



# International Agreement Report

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## Result of BETHSY Test 9.1.b Using RELAP5/MOD3

Prepared by  
S. Petelin, B. Mavko, O. Gortnar, I. Ravnikar, G. Cerne

University of Ljubljana  
"Jožef Stefan" Institute  
Ljubljana, Slovenia

Office of Nuclear Regulatory Research  
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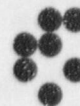
### **Abstract**

RELAP5 computer code was used to simulate an experiment designated 9.1.b, (2" Cold Leg Break without HPSI and with Delayed Ultimate Procedure) performed on BETHSY integral test facility. This test is characterized as beyond design transients scenarios with unavailability of some safety and protection systems. The calculations which have been completed using the computer Sun Sparcstation 20 aim to evidence the difference between experimental and computed data. Generally, an agreement of major transient trends is shown to be obtained in the simulation.



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### List of Abbreviations

|     |       |                                |
|-----|-------|--------------------------------|
| AFW | ..... | auxiliary feedwater            |
| DP  | ..... | pressure difference            |
| DT  | ..... | temperature difference         |
| IJS | ..... | "Jožef Stefan" institute       |
| ISP | ..... | international standard problem |
| MFW | ..... | main feedwater                 |
| NPP | ..... | nuclear power plant            |
| PWR | ..... | pressurized water reactor      |
| RCP | ..... | reactor coolant pump           |
| RCS | ..... | reactor coolant system         |
| SG  | ..... | steam generator                |

### Nomenclature

|          |      |                                     |
|----------|------|-------------------------------------|
| A        | .... | flow area ( $m^2$ )                 |
| g        | .... | acceleration of gravity ( $m/s^2$ ) |
| h        | .... | elevation change (m)                |
| p        | .... | pressure (Pa)                       |
| v        | .... | velocity (m/s)                      |
| x        | .... | length coordinate (m)               |
| $\alpha$ | .... | vapour void fraction ( $m^3/m^3$ )  |
| $\rho$   | .... | density ( $kg/m^3$ )                |

### Subscripts and Superscripts

|      |      |             |
|------|------|-------------|
| cold | .... | in cold leg |
| hot  | .... | in hot leg  |



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## 1 Introduction

The objective of Jožef Stefan Institute (IJS) activities in area of RELAP5 analyses is to extend the experiences in simulations of small break loss of coolant accidents and two-phase natural circulation cooling. With an attempt to investigate all BETHSY experiments available IJS has developed its own RELAP5 model of this facility. The on BETHSY experiences based improved modelling methods will be used in simulations of real plant transients and evaluation of plant accidents management procedures.

The main goal of the calculation is the assessment of the simulation capability of the code for the following phenomena occurring during the small break LOCA experimental test, particularly for the large core uncover and fuel heat-up, requiring the implementation of an ultimate procedure.

The present analysis includes also assessment of three different versions of RELAP5 code (MOD2, MOD3.1 and MOD3.1.2 without any modification of the codes and with guidelines consideration) using experimental data of the BETHSY experiment 9.1.b (OECD-ISP-27). The goal of the comparison among different versions of RELAP5 code was to optimize CPU time and time for new model development.

The report describes the results of the calculation performed by the RELAP5/MOD3 codes and shows the comparisons with the major variables obtained in the experiment. A brief description of the BETHSY facility is provided in Section 2. Section 3 describes discusses the pre-test and post-test results, sensitivity studies are in Section 4 and run statistic is described in Section 5.

## 2 BETHSY facility and corresponding RELAP5 input model

BETHSY facility is located at Centre D'Etudes Nucleaires de Grenoble (France). It is a scaled down model of the three loop 2775 MWt (900 MWe) Framatome PWR power plant, which is designed to simulate most PWR accidents of interest and to study accident management procedures (Fig. 2.1).

Six important choices have been made which characterize indeed the general design of the Bethsy facility. They concern: the number of loops, the rated pressure of both the primary and the secondary side, the maximum core power level, the maximum flow rate of primary pumps, the general scaling factors and the connected circuits and systems. Volume, mass flow and power are scaled to 1/100 full plant size [1,2,3]. The correct Froude number is also maintained in the reactor coolant system (RCS) piping.

IJS RELAP5 base input model, which was developed according to the specified data, is represented on Fig. 2.2. During post test analyses this model was upgraded to the middle and large input model which is presented on figure 2.4 and 2.3 respectively. The models are described in nodalization study in Section 4.



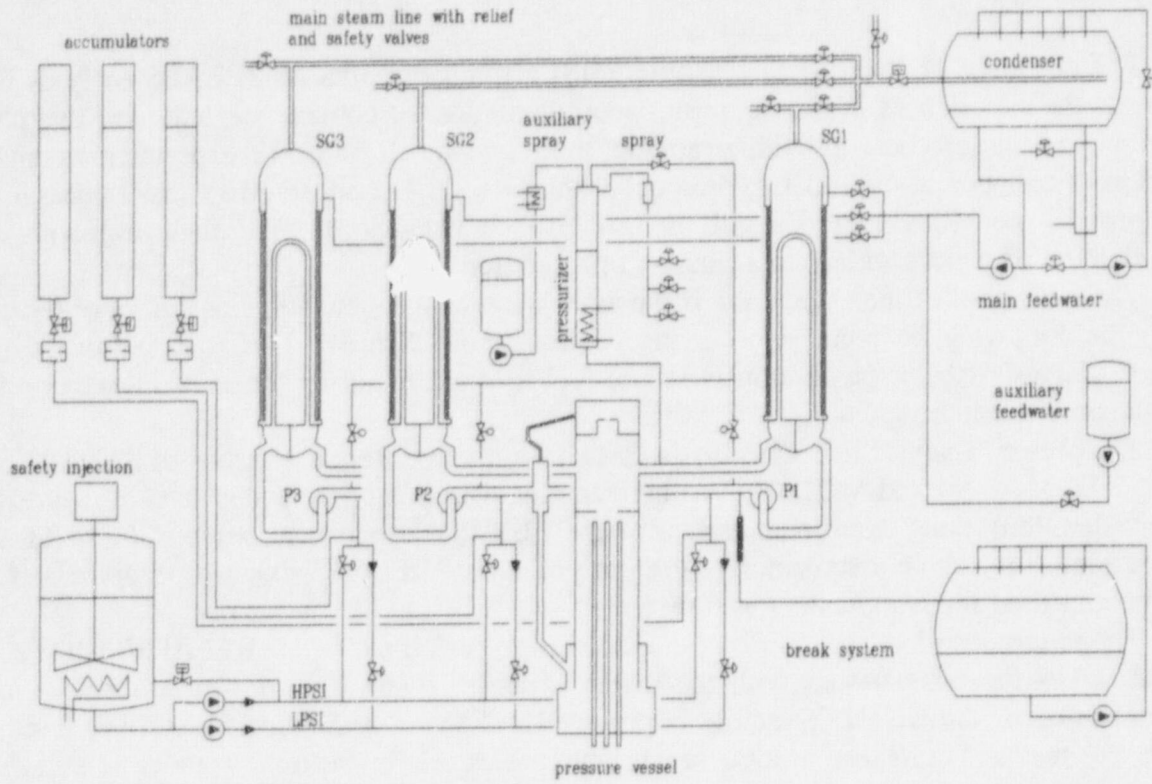


Figure 2.1: BETHSY facility

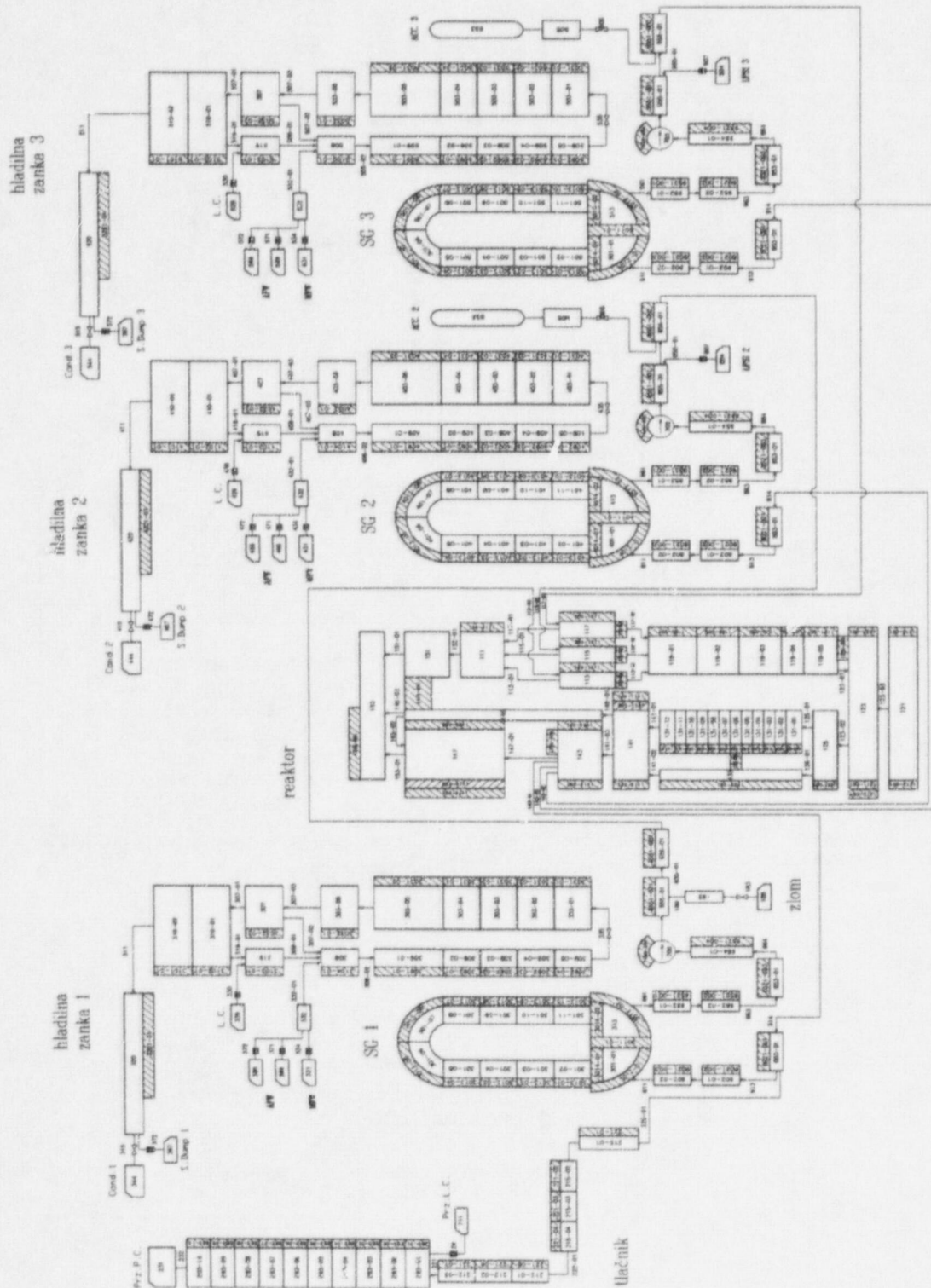


Figure 2.2: Base RELAP5 input model of BETHSY facility

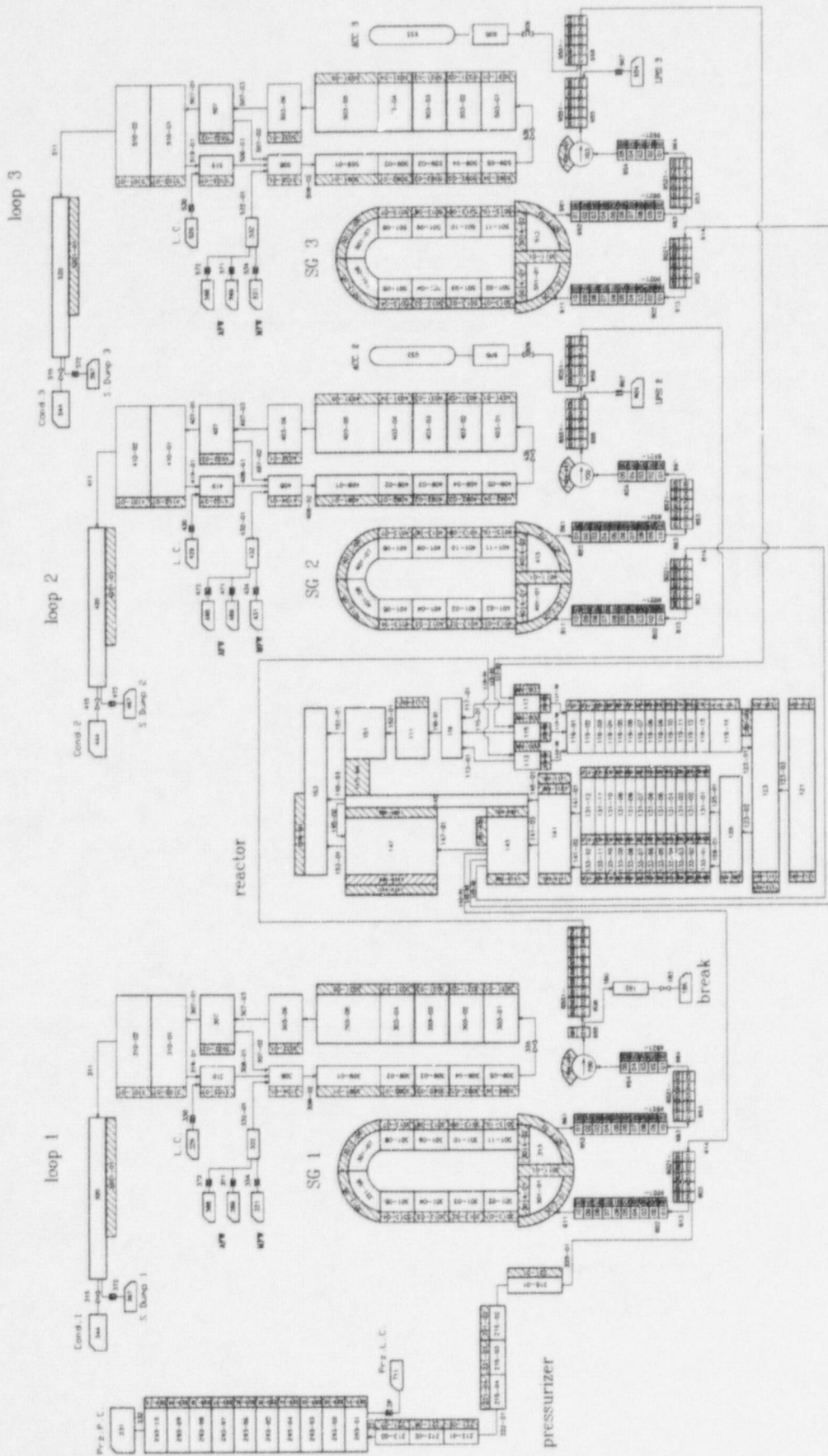


Figure 2.3: Enlarged (detailed) RELAP5 input model of BETHSY facility

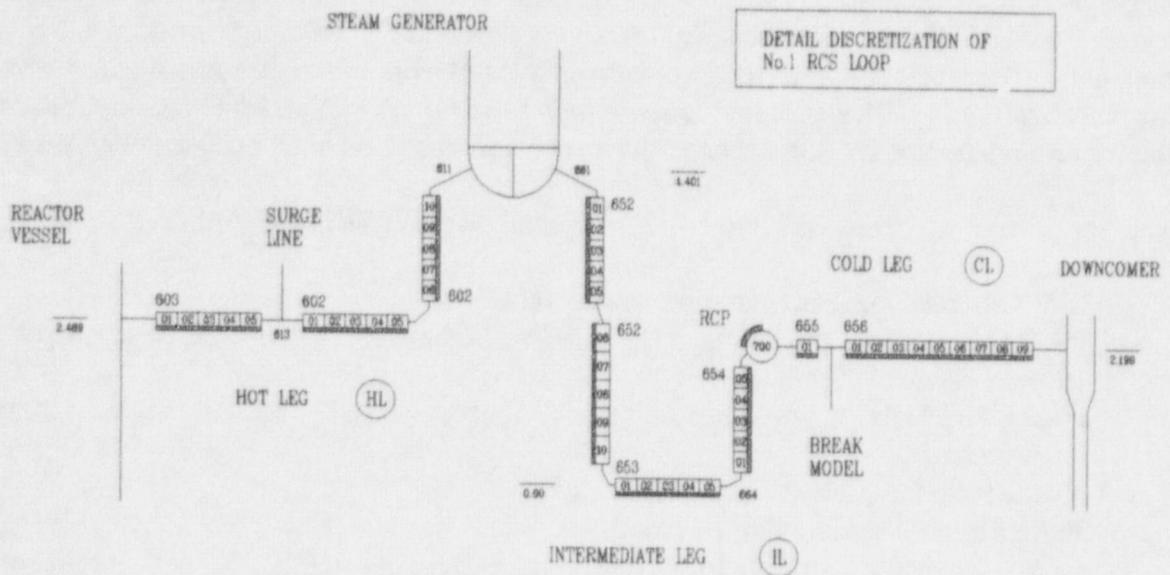


Figure 2.4: RCS renodalization (from Fig. 2.3)

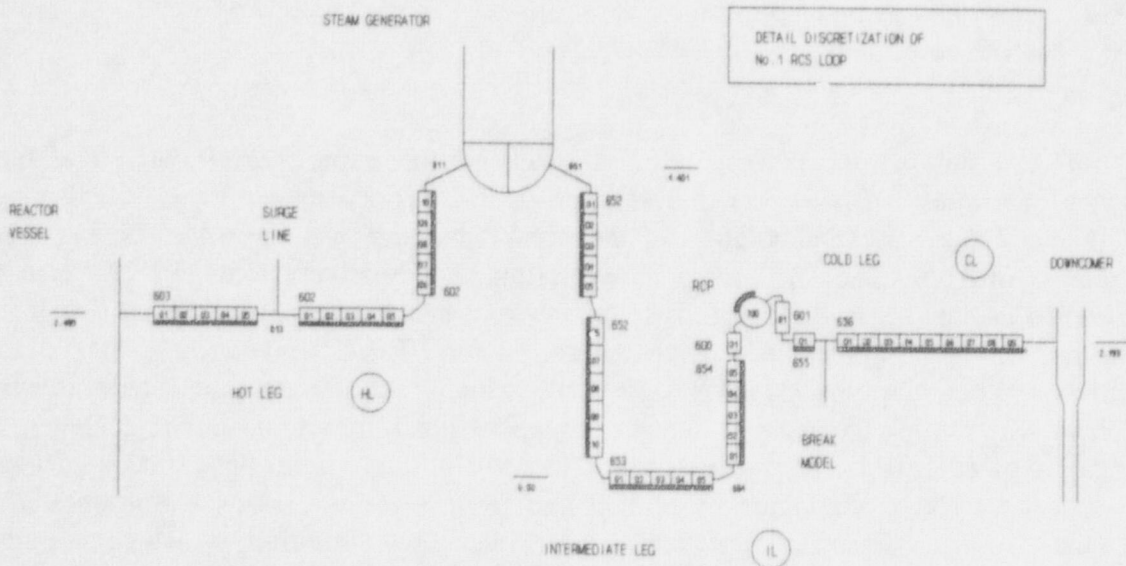


Figure 2.5: RCS and RCP renodalization (RCP renodalization not shown on Fig. 2.3)

### 3 Results

#### 3.1 Pre-test calculations of test 9.1.b (ISP-27)

IJS has participated in the International Standard Problem No.27 (OECD ISP-27) based on test 9.1.b. ISP-27 transient scenario involving a scaled 2" cold led break without high pressure safety injection (HPSI) and with delayed operator action for secondary system depressurization [4]. This transient leads to a large core uncover and fuel heat-up, requiring the implementation of an ultimate procedure. The test was performed on December 19, 1989.

The scenario of the test starts at 10% nominal power (NP), the following actions are achieved:

- **t=0 s:** break opening (initiation of the transient)
- **P+P (pressurizer pressure) = 13.1 MPa:** Scram signal, the core power trip (from 10% NP) starts 17 s latter
- **P+P=11.9MPa** Safety injection signal, but no HPSI, turbine bypass and main feedwater off
- **30 s after SI signal:** Auxiliary feedwater on.
- **300 s after SI signal:** Pump coastdown
- **As the maximum core cladding temperature reaches 450°C:** Implementation of the ultimate procedure consisting in full opening of 3 steam dumps to atmosphere.
- **P+P = 4.2 MPa:** Accumulator injection starts, on the 2 intact loops only.
- **P+P = 1.5 MPa:** Accumulator isolation
- **P+P = 0.91 MPa:** LPIS injection starts, on the 2 intact loops only.
- **When stable RHRS operating condition prevail:** Core outlet fluid temperature < 177°C, P+P < 2.5 Mpa, saturation margin > 20°C, The transient is terminated.

IJS has performed blind pre-test and post-test analyses using computer codes RELAP5/MOD2.36.05 and RELAP5/MOD3.1.

The pre-test simulations correspond quite well to the experimental data. The main deficiency of pre-test analysis was the selection of the "cross" option for the break single junction. Since the correct simulation of the break flow rate was shown to be extremely important in order to determine the time evolution of a relatively long ISP-27 transient, modelling of critical break discharge was studied in post-test analyses of ISP-27 [5]. It was shown, that very good agreement between measured and RELAP5 predicted break flow can be achieved when applying suitably adjusted discharge coefficients of single junction component with abrupt area change and homogeneous junction options (junction flags). An investigation of RELAP5 critical flow prediction for discharge of strongly subcooled liquid was performed. The modification of MOD2 and MOD3 code versions was suggested to correct the erroneous departure from subcooled choked flow condition, which occurs when applying coupled abrupt area change and choking junction options [6].

Since the calculation of critical discharge through the break nozzle is strongly influenced by the break boundary condition, in IJS post-test analyses an attempt was made to improve the prediction of vapour void fraction in the broken No.1 cold leg. Some other RELAP5 participants of ISP-27 also tried to improve their predictions of RCS void distribution during post-test analyses [7,8].

### 3.2 Post-test calculations of test 9.1.b (ISP-27)

A wide sensitivity study to improve the RCS void distribution, which was performed by RELAP5/MOD3.1, dealt with following items:

- decrease of break discharge coefficients
- renodalization of downcomer to upper head bypass introducing the more precise description of flow path
- introduction of homogeneous option for velocity calculation in reactor head junctions
- unrealistic reduction of bypass flow area and unrealistic increase of bypass hydraulic losses
- RCS renodalization increasing the number of nodes from 9 to 45 for RCS piping (Fig. 2.4), from 1 to 12 for core bypass, and from 1 to 14 for the reactor vessel downcomer (Figs. 2.3 and 2.4)
- reduction of two-phase head and torque multipliers in RELAP5 reactor coolant pump (RCP) model
- modifications of initial condition decreasing the average RCS temperature to the lower margin of instrumentation uncertainty range (-0.5K) and increasing the RCS mass flow rate to the upper margin of instrumentation accuracy (+3%)
- increase of RCS heat losses (+20%)
- increase of secondary heat sink changing the steam generator pressure control
- renodalization of reactor coolant pumps (Fig. 2.5).

1. No above parameter or model feature was found with significant influence on vapour void fraction during the first transient phase up to the reactor coolant pumps trip. During this phase the core generated steam bubbles (saturation condition) are driven with (captured in) forced circulation flow - reactor coolant pumps remain running up to 300 seconds after the safety injection signal.
2. None of the above model modifications could essentially contribute to the reduction of No.1 cold leg vapour void fraction during second transient phase following the reactor coolant pumps trip.

In recent calculations the prediction of RCS coolant distribution was shown to be strongly dependent on modelling of the connection from guide tube to upper head: due to the misinterpretation, the annular orifice, J200 (located in guide tube), was connected to the upper plenum instead of to the upper head. The correction of this model inadequacy has improved the prediction of vapour void fraction in the broken No.1 cold leg (comparison of "base case" with "guid.renod." case on Fig. 3.1).

Furthermore, this guide tube renodalization resulted in the time shift of key transient events, which can be observed by comparing the case "RCP+guide" with the base "R5/MOD3.1" calculation on Figs. 3.2 to 3.12. Following the guide tube renodalization, the core uncover and fuel temperature rise started earlier (Figs. 3.4 and 3.6), and therefore the initiation of the "ultimate procedure" was also predicted to occur earlier (Fig. 3.11).

An additional MOD3.1 calculation is planned to be performed with vertical stratification model turned off in guide tube volumes [7,9].

In table 3.1 the measured data from experiment served as a initial conditions for BETHSY model. Data uncertainties are also provided.

Table 3.1: Test 9.1.b (ISP-27), initial condition

|                                     | measured<br>([2]; 10% nominal power)<br>± data uncertainties | BETHSY model<br>(RELAP5/MOD3.1<br>initialization)         |
|-------------------------------------|--|---|
| core thermal power                  | 2864 ± 30 kW   | 2864 kW   |
| cold leg temperature                | 559.9 ± 0.5 K  | 560.3 K (core inlet)                                      |
| downcomer mass flow rate            | 150.0 ± 5.0 kg/s   | 154.3 kg/s  |
| reactor coolant pump speed          | 2940 ± 30 rpm  | 2940 rpm  |
| pressurizer pressure                | 155.1 ± 0.9 bar  | 155.1 bar   |
| pressurizer level                   | 4.08 ± 0.1 m   | 4.12 m  |
| RCS coolant mass                    | 1960 ± 40 kg   | 1948 kg   |
| secondary side pressure             | 69.1 ± 0.4 bar   | 68.1 bar !  |
| steam generator level (short range) | 13.45 ± 0.05 m   | 13.45 m !   |
| feedwater temperature               | 491.1 ± 2.0 K  | 491.0 K   |
| secondary coolant mass (one SG)     | 820 ± 30 kg  | 821 kg !  |
| RCS trace heating                   | 53.5 kW  | no heat losses considering<br>the trace heating system on |

! averaged for all the three steam generators

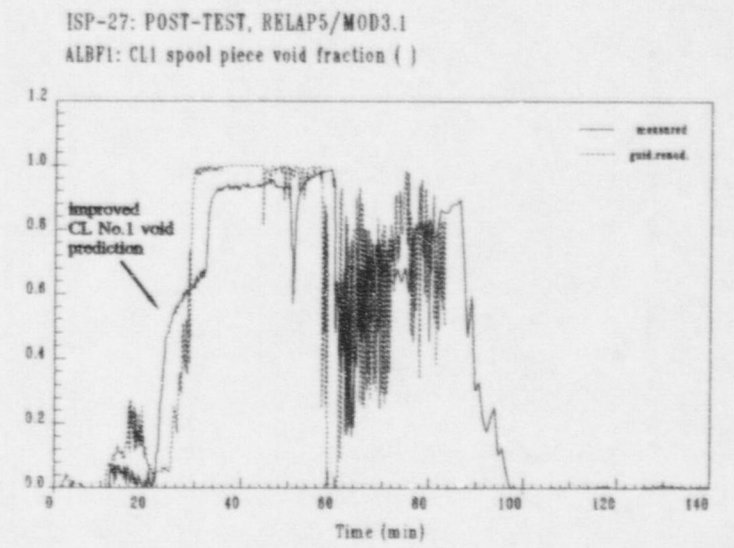
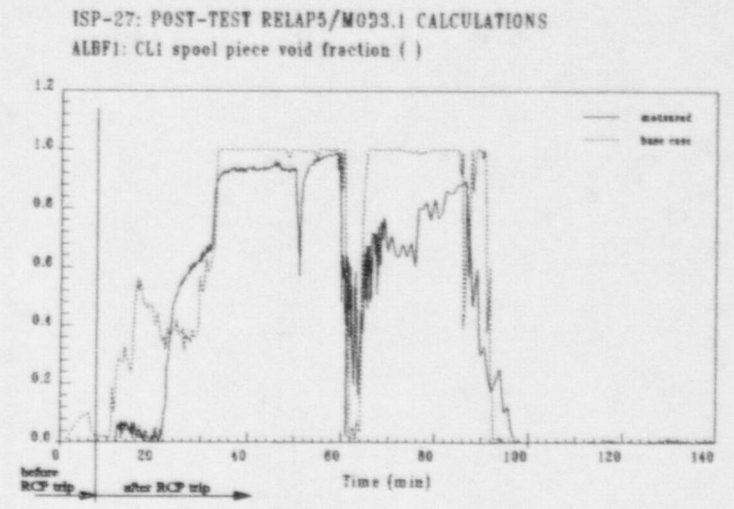
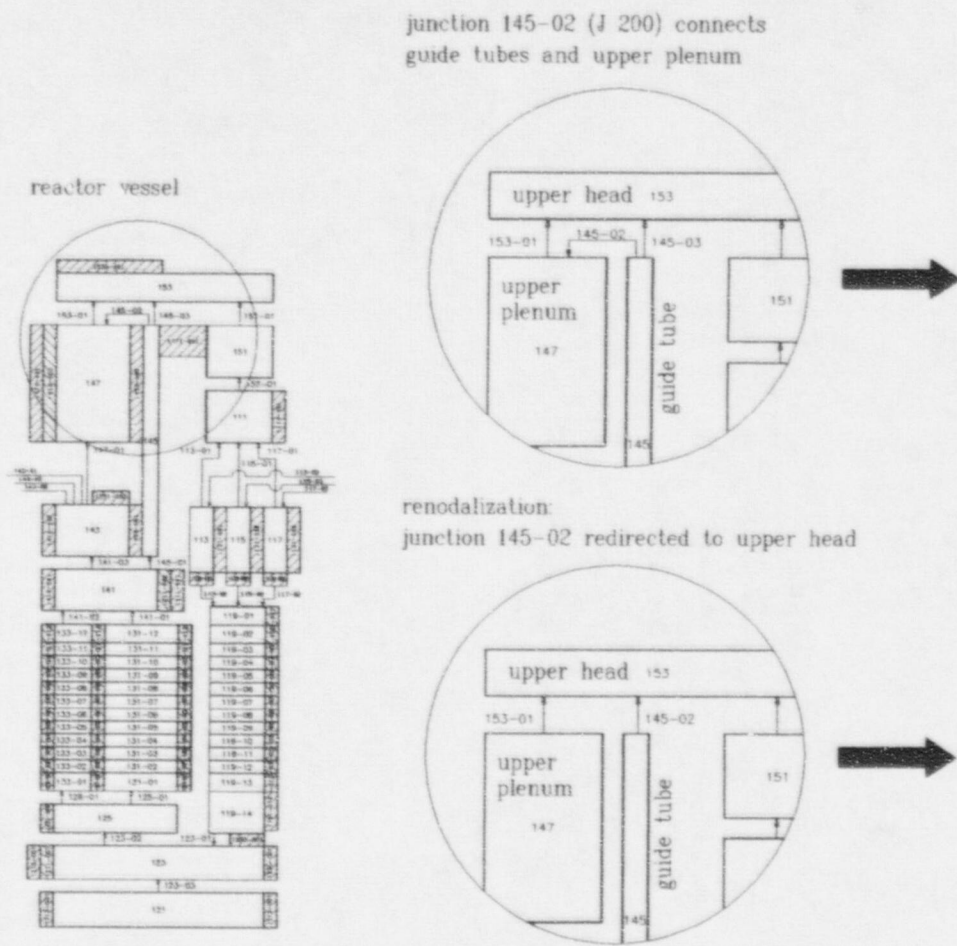


Figure 3.1: The influence of guide tube renodalization



ISP-27: POST-TEST, RELAP5/MOD3.1  
P+P: pressurizer top pressure (MPa)

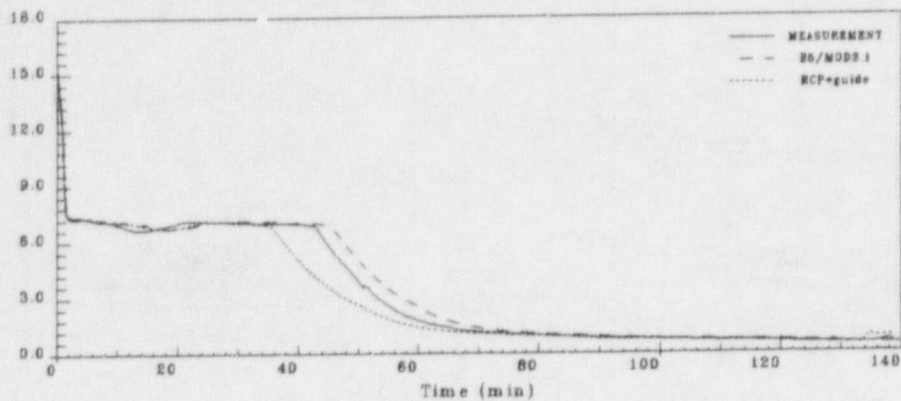


Figure 3.2: Test 9.1.b, Pressurizer pressure

ISP-27: POST-TEST, RELAP5/MOD3.1  
P+57: SG2 steam dome pressure (MPa)

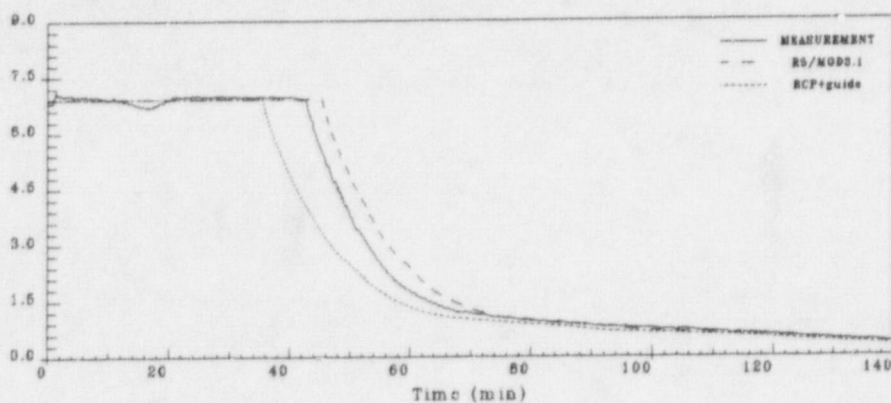


Figure 3.3: Test 9.1.b, No.2 SG steam dome pressure

ISP-27: POST-TEST, RELAP5/MOD3.1  
ZT0200: core collapsed liquid level (m)

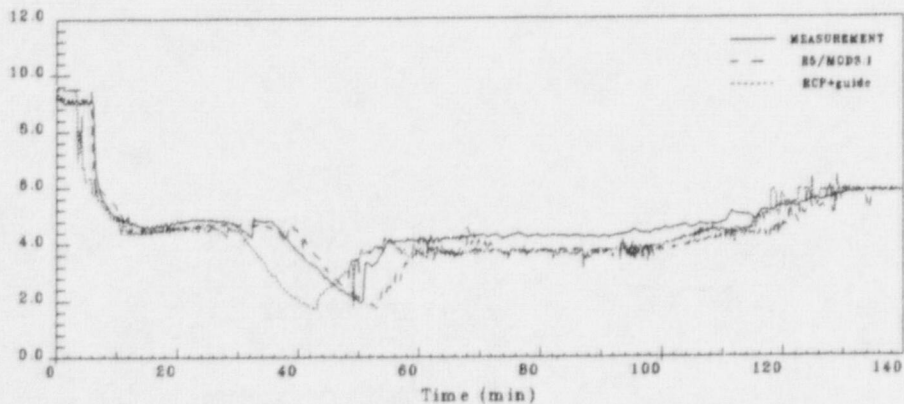


Figure 3.4: Test 9.1.b, Core collapsed liquid level

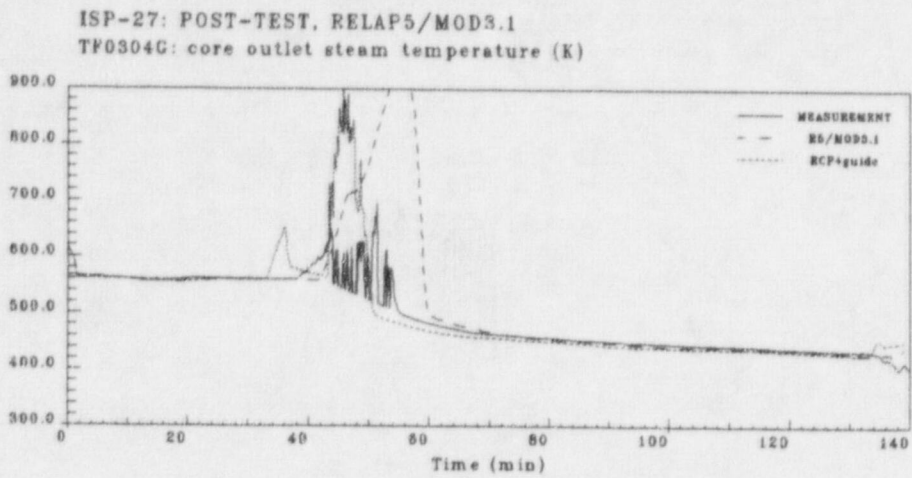


Figure 3.5: Test 9.1.b, Core outlet steam temperature

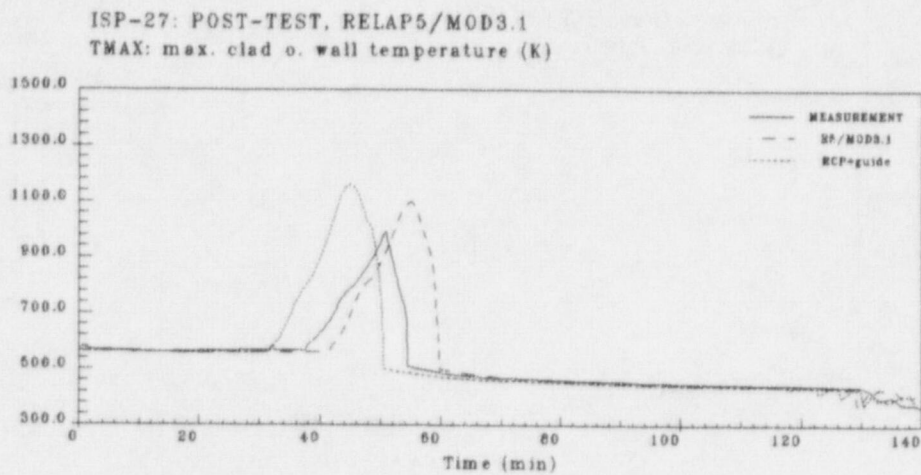


Figure 3.6: Test 9.1.b, Maximum cladding temperature

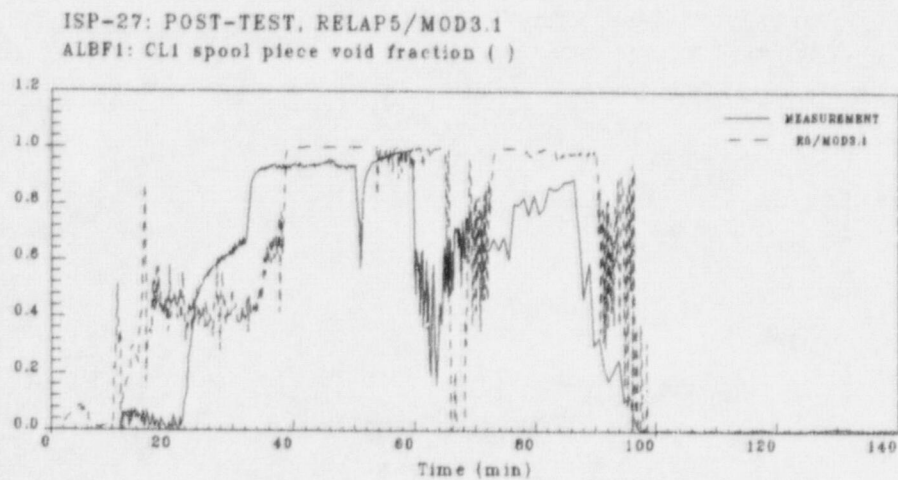


Figure 3.7: Test 9.1.b, No.1 CL spool piece void fraction, base case

ISP-27: POST-TEST, RELAP5/MOD3.1  
ALBF1: CLI spool piece void fraction ( )

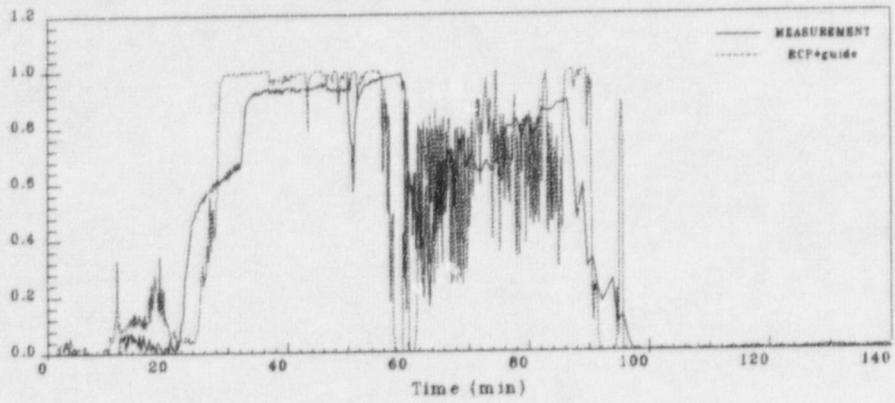


Figure 3.8: Test 9.1.b, No.1 CL void fraction, renod. of guide tube

ISP-27: POST-TEST, RELAP5/MOD3.1  
QMB: break mass flow rate (kg/s)

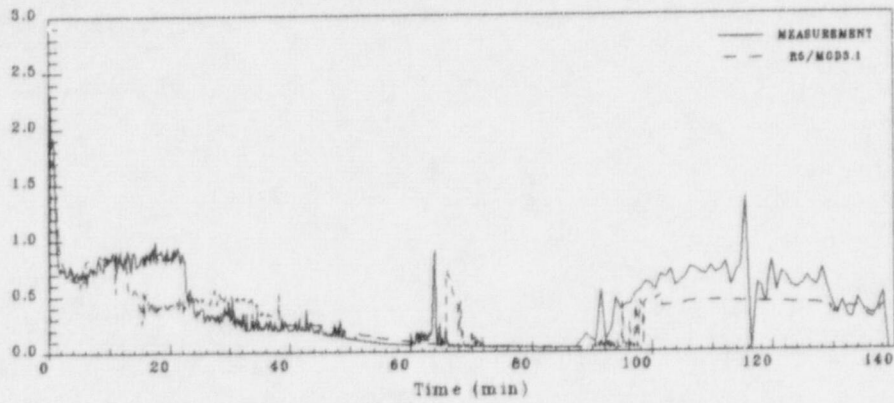


Figure 3.9: Test 9.1.b, Break mass flow rate, base case

ISP-27: POST-TEST, RELAP5/MOD3.1  
QMB: break mass flow rate (kg/s)

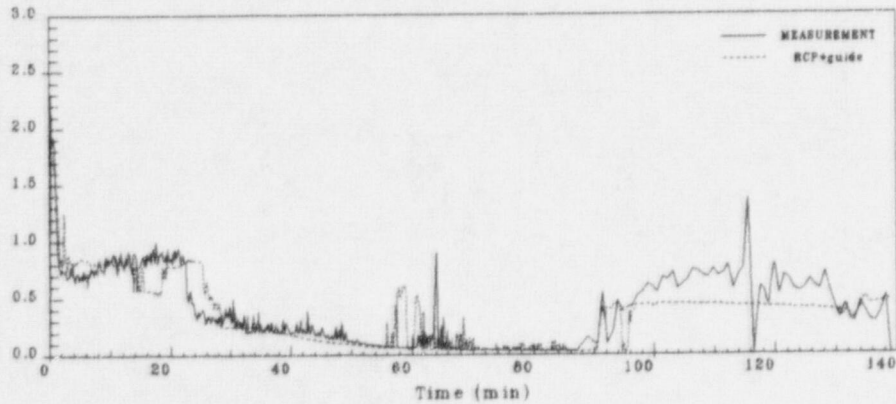


Figure 3.10: Test 9.1.b, Break mass flow rate, renod. of guide tube

ISP-27: POST-TEST, RELAP5/MOD3.1  
MGV2: SG2 secondary side mass inventory (kg)

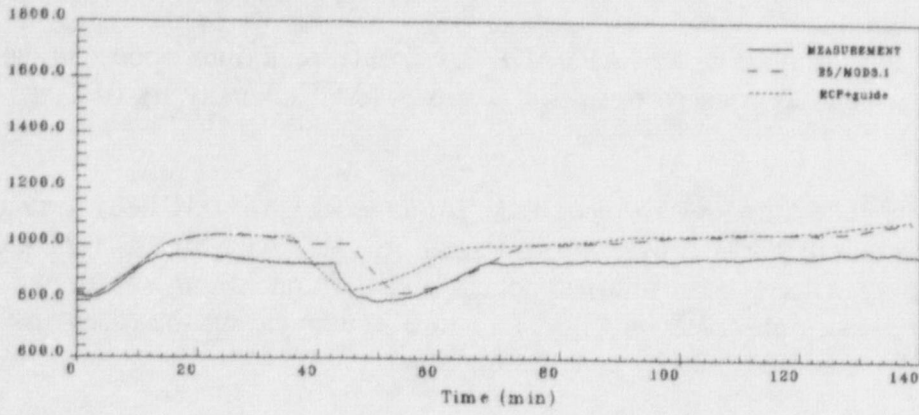


Figure 3.11: Test 9.1.b, Secondary side mass inventory

ISP-27: POST-TEST, RELAP5/MOD3.1  
INTQMB: break discharged mass (kg)

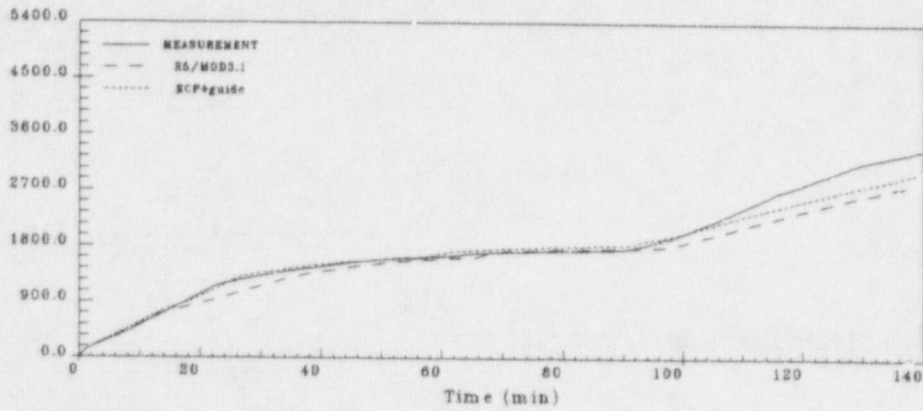


Figure 3.12: Test 9.1.b, Break discharged mass

### 3.3 RELAP5/MOD3.1.2 simulation realized at Texas A&M University

The time shift problem of RELAP5/MOD3.1 simulation did not appear in the last ISP-27 calculation, which has been performed at Texas A&M University by RELAP5/MOD3.1.2 code.

Base IJS input deck and restart input decks from the RELAP5/MOD3.1 simulation of ISP-27 have been sent to A&M University for testing on a RELAP5/MOD3.1.2 simulation. The results of the test have been returned to IJS and the conclusion was drawn that all the transient differences observed on Figs. 3.13 to 3.21 comparing the cases "MOD3.1" and "MOD3.1.2" are caused only by code differences.

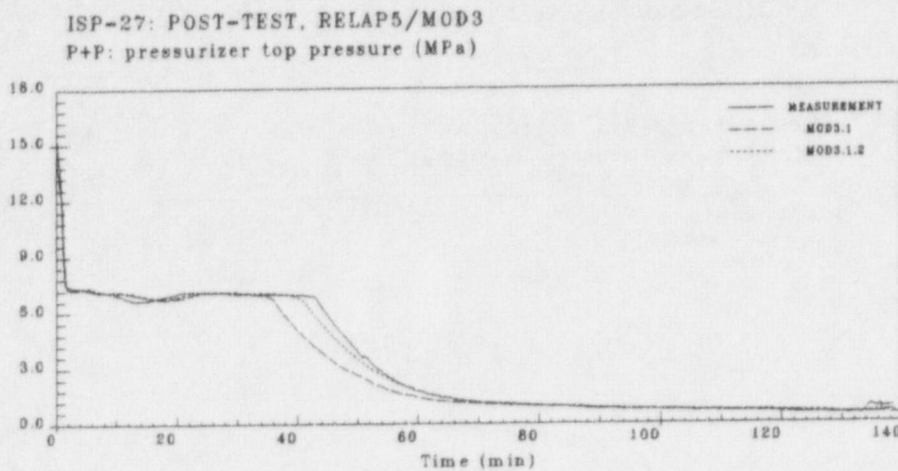


Figure 3.13: Test 9.1.b, Pressurizer pressure

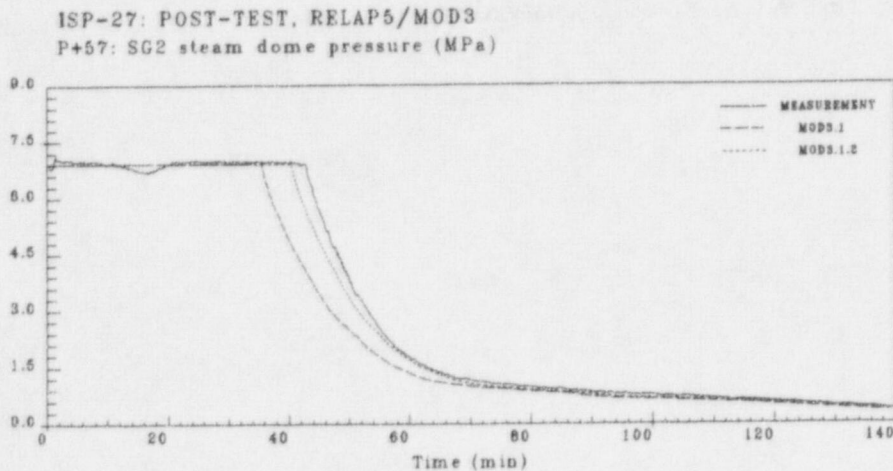


Figure 3.14: Test 9.1.b, No.2 SG steam dome pressure

ISP-27: POST-TEST, RELAP5/MOD3  
ZT0200: core collapsed liquid level (m)

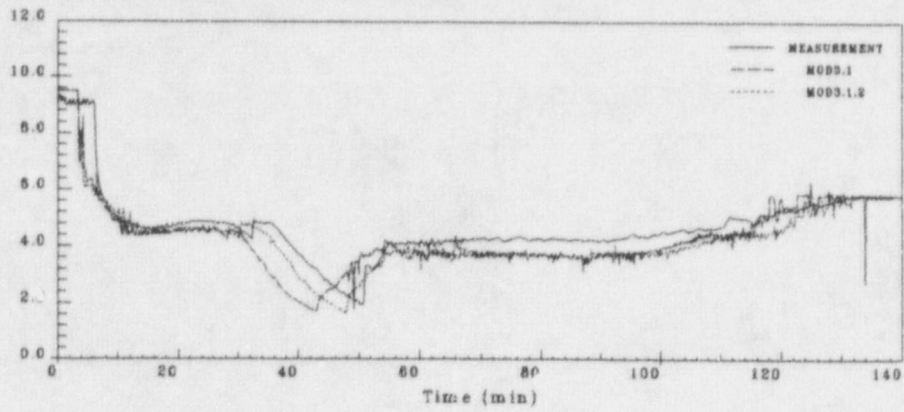


Figure 3.15: Test 9.1.b, Core collapsed liquid level

ISP-27: POST-TEST, RELAP5/MOD3  
TF0304G: core outlet steam temperature (K)

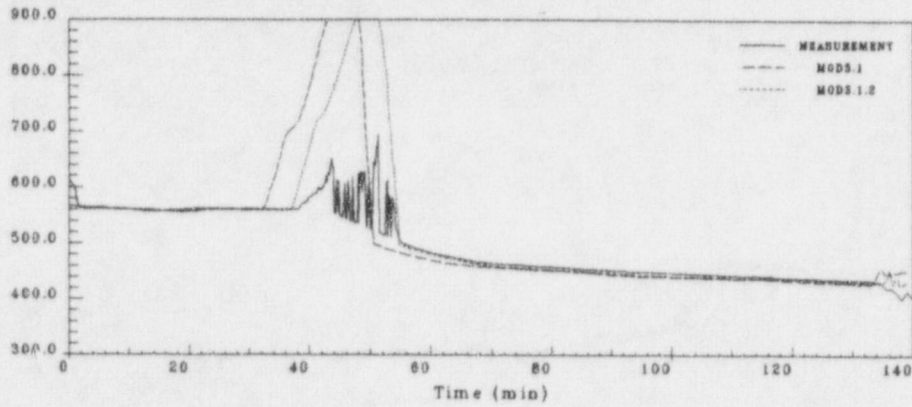


Figure 3.16: Test 9.1.b, Core outlet steam temperature

ISP-27: POST-TEST, RELAP5/MOD3  
TMAX: max. clad o. wall temperature (K)

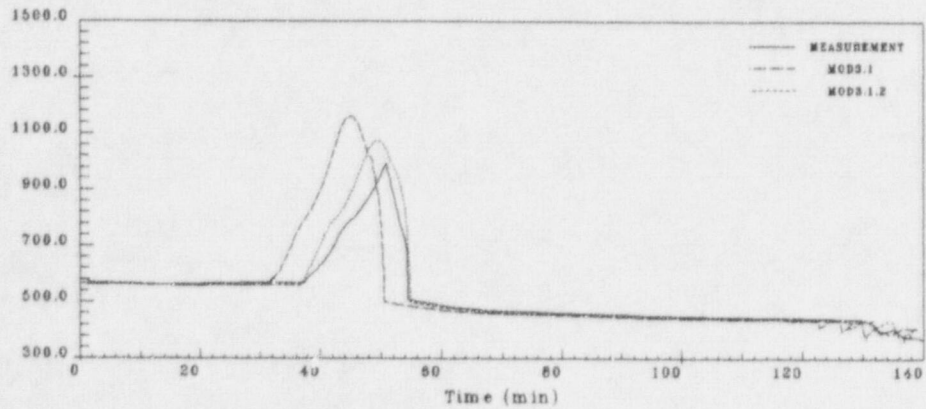


Figure 3.17: Test 9.1.b, Maximum cladding temperature

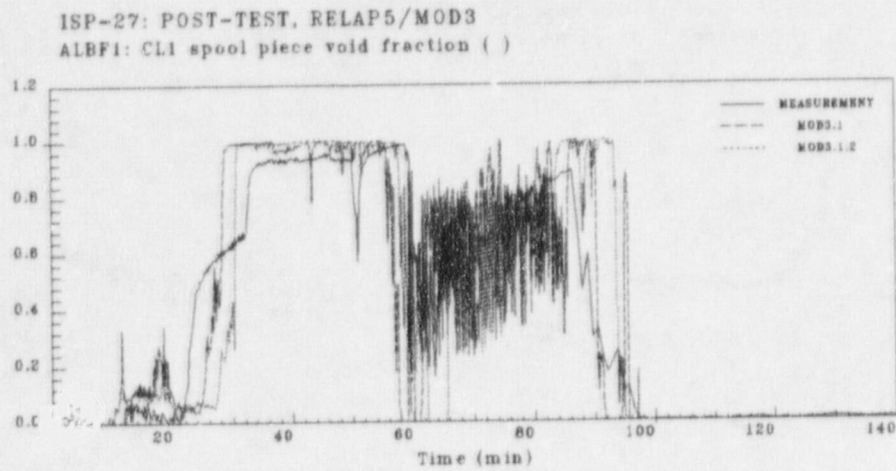


Figure 3.18: Test 9.1.b, No.1 CL spool piece void fraction

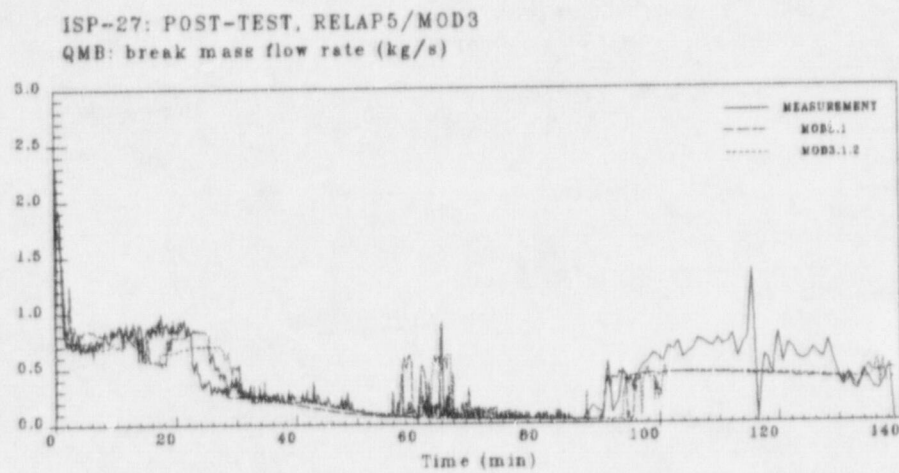


Figure 3.19: Test 9.1.b, Break mass flow rate

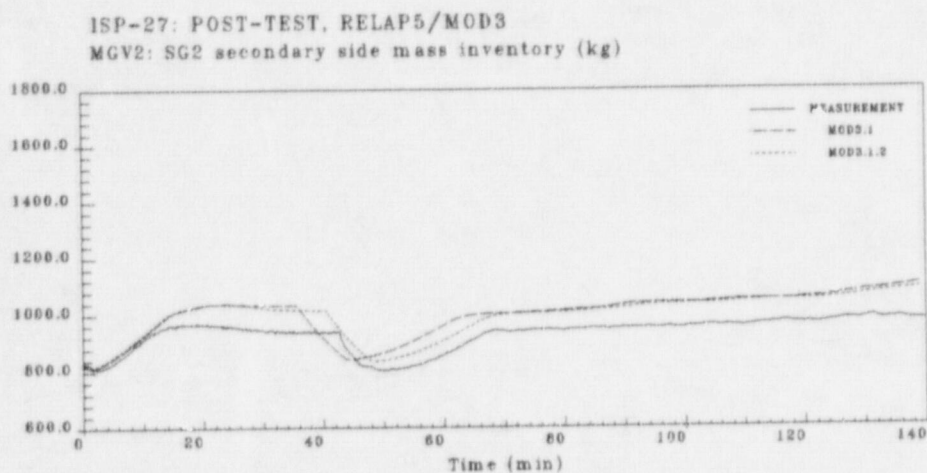


Figure 3.20: Test 9.1.b, Secondary side mass inventory

ISP-27: POST-TEST, RELAP5/MOD3  
INTQMB: break discharged mass (kg)

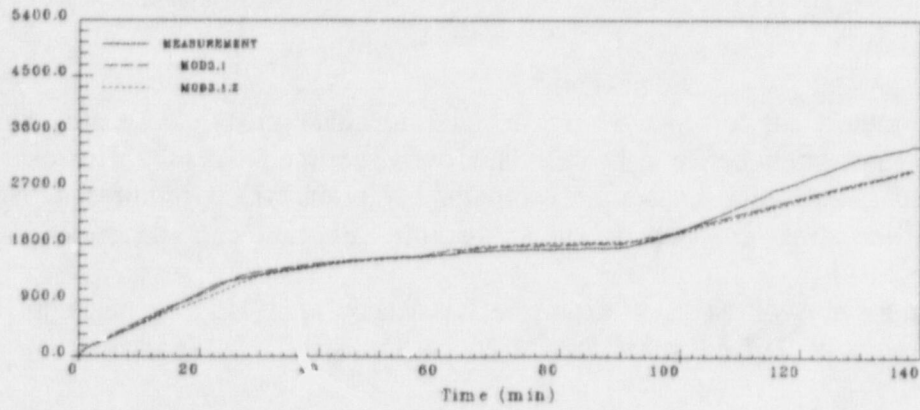


Figure 3.21: Test 9.1.b, Break discharged mass



## 4 Nodalization Study for BETHSY Experiment

### 4.1 Description

Some authors suggest that a more detailed nodalization should be utilized in order to achieve better agreement between the calculated and experimental results. However, sometime more detailed nodalization causes an oscillatory solution which requires a much smaller current and computing time step. In such situations CPU time can become excessive.

A comparison of existing experimental data of BETHSY experiment 9.1.b with simulation results of RELAP5/ MOD2, MOD3.1 and MOD3.1.2 is made.

The IJS RELAP5/MOD2 input model was developed and initialized according to the specified data for each test. Each of the three coolant loops is represented explicitly without taking into account the small asymmetry between the loops. This base input (Fig. 2.2) consisted of 196 volumes, 207 junctions, 191 heat structures, 125 control variables and 13 trips. On this base RELAP5/MOD2 input model was further upgraded to RELAP5/MOD3.1 and RELAP5/MOD3.1.2. During post-test analyses, the base input model was renodalized, increasing the number of nodes in reactor coolant system piping, reactor coolant pumps, core bypass section and reactor vessel downcomer. The elevations of parallel volumes of the reactor downcomer in bypass reactor core, hot leg and cold leg were preserved. Nodalization of the reactor core, pressurizer, steam generators, reactor head, upper plenum and lower plenum remained the same for middle input which is presented in figure 2.4. Further, middle RELAP5 model was again upgraded, increasing the number of nodes only in steam generator. The detailed RELAP5 model of BETHSY facility contains 332 volumes, 343 junctions and 330 heat structures (Figs. 2.3, 2.4, 2.5). All three inputs based on different nodalization should represent the same situation using different computer codes. These were assured with strict consideration of RELAP5 code manuals. Table 4.1. presents number of volumes, junctions, heat structures and mesh points for various inputs nodalization [10].

The comparison of experimental data with simulation results concentrated on only a few important variables such as cold leg no#1 spool piece void fraction, maximal clad temperature, core collapsed liquid level and break mass flow rate [11,12,13].

Table 4.1.: Three nodalizations.

| Nodalizations | Volumes | Junctions | Heat Str./M.P. |
|---------------|---------|-----------|----------------|
| Small Input   | 196     | 207       | 191/754        |
| Middle Input  | 332     | 343       | 330/1290       |
| Large Input   | 398     | 408       | 396/1554       |

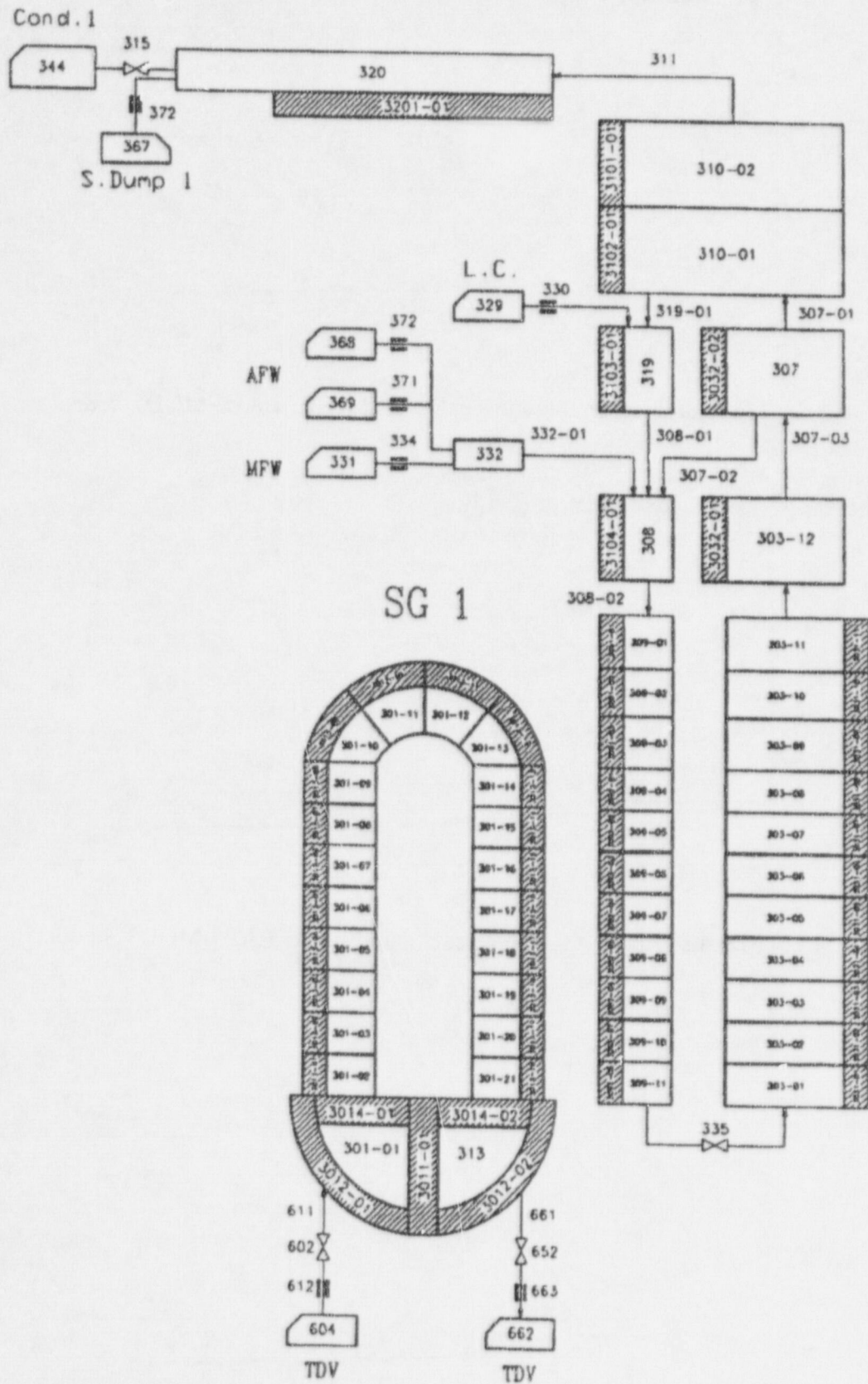


Figure 4.1: Steam generator nodalization for large input model

ISP-27: POST-TEST, RELAP5/MOD2  
TMAX: max. clad o. wall temperature (K)

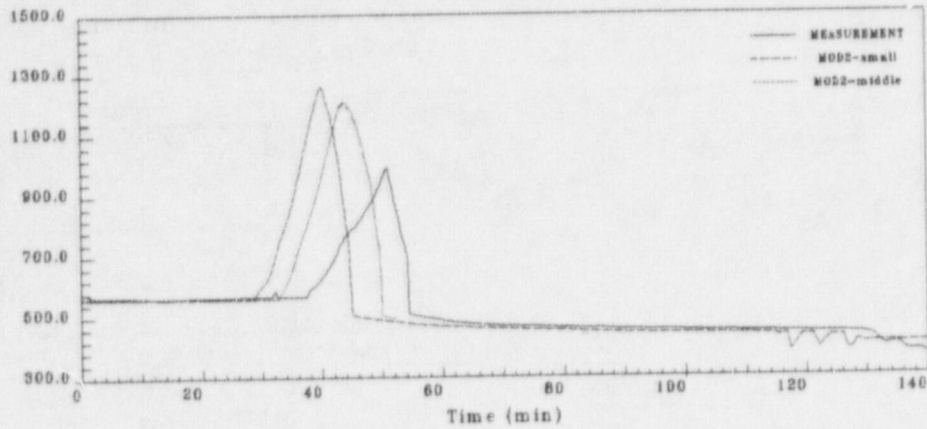


Figure 4.2: Maximal clad temperature calculated by RELAP5/MOD2 code.

ISP-27: POST-TEST, RELAP5/MOD31  
TMAX: max. clad o. wall temperature (K)

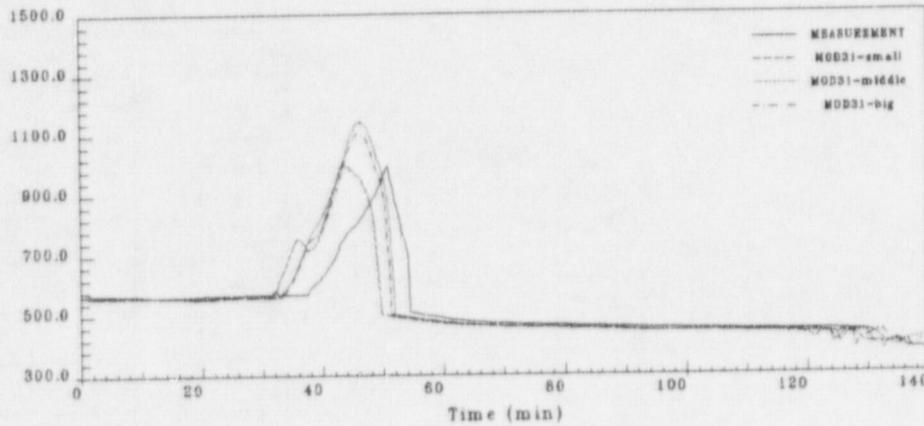


Figure 4.3: Maximal clad temperature calculated by RELAP5/MOD3.1 code.

ISP-27: POST-TEST, RELAP5/MOD3.1.2  
TMAX: max. clad o. wall temperature (K)

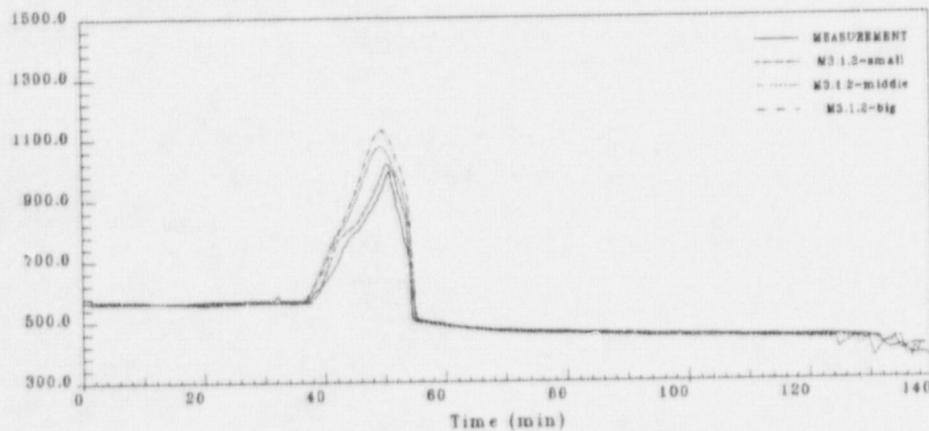


Figure 4.4: Maximal clad temperature calculated by RELAP5/MOD3.1.2 code.

## 5 Run Statistics

The original RELAP5/MOD3.1 code with no modifications and with guidelines consideration was used. Calculations were done on Sun Sparcstation 20 (4 processor workstation) which uses multiuser and multitasking operating system SOLARIS 2.5.

The time step was limited at  $1.0E-6$  as a minimum time step and  $2.0E-2$  as a maximum time step. During the calculation the thermodynamic property error (liquid phase property error) at time 4119.642 sec. Therefore, restart calculation with the reduced maximum time step of  $1.0E-4$  was applied for the next 50 seconds to overcome this.

The computational efficiency for middle nodalization (Table 4.1) is summarized in Table 5.1 14

Table 5.1.: Computational efficiency

| Calculation | Computer Time (CPU), sec | Number of time Step (DT) | Number of volume (N) | Grind Time CPU/(N*DT) |
|-------------|--------------------------|--------------------------|----------------------|-----------------------|
| RELAP5/MOD3 | 72064 sec                | 491413                   | 332                  | 0.00044               |

Listing of the base input model and restart one are in Appendix A.

## 6 Conclusion

RELAP5/MOD3.1 computer code was used to simulate experiment performed on BETHSY integral test facility (dealing with small break loss of coolant accidents). The main discrepancies between the simulations presented and the measured data were found to be connected with the predictions of critical discharge, collapsed core liquid level and loop seal clearance phenomena. It should be noted that the reasons for all the problems encountered are not yet well understood.

The wide RELAP5/MOD3.1 sensitivity study, which was performed to improve the prediction of RCS void distribution for test 9.1.b (ISP-27), succeeded with the correction of an input model inadequacy: the orifice J200 (located in guide tube) has been connected to the upper plenum instead of to the upper head. Following this error correction, the prediction of vapour void fraction in broken No.1 cold leg was improved. Especially good agreement with experimental data was achieved in the last ISP-27 simulation which was performed by RELAP5/MOD3.1.2 code version at Texas A&M University.

In general, we found that a more detailed nodalization may lead to more accurate prediction of void fraction but it also may lead to less accurate prediction of other variables, for example maximal clad temperature (figures 2.2 through 2.4).

More detailed nodalization may also lead to an oscillatory solution which needs a very small time step and therefore extensive CPU time. Such calculations can be very sensitive to certain control volumes with regard to numerical stability resulting water property error.

Further, we found that for the most parameters and control variables there are no essential differences between the results of the more detailed and less detailed nodalizations.

Comparison of the results of MOD2, MOD3.1 and MOD3.1.2 shows that in general the best

results are obtained from MOD3.1.2. This version of RELAP5 code seems to be less sensitive on users affects. What means that different manner of modelling the same flow path are no more so sensitive.

The participation in BETHSY program provided additional knowledge which is needed for good understanding of RCS phenomena during SB LOCA (e.g. RELAP5 simulation of DP measurements observing the loop seal clearance phenomena). Further comparison of existing experimental data with simulation results will lead to the modifications and improvements of developed input models of experimental facilities and real plants. Experiences gained in analyses of BETHSY experiments will also be used in simulations of real plant transients which consider similar transient scenarios. Furthermore, IJS analyses also aim to answer some basic questions concerning the effect on two-phase flows of scaling a commercial nuclear plant down to the size of experimental facilities.

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## **APPENDIX A**

Listing of the middle BETHSY nodalization

- base input
- restart input

## Appendix A - Listing of the middle BETSY nodalization - base input

```

* bethsy - standardni eksperiment: po 5.3.1991
* relap5/mod3
*
* posttestni komentarji:
*
* podrobnejša diskretizacija primarnih cevovodov
* tudi podrobnejša diskretizacija toplotnih teles na RCS
cevovodih
* (trase heating so sicer ugesnili sele po vbrizgu
akumulatorjev v 86.min)
* s korekcijo: vseh ISP-27 DP tlačnih raznaval po
renodalizaciji RCS (R+)
* vseh ISP-27 VOIDG senzorjev po renodalizaciji
RCS (R+)
*
* RCP+ : dh renodalizacija RCP (1->3 vol.)
* R- : komentar najpomembnejših dodatnih sprememb na 5x
gostejši mreži
* **** : iz nbam3.dat je vzet realistični model bypassa v
glavo reaktorja
* fff : spremembe flagov spojev v glavi reaktorja iz 3-
centrally na 1-upward
* hbb : renod. obtoka 133 (1->12 vol. in pipe(119,131,133)
fvcas v:3->0)
* ddd : renod. downcomerja 119 (5->14 vol., elevacije
ustrezno sredici 131)
* ggg : spoj 145-03 (j200) prenesen na mesto 145-02 (j21)
*
* tokrat nobenih poizkusov s homogeno glavo!
*
* * # : znižanje Tcold reference s 560.35 K (+0.5 K) na 559.35
K (-0.5 K)
* * # : povečanje mRCS na zgornjo tolerancno mejo 150 kg/s ->
155 kg/s
* ffl : potrebni izklop inicializacije toplotnega telesa
*
*****
*
* rxxx, rxxxcc : reaktorska posoda, rx ctv blok
* ssgg, ssggcc : uparjalnik, sg ctv blok
* rrrc, rcp- : primarni cevovod, crpalka
* pprzz, sline : tlacnik, prelivni vod
* smff, ssll : glavno napajanje, parovod
* llpp : lpsi in akumulatorji
* aaff, rzll : pomožno napajanje in steam dump, cll zlom
* bhss, hhll : blok toplotnih teles, model toplotnih izgub
* ccc, ccci : regulacijski sistem, reg. sistem za
inicializacijo
* ccvv, ccvvi : blok kontrolnih spremenljivk, b.k.s. za
inicializacijo
* ttrr : blok tripov
* ddhh : dh korekcija tlačnih raznaval
*
* predtestni komentarji:
*
* ** : opozorilo ali pomanjkljivost
* *! : uglasitev dp hidravličnih izgub
* kkk : komentar

```

```

*****
*
100 new transnt * 0 ... z izpisom
* 100 new stdy-st
* 101 inp-chk
*
110 nitrogen
120 121010000 0.0 h2o prim
121 303010000 9.912 h2o sek1
122 403010000 9.912 h2o sek2
123 503010000 9.912 h2o sek3
*
201 200.0 1.0-6 0.1 3 100 1000 1000
*
*****
** mnee minor edit - initialization
*
*****
**
** rx
*301 cntrlvar 102 * reactor vessel inventory mass
[kg]
*302 cntrlvar 120 * total core power [kw]
*303 cntrlvar 110 * core level [m]
*304 cntrlvar 111 * reactor vessel level [m]
*305 mflowj 123010000 * rx downcomer mass flow [kg/s]
**
*306 mflowj 180000000 * cll break mass flow [kg/s]
**
** prz
*307 p 203100000 * prz pressure [pa]
*308 cntrlvar 203 * prz level [m]
*309 q 203010000 * heater power [w]
**
** rcs - loop 1
*310 tempf 602010000 * loop 1 thot [k]
*311 tempf 655010000 * loop 1 tcold [k]
*312 mflowj 611000000 * loop 1 loop mass flow [kg/s]
*313 pmpvel 701 * loop 1 pump speed [rad/s]
**
** rcs - loop 2
*314 tempf 802010000 * loop 2 thot [k]
*315 tempf 855010000 * loop 2 tcold [k]
*316 mflowj 811000000 * loop 2 loop mass flow [kg/s]
*317 pmpvel 702 * loop 2 pump speed [rad/s]
*318 mflowj 806000000 * accum. 2 mass flow [kg/s]
*319 mflowj 807000000 * lpsi 2 mass flow [kg/s]
**
** rcs - loop 3
*320 tempf 902010000 * loop 3 thot [k]
*321 tempf 955010000 * loop 3 tcold [k]
*322 mflowj 911000000 * loop 3 loop mass flow [kg/s]
*323 pmpvel 703 * loop 3 pump speed [rad/s]
*324 mflowj 906000000 * accum. 3 mass flow [kg/s]
*325 mflowj 907000000 * lpsi 3 mass flow [kg/s]
**
** sg 1
*331 p 310010000 * sg 1 pressure [pa]
*332 mflowj 311000000 * sg 1 steam flow [kg/s]

```

```

*333 cntrlvar 305 * sg 1 sec. mass [kg]
*334 cntrlvar 303 * sg 1 downcomer level [m]
*335 mflowj 335000000 * sg 1 recirculation mass flow
[kg/s]
*336 mflowj 334000000 * mfw 1 mass flow - constant [kg/s]
*337 mflowj 332010000 * total feed1 flow [kg/s]
*338 mflowj 372000000 * steam dump 1 flow [kg/s]
**
** sg 2
*341 p 410010000 * sg 2 pressure [pa]
*342 mflowj 411000000 * sg 2 steam flow [kg/s]
*343 cntrlvar 405 * sg 2 sec. mass [kg]
*344 cntrlvar 403 * sg 2 downcomer level [m]
*345 mflowj 435000000 * sg 2 recirculation mass flow
[kg/s]
*346 mflowj 434000000 * mfw 2 mass flow - constant [kg/s]
*347 mflowj 432010000 * total feed2 flow [kg/s]
*348 mflowj 472000000 * steam dump 2 flow [kg/s]
**
** sg 3
*351 p 510010000 * sg 3 pressure [pa]
*352 mflowj 511000000 * sg 3 steam flow [kg/s]
*353 cntrlvar 505 * sg 3 sec. mass [kg]
*354 cntrlvar 503 * sg 3 downcomer level [m]
*355 mflowj 535000000 * sg 3 recirculation mass flow
[kg/s]
*356 mflowj 534000000 * mfw 3 mass flow - constant [kg/s]
*357 mflowj 532010000 * total feed3 flow [kg/s]
*358 mflowj 572000000 * steam dump 3 flow [kg/s]
**
*360 cntrlvar 235 * heat losses
**
*****
**
** prz:
*388 mflowj 232000000 * umprz flow
*389 mflowj 712000000 * uschar flow
**
** sg:
*390 cntrlvar 300 * 11 delta tcold
*391 cntrlvar 324 * sg 1 recirculation control
*392 mflowj 330000000 * mfw 1 mass flow - sg level
control
**
*393 cntrlvar 400 * 12 delta tcold
*394 cntrlvar 424 * sg 2 recirculation control
*395 mflowj 430000000 * mfw 2 mass flow - sg level
control
**
*396 cntrlvar 500 * 13 delta tcold
*397 cntrlvar 524 * sg 3 recirculation control
*398 mflowj 530000000 * mfw 3 mass flow - sg level
control
**
*****
** mnee requested minor edit
*

```



```

*****
*****
**
*301 voidg 603030000 * albc1: h11 spool piece void
fraction [ ] R+
*302 voidg 656070000 * albf1: c11 spool piece void
fraction [ ] R+
*303 voidg 803030000 * albc2: h12 spool piece void
fraction [ ] R+
*304 voidg 856070000 * albf2: c12 spool piece void
fraction [ ] R+
*305 voidg 903040000 * albc3: h13 spool piece void
fraction [ ] R+
*306 voidg 956070000 * albf3: c13 spool piece void
fraction [ ] R+
**
*** dp = p(low press. tap) - p(high press. tap)
**
*307 cntrlvar 240 * dp0200 : core heat. length diff.
press. [kpa]
*308 cntrlvar 241 * dpup1 : upper plenum diff.
press. [kpa]
*309 cntrlvar 242 * dp034 : guide tube dif. press.
[kpa]
*310 cntrlvar 243 * dpuhear : upper head dif. press.
[kpa]
*311 cntrlvar 244 * dp050 : downcomer to upp. head
dif. p. [kpa]
*312 cntrlvar 245 * dp0r1 : pressure vessel dif.
press. [kpa]
**
*313 cntrlvar 246 * dp1 : c11 to h11 diff. press.
[kpa]
*314 cntrlvar 247 * dp12pg : pump 1 diff. press.
[kpa]
*315 cntrlvar 248 * dp12vg : loop seal 1 downf. side
dif. p. [kpa]
*316 cntrlvar 249 * dp12vp : loop seal 1 upflow. side
dif. p. [kpa]
**
*317 cntrlvar 250 * dp2 : c12 to h12 diff. press.
[kpa]
*318 cntrlvar 251 * dp22pg : pump 2 diff. press.
[kpa]
*319 cntrlvar 252 * dp22vg : loop seal 2 downf. side
dif. p. [kpa]
*320 cntrlvar 253 * dp22vp : loop seal 2 upflow. side
dif. p. [kpa]
**
*321 cntrlvar 254 * dp3 : c13 to h13 diff. press.
[kpa]
*322 cntrlvar 255 * dp32pg : pump 3 diff. press.
[kpa]
*323 cntrlvar 256 * dp32vg : loop seal 3 downf. side
dif. p. [kpa]
*324 cntrlvar 257 * dp32vp : loop seal 3 upflow. side
dif. p. [kpa]
**
*325 cntrlvar 258 * dp4 : sg1 u-tube in. to outlet
dif. p. [kpa]
*326 cntrlvar 259 * dp41 : sg1 inlet plenum diff.
press. [kpa]
*327 cntrlvar 260 * dp426 : sg1 u-tube upflow side
dif. p. [kpa]
*328 cntrlvar 261 * dp4r2 : sg1 boiler section diff.
press. [kpa]

```

```

**
*329 cntrlvar 262 * dp5 : sg2 u-tube in. to outlet
dif. p. [kpa]
*330 cntrlvar 263 * dp51 : sg2 inlet plenum dif.
press. [kpa]
*331 cntrlvar 264 * dp526 : sg2 u-tube upflow side
dif. p. [kpa]
*332 cntrlvar 265 * dp5r2 : sg2 boiler section diff.
press. [kpa]
**
*333 cntrlvar 266 * dp6 : sg3 u-tube in. to outlet
dif. p. [kpa]
*334 cntrlvar 267 * dp61 : sg3 inlet plenum diff.
press. [kpa]
*335 cntrlvar 268 * dp626 : sg3 u-tube upflow side
dif. p. [kpa]
*336 cntrlvar 269 * dp6r2 : sg3 boiler section diff.
press. [kpa]
**
*337 cntrlvar 270 * dppl : pressurizer diff. press.
[kpa] ***
**
*338 cntrlvar 271 * intqmb : time integrated break
mass flow [kg]
*339 cntrlvar 274 * intqms1 : time integrated lpsi
mass flow [kg]
*340 cntrlvar 305 * mgv1 : sg1 secondary side mass
invt. [kg]
*341 cntrlvar 405 * mgv2 : sg2 secondary side mass
invt. [kg]
*342 cntrlvar 505 * mgv3 : sg3 secondary side mass
invt. [kg]
*343 cntrlvar 275 * msm2 : accumulator 2 mass
inventory [kg]
*344 cntrlvar 276 * msm3 : accumulator 3 mass
inventory [kg]
**
*345 cntrlvar 277 * p+47 : sg1 steam dome pressure
[mpa]
*346 cntrlvar 278 * p+57 : sg2 steam dome pressure
[mpa]
*347 cntrlvar 279 * p+67 : sg3 steam dome pressure
[mpa]
*348 cntrlvar 280 * p+p : pressurizer top pressure
[mpa]
*349 cntrlvar 281 * p+sm2 : accumulator 2 gas phase
pressure [mpa]
*350 cntrlvar 282 * p+sm3 : accumulator 3 gas phase
pressure [mpa]
**
*351 mflowj 123010000 * qm05 : downcomer mass flow rate
[kg/s]
*352 mflowj 332010000 * qman31 : sg1 feedwater mass flow
rate [kg/s]
*353 mflowj 432010000 * qman32 : sg2 feedwater mass flow
rate [kg/s]
*354 mflowj 532010000 * qman33 : sg3 feedwater mass flow
rate [kg/s]
*355 mflowj 180000000 * qmb : break mass flow rate
[kg/s]
*356 mflowj 311000000 * qmgv11 : sg1 steam line mass flow
rate [kg/s]
*357 mflowj 411000000 * qmgv12 : sg2 steam line mass flow
rate [kg/s]
*358 mflowj 511000000 * qmgv13 : sg3 steam line mass flow
rate [kg/s]

```

```

*359 mflowj 807000000 * qmab12 : lpsi in c12 mass flow
rate [kg/s]
*360 mflowj 907000000 * qmab13 : lpsi in c13 mass flow
rate [kg/s]
**
*361 cntrlvar 283 * sebreak : break specific enthalpy
[kj/kg]
**
*362 tempf 123010000 * tf012a : core inlet temperature
[k]
*363 tempf 141010000 * tf0304 : core outlet temperature
[k]
*364 tempf 151010000 * tf041 : upper head (bottom)
temperature [k]
*365 tempf 153010000 * tf042 : upper head (top)
temperature [k]
*366 tempf 602010000 * tf112 : hot leg 1 temperature
[k]
*367 tempf 656050000 * tf133 : cold leg 1 temperature
[k] * R+
*368 tempf 802010000 * tf212 : hot leg 2 temperature
[k]
*369 tempf 856010000 * tf233 : cold leg 2 temperature
[k] * R+
*370 tempf 902020000 * tf312 : hot leg 3 temperature
[k] * R+
*371 tempf 956010000 * tf333 : cold leg 3 temperature
[k] * R+
*372 tempf 309050000 * tf454c : bottom of sg1 downcomer
temperature [k]
*373 tempf 409050000 * tf554c : bottom of sg2 downcomer
temperature [k]
*374 tempf 509050000 * tf654c : bottom of sg3 downcomer
temperature [k]
**
*375 htemp 131000701 * ts02091 :
*376 htemp 131000801 * ts02151 :
*377 htemp 131000901 * ts02191 : rod temperature from
middle to
*378 htemp 131001001 * ts02201 : top core elevation [k]
*379 htemp 131001101 * ts02241 : ** ts = ? (le omemba v
tab.1 str.28/87)
*380 htemp 131001201 * ts02281 :
*381 cntrlvar 146 * tmax : max. clad temperature
[k]
**
*382 cntrlvar 286 * vp1 : pump 1 rotation speed
[rpm]
*383 cntrlvar 287 * vp2 : pump 2 rotation speed
[rpm]
*384 cntrlvar 288 * vp3 : pump 3 rotation speed
[rpm]
**
*385 cntrlvar 289 * w+02 : core (electrical) power
[kw]
*386 cntrlvar 290 * w+trac : trace heating [kw]
**
*387 cntrlvar 110 * zt0200 : core level [m]
*388 cntrlvar 291 * zscore : swollen level [m]
***
*
*389 dt 0 * dtcalc : time step along
transient [s]
*390 emass 0 * mer : mass error [kg]
**
**

```

```

*****
* comparison report variables request
*
301 cntrlvar 280 * p1p : PRESSURIZER TOP PRESSURE
[mpa]
302 cntrlvar 278 * p=57 : #92 STEAM DOME PRESSURE
[mpa]
303 cntrlvar 163 * zt0200 : CORE COLLAPSED LIQUID
LEVEL [m]
* 304 temp99 131120000 * tf03046 : CORE OUTLET STEAM
TEMPERATURE [K]
304 temp99 141010000 * tf03046 : CORE OUTLET STEAM
TEMPERATURE [K]
305 cntrlvar 146 * tmax : MAX CLAD WALL
TEMPERATURE [K]
* 306 void99 656010000 * alb1f : c11 SPOOL PIECE VOID
FRACTION [ ]
306 void99 656070000 * alb1f : c11 SPOOL PIECE VOID
FRACTION [ ]
307 mflow 180000000 * qmb : BREAK M'S FLOW RATE
[KG/S]
308 cntrlvar 405 * msv2 : #92 SECONDARY SIDE MASS
INVT. [KG]
309 cntrlvar 170 * mcp : PRIMARY MASS INVENTORY
[KG]
*
310 cntrlvar 271 * intqmb : BREAK DISCHARGED MASS
[KG]
*
313 cntrlvar 110 * zt0200 : SIMPL. CORE COLLAPSED
LIQUID LEVEL [m]
*****
* expanded minor edit requests
20800001 satbf 182010000 * liquid spec. enthalpy at sat.
cond. [J/Kg]
20800002 satbg 182010000 * vapor spec. enthalpy at sat.
cond. [J/Kg]
*
20800003 httemp 131000105 * cladding temperatures [K] (m.p.
5.)
20800004 httemp 131000205 *
20800005 httemp 131000305 *
20800006 httemp 131000405 *
20800007 httemp 131000505 *
20800008 httemp 131000605 *
20800009 httemp 131000705 *
20800010 httemp 131000805 *
20800011 httemp 131000905 *
20800013 httemp 131001005 *
20800014 httemp 131001105 *
20800015 httemp 131001205 *
*
20800016 dt 0 * the current time step [s]
*
*****
* control variables for requested minor edit
*
ccvv

```

```

*****
* dp * p(low pressure tap) - p (high pressure tap)
*
* cv 240: dp0200: core heat. length diff. press. [kpa]
20524000 dp0200 sum 1.0e-03 0.0 1
20524001 0.0 1.0 p 123010000 -1.0 p 141010000 2.531 rho
131070000
* korekcija: 0.258*9.81=2.531
*
* cv 241: dpup1 : upper plenum diff. press. [kpa]
20524100 dpup1 sum 1.0e-03 0.0 1
20524101 0.0 1.0 p 141010000 -1.0 p 147010000 13.400 rho
143010000
* korekcija: 1.366*9.81=13.400
*
* cv 242: dp034 : guide tube dif. press. [kpa] ** ni opisa v
bazi
20524200 dpup1 sum 1.0e-03 0.0 1
20524201 0.0 1.0 p 141010000 -1.0 p 153010000
*
* cv 243: dpthead : upper head diff. press. [kpa]
20524300 dpup1 sum 1.0e-03 0.0 1
20524301 0.0 1.0 p 151010000 -1.0 p 153010000 5.582 rho
151010000
* korekcija: 0.569*9.81=5.582
*
* cv 244: dp050: downcomer to upp. head dif. press. [kpa]
20524400 dp050 sum 1.0e-03 0.0 1
20524401 0.0 1.0 p 111010000 -1.0 p 151010000 -3.267 rho
111010000
* korekcija: -0.333*9.81=-3.267
*
* cv 245: dp0r1: pressure vessel dif. press. [kpa]
20524500 dp0r1 sum 1.0e-03 0.0 1
20524501 0.0 1.0 p 123010000 -1.0 p 153010000 5.150 rho
131070000
* korekcija: 0.525*9.81=5.150
*
* cv 246: dp1: c11 to h11 diff. press. [kpa]
20524600 dp1 sum 1.0e-03 0.0 1
20524601 0.0 1.0 p 656090000 -1.0 p 603010000 * R+
*
* cv 247: dp12pg: pump 1 diff. press. [kpa]
20524700 dp12pg sum 1.0e-03 0.0 1
20524701 0.0 1.0 p 1.0 p 624 -1.0 p 655010000
*
* cv 248: dp12vg: loop seal 1 downflow side diff. press. [kpa]
20524800 dp12vg sum 1.0e-03 0.0 1
20524801 0.0 1.0 p 1.0 p 623 -1.0 p 622
*
* cv 249: dp12vp: loop seal 1 upflow side diff. press. [kpa]
20524900 dp12vp sum 1.0e-03 0.0 1
20524901 0.0 1.0 p 623 -1.0 p 624
*
* cv 250: dp2: c12 to h12 diff. press. [kpa]
20525000 dp2 sum 1.0e-03 0.0 1
20525001 0.0 1.0 p 856050000 -1.0 p 803010000 * R+
*
* cv 251: dp22pg: pump 2 diff. press. [kpa]
20525100 dp22pg sum 1.0e-03 0.0 1
20525101 0.0 1.0 p 1.0 p 824 -1.0 p 855010000

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* cv 252: dp22vg: loop seal 2 downflow side diff. press. [kpa]
20525200 dp22vg sum 1.0e-03 0.0 1
20525201 0.0 1.0 p 823 -1.0 p 822
*
* cv 253: dp22vp: loop seal 2 upflow side diff. press. [kpa]
20525300 dp22vp sum 1.0e-03 0.0 1
20525301 0.0 1.0 p 823 -1.0 p 824
*
* cv 254: dp3: c13 to h13 diff. press. [kpa]
20525400 dp3 sum 1.0e-03 0.0 1
20525401 0.0 1.0 p 956050000 -1.0 p 903010000 * R+
*
* cv 255: dp32pg: pump 3 diff. press. [kpa]
20525500 dp32pg sum 1.0e-03 0.0 1
20525501 0.0 1.0 p 924 -1.0 p 955010000
*
* cv 256: dp32vg: loop seal 3 downflow side diff. press. [kpa]
20525600 dp32vg sum 1.0e-03 0.0 1
20525601 0.0 1.0 p 923 -1.0 p 922
*
* cv 257: dp32vp: loop seal 3 upflow side diff. press. [kpa]
20525700 dp32vp sum 1.0e-03 0.0 1
20525701 0.0 1.0 p 923 -1.0 p 924
*
* cv 258: dp4: sg1 u-tube in. to outlet diff. press. [kpa]
20525800 dp4 sum 1.0e-03 0.0 1
20525801 0.0 -1.0 p 301010000 1.0 p 31010000 * R+
*
* cv 259: dp41: sg1 inlet plenum diff. press. [kpa]
20525900 dp41 sum 1.0e-03 0.0 1
20525901 0.0 1.0 p 620 -1.0 p 301010000
*
* cv 260: dp426: sg1 u-tube upflow side diff. p. [kpa]
20526000 dp426 sum 1.0e-03 0.0 1
20526001 0.0 1.0 p 301010000 -1.0 p 521
*
* cv 261: dp4r2: sg1 boiler section diff. press. [kpa]
20526100 dp4r2 sum 1.0e-03 0.0 1
20526101 0.0 1.0 p 306010000 -1.0 p 310020000
*
* cv 262: dp5: sg2 u-tube in. to outlet diff. press. [kpa]
20526200 dp5 sum 1.0e-03 0.0 1
20526201 0.0 -1.0 p 401010000 1.0 p 41010000 * R+
*
* cv 263: dp51: sg2 inlet plenum diff. press. [kpa]
20526300 dp51 sum 1.0e-03 0.0 1
20526301 0.0 1.0 p 820 -1.0 p 401010000
*
* cv 264: dp526: sg2 u-tube upflow side diff. p. [kpa]
20526400 dp526 sum 1.0e-03 0.0 1
20526401 0.0 1.0 p 401010000 -1.0 p 821
*
* cv 265: dp5r2: sg2 boiler section diff. press. [kpa]
20526500 dp5r2 sum 1.0e-03 0.0 1
20526501 0.0 1.0 p 408010000 -1.0 p 410020000
*
*
* cv 266: dp6: sg1 u-tube in. to outlet diff. press. [kpa]
20526600 dp6 sum 1.0e-03 0.0 1
20526601 0.0 -1.0 p 501010000 1.0 p 513010000 * R+
*
* cv 267: dp61: sg1 inlet plenum diff. press. [kpa]
20526700 dp61 sum 1.0e-03 0.0 1

```

```

2052701 0.0 1.0 cntrlvar 9.0 -1.0 p 501010000
* cv 268: dp626: sg3 u-tube upflow side diff. p. [kpa]
2052600 dp626 sum 1.0e-03 0.0 1
20526801 0.0 1.0 p 501010000 -1.0 cntrlvar 284 1.0 mathf 182010000 -1.0
cntrlvar 285
* cv 269: dp6r2: sg3 boiler section diff. press. [kpa]
20526900 dp6r2 sum 1.0e-03 0.0 1
20526901 0.0 1.0 p 506810000 -1.0 p 510020000
* cv 270: dp6l1: pressurizer diff. press. [kpa]
20527000 dp6l1 sum 1.0e-03 0.0 1
20527001 0.0 1.0 p 203010000 -1.0 p 203100000
* cv 271: intgmb: time integrated break mass flow [kg]
20527100 intgmb integral 1.0 0.0 0 1 0.0
20527101 mflowj 180900000
* cv 272: intsi2: time integrated lpsi 2 mass flow [kg]
20527200 intsi2 integral 1.0 0.0 0 1 0.0
20527201 mflowj 807000000
* cv 273: intsi3: time integrated lpsi 2 mass flow [kg]
20527300 intsi3 integral 1.0 0.0 0 1 0.0
20527301 mflowj 907000000
* cv 274: intsi23: time integrated lpsi 2+3 mass flow [kg]
20527400 intsi23 sum 1.0 0.0 0 1 0.0
20527401 0.0 1.0 cntrlvar 272 1.0 cntrlvar 273
* cv 275: nsm2: accumulator 2 mass inventory [kg]
20527500 nsm2 mult 1.0 0.0 1
20527501 acvliq 911. rhof 833010000
* cv 276: nsm3: accumulator 3 mass inventory [kg]
20527600 nsm3 mult 1.0 0.0 1
20527601 acvliq 933 rhof 933010000
* cv 277: p+47: sg1 steam dome pressure [mpa]
20527700 p+47 sum 1.0e-06 0.0 1
20527701 0.0 1.0 p 310020000
* cv 278: p+57: sg2 steam dome pressure [mpa]
20527800 p+57 sum 1.0e-06 0.0 1
20527801 0.0 1.0 p 410020000
* cv 279: p+67: sg3 steam dome pressure [mpa]
20527900 p+67 sum 1.0e-06 0.0 1
20527901 0.0 1.0 p 510020000
* cv 280: p+p: pressurizer top pressure [mpa]
20528000 p+p sum 1.0e-06 0.0 1
20528001 0.0 1.0 p 203100000
* cv 281: p+sm2: accumulator 2 gas phase pressure [mpa]
20528100 p+sm2 sum 1.0e-06 0.0 1
20528101 0.0 1.0 p 833010000
* cv 282: p+sm3: accumulator 3 gas phase pressure [mpa]
20528200 p+sm3 sum 1.0e-06 0.0 1
20528201 0.0 1.0 p 933010000
* cv 283: sebreak: break specific enthalpy [kj/kg] ***
h = x*stg + (1-x)*seathf
20528300 sebreak sum 1.0e-03 0.0 1
20528301 0.0 1.0 cntrlvar 284 1.0 mathf 182010000 -1.0
cntrlvar 285
* cv 284: x*stg [j/kg]
20528400 bvaph mult 1.0 0.0 1
20528401 quals 182010000 stgth 182010000
* cv 285: x*stghe [j/kg]
20528500 bliqh mult 1.0 0.0 1
20528501 quals 182010000 stghf 182010000
* cv 295: sebreak: break specific enthalpy [kj/kg] ***
u = x*ug + (1-x)*ul
h = u + p/rho
20529500 sebreak sum 1.0e-03 0.0 1
20529501 0.0 1.0 cntrlvar 298 1.0 cntrlvar 299
* cv 296: x*ug [j/kg]
20529600 bvapu mult 1.0 0.0 1
20529601 quals 182010000 ug 182010000
* cv 297: x*ul [j/kg]
20529700 bliqu mult 1.0 0.0 1
20529701 quals 182010000 ul 182010000
* ^: ^g: u = x*ug + (1-x)*ul [j/kg]
-0529800 - sum 1.0 0.0 1
20529801 0.0 1.0 cntrlvar 296 :.0 uf 182010000 -1.0
cntrlvar 297
* cv 299: p/rho [j/kg]
20529900 bliqu div 1.0 0.0 1
20529901 rho 182010000 p 182010000
* cv 286: vp1_rump 1 rotation speed [rpm]
20528600 vp1 mult 9.5493 0.0 1
20528601 pmprel 701
* cv 287: vp2 pump 2 rotation speed [rpm]
20528700 vp2 mult 9.5493 0.0 1
20528701 pmpvel 702
* cv 288: vp3 pump 3 rotation speed [rpm]
20528800 vp3 mult 9.5493 0.0 1
20528801 pmpvel 703
* cv 289: w+02: core power [kw]
20528900 w+02 function 1.0e-03 0.0 1
20528901 time 0 100
* cv 290: w+trac: trace heating [kw]
20529000 w+trac function 1.0e-03 0.0 1
20529001 time 0 102
20310200 power 670 * accum. injection
20310201 -1.0 107.5e+03
20310202 0.0 107.5e+03
20310203 1.0 0.0e+03
* cv 291: zscore: swollen level [m] ***

```

```

20529100 zscore constant 0.0
* ttrr
* break
501 time 0 gt null 0 1000.0 n * break
603 -501 or -501
break
503 p 203090000 lt null 0 131.0e+05 n * scream
signal
505 p 203090000 lt null 0 119.0e+05 n * si
signal
515 time 0 gt timeof 505 30.0 n * aux.
feed on
520 p 203090000 lt null 0 41.6e+05 n * accum.
injection
loops only 2.3
521 p 203090000 lt null 0 14.6e+05 n *
accum.isolation
526 cntrlvar 146 gt null 0 733.0 i *
ultimate procedure
527 time 0 gt timeof 505 30.0 n * afw
actuation on si
626 527 and -526 n * afw: on si and before ultimate
procedure
657 -521 or -521 n * prz pressure gt 14.6 bar
659 520 and 657 n * accumulator open trip
670 659 or 659 i * trace heating off --> heat losses
* rrxccv
* rrxccvv r x c n t r o l v a r i a b l e s
* cv 100: core bypass inventory mass [kg] bbb
20510000 coremass sum 1 0-3 0 1
20510001 0.0 7.5047 rho 133010000 3.6955 rho 133020000 *
c-bypass
20510002 3.6955 rho 133030000 3.6955 rho 133040000
20510003 3.6955 rho 133050000 3.6955 rho 133060000
20510004 3.6955 rho 133070000 3.6955 rho 133080000
20510005 3.6955 rho 133090000 3.6955 rho 133100000
20510006 3.6955 rho 133110000 7.5047 rho 133120000
* cv 101: core inventory mass [kg]
20510100 coremass sum 1.0-3 0 1

```

```

20510101 0.0 22.5984 rho 131010000 11.1280 rho 131020000 *
core
20510102 11.1280 rho 131030000 11.1280 rho 131040000
20510103 11.1280 rho 131050000 11.1280 rho 131060000
20510104 11.1280 rho 131070000 11.1280 rho 131080000
20510105 11.1280 rho 131090000 11.1280 rho 131100000
20510106 11.1280 rho 131110000 22.5984 rho 131120000
*
* ctv 102: reactor vessel inventory mass (kg)
20510200 vessmass sum 1.0-3 0. 1
20510201 0.0 20.2492 rho 111010000
*
upp.downc.
20510202 14.4648 rho 113010000 14.4648 rho 115010000 *
core inlet
20510203 14.4648 rho 117010000
*
core inlet
* ddd ++ art.
20510204 31.9369 rho 119010000 31.9369 rho 119050000 *
downcommer
20510205 31.9369 rho 119070000
*
downcommer
20510206 18.3410 rho 119100000 27.9758 rho 119140000 *
downcommer
*
20510207 65.9122 rho 121010000 87.3224 rho 123010000 *
low.head+plen.
20510208 68.3618 rho 125010000
*
core inlet
20510209 1000.0000 cntrlvar 101
core
*
20510210 1000.0000 cntrlvar 100
c.bypass hbb
20510211 69.9396 rho 141010000 98.7564 rho 143010000 *
upp.plen.
20510212 9.2280 rho 145010000
*
guide tube
20510213 110.1513 rho 147010000
*
upp.plen.
20510214 75.1800 rho 151010000 49.9430 rho 153010000 *
upp.head
*
* ctv 110: core level (m)
20511000 corelevl sum 1.0 0. 1
20511001 0.0 .528 voidf 131010000 0.26 voidf 131020000 0.26
voidf 131030000
20511002 0.26 voidf 131040000 0.26 voidf 131050000 0.26
voidf 131060000
20511003 0.26 voidf 131070000 0.26 voidf 131080000 0.26
voidf 131090000
20511004 0.26 voidf 131100000 0.26 voidf 131110000 .528
voidf 131120000
*
* ctv 111: reactor vessel level (m)
20511100 vesslevl sum 1.0 0. 1
20511101 0.0 0.4 voidf 121010000 0.6 voidf 123010000 1.164
voidf 125010000
20511102 1.0 cntrlvar 110
20511103 .8245 voidf 141010000 1.127 voidf 143010000 2.155
voidf 147010000
20511104 4545 voidf 153010000
*
* ctv 120: reactor power (kw)
20512000 rktpower sum 1.0-3 2864. 1
20512001 0.0 1.0 q 131010000 1.0 q 131020000 1.0 q 131030000
20512002 1.0 q 131040000 1.0 q 131050000 1.0 q 131060000
20512003 1.0 q 131070000 1.0 q 131080000 1.0 q 131090000

```

```

20512004 1.0 q 131100000 1.0 q 131110000 1.0 q 131120000
20512005 1.0 q 133010000
*
* ctv 146: maxl.am htemp rx core, left surface
20514600 maxrxt stdfnctn 1.0 600. 1
20514601 max htemp 131000105 htemp 131000205
20514602 htemp 131000305 htemp 131000405
20514603 htemp 131000505 htemp 131000605
20514604 htemp 131000705 htemp 131000805
20514605 htemp 131000805 htemp 131001005
20514606 htemp 131000905 htemp 131001205
*
*
*****
*
*
* rrx reactor vessel
*
*
*****
*
* region 110: vessel inlet part + downcommer (upper + lower)
*
*****
*
* * component 111: upper downcommer - upper head connection
* 1110000 dc-uphea branch
* 1110001 0
* 1110101 0. 4.09485 41.9464-3 0. 90. 2.1049 5.-5 5.693-2 00
* * geom v25-33+(v34+v35+v36del)/2
*
*****
*
* **** nov model bypass v glav0
* v34:
1100000 v34 branch
1100001 1 1
1100101 0.0 0.4635 21.7085e-03 0.0 90.0 0.4635 5.-5
0.250 00
1100200 100 1.58645e+07 1.24844e+06 2.43927e+06 0.00000e+00
* 1101101 110010000 111000000 1.901e-03 0.1 1.0 130000
* ++ ENTR MODEL
1101101 110010000 111000000 1.901e-03 0.1 1.0 110000 *
fff
1101201 2.13960e+00 2.13960e+00 0.00000e+00
*
* v31-v26 upper downcommer - upper head connection
1110000 dc-uphea branch
1110001 0
1110101 1.901e-03 3.1314 0.0 0.0 18. 1.1414 5.-5 0.0492
00
1110200 100 1.58559e+07 1.24844e+06 2.43948e+06 0.00000e+00
*
* v25:
1120000 v25 branch
1120001 1 1
1120101 0.0 0.5 13.055e-03 0.0 90.0 0.5 5.-5 0.170 00
1120200 100 1.58487e+07 1.24844e+06 2.4395e+06 0.00000e+00

```

```

1121101 111010000 112000000 1.901e-03 1.0 0.1 130000 *
++ ENTR MODEL
1121201 2.13960e+00 2.13960e+00 0.00000e+00
*
* component 152: bypass into vessel head
1570000 headbyps valve * angljun
* 1520101 112010000 151000000 2.454-4 0. 0. 100000 * geom j2b
1520101 112010000 151000000 2.454-4 0. 0. 100000 * geom j25 *
fff
1520110 0.017 0.0 1.0 1.0
1520300 grvvlv
1520301 152
1520401 0.01 0.1 0.1
1520402 1.0 33.0 33.0
*
* ccci : ctv 152: flow regulation into vessel head
20515200 valve152 sum 1. 0.2956 0 3 0.01 1.
20515201 0.0306 -0.01 mflowj 152000000 1.0 cntrlvar 152
*
*****
*
* component 113: vessel inlet (1 of 3)
1130000 vess-in1 branch
1130001 3
*
geom
(v34+v35+v36del)/6
1130101 0. 0.4635 7.2324-3 0. -90. -0.4635 5.-5 123.47-3 00
* 1131101 113000000 111000000 1.5612-2 2.1 2.1 130000 * geom
j35/3
1131101 113000000 110000000 1.5612-2 2.1 2.1 110000 * geom
j35/3 * **** fff
1132101 113010000 119000000 1.5612-2 0.3 0.3 130000 * geom
j35/3
1133101 656010000 113000000 1.09358-2 1. 1. 130000 * geom
j340
*
* component 115: vessel inlet (2 of 3)
1150000 vess-in2 branch
1150001 3
*
geom
(v34+v35+v36del)/6
1150101 0. 0.4635 7.2324-3 0. -90. -0.4635 5.-5 123.47-3 00
* 1151101 115000000 111000000 1.5612-2 2.1 2.1 130000 * geom
j35/3
1151101 115000000 110000000 1.5612-2 2.1 2.1 110000 * geom
j35/3 * **** fff
1152101 115010000 119000000 1.5612-2 0.3 0.3 130000 * geom
j35/3
1153101 856010000 115000000 1.09358-2 1. 1. 130000 * geom
j340
*
* component 117: vessel inlet (3 of 3)
1170000 vess-in3 branch
1170001 3
*
geom
(v34+v35+v36del)/6
1170101 0. 0.4635 7.2324-3 0. -90. -0.4635 5.-5 123.47-3 00
* 1171101 117000000 111000000 1.5612-2 2.1 2.1 130000 * geom
j35/3
1171101 117000000 110000000 1.5612-2 2.1 2.1 110000 * geom
j35/3 * **** fff
1172101 117010000 119000000 1.5612-2 0.3 0.3 130000 * geom
j35/3
1173101 956010000 117000000 1.09358-2 1. 1. 130000 * geom
j340

```

1260401 0.01 0.1 0.1 0.1  
 1260402 1.0 33.0 33.0  
 \* cccl: cvt 126: flow regulation into core bypass  
 20512600 valve126 sum 1.0 6491 0 3 0 1  
 20512601 0.045 -0.01 mflowj 12600000 1.0 cntrlvar 126  
 \* region 130: core + core bypass  
 \* component 131: core  
 1310000 core pipe  
 1310001 12  
 1310101 4.28-2 12 \* geom j6+j7+j8  
 1310301 0.528 1 0.26 11 0.528 12 \* geom v7  
 1310601 90 12  
 1310801 5.-5 11.3-3 12 \* geom j6+j7+j8  
 1310901 0.1 0.1 11  
 1311001 00100 12  
 1311101 100000 11  
 1311401 0.0113 0.0 1.0 1.0 11  
 \* component 133: core bypass \* bbb  
 1330000 corebyps englvol  
 1330101 0.3 656 51.9532-3 0.90 3 656 5.-5 24.7-3 00 \* geom  
 v50(del)  
 1330000 corebyps pipe \* bbb  
 1330001 12  
 1330101 0.01421 12  
 1330301 0.528 1 0.26 11 0.528 12  
 1330601 90 12  
 1330801 5.-5 24.7-3 12  
 1330901 0.0 0.0 11  
 1331001 00000 12  
 1331101 -00000 11  
 1331401 24.7-3 0.0 1.0 1.0 11  
 \* component 143: upper plenum  
 1430000 aro-uppl branch  
 1430001 1  
 1430101 0.2 7185 159.3263-3 0.90 2 7185 5.-5 1.-1 00 \* geom  
 v12(del)-v19  
 1431101 143010000 147000000 0.0 0.0 130000 \*(geom j14)  
 1471101 143010000 147000000 0.0 0.0 110000 \*(geom j14)  
 \* component 147: upper plenum  
 1470000 upper-pl branch  
 1470001 1  
 1470101 0.2 7185 159.3263-3 0.90 2 7185 5.-5 1.-1 00 \* geom  
 v12(del)-v19  
 1471101 143010000 147000000 0.0 0.0 130000 \*(geom j14)  
 \* component 151: upper head (lower part, around upper plenum)  
 1510000 aro-uppl branch  
 1510001 1  
 1510101 0.0 9035 75.1799-3 0.90 0 9035 5.-5 0.17 00 \* geom  
 v23(del)-v24  
 1511101 151010000 153000000 7.878-2 0.0 130000 \* geom j23  
 or j24  
 1511101 151010000 153000000 7.878-2 0.0 110000 \* geom j23 or  
 j24 \* fff  
 1511110 0.017 0.0 1.0 1.0  
 \* component 152: bypass into vessel head  
 1520000 headbyps valve \* sngljun  
 1520101 111010000 151000000 2.454-4 0.0 100000 \* geom j25  
 1520110 0.017 0.0 1.0 1.0  
 1520300 srwlv  
 1520301 152  
 1520401 0.01 0.1 0.1  
 1520402 1.0 33.0 33.0  
 \* cccl: cvt 152: flow regulation into vessel head  
 20515200 valve152 sum 1.0 2956 0 3 0.01 1  
 20515201 0.0306 -0.01 mflowj 152000000 1.0 cntrlvar 152

1260401 0.01 0.1 0.1 0.1  
 1260402 1.0 33.0 33.0  
 \* cccl: cvt 126: flow regulation into core bypass  
 20512600 valve126 sum 1.0 6491 0 3 0 1  
 20512601 0.045 -0.01 mflowj 12600000 1.0 cntrlvar 126  
 \* region 130: core + core bypass  
 \* component 131: core  
 1310000 core pipe  
 1310001 12  
 1310101 4.28-2 12 \* geom j6+j7+j8  
 1310301 0.528 1 0.26 11 0.528 12 \* geom v7  
 1310601 90 12  
 1310801 5.-5 11.3-3 12 \* geom j6+j7+j8  
 1310901 0.1 0.1 11  
 1311001 00100 12  
 1311101 100000 11  
 1311401 0.0113 0.0 1.0 1.0 11  
 \* component 133: core bypass \* bbb  
 1330000 corebyps englvol  
 1330101 0.3 656 51.9532-3 0.90 3 656 5.-5 24.7-3 00 \* geom  
 v50(del)  
 1330000 corebyps pipe \* bbb  
 1330001 12  
 1330101 0.01421 12  
 1330301 0.528 1 0.26 11 0.528 12  
 1330601 90 12  
 1330801 5.-5 24.7-3 12  
 1330901 0.0 0.0 11  
 1331001 00000 12  
 1331101 -00000 11  
 1331401 24.7-3 0.0 1.0 1.0 11  
 \* component 143: upper plenum  
 1430000 aro-uppl branch  
 1430001 1  
 1430101 0.2 7185 159.3263-3 0.90 2 7185 5.-5 1.-1 00 \* geom  
 v12(del)-v19  
 1431101 143010000 147000000 0.0 0.0 130000 \*(geom j14)  
 1471101 143010000 147000000 0.0 0.0 110000 \*(geom j14)  
 \* component 147: upper plenum  
 1470000 upper-pl branch  
 1470001 1  
 1470101 0.2 7185 159.3263-3 0.90 2 7185 5.-5 1.-1 00 \* geom  
 v12(del)-v19  
 1471101 143010000 147000000 0.0 0.0 130000 \*(geom j14)  
 \* component 151: upper head (lower part, around upper plenum)  
 1510000 aro-uppl branch  
 1510001 1  
 1510101 0.0 9035 75.1799-3 0.90 0 9035 5.-5 0.17 00 \* geom  
 v23(del)-v24  
 1511101 151010000 153000000 7.878-2 0.0 130000 \* geom j23  
 or j24  
 1511101 151010000 153000000 7.878-2 0.0 110000 \* geom j23 or  
 j24 \* fff  
 1511110 0.017 0.0 1.0 1.0  
 \* component 152: bypass into vessel head  
 1520000 headbyps valve \* sngljun  
 1520101 111010000 151000000 2.454-4 0.0 100000 \* geom j25  
 1520110 0.017 0.0 1.0 1.0  
 1520300 srwlv  
 1520301 152  
 1520401 0.01 0.1 0.1  
 1520402 1.0 33.0 33.0  
 \* cccl: cvt 152: flow regulation into vessel head  
 20515200 valve152 sum 1.0 2956 0 3 0.01 1  
 20515201 0.0306 -0.01 mflowj 152000000 1.0 cntrlvar 152

\* component 119: downcomer  
 1190000 downcom pipe  
 1190001 5  
 1190101 0.5  
 1190301 1.348833 3 0.779367 4 1.054 5 \* geom  
 v06del+v37+v38-39+v40  
 1190401 31.9457-3 18.341-3 4 27.9758-3 5 \* geom  
 v16del+v37+v38-39+v40  
 1190501 -90 3 -39.3 4 -90 5  
 1190701 -1.348833 3 -0.49405 4 -0.95406 5  
 1190801 5.-5 0.18 1 5.-5 0.1731 4 5.-5 0.045 5 \* geom j37-  
 j40+j41  
 1190901 0.0 2 0.83 0.83 4  
 1191001 0.5  
 1191101 100000 4  
 \* component 119: downcomer ddd  
 1190000 downcom pipe  
 1190001 14  
 1190101 2.36-2 13 2.65-2 14  
 1190301 0.6746 1 0.528 2 0.26 12 0.528 13 1.1640 14  
 1190601 -90 14 \* \*\* appr.  
 1190801 5.-5 0.18 1 5.-5 0.1731 13 5.-5 0.045 14  
 1190901 0.0 12 0.83 0.83 13  
 1191001 0.14  
 1191101 100000 13  
 \* region 120: vessel bottom + lower plenum + core inlet  
 \* component 121: bottom of reactor  
 1210000 botmden englvol  
 1210101 0.0 0.4 65.9322-3 0.90 0.0 4 5.-5 44.8493-3 00 \* geom  
 v1  
 \* component 123: lower plenum  
 1230000 lower-pl branch  
 1230001 3  
 1230101 0.0 6 87.3224-3 0.90 0.0 6 5.-5 36.44-3 00 \* geom  
 v2+v3+v4  
 1231101 119010000 123010000 2.6543-2 0.0 00000 \* geom  
 j41  
 1231101 119010000 123010000 2.6543-2 2.8 2.8 130000 \* geom  
 j41 + dddaten k  
 1232101 123010000 125000000 5.8910-2 1.8 1.8 130000 \* geom j5  
 1233101 123010000 123000000 16.2858-2 0.0 130000 \* geom j2  
 1231110 0.045 0.0 1.0 1.0  
 \* component 125: core inlet  
 1250000 coreinit branch  
 1250001 1  
 1250101 0.1 164 68.3618-3 0.90 1.164 5.-5 15.8743-3 00 \*  
 geom v5+v6+v50(del)  
 1251101 125010000 131000000 4.28-2 0.0 130000 \* geom j6  
 \* component 126: core bypass inlet junction  
 1260000 intrbyps valve \* sngljun  
 1260101 125010000 131000000 0.2143-2 0.0 100000 \* geom j50  
 1260110 0.0147 0.0 1.0 1.0  
 1260300 srwlv  
 1260301 126



```

1110301 0.1 1. 3 0. 5
1110401 570. 6
1110501 0 0 0 0. 0 12
1110601 134010000 0 1 1 225.384 3 * +0.528*428
1110701 134020000 100*0 1 1 111.28 11 * -0.26 *428
1110801 131120000 0 1 1 225.384 12 * +0.528*428
1110901 100 0.0766824 0 0 1
1111001 100 0.0490314 0 0 2
1111101 100 0.0682176 0 0 3
1111201 100 0.0874038 0 0 4
1111301 100 0.1051688 0 0 5
1111401 100 0.1136950 0 0 6
1111501 100 0.1136950 0 0 7
1111601 100 0.1051688 0 0 8
1111701 100 0.0682176 0 0 9
1111801 100 0.0490314 0 0 10
1111901 100 0.0490314 0 0 11
1112001 100 0.0766824 0 0 12
1112101 0.011875 10. 10. 0. 0. 0. 1. 12
*
* tab.100: scram table
20210000 power 503 * power versus time
20210001 -1.0 2864.0+3 0.0 2864.0+3 17.0
2864.0+3
20210002 17.6 2720.0+3 19.0 2578.0+3 21.5
2434.0+3
20210003 24.0 2290.0+3 26.8 2148.0+3 29.7
2005.0+3
20210004 32.6 1862.0+3 36.0 1750.0+3 44.0
1550.0+3
20210005 52.0 1385.0+3 63.0 1265.0+3 74.0
1170.0+3
20210006 84.0 1110.0+3 94.0 1050.0+3 104.0
950.0+3
20210007 123.0 964.0+3 153.0 906.0+3 198.0
854.0+3
20210008 273.0 812.0+3 373.0 750.0+3 423.0
725.0+3
20210009 523.0 706.0+3 673.0 680.0+3 723.0
562.0+3
20210010 823.0 647.0+3 923.0 629.0+3 1923.0
510.0+3
20210011 3123.0 439.0+3 5123.0 380.0+3 7123.0
340.0+3
20210012 9123.0 324.0+3 18123.0 271.0+3
*
*****
* hbms reactor vessel heat structures - passive
*****
*
* upper downcomer
1110000 1 3 2 1 0.021659
1110100 0 1
1110200 2 0.0434
1110301 2
1110301 0 2
1110401 560. 3
1110501 111010000 0 1 1 3.61135 1
1110601 0 0 1 3.61135 1
1110701 0 0. 0. 1
1110801 0 10. 10. 0. 0. 0. 0. 1. 1
*

```

```

* vessel inlet (cold leg connection)
1113000 3 3 2 1 0.123786
1113100 0 1
1113200 2 0.163047
1113301 1 2
1113301 0 2
1113301 0 2
1113401 560. 3
1113501 111010000 2000000 1 1 0.309 3 * 0.927/3=0.309
1113601 0
1113701 0 0. 0. 0. 3 0 1 0.309 3
*
1113801 0 10. 10. 0. 0. 0. 0. 1. 3
*
* trefoil shaped piece
1113100 3 3 1 0.
1113100 0 1
1113101 2 6.-3
1113201 1 2
1113301 0 2
1113401 560. 3
1113501 111010000 2000000 1 1 0.11 3
1113601 111010000 2000000 1 1 0.11 2
1113701 111010000 2000000 1 1 0.11 3
1113801 0 0. 0. 0. 0. 3 0 1 0.11 3
1113901 0 10. 10. 0. 0. 0. 0. 1. 3
1114001 10. 10. 0. 0. 0. 0. 1. 3
*
* downcomer (upper part): bh11 * ddd
1119000 13 3 2 1 86.1805.-3
1119100 0 1
1119200 2 110.8785.-3
1119301 1.0 2
1119401 560. 3
1119501 119010000 0 1 1 0.6746 1
1119601 0 0 1 0.5280 2
1119701 10223 0.0714 0. 0. 11
1119801 0 10. 10. 0. 0. 0. 0. 1. 13
1190601 0 0 1 0.6746 1
1190602 0 0 1 0.5280 2
1190603 0 0 1 0.2500 12
1190604 0 0 1 0.5280 13
1190701 10223 0.0714 0. 0. 11
1190801 0 10. 10. 0. 0. 0. 0. 1. 13
*
* downcomer (lower part): bh11 * ddd
11191000 13 3 2 1 0.158778
11191100 0 1
11191101 2 0.236226
11191201 1 2
11191301 1.0 2
11191401 563. 3
11191501 119140000 0 1 1 1.164 1
1191501 0 0 1 1.164 1
1191701 10223 0.0714 0. 0. 1
1191801 0 10. 10. 0. 0. 0. 0. 1. 1
*
* Bottom Head
1121000 13 3 2 1 0.249359
11210100 0 1
11210101 2 0.322224
11210201 1 2
11210301 0 2
11210401 560. 3
11210501 121010000 0 1 1 0.4 1
11210601 0 0 1 0.4 1
11210701 0 0. 0. 0. 1
*

```

```

11210801 0. 10. 10. 0. 0. 0. 0. 1. 1
*
* reactor core: 428 heater rods - inactive part
11211000 4 3 2 1 0.
11211000 2 3 2 1 0.
11211100 0 1
11211101 2 4.75-3
11211201 1 2
11211301 0 2
11211401 560. 3
11211501 0 0 0 0. 0 4
11211501 0 0 0 0. 0 2
11211601 121010000 0 1 1.71.200 1 * +0.400*428
11211602 123010000 0 1 1.256.800 2 * -0.200*428
11211603 125010000 0 1 1.498.192 3 * -1.164*428
11211604 125010000 0 1 1.75.756 4 * -0.177*428
*
* coupled
11211601 123010000 0 1 1.926.192 1 * +0.4+0.6+1.164*428
11211602 125010000 0 1 1.75.756 2 * -0.177*428
*
* tie rods (8 rods)
11212000 3 3 2 1 0.
11212000 1 3 3 2 1 0.
11212100 0 1
11212101 2 7.-3
11212201 1 2
11212301 0 2
11212401 560. 3
11212501 0 0 1 0. 0 3
11212501 0 0 1 0. 0 1
11212601 121010000 0 1 1 3.2 1 * 8*0.4
11212602 123010000 0 1 1.4.8 2 * 8*0.6
11212603 125010000 0 1 1.8.432 3 * 8*1.054
*
* coupled
11212601 123010000 0 1 1.16.432 1 * 8*(0.4+0.6+1.054)
11212701 0 0. 0. 0. 3
11212901 0 0. 0. 0. 3
11212901 0 10. 10. 0. 0. 0. 0. 1. 1
*
* water chamber
11213000 1 3 1 0.
11213100 0 1
11213101 2 0.976426 * 0.162 m3 + 4/3*0.02234 m3 (for
water)
11213201 1 2
11213301 0 2
11213401 560. 3
11213501 121010000 0 1 1 0.166 1
11213601 0 0 1 0.166 1 * this end has 155 c (cooling)
- ignored !!
11213701 0 0. 0. 0. 1
11213801 0 10. 10. 0. 0. 0. 0. 1. 1
*
* lower plenum: bh11
11230000 13 3 2 1 0.242895
11230100 0 1
11230101 2 0.274279
11230201 1 2
11230301 1.0 2

```





\* sags

\* prim. sistem: sg izstop

\* 3010000 sg-cl engljun

\* 6100000 sg-cl engljun

\* 6110000 sg-cl engljun

\* 6120000 sg-cl engljun

\* 6130000 sg-cl engljun

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\* 9010000 sg-cl engljun

\* 9020000 sg-cl engljun

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\* 9040000 sg-cl engljun

\* 9050000 sg-cl engljun

\* 9060000 sg-cl engljun

\* 9070000 sg-cl engljun

\* 9080000 sg-cl engljun

\* 9090000 sg-cl engljun

\* 9100000 sg-cl engljun

\* 9110000 sg-cl engljun

\* 9120000 sg-cl engljun

\* 9130000 sg-cl engljun

\* 9140000 sg-cl engljun

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\* 9320000 sg-cl engljun

\* 9330000 sg-cl engljun

\* 9340000 sg-cl engljun

\* 9350000 sg-cl engljun

\* 9360000 sg-cl engljun

\* 9370000 sg-cl engljun

\* 9380000 sg-cl engljun

\* 9390000 sg-cl engljun

\* 9400000 sg-cl engljun

\* 9410000 sg-cl engljun

\* 9420000 sg-cl engljun

\* 9430000 sg-cl engljun

\* 9440000 sg-cl engljun

\* 9450000 sg-cl engljun

\* 9460000 sg-cl engljun

\* 9470000 sg-cl engljun

\* 9480000 sg-cl engljun

\* 9490000 sg-cl engljun

\* 9500000 sg-cl engljun

\* 9510000 sg-cl engljun

\* 9520000 sg-cl engljun

\* 9530000 sg-cl engljun

\* 9540000 sg-cl engljun

\* 9550000 sg-cl engljun

\* 9560000 sg-cl engljun

\* 9570000 sg-cl engljun

\* 9580000 sg-cl engljun

\* 9590000 sg-cl engljun

\* 9600000 sg-cl engljun

\* 9610000 sg-cl engljun

\* 9620000 sg-cl engljun

\* 9630000 sg-cl engljun

\* 9640000 sg-cl engljun

\* 9650000 sg-cl engljun

\* 9660000 sg-cl engljun

\* 9670000 sg-cl engljun

\* 9680000 sg-cl engljun

\* 9690000 sg-cl engljun

\* 9700000 sg-cl engljun

\* 9710000 sg-cl engljun

\* 9720000 sg-cl engljun

\* 9730000 sg-cl engljun

\* 9740000 sg-cl engljun

\* 9750000 sg-cl engljun

\* 9760000 sg-cl engljun

\* 9770000 sg-cl engljun

\* 9780000 sg-cl engljun

\* 9790000 sg-cl engljun

\* 9800000 sg-cl engljun

\* 9810000 sg-cl engljun

\* 9820000 sg-cl engljun

\* 9830000 sg-cl engljun

\* 9840000 sg-cl engljun

\* 9850000 sg-cl engljun

\* 9860000 sg-cl engljun

\* 9870000 sg-cl engljun

\* 9880000 sg-cl engljun

\* 9890000 sg-cl engljun

\* 9900000 sg-cl engljun

\* 9910000 sg-cl engljun

\* 9920000 sg-cl engljun

\* 9930000 sg-cl engljun

\* 9940000 sg-cl engljun

\* 9950000 sg-cl engljun

\* 9960000 sg-cl engljun

\* 9970000 sg-cl engljun

\* 9980000 sg-cl engljun

\* 9990000 sg-cl engljun

\* 10000000 sg-cl engljun

\* prim. sistem: dvizni kanal

\* 3030000 riser pipe

\* 3030001 6

\* 3030101 0 0 6

\* 3030201 0.01291 1 0 0214 4 0.048695 5

\* 3030301 2 0 4 2.9605 5 0.8295 5

\* 3030401 0.11513 4 0.11711 5 0.04041 6

\* 3030501 0 6

\* 3030601 90 0 6

\* 3030701 2 0 4 2.9605 5 0.8295 6

\* 3030801 0.1e-03 0.03503 5 0.1e-03 0.249 6

\* 3030901 5.46 5.46 1 3.32 3.32 4 0.1 0.1 5

\* 3031001 90 6

\* 3031101 100100 4 100000 5

\* 3031201 100 6.86631e+06 1.24544e+06 2.58278e+06 5.52550e-02

\* 0.00000e+00 1

\* 3031202 100 6.87343e+06 1.25147e+06 2.58289e+06 1.89420e-01

\* 0.00000e+00 2

\* 3031203 100 6.86222e+06 1.25111e+06 2.58295e+06 2.99440e-01

\* 0.00000e+00 3

\* 3031204 100 6.85237e+06 1.25062e+06 2.58305e+06 3.94750e-01

\* 0.00000e+00 4

\* 3031205 100 6.84122e+06 1.25006e+06 2.58314e+06 4.99880e-01

\* 0.00000e+00 5

\* 3031206 100 6.83286e+06 1.24938e+06 2.58318e+06 4.01760e-01

\* 0.00000e+00 6

\* 3031300 0

\* 3031301 4.72642e-02 2.73680e-01 0.00000e+00 1

\* 3031302 5.13242e-02 3.89180e-01 0.00000e+00 2

\* 3031303 5.53470e-02 4.40650e-01 0.00000e+00 3

\* 3031304 6.06003e-02 4.89460e-01 0.00000e+00 4

\* 3031305 7.43034e-02 7.34730e-01 0.00000e+00 5

\* 3031401 0.027 0 0 1.0 1.0 5

\*\* ++

\* sek. sistem: separator pare

\* 3070000 sear

\* 3070001 3 0

\* 3070101 0 0 1.9430 0.09467 0 90 0 1.9430 0.1e-04 0.24e

\* 0

\* 3070200 100 6.82485e+05 1.24923e+06 2.58325e+06 1.46060e-01

\* 3071101 307010000 310000000 4.8695e-02 0.82 0.14 01000

\* 0 0

\* 3072101 307000000 308000000 44.9150e-02 0.26 0.23 01000

\* 0 0

\* 3073101 303010000 307000000 4.8695e-02 0.0 0.0 01000

\* 3074201 9.27829e-02 3.06390e-01 0.00000e+00

\* 3075201 4.65466e-03 1.70169e-02 0.00000e+00

\* 3076201 7.22492e-02 7.61560e-01 0.00000e+00

\*\* ++

\* sek. sistem: zgornji parni prostor

\* 3100000 stadsome pipe

\* prim. sistem: sg izstopni prekat in u-cvi

\* 3010000 sg-tube pipe

\* 3010001 11

\* 3010101 0.04394 1 0.010342 11

\* 3010201 0.04394 1 0.0103423 11

\* 3010301 0.998 1 2.0 5 1.725 7 2.0 11

\* 3010401 0 11

\* 3010501 0 11

\* 3010601 83 0 1 90 0 5 45 0 6 -45 0 7 -90 0 11

\* 3010701 0.728 1 2 0 5 1.685 5 -1.685 7 -2 0 11

\* 3010801 0.1e-03 0.091 1 0.01e-03 0.01968 11

\* 3010901 0.1e-05 0.091 1 0.01e-07 0.01968 11

\* 3011001 0.44 0.44 0.61 0.01 5 0.32 0.22 6 0.01

\* 0 0 10

\* 3011001 0 0 1 0.01 1 0 0 0 10

\* 3011001 00 11

\* 3011101 00100 1 00000 10

\* 3011101 100000 10

\* 3011201 103 1.55556e+07 5.6174e+02 0.00000e+00 0 0 1

\* 3011202 103 1.55187e+07 5.6172e+02 0.00000e+00 0 0 2

\* 3011203 103 1.54826e+07 5.62658e+02 0.00000e+00 0 0 3

\* 3011204 103 1.54455e+07 5.62199e+02 0.00000e+00 0 0 4

\* 3011205 103 1.54105e+07 5.61785e+02 0.00000e+00 0 0 5

\* 3011206 103 1.53770e+07 5.61455e+02 0.00000e+00 0 0 6

\* 3011207 103 1.53486e+07 5.61159e+02 0.00000e+00 0 0 7

\* 3011208 103 1.53236e+07 5.60864e+02 0.00000e+00 0 0 8

\* 3011209 103 1.53456e+07 5.60605e+02 0.00000e+00 0 0 9

\* 3011210 103 1.53190e+07 5.60379e+02 0.00000e+00 0 0 10

\* 3011211 103 1.53324e+07 5.60181e+02 0.00000e+00 0 0 11

\* 3011300 0

\* 3011301 6.73470e+00 6.73470e+00 0.00000e+00 1

\* 3011302 6.72540e+00 6.72540e+00 0.00000e+00 2

\* 3011303 6.71720e+00 6.71720e+00 0.00000e+00 3

\* 3011304 6.71000e+00 6.71000e+00 0.00000e+00 4

\* 3011305 6.70360e+00 6.70360e+00 0.00000e+00 5

\* 3011306 6.69850e+00 6.69850e+00 0.00000e+00 6

\* 3011307 6.69390e+00 6.69390e+00 0.00000e+00 7

\* 3011308 6.68910e+00 6.68910e+00 0.00000e+00 8

\* 3011309 6.68490e+00 6.68490e+00 0.00000e+00 9

\* 3011310 6.68580e+00 6.68580e+00 0.00000e+00 10

\* 3011401 0.1968 0 0 1.0 1.0 10

\* prim. sistem: sg izstopni prekat

\* 3130000 c-ch branch

\* 3130001 1 0

\* 3130101 0 0 0.798 35.061e-03 0 0 -85 0 -0.728 0.1e-03

\* 0.091 00

\* 3130101 0 0 0.798 35.061e-03 0 0 -85 0 -0.728 0.1e-04

\* 0.091 00

\* 3130200 103 1.53426e+07 5.60188e+02

\* 3131101 301010000 313000000 0.0103423 0.3 0.2 130000

\* 3131101 301010000 313000000 0.0103423 0.3 0.2 130000





3200101 0.0 31.65 68.5e-03 0 -45.0 -18.670 0.01-3 0.0525  
 00  
 3200200 102 6.81250e+06 1.00000e+00  
 \* hbe8  
 \* 13201000 1 4 2 1 0.0525  
 13201000 1 4 2 0 0.0525 \* ffill  
 13201100 0 1  
 13201200 3 0.0603  
 13201300 1 3  
 13201400 3 0.0603  
 13201500 0 3  
 13201600 1 566.810 2 563.420 3 560.15 4  
 13201700 1 320010000 0 1 31.65 1  
 13201800 0 0 1 31.65 1  
 13201900 0 0 0 1  
 13202000 0 10 10 0 0 0 1 1  
 13202100 0 10 10 0 0 0 1 1  
 \*  
 \* prim. sistem: hot leg spoj pri sl  
 6130000 hie13 anglju  
 \* 6130101 603010000 602000000 0 0 0 0 0 00000  
 6130101 603010000 602000000 0 0 0 265 130000  
 6130201 0 6.36880e+00 6.36880e+00 0.00000e+00  
 \*  
 \* prim. sistem: hot leg od sl do sg  
 6020000 hleg pipe  
 \* 6020001 2  
 \* 6020101 0.010936 2  
 \* 6020201 0.010936 1  
 \* 6020301 1.1891 1 1.8558 2  
 \* 6020401 0.0 2  
 \* 6020501 0.0 2  
 \* 6020601 9.0 1 70.0 2  
 \* 6020701 0.1800 1 1.7317 2  
 \* 6020801 0.1e-03 0.1180 2  
 \* \* 6020901 0.31 0.31 1  
 \* 6021001 0.24 0.24 1  
 \* 6021101 0.0 2  
 \* 6021201 100000 1  
 \* 6021301 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 1  
 \* 6021402 103 1.55738e+07 5.63790e+02 0.00000e+00 0 0 2  
 \* 6021300 0  
 \* 6021301 6.29880e+00 6.29880e+00 0.00000e+00 1  
 \*  
 6020000 hleg pipe  
 6020101 0.010936 10  
 6020201 0.010936 9  
 6020301 0.23782 5 0.37116 10  
 6020401 0.0 10  
 6020501 0.0 10  
 6020601 9.0 5 70.0 10  
 6020701 0.036 5 0.3461 10 \* \*\*  
 6020801 0.1e-03 0.1180 10  
 6020901 0.267 0.267 9  
 6021001 0.0 10  
 6021101 100000 9 \* v=0  
 6021201 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 1  
 6021301 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 2  
 6021402 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 3  
 6021201 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 3  
 6021204 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 4  
 6021205 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 5  
 6021206 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 6  
 6021207 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 7  
 6021208 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 8  
 6021209 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 9

6021210 103 1.55637e+07 5.63794e+02 0.00000e+00 0 0 10  
 6021300 0  
 6021301 6.36880e+00 6.36880e+00 0.00000e+00 1  
 6021302 6.36880e+00 6.36880e+00 0.00000e+00 2  
 6021303 6.36880e+00 6.36880e+00 0.00000e+00 3  
 6021304 6.36880e+00 6.36880e+00 0.00000e+00 4  
 6021305 6.36880e+00 6.36880e+00 0.00000e+00 5  
 6021306 6.36880e+00 6.36880e+00 0.00000e+00 6  
 6021307 6.36880e+00 6.36880e+00 0.00000e+00 7  
 6021308 6.36880e+00 6.36880e+00 0.00000e+00 8  
 6021309 6.36880e+00 6.36880e+00 0.00000e+00 9  
 \*  
 \* prim. sistem: hot leg spoj pri sl  
 6130000 hie13 anglju  
 \* 6130101 603010000 602000000 0 0 0 0 0 00000  
 6130101 603010000 602000000 0 0 0 265 130000  
 6130201 0 6.36880e+00 6.36880e+00 0.00000e+00  
 \*  
 \* prim. sistem: hot leg od sl do sg  
 6020000 hleg pipe  
 \* 6020001 2  
 \* 6020101 0.010936 2  
 \* 6020201 0.010936 1  
 \* 6020301 1.1891 1 1.8558 2  
 \* 6020401 0.0 2  
 \* 6020501 0.0 2  
 \* 6020601 9.0 1 70.0 2  
 \* 6020701 0.1800 1 1.7317 2  
 \* 6020801 0.1e-03 0.1180 2  
 \* \* 6020901 0.31 0.31 1  
 \* 6021001 0.24 0.24 1  
 \* 6021101 0.0 2  
 \* 6021201 100000 1  
 \* 6021301 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 1  
 \* 6021402 103 1.55738e+07 5.63790e+02 0.00000e+00 0 0 2  
 \* 6021300 0  
 \* 6021301 6.29880e+00 6.29880e+00 0.00000e+00 1  
 \*  
 6020000 hleg pipe  
 6020101 0.010936 10  
 6020201 0.010936 9  
 6020301 0.23782 5 0.37116 10  
 6020401 0.0 10  
 6020501 0.0 10  
 6020601 9.0 5 70.0 10  
 6020701 0.036 5 0.3461 10 \* \*\*  
 6020801 0.1e-03 0.1180 10  
 6020901 0.267 0.267 9  
 6021001 0.0 10  
 6021101 100000 9 \* v=0  
 6021201 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 1  
 6021301 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 2  
 6021402 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 3  
 6021201 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 3  
 6021204 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 4  
 6021205 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 5  
 6021206 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 6  
 6021207 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 7  
 6021208 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 8  
 6021209 103 1.55880e+07 5.63790e+02 0.00000e+00 0 0 9

3400000 turbina tmdpvol  
 3440101 10 0 0 0.1900 0 0 0 0 0 2e-03 0 0  
 3440200 2 0 cntrlvar 344  
 3440201 -1.0 58 12e+05 1.0  
 3440202 1.0e+05 58 12e+05 1.0  
 3440203 100.0e+05 100.0e+05 1.0  
 \*  
 \* rcccs  
 cevovodi primarnega kroga 1  
 \*  
 \* prim. sistem: hot leg do surge line  
 6030000 hleg anglju  
 \* 6030101 0.010936 1.4441 0.0 0.0 0.0 0.0 0.1e-03 0.1180  
 00  
 \* 6030200 103 1.55957e+07 5.63790e+02  
 6030001 5  
 6030101 0.010936 5  
 6030201 0.010936 4  
 6030301 0.2882 5  
 6030401 0.0 5  
 6030501 0.0 5



5560000 cleg\_b pipe \* R+
5560021 597.0 1 588.0 2 570.0 3 561.0 4
16021401 597.0 1 588.0 2 570.0 3 561.0 4
16021501 603010000 10000 1 0 0.1070 5
16021502 602010000 10000 1 0 0.0881 10
16021503 602060000 18000 1 0 0.1376 15
16021601 0 0 0 0 0.1070 5
16021602 0 0 0 0.0881 10
16021603 0 0 0 0.1376 15
16021701 10226 0.0667 0 0 0.15
16021801 0 10.10 0.0 0.0 1.15
16021901 0 10.10 0.0 0.0 1.15
\*\* intermediate leg - cev s prirobnicami: hhl1
\*\* 16521000 4 4 1 1 0.0
\*\* 16521100 0 1
\*\* 16521201 3 0.0226
\*\* 16521201 1 3
\*\* 16521301 1.0 3
\*\* 16521401 597.0 1 588.0 2 570.0 3 561.0 4
\*\* 16521501 652010000 10000 1 0 0.1313 2
\*\* 16521502 652020000 0 1 0 0.7673 1
\*\* 16521503 653010000 0 1 0 0.4088 3
\*\* 16521504 654010000 0 1 0 0.6625 4
\*\* 16521601 0 0 0 0.9313 1
\*\* 16521602 0 0 0 0.7673 2
\*\* 16521603 0 0 0 0.4088 3
\*\* 16521604 0 0 0 0.6625 4
\*\* 16521701 10224 0.166 0 0 0.4
\*\* 16521801 0 10.10 0.0 0.0 1.15
\*\* 16521901 0 10.10 0.0 0.0 1.15
\*\* intermediate leg - cev s prirobnicami: hhl1
\*\* 16521000 20 4 1 1 0.0
\*\* 16521100 0 1
\*\* 16521201 3 0.0226
\*\* 16521201 1 3
\*\* 16521301 1.0 3
\*\* 16521401 597.0 1 588.0 2 570.0 3 561.0 4
\*\* 16521501 652010000 10000 1 0 0.1313 2
\*\* 16521502 652060000 10000 1 0 0.1515 10
\*\* 16521503 653010000 10000 1 0 0.0818 15
\*\* 16521504 654010000 10000 1 0 0.1325 20
\*\* 16521601 0 0 0 0.1863 5
\*\* 16521602 0 0 0 0.1535 10
\*\* 16521603 0 0 0 0.0818 15
\*\* 16521604 0 0 0 0.1325 20
\*\* 16521701 10224 0.166 0 0 0.4
\*\* 16521801 0 10.10 0.0 0.0 1.15
\*\* 16521901 0 10.10 0.0 0.0 1.15
\*\* cold leg - cev s prirobnicami: hhl1
\*\* 16551000 2 4 1 1 0.0
\*\* 16551100 0 1
\*\* 16551201 3 0.0279
\*\* 16551301 1.0 3
\*\* 16551401 597.0 1 588.0 2 570.0 3 561.0 4
\*\* 16551501 655010000 10000 1 0 0.1383 1
\*\* 16551502 656010000 10000 1 0 0.1383 10
\*\* 16551601 0 0 0 0.1383 1
\*\* 16551602 0 0 0 0.1383 10
\*\* 16551701 10224 0.0332 0 0 0.10
\*\* 16551801 0 10.10 0.0 0.0 1.10
\*\* 16551901 0 10.10 0.0 0.0 1.10
\*\* dbhhl : db korekcija nekaterih rcsi tlacnih zaznaval
\*\* cv 620 : db korigirano tlacno zaznavalo 602-10 [pa]
\*\* 20562000 pk62020 sum 9.8067 0.0 1
\*\* 20562001 0.0 0.10197 p 602100000 -0.15 rho 602100000 \* R+
\*\* cv 621 : db korigirano tlacno zaznavalo 301-06 [pa]
\*\* 20562100 pk30106 sum 9.8067 0.0 1
\*\* 20562101 0.0 0.10197 p 301060000 -0.8425 rho 301060000
\*\* cv 622 : db korigirano tlacno zaznavalo 652-01 [pa]
\*\* 20562200 pk65201 sum 9.8067 0.0 1
\*\* 20562201 0.0 0.10197 p 652100000 -0.15 rho 652100000 \* R+
\*\* cv 623 : db korigirano tlacno zaznavalo 652-10 [pa]
\*\* 20562300 pk65202 sum 9.8067 0.0 1
\*\* 20562301 0.0 0.10197 p 652100000 0.15 rho 652100000 \* R+
\*\* cv 624 : db korigirano tlacno zaznavalo 654-05 [pa]
\*\* 20562400 pk65401 sum 9.8067 0.0 1
\*\* 20562401 0.0 0.10197 p 654050000 -0.15 rho 654050000 \* R+
\*\* cvvii : dpmeasured - gravity term - zanka 1
\*\* ka blok cv je upravljan med rcsi dp inicializacijo
\*\* upostevane so vse db korekcije tlacnih zaznaval
\*\* cv 630 : dpilh [bar]
\*\* 20563000 dpilh sum 1.0e-05 -0.0763 0
\*\* 20563001 0.0 1.0 p 602010000 -1.0 p 603010000 \* db=0.0m
\*\* cv 631 : dpilh [bar]
\*\* 20563100 dpilh sum 1.0e-05 -0.0792 0
\*\* 20563101 0.0 1.0 p 602020000 -1.0 p 602010000 1.0
\*\* 20563101 0.0 1.0 cncrivar 620 -1.0 p 602010000 1.0
\*\* cncrivar 632
\*\* 20563101 0.0 1.0 cncrivar 632
\*\* cv 632 : dpilh gravity term [pa]
\*\* 16021000 15 4 1 1 0.0
\*\* 16021100 0 1
\*\* 16021101 3 0.0286
\*\* 16021201 1 3
\*\* 16021301 1.0 3
\*\* hot leg - cev s prirobnicami: hhl1
\*\* 16021000 2 4 1 1 0.0
\*\* 16021100 0 1
\*\* 16021101 3 0.0286
\*\* 16021201 1 3
\*\* 16021301 1.0 3
\*\* hot leg - cev s prirobnicami: hhl1
\*\* 16021401 597.0 1 588.0 2 570.0 3 561.0 4
\*\* 16021501 603010000 10000 1 0 0.5353 1
\*\* 16021502 602010000 10000 1 0 0.4408 2
\*\* 16021503 602020000 10000 1 0 0.6879 3
\*\* 16021601 0 0 0 0.5353 1
\*\* 16021602 0 0 0 0.4408 2
\*\* 16021603 0 0 0 0.6879 3
\*\* 16021701 10226 0.333 0 0 0.3
\*\* 16021801 0 10.10 0.0 0.0 1.13
\*\* 16021901 0 10.10 0.0 0.0 1.13
\*\* hot leg - cev s prirobnicami: hhl1
\*\* 16021000 15 4 1 1 0.0
\*\* 16021100 0 1
\*\* 16021101 3 0.0286
\*\* 16021201 1 3
\*\* 16021301 1.0 3
\*\* vsa toplotna telesa primarnih cevovodov so poenostavljena v
\*\* ploste
\*\* hhsse toplotna telesa - primarni cevovod 1
\*\* hot leg - cev s prirobnicami: hhl1
\*\* 16021000 2 4 1 1 0.0
\*\* 16021100 0 1
\*\* 16021101 3 0.0286
\*\* 16021201 1 3
\*\* 16021301 1.0 3
\*\* hot leg - cev s prirobnicami: hhl1
\*\* 16021401 597.0 1 588.0 2 570.0 3 561.0 4
\*\* 16021501 603010000 10000 1 0 0.5353 1
\*\* 16021502 602010000 10000 1 0 0.4408 2
\*\* 16021503 602020000 10000 1 0 0.6879 3
\*\* 16021601 0 0 0 0.5353 1
\*\* 16021602 0 0 0 0.4408 2
\*\* 16021603 0 0 0 0.6879 3
\*\* 16021701 10226 0.333 0 0 0.3
\*\* 16021801 0 10.10 0.0 0.0 1.13
\*\* 16021901 0 10.10 0.0 0.0 1.13
\*\* hot leg - cev s prirobnicami: hhl1
\*\* 16021000 15 4 1 1 0.0
\*\* 16021100 0 1
\*\* 16021101 3 0.0286
\*\* 16021201 1 3
\*\* 16021301 1.0 3







14032602 407010000 0 1 0 1.5537 2  
14032701 0 0 0 0 2  
14032801 0 10 10 0 0 0 1.2  
14032901 0 10 10 0 0 0 1.2  
\* upper sleeve and upper head ---> plošca 14101...14104  
14101000 1 4 1 1 0 0  
14101100 0 1  
14101200 0 0 0 0.0210  
14101301 1 3  
14101401 0 0 3  
14101501 597.0 1 588.0 2 570.0 3 561.0 4  
14101601 0 0 0 0 1.2005 1  
14101701 4100200 0 1 0 1.005 1  
14101801 0 0 0 0 1  
14101901 0 10 10 0 0 0 1.1  
14102000 1 4 1 1 0 0  
14102100 0 1  
14102201 1 3  
14102301 0 0 3  
14102401 597.0 1 588.0 2 570.0 3 561.0 4  
14102501 0 0 0 0 3.3870 1  
14102601 410010000 0 1 0 3.3870 1  
14102701 0 0 0 0 1  
14102801 0 10 10 0 0 0 1.1  
14102901 0 10 10 0 0 0 1.1  
\* riser (brez upper cylindrical shell) ---> plošca: h=11  
14031000 5 4 1 1 0 0  
14031100 0 1  
14031201 1 3  
14031301 1 0 3  
14031401 597.0 1 588.0 2 570.0 3 561.0 4  
14031501 403010000 0 1 0 2.895 1  
14031602 0 0 0 2.895 2  
14031701 0 0 0 2.895 3  
14031801 0 0 0 2.895 4  
14031901 0 10 10 0 0 0 1.2  
14032000 0 10 10 0 0 0 1.2  
\* riser (brez upper cylindrical shell) ---> plošca: h=11  
14031000 5 4 1 1 0 0  
14031100 0 1  
14031201 1 3  
14031301 1 0 3  
14031401 597.0 1 588.0 2 570.0 3 561.0 4  
14031501 403010000 0 1 0 2.895 1  
14031602 0 0 0 2.895 2  
14031701 0 0 0 2.895 3  
14031801 0 0 0 2.895 4  
14031901 0 10 10 0 0 0 1.2  
14032000 0 10 10 0 0 0 1.2  
\* upper-inner cylindrical shell ---> plošca  
14032000 2 4 1 1 0 0  
14032100 0 1  
14032201 0 3  
14032301 0 0 3  
14032401 597.0 1 588.0 2 570.0 3 561.0 4  
14032501 408010000 0 1 0 0.6633 1  
14032601 419010000 0 1 0 1.5537 2  
14032701 403060000 0 1 0 0.6633 1

14092000 4 4 1 1 0 0  
14092100 0 1  
14092101 3 0 00276  
14092201 1 3  
14092301 0 0 3  
14092401 597.0 1 588.0 2 570.0 3 561.0 4  
14092501 0 0 0 0 1.2028 1  
14092502 0 0 0 0 1.2028 2  
14092503 0 0 0 0 1.2028 3  
14092504 0 0 0 0 1.2028 4  
14092601 409020000 0 1 0 1.2028 1  
14092602 409030000 0 1 0 1.2028 2  
14092603 409040000 0 1 0 1.2028 3  
14092604 409050000 0 1 0 1.2028 4  
14092701 0 0 0 0 4  
14092801 0 10 10 0 0 0 1.4  
14092901 0 10 10 0 0 0 1.4  
\* sggecevy sg 2 kontrolne spremljivke  
\* cv 403: sg2: nivo v povratnem kanalu [m]  
20540300 levdc sum 1.0 13.45 1  
20540301 0.0 2.0 voidf 409050000 2.0 voidf 409040000  
20540302 2.9625 voidf 409010000 0.8275 voidf 408010000  
20540304 1.9430 voidf 419010000  
\* cv 405: sg2: masa sekundarnega hladila [kg]  
20540500 segmass sum 1.0 790.0 1  
\*\* 20540501 0.0 0.11513 rbo 403010000 0.11513 rbo  
403020000  
\*\* 20540502 0.11513 rbo 403030000 0.11513 rbo  
403040000  
\*\* 20540503 0.17171 rbo 403050000 0.04041 rbo  
403060000  
20540501 0.0 0.12513 rbo 403010000 0.12513 rbo 403020000  
20540502 0.12513 rbo 403030000 0.12513 rbo 403040000  
20540503 0.18171 rbo 403050000 0.04041 rbo 403060000  
20540504 0.09466 rbo 407010000 0.54287 rbo 410010000  
20540505 0.13404 rbo 410020000 0.30780 rbo 419010000  
20540506 0.08372 rbo 408010000 0.06909 rbo 409010000  
20540507 0.01167 rbo 409020000 0.01167 rbo 409030000  
20540508 0.01167 rbo 409040000 0.01167 rbo 409050000  
\* main feedwater 2  
\* rsnff  
\* konstantni mfw tok  
43' ~00 mfw tmqpljun  
101 43100000 432000000 0.0266  
4340200 1 595 \* si  
4340201 1.0 0.52517 0.0  
4340202 0.0 0.52517 0.0

14032602 407010000 0 1 0 1.5537 2  
14032701 0 0 0 0 2  
14032801 0 10 10 0 0 0 1.2  
14032901 0 10 10 0 0 0 1.2  
\* upper sleeve and upper head ---> plošca 14101...14104  
14101000 1 4 1 1 0 0  
14101100 0 1  
14101200 0 0 0 0.0210  
14101301 1 3  
14101401 0 0 3  
14101501 597.0 1 588.0 2 570.0 3 561.0 4  
14101601 0 0 0 0 1.2005 1  
14101701 4100200 0 1 0 1.005 1  
14101801 0 0 0 0 1  
14101901 0 10 10 0 0 0 1.1  
14102000 1 4 1 1 0 0  
14102100 0 1  
14102201 1 3  
14102301 0 0 3  
14102401 597.0 1 588.0 2 570.0 3 561.0 4  
14102501 0 0 0 0 3.3870 1  
14102601 410010000 0 1 0 3.3870 1  
14102701 0 0 0 0 1  
14102801 0 10 10 0 0 0 1.1  
14102901 0 10 10 0 0 0 1.1  
\* riser (brez upper cylindrical shell) ---> plošca: h=11  
14031000 5 4 1 1 0 0  
14031100 0 1  
14031201 1 3  
14031301 1 0 3  
14031401 597.0 1 588.0 2 570.0 3 561.0 4  
14031501 403010000 0 1 0 2.895 1  
14031602 0 0 0 2.895 2  
14031701 0 0 0 2.895 3  
14031801 0 0 0 2.895 4  
14031901 0 10 10 0 0 0 1.2  
14032000 0 10 10 0 0 0 1.2  
\* upper-inner cylindrical shell ---> plošca  
14032000 2 4 1 1 0 0  
14032100 0 1  
14032201 0 3  
14032301 0 0 3  
14032401 597.0 1 588.0 2 570.0 3 561.0 4  
14032501 408010000 0 1 0 0.6633 1  
14032601 419010000 0 1 0 1.5537 2  
14032701 403060000 0 1 0 0.6633 1

14201101 3 0.0603  
 14201201 1 3  
 14201301 0.0 3  
 14201401 570.330 1 566.810 2 563.420 3 560.15 4  
 14201501 420010000 0 1 1 31.65 1  
 14201601 0 0 0 1 31.65 1  
 14201701 0 0 0 0 1  
 14201801 0 10.10 0.0 0.0 1.1  
 14201901 0 10.10 0.0 0.0 1.1

\*\*\*\*\*  
 \* prim. sistem: hot leg spoj pri sl  
 8130000 hleg slngljun  
 \* 8130101 803010000 802000000 0.0 0.0 0.0 00000  
 8131001 803010000 802000000 0.0 0.265 0.265 130000  
 8132001 0 6.36770e+00 5.63762e+02 0.00000e+00

\*\*\*\*\*  
 \* prim. sistem: hot leg od sl do sg  
 6020000 hleg pipe  
 \* 6020001 2  
 \* 6020101 0.010936 2  
 \* 6020201 0.010936 1  
 \* 6020301 1.1891 1 1.8558 2  
 \* 6020401 0.0 2  
 \* 6020501 0.0 2  
 \* 6020601 9.0 1 70.0 2  
 \* 6020701 0.1800 1 1.7317 2  
 \* 6020801 0.1e-03 0.1180 2  
 \* 6020901 0.31 0.31 1  
 \* 6021001 0.24 0.24 1  
 \* 6021101 0.0 2  
 \* 6021201 100000 1  
 \* 6021301 103 1.55820e+07 5.63790e+02 0.00000e+00 0 0 1  
 \* 6021401 103 1.55793e+07 5.63790e+02 0.00000e+00 0 0 2  
 \* 6021501 0 10  
 \* 6021601 6.29920e+00 6.29920e+00 0.00000e+00 1  
 \* 6021701 10  
 \* 6021801 0.078936 9  
 \* 6021901 0.23782 5 0.37116 10  
 \* 6022001 0.0 10  
 \* 6022101 9.0 5 70.0 10  
 \* 6022201 0.036 5 0.34634 10 \*\*  
 \* 6022301 0.1e-03 0.1180 10  
 \* 6022401 0.0267 0.0267 9  
 \* 6022501 0.0 10  
 \* 6022601 100000 5 100000 9 \* v=0  
 \* 6022701 103 1.55885e+07 5.63760e+02 0.00000e+00 0 0 1  
 \* 6022801 103 1.55853e+07 5.63760e+02 0.00000e+00 0 0 2  
 \* 6022901 103 1.55841e+07 5.63760e+02 0.00000e+00 0 0 3  
 \* 6023001 103 1.55829e+07 5.63759e+02 0.00000e+00 0 0 4  
 \* 6023101 103 1.55816e+07 5.63759e+02 0.00000e+00 0 0 5  
 \* 6023201 103 1.55791e+07 5.63758e+02 0.00000e+00 0 0 6  
 \* 6023301 103 1.55752e+07 5.63757e+02 0.00000e+00 0 0 7  
 \* 6023401 103 1.55714e+07 5.63756e+02 0.00000e+00 0 0 8  
 \* 6023501 103 1.55676e+07 5.63755e+02 0.00000e+00 0 0 9  
 \* 6023601 103 1.55637e+07 5.63754e+02 0.00000e+00 0 0 10  
 \* 6023701 0 5  
 \* 6023801 6.36770e+00 5.63770e+02 0.00000e+00 1  
 \* 6023901 6.36770e+00 5.63770e+02 0.00000e+00 3  
 \* 6024001 6.36770e+00 5.63770e+02 0.00000e+00 4  
 \* 6024101 6.36770e+00 5.63770e+02 0.00000e+00 5  
 \* 6024201 6.36770e+00 5.63770e+02 0.00000e+00 6

14201101 3 0.0603  
 14201201 1 3  
 14201301 0.0 3  
 14201401 570.330 1 566.810 2 563.420 3 560.15 4  
 14201501 420010000 0 1 1 31.65 1  
 14201601 0 0 0 1 31.65 1  
 14201701 0 0 0 0 1  
 14201801 0 10.10 0.0 0.0 1.1  
 14201901 0 10.10 0.0 0.0 1.1

\*\*\*\*\*  
 \* delta tcold : bethay referenca : 559.85 k  
 20540000 dtcold sum 1.0 0.0 0  
 20540001 560.35 -1.0 tempf 855010000  
 \* 20540001 559.35 -1.0 tempf 855010000 \* t8  
 20544400 p444 sum 1.0 58.12e+05 0  
 20544401 0.0 1.0 p 444010000 300. cntrivar 400

4150000 venturi engljun  
 4150101 420010000 444000000 0.0 0.0 0.0 130000  
 4150201 0 6.87740e+00 6.87740e+00 0.00000e+00

4480000 turbine tmdpvol  
 4480101 10.0 0.0 1000.0 0.0 0.0 0.2e-03 0 0  
 4480201 2 0 cntrivar 444  
 4480301 -1.0 68.12e+05 1.0  
 4480401 1.0e+05 1.0e+05 1.0  
 4480501 100.0e+05 100.0e+05 1.0

\*\*\*\*\*  
 \* rrces cevovodi primarnega kroga 2  
 \*\*\*\*\*  
 \* prim. sistem: hot leg do surge line  
 \* 6030000 hleg slngljun  
 \* 6030101 0.010936 1.4441 0.0 0.0 0.0 0.1e-03 0.1180  
 00  
 \* 6030200 103 1.55957e+07 5.63790e+02

8030000 hleg pipe  
 8030001 5  
 8030101 0.010936 5  
 8030201 0.010936 4  
 8030301 0.2882 5  
 8030401 0.0 5  
 8030501 0.0 5  
 8030601 0.0 5  
 8030701 0.0 5  
 8030801 0.1e-03 0.1180 5  
 8030901 0.0 0.0 4  
 8031001 0.0 5  
 8031101 100000 4 +fvcahs.v=0  
 should be input as not used  
 8031201 103 1.55942e+07 5.63762e+02 0.00000e+00 0 0 1

4340203 6.0 0.0 0.0  
 \* volumski mfw tok  
 \* 20540200 mflow div 1.0 0.0 1  
 \* 20540201 tbof 432010000 mflow 432010000

\* feedwater line  
 4320000 fwline branch  
 4320001 0  
 43200101 5.557e-04 10.0 0.0 60.0 7.0 0.01e-03 0.0266 00  
 4320020 103 6.86275e+05 4.90974e+02  
 \* 4321101 432010000 408000000 0.0006786 0.0 0.00100  
 4321101 432010000 408000000 0.0 1.0 0.0 130100  
 4321201 1.11560e+00 1.11560e+00 0.00000e+00

\*\*\*\*\*  
 \* vir nepajrsine vode  
 4330000 fsource tmdpvol  
 4330101 1.0 0.0 10.0 0.0 0.0 0.01e-03 0.0 00  
 4330200 103  
 4330201 70.0e+5 491.0

\*\*\*\*\*  
 \* ccci "regulacija" sg2 nivoja  
 \* tl. konstantni mfw 434 reguliramo nivo v povratnem kanalu  
 4290000 v429 tmdpvol  
 4290101 1.0 0.0 10.0 0.0 0.0 0.2e-03 0.0 0  
 4290200 103  
 4290201 0 70.0e+5 491.0

4300000 j430 tmdpjun  
 4300101 429000000 419010000 0.0  
 4300201 1.0 0.0 0.0 0.0 0.0  
 4300301 -1.0 0.0 0.0 0.0  
 4300401 1.5 0.0 0.0  
 4300501 13.45 0.0 0.0  
 4300601 13.45 0.0 0.0  
 4300701 13.45 -1.5 0.0 0.0

\*\*\*\*\*  
 \* 4300000 j430 tmdpjun  
 \* 4300101 429000000 419010000 0.0  
 \* 4300201 1.0 0.0 0.0 0.0  
 \* 4300301 -1.0 0.0 0.0 0.0  
 \* 4300401 1.5 0.0 0.0 0.0  
 \* 4300501 13.45 0.0 0.0 0.0  
 \* 4300601 13.45 0.0 0.0 0.0

\*\*\*\*\*  
 \* parovod 2  
 \* sgl  
 \* 4200000 stline slngljun  
 4200101 0.0 31.65 68.5e-03 0 -85.0 -18.670 0.01-3 0.0525  
 00  
 4200200 102 6.81255e+06 1.00000e+00

\*\*\*\*\*  
 \* bhss  
 \* 14201000 1 4 2 1 0.0525  
 14201000 1 4 2 0 0.0525 \* #f11  
 14201100 0 1

```

8021107 6.36789e+00 5.64560e+00 0.00000e+00 7
8021108 6.36789e+00 5.64570e+00 0.00000e+00 8
8021109 6.36790e+00 5.64580e+00 0.00000e+00 9
*****
** prim. sistem: intermediate leg down
** 8520000 ileg_a pipe
** 8520001 2
** 8520101 0.010936 2
** 8520201 0.010936 1
** 8520301 2.5122 3 2.0697 2
** 8520401 0.0 2
** 8520501 0.0 2
** 8520601 -76.0 1 -72.0 2
** 8520701 -2.4337 1 -1.9670 2
** 8520801 0.1e-03 0.1180 2
** 8520901 0.11 0.11 1
** 8521001 0.1 0.1 1
** 8521101 100000 1
** 8521201 103 1.53406e+07 5.60210e+02 0.00000e+00 0 0 1
** 8521302 103 1.53516e+07 5.60220e+02 0.00000e+00 0 0 2
** 8521303 5 0.41394 10
** 8521304 5 0.41394 10
8520401 0 0 10
8520501 0 0 10
8520601 -76.0 5 -72.0 10
8520701 -0.48674 5 -0.39340 10
** 8520801 0.1e-03 0.1180 10
8520901 0.11 0.11 9
8520901 0.011 0.011 9
8521001 00 10
8521101 100000 9
8521201 103 1.53271e+07 5.60182e+02 0.00000e+00 0 0 1
8521202 103 1.53297e+07 5.60183e+02 0.00000e+00 0 0 2
8521203 103 1.53323e+07 5.60185e+02 0.00000e+00 0 0 3
8521204 103 1.53349e+07 5.60186e+02 0.00000e+00 0 0 4
8521205 103 1.53375e+07 5.60187e+02 0.00000e+00 0 0 5
8521206 103 1.53399e+07 5.60188e+02 0.00000e+00 0 0 6
8521207 103 1.53418e+07 5.60189e+02 0.00000e+00 0 0 7
8521208 103 1.53439e+07 5.60189e+02 0.00000e+00 0 0 8
8521209 103 1.53459e+07 5.60190e+02 0.00000e+00 0 0 9
8521210 103 1.53480e+07 5.60191e+02 0.00000e+00 0 0 10
8521300 10
8521301 6.31440e+00 6.59410e+00 0.00000e+00 1
8521302 6.31450e+00 6.59400e+00 0.00000e+00 2
8521303 6.31450e+00 6.59400e+00 0.00000e+00 3
8521304 6.31440e+00 6.59400e+00 0.00000e+00 4
8521305 6.31440e+00 6.59390e+00 0.00000e+00 5
8521306 6.31440e+00 6.59390e+00 0.00000e+00 6
8521307 6.31440e+00 6.59390e+00 0.00000e+00 7
8521308 6.31440e+00 6.59380e+00 0.00000e+00 8
8521309 6.31440e+00 6.59380e+00 0.00000e+00 9
*****
8021307 6.36789e+00 5.64560e+00 0.00000e+00 7
8021308 6.36789e+00 5.64570e+00 0.00000e+00 8
8021309 6.36790e+00 5.64580e+00 0.00000e+00 9
*****
** prim. sistem: intermediate leg
** 8530000 ileg_b singlvol
** 8530101 0.010936 1.1027 0 0 0 9 0 0.180 0.1e-13
0.1180 00
** 8530200 103 1.53553e+07 5.60220e+02
*****
8530000 ileg_b pipe
8530001 5
8530101 0.010936 5
8530201 0.010936 4
8530301 0.22054 5
8530401 0.0 5
8530501 0.0 5
8530601 9.0 5
8530701 0.036 5
8530801 0.1e-03 0.1180 5
8530901 0 0 0 4
8531001 0 0 5
8531101 100000 4
8531201 103 1.53487e+07 5.60192e+02 0.00000e+00 0 0 1
8531202 103 1.53479e+07 5.60191e+02 0.00000e+00 0 0 2
8531203 103 1.53479e+07 5.60191e+02 0.00000e+00 0 0 3
8531204 103 1.53463e+07 5.60191e+02 0.00000e+00 0 0 4
8531205 103 1.53455e+07 5.60191e+02 0.00000e+00 0 0 5
8531300 0
8531301 6.31430e+00 6.31430e+00 0.00000e+00 1
8531302 6.31440e+00 6.31440e+00 0.00000e+00 2
8531303 5.31480e+00 6.31440e+00 0.00000e+00 3
8531304 5.31440e+00 6.31440e+00 0.00000e+00 4
*****
8640000 junb64 engljun
** 8640101 853010000 8540-0000 0.0 0.20 0.20 00000
8640101 853010000 854000000 0.0 0.0 0.0 130000
8640201 0 6.31440e+00 6.31440e+00 0.00000e+00
*****
** prim. sistem: intermediate leg up
** 8540000 ileg_c singlvol
** 8540101 0.010936 1.7870 0 0 0 0.90 0 1.7870 0.1e-03
0.1180 00
** 8540101 0.010936 1.7871 0 0 0 0.90 0 1.7871 0.1e-03
0.1180 00
** 8540101 0.010936 1.7871 0 0 0 0.90 0 1.7871 0.1e-03
0.1180 00
** ** podaljsek 0.1 mm zaradi sklenitve rcs elevacij v rx
(inapaka bare pod.)
** 8540200 103 1.53446e+07 5.60220e+02
*****
8540000 ileg_c pipe
8540001 5
8540101 0.010936 5
8540201 0.010936 4
8540301 0.3E742 5
8540401 0.0 5
8540501 0.0 5
8540601 90.0 5
8540701 0.35742 5
8540801 0.1e-03 0.1180 5
8540901 0.0 0.0 4
8541001 0.0 5
8541101 100000 4
8541201 103 1.53446e+07 5.60220e+02
should be input as not used
*****
8016000 oul2 branch
8016001 1 0
*****

```



```

18551000 10 4 1 1 0.0
18551100 0 1
18551101 3 0.0279
18551201 1 3
18551301 1.0 3
18551401 587.0 1 588.0 2 570.0 3 561.0 4
18551501 855010000 10000 1 0 0.1183 5
18551502 856010000 10000 1 0 0.1183 10
18551601 0 0 0 0 0.1183 5
18551602 0 0 0 0 0.1183 10
18551701 1027 0.0332 0 0 10
18551801 0 10. 10. 0. 0. 0. 1. 10
18551901 0 10. 10. 0. 0. 0. 1. 10
*****
* ddbh2 : dh korekcija nekaterih rms2 tlačnih zarnaval
*****
* cv 820 : dh korigirano tlačno zarnaval 802-10 [pa]
20582000 pk80202 sum 9.8067 0.0 1
20582001 0.0 0.10197 p 802100000 -0.15 rho 802100000 * R*
* cv 821 : dh korigirano tlačno zarnaval 401-06 [pa]
20582100 pk40106 sum 9.8067 0.0 1
20582101 0.0 0.10197 p 401060000 -0.8425 rho 401060000
* cv 822 : dh korigirano tlačno zarnaval 852-01 [pa]
20582200 pk85201 sum 9.8067 0.0 1
20582201 0.0 0.10197 p 852010000 -0.15 rho 852010000 * R*
* cv 823 : dh korigirano tlačno zarnaval 852-10 [pa]
20582300 pk85202 sum 9.8067 0.0 1
20582301 0.0 0.10197 p 852100000 -0.15 rho 852100000 * R*
* cv 824 : dh korigirano tlačno zarnaval 854-05 [pa]
20582400 pk85401 sum 9.8067 0.0 1
20582401 0.0 0.10197 p 854050000 -0.15 rho 854050000 * R*
*****
* ccrv11 : dmeasured - gravity term - zanka 2
*****
** ta blok cv je uporabljen med rms2 dp inicializacijo
** upostevane so vse dh korekcije tlačnih zarnaval
*****
** cv 830 : dp21v [bar]
*20583000 dp21v sum 1.0e-05 -0.0763 0
*20583001 0.0 1.0 p 802010000 -1.0 p 803010000 * dh=0.0m
**
** cv 831 : dp21v [bar]
*20583100 dp21v sum 1.0e-05 -0.0792 0
*20583101 0.0 1.0 p 802020000 -1.0 p 802010000 1.0
cntrlvar 832
*20583101 0.0 1.0 cntrlvar 820 -1.0 p 802010000 1.0
cntrlvar 832
*****

```

```

** cv 832 : dp21v gravity term [pa]
*20583200 dp21v sum 9.8067 0.0 1
*20583201 0.0 1.7117 rho 802010000
**
** cv 833 : dp51 [bar]
*20583300 dp51 sum 1.0e-05 -0.0562 0
*20583301 0.0 1.0 p 401010000 -1.0 p 802020000 1.0
cntrlvar 834
*20583301 0.0 1.0 p 401010000 -1.0 cntrlvar 820 1.0
cntrlvar 834
**
** cv 834 : dp51 gravity term [pa]
*20583400 dp51 sum 9.8067 0.0 1
*20583401 0.0 0.364 rho 802020000
**
** cv 835 : hot leg dp [bar]
*20583500 hldp sum 1.0e-05 -0.2117 0
*20583501 0.0 1.0 p 401010000 -1.0 p 803010000 1.0 cntrlvar
836
**
** cv 836 : hldp gravity term [pa]
*20583600 dp21v sum 9.8067 0.0 1
*20583601 0.0 2.0957 rho 802010000
**
** cv 837 : dp52x [bar]
*20583700 dp52x sum 1.0e-05 -1.1424 0
*20583701 0.0 1.0 p 401060000 -1.0 p 401010000 1.0
cntrlvar 838
*20583701 0.0 1.0 cntrlvar 821 -1.0 p 401010000 1.0
cntrlvar 838
**
** cv 838 : dp52x gravity term [pa]
*20583800 dp21v sum 9.8067 0.0 1
*20583801 0.0 9.2065 rho 401020000
**
** cv 839 : dp53x [bar]
*20583900 dp53x sum 1.0e-05 -0.9681 0
*20583901 0.0 1.0 p 413010000 -1.0 p 401060000 1.0
cntrlvar 840
*20583901 0.0 1.0 p 413010000 -1.0 cntrlvar 821 1.0
cntrlvar 840
**
** cv 840 : dp53x gravity term [pa]
*20584000 dp21v sum 9.8067 0.0 1
*20584001 0.0 -9.2065 rho 401080000
**
** cv 841 : steam generator dp [bar]
*20584100 sgdp sum 1.0e-05 -2.1105 0
*20584101 0.0 1.0 p 413010000 -1.0 p 401010000 * dh=0.0m
**
** cv 842 : dp54 [bar]
*20584200 dp54 sum 1.0e-05 -0.1801 0
*20584201 0.0 1.0 p 852010000 -1.0 p 413010000 1.0
cntrlvar 843
*20584201 0.0 1.0 cntrlvar 822 -1.0 p 413010000 1.0
cntrlvar 843
**
** cv 843 : dp54 gravity term [pa]
*20584300 dp21v sum 9.8067 0.0 1
*20584301 0.0 -0.364 rho 852010000
*****

```

```

** cv 844 : dp22vg [bar]
*20584400 dp22vg sum 1.0e-05 -0.0576 0
*20584401 0.0 1.0 p 852010000 -1.0 p 852010000 1.0
cntrlvar 845
*20584401 0.0 1.0 cntrlvar 823 -1.0 cntrlvar 822 1.0
cntrlvar 845
**
** cv 845 : dp22vg gravity term [pa]
*20584500 dp22vg sum 9.8067 0.0 1
*20584501 0.0 -4.4007 rho 852020000
**
** cv 846 : dp22vp [bar]
*20584600 dp22vp sum 1.0e-05 -0.0634 0
*20584601 0.0 1.0 p 854010000 -1.0 p 852020000 1.0
cntrlvar 847
*20584601 0.0 1.0 cntrlvar 824 -1.0 cntrlvar 823 1.0
cntrlvar 847
**
** cv 847 : dp22vp gravity term [pa]
*20584700 dp22vp sum 9.8067 0.0 1
*20584701 0.0 1.967 rho 853010000
**
** cv 848 : intermediate leg dp [bar]
*20584800 hldp sum 1.0e-05 -0.3011 0
*20584801 0.0 1.0 p 854010000 -1.0 p 413010000 1.0
cntrlvar 849
*20584801 0.0 1.0 cntrlvar 824 -1.0 p 413010000 1.0
cntrlvar 849
**
** cv 849 : hldp gravity term [pa]
*20584900 dp21v sum 9.8067 0.0 1
*20584901 0.0 -2.797 rho 852020000
**
** cv 850 : dp22p [bar]
*20585000 dp22p sum 1.0e-05 0.0 1
*20585001 0.0 1.0 p 855010000 -1.0 p 854010000 1.0
cntrlvar 851
*20585001 0.0 1.0 p 855010000 -1.0 cntrlvar 824 1.0
cntrlvar 851
**
** cv 851 : dp22p gravity term [pa]
*20585100 dp22p sum 9.8067 0.0 1
*20585101 0.0 0.232 rho 854010000
**
** cv 852 : dp23h [bar]
*20585200 dp23h sum 1.0e-05 -0.0303 0
*20585201 0.0 1.0 p 856010000 -1.0 p 855010000 * dh=0.0m
**
*****
** segg
*****
*****
*****
*****

```

\* kkk : inicializacija uparjalnika  
 \* masa sekundarnega hladila je ustrezna (. = 790 kg - spodnja meja)  
 \* pri recirkulacijskem razmerju 4x  
 \* kasneje je bila masa ob dvignu nivoja povečana na 800 kg, downcomer  
 \* je nekoliko povečan, da preprečimo prelivanje kapljevine  
 \* odstopki tlaka na sekundarni strani (1.1 bar) zmanjšan z dvignom  
 \* tcolid na zgornjo tolerančno mejo (=0.5 k) --> psek skora)  
 \* spodnjo toleranco (68.7 bar) : 68.59 bar  
 \* rcs tcolid : 286.7 c +- 0.5 c (559.85 k)  
 \* .....  
 \* prim. sistem: eg vstop  
 \* 9110000 hl-eg englujn  
 \* \* 9110101 902010000 501000000 1.0936e-02 0.57 0.46 00100  
 \* 9110101 902010000 501000000 1.0936e-02 0.616 0.46 130100  
 \* 9110201 0 6.36790e+00 6.56940e+00 0.00000e+00  
 \* .....  
 \* prim. sistem: eg vstopni prekat in u-cevi  
 \* 5010000 eg-tube pipe  
 \* 5010001 11  
 \* \* 5010101 0.04394 1 0.010342 11  
 \* 5010201 0 10  
 \* 5010301 0.798 1 2.0 5 1.725 7 2.0 11  
 \* 5010401 0 11  
 \* 5010501 0 11  
 \* 5010601 85.0 1 90.0 5 45.0 6 -45.0 7 -90.0 11  
 \* 5010701 0.728 1 2.0 5 1.685 6 -1.685 7 -2.0 11  
 \* \* 5010801 0.1e-03 0.091 1 0.01e-03 0.01968 11  
 \* 5010801 0.1e-05 0.091 1 0.01e-07 0.01968 11  
 \* \* 5010901 0.44 0.60 1 0.01 0.01 5 0.22 0.22 6 0.01  
 \* 0.01 10  
 \* 5010901 0.01 0.01 1 0.0 0.0 10  
 \* 5011001 00 11  
 \* \* 5011101 00100 1 00000 10  
 \* 5011101 100000 10  
 \* 5011201 103 1.5555e+07 5.6374e+02 0.0000e+00 0 0 1  
 \* 5011202 103 1.5518e+07 5.6317e+02 0.0000e+00 0 0 2  
 \* 5011203 103 1.5482e+07 5.6265e+02 0.0000e+00 0 0 3  
 \* 5011204 103 1.5445e+07 5.6219e+02 0.0000e+00 0 0 4  
 \* 5011205 103 1.5410e+07 5.6178e+02 0.0000e+00 0 0 5  
 \* 5011206 103 1.5377e+07 5.6145e+02 0.0000e+00 0 0 6  
 \* 5011207 103 1.5358e+07 5.6135e+02 0.0000e+00 0 0 7  
 \* 5011208 103 1.5352e+07 5.6086e+02 0.0000e+00 0 0 8  
 \* 5011209 103 1.5345e+07 5.6060e+02 0.0000e+00 0 0 9  
 \* 5011210 103 1.5339e+07 5.6037e+02 0.0000e+00 0 0 10  
 \* 5011211 103 1.5335e+07 5.6018e+02 0.0000e+00 0 0 11  
 \* 5011300 0  
 \* 5011301 6.73340e+00 6.73340e+00 0.0000e+00 1  
 \* 5011302 6.72420e+00 6.72420e+00 0.0000e+00 2  
 \* 5011303 6.71600e+00 6.71600e+00 0.0000e+00 3  
 \* 5011304 6.70880e+00 6.70880e+00 0.0000e+00 4  
 \* 5011305 6.70230e+00 6.70230e+00 0.0000e+00 5  
 \* 5011306 6.69730e+00 6.69730e+00 0.0000e+00 6  
 \* 5011307 6.69270e+00 6.69270e+00 0.0000e+00 7

5011308 6.68790e+00 6.68790e+00 0.0000e+00 8  
 5011309 6.68370e+00 6.68370e+00 0.0000e+00 9  
 5011310 5.86580e+00 5.86580e+00 0.0000e+00 10  
 5011401 0.1968 0.0 1.0 1.0 10  
 \* prim. sistem: eg izstopni prekat  
 \* 5130000 o-ch branch  
 \* 5130001 1 0  
 \* \* 5130101 0.0 0.0 7.98 35.061e-03 0.0 -85.0 -0.728 0.1e-03  
 \* 0.091 00  
 \* 5130201 0.0 0.0 7.98 35.061e-03 0.0 -85.0 -0.728 0.1e-04  
 \* 0.091 00  
 \* 5130202 103 1.5347e+07 5.6018e+02  
 \* \* 5131101 501010000 513000000 0.010342 0.40 0.44 00100  
 \* 5131101 501010000 513000000 0.010342 0.3 0.2 130000  
 \* 513' 6.67690e+00 6.96280e+00 0.00000e+00  
 \* .....  
 \* prim. sistem: eg izstop  
 \* 9610000 eg-cl englujn  
 \* \* 9610101 513010000 952000000 1.0936e-02 0.46 0.57 00100  
 \* 9610101 513010000 952000000 1.0936e-02 0.01 0.02 130100  
 \* 9610201 0 6.31440e+00 6.51290e+00 0.00000e+00  
 \* .....  
 \* sek. sistem: dvizni kanal  
 \* 5030000 riser pipe  
 \* 5030001 6  
 \* 5030101 0.0 6  
 \* 5030201 0.01291 1 0.0214 4 0.048695 5  
 \* 5030301 2.0 4 2.9605 5 0.8295 6  
 \* \* povečanje mase sekundarnega hladila  
 \* \*\* 5030401 0.13513 4 0.17171 5 0.04041 6  
 \* 5030401 0.12513 4 0.18171 5 0.04041 6  
 \* 5030501 0 6  
 \* 5030601 90.0 6  
 \* 5030701 2.0 4 2.9605 5 0.8295 6  
 \* 5030801 0.1e-03 0.0303 5 0.1e-03 0.249 6  
 \* 5030901 5.46 5.46 1 3.32 3.32 4 0.1 0.1 5  
 \* 5031001 00 6  
 \* 5031101 100100 4 100000 5  
 \* 5031201 100 6.88635e+06 1.24544e+06 2.58278e+06 6.52236e-02  
 \* 0.00000e+00 1  
 \* 5031202 100 6.87346e+06 1.25147e+06 2.58289e+06 1.89380e-01  
 \* 0.00000e+00 2  
 \* 5031203 100 6.86224e+06 1.25111e+06 2.58298e+06 2.99390e-01  
 \* 0.00000e+00 3  
 \* 5031204 100 6.85241e+06 1.25062e+06 2.58305e+06 3.94690e-01  
 \* 0.00000e+00 4  
 \* 5031205 100 6.84126e+06 1.25006e+06 2.58314e+06 4.19940e-01  
 \* 0.00000e+00 5  
 \* 5031206 100 6.83290e+06 1.24938e+06 2.58318e+06 4.01729e-01  
 \* 0.00000e+00 6  
 \* 5031300 0  
 \* 5031301 4.72634e-02 2.73670e-01 0.00000e+00 1  
 \* 5031302 5.1251e-02 3.89160e-01 0.00000e+00 2  
 \* 5031303 5.53478e-02 4.40620e-01 0.00000e+00 3  
 \* 5031304 6.0600e-02 4.89430e-01 0.00000e+00 4  
 \* 5031305 7.43053e-02 7.34650e-01 0.00000e+00 5  
 \* 5031401 0.027 0.0 1.0 1.0 5  
 \* .....  
 \* sek. sistem: separator pare  
 \* 5070000 sepr separator  
 \* 5070001 5

5070001 3 0  
 5070101 0.0 1.9430 0.09467 0 90.0 1.9430 0.1e-04 0.249  
 00  
 5070200 100 6.82488e+06 1.24924e+06 2.58322e+06 1.46505e-01  
 5071101 507010000 510000000 4.8695e-02 0.82 0.14 01000  
 0.0  
 5072101 507000000 508000000 44.9150e-02 0.26 0.23 01000  
 0.0  
 5073101 503010000 507007000 4.8695e-02 0.0 0.0 01000  
 5071201 -9.28200e-02 3.06330e-01 0.00000e+00  
 5072201 4.68581e-03 -1.70166e-02 0.00000e+00  
 5073201 7.22506e-02 7.61480e-01 0.00000e+00  
 \* sek. sistem: zgornji parni prostor  
 \* 5100000 standone pipe  
 \* 5100001 2  
 \* 5100101 0.0 2  
 \* 5100201 0.0 1  
 \* 5100301 1.0800 1 0.4000 2  
 \* 5100401 0.54287 1 0.134040 2  
 \* 5100501 0.0 2  
 \* 5100601 90.0 2  
 \* 5100701 1.0800 1 0.4000 2  
 \* 5100801 0.1e-03 0.8000 1 0.1e-03 0.41905 2  
 \* 5100901 0.0 0.0 1  
 \* 5101001 00 2  
 \* 5101101 100000 1  
 \* 5101201 102 6.81865e+06 1.00000e+00 0.00000e+00 0 0 1  
 \* 5101202 102 6.81840e+06 1.00000e+00 0.00000e+00 0 0 2  
 \* 5101300 0  
 \* 5101301 -9.21296e-03 4.43731e-02 0.00000e+00 1  
 \* .....  
 \* sek. sistem: spoj uparjalnika in parovoda  
 \* 5110000 sg-sl englujn  
 \* 5110101 51010000 520000000 0.0011401 0.222 1.6 130100  
 \* 5110201 0 6.85760e+00 6.87050e+00 0.00000e+00  
 \* .....  
 \* sek. sistem: povratni kanal (zgornji obročasti del)  
 \* 5190000 udownann branch  
 \* 5190001 1 0  
 \* 5190101 0.0 1.9430 0.3078 0 90.0 1.9430 0.1e-03 0.1930  
 00  
 5190200 102 6.82494e+06 1.01000e-03  
 \* 5191101 510000000 519010000 0.44915 0.0 0.0 00100  
 5191101 510000000 519010000 0.0 0.5 0.5 130100  
 5191110 0.1930 0.0 1.0 1.0  
 5191201 3.94500e-01 3.67449e-04 0.00000e+00  
 \* .....  
 \* sek. sistem: povratni kanal (srednji obročasti del)  
 \* 5080000 udownann branch  
 \* 5080001 2 0  
 \* 5080101 0.0 0.8275 0.081723 0 -90.0 -0.8275 0.1e-03  
 0.176 00  
 5080200 102 6.83416e+06 0.00000e+00  
 5081101 519000000 508000000 0.0 0.09 0.15 00000  
 \* 5082101 508010000 509000000 0.030413 0.0 0.0 00100  
 5082110 0.1930 0.0 1.0 1.0  
 5082120 1.76446e-04 -3.00110e-01 0.00000e+00  
 5082201 1.16890e-01 1.38490e-01 0.00000e+00  
 \* sek. sistem: povratni kanal (spodnji cevni del)  
 \* 5090000 pipedown pipe  
 \* 5090001 5  
 5090101 0.0 5



```

15102601 510010000 0 1 0 3 3870 1
15102701 0 0 0 0 1
15102801 0 10 10 0 0 0 0 1 1
15102901 0 10 10 0 0 0 0 1 1
*
15103000 1 4 1 1 0 0
15103100 0 1
15103201 0 0 0.0947
15103301 1 3
15103401 0 0 3
15103501 597.0 1 588.0 2 570.0 3 561.0 4
15103601 0 0 0 0 0.4463 1
15103701 519010000 0 1 0 0.4463 1
15103801 0 0 0 1
15103901 0 10 10 0 0 0 1 1
15104000 1 4 1 1 0 0
15104100 0 1
15104200 3 0.0245
15104301 1 3
15104401 0 0 3
15104501 597.0 1 588.0 2 570.0 3 561.0 4
15104601 508010000 0 1 0 3.2448 1
15104701 0 0 0 0 1
15104801 0 10 10 0 0 0 1 1
15104901 0 10 10 0 0 0 1 1
*
*****
* downcomer --> plošce 5091-01, 5092-01-02-03-04
15091000 1 4 1 1 0 0
15091100 0 1
15091201 3 0.00394
15091301 0 0 3
15091401 597.0 1 588.0 2 570.0 3 561.0 4
15091501 0 0 0 0 4.0116 1
15091601 509010000 0 1 0 4.0116 1
15091701 0 0 0 0 1
15091801 0 10 10 0 0 0 1 1
15091901 0 10 10 0 0 0 1 1
*
15092000 4 4 1 1 0 0
15092100 0 1
15092201 3 0.00276
15092301 1 3
15092401 0 0 3
15092501 597.0 1 588.0 2 570.0 3 561.0 4
15092601 0 0 0 1.2028 1
15092701 0 0 0 1.2028 2
15092801 0 0 0 1.2028 3
15092901 0 0 0 1.2028 4
15093000 509020000 0 1 0 1.2028 1
15093100 509030000 0 1 0 1.2028 2
15093200 509040000 0 1 0 1.2028 3
15093300 509050000 0 1 0 1.2028 4
15093400 509060000 0 1 0 1.2028 1
15093500 509070000 0 1 0 1.2028 2
15093600 509080000 0 1 0 1.2028 3
15093700 509090000 0 1 0 1.2028 4
15093800 0 10 10 0 0 0 1 1
15093901 0 10 10 0 0 0 1 1
*
*****
* sg3 kontrolne spreminiljive
*
*****
* sggccvv sg 3 kontrolne spreminiljive
*
*****

```

```

* cv 503: sg3: nivo v povratnem kanalu [m]
20550300 levdc sum 1.0 13.45 1
20550301 0 2.0 voidf 509050000 2.0 voidf 509040000
20550302 2.0 voidf 509030000 2.0 voidf 509020000
20550303 2.9625 voidf 509010000 0.8275 voidf 508013000
20550304 1.9430 voidf 519010000
*
* cv 505: sg3: masa sekundarnega hladila [kg]
20550500 segmas sum 1.0 790.0 1
** 20550501 0.0 0.11513 rho 503010000 0.11513 rho
503020000
** 20550502 0.11513 rho 503030000 0.11513 rho
503040000
** 20550503 0.17171 rho 503050000 0.04041 rho
503060000
20550501 0.0 0.12513 rho 503010000 0.12513 rho 503020000
20550502 0.12513 rho 503030000 0.12513 rho 503040000
20550503 0.18171 rho 503050000 0.04041 rho 503060000
20550504 0.09466 rho 507010000 0.54287 rho 510010000
20550505 0.13404 rho 510020000 0.30780 rho 519010000
20550506 0.08172 rho 508010000 0.06909 rho 509010000
20550507 0.01167 rho 509020000 0.01167 rho 509030000
20550508 0.01167 rho 509040000 0.01456 rho 509050000
*
*****
* main feedwater 3
*
*****
* mfff
*
*****
* konstantni mfw tok
5340000 mfw tmpjurn
5340101 531000000 532000000 0.0266
5340200 1 505 * si
5340201 -1.0 0.52517 0. 0.
5340202 0.0 0.52517 0. 0.
5340203 6.0 0.0 0. 0.
*
* volumski mfw tok
*20550200 vmfw div 1.0 0.0 1
*20550201 tbof 532010000 mflow 532010000
*
* feedwater line
5320000 fwlins branch
5320001 0
5320101 5.5575-04 10.0 0 0 60.0 7.0 0.01e-03 0.0266 00
5320200 103 6.86275e+06 4.90974e-02
*5321101 532010500 508050000 0.006786 0. 0. 00100
5321101 532010000 508000000 0.0 1.0 0. 130100
5321201 1.11560e+00 1.11560e+00 0.00000e+00
*
* vir napajalne vode
5310000 fsource tmpjvcl
5310101 1.0 0.0 10.0 0 0 0 0.01e-03 0.0 00
5310200 103
5310201 0 70.0+5 491.0
*
*****

```

```

* ccci "regulacija" sg3 nivoja
* ob konstantni mfw 534 reguliramo nivo v povratnem kanalu
5390000 v529 tmpjvcl
5290101 1.0 0.0 10.0 0 0 0.0 0.0 0.2e-03 0.0 0
5290200 103
5290201 0 70.0+5 491.0
*
5100000 j530 tmpjurn
5300101 529000000 519010000 0.0
5300200 1 0 cntrivar 503 * sg level
5300201 -1.0 0.0 0.0 0.0 0.0
5300202 13.35 0.0 1.5 0.0 0.0 0.0
5300203 13.45 0.0 0.0 0.0 0.0 0.0
5300204 13.55 -1.5 0.0 0.0 0.0 0.0
*
*5300000 j530 tmpjurn
*5300101 529000000 519010000 0.0
*5300200 1 0 cntrivar 503 * sg mass
*5300201 -1.0 0.0 0.0 0.0 0.0 0.0
*5300202 790.0 1.5 0.0 0.0 0.0
*5300203 800.0 0.0 0.0 0.0 0.0
*5300204 810.0 -0.50 0.0 0.0 0.0
*
*****
*
*****
* sell parovod 3
*
*****
*
*****
* steam line from povr-sv-mliv
5200005 stmlins sgvliv
5200101 0.0 31.65 68.5e-03 0 -45.0 -18.670 0.01-3 0.0525
00
5200200 102 6.81255e+06 1.00000e+00
*
* hhas
* 15201000 1 4 2 1 0.0525
15201000 1 4 2 0 0.0525 * ffl1
15201100 0 1
15201101 3 0.0603
15201201 1 3
15201301 0 0 3
15201401 570.330 1 566.810 2 563.420 3 560.15 4
15201501 520010000 0 1 1 31.65 1
15201601 0 0 0 1 31.65 1
15201701 0 0 0 0 1
15201801 0 10 10 0 0 0 1 1
15201901 0 10 10 0 0 0 1 1
*
*****
* ccci regulacija tcold 3 preko tlaka sekundarne strani
*
*****
*
*****
* delta tcold : bethey referenca : 55.85 k
20550000 dtcold sum 1.0 0.0 0
20550001 560.35 -1.0 tempf 955010000
* 20550001 559.35 -1.0 tempf 955010000 * #
20554400 p544 sum 1.0 68 12e-05 0

```









```

**
** 20553601 0.0 2.0957 rho 902010000
**
**
** cv 937 : dp62x [bar]
** 20593700 dp62x sum 1.0e-05 -1.1424 0
** 20593701 0.0 1.0 p 501060000 -1.0 p 501010000 1.0
** cntrlvar 938
** 20593701 0.0 1.0 cntrlvar 921 -1.0 p 501010000 1.0
** cntrlvar 938
**
**
** cv 938 : dp62x gravity term [pa]
** 20593800 dp62x sum 9.8067 0.0 1
** 20593801 0.0 9.2065 rho 501020000
**
**
**
** cv 939 : dp63x [bar]
** 20593900 dp63x sum 1.0e-05 -0.9681 0
** 20593901 0.0 1.0 p 513010000 -1.0 p 501060000 1.0
** cntrlvar 940
** 20593901 0.0 1.0 p 513010000 -1.0 cntrlvar 921 1.0
** cntrlvar 940
**
**
** cv 940 : dp63x gravity term [pa]
** 20594000 dp63x sum 9.8067 0.0 1
** 20594001 0.0 -9.2065 rho 501080000
**
**
**
** cv 941 : steam generator dp [bar]
** 20594100 sgdp sum 1.0e-05 -2.1105 0
** 20594101 0.0 1.0 p 513010000 -1.0 p 501010000 * dh=0.0m
**
**
**
** cv 942 : dp64 [bar]
** 20594200 dp64 sum 1.0e-05 -0.1801 0
** 20594201 0.0 1.0 p 952010000 -1.0 p 513010000 1.0
** cntrlvar 943
** 20594201 0.0 1.0 cntrlvar 922 -1.0 p 513010000 1.0
** cntrlvar 943
**
**
** cv 943 : dp64 gravity term [pa]
** 20594300 dp64 sum 9.8067 0.0 1
** 20594301 0.0 -0.364 rho 952010000
**
**
**
** cv 944 : dp32vg [bar]
** 20594400 dp32vg sum 1.0e-05 -0.0576 0
** 20594401 0.0 1.0 p 952020000 -1.0 p 952010000 1.0
** cntrlvar 945
** 20594401 0.0 1.0 cntrlvar 923 -1.0 cntrlvar 922 1.0
** cntrlvar 945
**
**
** cv 945 : dp32vg gravity term [pa]
** 20594500 dp32vg sum 9.8067 0.0 1
** 20594501 0.0 -4.4007 rho 952020000
**
**
**
** cv 946 : dp32vp [bar]
** 20594600 dp32vp sum 1.0e-05 -0.0634 0
** 20594601 0.0 1.0 p 954010000 -1.0 p 952020000 1.0
** cntrlvar 947
** 20594601 0.0 1.0 cntrlvar 924 -1.0 cntrlvar 923 1.0
** cntrlvar 947
**
**
** cv 947 : dp32vp gravity term [pa]
** 20594700 dp32vp sum 9.8067 0.0 1
** 20594701 0.0 1.967 rho 953010000
**
**
**
** cv 948 : intermediate leg dp [bar]
** 20594800 i1dp sum 1.0e-05 -0.3011 0
** 20594801 0.0 1.0 p 954010000 -1.0 p 513010000 1.0
** cntrlvar 949
** 20594801 0.0 1.0 cntrlvar 924 -1.0 p 513010000 1.0
** cntrlvar 943
**
**
** cv 949 : i1dp gravity term [pa]
** 20594900 dp32p sum 9.8067 0.0 1
** 20594901 0.0 -2.797 rho 952020000
**
**
**
** cv 950 : dp32p [bar]
** 20595000 dp32p sum 1.0e-05 0.0 1
** 20595001 0.0 1.0 p 955010000 -1.0 p 954010000 1.0
** cntrlvar 951
** 20595001 0.0 1.0 p 955010000 -1.0 cntrlvar 924 1.0
** cntrlvar 951
**
**
** cv 951 : dp32p gravity term [pa]
** 20595100 dp32p sum 9.8067 0.0 1
** 20595101 0.0 0.232 rho 954010000
**
**
**
** cv 952 : dp33h [bar]
** 20595200 dp33h sum 1.0e-05 -0.0303 0
** 20595201 0.0 1.0 p 956010000 -1.0 p 955010000 * dh=0.0m
**
**
**
**
**
**
**
**
**
**
** cv 953 : dp052 [bar]
** 20595300 dp052 sum 1.0e-05 -0.5301 0
** 20595301 0.0 1.0 p 119040000 -1.0 p 956010000 1.0 cntrlvar
954
**
**
** cv 954 : dp052 gravity term [pa]
** 20595400 dp052 sum 9.8067 0.0 1
** 20595401 0.0 -4.498 rho 119030000
**
**
**
** cv 955 : dp053 [bar]
** 20595500 dp053 sum 1.0e-05 -0.9551 0
** 20595501 0.0 1.0 p 123010000 -1.0 p 119040000 1.0 cntrlvar
956
**
**
** cv 956 : dp053 gravity term [pa]
** 20595600 dp053 sum 9.8067 0.0 1
** 20595601 0.0 -1.503 rho 119050000
**
**
**
** cv 957 : dp0200 [bar]
** 20595700 dp0200 sum 1.0e-05 -1.2043 0
** 20595701 0.0 1.0 p 141010000 -1.0 p 123010000 1.0 cntrlvar
958
**
**
** cv 958 : dp0200 gravity term [pa]
** 20595800 dp0200 sum 9.8067 0.0 1
** 20595801 0.0 5.552 rho 131070000
**
**
**
** cv 959 : dp6-3 [bar]

```







```

* cv 221: core bypass heat losses
20522100 cobyhl function 1.0 0.0 1 3 -4576.0 0.0
20522101 tempf 131010000 221
20222100 reac-t 670
20222101 -1.0 0.0
20222102 298.0 0.0
20222103 560.0 -4576.0
*
* cv 222: upper plenum + upper head heat losses
20522200 sphl function 1.0 0.0 1 3 -6292.0 0.0
20522201 tempf 153010000 222
20222200 reac-t 670
20222201 -1.0 0.0
20222202 298.0 0.0
20222203 560.0 -6292.0
*
* cv 223: reactor downcomer heat losses
20522300 dmhl function 1.0 0.0 1 3 -6032.0 0.0
20522301 tempf 119040000 223
20222300 reac-t 670
20222301 -1.0 0.0
20222302 298.0 0.0
20222303 560.0 -6032.0
*
* cv 224: cold leg 1 heat losses
20522400 clhl function 1.0 0.0 1 3 -5156.0 0.0
20522401 tempf 653010000 224
20222400 reac-t 670
20222401 -1.0 0.0
20222402 298.0 0.0
20222403 560.0 -5156.0
*
* cv 225: steam generator 1 heat losses
20522500 sg1hl function 1.0 0.0 1 3 -18096.0 0.0
20522501 tempf 303020000 225
20222500 reac-t 670
20222501 -1.0 0.0
20222502 298.0 0.0
20222503 555.0 -18096.0
*
* cv 226: hot leg 1 heat losses
20522600 hlhl function 1.0 0.0 1 3 -2704.0 0.0
20522601 tempf 656010000 226
20222600 reac-t 670
20222601 -1.0 0.0
20222602 298.0 0.0
20222603 564.0 -2704.0
*
* cv 227: cold leg 2 heat losses
20522700 cl2hl function 1.0 0.0 1 3 -5156.0 0.0
20522701 tempf 853010000 224
*
* cv 228: steam generator 2 heat losses
20522800 sg2hl function 1.0 0.0 1 3 -18096.0 0.0
20522801 tempf 303020000 225
20222800 reac-t 670
20222801 -1.0 0.0
20222802 298.0 0.0
20222803 555.0 -18096.0
*
* cv 229: hot leg 2 heat losses
20522900 hl2hl function 1.0 0.0 1 3 -2704.0 0.0
20522901 tempf 856010000 226
20222900 reac-t 670
20222901 -1.0 0.0
20222902 298.0 0.0
20222903 560.0 -2704.0
*
* cv 230: cold leg 3 heat losses
20523000 cl3hl function 1.0 0.0 1 3 -5356.0 0.0
20523001 tempf 953010000 224
20223000 reac-t 670
20223001 -1.0 0.0
20223002 298.0 0.0
20223003 568.0 -5356.0
*
* cv 231: steam generator 3 heat losses
20523100 sg3hl function 1.0 0.0 1 3 -18096.0 0.0
20523101 tempf 503020000 225
20223100 reac-t 670
20223101 -1.0 0.0
20223102 298.0 0.0
20223103 568.0 -18096.0
*
* cv 232: hot leg 3 heat losses
20523200 hl3hl function 1.0 0.0 1 3 -2704.0 0.0
20523201 tempf 956010000 226
20223200 reac-t 670
20223201 -1.0 0.0
20223202 298.0 0.0
20223203 568.0 -2704.0
*
* cv 233: surge line heat losses
20523300 slhl function 1.0 0.0 1 3 -3560.0 0.0
20523301 tempf 215010000 233
20223300 reac-t 670
20223301 -1.0 0.0
20223302 298.0 0.0
20223303 568.0 -3560.0
*
* cv 234: pressurizer heat losses
20523400 przh function 1.0 0.0 1 3 -4000.0 0.0
20523401 tempf 203020000 234
20223400 reac-t 670
20223401 -1.0 0.0
20223402 298.0 0.0
20223403 618.0 -4000.0
*
* cv 235: system heat losses
20523500 sumhl sum 1.0 0.0 1
20523501 0.0 1.0 cctrlvar 220 1.0 cctrlvar 221 1.0 cctrlvar
222
20523502 1.0 cctrlvar 223 1.0 cctrlvar 224 1.0 cctrlvar
225
20523503 1.0 cctrlvar 226 1.0 cctrlvar 227 1.0 cctrlvar
228
20523504 1.0 cctrlvar 229 1.0 cctrlvar 230 1.0 cctrlvar
231
20523505 1.0 cctrlvar 232 1.0 cctrlvar 233 1.0 cctrlvar
234
20523506 3.0 cctrlvar 701
*
* hhs heat structure thermal property data
*
* comparison report dodatk1
20516000 avgrhof sum 0.0833 0.0 1
20516001 0.0 1.0 rhof 131010000 1.0 rhof 131020000 1.0 rhof
131030000
20516002 1.0 rhof 131040000 1.0 rhof 131050000 1.0 rhof
131060000
20516003 1.0 rhof 131070000 1.0 rhof 131080000 1.0 rhof
131090000
20516004 1.0 rhof 131100000 1.0 rhof 131110000 1.0 rhof
131120000
*
20516100 clevl sum 1.0 0.0 1 * 101.94 = 1000*1/9.81
[pa-->pa]
20516101 0.0 101.94 cctrlvar 240 -5.81 rhog 131040000
20516200 clev2 sum 1.0 0.0 1
20516201 0.0 1.0 cctrlvar 160 -1.0 rhog 131060000
*
* ctv 161: collapsed liquid core level (m)
20516300 corelevl div 1.0 0.1 3 0.0 9.5
20516301 cctrlvar 162 cctrlvar 161
*
* cv 146: maximum htemp ix core, right-wall surface
20514600 maxwxt stdfnctn 1.0 600. 1
20514601 max htemp 131000106 htemp 131000206
20514602 htemp 131000306 htemp 131000406
20514603 htemp 131000506 htemp 131000606
20514604 htemp 131000706 htemp 131000806
*
* composition type and data format

```



```
20514505      httemp 131000806 httemp 131001006
20514506      httemp 131000906 httemp 131001206
*
* recetno stanje: wcp(0) + mem2(0) + mem3(0)
*      1949 KG + 286 KG + 286 KG * 2521 KG
20517000 wcp sum 1.0 1949.0 0
20517001 2521.0 -1.0 cntrlvar 271 -1.0 cntrlvar 275
20517002 -1.0 cntrlvar 276 +1.0 cntrlvar 274
*
*****
*
*      . **** end ****
```

# Appendix A - Listing of the middle BETSY nodalization - restart input

```

* bethsy - bethalhi.dat restart (100 - 8630.0 sec)
* comparison report zahteva dodatne cv
*
*
* spuscena spodnja meja s. lastnosti za borov nitrid
*
* v post-test preračunu (november 91 -->):
* odprava separatorjev
* abrupt-normal zlom
* razširjena tabela topl. prev. za material 1 (brez
ekstrapolacije)
*
* končni spoj-zlom iz btestm2n2.dat (junij 1993)
* niso upošteevane tudi nbam31.dat spremembe (se isamo npr
mtrlv 183)
*
* zlom v 300. sekundi
*
* ** opozorilo !
*
100 restart transnt
101 8000
*
201 1450.0 1.0-6 0.02 3 500 25000 25000
202 1700.0 1.0-6 0.005 3 2000 40000 40000
203 8630.0 1.0-6 0.02 3 500 25000 25000
* 202 2800.0 1.0-6 0.04 3 500 25000 25000
* 202 1400.0 1.0-6 0.04 3 500 25000 25000
*
*
*****
** msee requested minor edit
*****
**
*301 voidg 603010000 * albc1: h11 spool piece void
fraction [ ]
*302 voidg 656010000 * albf1: c11 spool piece void
fraction [ ]
*303 voidg 803010000 * albc2: h12 spool piece void
fraction [ ]
*304 voidg 856010000 * albf2: c12 spool piece void
fraction [ ]
*305 voidg 903010000 * albc3: h13 spool piece void
fraction [ ]
*306 voidg 956010000 * albf3: c13 spool piece void
fraction [ ]
**
*** dp = p(low press. tap) - p(high press. tap)
**
*307 cntrlvar 240 * dp0200 : core heat. length diff.
press. [kpa]
*308 cntrlvar 241 * dpup1 : upper plenum diff.
press. [kpa]
*309 cntrlvar 242 * dp034 : guide tube dif. press.
[kpa]
*310 cntrlvar 243 * dpuhead : upper head dif. press.
[kpa]

```

```

*311 cntrlvar 244 dif. p. [kpa]
*312 cntrlvar 245 press. [kpa]
**
*313 cntrlvar 246 [kpa]
*314 cntrlvar 247 [kpa]
*315 cntrlvar 248 dif. p. [kpa]
*316 cntrlvar 249 side diff. p. [kpa]
**
*317 cntrlvar 250 [kpa]
*318 cntrlvar 251 [kpa]
*319 cntrlvar 252 dif. p. [kpa]
*320 cntrlvar 253 side diff. p. [kpa]
**
*321 cntrlvar 254 [kpa]
*322 cntrlvar 255 [kpa]
*323 cntrlvar 256 dif. p. [kpa]
*324 cntrlvar 257 side diff. p. [kpa]
**
*325 cntrlvar 258 outlet diff. p. [kpa]
*326 cntrlvar 259 press. [kpa]
*327 cntrlvar 260 dif. p. [kpa]
*328 cntrlvar 261 diff. press. [kpa]
**
*329 cntrlvar 262 outlet diff. p. [kpa]
*330 cntrlvar 263 press. [kpa]
*331 cntrlvar 264 dif. p. [kpa]
*332 cntrlvar 265 diff. press. [kpa]
**
*333 cntrlvar 266 outlet diff. p. [kpa]
*334 cntrlvar 267 press. [kpa]
*335 cntrlvar 268 dif. p. [kpa]
*336 cntrlvar 269 diff. press. [kpa]
**
*337 cntrlvar 270 press. [kpa] ***
**
* dp050 : downcomer to upp. head
* dp0r1 : pressure vessel dif.
*
* dp1 : c11 to h11 diff. press.
* dp12pg : pump 1 diff. press.
* dp12vg : loop seal 1 downf. side
* dp12vp : loop seal 1 upflow.
* dp2 : c12 to h12 diff. press.
* dp22pg : pump 2 diff. press.
* dp22vg : loop seal 2 downf. side
* dp22vp : loop seal 2 upflow.
* dp3 : c13 to h13 diff. press.
* dp32pg : pump 3 diff. press.
* dp32vg : loop seal 3 downf. side
* dp32vp : loop seal 3 upflow.
* dp4 : sg1 u-tube in. to
* dp41 : sg1 inlet plenum diff.
* dp426 : sg1 u-tube upflow side
* dp4r2 : sg1 boiler section
* dp5 : sg2 u-tube in. to
* dp51 : sg2 inlet plenum diff.
* dp526 : sg2 u-tube upflow side
* dp5r2 : sg2 boiler section
* dp6 : sg3 u-tube in. to
* dp61 : sg3 inlet plenum diff.
* dp626 : sg3 u-tube upflow side
* dp6r2 : sg3 boiler section
* dpp1 : pressurizer diff.

```

```

*338 cntrlvar 271 mass flow [kg]
*339 cntrlvar 274 mass flow [kg]
*340 cntrlvar 305 invet. [kg]
*341 cntrlvar 405 invet. [kg]
*342 cntrlvar 505 invet. [kg]
*343 cntrlvar 275 invetory [kg]
*344 cntrlvar 276 invetory [kg]
**
*345 cntrlvar 277 [mpa]
*346 cntrlvar 278 [mpa]
*347 cntrlvar 279 [mpa]
*348 cntrlvar 280 pressure [mpa]
*349 cntrlvar 281 pressure [mpa]
*350 cntrlvar 282 pressure [mpa]
**
*351 mflowj 123010000 rate [kg/s]
*352 mflowj 332010000 rate [kg/s]
*353 mflowj 432010000 rate [kg/s]
*354 mflowj 532010000 rate [kg/s]
*355 mflowj 180000000 [kg/s]
*356 mflowj 311000000 flow rate [kg/s]
*357 mflowj 411000000 flow rate [kg/s]
*358 mflowj 511000000 flow rate [kg/s]
*359 mflowj 807000000 rate [kg/s]
*360 mflowj 907000000 rate [kg/s]
**
*361 cntrlvar 283 [kj/kg]
**
*362 tempf 123010000 * tf012a : core inlet temperature [k]
*363 tempf 141010000 * tf0304 : core outlet temperature [k]
*364 tempf 151010000 * tf041 : upper head (bottom) temperature [k]
*365 tempf 153010000 * tf042 : upper head (top) temperature [k]
*366 tempf 602010000 * tf112 : hot leg 1 temperature [k]
* intqmb : time integrated break
* intqms1 : time integrated lpsi
* mgv1 : sg1 secondary side mass
* mgv2 : sg2 secondary side mass
* mgv3 : sg3 secondary side mass
* mm2 : accumulator 2 mass
* mm3 : accumulator 3 mass
* p+47 : sg1 steam dome pressure
* p+57 : sg2 steam dome pressure
* p+67 : sg3 steam dome pressure
* p+p : pressurizer top
* p+sm2 : accumulator 2 gas phase
* p+sm3 : accumulator 3 gas phase
* qm05 : downcomer mass flow
* qman1 : sg1 feedwater mass flow
* qman2 : sg2 feedwater mass flow
* qman3 : sg3 feedwater mass flow
* qmb : break mass flow rate
* qmgv11 : sg1 steam line mass flow rate [kg/s]
* qmgv12 : sg2 steam line mass flow rate [kg/s]
* qmgv13 : sg3 steam line mass flow rate [kg/s]
* qmeb12 : lpsi in c12 mass flow
* qmeb13 : lpsi in c13 mass flow
* sebreak : break specific enthalpy [kj/kg]

```

```

*367 tempf 655010000 * tf133 : cold leg 1 temperature
[k]
*368 tempf 802010000 * tf212 : hot leg 2 temperature
[k]
*369 tempf 855010000 * tf233 : cold leg 2 temperature
[k]
*370 tempf 902010000 * tf312 : hot leg 3 temperature
[k]
*371 tempf 955010000 * tf333 : cold leg 3 temperature
[k]
*372 tempf 309050000 * tf454c : bottom of sg1 downcomer
temperature [k]
*373 tempf 409050000 * tf554c : bottom of sg2 downcomer
temperature [k]
*374 tempf 509050000 * tf654c : bottom of sg3 downcomer
temperature [k]
**
*375 httemp 131000701 * ts02091 :
*376 httemp 131000801 * ts02151 :
*377 httemp 131000901 * ts02191 : rod temperature from
middle to
*378 httemp 131001001 * ts02201 : top core elevation [k]
*379 httemp 131001101 * ts02241 : ** ts = ? (le oemba v
tab 1 str.28/87)
*380 httemp 131001201 * ts02281 :
*381 cntrlvar 146 * tmax : max. clad temperature
[k]
**
*382 cntrlvar 286 * vp1 : pump 1 rotation speed
[rpm]
*383 cntrlvar 287 * vp2 : pump 2 rotation speed
[rpm]
*384 cntrlvar 288 * vp3 : pump 3 rotation speed
[rpm]
**
*385 cntrlvar 289 * w+02 : core (electrical) power
[kw]
*386 cntrlvar 290 * w+trac : trace heating [kw]
**
*387 cntrlvar 110 * zt0200 : core level [m]
*388 cntrlvar 291 * zscore : swollen level [m]
**
*389 dt 0 * dtcalc : time step along
transient [s]
*390 emass 0 * mer : mass error [kg]
**
*****
**
** dodadni *kontrolni* izpis:
**
*391 cntrlvar 111 * reactor vessel level [m]
*392 cntrlvar 203 * prz level [m]
*393 cntrlvar 303 * sg 1 downcomer level [m]
*394 cntrlvar 403 * sg 2 downcomer level [m]
*395 cntrlvar 503 * sg 3 downcomer level [m]
*396 cntrlvar 235 * heat losses [W]
*397 cntrlvar 283 * sebreak : break specific enthalpy
[kj/kg]
*398 cntrlvar 295 * sebreak : break specific enthalpy
[kj/kg]
**
*****

```

```

*
* comparison report variables request
*
301 cntrlvar 280 * p+p : PRESSURIZER TOP PRESSURE
[mpa]
302 cntrlvar 278 * p+57 : sg2 STEAM DOME PRESSURE
[mpa]
303 cntrlvar 163 * zt0200 : CORE COLLAPSED LIQUID
LEVEL [M]
304 tempf 131120000 * tf03046 : COOLANT OUTLET STEAM
TEMPERATURE [k]
305 cntrlvar 146 * tmax : MAX. CLAD WALL
TEMPERATURE [k]
306 voidg 656070000 * albf1 : FULL SPOOL PIRCE VOID
FRACTION [ ] R+
307 mflowj 180000000 * qmb : BREAK MASS FLOW RATE
[KG/S]
308 cntrlvar 405 * mgv2 : sg2 SECONDARY SIDE MASS
INVT. [KG]
309 cntrlvar 170 * mcp : PRIMARY MASS INVENTORY
[KG]
*
310 cntrlvar 271 * in+qmb : BREAK DISCHARGED MASS
[KG]
*
313 cntrlvar 110 * zt0200 : SIMPL. CORE COLLAPSED
LIQUID LEVEL [M]
*
*****
*
317 cntrlvar 240 * dp0200 : CORE HEAT. LENGTH DIFF.
PRESS. [Kpa]
318 cntrlvar 241 * dpup1 : UPPER PLENUM DIFF.
PRESS. [Kpa]
319 cntrlvar 242 * dp034 : GUIDE TUBE DIF. PRESS.
[Kpa]
320 cntrlvar 243 * dpuhead : UPPER HEAD DIF. PRESS.
[Kpa]
321 cntrlvar 244 * dp050 : DOWNCOMER TO UPP. HEAD
DIF. P. [Kpa]
322 cntrlvar 245 * dp0r1 : PRESSURE VESSEL F.
PRESS. [Kpa]
*
323 cntrlvar 246 * dp1 : c11 TO h11 DIF. PRESS.
[Kpa]
324 cntrlvar 247 * dp12pg : pump 1 DIF. PRESS.
[Kpa]
325 cntrlvar 248 * dp12vg : LOOP SEAL 1 DOWNF. SIDE
DIF. P. [Kpa]
326 cntrlvar 249 * dp12vp : LOOP SEAL 1 UPFLOW. SIDE
DIF. P. [Kpa]
*
327 cntrlvar 250 * dp2 : c12 TO h12 DIF. PRESS.
[Kpa]
328 cntrlvar 251 * dp22pg : pump 2 DIF. PRESS.
[Kpa]
329 cntrlvar 252 * dp22vg : LOOP SEAL 2 DOWNF. SIDE
DIF. P. [Kpa]
330 cntrlvar 253 * dp22vp : LOOP SEAL 2 UPFLOW. SIDE
DIF. P. [Kpa]
*
331 cntrlvar 254 * dp3 : c13 TO h13 DIF. PRESS.
[Kpa]
332 cntrlvar 255 * dp32pg : pump 3 DIF. PRESS.
[Kpa]

```

```

333 cntrlvar 256 * dp32vg : LOOP SEAL 3 DOWNF. SIDE
DIF. P. [Kpa]
334 cntrlvar 257 * dp32vp : LOOP SEAL 3 UPFLOW. SIDE
DIF. P. [Kpa]
*
335 cntrlvar 258 * dp4 : sg1 u-TUBE IN. TO OUTLET
DIF. P. [Kpa]
336 cntrlvar 259 * dp41 : sg1 INLET PLENUM DIF.
PRESS. [Kpa]
337 cntrlvar 260 * dp426 : sg1 u-TUBE UPFLOW SIDE
DIF. P. [Kpa]
338 cntrlvar 261 * dp4r2 : sg1 BOILER SECTION DIF.
PRESS. [Kpa]
*
339 cntrlvar 262 * dp5 : sg2 u-TUBE IN. TO OUTLET
DIF. P. [Kpa]
340 cntrlvar 263 * dp51 : sg2 INLET PLENUM DIF.
PRESS. [Kpa]
341 cntrlvar 264 * dp526 : sg2 u-TUBE UPFLOW SIDE
DIF. P. [Kpa]
342 cntrlvar 265 * dp5r2 : sg2 BOILER SECTION DIF.
PRESS. [Kpa]
*
343 cntrlvar 266 * dp6 : sg3 u-TUBE IN. TO OUTLET
DIF. P. [Kpa]
344 cntrlvar 267 * dp61 : sg3 INLET PLENUM DIF.
PRESS. [Kpa]
345 cntrlvar 268 * dp626 : sg3 u-TUBE UPFLOW SIDE
DIF. P. [Kpa]
346 cntrlvar 269 * dp6r2 : sg3 BOILER SECTION DIF.
PRESS. [Kpa]
*
347 cntrlvar 270 * dpp1 : PRESSURIZER DIF. PRESS
[Kpa] ***
*
348 cntrlvar 271 * intqmb : TIME INTEGRATED BREAK
MASS FLOW [KG]
349 cntrlvar 274 * intqms1 : TIME INTEGRATED lpsi
MASS FLOW [KG]
350 cntrlvar 305 * mgv1 : sg1 SECONDARY SIDE MASS
INVT. [KG]
351 cntrlvar 405 * mgv2 : sg2 SECONDARY SIDE MASS
INVT. [KG]
352 cntrlvar 505 * mgv3 : sg3 SECONDARY SIDE MASS
INVT. [KG]
353 cntrlvar 275 * mam2 : ACCUMULATOR 2 MASS
INVENTORY [KG]
354 cntrlvar 276 * mam3 : ACCUMULATOR 3 MASS
INVENTORY [KG]
*
355 cntrlvar 277 * p+47 : sg1 STEAM DOME PRESSURE
[mpa]
356 cntrlvar 278 * p+57 : sg2 STEAM DOME PRESSURE
[mpa]
357 cntrlvar 279 * p+67 : sg3 STEAM DOME PRESSURE
[mpa]
358 cntrlvar 280 * p+p : PRESSURIZER TOP PRESSURE
[mpa]
359 cntrlvar 281 * p+am2 : ACCUMULATOR 2 GAS PHASE
PRESSURE [mpa]
360 cntrlvar 282 * p+am3 : ACCUMULATOR 3 GAS PHASE
PRESSURE [mpa]
*
361 mflowj 123010000 * qm05 : DOWNCOMER MASS FLOW RATE
[KG/S]

```

```

362 mflow] 332010000 * qman11 : sg1 FEEDWATER MASS FLOW
RATE [KG/S]
363 mflow] 432010000 * qman12 : sg2 FEEDWATER MASS FLOW
RATE [KG/S]
364 mflow] 532010000 * qman13 : sg3 FEEDWATER MASS FLOW
RATE [KG/S]
365 mflow] 180000000 * qmb : BREAK MASS FLOW RATE
[KG/S]
366 mflow] 311000000 * qmgv11 : sg1 STREAM LINE MASS FLOW
RATE [KG/S]
367 mflow] 411000000 * qmgv12 : sg2 STREAM LINE MASS FLOW
RATE [KG/S]
368 mflow] 511000000 * qmgv13 : sg3 STREAM LINE MASS FLOW
RATE [KG/S]
369 mflow] 807000000 * qmb12 : lpsi IN c12 MASS FLOW
RATE [KG/S]
370 mflow] 907000000 * qmb13 : lpsi IN c13 MASS FLOW
RATE [KG/S]
*
371 cntrlvar 283 * sebreak : BREAK SPECIFIC ENTHALPY
[KJ/KG]
*
372 tempf 123010000 * tf012a : CORE INLET TEMPERATURE
[k]
373 tempf 141010000 * tf0304 : CORE OUTLET TEMPERATURE
[k]
374 tempf 151010000 * tf041 : UPPER HEAD (BOTTOM)
TEMPERATURE [k]
375 tempf 153010000 * tf042 : UPPER HEAD (TOP)
TEMPERATURE [k]
376 tempf 602010000 * tf112 : HOT LRG 1 TEMPERATURE
[k]
377 tempf 655010000 * tf133 : COLD LRG 1 TEMPERATURE
[k]
378 tempf 802010000 * tf212 : HOT LRG 2 TEMPERATURE
[k]
379 tempf 855010000 * tf233 : COLD LRG 2 TEMPERATURE
[k]
380 tempf 902010000 * tf312 : HOT LRG 3 TEMPERATURE
[k]
381 tempf 955010000 * tf333 : COLD LRG 3 TEMPERATURE
[k]
382 tempf 309050000 * tf454c : BOTTOM OF sg1 DOWNCOMER
TEMPERATURE [k]
383 tempf 409050000 * tf554c : BOTTOM OF sg2 DOWNCOMER
TEMPERATURE [k]
384 tempf 509050000 * tf654c : BOTTOM OF sg3 DOWNCOMER
TEMPERATURE [k]
*
385 httemp 131000701 * ts02091 :
386 httemp 131000801 * ts02151 :
387 httemp 131000901 * ts02191 : ROD TEMPERATURE FROM
MIDDLE TO
388 httemp 131001001 * ts02201 : TOP CORE ELEVATION [k]
389 httemp 131001101 * ts02241 : *** ts = ? (LE OMEMBA V
TAB.1 STR 28/87)
390 httemp 131001201 * ts02281 :
391 cntrlvar 146 * tmax : MAX. CLAD TEMPERATURE
[k]
*
392 cntrlvar 286 * vp1 : PUMP 1 ROTATION SPEED
[RPM]
393 cntrlvar 287 * vp2 : PUMP 2 ROTATION SPEED
[RPM]
394 cntrlvar 288 * vp3 : PUMP 3 ROTATION SPEED
[RPM]

```

```

*
395 cntrlvar 285 * w+02 : CORE (ELECTRICAL) POWER
[Kw]
396 cntrlvar 290 * w+trac : TRACE HEATING [Kw]
*
397 cntrlvar 291 * wscore : SWOLLEN LEVEL [M]
***
*
398 dt 0 * dtcalc : TIME STRP ALONG
TRANSIENT [S]
399 emass 0 * mer : MASS ERROR [KG]
*
*
*****
* ttrr tripi
*
*****
501 time 0 gt null 0 300.0 n * break
*
604 -526 or -526 n * sg pressure control on - before
u. p.
*
*
*****
* ffii fiksiranje zacetnega stanja
*
*****
20512600 noname constant 0.648349 * rx flows
20515200 noname constant 0.295703
*
20532400 noname constant 2.8779e-02 * sg recirculation
20542400 noname constant 2.9092e-02
20552400 noname constant 2.9088e-02
*
20521800 noname constant 0.0 * prz. heater
*
3290000 noname delete * art. feedwate
3300000 noname delete
4290000 noname delete
4300000 noname delete
5290000 noname delete
5300000 noname delete
*
7110000 noname delete * art. pressurizer
7120000 noname delete
2310000 noname delete
2320000 noname delete
*
*****
* lppp l.p.s.i. in akumulatorji
*
*****
* trip 659 : trip ventil odpre akumulatorja 2 in 3
*
*

```

```

* accumulator vessel2
8330000 accumu2 accum
8330101 0.0 8.358 0.423 0.0 90.0 8.358 3.96-5 0.0 00
8330200 41.8+5 290. 0.0
* zeta iztoka je 0.335, zeta kolena je 0.2, upostevamo 5 kolen
8331101 805000000 0.00114 1.335 1.335 000000
8332200 0.286 0.0 0.119 0.119 0.00927 0 0 0
*
* accumulator no 2 pipe
8050000 acc12 englvol
8050101 0.0 21. 0.0239 0.0 20.0 10.005 1.0-4 0.0 00
8050200 3 41.8+5 290.
*
* accumulator no 2 valve
8060000 accv12 valve
* zeta kolena je 0.2, upostevamo 5 kolen od 10
8060101 805010000 856000000 0.00114 1.0 1.0 100000
8060201 0 0.00000e+00 0.00000e+00 0.00000e+00
8060300 trpv1v
8060301 659
*8060300 mtrvlv
*8060301 659 658 5.0 0.0
*
*
* accumulator vessel3
9330000 accum3 accum
9330101 0.0 8.358 0.423 0.0 90.0 8.358 3.96-5 0.0 00
9330200 41.8+5 290. 0.0
* zeta iztoka je 0.335, zeta kolena je 0.2, upostevamo 4
kolena
* kot accum. 833
9331101 905000000 0.00114 1.335 1.335 000000
9332200 0.286 0.0 0.119 0.119 0.00927 0 0 0
*
* accumulator no 3 pipe
9050000 acc13 englvol
9050101 0.0 21. 0.0239 0.0 20.0 10.005 1.0-4 0.0 00
9050200 3 41.8+5 290.
*
* accumulator no 2 valve
9060000 accv12 valve
* zeta kolena je 0.2 upostevamo 4 kolena od 8
9060101 905010000 956000000 0.00114 0.80 0.80 100000
9060201 0 0.00000e+00 0.00000e+00 0.00000e+00
9060300 trpv1v
9060301 659
*9060300 mtrvlv
*9060301 659 658 5.0 0.0
*
*
*****
*
* lpsi pump no 2
8070000 lpsi2 tmdpjun
8070101 804000000 855010000 0.00599 *** presek
8070200 1 0 p 203080000
* ena qsb crpalka za obe cl veji (2+3)
8070201 0.0 0.0 0.0 0.0
8070202 0.6779+5 0.9447 0.0 0.0
8070203 1.5411+5 0.8950 0.0 0.0
8070204 3.8507+5 0.7458 0.0 0.0
8070205 6.767+5 0.4972 0.0 0.0
8070206 8.517+5 0.2486 0.0 0.0
8070207 9.077+5 0.0497 0.0 0.0
8070208 9.100+5 0.0 0.0 0.0

```



\* cv 321 : narrow range sg1 level [m]  
20532100 atlr -lv 1.0 0.0 1  
20532101 rho 3.0e+10000 cnlrivar 320  
\* cv 322 : wide range sg1 level [m]  
20532200 stsg1 sum 1.0 0.0 1  
20532201 11.255 1.0 cnlrivar 321

\* afw pump no. 1 - before ultimate procedure  
3700000 afw111 tmdpjun  
3700101 36800000 33200000 0.0006786  
3700200 1 626 cnlrivar 322  
3700201 -1.0 0.0 0.0 0.0  
3700202 0.0 0.30329 0.0 0.0  
3700203 13.32 0.30329 0.0 0.0  
3700204 13.4 0.24263 0.0 0.0  
3700205 13.5 0.16726 0.0 0.0  
3700206 13.6 0.09169 0.0 0.0  
3700207 13.7 0.01611 0.0 0.0  
3700208 13.71 0.00855 0.0 0.0  
3700209 13.715 0.00477 0.0 0.0  
3700210 13.72 0.0 0.0 0.0

\* afw pump no. 2 - after ultimate procedure  
3710000 afw211 tmdpjun  
3710101 36900000 33200000 0.0006786  
3710200 1 526 cnlrivar 322  
3710201 -1.0 0.0 0.0 0.0  
3710202 0.0 0.30329 0.0 0.0  
3710203 13.14 0.30329 0.0 0.0  
3710204 13.20 0.24263 0.0 0.0  
3710205 13.25 0.16726 0.0 0.0  
3710206 13.30 0.09169 0.0 0.0  
3710207 13.325 0.01611 0.0 0.0  
3710208 13.34 0.00855 0.0 0.0  
3710209 13.35 0.00477 0.0 0.0

\* afw tank-i no. 1 - after ultimate procedure  
3710300 afw311 tmdpjun  
3710401 36900000 33200000 0.0006786  
3710500 1 526 cnlrivar 322  
3710501 -1.0 0.0 0.0 0.0  
3710502 0.0 0.30329 0.0 0.0  
3710503 13.14 0.30329 0.0 0.0  
3710504 13.20 0.24263 0.0 0.0  
3710505 13.25 0.16726 0.0 0.0  
3710506 13.30 0.09169 0.0 0.0  
3710507 13.325 0.01611 0.0 0.0  
3710508 13.34 0.00855 0.0 0.0  
3710509 13.35 0.00477 0.0 0.0

\* afw tank-ii no. 1  
3690000 afw211 tmdpvol  
3690101 0.0 6.1 28.32 0.0 90.0 6.1 1.0-4 0.0 0  
3690200 003  
3690201 0.0 1.02+5 307.0  
\* cv 420 : dp sg2 nr level [pa/g]  
0.0197 = 1/9 8067  
20542000 dp2r2 sum 1.0 0.0 1  
20542001 0.0 0.10197 p 408010000 -0.10197 p 410010000  
20542002 0.121 rho 408010000 0.440 rho 410010000

\* cv 421 : narrow range sg2 level [m]  
20542100 st2r2 div 1.0 0.0 1  
20542101 rho 408010000 cnlrivar 420  
\* cv 422 : wide range sg2 level [m]  
20542200 stsg2 sum 1.0 0.0 1  
20542201 11.255 1.0 cnlrivar 421

\* afw pump no. 2 - before ultimate procedure  
4700000 afw21 tmdpjun  
4700101 46800000 43200000 0.0006786  
4700200 1 626 cnlrivar 422  
4700201 -1.0 0.0 0.0 0.0  
4700202 0.0 0.30329 0.0 0.0  
4700203 13.32 0.30329 0.0 0.0  
4700204 13.4 0.24263 0.0 0.0  
4700205 13.5 0.16726 0.0 0.0  
4700206 13.6 0.09169 0.0 0.0  
4700207 13.7 0.01611 0.0 0.0  
4700208 13.71 0.00855 0.0 0.0  
4700209 13.715 0.00477 0.0 0.0  
4700210 13.72 0.0 0.0 0.0

\* afw pump no. 2 - after ultimate procedure  
4710000 afw211 tmdpjun  
4710101 46900000 43200000 0.0006786  
4710200 1 526 cnlrivar 422  
4710201 -1.0 0.0 0.0 0.0  
4710202 0.0 0.30329 0.0 0.0  
4710203 13.14 0.30329 0.0 0.0  
4710204 13.20 0.24263 0.0 0.0  
4710205 13.25 0.16726 0.0 0.0  
4710206 13.30 0.09169 0.0 0.0  
4710207 13.325 0.01611 0.0 0.0  
4710208 13.34 0.00855 0.0 0.0  
4710209 13.35 0.00477 0.0 0.0

\* afw tank-i no. 2  
4680000 afw211 tmdpvol  
4680101 0.0 6.1 28.32 0.0 90.0 6.1 1.0-4 0.0 0  
4680200 003  
4680201 0.0 1.02+5 307.0  
\* cv 520 : dp sg3 nr level [pa/g]  
0.0197 = 1/9 8067  
20552000 dp3r2 sum 1.0 0.0 1  
20552001 0.0 0.10197 p 508010000 -0.10197 p 510010000  
20552002 0.121 rho 508010000 0.440 rho 510010000

\* cv 521 : narrow range sg3 level [m]  
20552100 st3r2 div 1.0 0.0 1  
20552101 rho 508010000 cnlrivar 520  
\* cv 522 : wide range sg3 level [m]  
20552200 stsg3 sum 1.0 0.0 1  
20552201 11.255 1.0 cnlrivar 521  
\* afw pump no. 3 - before ultimate procedure  
5700000 afw31 tmdpjun  
5700101 56800000 53200000 0.0006786  
5700200 1 626 cnlrivar 522  
5700201 -1.0 0.0 0.0 0.0

\* afw tank-ii no. 2  
5680000 afw311 tmdpvol  
5680101 0.0 6.1 28.32 0.0 90.0 6.1 1.0-4 0.0 0  
5680200 003  
5680201 0.0 1.02+5 307.0  
\* cv 520 : dp sg3 nr level [pa/g]  
0.0197 = 1/9 8067  
20552000 dp3r2 sum 1.0 0.0 1  
20552001 0.0 0.10197 p 508010000 -0.10197 p 510010000  
20552002 0.121 rho 508010000 0.440 rho 510010000

\* cv 521 : narrow range sg3 level [m]  
20552100 st3r2 div 1.0 0.0 1  
20552101 rho 508010000 cnlrivar 520  
\* cv 522 : wide range sg3 level [m]  
20552200 stsg3 sum 1.0 0.0 1  
20552201 11.255 1.0 cnlrivar 521  
\* afw pump no. 3 - before ultimate procedure  
5700000 afw31 tmdpjun  
5700101 56800000 53200000 0.0006786  
5700200 1 626 cnlrivar 522  
5700201 -1.0 0.0 0.0 0.0

5700202 0.0 0.30329 0.0 0.0  
5700203 13.32 0.30329 0.0 0.0  
5700204 13.4 0.24263 0.0 0.0  
5700205 13.5 0.16726 0.0 0.0  
5700206 13.6 0.09169 0.0 0.0  
5700207 13.7 0.01611 0.0 0.0  
5700208 13.71 0.00855 0.0 0.0  
5700209 13.715 0.00477 0.0 0.0  
5700210 13.72 0.0 0.0 0.0

\* afw pump no. 3 - after ultimate procedure  
5710000 afw311 tmdpjun  
5710101 56900000 53200000 0.0006786  
5710200 1 526 cnlrivar 522  
5710201 -1.0 0.0 0.0 0.0  
5710202 0.0 0.30329 0.0 0.0  
5710203 13.14 0.30329 0.0 0.0  
5710204 13.20 0.24263 0.0 0.0  
5710205 13.25 0.16726 0.0 0.0  
5710206 13.30 0.09169 0.0 0.0  
5710207 13.325 0.01611 0.0 0.0  
5710208 13.34 0.00855 0.0 0.0  
5710209 13.35 0.00477 0.0 0.0

\* afw tank-i no. 3  
5680000 afw311 tmdpvol  
5680101 0.0 6.1 28.32 0.0 90.0 6.1 1.0-4 0.0 0  
5680200 003  
5680201 0.0 1.02+5 307.0  
\* afw tank-ii no. 3  
5690000 afw311 tmdpvol  
5690101 0.0 6.1 28.32 0.0 90.0 6.1 1.0-4 0.0 0  
5690200 003  
5690201 0.0 1.02+5 307.0

\* cv 520 : dp sg3 nr level [pa/g]  
0.0197 = 1/9 8067  
20552000 dp3r2 sum 1.0 0.0 1  
20552001 0.0 0.10197 p 508010000 -0.10197 p 510010000  
20552002 0.121 rho 508010000 0.440 rho 510010000  
\* cv 521 : narrow range sg3 level [m]  
20552100 st3r2 div 1.0 0.0 1  
20552101 rho 508010000 cnlrivar 520  
\* cv 522 : wide range sg3 level [m]  
20552200 stsg3 sum 1.0 0.0 1  
20552201 11.255 1.0 cnlrivar 521  
\* afw pump no. 3 - before ultimate procedure  
5700000 afw31 tmdpjun  
5700101 56800000 53200000 0.0006786  
5700200 1 626 cnlrivar 522  
5700201 -1.0 0.0 0.0 0.0

\* afw tank-ii no. 3  
5690000 afw311 tmdpvol  
5690101 0.0 6.1 28.32 0.0 90.0 6.1 1.0-4 0.0 0  
5690200 003  
5690201 0.0 1.02+5 307.0  
\* cv 520 : dp sg3 nr level [pa/g]  
0.0197 = 1/9 8067  
20552000 dp3r2 sum 1.0 0.0 1  
20552001 0.0 0.10197 p 508010000 -0.10197 p 510010000  
20552002 0.121 rho 508010000 0.440 rho 510010000  
\* cv 521 : narrow range sg3 level [m]  
20552100 st3r2 div 1.0 0.0 1  
20552101 rho 508010000 cnlrivar 520  
\* cv 522 : wide range sg3 level [m]  
20552200 stsg3 sum 1.0 0.0 1  
20552201 11.255 1.0 cnlrivar 521  
\* afw pump no. 3 - before ultimate procedure  
5700000 afw31 tmdpjun  
5700101 56800000 53200000 0.0006786  
5700200 1 626 cnlrivar 522  
5700201 -1.0 0.0 0.0 0.0

\* cv 520 : dp sg3 nr level [pa/g]  
0.0197 = 1/9 8067  
20552000 dp3r2 sum 1.0 0.0 1  
20552001 0.0 0.10197 p 508010000 -0.10197 p 510010000  
20552002 0.121 rho 508010000 0.440 rho 510010000  
\* cv 521 : narrow range sg3 level [m]  
20552100 st3r2 div 1.0 0.0 1  
20552101 rho 508010000 cnlrivar 520  
\* cv 522 : wide range sg3 level [m]  
20552200 stsg3 sum 1.0 0.0 1  
20552201 11.255 1.0 cnlrivar 521  
\* afw pump no. 3 - before ultimate procedure  
5700000 afw31 tmdpjun  
5700101 56800000 53200000 0.0006786  
5700200 1 626 cnlrivar 522  
5700201 -1.0 0.0 0.0 0.0

1830000 bvent valve

```

1830101 182010000 186000000 1.6600e-03 0.0 0.0 100100
1830201 0 0.0 0.0 0.0
1830300 mrvlv
1830301 501 603 20. 0.0
*
1860000 tank tmdpvol
1860101 1.0 0.0 5.02 0.0 0.0 0.0 1.0e-04 0.0 00
1860200 2
1860201 0.0 1.0e+05 1.0
*
slowdown tanks keep the pressure at a level which is
not likely
*
to influence the break flow rate (str.25/50)
*
*
*****
separator pare ---> branch
*
*****
* sek. sistem: separator pare
3070000 separ branch
3070001 3 0
3070101 0.0 1.9430 0.09467 P 90.0 1.9430 0.1e-04 0.249
00
3070200 100 6.84720e+06 1.24232e+06 2.58325e+06 1.51410e-
01
3071101 307010000 310000000 4.8695e-02 0.82 0.14 00000
3072101 307000000 308000000 44.9150e-02 0.26 0.23 00000
3073101 303010000 307000000 4.8695e-02 0.0 0.0 00000
3071201 3.70160e-01 3.98960e-01 0.00000e+00
3072201 -3.15359e-03 -4.57842e-03 0.00000e+00
3073201 3.41760e-01 3.73780e-01 0.00000e+00
*
* sek. sistem: separator pare
4070000 separ branch
4070001 3 0
4070101 0.0 1.9430 0.09467 0 90.0 1.9430 0.1e-04 0.249
00
4070200 100 6.84752e+06 1.24169e+06 2.58326e+06 1.34150e-
01
4071101 407010000 410000000 4.8695e-02 0.82 0.14 00000
4072101 407000000 408000000 44.9150e-02 0.26 0.23 00000
4073101 403010000 407000000 4.8695e-02 0.0 0.0 00000
4071201 2.81190e-01 3.10730e-01 0.00000e+00
4072201 6.34319e-03 4.91488e-03 0.00000e+00
4073201 3.39400e-01 3.73280e-01 0.00000e+00
*
* sek. sistem: separator pare
5070000 separ branch
5070001 3 0
5070101 0.0 1.9430 0.09467 0 90.0 1.9430 0.1e-04 0.249
00
5070200 100 6.84752e+06 1.24169e+06 2.58326e+06 1.34150e-
01
5071101 507010000 510000000 4.8695e-02 0.82 0.14 00000
5072101 507000000 508000000 44.9150e-02 0.26 0.23 00000
5073101 503010000 507000000 4.8695e-02 0.0 0.0 00000
5071201 2.81210e-01 3.10750e-01 0.00000e+00
5072201 6.34086e-03 4.91256e-03 0.00000e+00
5073201 3.39400e-01 3.73280e-01 0.00000e+00
*
*

```

```

*****
*
* hhs heat structure thermal property data
*
*
*****
* composition type and data format
*
20100100 tbl/fctn 1 -1 * stainless steel
20100200 tbl/fctn 2 2 * boron nitride (heater rods)
20100300 tbl/fctn 1 -1 * inconel 600
*
* thermal conductivity data
*
* stainless steel
20100101 293. 13.9, 373. 15.1, 473. 16.7, 573. 18.3, 673.
19.8, 873. 23.0.
*! 20100102 1073. 26.1
20100102 1073. 26.1 1473. 26.1
* boron nitride
*! 20100201 473. 1073. 2. 0. 0. 0. 0. 0. 0.
20100201 293. 1473. 2. 0. 0. 0. 0. 0. 0.
* inconel 600
20100301 293. 14.9, 373. 15.6, 473. 17.2, 673. 20.4, 873.
23.7, 1073. 27.4
*
* volumetric heat capacity data
*
* stainless steel
20100151 3.57870+6, 3.88778+6, 4.09768+6, 4.20898+6,
4.26474+6, 4.41405+6,
*! 20100152 4.65555+6
20100152 4.65555+6 4.65555+6
* boron nitride
*! 20100251 473. 1073. 1.46+6 1.62+3 0. 0. 0. 0. 0.
20100251 293. 1473. 1.46+6 1.62+3 0. 0. 0. 0. 0.
* inconel 600
20100351 3.76320+6, 3.85526+6, 4.02919+6, 4.26422+6,
4.68003+6, 4.98467+6
*
*
*****
* comparison report dodatki
*
20516000 avgrhof sum 0.0833 0.0 1
20516001 0.0 1.0 rhof 131010000 1.0 rhof 131020000 1.0
rhof 131030000
20516002 1.0 rhof 131040000 1.0 rhof 131050000 1.0
rhof 131060000
20516003 1.0 rhof 131070000 1.0 rhof 131080000 1.0
rhof 131090000
20516004 1.0 rhof 131100000 1.0 rhof 131110000 1.0
rhof 131120000
*
20516100 clev1 sum 1.0 0.0 1 * 101.94 = 1000*1/9.81
[KPa-->Pa]
20516101 0.0 101.94 cntrlvar 240 -5.61 rhog 131060000
*
20516200 clev2 sum 1.0 0.01 1

```

```

20516201 0.0 1.0 cntrlvar 160 -1.0 rhog 131060000
*
* ctv 163: collapsed liquid core level (m)
20516300 corelev1 div 1.0 0.1 3 0.0 9.5
20516301 cntrlvar 162 cntrlvar 161
*
*****
*
* ctv 146: maximum htemp rx core, right-wall surface
20514600 maxrxt stdfctn 1.0 600. 1
20514601 max htemp 131000106 htemp 131000206
20514602 htemp 131000306 htemp 131000406
20514603 htemp 131000506 htemp 131000606
20514604 htemp 131000706 htemp 131000806
20514605 htemp 131000806 htemp 131001006
20514606 htemp 131000906 htemp 131001206
*
* zacetno stanje: mcp(0) + mm2(0) + mm3(0)
* 1949 KG + 286 KG + 286 KG = 2521 KG
20517000 mcp sum 1.0 1949.0 0
20517001 -1.0 cntrlvar 271 -1.0 cntrlvar 275
20517002 -1.0 cntrlvar 276 +1.0 cntrlvar 274
*
*****
*
* ***** end *****

```

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(See instructions on the reverse)

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10. SUPPLEMENTARY NOTES

S. Smith, NRC Project Manager

11. ABSTRACT (200 words or less)

RELAP5 computer code was used to simulate an experiment designated 9.1.b, (2" Cold Leg Break without HPSI and with Delayed Ultimate Procedure) performed on BETHSY integral test facility. This test is characterized as beyond design transients scenarios with unavailability of some safety and protection systems. The calculations which have been completed using the computer Sun Sparcstation 20 aim to evidence the difference between experimental and computed data. Generally, an agreement of major transient trends is shown to be obtained in the simulation.

12. KEY WORDS/DESCRIPTORS (List words or phrases that will assist researchers in locating the report.)

RELAP5, BETHSY, Beyond Design Basis Accidents (BDBA)

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