7	1 1	is in	7 1	- 0	-	200	7	=	= ::	7						2 0				7 1:14		3 ER	× 6	7 0	-	*	1 2 X	-	.7
2					-	-				-	-		-	-	-	-	-	-	-	**	-1	*:	-1	71	.1	51	71	*1	*	-	-	-	**	**	**

TABLE 6 (CONT)

					-	(For S	ect	Section 2.	2.2	4	unite in	93	in mrem/year	m/y		-	per C1/m3)					
3	-11	AGE THEAN	DE TAT	NOT																		
1	3	TENTONE	ż	BOBY	>	CHANNELL	2	DOME		2	LIVER		F. FORE Y	_	LIING		01-11	-	BAIN		CE	CRITICA
77		66	0.00	9- 30	9.1	0.000E	0	D. 000E	10	0.0	9000	10	0.000E	10	0.000	10	0.000E	-01	0.000€	1	3	100
17	Ė	1.6	0.00	7	-	0.00m					3000	10		10		10		01	0.000E	0	2	201
313			00.00		-		10		1		BOOOE	0.	3000.0	0		10	0.0001	T		10	3	FUIL
35			6,90	T	10		E		10		OUGE	10	0.000E	10		10	0.0001	0	9.000E	1	3	197
40			6.00	- 1	-	10	3	0.00SE	1	0.0	ODOE-	10	0.00CE	10	0.000E	10	1000.0	0.1	3000.0	. 1	3	104
7			0.66	7	-	30000.6	0.8			0.0	3000	10	0.000E	10	0.000t	10	0.00vl	10		1	3	Pini
=		105	0.00			\$000 . 0		B.000E	2		3000	10	30000.0	10	3000'0	10	0.0001	5	C 000E	0	i	104
1.5	2	104	6.30	Ŧ.	-	0.000E	B	0.000E	10-	0.0	3000	7	0.0001	10	0.000E	10	0.0001	70	3000 ·	1	i	PHILIP
-	:	11011	0.60		-	8.300E	T	D.000E	0	9.9	3000	10	30:00.0	0	0.000E	10	0.0001	0	0.000E	10	3	FLIB
-	4	11:14	0.63	T	10	\$.000F	0	0.000E	7.		3000	7	0.000E	10	3000.0	10-	0.0001	7	0.000E	1	ż	=
-1	3	134	0.03	Т		0.000E	7	3000.0	T	0.0	3000	10	3000.0	10	3000.0	18	0.0001	7	0.000E	*	3	1.00
2	-	Harry I	0.00	7	_	0.000	0.1	0.000E	1	0.0	3000	10	0.000E-	10	9000.0	0.	1.00.0	10-	0.000E	- 1	3	107
=	=	13.78	0.00		-	B. Gabe	0	O. ODOE		0.0	BOOK	0	3000'0	0	0.000E	0.0	0.00ct	10	0.060E	10	3	FUE
4.5	=		0.00	T	10	Q 2000	E	*	0.4		3000	7	TOOC.	0		10	0.000t	70	9000 · 0	19-	3	=======================================
07	**	11351	00.00		*	3,000,6	×	4,0064	+		3000	10	0.000E	10	0.000E	10	0.0004	17	0.000E	1	3	Pull
7:	=	67.7	0.00			0.000k	10	9.0006	F		DOOF	10	3007 O	77	0.000E	10	0.000	10	0.000E	1	i	bill
00	=	13111	0.00		**	D. Guist	30	0.0000			3000	10		0	0.000E	10	0.0000	10	0.000	4	i	=
77	-	131	00.00	7	9.0	0.00oc	D	*	10		3000	7	*	10	0.000E	10	0.0001	00	3000 t	3	i	=
7	=	132	09.0	T	-	*	Ž.	6.00JE	D	0.0	TOOO	10		10	0.000E	0	0.00ol	-	0.000	10	=	=
3	-	130	0,00	F			T	0.0000	0	0.0	1000	10	0.000	0.1		70	1000.0	7	0.00ck	10	3	=
1	-	111	0.00		-	9.00th	7	9.000E	T.	*	3000	3		10	0.000E	0	D. Ourif	7	10000.0	0	i	1:43
1:	-	1.4.1	0.00	-	-	D. auck	5	0.0000	T.		DOOE	10		0	0.0001	0	0.0001	-0		10	3	1131
7	-	1.1.1	00.00	*	_	3000 °C	0	0.000	1	0.	1009	5	*	10	0.000E	0		0	0.000F	10	i	=
-	-	14	6.00		-	0.00.0g	0	0.000	1		Sono	0	0.000	10	0.000	0	0.0001	2	9000 · 9	3	=	1111
00	_	1474	0.00	77	-	0.000	Z.	W.	-	*	1000	70		5	0.6901	0	O. tring	=	0.0001	10	ż	F138
-	1	111	0.00		30	0.000F	1				1000	10		10	9.000E	10	0.00nt	-	0.00JE	0	3	1111
0.	1	1.55	00.0		0.0	6.000E	0	0.0001	T.	0.0	Deof	0	1000.0	10	0.000	0.1	0.0001	10	0.000	10-	ż	1
45.47	-	1.1.1	0.05	7	10	1000.0	0	0.0000	0	9	COOK	0	0.000t	0	0.000	0.1	0.0000	0	0.030E	10-	ż	101
-:	-	1.10	0.00		440	10000.0		*	0.1	*	3000	10	1000.0	0	0.000	10	0.000E	0	9000.0	10	i	=
****	-	1.59	0.03		_		0		T.		1000	10		10	0.000E	0	*	0	0.000€	0	3	3
*1.00		1.47	0.00		_		0		J.	180	1000	0.1		0	0.0001	0		5	C.000E	10	3	=
***		140	0.0			0.000	0		0	*	3000	ē	0.coor	10	0.000F	0.8		10	\$000°0	0	ż	3
			0.00		60	Je00.0	3	0.000€			1000	7	*	3	3000.0	Ģ		0	0.000E	0.3	ż	E ST
*	11.1	77.	6.0001			1000.0	T.	JC00'0	10		1000	10	10000.0	10		10		70	0.000	10	=	Dill.
?	-	1 10	0.00		70	0.00CE	0	0.000E	1	0.0	1000	10	10000.0	0	0.000E	10	0.0001	10	0.000	0	i	2411

t disciplination of the contraction of the contract

TABLE 6 (CONT)

Puge 39 of 39

(For Section 2.2.2.b, units in mrem/year per 1101/m3).

GAL I DIFABILITATION

=	*	,,	2.5	*	3.5	>	11	,,	*		*	,
RITICAL	3	50	10.1	=======================================	7	FOI	=	=	FE	Bell	Dill	100
CRI	3	i	i	i	=	ż	ż	:	i	=	3	i
	0	10	10	10	10	10	10	10-	10	10	10	10
BKIN	300	300	-300	300	00E	SOF	BOO	300	-300	SOF	JUE	COL
EN	0.0	0.0	0.0	0.0	0.0	0.000E	0.0	0.0	0.0	0.0	0.0	0.0
	3	3	03	-	70	3	0	-	3	50	0	-
111 18	300	100	COL	100	130	100	100	. Hear	1.0	Ju.	COME	JOE
3	0.0	0.0	0.0	0.0	0.0	0.0001	0.0	0.0	0.0	0.0	0.0	0.0
	10	3	-	-	10	10	-	10	10	10	10	0
111110	OOE	100	OOF	300	Out	300	OCL	SOF	DOL	OOL	400	300
3	0.0	0.0	0.0	0.0	0.0	- 3000 O	0.0	0.0	0.0	0.0	0.0	0.0
	3	a	0	0	9	0	-	ā	-	0	0	0
KIDNEY	100	300	100	300	00E	300	DOE	100	OCE	170	300	300
7	0.0	0.0	0.0	0.0	0.0	0.000E	0.0	0.0	0.0	0.0	0.0	0.0
	0	10	-	10		10	10	10	10	10	10	0
LIVER	DOE	- 300	- 30C	-300	DOE	300	300	DOE	300	390	-300	9.9E
-	0.0	0.0	0.0	0.0	0.0	0.0006.01	0.0	0.0	0.0	0.0	0.0	0.0
	10	50	10	10	10	10	10	10	-	-	10	-
¥	300	300	300	SOF	300	300	DOE	300	300	300	COF	300
DONE	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	0	10	10	10	01	-01 0.000E-	10	0	70	10	0	10
HYKOIB	100	OOF	300	OOF	SOO	3000.0	OOL	HOOF	100	SOLE	300	300
Ξ	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
*	0	0	0	10	0	10	0	0	10	3	10	0
MINE	100	700	SOF	OOF	OOF	1000	\$00	Ditte.	DOF	OOK	OOF.	100
ż	0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.001051 00	1.43	-	-	1 1 1	141	111	-	1112	187	12	1 5:1	2.59
150	=	=	-	3	=	=	Ē	=	=	=	=	=
=	-	77	7.5	1.	27	7.	7.7	=,	5%	611		

TABLE 7

CONTROLLING RECEPTORS, LOCATIONS, PATHWAYS, AND ATMOSPHERIC DISPERSION PARAMETERS

Sector	Distance (meters)	Pachways	Age Group	X/Q _I	D/Q
1*	870	Inhalaction	Infant	3.76E-07	8.09E-09
ME	900	Vegetation	Infant	1.19E-06	1.39E-08
E**	900	Inhalation	Child	1.26E-06	1.58E-08
NE	-		-		
**	-	-			
ESE**	-	******	******		
E***	8000	Cow/Milk	Infant	3.43E-08	1.45E-10
SSE	2680	Vegetation	Child	7.38E-08	9.13E-10
5	1990	Vegetation	Child	7.66E-08	1.29E-09
SSW	1000	Vegetation	Child	1.92E-07	4.18E-09
W	990	Vegetation	Child	3.10E-07	5.642-09
VSW	4250	Cow/Milk	Infant	5.74E-08	5.36E-10
a .	980	Vegetation	Child	6.21E-07	9.582-09
AUG W	2500	Vegetation	Child	8.582-08	8.51E-10
WE	1160	Vegeration	Child	2.29E-07	1.97E-09
MMW	1250	Vegetation	Child	2.51E-07	1.79E-09

^{*}Default value, no vegetable gardens within five miles.

^{**}These sectors are located over Lake Erie, so no ingestion pathways are present.

^{***}Default value, no real receptors within five miles.

TABLE 8

Page 1 of 2

SAMPLING LOCATIONS, DAVIS-BESSE NUCLEAR POWER STATION

Code	Appendix A Page Reference	Type of Location *	Location
T-L	A-16	ī	Sire boundary, 0.96 km NE of station, near intake canal.
T-2	A-17	r	Site boundary, 1.44 km E of Station.
T-3	A-18	I	Site boundary, 2.24 km ESE of station, near Toussaint River and storm drain.
T-4	A-19	I	Site boundary, 1.28 km S of station, near Locust Point and Toussaint River.
T-5	A-20	I .	Main entrance to size, 0.30 km W of station.
T-7	A-21	I	Sand Beach, 1.44 km NNW of site.
8-T	A-22	I	Earl Moore Farm, 4.32 km WSW of site.
T-9	A-23	C	Cak Harbor, 10.9 km SSW of site.
T-11	A-24	c	Port Clinton, 18.4 km SE of site.
T-12	A-25	c	Toledo, 37.6 km WNW of site (water samples are taken from an intake located 17.6 km NNW of site).
T-17	A-26	I	Irv Fick's well on site, 1.12 km SW of station.
T-20	A-27	C	Carl Gaeth, 12639 W. Toussaint E Road, 7.20 km WSW of size.
T-24	A-28, A-29	c	Sandusky, 39.3 km SE of site.
T-25	A-30	I	Miller Farm, 5.92 km S of size.
T-27	A-31	C	Magee Marsh, 8.48 km WNW of size.
T-28	A-32	I	Unit 1 treated and untreated water supply, onsite.
T-33	A-33	I	Lake Erie, within a 8.0 km radius of site.
T-35	A-34	C	Lake Erie, greater than 16.0 km radius of site.
T-37	A-35	C	Fruit stand, 19.2 km SW of station (or the farm 16 to 30 km from the site in the least prevalent wind direction).
T-38	A-36	I	Site boundary 0.96 km ENE of station near lake.
T-40	A-37	I	Site boundary 1.12 km SE of station near ditch to Toussaint.
T-41	A-38	r	Site boundary 0.96 km SSE of station near ditch to Toussaint.

^{*} I=Indicator locations; C=Control Locations

TABLE 8 (continued) Page 2 of 2

SAMPLING LOCATIONS, DAVIS-BESSE NUCLEAR POWER STATION

Code	Appendix A Page Reference	Type of Location *	Location
T-42	A-39	I	Site boundary 1.28 km SSW of station by ECC.
T-43	A-40	I	Site boundary 0.80 km SW of station along Rouse 2 fence.
T-44	A-41	r	Site boundary 0.80 km WSW of station by railroad tracks.
T-45	A-42	I	Site boundary 0.30 km WNW of station on access road behind Cooling Tower.
T-46	A-43	r	Site boundary 0.80 km NW of station along - access road.
T-47	A-44	ī	Sice boundary 0.80 km N of station along access road by gate.
T-48	A-45	I	Site boundary 0.80 km NNE of station along access road by lake.
T-50	A-46	I	Erie Industrial Park 7.20 km SE of station by Water Tower.
T-51	A-47	I	Daup Farm, 600 Terrau Road, Fort Clincon, Ohio 8.80 km SSE of the station.
T-52	A-48	ı ı	Miller Farm 5.92 km S of size on West Camp Perry Road W.
T-54	A-49	ı	M. Beier Farm 7.68 km SW of site on Genzman Road.
T-55	A-50	τ	King Farms 8.0 km W of site on Route 2.

^{*} I=Indicator location; C=Control locations.

Page 1 of 2

Type and Frequency of Sample Collection Environmental Madiation Monitoring Program

Location	Type	Weckly	Monthly	Quarterly	Semi-annually	Annually
-	-	AP AI		TLD		
7	-	AP AI		TID		
	-	AP AI SWII		TLD		
4	-	AP AT SWU ^a		TLD		
5	-			TI.D		
1	-			TLD		
20	-		HP GI.V	TLD		
6	3	AP AI		TLD		
=	3			TLD		
12	9	AP AI SWIIA SWF		пр		
11	-			3		
20	-		a			
24	9			TLD		
25	-		GI.V ^d			
23	9			TLD	88.2	
28	-	SWr				
11	-					
15	9					
33	9		GLV ^d			
38	-			TLD		
40	-			TLD		
***				TLD		

(Continued on next page)



Table 9, continued

Page 2 of 2

Type and Frequency of Semple Collection Environmental Radiation Monitoring Program (Continued)

Annual 1	Semi-unmaily	Quarterly	Honthly	Weekly	Type	Locat Ion
		TLD			ı í	42
		T1.0			1	43
		TLD			1	44
		TLD			1	45
		TLD			1	46
		TLD			1	47
		TI.D			1	48
		TI.D			1	50
		TLD			1	51
		TLD			1	52
		T1.D		1.4274	1	54
		TLD		A CONTRACTOR	1	55

[&]quot;Composite sample over 1-week period

Semi-monthly when animals are on pasture (May-October), monthly at other times

Sommer months

Monthly when available (July, August, September)

Table 10 Sample Collection Codes

Code	Description
AP	Airborne Particulates
AI	Airborne Iodine
πο	Thermoluminescent Dosimeter
м	Mf1k
WW	Well Water (Ground Water)
GLV	Green Leafy Vegetables
TWZ	Surface Water - Treated
SWU	Surface Water - Untreated
F	Fish
85	Bottom Sediments

OFFSITE DOSE CALCULATION MANUAL

APPENDIX J

JUSTIFICATIONS

Safety Evaluation for the Davis-Besse Radiological Effluent Technical Specifications Amendment

Overview

Revisions to the Davis-Besse Appendix A and Appendix B Technical Specifications are proposed which will implement the regulatory requirement of 10 CFR 50, Appendix I on ALARA for radioactive effluents and other NRC regulations and criteria on radioactive material monitoring instrumentation, radioactive material control, and radiological environmental monitoring. In keeping with NRC guidelines, all radiological requirements are being deleted from Appendix B and placed in Appendix A.

This proposed amendment is a revision to a previously submitted amendment to the NRC dated March 16, 1979 (Serial No. 488).

The major areas that are addressed in the revised submittal are as follows:

- Liquid and gaseous effluent monitoring instrumentation--operation and periodic operability checks;
- Liquid and gaseous radioactive material releases--maximum release rates, quarterly does limits and yearly dose limits;
- Sampling and analysis requirements on batch and continuous radioactive material releases;
- Operation requirements on the liquid radwaste treatment system;
- Curie inventory limit on outside temporary liquid storage tanks;
- Maximum allowable oxygen concentration in the waste gas system;

- Requirements to assure all solid waste meets applicable burial site requirements;
- Radiological environmental monitoring program--minor revisions to reflect current program and current NRC guidelines.

Changes have also been made to Section 6 of Appendix A to reflect the applicable administrative controls needed for the Section 3/4 revisions.

A notable addition to the amendment is the inclusion of a requirement for an Off-site Dose Calculation Manual (ODCM) and a Process Control Program (PCP). The ODCM and PCP are not licensed documents but are referenced in the Technical Specification as presenting acceptable methods for evaluating compliance with applicable Technical Specification requirements. The ODCM provides calculational methods for determining radioactive effluent instrumentation alarm setpoints, and for evaluating releases of radioactive effluents and corresponding doses. The ODCM also includes the sampling locations for the environmental monitoring program. The PCP presents the methods used to verify that waste (dewatered resins) as processed for disposal meets appropriate shipping and burial ground regulations. Changes may be made to these documents without NRC approval; review by the SRB is required.

Safety Evaluation

An evaluation of the revised amendment has been performed to assure that the revisions as proposed do not involve an unreviewed safety question as defined in 10 CFR 50.59. The three criteria of 10 CFR 50.59 for the unreviewed safety question determination are addressed below.

i) Probability of occurrence or the consequences of an accident or malfunction of equipment important to safety previously evaluated in the safety analysis report. Except for the addition of the turbine building liquid effluent radiation monitor (for which an FCR has already been initiated), no plant equipment modifications are required by the proposed amendment. Certain procedural requirements will need to be developed but these address routine radioactive material effluents and controls; no accident procedures are involved.

ii) Probability for accident or malfunction of a different type than any evaluated previously in the SAR may be created.

For reasons as stated in response to item (i) above, the proposed amendment does not directly or indirectly pose a probability for an accident or
malfunction. The amendment will implement the NRC regulations for routine
releases and controls of radioactive material. The amendment does not
address any engineered safety features of the plant design.

(iii) Margin of safety as defined in the basis for any technical specification is reduced.

The proposed amendment does not reduce the margin of safety. The proposed amendment addresses routine releases and control of radioactive material; except as noted in item (i), no plant modifications are involved. Several operating procedure changes may be needed, but these changes will be only for routine operations and will have no impact on accident probability or consequences.

For the reasons discussed above for each of the criteria of 10 CFR 50.59, it is concluded that the amendment as proposed does not involve an unreviewed safety question.

Service Water System -- Radiological Effluent Monitoring Requirements

The service water system is classified as a non-radioactive system, being removed from radioactive systems by two boundaries. Radioactive systems are serviced by the component cooling water system interface; and, the service water system provides cooling to the component cooling water system through closed loop heat exchangers. Therefore, any leaks from radioactive systems into the plant water systems would first be identified by the monitoring of the component cooling water system prior to any additional unexpected leakage into the service water system. As a prudent measure, the service water system is monitored in accordance with the NRC guidance of Standard Review Plan, Section 11.5. However, because this system is a non-radioactive system and is separated from radioactive systems through two closed-loop boundaries, no Technical Specification requirements are needed for routine monitoring and analysis for radioactive effluents.

Radioactive Effluent Instrumentation -- Automatic Isolation Feature

The radioactive effluent monitoring instrumentation at Davis-Besse does not include provisions as called for in the NRC Standard Radiological Effluent Technical Specifications for automatic isolation should any of the following conditions exist: circuit failure, downscale failure, or instrument not set in operate mode. Even though the automatic isolation features do not exist, administrative controls have been established such that should any of these conditions exist the control of radioactive effluents would not be significantly impacted. Essentially all releases of liquid radwaste are controlled as individual batch releases with predetermined allowable release conditions. Thereby the radiation monitor serves mainly as a back-up; primary control is established by the prerelease radiological analyses and evaluations. To assure the availability of the back-up monitoring, the status of the instruments is checked once per shift by the control room operators. Indicator lights on the instrument panel are checked to verify operability. An indicator would illuminate should a failure occur such as the ones delineated above. Therefore, in addition to the administrative controls on allowable releases, the verification of instrument operability prior to releases of radioactive effluents and the "once per shift" status check by the control room operators provides adequate assurance of the proper control of the radioactive effluents.

Technical Bases for Eliminating Curie Inventory Limit for Gaseous Waste Decay Tanks

The NRC Standard Technical Specifications include a limit for the amount of radioactivity that can be stored in a single waste gas decay tank. This curie inventory limit is established to assure that in the event of a tank failure releasing the radioactive content to the environment the resulting total body dose at the site boundary would not exceed 0.5 rem. For Davis-Besse the inventory limit in the waste gas storage tank has been determined to be approximately 45,000 curies (Xe-133, equivalent).

An allowable primary coolant radioactivity concentration is established by the Technical Specifications which limit the primary coolant radioactivity concentrations to 100/E with E being the average energy of the radioactivity in Mev. This equation yields an upper primary coolant gross activity limit of about $200~\mu\text{Ci/ml}$. By applying this activity concentration limit to the total liquid volume of the primary system, a total activity limit can be determined. For Davis-Besse the primary system volume is about 56,000~gallons, which yields a limiting total inventory of approximately 41,000~Ci.

By assuming a typical radionuclide distribution an equivalent Xe-133 inventory can be determined. Table 1 provides the typical radionuclide (noble gases) distribution and the Xe-133 equivalent concentration. The equivalent concentration is determined by multiplying the radionuclide concentration by the ratio of the nuclide total body dose factor to the Xe-133 total body dose factor. Summing all the individual radionuclide equivalent concentrations provides the overall Xe-133 equivalent concentration. For determining concentration in a waste gas decay tank, a conservative assumption of 48 hours decay in degassing the primary system has been used to correct the primary coolant concentrations. The data show that the equivalent concentration (decay corrected) is less than the gross concentration (i.e., $16~\mu\text{Ci/gm}$ total in primary coolant versus $12~\mu\text{Ci/gm}$ equivalent). The resulting Xe-133 equivalent curie inventory for WGDT input is approximately 31,000 Ci.

Therefore, even if the total primary system at the maximum Tech Spec allowable concentration was degassed to a single waste gas decay tank, the tank curie inventory would be well below the 45,000 Ci limit. Based on this evaluation, the curie inventory limit on a single waste gas storage tank has not been included as a Technical Specification requirement.

Table 1

Xe-133 Effective Concentration

	Primary* Coolant (µCi/GM)	Half-life	Concentration @ 48 hr decay (µCi/ml)	Reg Guide 1.109 TB Dose Factor mrem/yr pCi/m ³	Ratio TB DF Xe-133 DF	Xe-133 Effective Conc @ 48 hr decay (µCi/ml)
Kr-83M	2.0-02	1.9 hr		7.6x10 ⁻⁸		
Kr-85M	1.1-01	4.5 hr		1.2x10 ⁻³	4.1	
Kr-85	7.4-02	10.7 yr	7.4x10 ⁻²	1.6x10 ⁻⁵	0.06	4.4x10 ⁻³
Kr-87	5.8-02	76.3 min		5.2x10 ⁻³	20.	
Kr-88	1.9-01	2.84 hr		1.5x10 ⁻²	52.	
Kr-89	4.8-03	3.16 min		1.7x10 ⁻²	57.	
Xe-131M	8.4-02	12 days	7.5x10 ⁻²	9.2x10 ⁻⁵	0.32	2.4x10 ⁻²
133M	2.0-01	2.2 days	1.1x10 ⁻¹	2.5x10 ⁻⁴	0.86	9.5x10 ⁻²
Xe-133	1.5+01	5.3 days	1.2x10 ⁺¹	2.9x10-4	1.0	1.2x10 ⁺¹
Xe-135M	1.3-02	16 min		3.1x10 ⁻³	11.	
Xe-135	3.3-01	9.1 hr	8.5x10 ⁻³	1.8x10 ⁻³	6.2	5.3x10 ⁻²
Xe-137	8.7-03	4 min		1.4x10 ⁻³	4.8	
Xe-138	4.3-02	17 min	-	8.8x10 ⁻³	30	
Total	1.6x10 ⁺¹		1.2x10 ⁺¹			1.2x10 ⁺¹

^{*}Adapted from Dav's-Besse Evaluation of Compliance with Appendix I to 10 CFR 50, June 4, 1976.

Lower Limit of Detection--Decay Correction Factor

The equation and definition of the lower limit of detection in the NRC Standard Radiological Effluent Technical Specification include the term $e^{-\lambda t}$ which is used to decay correct the analysis. The LLD is further defined as an <u>a priori</u> (before the fact) limit representing the capabilities of a measurement system and not an <u>a posteriori</u> (after the fact) limit for a particular measurement.

Providing a decay correction for an evaluation of the capabilities of a system does not appear appropriate. It may be appropriate to decay correct certain analyses of specific samples to determine radionuclide concentrations at the time of release. Even in this case, such a correction is not appropriate for batch releases. Analyses are performed prior to any release; and, the sample will be decaying at the same rate as the batch from which the sample was taken. For continuous releases, decay correcting analyses of samples obtained over a specified sampling interval must take into account the accumulation of radioactivity in the sampling medium, the decay during the sampling interval and, especially for short lived radionuclides, equilibrium or quasi-equilibrium conditions that may be achieved.

Short-lived radionuclides will tend to reach an equilibrium value in the sampling medium as a function of source input and half-life. A single decay correction to adjust for sampling interval will provide an unacceptable overestimate. Equilibrium concentrations must be considered if analyses are to be indicative of actual release quantities.

Employing $\exp(-\lambda \Delta t)$ to adjust for radioactive decay between the end of sampling and the time of analysis is straightforward. However, to attempt to use the same term to adjust for decay during the sampling period is not proper. As a practical matter, when the half-life of a radionuclide is long relative to the sampling time and the time between sampling and analysis, i.e., minimal decay, the correction term will be near unity. In that event, the correction term is relatively unimportant.

At the other extreme, when the half-life of a radionuclide is much shorter than the sampling time or the time between the end of sampling and the analysis, the term $\exp(-\lambda \Delta t)$ could be used to adjust for decay between the end of sampling and the analysis. However, it would not be appropriate in that case to use the same term to attempt to adjust for decay during sampling.

The relationship between the radioactivity in a sample at the end of sampling and the activity concentration in the medium being sampled is somewhat more involved. To explain this in the simplest condition, assume the radionuclide concentration is constant in the medium being sampled and that the medium is sampled at a constant rate.

In the instance of water sampling, the relationship between the activity concentration in the water being sampled and the activity concentration in the water sample at the end of sampling is:

$$C_1 = C_2 \frac{\lambda t}{1 - e^{-\lambda t}} \tag{2}$$

where

C1 = radionuclide concentration in the water being sampled

C₂ = radionuclide concentration in the water sample at the end of sampling

t = duration of sampling

λ = radionuclide decay constant

when $\lambda t >> 1$, $C_1 = C_2 \lambda t$

In the separate case of sampling a radionuclide in air by filtering the air and analyzing radioactive material collected on the filter, the radionuclide of interest is concentrated. Absent diluent air in the sample being analyzed, the relation between radioactivity on the sample media and radionuclide concentration in the air being sampled is:

$$C_1 = C \frac{\lambda t}{F(1 - e^{-\lambda t})}$$
 (2)

where

C1 = radionuclide concentration in the air being sampled

q = radioactivity on the sample media (assuming 100% collection efficiency)

F = sampler flow rate (volume/time)

λ = radionuclide decay constant

t = duration of sampling

when λ t >> 1, C_1 q λ/F .

This merely recognizes that the rate of loss from the filter by radioactive decay equals the rate of collection onto the filter at equilibrium.

The NRC proposed equation appears to incorporate an adulterated way of encouraging analysis soon after the end of sampling and to encourage efficient sample concentration or radiochemical extraction. Although not rigorous, it combines both objectives in a simple and thus practical way, provided the decay correction is not extrapolated to a time earlier than the end of sampling.

A more nearly rigorous way of determining the activity concentration (or minimum detectable activity) in the medium being sampled is to assess the LLD in the sample at the time of analysis. Then the activity concentration in the medium being sampled can be calculated with the product of $\exp(-\lambda \Delta t)$ for decay between the end of sampling and the analysis and one of the equations derived herein for the relation between the medium being sampled and the activity in the sample at the end of sampling.

However, this method is not very practical or necessary considering the types of sampling and analysis at nuclear power plants, the significant radionuclides, and the offsite potential doses. The bulk of the radioactivity is released as batch releases with all sampling and analysis performed prior to release. Therefore, no decay corrections are applicable. It is in the sampling and analysis of continuous releases that the accumulation and decay of the radioactive material may need to be considered. The use of NRC's guidance for decay correction to the mid-point of the sampling period can grossly overestimate actual release qualities of short-lived radionuclides, while providing little improvement for the

quantification of the longer half-life radionuclides that are the major dose contributors.

Overall, it may be appropriate to decay correct certain analysis to account for radionuclide decay during the sampling period. However, simple decay correction to the mid-point of sampling will grossly overestimate any short-lived radionuclides that may be detected. More consideration needs to be given by the NRC to address this problem. In any case, the use of a decay correction factor in defining a lower limit of detection is inappropriate. The LLD is a measurement of the capability of the measurement system and should not be used to try to establish a regulatory position on sampling and decay correction for quantification of releases.

At Davis-Besse, the operation of the waste gas decay system is essentially continuous, similar to the routine operation of such a system at other PWRs. The system consists of a surge tank which receives the waste gases from the primary system, dual compressors (one in-service and the other in reserve), and three waste gas hold-up tanks (one in-service, one isolated for gas decay, and the third in reserve). Once the system is on-line with a waste gas decay tank receiving primary system gases for the surge tank, operation is automatic; no operator actions are required.

The operating philosophy at Davis-Besse is to essentially operate the waste gas system continuously. Not only is this philosophy prudent from an ALARA standpoint, but it is also conservative and protective from an operational standpoint. Having to periodically evaluate primary system off-gas activity levels and anticipate unexpected increases in radioactivity would be an unnecessary burden in determining needed waste gas system operation.

For the ventilation systems, the operating philosophy is similar to that for the waste gas system; operation is continuous. But for the ventilation systems, the reasons for continuous operation are even more straightforward. Areas within the plant must be provided with outside air in order to provide an inside environment suitable for continued occupancy. Without continuous ventilation system operation, heat, humidity, and airborne radioactive material levels would increase and worker occupancy would be jeopardized.

As described in the Davis-Besse Appendix I evaluation, the ventilation systems contain HEPA filters for removal of airborne radioactive particulate material prior to release to the outside environment. (As evaluated for Appendix I compliance, only the waste gas vent includes charcoal filters for removal of radioiodines) The operation of the systems can essentially be considered a passive operation. No active operational

procedures are required for normal system operation for removal of airborne radioactive material.

Davis-Besse's operating philosophy (and operating procedures) for the waste gas system and ventilation systems is a commitment in itself to the routine continuous operation of the systems. Having to commit to such a requirement (in lieu of a technical specification requirement on operation) without appropriate consideration of system down-time and plant shut-down (where operation may not be needed or feasible) is unacceptable and not in keeping with the principles of ALARA. Including special technical specifications that would impose additional procedures and periodic surveillance requirements in excess of those already established (which at present assure appropriate operation) is unnecessary and excessive.

Radiological Effluent Dose Analysis--Meteorology for Short Term Releases

Except for the waste gas decay tank (WGDT) releases and the containment purges releases, gaseous effluents from the Davis-Besse Station are from ventilation systems and are considered continuous releases. Most of the radioactive material in gaseous effluents is released from the WGDT. However, because of the essentially random nature of WGDT releases (i.e., no prescribed diurnal time, frequency or duration), the dose analysis of these releases is better modeled by the use of annual average meteorological conditions rather than short term meteorology. Containment purges are so infrequent that special meteorological analyses are not warranted; reasonable evaluations of off-site doses can be provided by the use of annual average meteorological conditions.

Radiological Environmental Reporting Levels

Only the radionuclides listed in Table 3.12-2 of the proposed Radiological Effluent Technical Specifications for Davis-Besse are considered in the reporting requirements for elevated levels of radioactive material in environmental sampling media. The radionuclides listed are those that are dominant in the plant effluents and contribute essentially all of the environmental dose. Other radionuclides will be present in plant effluents, but their contribution to the calculated total environmental dose will be minor compared to the contribution of the radionuclides listed in Table 3.12-2. Even the contents of the NRC's Standard RETS reflect this position; not all pathways include reporting levels for all the radionuclides listed (e.g., no reporting levels are presented for Co-58, Co-60, or Fe-59 for the milk, airborne particulate, or vegetable pathway). This very selective identification of pathway and important radionuclides reflects the very well defined concept of significant radionuclides for each particular pathway.

Based on past experience in monitoring plant effluents and environmental sampling media, it can be stated with confidence that for the routine operation of Davis-Besse the radionuclides listed in Table 3.12-2 with applicable reporting levels by the identified pathways are the only radionuclides that need be considered when evaluating potential doses in the offsite environment. Also, even if reporting levels were included for other radionuclides, the values would be higher than those for the significant radionuclides and would have a very minor role in determining actual reporting requirements. The reporting levels for the significant radionuclides would be reached well before any identified levels of other radionuclides would even be controlling.

Technical Basis for Eliminating Curie Inventory Limit of Outside Liquid Tanks

At Davis-Besse, outside liquid tanks that potentially contain radioactive material are limited to the borated water storage tanks (2 tanks @ 550,000 gallons) and the primary water storage tank (1 tank, @ 140,000 gallons).

The borated water storage tanks are part of ECCS and are of seismic design. These tanks are designed to withstand extremely adverse environmental conditions and for purposes of this evaluation can be considered rupture-proof. Also, overflow from the tanks is piped back to radwaste. For these reasons, it is considered unnecessary to impose curie inventory limits on these tanks.

The primary water storage tank is used for normal make-up and letdown to the primary system. Water contained within the PW storage tank is typically processed primary coolant or clean (non-radioactive) water. Prior to adding primary system water to the PW storage tank, the water is processed by evaporation and demineralization. This processing limits the levels of radioactivity in the tank. Past sampling and analysis of the tank has indicated only detectable levels of tritium, no other radionuclides have been identified. Also, the overflow on the PW storage tank is piped to radwaste. Therefore, due to the processing of any radioactive waste prior to addition to the PW storage tank and the piping of the overflow to radwaste, the probability of any abnormal discharges to the environment that could exceed the concentrations of 10 CFR 20, Appendix B, Table II, Column 2 at the nearest drinking water supply is extremely remote.

Because of the design of the BWST and the design and operating conditions of the PW storage tank, it is considered unnecessary to impose curie inventory limits on these tanks. Having to routinely sample and analyze for radioactivity concentration imposes an undue burden on plant personnel without providing any additional assurance of the public health and safety.

Sampling Frequency for I-131: Significance of Power Changes and Increases in Coolant Activity Levels

The NRC guidance on effluent monitoring for I-131 (RETS Table 4.11-2, footnote c) calls for increased sampling frequency for I-131 during increases (or decreases) in reactor power level and increases in primary coolant level or noble gas effluent activity level. By system design, releases of radioactive material from plant operation are minor. Trying to identify small increases in I-131 releases that may (or may not) be associated with power changes is unnecessary. To evaluate the potential significance of increases in I-131 releases associated with power changes and the effect that sampling time may have on actual quantification of releases, the following example situation is evaluated.

Consider a power increase (or decrease) on the first day of a seven (7) day sampling period that leads to an increase in I-131 release rate by a factor of 10 for one (1) day. After this one day increase, the release rate returns to the steady-state condition for the remaining 6 days of the sampling period. To evaluate the amount of I-131 on the sampling cartridge as a function of sampling time and concentration, the following equation is used:

$$q_i = \frac{C_i F}{m \lambda_i} (1-e^{-\lambda_i t})$$

where:

Q_i = quantity of activity on collection medium C_i = air concentration of radionuclide i

i = decay constant for radionuclide i

t1 = sample time

m = correction factor for collection efficiency

Assuming 100% collection efficiency, at the end of the one day increase the total amount of activity (I-131) on the collection cartridge is determined to be 9.54 C.F. (For this example, the steady-state I-131 concentration is designated as C, and the one day increase is 10 C...) For the remainder of the sampling period with a concentration equal to C., the I-131 activity on the collection cartridge is equal to 4.66 C.F.

By decaying the activity on the collection cartridge for the one day increase to the end of the sampling period and adding this quantity to 4.66 C.F, the total I-131 activity is determined to be 10.3 C.F.

If this value is decay corrected to the mid-point of the sampling period in accordance with the guidance of Regulatory Guide 1.21, the I-131 activity which is used to determine the release quantity is equal to $14.0 \, \mathrm{C_iF.}$

If a similar analysis is performed for the case of analyzing the collection cartridge at the end of the one day increase and analyzing a new cartridge at the end of 6 days sampling (constituting a 7 day sampling period), the total activity (decay corrected to mid-point of sampling periods) is determined to be 16.0 C.F.

By not analyzing the collection cartridge at the end of the one day increase, the total quantity of I-131 is underestimated by 14%. This analysis represents a somewhat worse case situation. The later into the sampling period that the increase occurs, the less the error. If the increase in release rate occurs after the mid-point of the 7 day sampling period, the actual release will be overestimated.

Over a period of time involving numerous increases and decreases in effluent level, the rules of probability dictate that the overestimations and underestimations will tend to cancel out, providing an overall closer approximation to actual releases.

Both the NRC in-plant measurement program and a study by EPRI* have indicated that minor increases in I-131 releases may be associated with reactor power changes and the iodine spiking phenomenon. However, these studies also indicate that overall such increases are minor, not being a significant contributor to the total releases of I-131. As was concluded by the EPRI study for other PWRs, the main source of I-131 releases at Davis-Besse is associated with containment purges.

Regardless of the source, the total I-131 releases are negligible. Since initial start-up of Davis-Besse, the annual releases of I-131 have been less than 0.06 $\rm C_i$ and calculated maximum individual doses less than 0.01 mrem. Even considering a hypothetical 14% increase for sampling periods that may include iodine spiking in the primary coolant, the effect on

^{*}EPRI NP-939, "Sources of Radioiodine at Pressurized Water Reactors". Science Applications, Inc., November 1978

total releases and calculated doses is still negligible. The actual increase will be even more insignificant considering the fact that the major source of I-131 at Davis-Besse is from containment purges.

Based on a review of plant operating data and the above analysis of the I-131 release quantification as a function of concentration and sampling time, it is concluded that for Davis-Besse, a sampling frequency based on power changes and increases in primary coolant I-131 concentrations is not justified. Determining the releases (and the insignificant environmental doses of these releases) on a weekly basis is sufficient verification of the negligible impact of plant operation. Trying to "fine tune" these releases is not justified considering the manpower and material costs associated with the additional sampling and analysis.

The discharge from the condensate demineralizer backwash receiving tank is controlled on a batch-by-batch basis in lieu of continuous radioactive effluent monitoring. This method of operation has been determined to provide better control over the discharge of the backwash receiving tank, preventing any unanticipated, unevaluated releases of radioactively contaminated secondary-side clean-up resins to the on-site settling basin. Prior to discharge, the contents of the backwash receiving tank are sampled and analyzed for radioactivity. As required, radioactively contaminated resins are transferred to radwaste for processing and disposal as radioactive material.

The condensate demineralizer backwash receiving tank discharge line as originally designed included a radiation monitor. However, because of the nature of the resin-slurry mixture and the accumulation of resin beads in the monitor line, the radiation monitor has failed to provide the reliable indication of radioactivity and control as originally intended. For this reason, it has been determined that the sampling and analysis of each batch prior to discharge is needed to identify and evaluate radioactive contamination resulting from minor steam generator tube leaks (or residual radioactive material from previous leaks) that might otherwise go undetected and unevaluated by a gross radiation effluent monitor.

The condensate demineralizer backwash receiving tank discharges to an on-site settling basin. No resin discharges are made directly to the off-site environment. Therefore, even in the event of personnel error resulting in the inadvertent discharge of unacceptably radioactive, contaminated resins to the settling basin, no off-site releases would occur. All resins and radioactive material would be retained on-site within the settling basin. Appropriate follow-up measures could then be initiated to control the radioactive material and prevent any potential for releases to the off-site environment in excess of the regulatory limits.

Controlling the discharge of the condensate demineralizer backwash receiving tank on a batch-by-batch basis provides adequate control over the releases of any radioactive material to the off-site environment from this pathway. Also, the discharge is to an on-site settling basin, representing an additional passive barrier from release off-site. Even in the unlikely event of personnel error, by discharging to an on-site settling basin and its isolation from the off-site environment, the probability of unwanted, unevaluated releases of radioactive material to the off-site environment is exceedingly remote. Any additional protective measures provided by a continuous radiation monitor (for which operational performance and reliability are unlikely, based on past experience) are not considered needed.

Lower Limit Of Detection

Definition And Application To Detection Capabilities For Ce-144

The lower limit of detection (LLD), as defined in the Radiological Effluent Technical Specifications (RETS) is an "... a priori (before the fact) limit representing the capabilities of a measurement system and not as a posteriori (after the fact) limit for a particular measurement." As defined by this definition applicable to the detection capability for radioactive effluent analysis, the LLD is a statistical analysis of a background spectrum and represents the detection limits for a radionuclide if it is the only radionuclide present above background. LLDs should be determined based on an analysis of a blank (or background) sample.

However, even with this definition and application of LLD, it can be increasingly difficult to achieve a predesignated LLD value for particular radionuclides as the photon abundance (i.e., decay yield) decreases. To address this problem, specific radionuclides have been identified in the RETS as being the principal radionuclides for which the required LLD must be met. For the analysis of samples of liquid radioactive effluents, an LLD of 5 x 10-7 µCi/ml is required. For the principal gamma emitters listed, all have characteristic gammas with energy levels and abundances that provide for sufficient analytical sensitivity yielding LLDs within the required value of 5 x 10-7 µCi/ml - except Ce-144. With a 10.8% abundance and an energy level of 133.5 KeV, being able to meet the LLD of 5 x 10⁻⁷ µCi/ml requires optimum conditions--conditions which cannot be repeatedly achieved for an operational radiochemistry program at Davis-Besse. The low gamma yield is a major factor; however, with an energy level which is located within the Compton continuum, the detection capability for Ce-144 even for a blank, background sample is significantly higher compared with other so-called principal gamma emitters.

The equation for LLD in the Davis-Besse RETS is:

$$LLD = \frac{4.66 \text{ S}_b}{E \cdot V \cdot 2.22 \cdot Y}$$

where:

Sh = the standard deviation of the background counting rate

 $=\sqrt{R/T}$

R = background counting rate

T = counting time

E = counting efficiency

V = sample size

2.22 = conversion factor (transformations per minute per picocurie)

Y = fractional chemical yield (when applicable)

By substitution of typical values in this equation, the LLDs for different principal gamma emitters can be compared. For analysis of a typical background sample at Davis-Besse, the ratio of the LLDs for Ce-144 and Co-60 is about 5.35; for Ce-144 and Mn-54 the ratio is 8.34. These large ratios are demonstrative of some of the relative difficulties in achieving an LLD of 5 x 10^{-7} μ Ci/ml for Ce-144 compared with other principal gamma emitters.

Examining the equation of LLD, two main factors can be altered in an attempt to improve the detection capability - counting time and detector efficiency. (Altering sample size is not considered realistic since larger samples would pose operational and standard calibration problems. It can also be shown that increasing sample volume does not strongly influence efficiency for counting on contact with the detector face due in part to sample self-shielding and decreased relative efficiency for the increased volume).

LLD improves at best as the square root of the counting time. Therefore, increasing the counting time from 2000 seconds to 5000 seconds would only provide a 1.6 reduction in LLD. A 5000 second count is considered to be a reasonable maximum for radioactive effluent analysis. Having to extend to longer counting times would introduce a potential operational delay without commensurate improvement in detection capability.

An improvement in the efficiency can be accomplished by the use of a more efficient GeLi detector. However, this increased efficiency is negated in part by the corresponding increase in background count rate. A comparison of 5 GeLi detectors with relative efficiencies ranging from 7.2% to 22% was performed at the University of Michigan*. For a 500 ml sample on contact with the detectors, the 15% relative efficiency detector demonstrated the highest photopeak efficiency in the 80-200 KeV range. Even the 10% relative efficiency detector had a higher photopeak efficiency in this energy range than did the 21% and 22% relative efficiency detectors. Some unexplainable differences may be due to inherent manufacturer specifications; however, a valid conclusion is that increasing the detector efficiency provides little if any improvement in detection capability, especially in the low energy range (<200 KeV).

Therefore, the analysis of effluent samples at Davis-Besse with a 10% relative efficiency GeLi and a 5000 second counting time provides a detection system that is not only practical for an operational radio-chemistry program but can also be considered as representative of state-of-the-art for routine, general purpose radionuclide detection. Since the required LLD of 5 x $10^{-7} \, \mu \text{Ci/ml}$ can not be met on a routine basis for Ce-144, therefore the LLD for Ce-114 will be 2.0 x $10^{-6} \, \mu \text{Ci/ml}$ (Table 4.11-1, footnote b.).

DBP 4306G

^{*}D. M. Minnema, C. G. Hudson and J. D. Jones. "A Comparison of Ge(Li) Detectors with Different Efficiencies for Low-Level General Purpose Counting"; University of Michigan, 1978.

THE TOLEDO EDISON COMPANY DAVIS-BESSE NUCLEAR POWER STATION PROCESS CONTROL PROGRAM

Revision No.

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SOLID RADIOACTIVE WASTE PROCESS CONTROL PROGRAM

DAVIS-BESSE NUCLEAR POWER STATION

MARCH 1984

DAVIS-BESSE NUCLEAR POWER STATION

Solid Radioactive Waste Process Control Program

I. PURPOSE

The processing of radioactive waste for disposal at a licensed radioactive waste burial site requires that the waste be appropriately analyzed, processed and packaged, representing a final waste form that is acceptable for transportation to and burial at a licensed radioactive waste disposal site. The purpose of this Process Control Program is to document the radioactive waste processing methods and the quality control steps that are taken at Davis-Besse to verify compliance with applicable regulatory requirements and, in particular, to assure an acceptable waste product meeting the applicable waste stability characteristics of 10 CFR 61.56.

This Process Control Program covers all major waste processing streams at Davis-Besse and the resulting final waste products, including:

- Compressible and non-compressible trash;
- Spent aqueous system filter cartridges;
- Spent resins; and
- Use of contractor for waste processing.

II. REGULATORY OVERVIEW

All waste processing, packaging and shipping are conducted in accordance with approved procedures to assure compliance with applicable federal, state and burial site requirements. Waste processed for disposal is evaluated for compliance with:

- 1. The waste classification requirements of 10 CFR 61.55.
- 2. The waste characteristic requirements of 10 CFR 61.56.
- 3. The manifest reporting requirements of 10 CFR 20.311.

Packaging of waste is in containers meeting DOT specifications and is appropriate for the applicable waste class. Shipments are conducted in accordance with the requirements of 49 CFR 172-177 and 10 CFR 71.

All waste processing is performed in a manner consistent with the principles of ALARA. The procedures that have been developed to cover waste processing operations address appropriate radiation safety measures such as job preplanning (REP), radiation source shielding, and job prerequisites and material requirements so as to minimize stay times.

III. SOLID RADWASTE PROCESSING AND PACKAGING

Prior to the placing of any radioactive material in a container for shipment off-site, a visual inspection of the container's general condition and integrity is conducted. Specific items leading to potential container degradation that are examined and could result in rejection for use as a radwaste disposal container include:

- Punctures
- Corrosion
- Cracked, separated, incomplete, or otherwise defective seams and welds
- Bent, dented, cut, or degraded gaskets and/or sealing surfaces

Also, specific criteria prohibit the inclusion of liquid waste (e.g., wet decontamination mop heads, free liquids, and plastic wastes containing liquids) unless special provisions have been made for the removal of the liquids (e.g., for dewatering spent resins).

Compressible and Non-Compressible Waste

Miscellaneous compressible and non-compressible wastes are routinely collected throughout the radiologically controlled areas of the plant for the purposes of general housekeeping and radiological control.

Prior to filling a drum or a box with waste, the container is appropriately labeled, RADIOACTIVE - LSA. The loading of compressible and non-compressible waste is conducted in a manner consistent with the philosophy of volume reduction and minimization of void spacing. After completion of waste compaction and/or container loading, each container is sealed, weighed and placed in radwasts storage, pending shipment to a licensed waste disposal site.

Liquid System Cartridge Filters

Cartridge filters can be a high radiation and/or contamination hazard. All spent filter removals are performed under health physics surveillance. Filters are placed in shielded storage to allow for radioactive material decay prior to placing in an approved, appropriate shipping container (e.g., high integrity container or HIC).

Spent Resin - Primary System

Spent resins from the primary clean-up system are transferred from the Spent Resin Storage Tank to an appropriate disposable container in accordance with approved plant procedures. Normally, transfer is to an HIC; however, a carbon steel container may be used provided radioactive material levels meet the criteria for Class A waste per the requirements of 10 CFR 61.55. After transfer to a disposable container, the container is dewatered

in accordance with vendor-approved procedures that have been specifically developed for the dewatering of resins for the applicable vendor-supplied container. The specifics of the dewatering process must adequately demonstrate the removal of essentially all free standing water (i.e., meeting the free standing liquids requirements of 10 CFR 61.56).

Additional administrative controls taken to assure the proper dewatering of resin utilizing vendor-supplied procedures, are addressed in Section IV.

Spent Resin - Miscellaneous Waste Monitor Tank Influent Processing

The processing of liquid radwaste normally from the miscellaneous waste drain tank or detergent waste drain tank (dirty, aerated liquids) is performed by a contractor-supplied filtration/demineralization system. Refer to Section IV for the administrative and operational controls that are taken to assure the generation of an acceptable waste product.

Spent Resin - Condensate Polishing Demineralizer Holdup Tanks

The processing of resin slurries from the condensate polishing demineralizer holdup tanks is performed by a contractor-supplied system. Refer to Section IV below for the administrative and operational controls that are taken to ensure the generation of an acceptable waste product.

Spent Resin - Potential Exothermic Reactions

Since we are not solidifying at Davis-Besse, exothermic reactions which could potentially occur during the solidification process would not be a consideration. If in the future, a wolidification process is used, an appropriate time will be allowed before solidifying or capping to avoid any pressure extremes in the closed container or matrix.

IV. USE OF CONTRACTOR FOR WASTE PROCESSING

Contractor-supplied services may be used at Davis-Beese for the processing of radioactive waste, including miscellaneous radwaste liquids, oil waste, and other types of waste resulting from both routine and non-routine operations. For the operation of such process systems, it may be desirable to use process control measures and procedures developed by the contractor specifically for the system. Therefore, previously addressed process control measures for a particular waste stream may, as appropriate, be superseded by contractor-supplied measures. The following discussion addresses the administrative controls that are imposed to assure that contractor-supplied systems and services for processing radioactive waste for disposal at a burial site are compatible with plant operations, procedures and regulatory requirements.

Prior to the use of any contractor for the processing of waste at Davis-Besse, a management review of the contractor's process controls and operating procedures is performed for the purpose of assuring safe operation in accordance with plant procedures and applicable regulatory requirements. For the processing of waste that is intended to be shipped for disposal at a licensed radioactive waste burial site, additional precautions are taken to assure a final waste product that meets the appropriate waste characteristic requirements for solidification or dewatering. In particular, the following items, as applicable, are to be documented by the contractor (or Davis-Besse manuals or procedures) prior to utilization for solid waste processing:

- a general description of the solidification process, including type of solidification agent, major process equipment and interface with plant equipment, type of wastes that can be processed, and operating parameters
- a process control program that provides for the verification of the generation of a suitable waste product, including items such as representative sampling, laboratory tests to establish waste-to-process medium ratios, and criteria for evaluating acceptability of laboratory tests
- specifically approved procedures for the operation of the process equipment that will assure operation within the bounds as determined by the process control program
- appropriate acceptance criteria for evaluating the acceptability of the final waste product.

SPENT RESIN PROCESSING SYSTEM

