



International Agreement Report

Assessment of RELAP5/MOD3.2 Using LOFT Large Break LOCA Test, LP-02-6

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Abstract

The LOFT experiment LP-02-6 was simulated using the RELAP5/MOD3.2 code to assess its capability to predict the thermal-hydraulic phenomena in LBLOCA of the PWR. The reactor vessel was modeled with two core channels and split downcomer for a base calculation. The results of the base calculation show that the code can not predict the early bottom-up quenching which is a distinguished phenomenon of the experiment LP-02-6, mainly due to the deficiency of break flow model.

The discharge coefficient sensitivity study was performed to show that the calculated subcooled break flow which might significantly affect the early bottom-up quenching is dependent on the coefficient. More detailed modeling of the cross flow in the split downcomer was performed, but, resulted in little improvement on the predictability of bottom-up quenching. Additional calculation using the RELAP5/MOD3 1 instead of RELAP5/MOD3.2 showed that there is no large difference between the versions in the simulation of LBLOCA.

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Executive Summary

This report presents the results of RELAP5/MOD3.2 assessment in the prediction of the thermal-hydraulic behavior under the conditions of Loss of Fluid Test(LOFT) LBLOCA Experiment LP-02-6. The assessment was purposed to determine whether the code can predict the major phenomena of LOFT LP-02-6 and to provide some useful information to code developers and users.

Experiment LP-02-6 was conducted on October 3, 1983. It was the forth experiment conducted in the LOFT facility at the Idaho National Engineering Laboratory(INEL) under the auspices of the OECD. This experiment, which was designed to meet requirements outlined by the USNRC as specified in the OECD LOFT Project Agreement, simulated a double-ended off-set shear of a commercial PWR main coolant inlet pipe coincident with the loss of offsite power. Experiment LP-02-6 addressed the response of a PWR to conditions closely resembling a USNRC "Design Basis Accident" in that prepressurized fuel rods were installed and minimum US emergency coolant injections were used.

A base case calculation using RELAP5/MOD3.2 with the typical LOFT nodalization and default break flow model was conducted. The results of the calculation were compared with the experiment data in terms of loop behavior, ECCS performance, vessel phenomena, and fuel thermal response. It was disclosed from the comparison that the code has poor predictability of the important thermal-hydraulic phenomena such as the early bottom up quenching during the blowdown. A primary cause of this poor prediction was inferred as the overprediction of subcooled break flow. The overprediction of subcooled break flow bring about the early end of subcooled break flow, early core heat up during the blowdown, the early initiation of bottom-up quenching and little amount of bottom-up flow.

To identify the effect of break flow model in the base case calculation, several calculations were performed with changing discharge coefficient. It was concluded that de-

creased discharge coefficient reduces the peak subcooled break flow and it helps the code better predict the early bottom up quenching.

Another sensitivity study was performed to identify the effects of the modeling of cross flow in the split downcomer annulus. All the downcomer volumes of each side were connected by cross flow junctions while only the top volume of downcomer annulus was connected by a cross flow junction in the base case calculation. This change of alization resulted in little improvement on the prediction of bottom up quenching, which means that the core thermal-hydraulic behavior is not dependent on the number of cross flow junctions.

Additional calculation using the RELAP5/MOD3.1 was performed to catch the improved features of RELAP5/MOD3.2 compared with RELAP5/MOD3.1. The versions showed nearly identical results, but, RELAP5/MOD3.2 predicted better the thermal behavior in the both end parts of the core than RELAP5/MOD3.1.

1. INTRODUCTION

This report presents the results of code assessment of RELAP5/MOD3.2 using the LOFT experiment LP-02-6. The assessment was performed within the Code Applications and Maintenance Program(CAMP) organized by the U. S. Nuclear Regulatory Commission(NRC).

The experiment LP-02-6 was the first large break LOCA simulation which was designed to represent the design basis accident conditions. The distinguished thermal-hydraulic phenomena of the experiment LP-02-6 is a positive bottom-up core flow, which resulted in bottom-up quench of central fuel assembly during the blowdown period, due to the long-term pump coast down.

The objective of this study is to identify effectiveness and deficiencies of RELAP5/MOD3.2 in predicting thermal-hydraulic phenomenon specific to LBLOCA such as bottom-up quenching. RELAP5/MOD3.2 is a recently released version of RELAP5/MOD3 which was developed by improving the modeling base of RELAP5/MOD2. RELAP5/MOD2 was assessed using the LP-02-6 test data by Lübbesmeyer [2]. He concluded that it could not predict the early bottom-up rewetting which occurred between 4 and 8 seconds of the blowdown phase.

It is well known that RELAP code is very strongly dependent upon user specific input parameters. The discharge coefficient at the break valve affects significantly on the resultant thermal-hydraulic behavior in the analysis of LBLOCA. To find out the influence of discharge coefficient in the calculation of LP-02-6, sensitivity calculations on the discharge coefficient were carried out.

Transversal flow in the downcomer, which has been believed to have effects on the core flow behavior, has been modeled by cross flow junction between downcomer upper volumes of both loop sides. A more detailed modeling of the transversal flow by connecting all the volumes of both loop sides with six cross flow junctions was tried to get better

prediction of core flow behavior.

Finally, a calculation using RELAP5/MOD3.1 in place of RELAP5/MOD3.2 was conducted, though it is generally thought that there is no significant change between these versions in the analysis of LBLOCA, to get knowledge of the improved features of RELAP5/MOD3.2.

A brief description of the LOFT system and the LP-02-6 experiment are provided in Chapter 2. The code and modeling basis for the base case calculation is described in Chapter 3. The results of the base case calculation are discussed in Chapter 4. The scope and results of sensitivity studies are presented in Chapter 5. Chapter 6 describes the run statistics for the base case calculation and conclusions and recommendations from this assessment are presented in Chapter 7. The input list for steady-state run and transient run of the base case is attached in Appendix.

2. FACILITY AND TEST DESCRIPTIONS

2.1 LOFT facility

The LOFT(Loss of Fluid Test) facility at Idaho National Engineering Laboratory was designed to simulate the major component and system responses of commercial PWR during LOCA. It is a scaled representation of a commercial PWR of Westinghouse type having 4 loops with a volume ratio of 1/60. The experimental assembly includes five major subsystems which have been instrumented such that system variables can be measured and recorded during a LOCA simulation. The subsystems consist of a reactor vessel with a nuclear core, an intact loop, a broken loop, the blowdown suppression system, and the emergency core coolant system. The entire nuclear core consists of five square and four triangular fuel bundles with a total of 1300 fuel pins each of 1.67 m long and an outside diameter of 10.72 mm. The overall configuration is shown in Figure 2.1 and complete information on this system is provided in Reference 1.

2.2 Experiment LP-02-6

Experiment LP-02-6 was completed on October 3, 1983, in the LOFT facility located at the Idaho National Engineering Laboratory. It was the first large-break LOCA simulation and the fourth experiment conducted under the auspices of the Organization for Economic Cooperation and Development(OECD) LOFT Project. This experiment simulated a double-ended offset shear of a pressurized water reactor(PWR) main coolant inlet pipe, and was initiated from conditions similar to PWR operating conditions.

Prior to the experiment, LOFT facility was set to have a primary system pressure of 15.0 MPa, primary system cold leg and hot leg temperature of 560K, and 590K respectively, and a loop mass flow rate of 248.7 kg/sec. Initial reactor power level was 46

MW with a maximum linear heat generation rate (LHGR) of 48.8 kW/m. Table 2.1 presents a summary of initial conditions of the experiment.

The experiment was initiated by opening both the Quick Opening Blowdown Valves(QOBV) in hot and cold leg. Reactor was scrammed on low hot leg pressure at 0.1 secs and the pumps were tripped at 0.8 secs. The pumps coasted down until 16.5 secs when their rotational speed fell below the trip point and they were decoupled from their flywheels. Flow in the core reversed almost instantaneously with experiment initiation, and the fuel rod cladding temperatures started to increase due to stored thermal energy at 0.9 secs. The entire core heated up until 5.2 secs, when positive core flow was again established due to choking of the flow in the broken cold leg. This positive core flow quenched the lower $\sim 2/3$ of the core until ~ 10 secs when flow in the intact cold leg decreased to below that of the broken cold leg and the core again started to heat up. A partial top-down core quench initiated at 14.8 secs and lasted until 18.6 secs. The lower plenum was filled by 30.7 secs, the core quench was complete by 56 secs, and core re-flood was complete by 59 secs. Thermal-hydraulic sequence of main events observed in the experiment is summarized in Table 2.2.

3. CODE AND MODELING DESCRIPTION

RELAP5/MOD3.2 used in this assessment was **the very version(without any modification)** received at October 1995 from USNRC. Since any RELAP5 input specific to LP-02-6 experiment was not obtained from INEL, a reference input was developed by authors based on the input which was used in the previous LP-LB-1 assessment by Lübbesmeyer [3].

3.1 Input Modeling

The base nodalization used to simulate the LOFT experiment LP-02-6 in this study is shown in Figure 3.1. This nodalization and input deck are based on those used to calculate the LP-LB-1 experiment with RELAP5/MOD2 by Lübbesmeyer [3]. Modifications implemented into the original input are as follows : (1) General changes suitable to RELAP5/MOD3(e.g. heat structure), (2) Introduction of ECCMIX component, (3) Changes in the number of volumes of pressurizer (six to twelve), (4) Changes in the number of axial nodes of core channel, (5) LP-02-6 experiment specific modifications

The reactor vessel is modeled by three hydraulic channels representing reactor core(volume 230, 231, and 235), two downcomer channels(volume 200 to 210 and 270 to 280 respectively), lower plenum(volume 220 to 225) and upper plenum with the vessel dome(240-260). Top volumes of each downcomer channel(volume 200 and 270) are connected with single cross flow junction(junction 290) which has energy loss coefficient of 1.8341. Nozzle bypass from intact cold leg to upper plenum is also modeled. The core is modeled by 3 parallel channels; core bypass channel(volume 235) with 3 subvolumes, average and hot core channel(volume 230 and 231) subdivided into 12 equally spaced volumes respectively. It is assumed that the total mass flow rate through the core is shared approximately 79% by the average channel, 16% by the hot channel and 5% by

core bypass channel. The heat generated in the fuel pin is transferred to primary coolant by heat structures attached to the hot channel and the average channel. To include the effect of heat capacity of material, heat structures of the downcomer and lower plenum are modeled.

The intact loop consists of twenty volumes with several subvolumes. The pumping system is divided into two pump lines with two individual pumps numbered as 135 and 165 respectively.

The ECC injection system consists of five volumes and one valve. This system is connected to the intact loop cold leg volume modeled by the ECCMIX component(volume 185). The HPIS and LPIS are modeled by time dependent junctions numbered 635 and 625 respectively. Control valve(valve 610) in the accumulator line is to isolate the accumulator when the accumulator is emptied.

The steam generator consists of eight volumes on the primary system and fifteen volumes on the secondary system. Heat is exchanged between primary and secondary side of the steam generator via the u-tubes which is modeled by heat structures. Feed water system and steam condenser are modeled by time dependent volumes(volume 505 and 541, respectively). Feed water flow rate and steam flow rate are controlled by control logic to keep the required secondary pressure and level.

The pressurizer is modeled by surge line(volume 400 and 402), pressurizer vessel(volume 415) and pressurizer dome(volume 420). Pressurizer vessel was divided into twelve subvolumes.

The broken loop hot leg is modeled by four volumes(volume 300 to 315). Component 315 represents steam generator simulator. The broken loop cold leg is modeled by 4 volumes(volume 335 to 344). Reflood assist bypass line is modeled by 2 volumes(volume 370 and 380). The reflood assist bypass valve is modeled by a trip valve which is closed when the break valves are opened. At the end of each broken loop, two break valves which have to be opened by trip signal are placed and connected with the suppression

tank modeled by two time dependent volumes(700 and 705). The discharge coefficients of the break valves are 1.0 for the subcooled discharge and the saturated discharge.

In the input modeling delineated above, total number of hydrodynamic volumes, junctions and heat structures are 147, 152, and 47, respectively.

3.2 Initial and Boundary Conditions

To obtain the initial conditions proper to the test conditions over the whole system, a steady state calculation was performed with four steady state controllers and a time dependent volume : two primary coolant pump speed controllers, a charging and letdown controller, a feed water flow rate controller, and a time dependent volume to set pressurizer pressure to a designed value.

The results obtained from the steady state run were compared with the measured initial conditions [4] in Table 2.1. The calculated results generally agree with the experimental conditions except the broken loop hot leg temperature which was estimated lower than the measured data. The reason of such underprediction of the broken loop hot leg temperature was not clear, but, it was believed to have negligible effect on the overall system transient.

Based on the experiment data, the reactor power history, containment pressure and feedwater flow rate after scram were described as time dependent tables. Performance curves for HPSI and LPSI flow rate as function of cold leg pressure were provided in the input. The pump speed after trip was simulated by time dependent speed table. And the steam generator secondary side air-cooled condenser was modeled as a time dependent volume with a constant pressure of 2.069 MPa during the transient. All information of boundary conditions was provided in the steady and transient input deck.

4. RESULTS FROM BASE CASE CALCULATION

The LP-02-6 transient was calculated up to 80 secs from the initial conditions obtained from steady state run. Steady state controllers were deleted in the transient input deck to get proper initial conditions.

The sequence of hydraulic events during the transient calculation was summarized in Table 2.2 and compared with the experiment chronology. In general, the calculated sequence of events show good agreement with the experiment, but, the overall transient was calculated to progress more rapidly than the experiment because of rapid system depressurization.

In this chapter, the predicted important thermal-hydraulic parameters such as system pressure, loop mass flow rates and cladding temperatures are compared with the measured data. Table 4.1 summarizes the list of assessment parameters. It describes the identification of calculated parameters and corresponding instruments in addition to uncertainties of measurements. The corresponding figure numbers are also listed in the table.

4.1 Loop Behavior

The behavior of calculated system pressure in the intact loop hot leg is plotted with corresponding experimental data in Figure 4.1. It is easily found that the system pressure was calculated to be lower than the measured data during overall transient. This underestimation of system pressure might be a result of overprediction of break flow during the blowdown, which will be discussed later.

The calculated mass flow rate in the broken loop cold leg and hot leg are shown in Figure 4.2 and 4.3, respectively. As shown in the figures, the overall trends of mass flow in the broken leg were predicted well. However, the peak values of the mass flow were

highly overestimated to be about 741 kg/sec (the measured value is ~550 kg/sec) in the cold leg and 241 kg/sec (the measured value is ~193 kg/sec) in the hot leg. Such an overprediction of mass flow rate in the broken loop in the early period of transient is considered as a deficiency of RELAP5/MOD3.2 critical flow model. This might lead the intact loop to contain less inventory than the experiment.

The calculated mass flow rates in the intact loop cold leg and the intact loop hot leg were compared with the experimental data in Figure 4.4 and 4.5, respectively. It can be found that the calculated mass flow rates followed the trend of the measured data very well with slight underestimation of mass flow rate in the cold leg during the blowdown phase.

The mass flow rate in the broken loop cold leg was predicted to fall below the mass flow rate in the intact loop cold leg at ~3.3 secs as shown in Figure 4.6. The fact that the mass flow rate in the broken loop cold leg is lower than the mass flow rate in the intact loop cold leg means that the flow in the broken loop cold leg is saturated and the core is being filled with fluid from the intact loop cold leg. The phase transition of flow in the broken loop cold leg was observed at ~4 secs after transient initiation in the experiment.

4.2 ECCS Performance

Figure 4.7 shows the calculated accumulator pressure and Figure 4.8 shows the predicted liquid level in the accumulator with corresponding measured data. As shown in these figures, the accumulator injection was initiated at ~14.5 secs while it was started at 17.5 secs in the experiment. This earlier accumulator injection was resulted from rapid system depressurization.

Figure 4.9 shows the calculated LPSI mass flow rate with the measured data. The injection was predicted to be earlier and higher than the measured data. This earlier and

higher injection was also due to the underestimation of the primary system pressure during the injection period.

4.3 Vessel Phenomena

Figure 4.10 shows the calculated liquid temperature in the lower plenum. The liquid temperature was underpredicted after ~14 secs when the accumulator injection was initiated ~3 secs earlier than the experiment as stated in the previous section.

Figure 4.11 presents the collapsed liquid level in the two downcomer channels and the two core channels of reactor vessel. Since no experiment data for these collapsed liquid levels were available, the predicted levels are plotted only.

The liquid level in the core decreased rapidly after initiation of break and the core was completely emptied at ~3 secs until bottom up flow was initiated. The filling of the core with the bottom up flow was predicted to make the lower part of the core rewet. And then, the liquid level fell again below the bottom of core and was maintained low level until the ECC injection water reached the bottom of core at ~38 secs. The hot core reflood was completed at 64 secs, ~5 secs latter than the experiment.

In the early blowdown period up to ~3 secs, the liquid level in the broken side downcomer dropped more rapidly than that in the intact side one due to less flow resistance. The liquid level in the broken side downcomer increased for a short time from the end of subcooled blowdown because the break flow was reduced significantly due to saturation while the incoming flow from the intact loop cold leg was still maintained. During the core rewetting period, the liquid levels in the both sides decreased again. The decreasing rate of the broken side liquid level was smaller than that in intact side. This was due to upward water flow from the lower plenum to the broken side downcomer. The level in the intact side downcomer started to increase at ~22 secs mainly due to accumulator injection flow initiated at 14.5 secs. The level in the broken side downcomer

also started to increase at ~26 secs.

4.4 Fuel Thermal Response

Calculated cladding temperatures of hot rod at 12 axial hot core nodes are compared with the measured data of corresponding elevation in Figure 4.12 to Figure 4.23. From the comparison of the cladding temperature behavior, following features are observed.

- 1) The blowdown heat up was relatively well predicted over the core except at the highest node, but, it was calculated to occur little earlier than the measured data.
- 2) The blowdown heat up was underpredicted at the low heat flux region, and overpredicted at the high heat flux region. In the middle part of the core, the degree of overestimation is ~60K at the hottest elevation.
- 3) The early bottom-up quenching was predicted to occur at the 1/4 lower part of the core, while it was observed at the ~2/3 lower part of the core in the experiment. Even more, it was calculated to be initiated slightly earlier than the measured data. This prediction of earlier and little amount of bottom up quenching resulted from the overestimated peak mass flow rate in the broken loop cold leg, i.e. cold leg break flow and the early end of subcooled blowdown as mentioned in section 4.1.
- 4) The calculated second heat up was also calculated to start earlier than the measured data due to earlier bottom-up quenching.

The peak cladding temperature(PCT) during the blowdown phase in the core was calculated to occur at the elevation of 22 to 27.5 inches(node 5) while it was measured at 27 inches from the bottom of core. The calculated PCT is 1121 K, which is ~50 K higher

than that measured in the experiment. The calculated maximum cladding temperature during the reflood phase was approximately 960 K while it was 831 K in the experiment. Such an overestimation is a result from the deficiency of RELAP5/MOD3.2 not to be able to predict the early bottom-up quenching in the middle part of the core.

5. SENSITIVITY STUDIES

To investigate the influence of discharge coefficient on the resultant cladding temperature behaviors, two additional calculations were carried out. A brief note of these calculations is as follows :

| calculation ID | subcooled discharge coeff. | saturated discharge coeff. |
|----------------|----------------------------|----------------------------|
| DC1 | 1.1 | 1.1 |
| (Base case) | (1.0) | (1.0) |
| DC2 | 0.9 | 0.9 |

And to find out the effects of the cross flow junction between the intact side downcomer and the broken side downcomer, an additional calculation was performed with six cross flow junctions between all the volumes of both sides. The sum of mass flow through the cross flow junctions before the initiation of transient in the calculation is made to be nearly equal to that in the base case calculation by adjusting the energy loss coefficients of junctions. For the convenience of later discussion, the calculation was named SIXX.

Finally, a calculation using RELAP5/MOD3.1 was conducted to identify the effects of improved features of RELAP5/MOD3.2 for the LBLOCA analysis.

5.1 Influence of Discharge Coefficient

In Figure 5.1 and 5.2, the calculated mass flow rates in the broken loop cold leg and hot leg with various discharge coefficients are presented for comparison. These figures show that the mass flow rate in each broken leg during the blowdown is highly de-

pendent on the discharge coefficient.

Figure 5.3 contains the difference between mass flow rate in the intact loop cold leg and mass flow rate in the broken loop cold leg, and Figure 5.4 presents the calculated bottom-up core mass flux at the hot core inlet junction induced by the mass flow difference. From these figures, it can be found that the bottom-up core flow in the blowdown phase is dominated by the discharge coefficient at the break and the smaller discharge coefficient, in other words, the lower break flow induces the higher bottom-up core flow.

This correlation between the discharge coefficient and the bottom-up core flow can be made clear by Figure 5.5 and 5.6, which show the calculated cladding temperature behaviors at the hot core node 5 and 8, respectively. As shown in the figures, the more break flow rate was estimated in the blowdown phase, the less bottom-up quenching was predicted.

5.2 Influence of Cross Flow Modeling in the Downcomer

Figure 5.7 contains the calculated downcomer liquid levels both in the base case calculation and in the SIXX calculation. From the figure, one can find that the liquid levels of both sides of downcomer predicted in the calculations showed almost similar trend.

The difference between the base case and SIXX calculation for the core bottom-up flow is shown in Figure 5.8. As shown in the figure, the initiation and completion of bottom-up flow in the SIXX calculation was predicted to be little later than those in the base case, and the total bottom-up flow in the SIXX calculation is considered somewhat greater than that calculated in the base case calculation. Such a delayed and larger bottom-up flow resulted in lower and delayed second heat up.

Figure 5.9 shows the mass flux at the outlet of the core. The calculated top-down quenching flow in the base case was higher than that predicted in the SIXX calculation.

However, the cladding temperature behavior predicted in the both calculations didn't show any significant difference because the differences of flow behavior were not so large. The cladding temperature behaviors at hot core node 1, 5, and 10 are presented in Figure 5.10 to 5.12.

In conclusion, the hydraulic and thermal behavior in the core calculated by RELAP5/MOD3.2 was not strongly dependent on the number and position of the cross flow junctions in the downcomer.

5.3 Calculation Using RELAP5/MOD3.1

A calculation similar to the base case using RELAP5/MOD3.1, for which we didn't make any change after it was received at October in 1993 from USNRC , was performed to identify the difference between RELAP5/MOD3.1 and RELAP5/MOD3.2 for LBLOCA analysis.

The calculated hydraulic behavior by RELAP5/MOD3.1 is very similar to that predicted by RELAP5/MOD3.2. The mass flow rates in the broken loop cold leg and hot leg, for instance, showed nearly same trend as shown in Figure 5.13 and Figure 5.14. However, the cladding temperatures predicted by RELAP5/MOD3.1 showed less degree of heat up both in the blowdown phase and the reflood phase than those by RELAP5/MOD3.2. The cladding temperatures calculated by RELAP5/MOD3.1 at several elevations are presented in Figure 5.15 to Figure 5.17 with corresponding data by RELAP5/MOD3.2. More profound studies of these results were not tried because the predicted cladding temperature behavior by RELAP5/MOD3.1 and RELAP5/MOD3.2 showed no dramatic difference.

6. RUN STATISTICS

The computer used in the present calculations was HP9000/K200 workstation at KNFC, with OS Version 10.01.

Figure 6.1 presents the plot of the required CPU time for the transient time in the base case calculation. And the time step sizes are also plotted in Figure 6.2. The user-specified maximum time step was 0.01 sec up to 30 secs in real time and then reduced to 0.002 sec up to 80 secs. The run statistics from the major edit is summarized in Table 6.1 and the grind time can be calculated as follows.

$$\text{Computer time, } CPU = 2397.7 - 1 = 2396.7$$

$$\text{Number of time step, } DT = 28615 - 167 = 28448$$

$$\text{Number of volume, } C = 147$$

$$\text{Transient real time, } RT = 80 \text{ (secs)}$$

$$\text{Grind time} = CPU \times 1000 / (C \times DT) = 0.573 \text{ CPU m sec/vol/step}$$

6. CONCLUSIONS AND RECOMMENDATIONS

RELAP5/MOD3 code was assessed using LOFT LP-02-6 test data. A base case calculation using RELAP5/MOD3.2 was carried out as a reference case. Discharge coefficient sensitivity studies were performed to investigate the influence of this user-specific parameter in the analysis of LBLOCA. A more detailed modeling of cross flow in the inlet annulus and downcomer volume was tried to improve the code predictability of early bottom-up quenching in the blowdown phase. As a final case, a calculation using RELAP5/MOD3.1 was performed to identify the differences between RELAP5/MOD3.1 and RELAP5/MOD3.2. Based upon the results from the scope of this study, the following conclusions were made.

- 1) Using LOFT LBLOCA test data LP-02-6, a base calculation with a standard nodalization was successfully performed and matched relatively well with the experimental data.
- 2) RELAP5/MOD3.2 with standard nodalization can predict system hydraulic behavior. However the mass flow rates in the broken loop cold leg and hot leg during the subcooled blowdown were largely overestimated.
- 3) RELAP5/MOD3.2 can predict well the blowdown heat up of the core. However, the calculated blowdown heat up was initiated slightly earlier than the experiment due to the poor prediction of heat transfer in the fuel rod during blowdown. The calculated PCT was predicted to be ~50K higher than the measured data.
- 4) The bottom-up quenching in the middle part of hot core was not predicted

properly by RELAP5/MOD3.2, therefore, the maximum cladding temperature during the reflood phase was highly overestimated to be about 96f Δ .

- 5) RELAP5/MOD3.2 was so sensitive to the discharge coefficient that the resultant behavior of cladding temperatures was greatly varied with small change of discharge coefficient. The development of more accurate break flow model, which is known to be undergoing, should be made to remove the sensitiveness to this user accessible parameter.
- 6) From our analysis of cross flow modeling in the downcomer volume, it was revealed that the core flow behavior is not dependent on the position and number of cross flow junctions connected. In other words, single cross flow junction with a low energy loss coefficient and multiple cross flow junctions with a high energy loss coefficient might have similar effect on the resultant thermal behavior in the core.
- 7) Neither of code versions, RELAP5/MOD3.1 and RELAP5/MOD3.2, could predict properly the early bottom-up quenching in the middle part of the core. The only effect of improved features of RELAP5/MOD3.2 could be shown in the lower part of core, where RELAP5/MOD3.2 could predict the blowdown heat up better than RELAP5/MOD3.1.
- 8) It was revealed that RELAP5/MOD3 can be used as a best estimate tool for analysis of LBLOCA with the improvement of break flow model which has great influence on the predictability of early bottom-up quenching in the LBLOCA.

REFERENCES

- [1] LOFT System and Test Description, Reeder, D.G., NUREG/CR-0247 Tree-1208, 1978(update 9/80)
- [2] Post-Test-Analysis and Nodalization Studies of OECD LOFT Experiment LP-02-6 with RELAP5/MOD2 cy 36-02, D. Lübbesmeyer, Draft to NUREG Report
- [3] Post-Test-Analysis and Nodalization Studies of OECD LOFT Experiment LP-LB-1 with RELAP5/MOD2 cy 36-02, D. Lübbesmeyer, NUREG/IA-0089, October 1992
- [4] Quick-Look Report on OECD LOFT Experiment LP-02-6, J.P.Adams, K.G.Condie, D.L.Blatt, OECD LOFT-T-3404, October 1993
- [5] RELAP5/MOD3 code manual, The RELAP5 Development Team, NUREG/CR-5535, August 1995
- [6] TRAC-PF1/MOD1 Calculation of LOFT Experiment LP-02-6, P.Coddington, C.Gill, NUREG/IA-0027, April 1992

Table 2.1 Initial and boundary conditions for experiment LP-02-6

| Parameter | Measured Data | Calculated value |
|---|---------------|------------------|
| Power(MW) | 46.0±1.2 | 46.0 |
| Temperature Across Core(K) | 33.1±1.1 | 33.57 |
| Hot Leg Pressure(MPa) | 15.09±0.08 | 15.10 |
| Cold Leg Temperature(K) | 555.9±1.1 | 555.98 |
| Mass Flow Rate(Kg/s) | 248.7±2.6 | 248.69 |
| Pressurizer | | |
| Liquid Level(m) | 1.04±0.04 | 1.041 |
| Water Temperature(K) | 615.6±5.8 | 615.76 |
| Pressure(MPa) | 15.3±0.11 | 15.09 |
| Broken Loop | | |
| Cold Leg Temperature(K) | 553.0±6.0 | 555.8 |
| Hot Leg Temperature(K) | 560.0±6.0 | 555.9 |
| Emergency Core cooling System | | |
| Accumulator Liquid Level(m) | 2.10±0.0 | 2.10 |
| Accumulator Pressure(MPa) | 4.11±0.06 | 4.11 |
| Accumulator Liquid Temperature(K) | 302. ±6.1 | 302. |
| High Pressure Injection Flow Rate(l/s) | 1.04±0.04 | 1.04 |
| High Pressure Injection Liquid Temperature(K) | 305. ±7 | 305. |
| Low Pressure Injection Flow Rate(l/s) | a | a |
| Low Pressure Injection Liquid Temperature(K) | 305. ±7 | 305. |

a. Depending on pressure difference between LPIS and downcomer

Table 2.2 Chronology of event for experiment LP-02-6

| Event | Measured Data (seconds) | Calculated value (seconds) |
|---|----------------------------|-------------------------------|
| Blowdown Valve Open | 0.0 | 0.0 |
| Reactor Scrammed | 0.1 | 0.1 |
| Primary Coolant Pumps Tripped | 0.8 | 0.8 |
| Cladding Temperature Initially Deviated from Saturation | 0.9 | 0.5 |
| End of Subcooled Break Flow | 4.0 | 3.3 ^a |
| Blowdown Peak Cladding Temperature Reached | 4.9 | 3.8 |
| Bottom-up Core Rewet Initiated | 5.2 | 3.7 |
| Bottom-up Core Rewet Completed | 9.1 | 13.0 |
| Partial Core Top-down Quench Initiated | 14.8 | 14.5 |
| Pressurizer Empty | 15.5 | 14.0 |
| Accumulator Injection Initiated | 17.5 | 14.05 |
| Partial Core Top-down Quench Completed | 18.6 | 24.6 |
| High Pressure Injection Initiated | 21.8 | 21.8 |
| Lower Plenum Refill Completed | 30.7 | 32. ^b |
| Low Pressure Injection Initiated | 34.8 | 34.8 |
| Reflood Peak Cladding Temperature Reached | 41.0 | 26.3 |
| Accumulator Injection Completed | 57.0 | 50.0 |
| Core Quench Completed | 56.0 | 60.5 |
| Core Reflood Completed | 59.0 | 64.0 |

a. This value is based on the time when the junction void fraction in the cold leg break valve is less than 0.1

b. The measured time for complete refill of the lower plenum is based on when the lowest fuel rod cladding quenched.

Table 4.1 List of assessment parameters (LOFT LP-02-6)

| Description | Calculation | Measurement | Uncertainty | Figure |
|--|---------------|---|-----------------------|--------|
| Primary System Pressure | p 112-01 | PE-PC-002 | 0.036 MPa | 4.1 |
| BLCL Mass Flow Rate | mflowj 340-01 | FR-BL-105 | Not found | 4.2 |
| BLHL Mass Flow Rate | mflowj 305-01 | FR-BL-205 | " | 4.3 |
| ILCL Mass Flow Rate | mflowj 175-01 | FR-PC-100 | " | 4.4 |
| ILHL Mass Flow Rate | mflowj 112-01 | FR-PC-205 | " | 4.5 |
| Downcomer Fluid Temperature | tempf 210-02 | TE-1ST-002 | 5.1 K | 4.6 |
| Lower Plenum Fluid Temperature | tempf 220-01 | TE-5LP-001 | 5.1 K | 4.7 |
| LPIS Mass Flow Rate | mflowj 630-00 | FT-P120-085 | 0.25 l/s | 4.8 |
| Cladding Temperature (Central 2 inches) | httemp 231-01 | TE-5H02-002 | 5.2 K | 4.12 |
| Cladding Temperature (Central 5 inches) | httemp 231-01 | TE-5I06-005 TE-5J04-005 | " " | 4.12 |
| Cladding Temperature (Central 8 inches) | httemp 231-02 | TE-5H07-008 | " | 4.13 |
| Cladding Temperature (Central 11 inches) | httemp 231-02 | TE-5G06-011 | " | 4.13 |
| Cladding Temperature (Central 15 inches) | httemp 231-03 | TE-5F04-015 TE-5H05-015 TE-5M07-015 | " " " | 4.14 |
| Cladding Temperature (Central 21 inches) | httemp 231-04 | TE-5J04-021 TE-5J06-021 | " " | 4.15 |
| Cladding Temperature (Central 24 inches) | httemp 231-05 | TE-5H06-024 | " | 4.16 |
| Cladding Temperature (Central 26 inches) | httemp 231-05 | TE-5F04-026 TE-5F08-026 TE-5I08-026 TE-5J06-026 TE-5M07-026 | " " " " " | 4.16 |
| Cladding Temperature (Central 27 inches) | httemp 231-05 | TE-5D07-027 TE-5I04-027 | " " | 4.16 |
| Cladding Temperature (Central 28 inches) | httemp 231-06 | TE-5H06-028 | " | 4.17 |
| Cladding Temperature (Central 30 inches) | httemp 231-06 | TE-5G06-030 | " | 4.17 |

Table 4.1 List of assessment parameters (Continued)

| Description | Calculation | Measurement | Uncertainty | Figure |
|---|---------------|---|-------------|--------|
| Cladding Temperature (Central 31 inches) | httemp 231-06 | TE-5C07-031 TE-5D07-031 | 5.2 K " | 4.17 |
| Cladding Temperature (Central 32 inches) | httemp 231-06 | TE-5F04-032 TE-5H06-032 TE-5M07-032 | " " " | 4.17 |
| Cladding Temperature (Central 37 inches) | httemp 231-07 | TE-5H06-037 | " | 4.18 |
| Cladding Temperature (Central 39 inches) | httemp 231-08 | TE-5I06-039 TE-5I04-039 | " " | 4.19 |
| Cladding Temperature (Central 41 inches) | httemp 231-08 | TE-5H07-041 | " | 4.19 |
| Cladding Temperature (Central 43.8 inches) | httemp 231-08 | TE-5C07-43.8 TE-5I04-43.8 | " " | 4.19 |
| Cladding Temperature (Central 45 inches) | httemp 231-09 | TE-5G06-045 | " | 4.20 |
| Cladding Temperature (Central 49 inches) | httemp 231-09 | TE-5H05-049 | " | 4.20 |
| Cladding Temperature (Central 54 inches) | httemp 231-10 | TE-5I06-054 TE-5J04-054 | " " | 4.21 |
| Cladding Temperature (Central 58 inches) | httemp 231-11 | TE-5H07-058 | " | 4.22 |
| Cladding Temperature (Central 62 inches) | httemp 231-12 | TE-5F04-062 TE-5G06-062 | " " | 4.23 |

Table 6.1 Run statistics data in base case

| Transient time (sec) | CPU time (sec) | Attempted ADV | Repeated ADV | Last DT | Courant DT |
|-------------------------|-------------------|------------------|-----------------|------------|---------------|
| 0 | 1.00 | 0 | 0 | 0.01 | 0 |
| 10 | 94.46 | 1011 | 3 | 0.01 | 1.11175-2 |
| 20 | 189.78 | 2011 | 3 | 0.01 | 9.57746-3 |
| 30 | 291.52 | 3106 | 3 | 0.01 | 1.17485-2 |
| 40 | 784.41 | 8613 | 166 | 0.002 | 1.06071-2 |
| 50 | 1229.55 | 13615 | 167 | 0.002 | 1.84512-2 |
| 60 | 1676.05 | 18615 | 167 | 0.002 | 1.65845-2 |
| 70 | 1995.11 | 23615 | 167 | 0.002 | 4.72061-2 |
| 80 | 2397.70 | 28615 | 167 | 0.002 | 1.38078-2 |

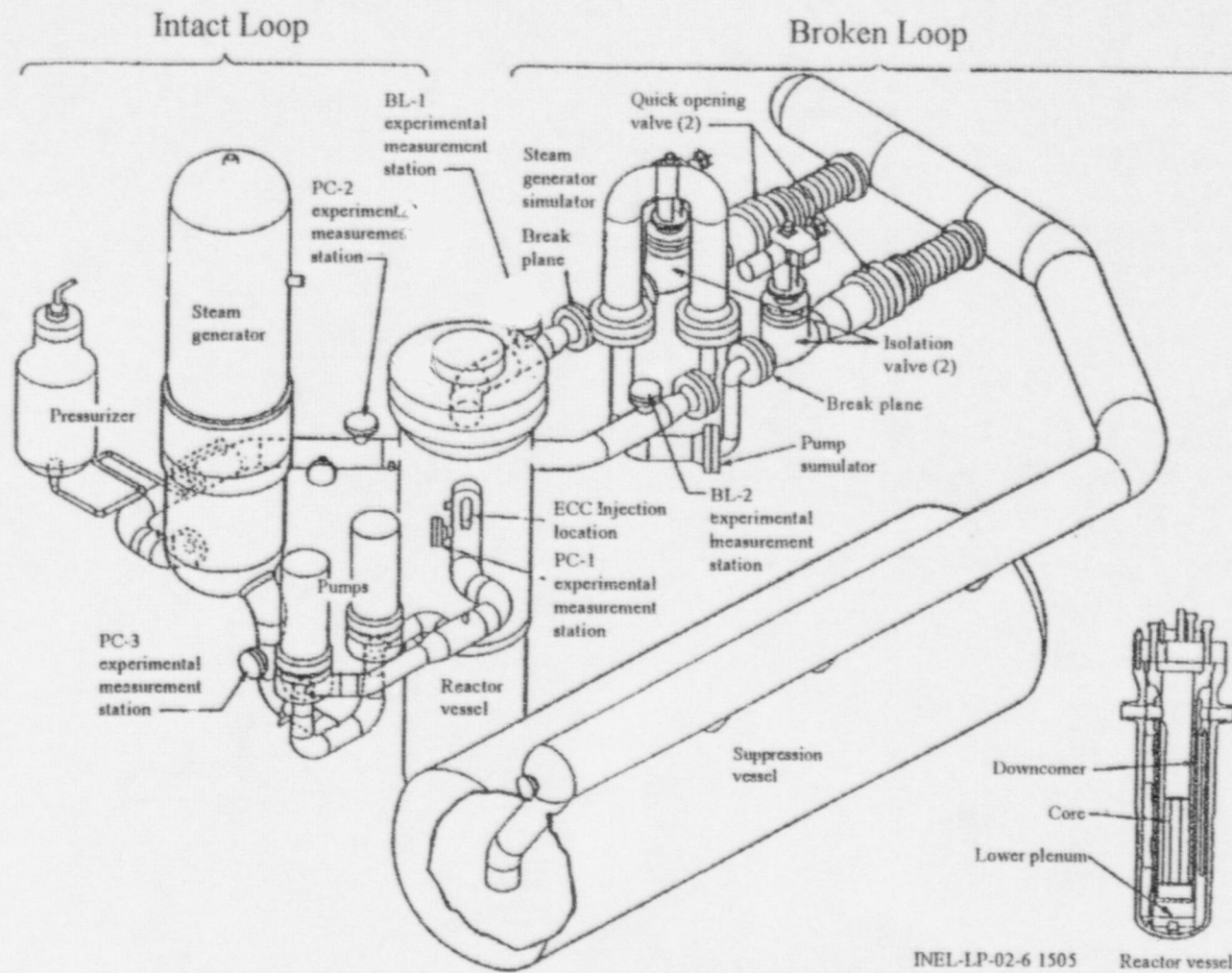


Figure 2.1 LOFT major component

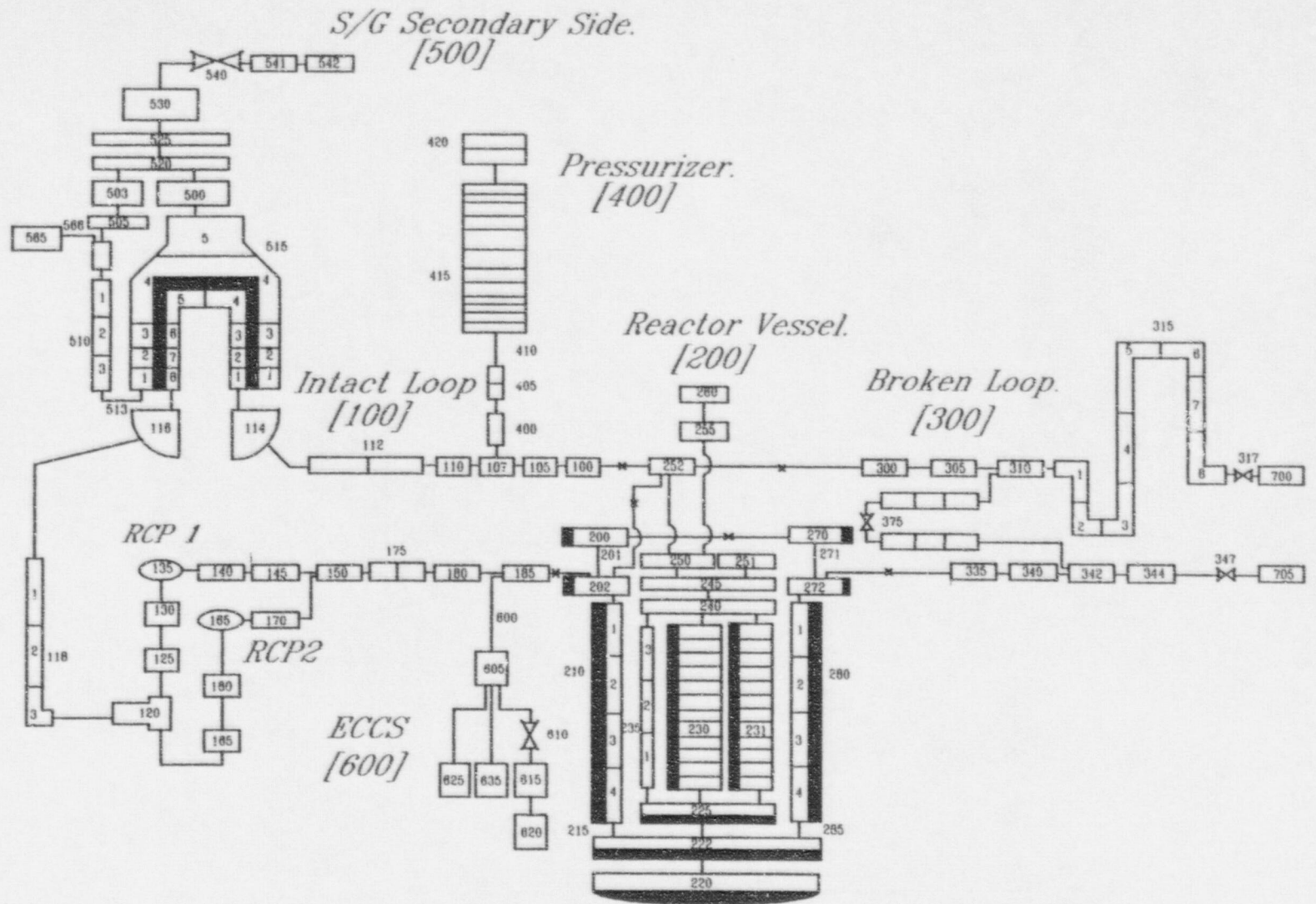


Figure 3.1 Schematic diagram of standard nodalization

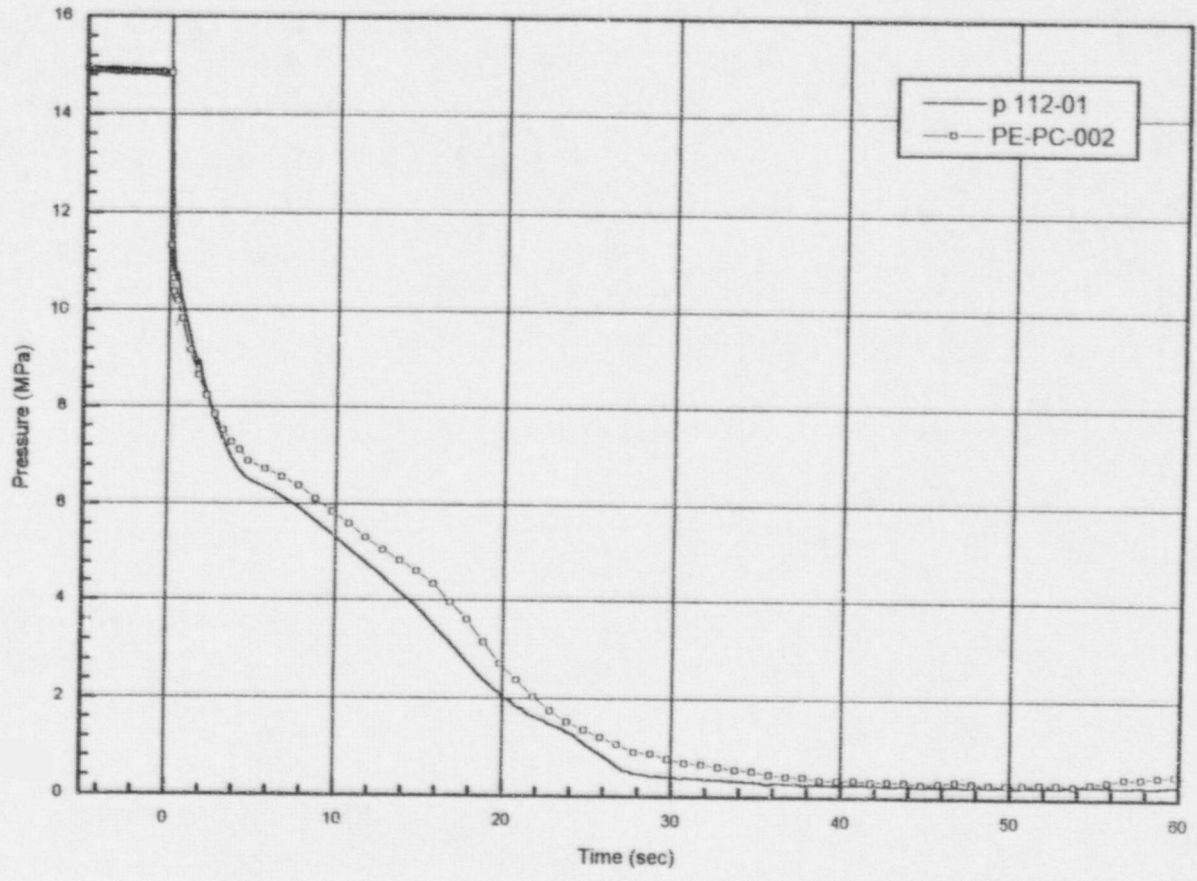


Figure 4.1 System pressure in the intact loop hot leg

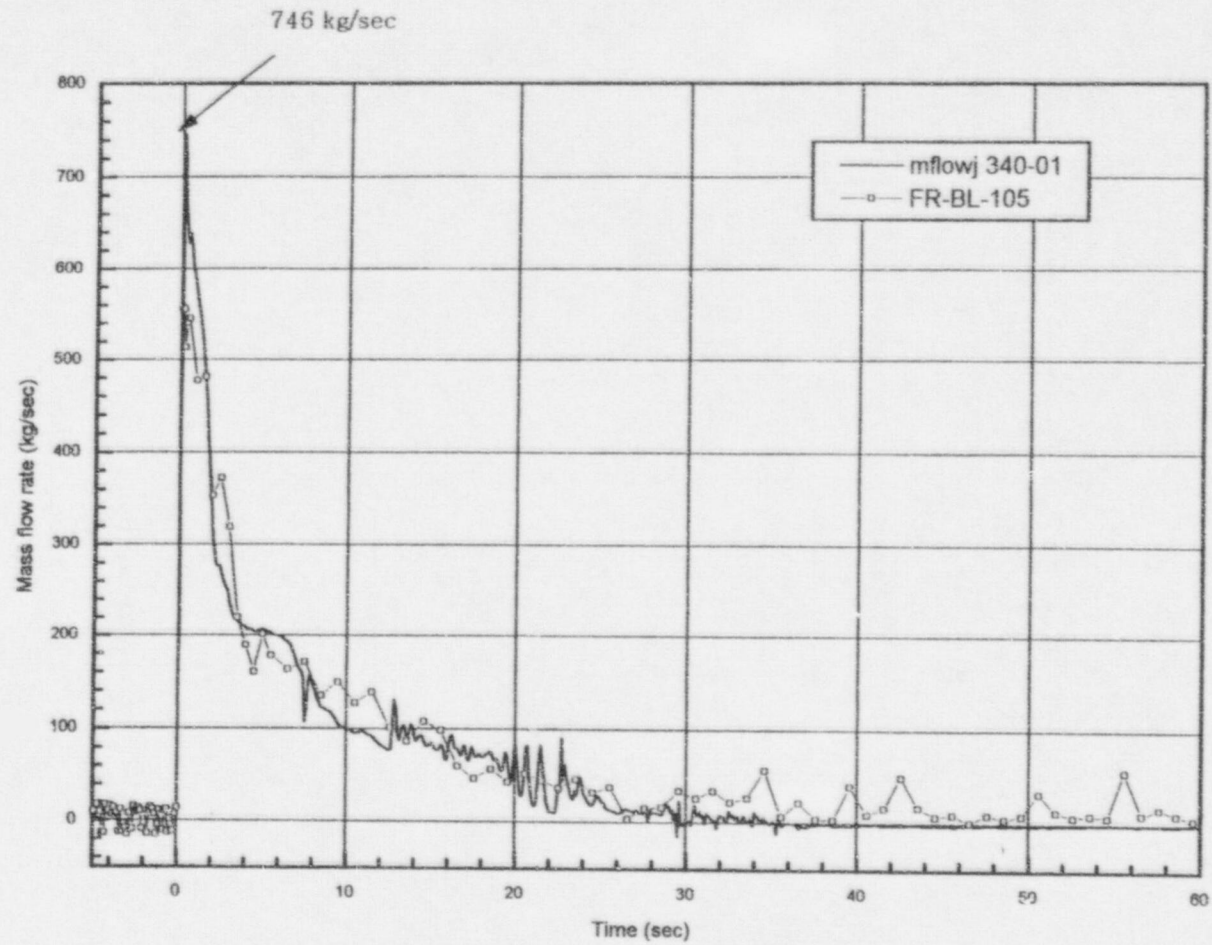


Figure 4.2 Mass flow rate in the broken loop cold leg

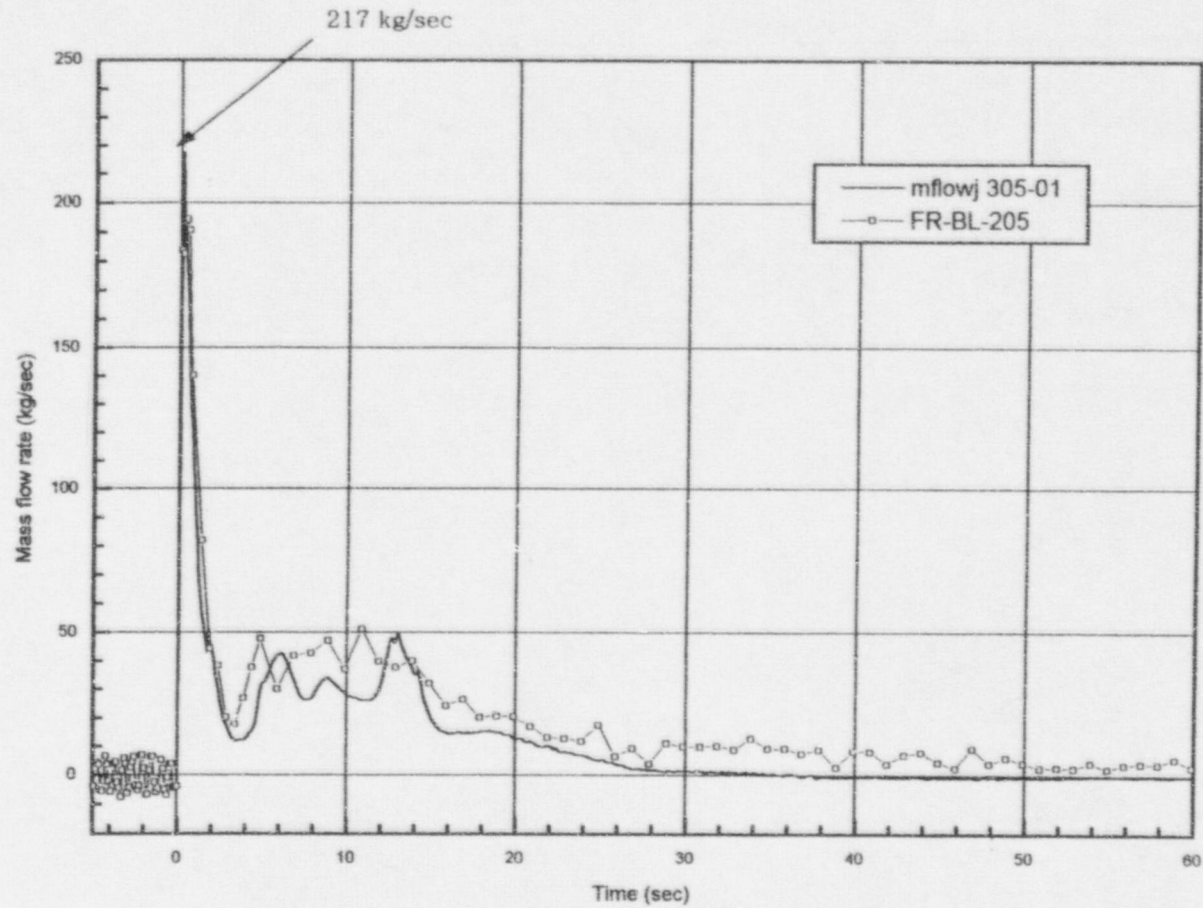


Figure 4.3 Mass flow rate in the broken loop hot leg

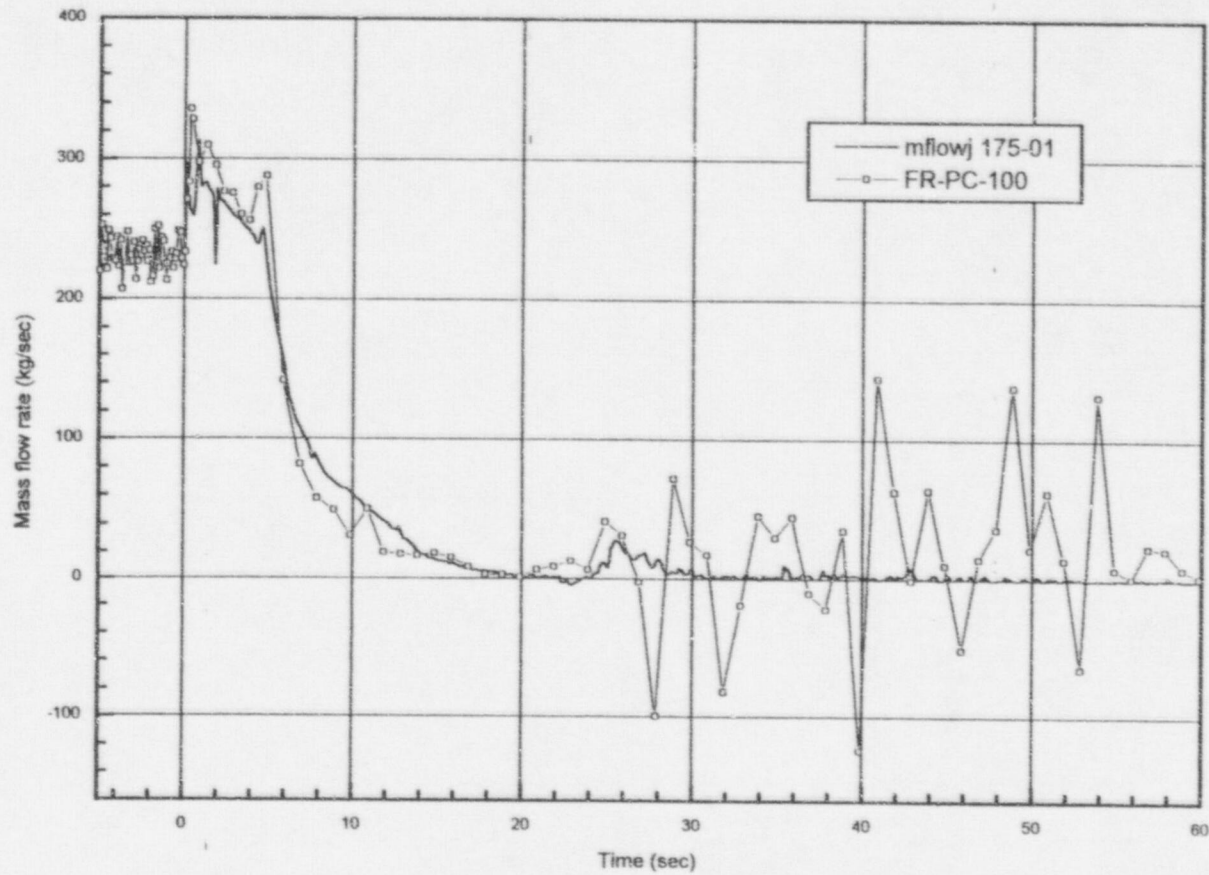


Figure 4.4 Mass flow rate in the intact loop cold leg

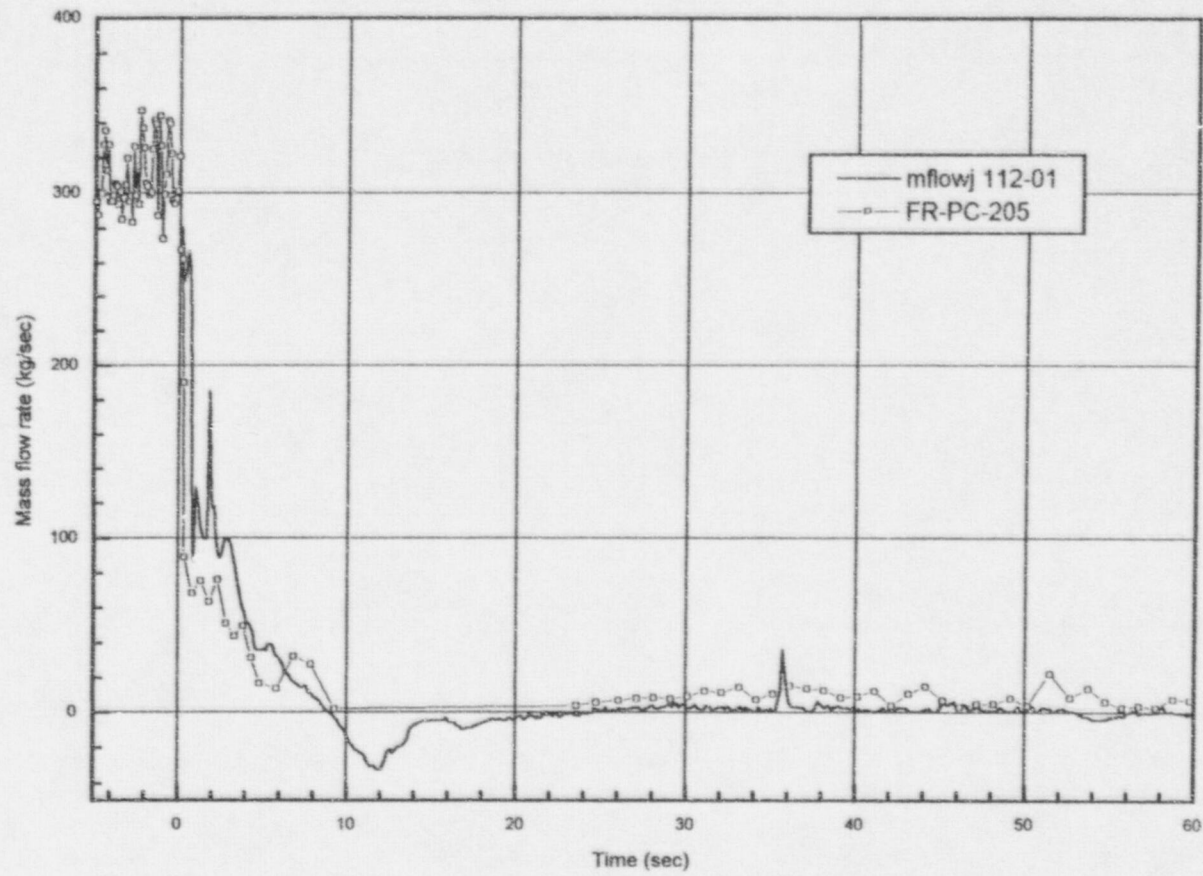


Figure 4.5 Mass flow rate in the intact loop hot leg

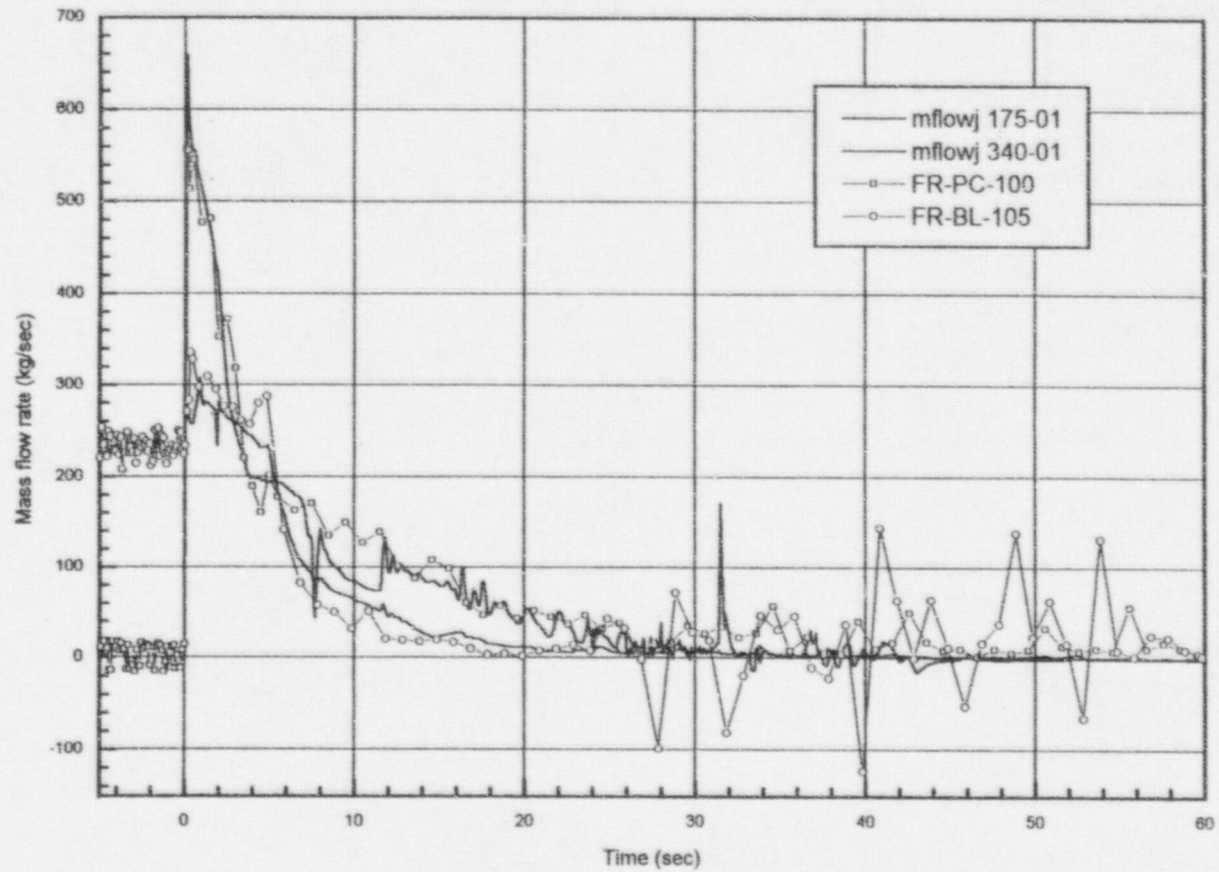


Figure 4.6 Mass flow in the broken loop cold leg and the intact loop cold leg

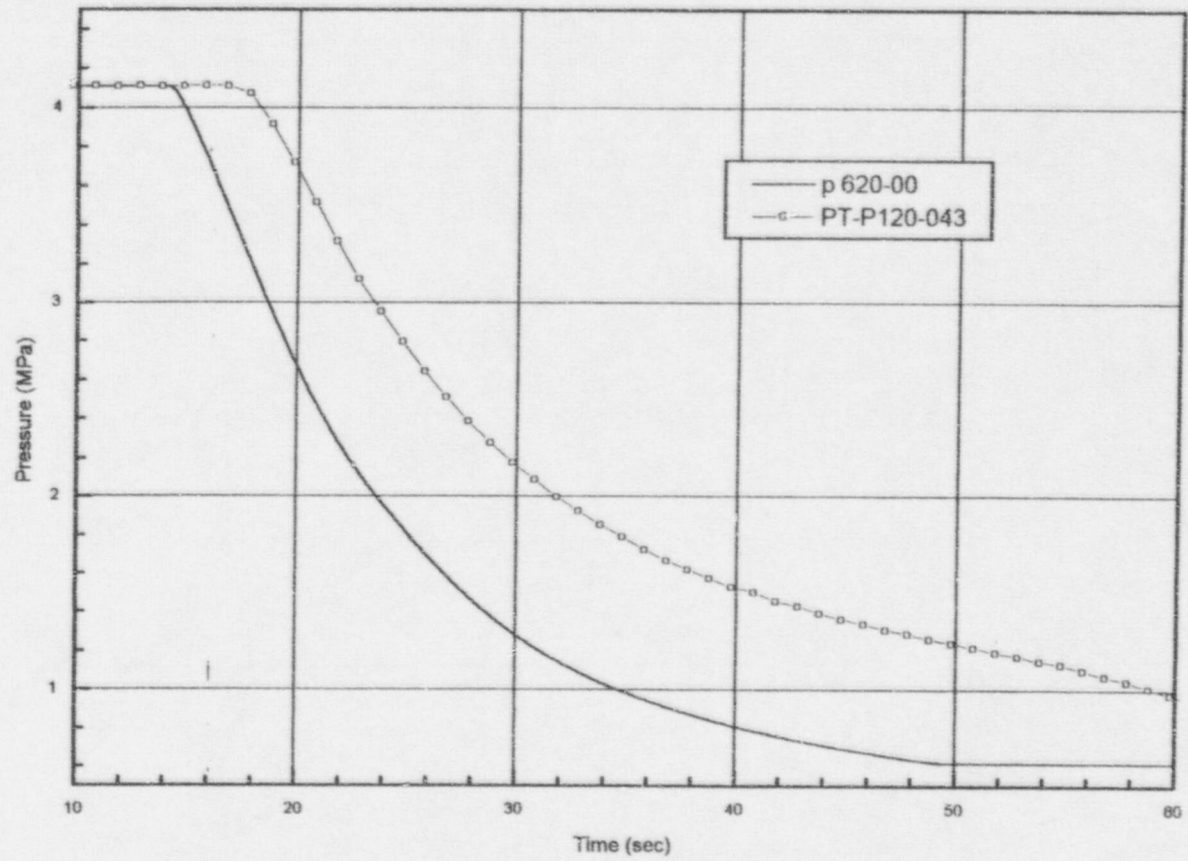


Figure 4.7 Accumulator pressure

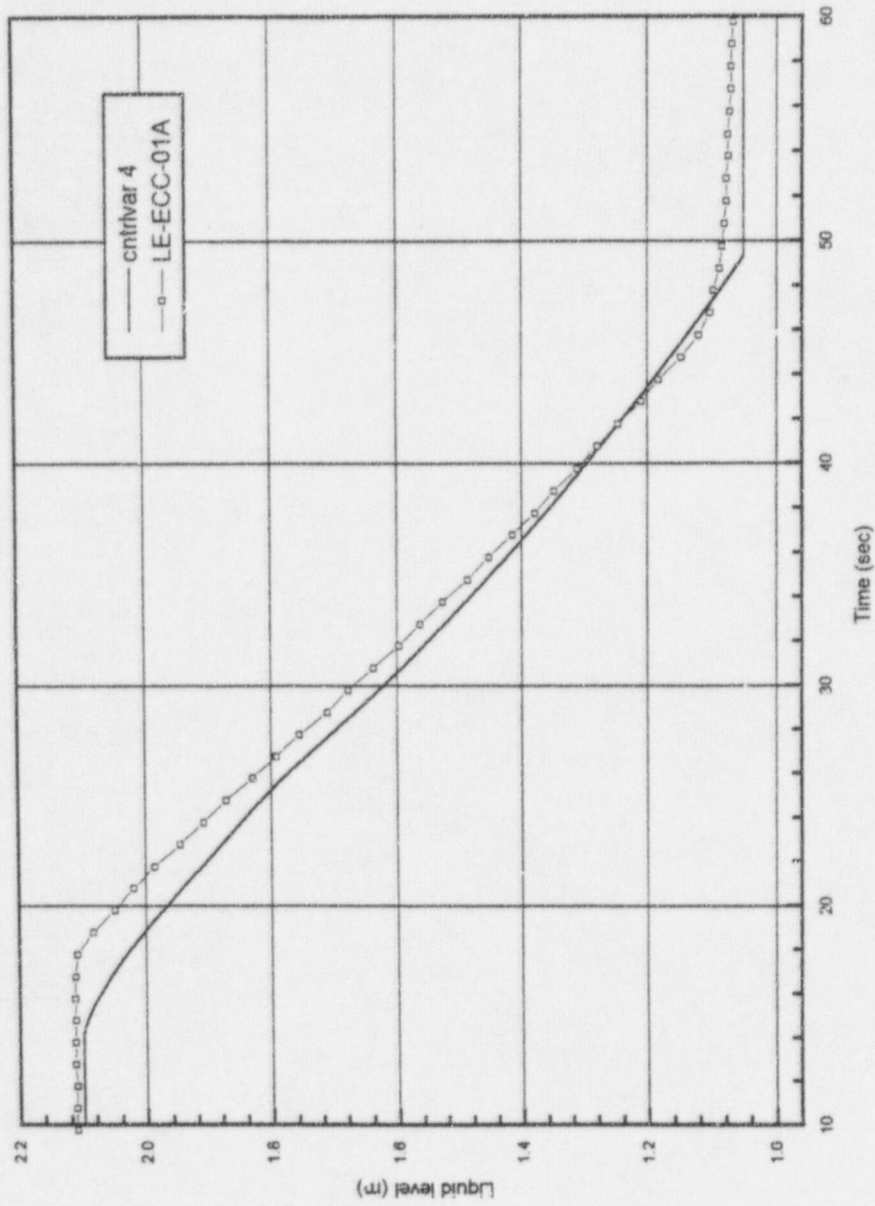


Figure 4.8 Accumulator liquid level

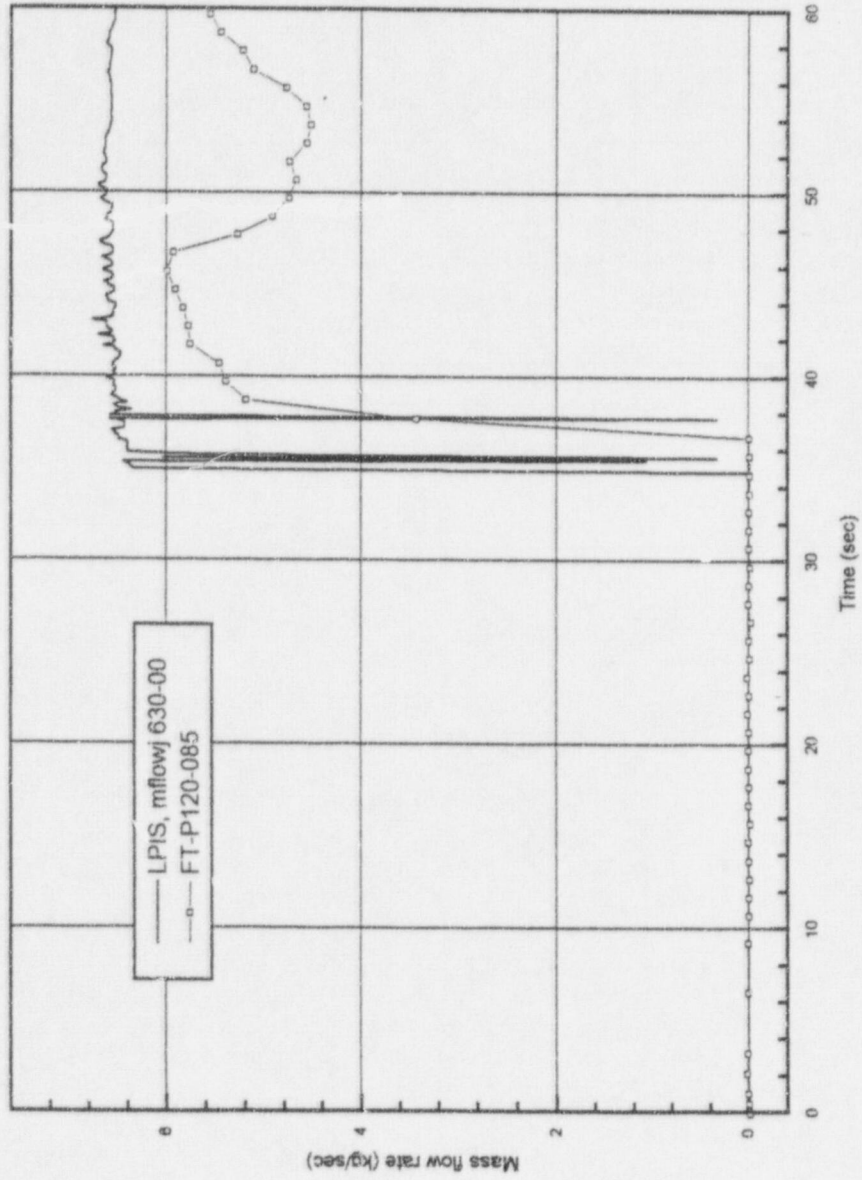


Figure 4.9 LPIS discharge flow rate

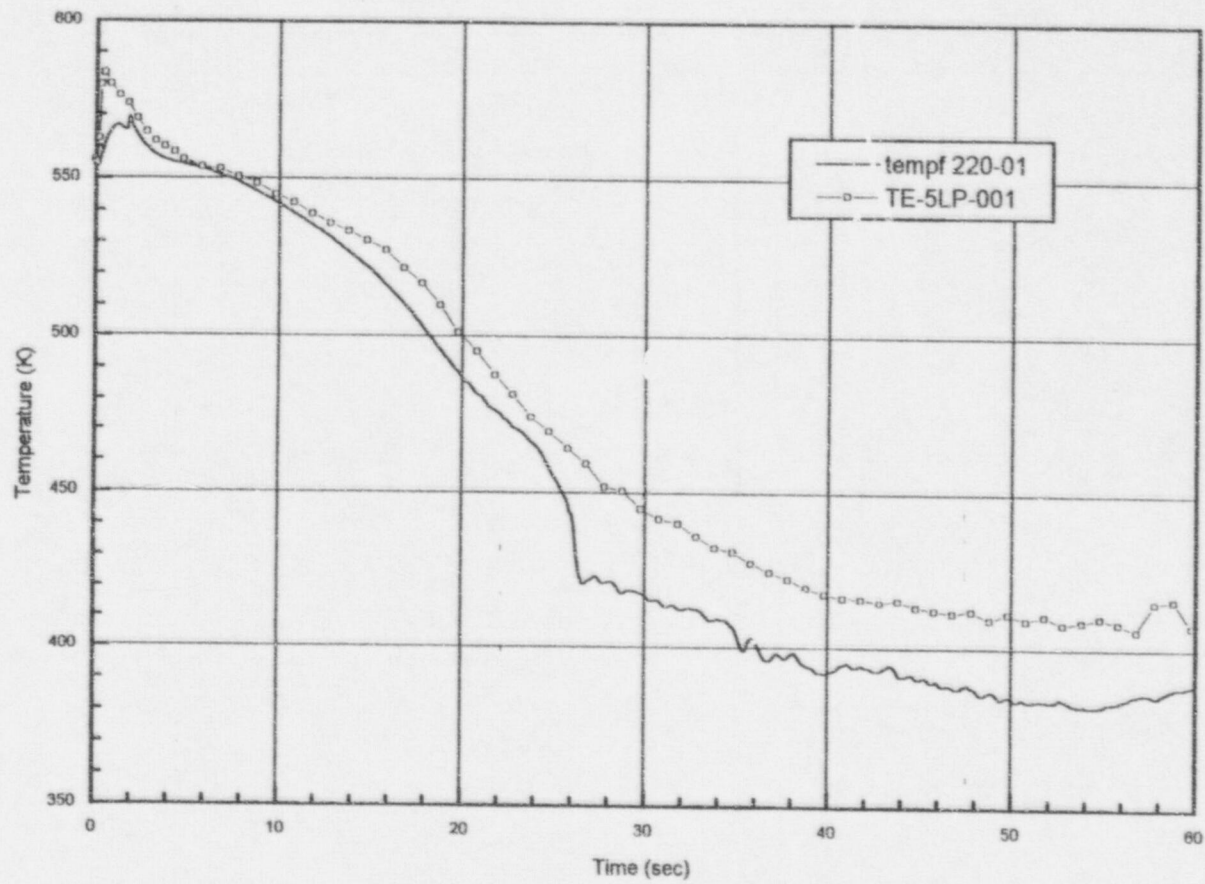


Figure 4.10 Fluid temperature in the lower plenum

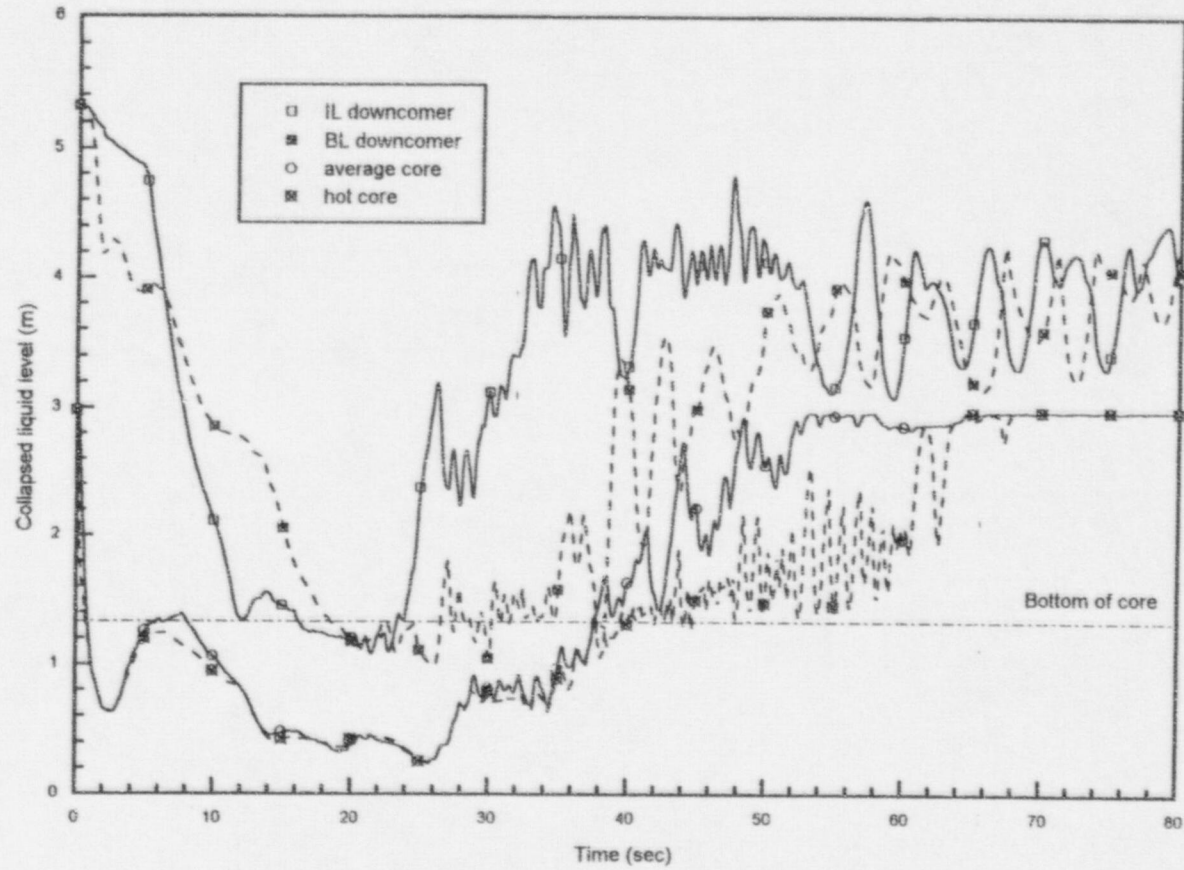


Figure 4.11 Collapsed liquid levels in the downcomer and core channels

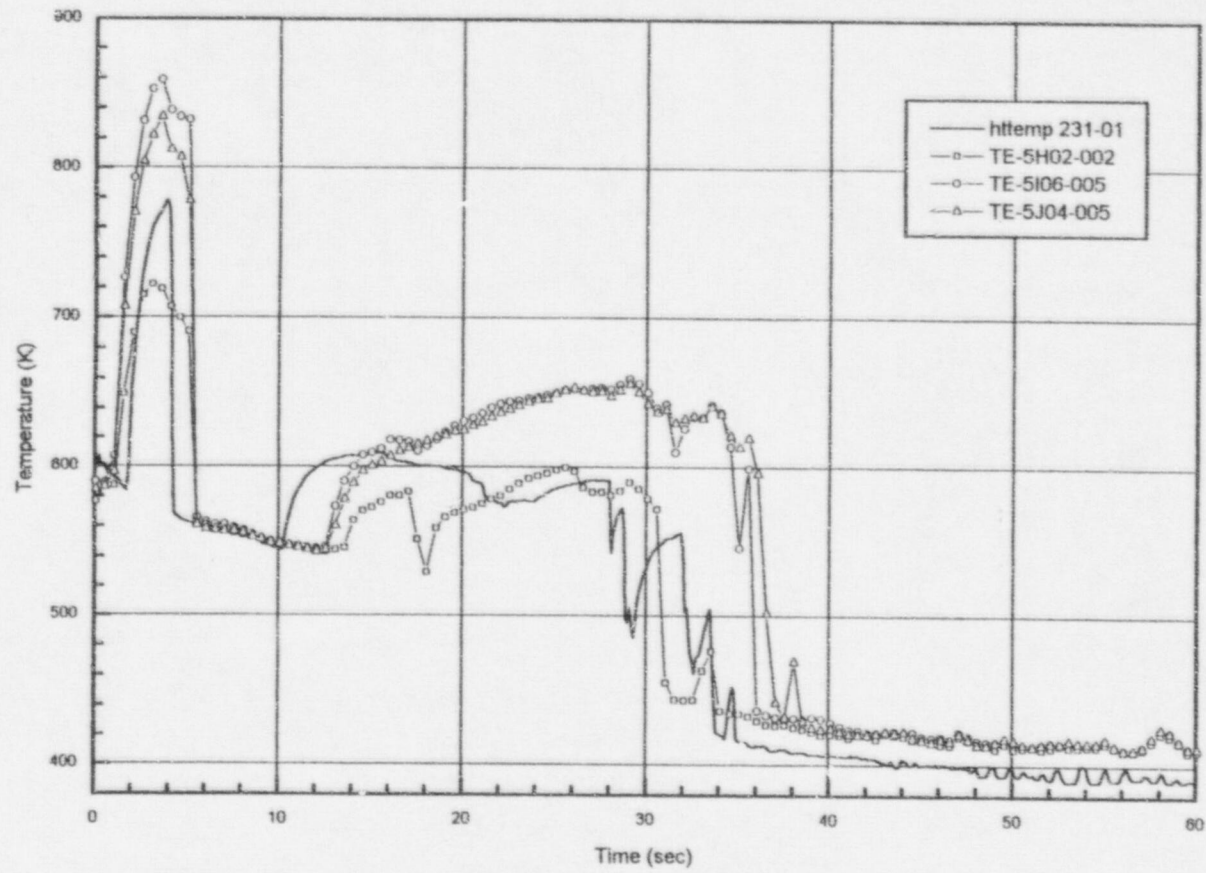


Figure 4.12 Cladding temperature at hot core node 1

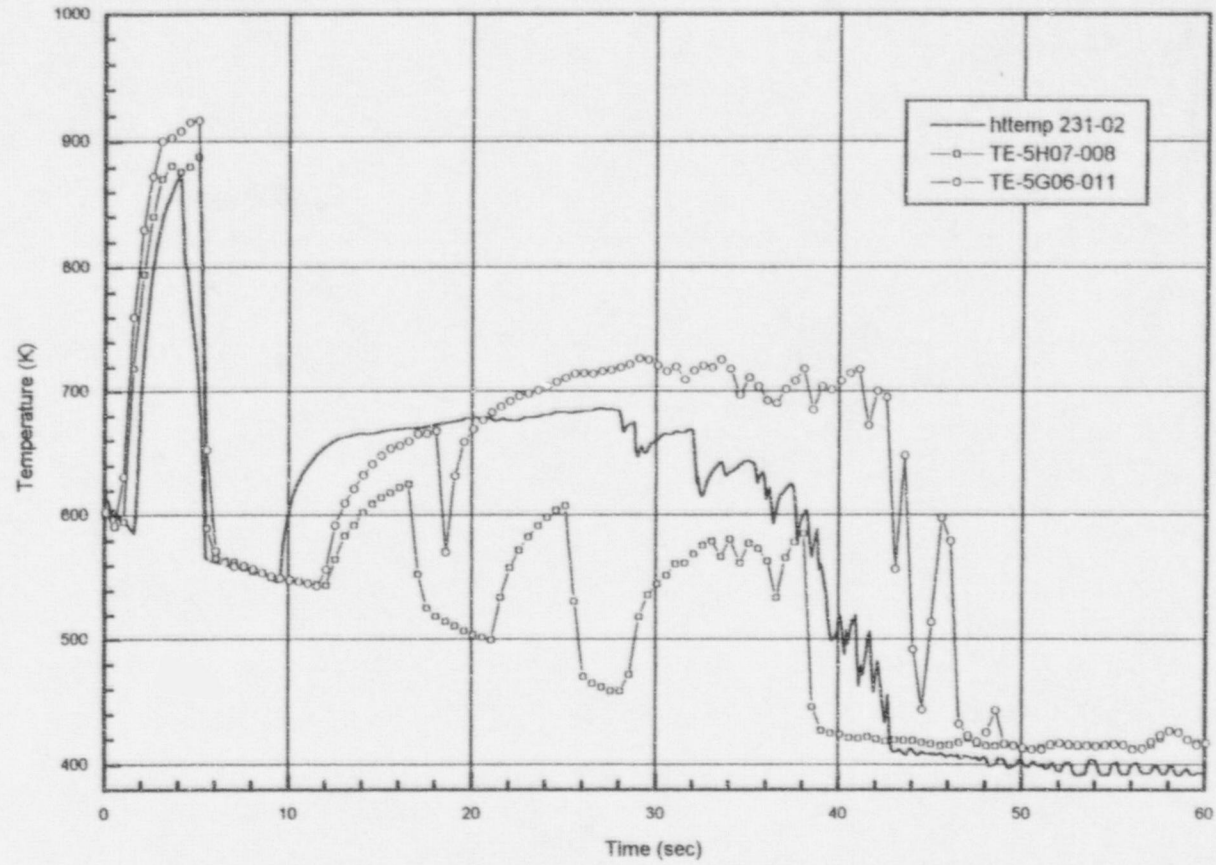


Figure 4.13 Cladding temperature at hot core node 2

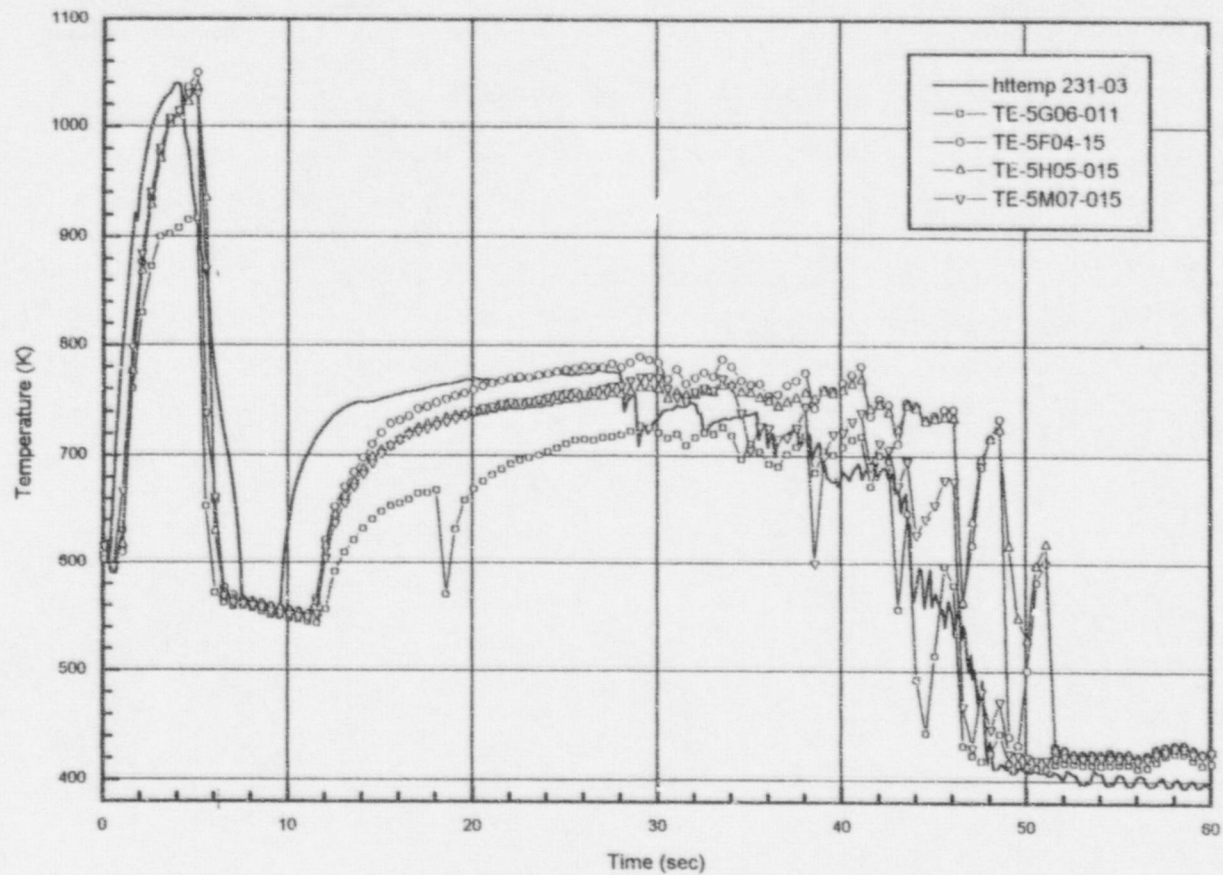


Figure 4.14 Cladding temperature at hot core node 3

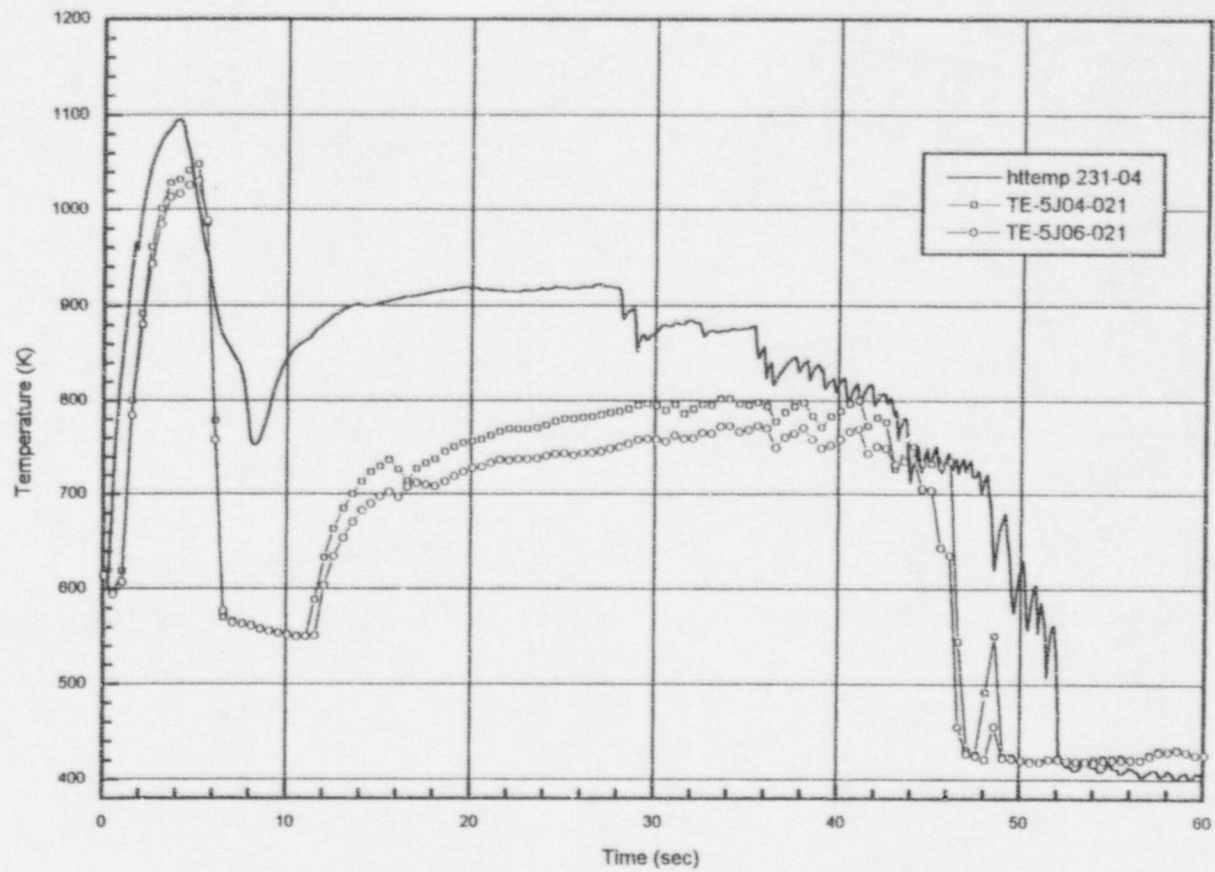


Figure 4.15 Cladding temperature at hot core node 4

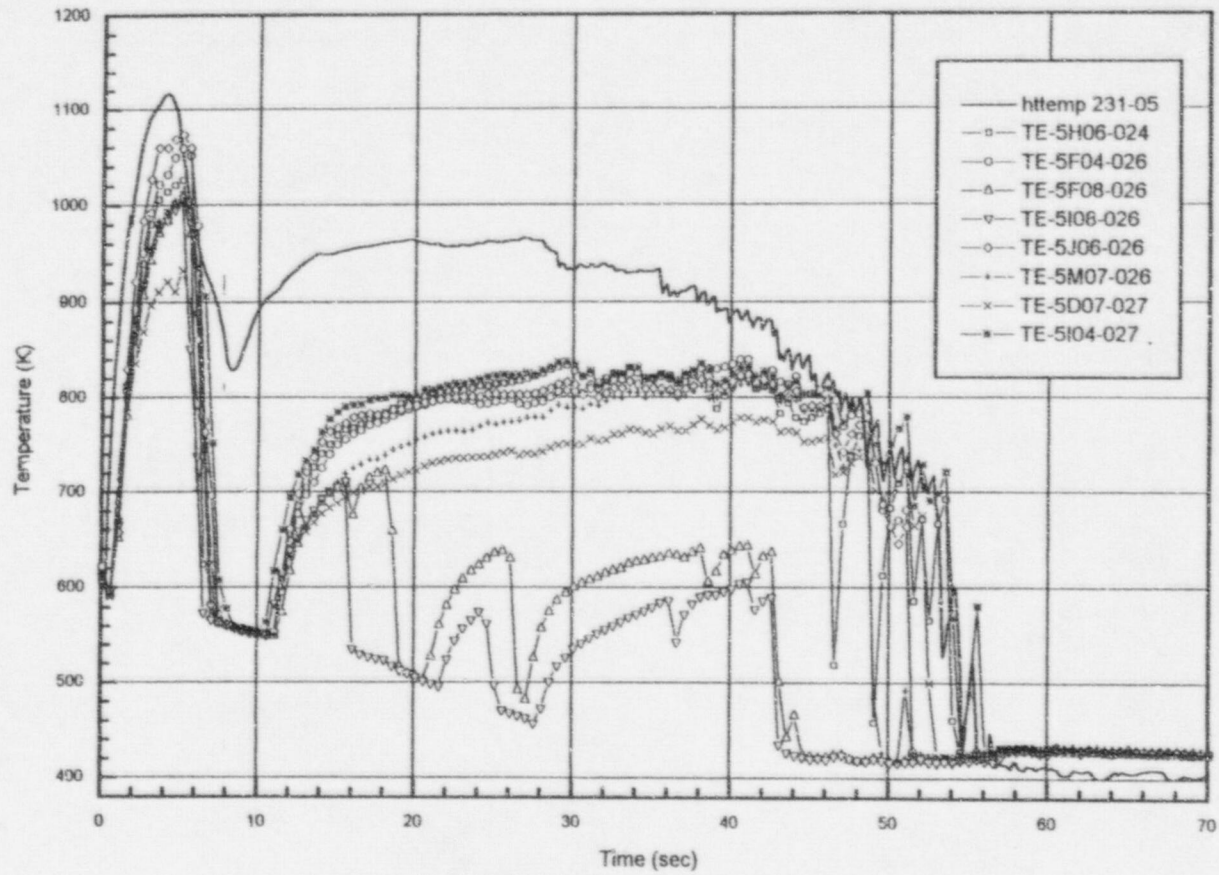


Figure 4.16 Cladding temperature at hot core node 5

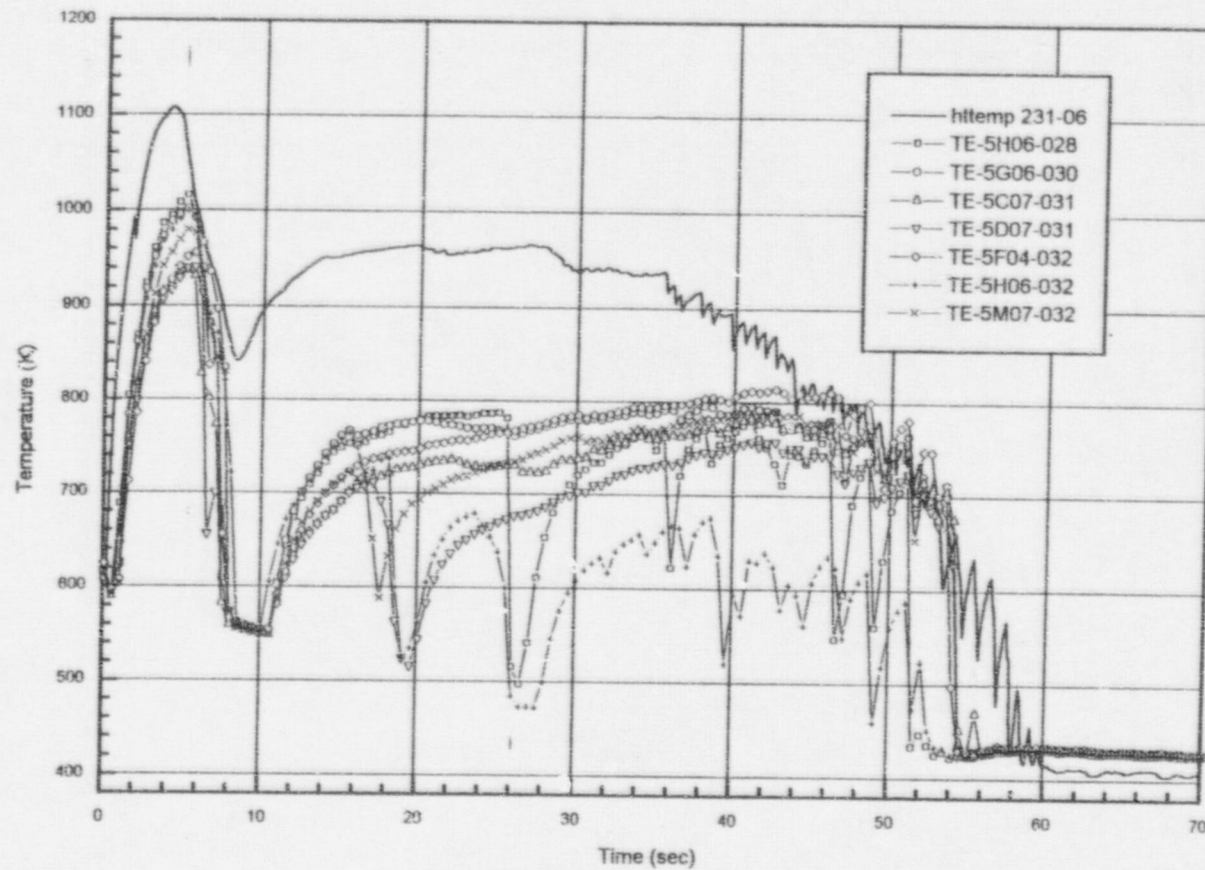


Figure 4.17 Cladding temperature at hot core node 6

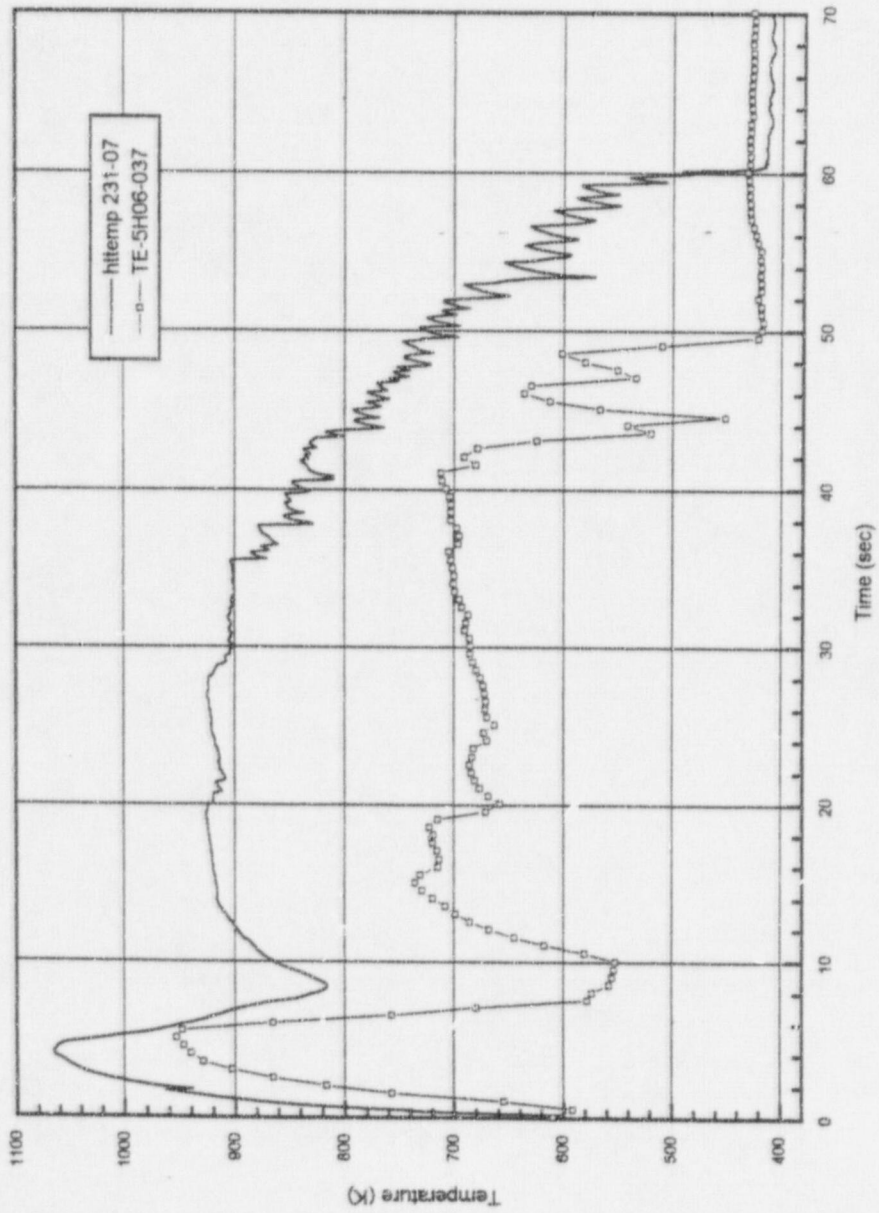


Figure 4.18 Cladding temperature at hot core node 7

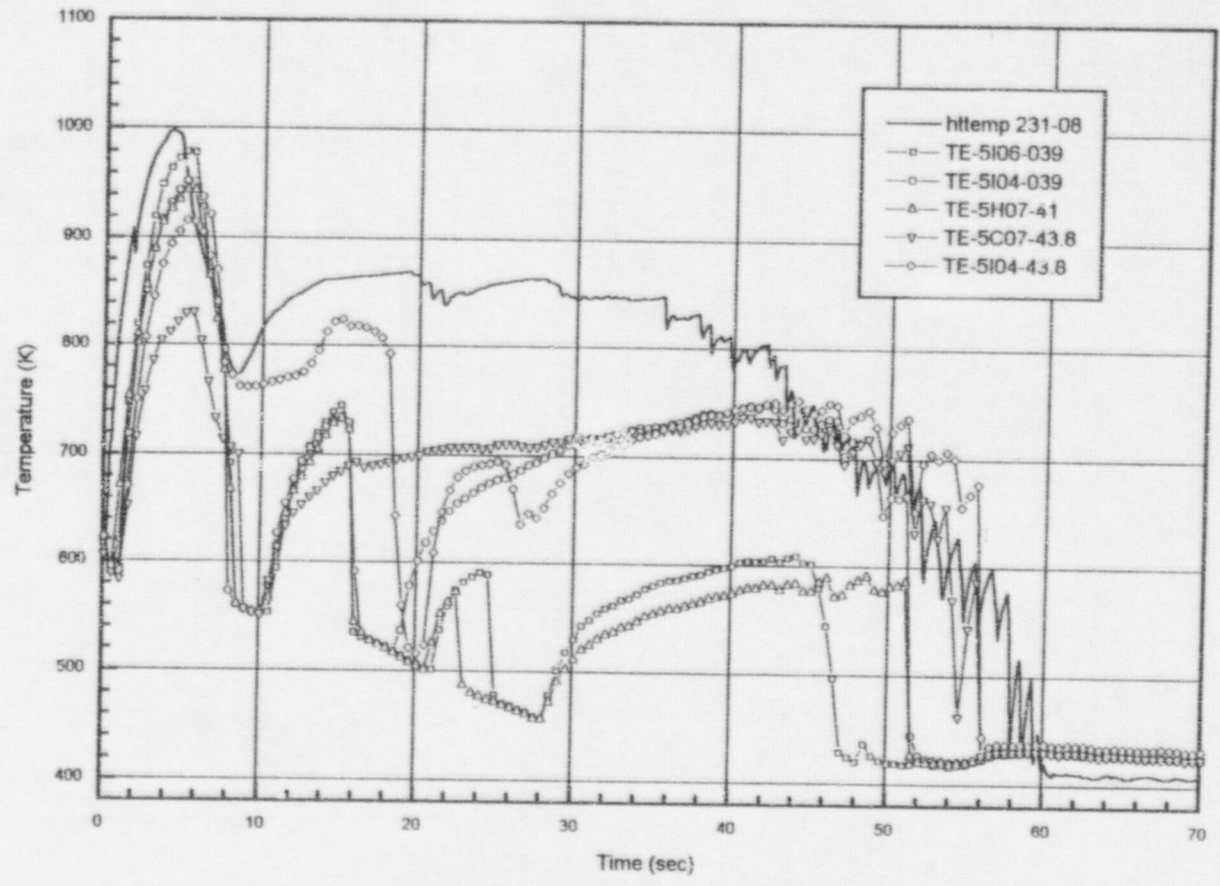


Figure 4.19 Cladding temperature at hot core node 8

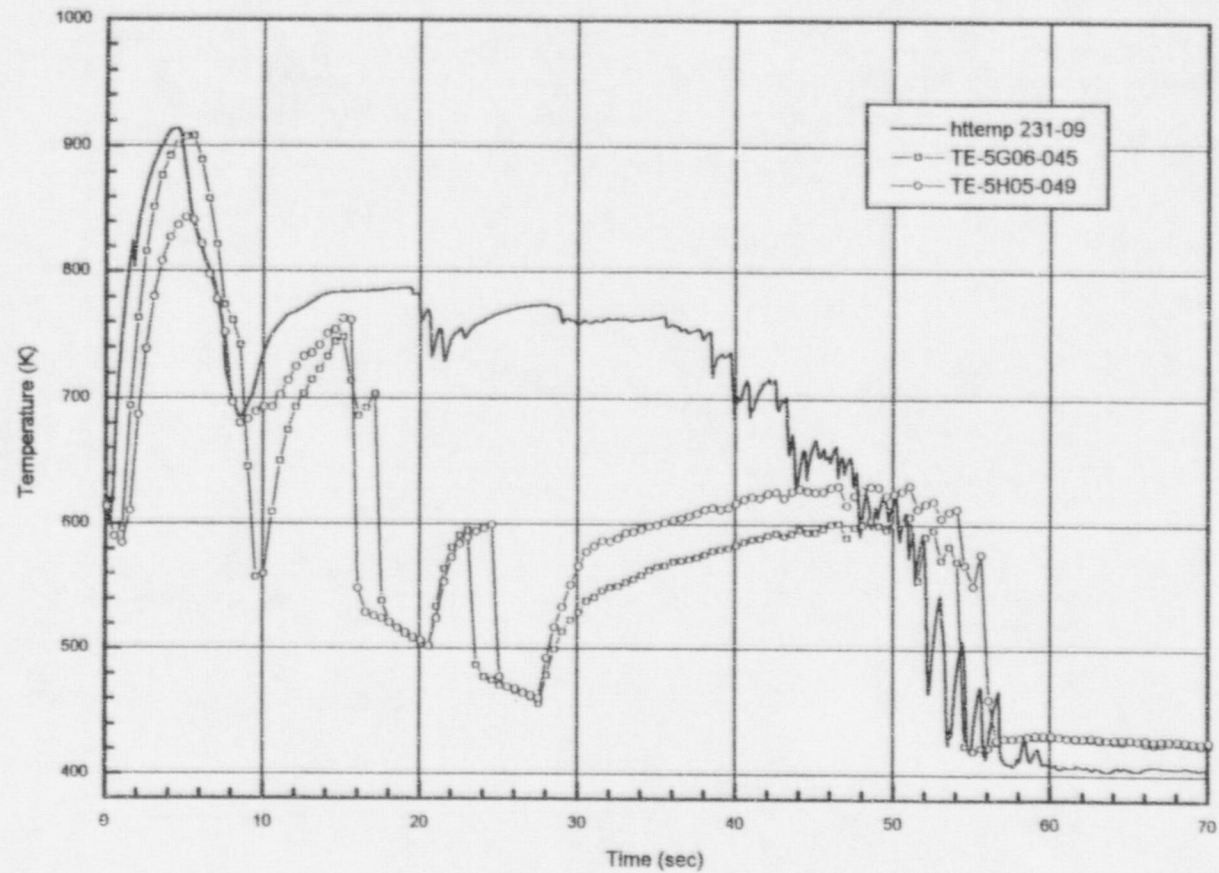


Figure 4.20 Cladding temperature at hot core node 9

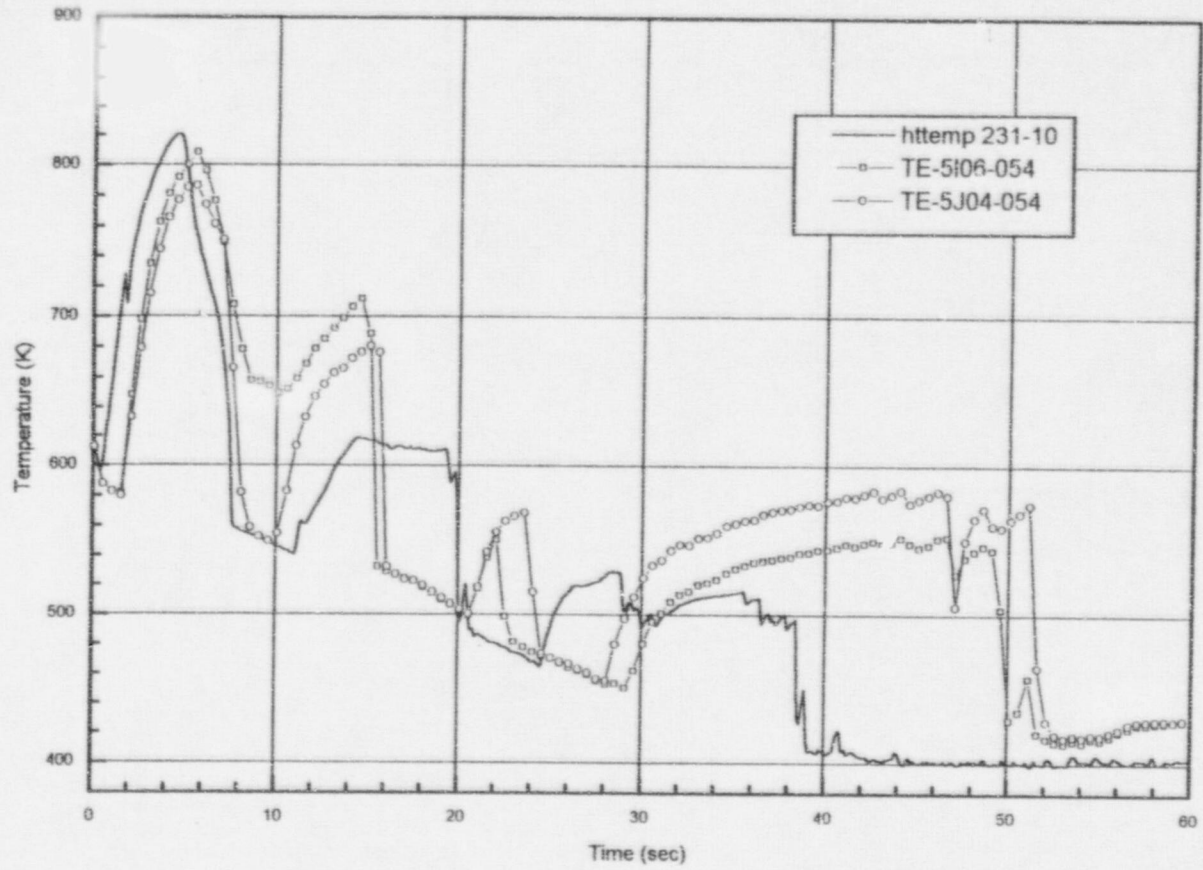


Figure 4.21 Cladding temperature at hot core node 10

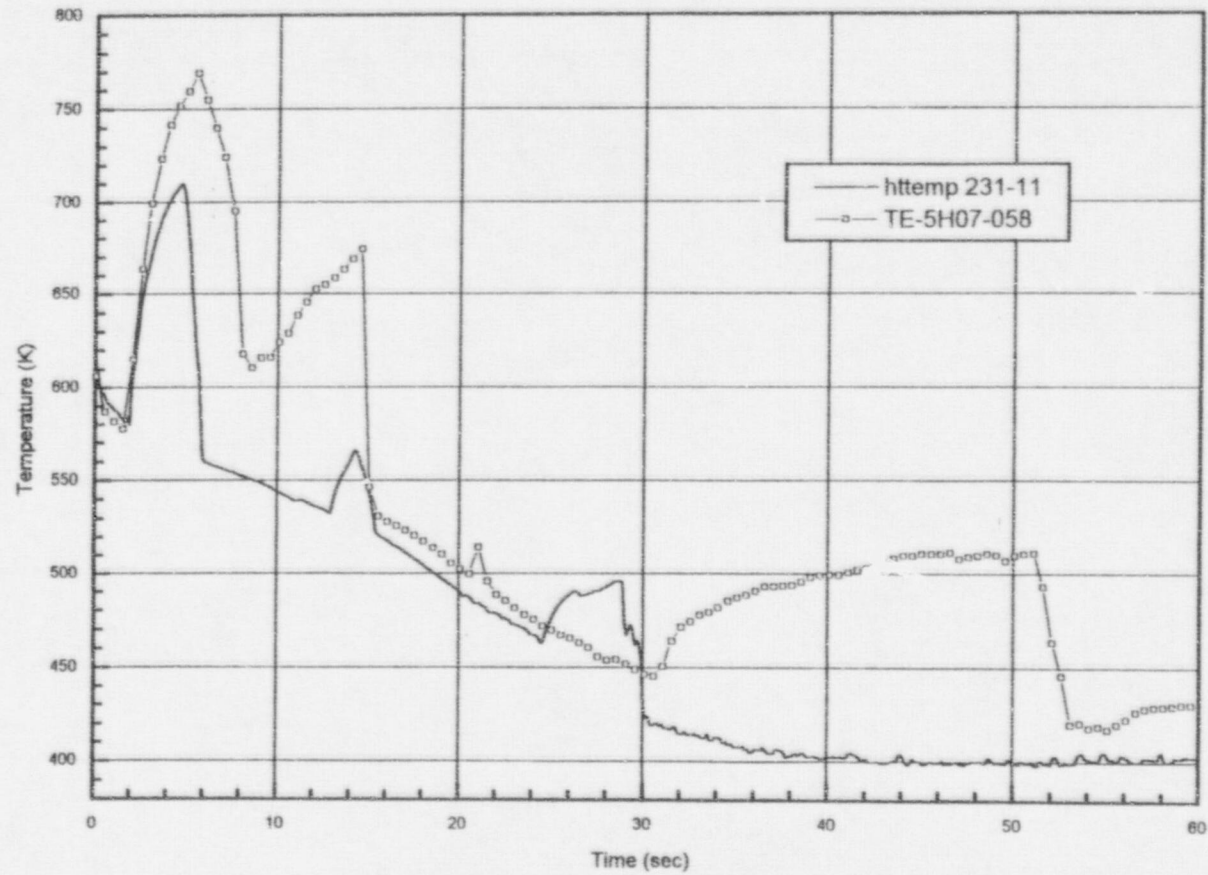


Figure 4.22 Cladding temperature at hot core node 11

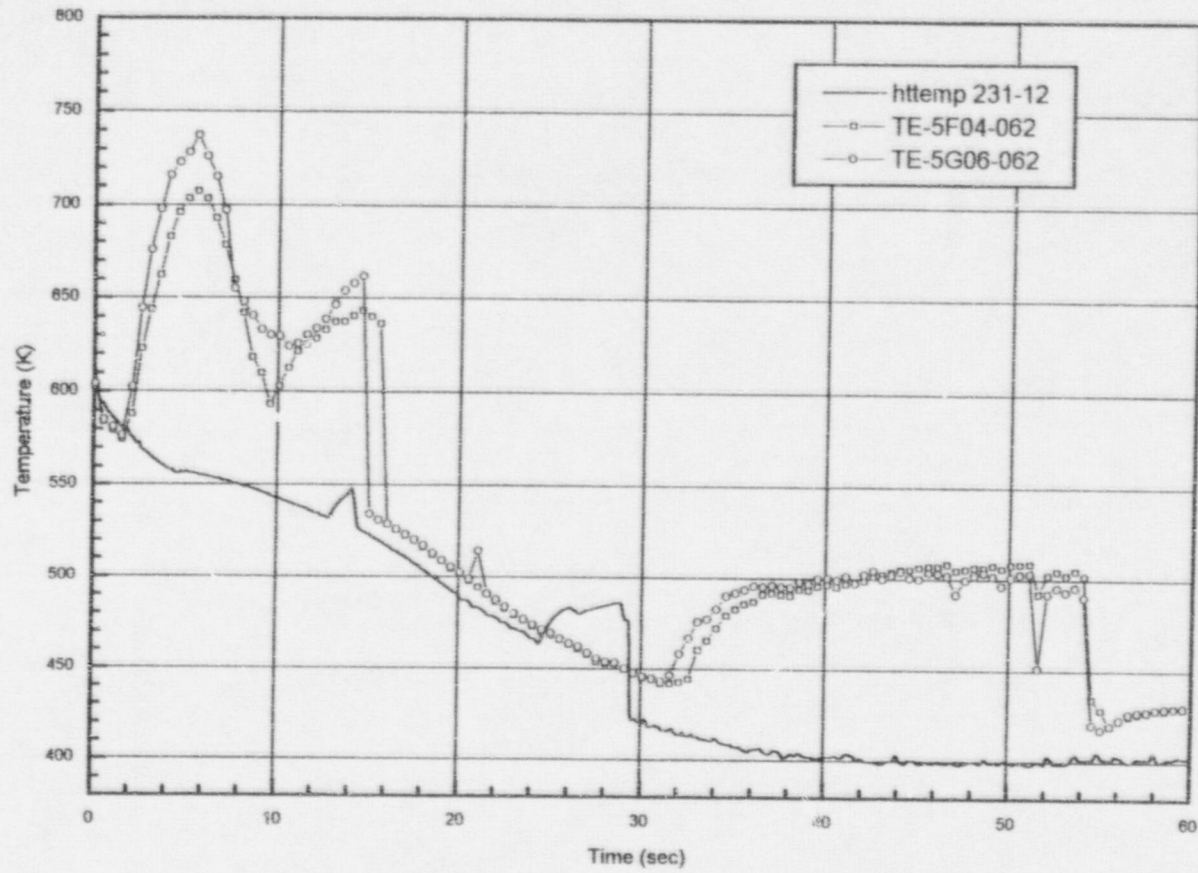


Figure 4.23 Cladding temperature at hot core node 12

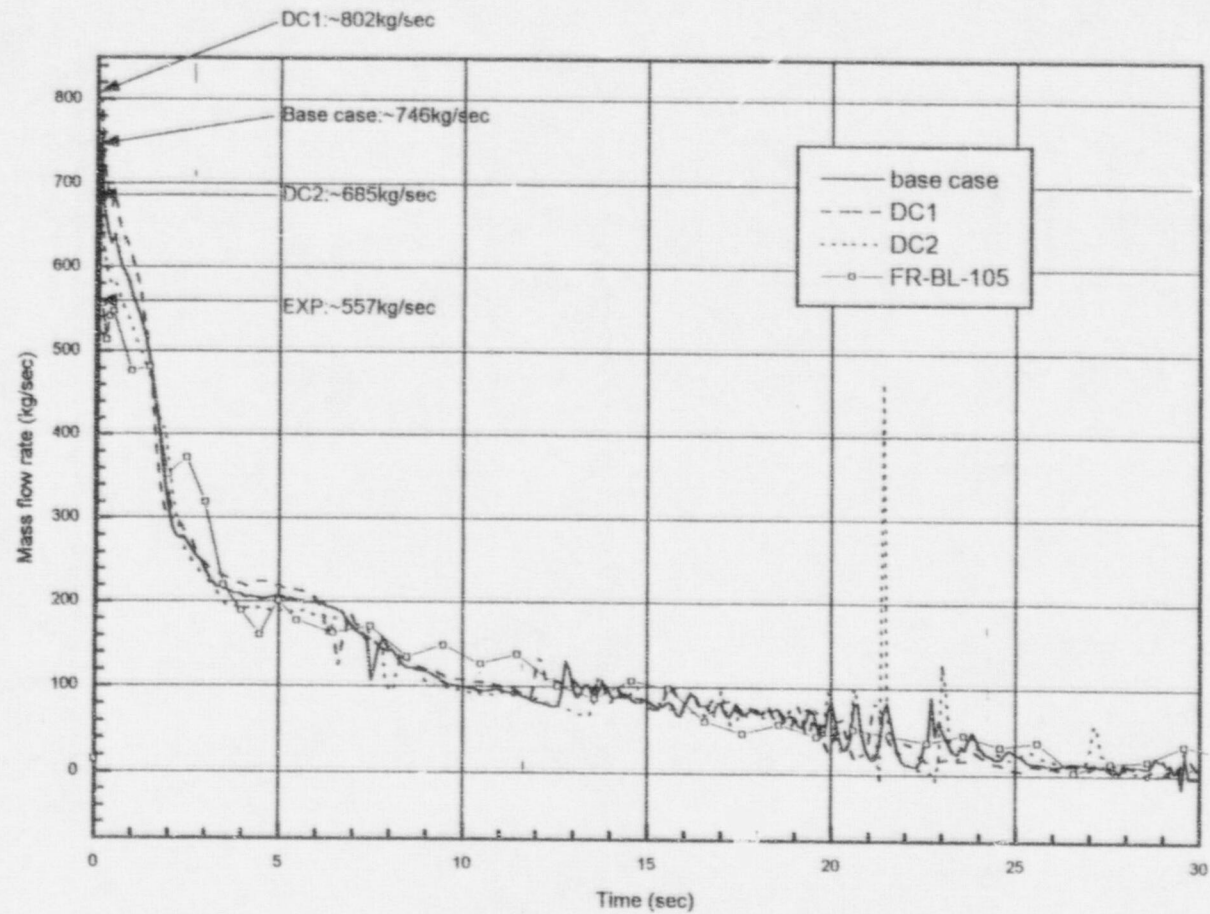


Figure 5.1 Mass flow rate in the broken loop cold leg with various discharge coefficients

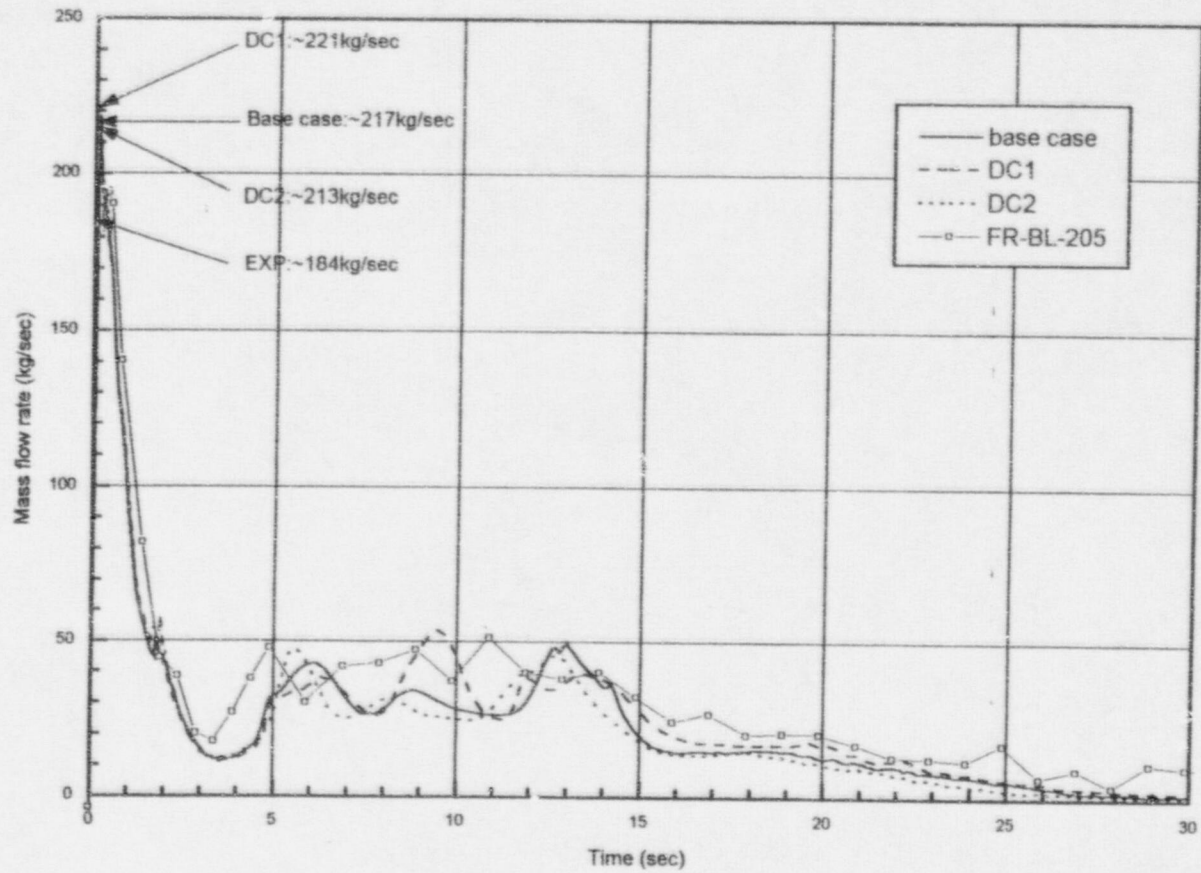


Figure 5.2 Mass flow rate in the broken loop hot leg with various discharge coefficients

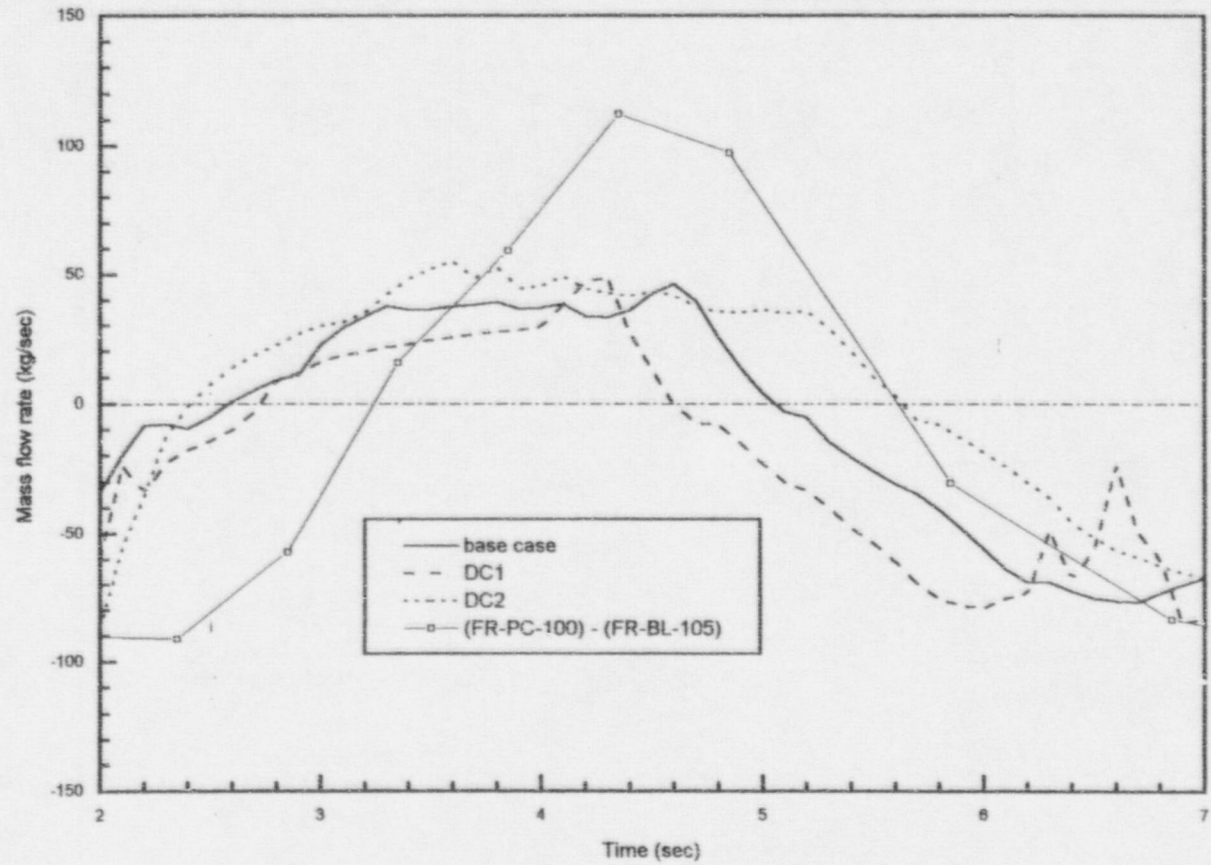


Figure 5.3 Mass flow difference between intact loop cold leg and broken loop cold leg

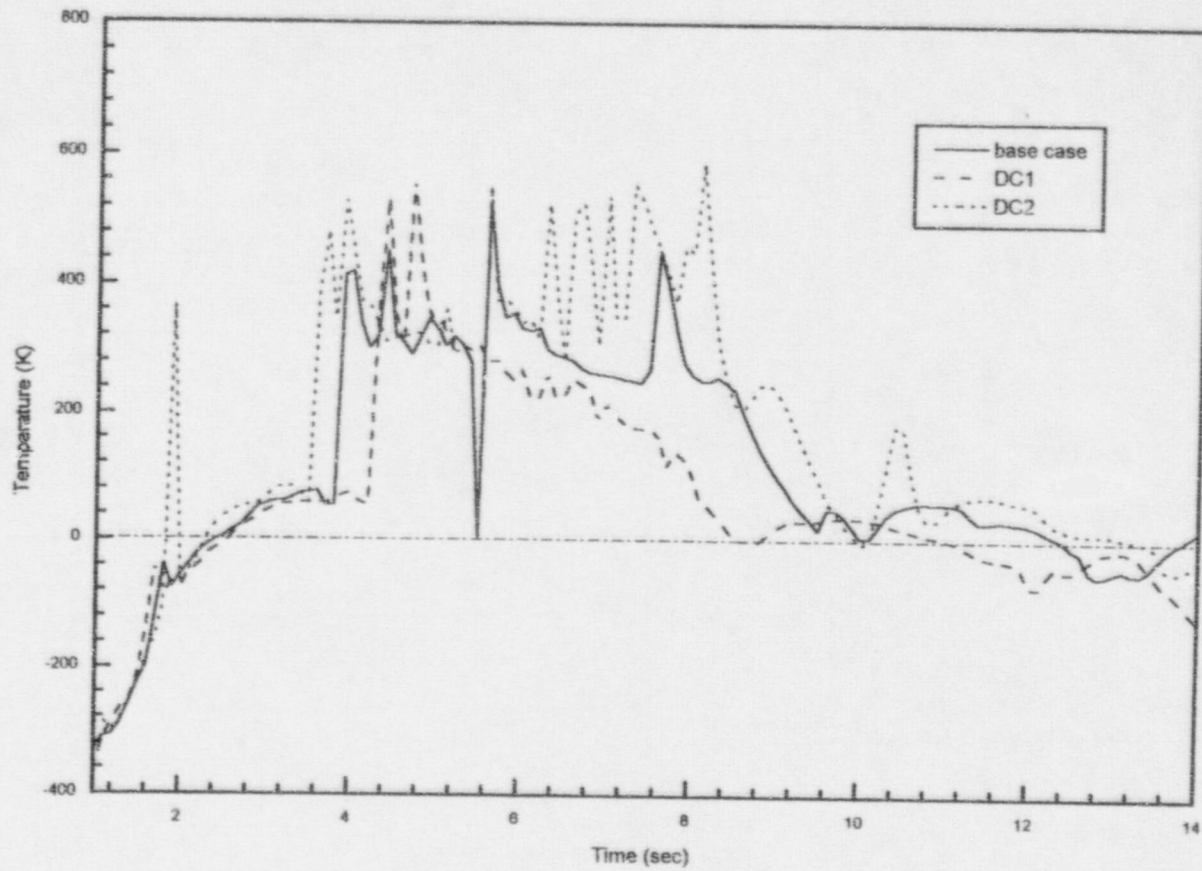


Figure 5.4 Mass flux at the core inlet junction with various discharge coefficients

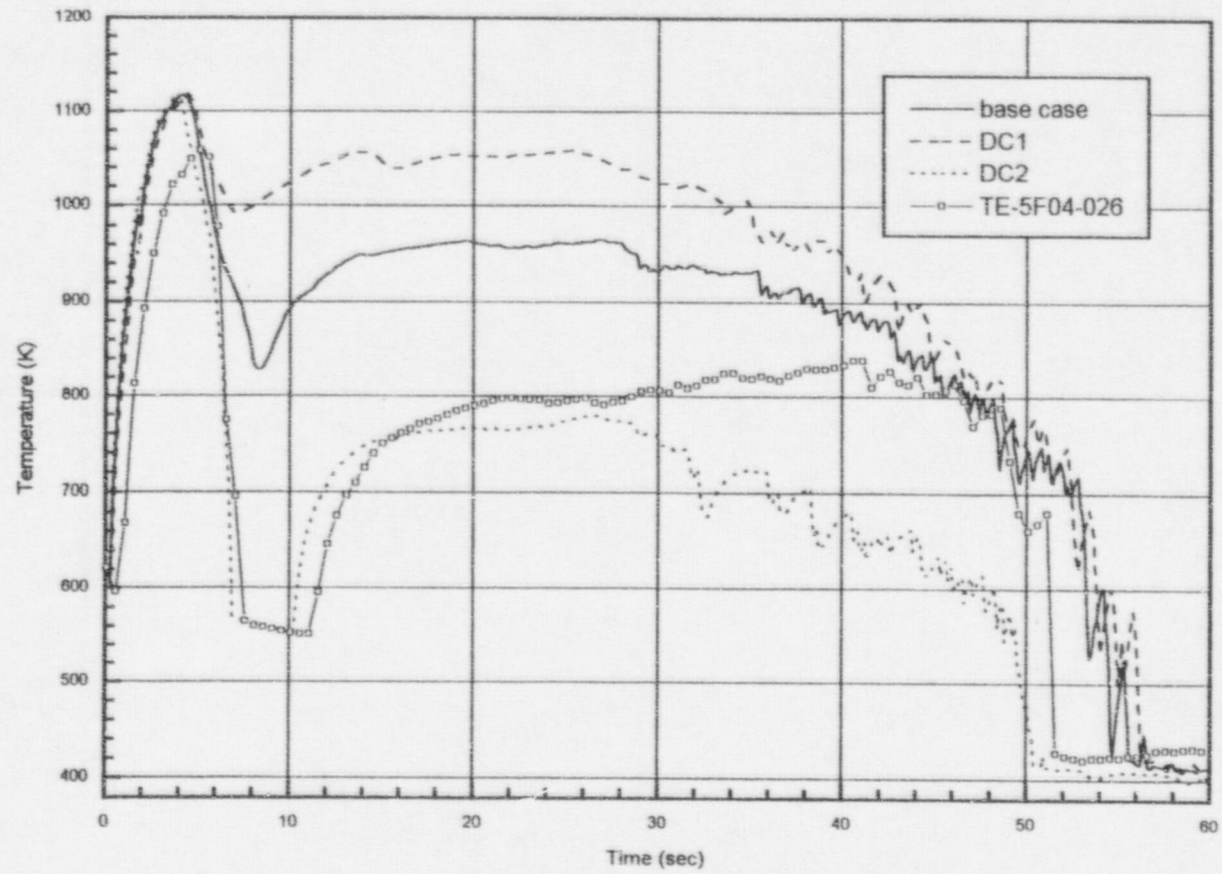


Figure 5.5 Cladding temperature at hot core node 5 with various discharge coefficients

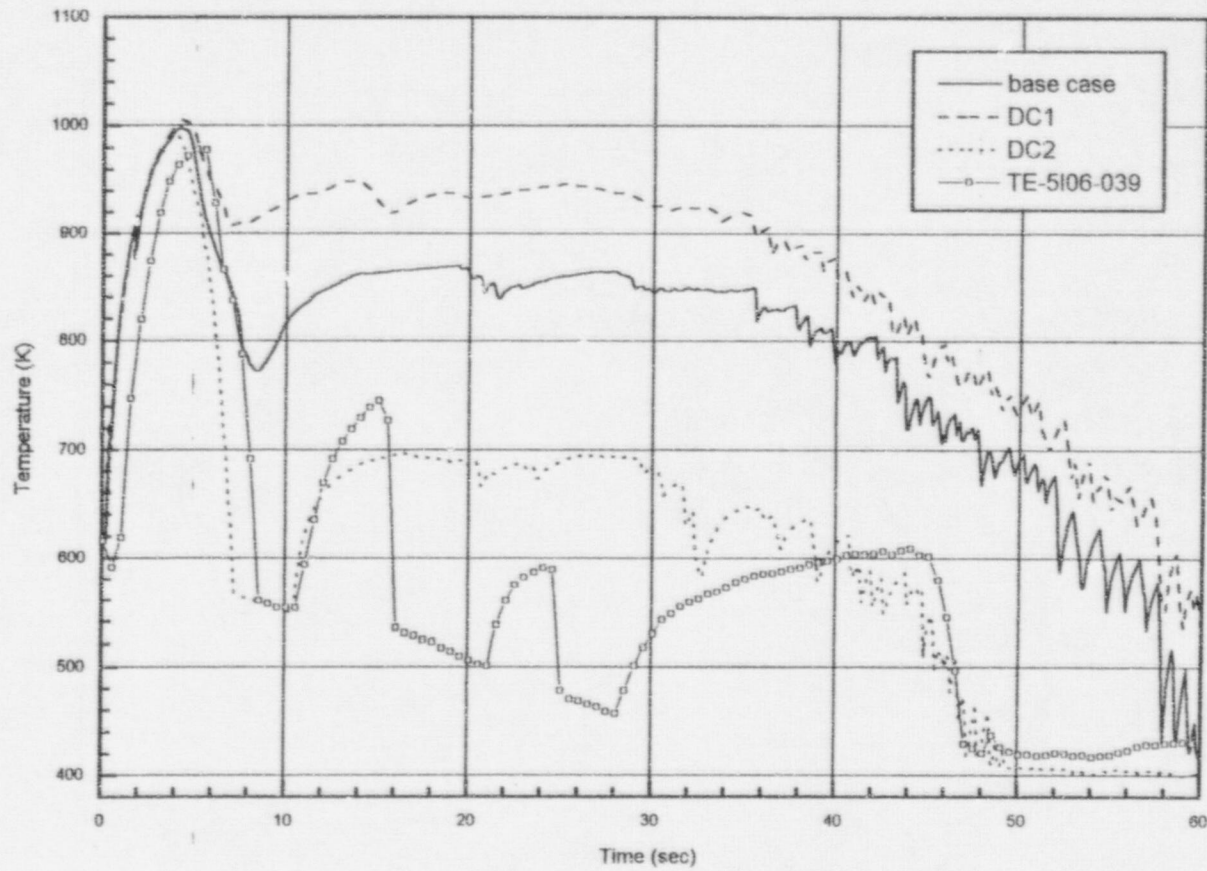


Figure 5.6 Cladding temperature at hot core node 8 with various discharge coefficients

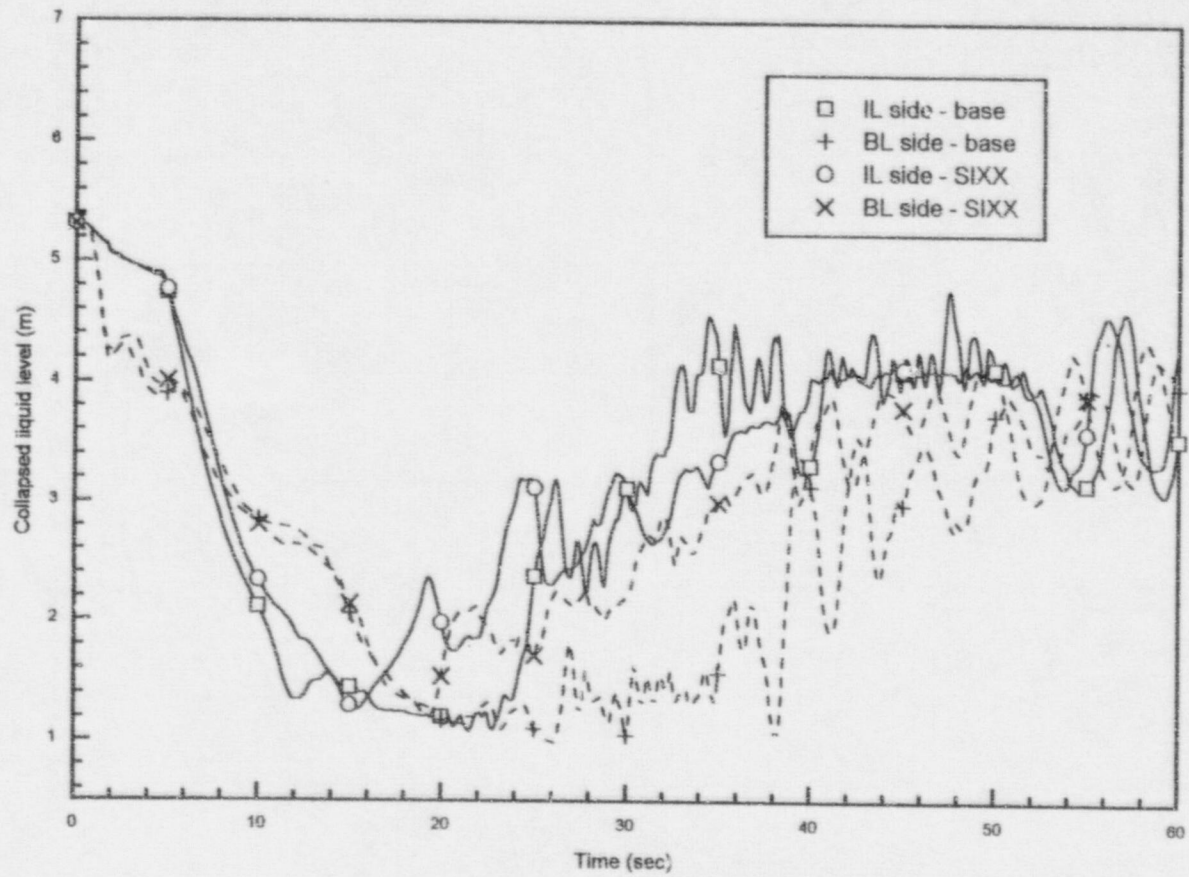


Figure 5.7 Collapsed liquid level in the downcomer from the base case and SIXX calculation

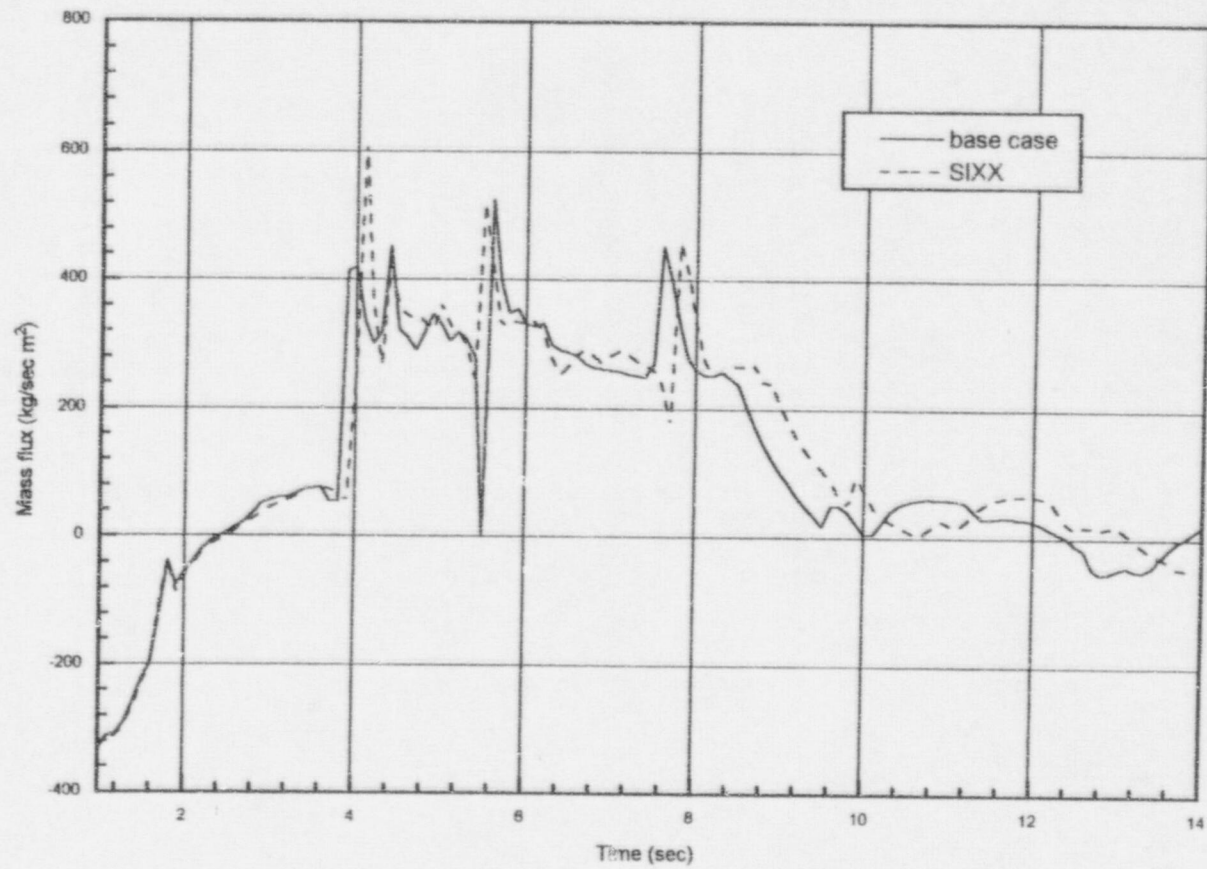


Figure 5.8 Mass flux at the inlet of core in the base case and SIXX calculation

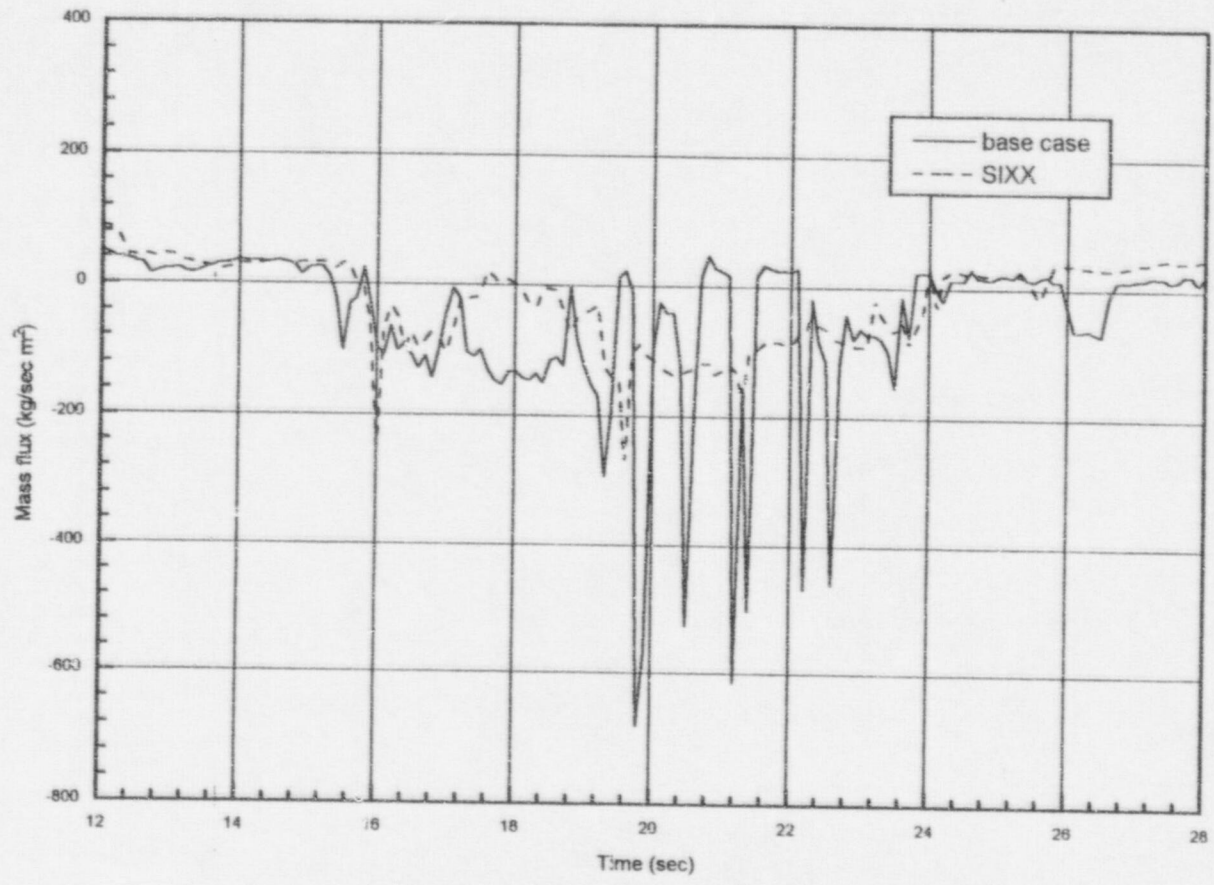


Figure 5.9 Mass flux at the outlet of core in the base case and SIXX calculation

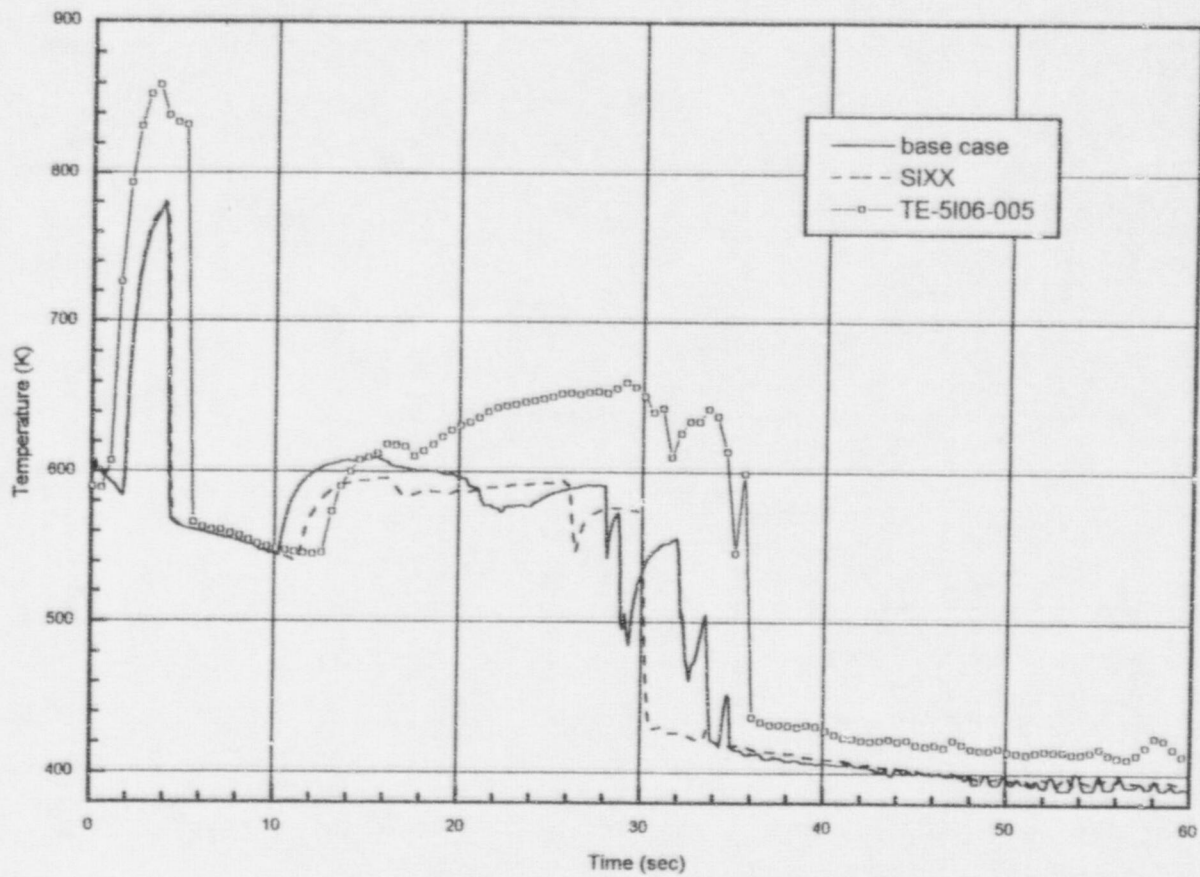


Figure 5.10 Calculated cladding temperature at hot core node 1 in the SIXX calculation

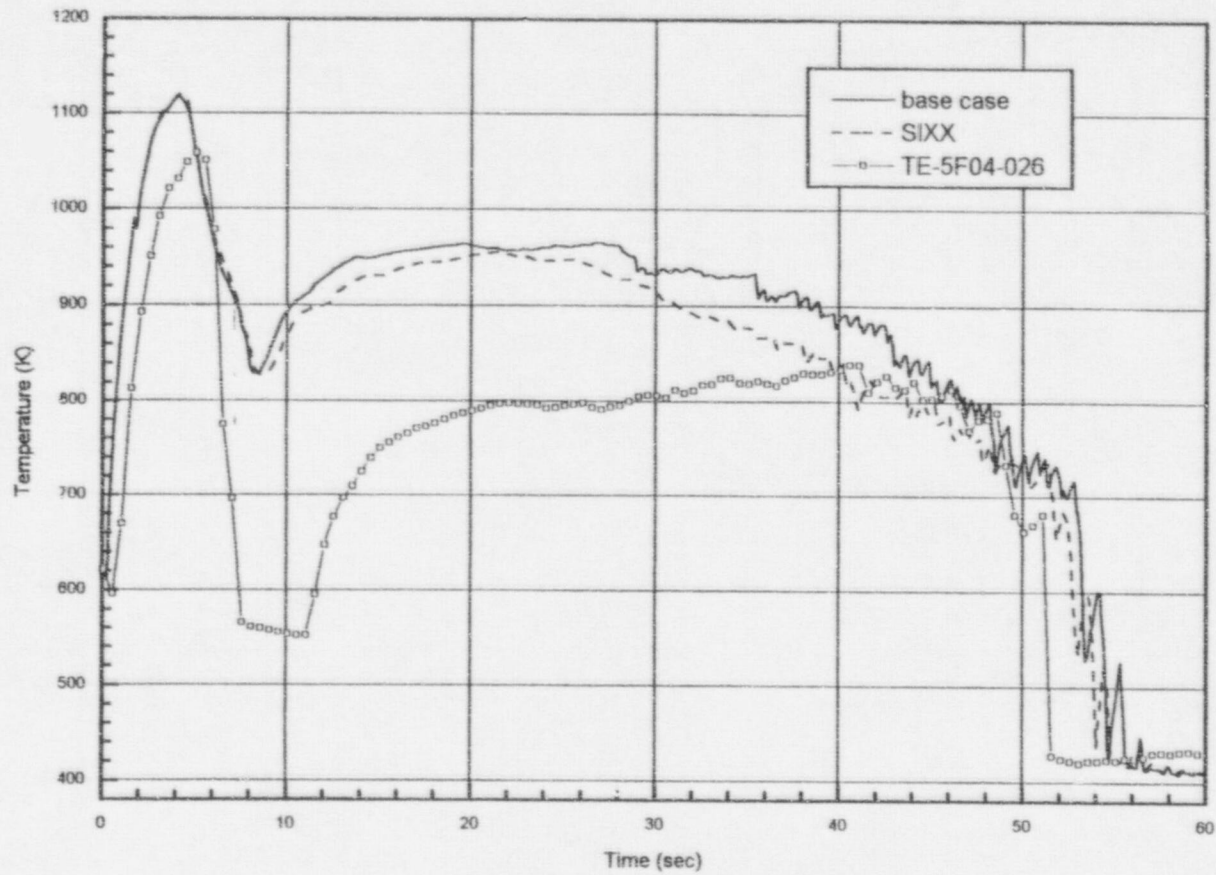


Figure 5.11 Cladding temperature at hot core node 5 in the SIXX calculation

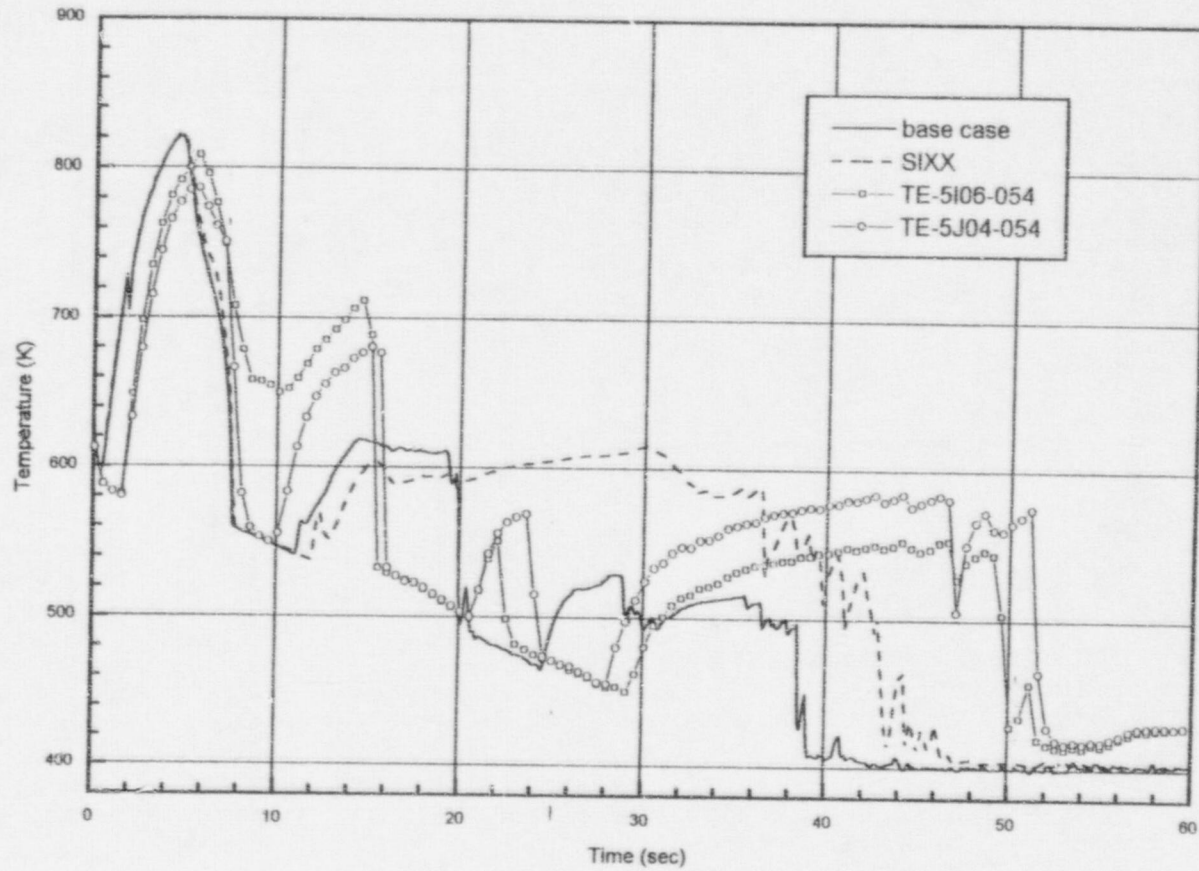


Figure 5.12 Cladding temperature at hot core node 10 in the SIXX calculation

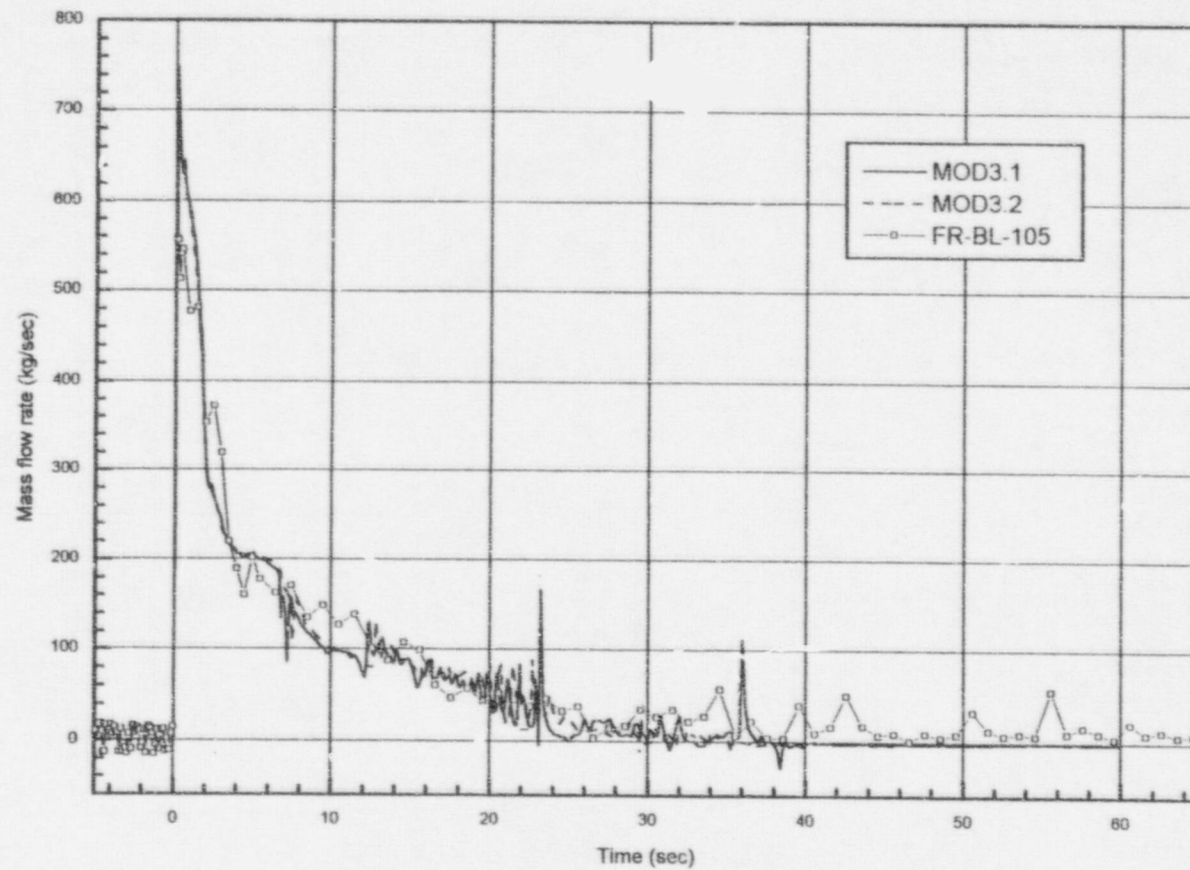


Figure 5.13 Mass flow rate in the broken loop cold leg by MOD3.1 and MOD3.2

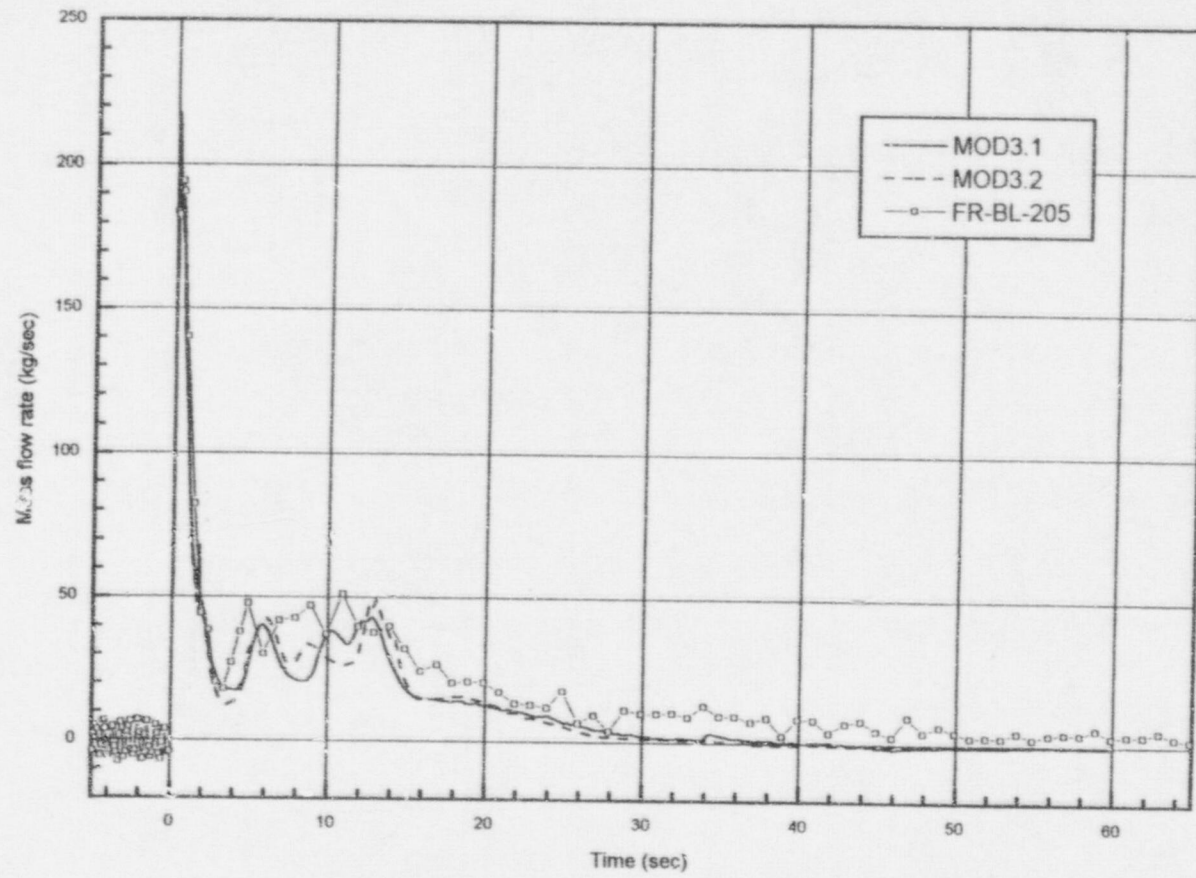


Figure 5.14 Mass flow rate in the broken loop hot leg by MOD3.1 and MOD3.2

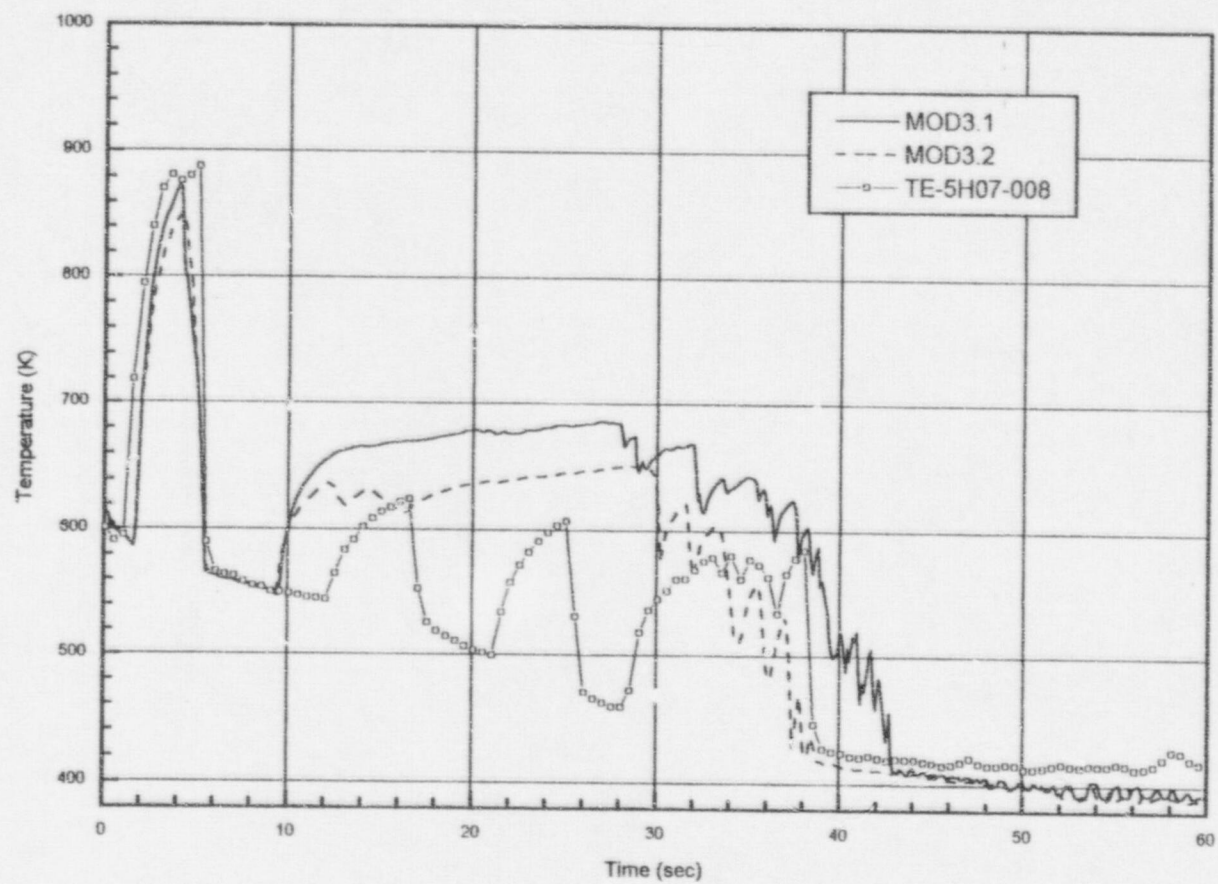


Figure 5.15 Cladding temperature at hot core node 2 by MOD3.1 and MOD3.2

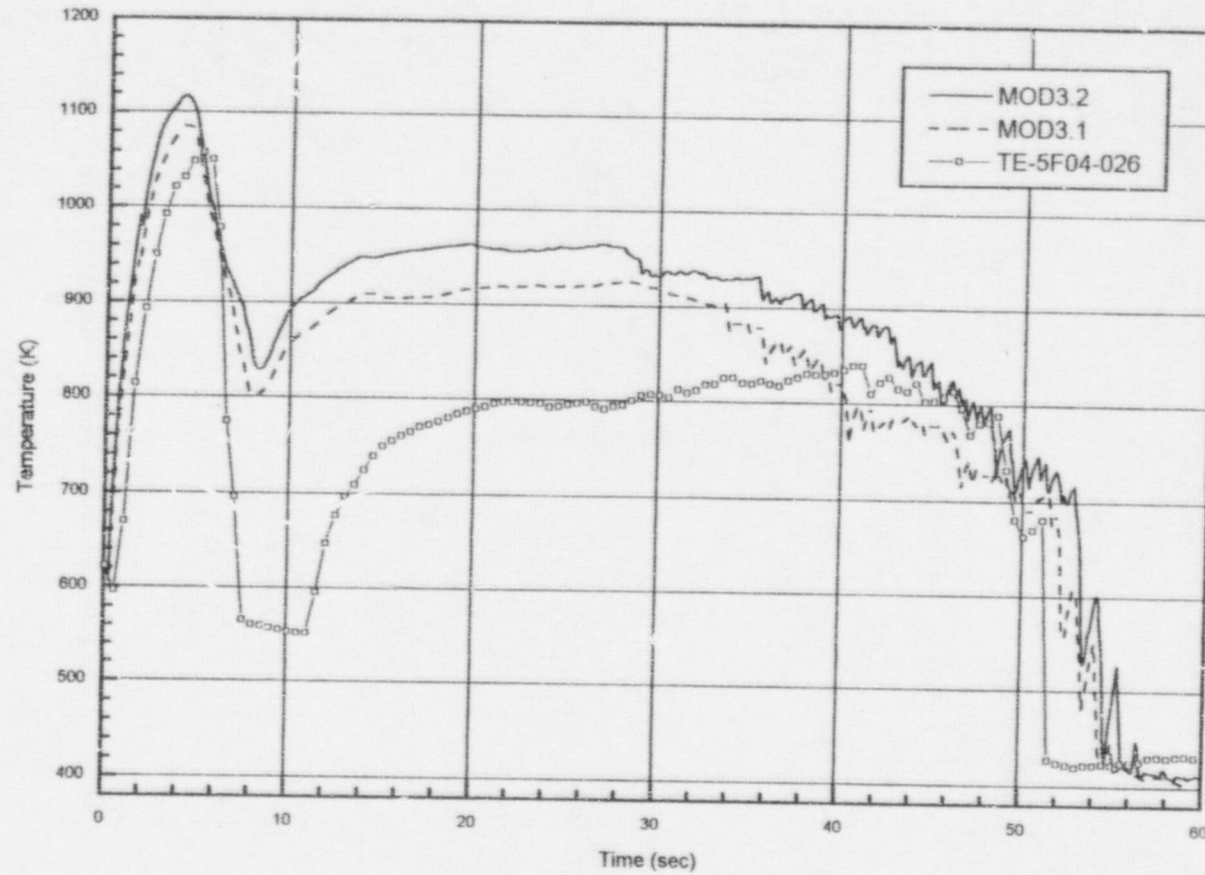


Figure 5.16 Cladding temperature at hot core node 5 by MOD3.1 and MOD3.2

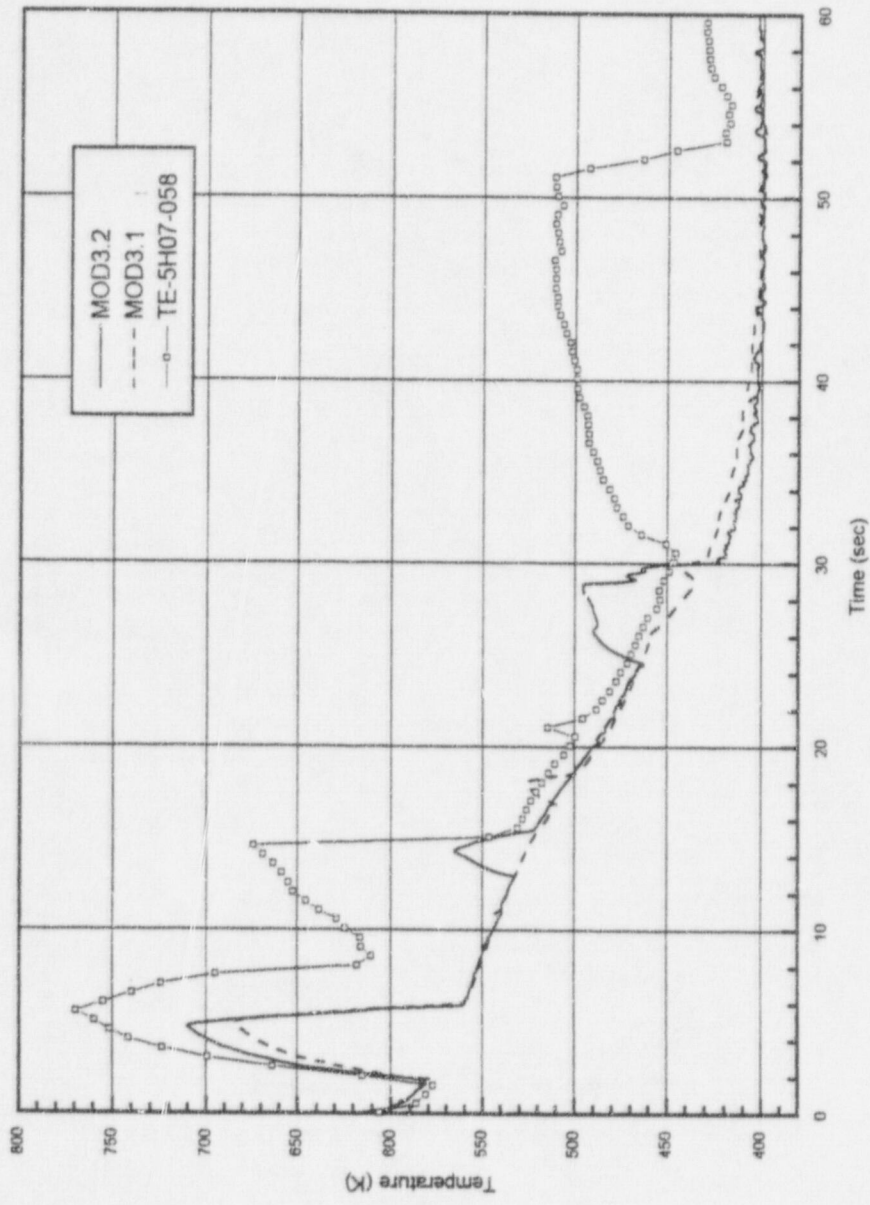


Figure 5.17 Cladding temperature at hot core node 11 by MOD3.1 and MOD3.2

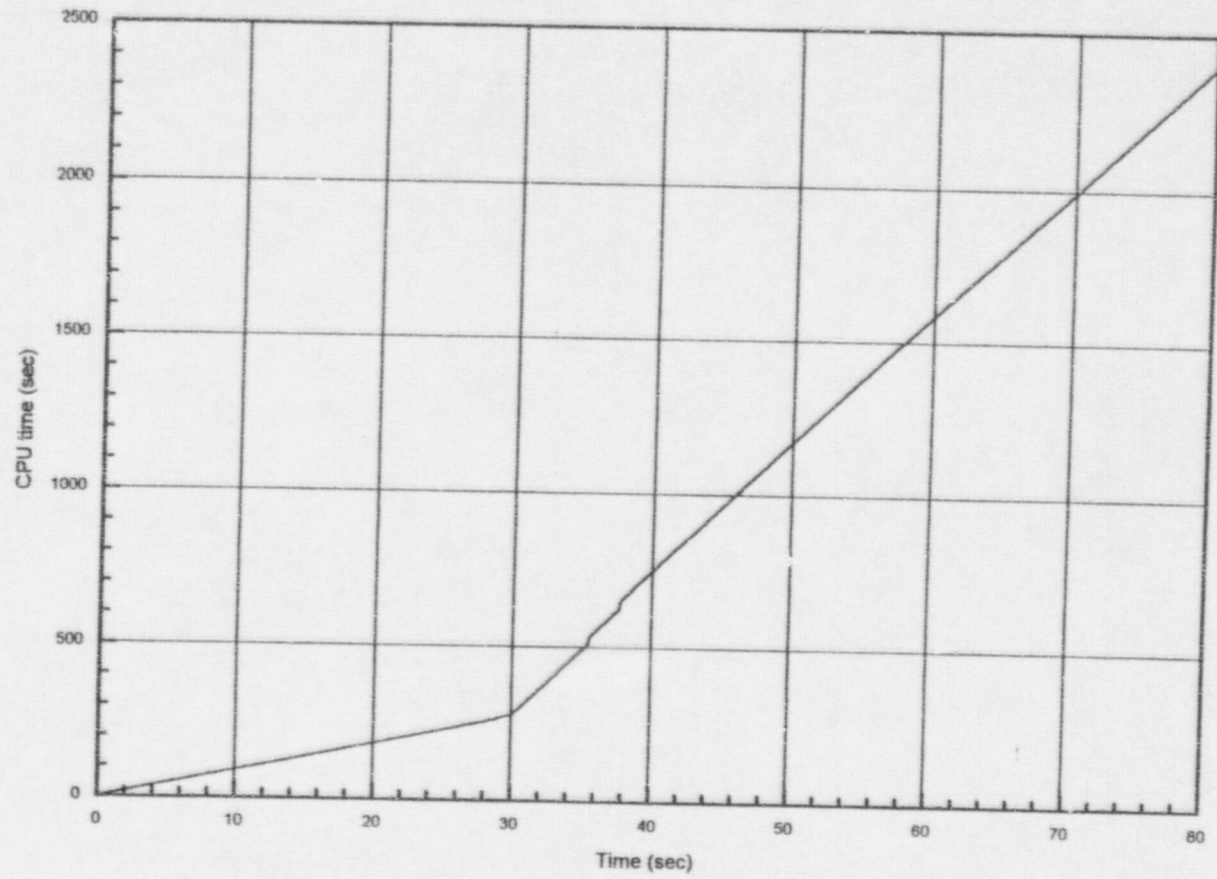


Figure 6.1 The required CPU time in the base case calculation

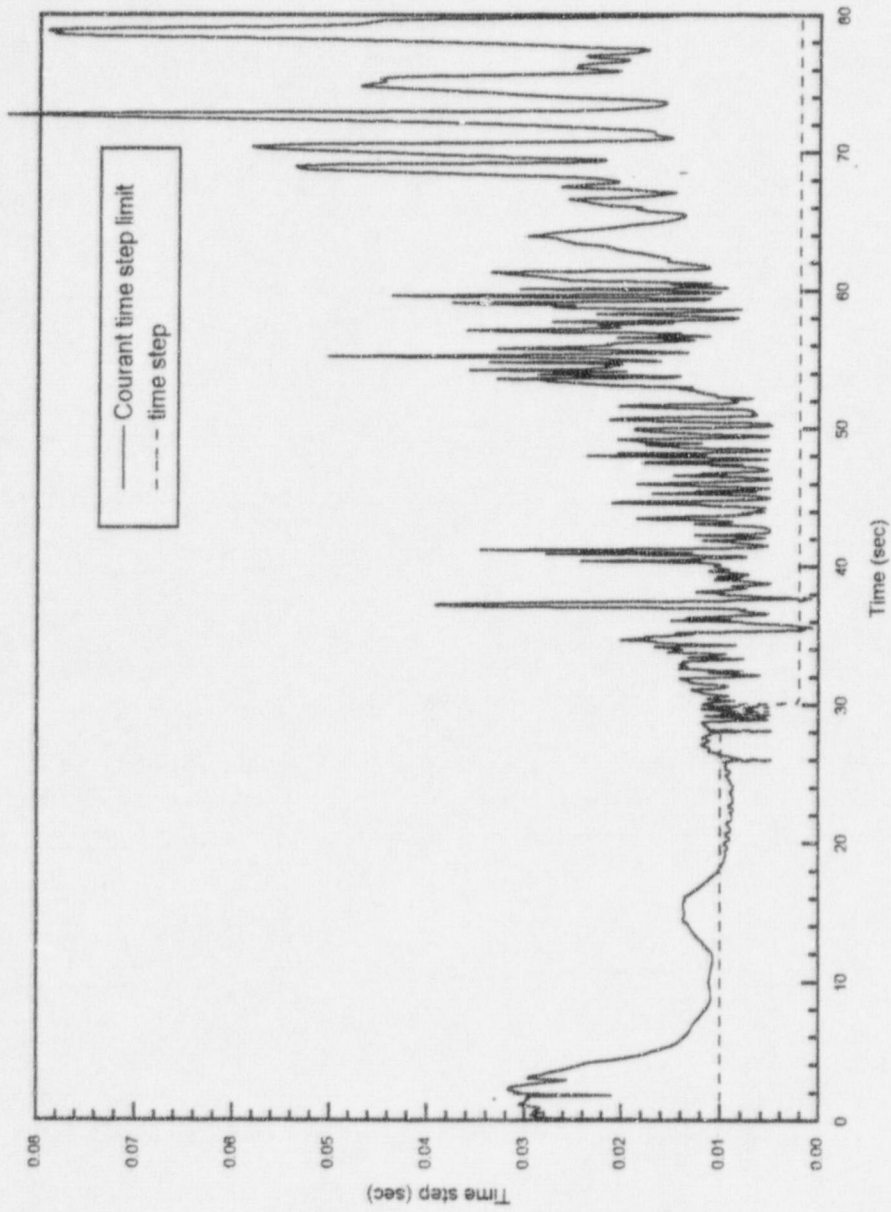


Figure 6.2 Time step size of base case calculation

APPENDIX : INPUT LISTING

| * pump suction piping | |
|----------------------------|--|
| 1180000 | pmpsucpp pipe |
| 1180601 | 3 |
| 1180101 | 0.0 3 |
| 1180201 | 0.0 2 |
| 1180301 | 0.546638 1 |
| 1180302 | 0.688596 2 |
| 1180303 | 0.558577 3 |
| 1180401 | 0.0445625 1 |
| 1180402 | 0.0445137 2 |
| 1180403 | 0.0354278 3 |
| 1180501 | 0.0 3 |
| 1180601 | -90.0 3 |
| 1180701 | -0.498052 1 |
| 1180702 | -0.688596 2 |
| 1180703 | -C.355604 3 |
| 1180801 | 4.-5 0.0 3 |
| 1180901 | 0.083 0.083 1 |
| 1180902 | 0.104 0.104 2 |
| 1181001 | 0.0000 3 |
| 1181101 | 0.0000 2 |
| 1181201 | 0 1.51001+7 1227210. 2457480. 0.0 0.0 1 |
| 1181202 | 0 1.50898+7 1227210. 2457490. 0.0 0.0 2 |
| 1181203 | 0 1.51020+7 1227210. 2457440. 0.0 0.0 3 |
| 1181300 | 0 |
| 1181301 | 5.0681000 5.3877000 0.0 1 |
| 1181302 | 5.1655000 5.4876000 0.0 2 |
| * pump suction tee | |
| 1200000 | pmpsuct branch |
| 1200001 | 3 0 |
| 1200101 | 0.0 0.759614 0.0487901 0.0 0.0 0.0 |
| 1200102 | 4.0-5 0.0 01000 |
| 1200200 | 0 1.51033+7 1227210. 2457410. 0.0 |
| 1201101 | 118010000 120000000 0.063427 0.0 0.0 0000 |
| 1202101 | 120010000 125000000 0.063427 1.075 1.25 0000 |
| 1203101 | 120010000 155000000 0.063427 1.075 1.25 0000 |
| 1201201 | 5.1654700 5.4874000 0.0 |
| 1202201 | 2.5827000 2.5827000 0.0 |
| 1203201 | 2.5826000 2.5826000 0.0 |
| * pump suction tee out let | |
| 1250000 | pmpisctt branch |
| 1250001 | 1 0 |
| 1250101 | 0.0 1.00308 0.0640548 0.0 90.0 0.520704 |
| 1250102 | 4.0-5 0.0 01000 |

| | |
|---------------------|--|
| 1150602 | -90.0 8 |
| 1150701 | 0.902 1 |
| 1150702 | 0.6096 3 |
| 1150703 | 0.299572 4 |
| 1150704 | -0.299572 5 |
| 1150705 | -0.6096 7 |
| 1150706 | -0.962 8 |
| 1150801 | 1.27-7 0.01022 8 |
| 1150901 | 0.0 0.0 7 |
| 1151001 | 01000 8 |
| 1151101 | 100000 7 |
| 1151201 | 0 1.51270+7 1372420. 2456830. 0.0 1 |
| 1151202 | 0 1.51192+7 1338080. 2457320. 0.0 2 |
| 1151203 | 0 1.51128+7 1309560. 2457180. 0.0 3 |
| 1151204 | 0 1.51077+7 1290670. 2457300. 0.0 4 |
| 1151205 | 0 1.51062+7 1274150. 2457340. 0.0 5 |
| 1151206 | 0 1.51077+7 1255880. 2457300. 0.0 6 |
| 1151207 | 0 1.51101+7 1240550. 2457240. 0.0 7 |
| 1151208 | 0 1.51132+7 1227210. 2451600. 0.0 8 |
| 1151300 | 0 |
| 1151301 | 2.3324000 2.5621000 0.0 1 |
| 1151302 | 2.2887000 2.5175000 0.0 2 |
| 1151303 | 2.2549000 2.4830000 0.0 3 |
| 1151304 | 2.2335000 2.4610000 0.0 4 |
| 1151305 | 2.2153000 2.4424000 0.0 5 |
| 1151306 | 2.1961000 2.4227000 0.0 6 |
| 1151307 | 2.1803000 2.4066000 0.0 7 |
| 1151401 | 0.01022 0.1 1 |
| 1151402 | 0.01022 0.1 2 |
| 1151403 | 0.01022 0.1 3 |
| 1151404 | 0.01022 0.1 4 |
| 1151405 | 0.01022 0.1 5 |
| 1151406 | 0.01022 0.1 6 |
| 1151407 | 0.01022 0.1 7 |
| * sg out let plenum | |
| 1160000 | sgoutpln branch |
| 1160001 | 2 0 |
| 1160101 | 0.0 0.629795 0.33532 0.0 -90.0 -0.512756 |
| 1160102 | 4.-5 0.0102 01000 |
| 1160200 | 0 1.51176+7 1227210. 2457160. 0.0 |
| 1161101 | 115010000 116000000 0.0 0.0 0100 |
| 1162101 | 116010000 118000000 0.0512 0.0 0.0 0.0 |
| 1161201 | 2.1672000 2.3880000 0.0 |
| 1162201 | 4.0188000 4.1687000 0.0 |
| 1161110 | 0.01022 0.1 1 |
| 1162110 | 0.0102 0.1 1 |

| | | | | | | | | | | |
|--|-----------|-----------|-----------|----------|-----------|------|--|--|---|--|
| 2020501 | 0.0 | 1 | | | | | | | | |
| 2020601 | -90.0 | 1 | | | | | | | | |
| 2020801 | 3.81-6 | 0.172 | 1 | | | | | | | |
| 2022301 | 3.81-6 | 0.172 | 1 | | | | | | | |
| 2021001 | 01000 | 1 | | | | | | | | |
| 2022701 | 00000 | 1 | | | | | | | | |
| 2021201 | 0 | 15201400. | 1227290. | 2455030. | 0.0 | 0.0 | | | 1 | |
| * junction - middle to lower inlet annulus intact side | | | | | | | | | | |
| 2050000 | inanmlin | sngljun | | | | | | | | |
| 2050101 | 202010000 | 210000000 | 0.0709408 | 0.0 | 0.0 | 0100 | | | | |
| 2050110 | 0.172 | 0.0 | 1.0 | 1.0 | | | | | | |
| 2050201 | 0 | 1.7724 | 1.8718 | 0.0 | | | | | | |
| * inlet annulus lower volume intact side | | | | | | | | | | |
| 2100000 | inanlwri | annulus | | | | | | | | |
| 2100001 | 4 | | | | | | | | | |
| 2100101 | 0.0710000 | 1 | | | | | | | | |
| 2101601 | 0.0258470 | 1 | | | | | | | | |
| 2101602 | 0.1550460 | 2 | | | | | | | | |
| 2101603 | 0.1286870 | 3 | | | | | | | | |
| 2101604 | 0.1100840 | 4 | | | | | | | | |
| 2100102 | 0.0 | 4 | | | | | | | | |
| 2100201 | 0.0709408 | 3 | | | | | | | | |
| 2100301 | 0.2534239 | 1 | | | | | | | | |
| 2100302 | 1.5200561 | 2 | | | | | | | | |
| 2100303 | 1.2616333 | 3 | | | | | | | | |
| 2100304 | 1.0792591 | 4 | | | | | | | | |
| 2101801 | 0.6961386 | 1 | | | | | | | | |
| 2101802 | 1.0202559 | 2 | | | | | | | | |
| 2101803 | 0.9457054 | 3 | | | | | | | | |
| 2101804 | 0.8964118 | 4 | | | | | | | | |
| 2100401 | 0.0 | 1 | | | | | | | | |
| 2100402 | 0.1581866 | 2 | | | | | | | | |
| 2100403 | 0.1217000 | 3 | | | | | | | | |
| 2100404 | 0.0986806 | 4 | | | | | | | | |
| 2100501 | 0.0 | 4 | | | | | | | | |
| 2100601 | -90.0 | 4 | | | | | | | | |
| 2100801 | 3.81-6 | 0.102 | 4 | | | | | | | |
| 2102301 | 3.81-6 | 0.102 | 4 | | | | | | | |
| 2100901 | 0.0 | 0.0 | 3 | | | | | | | |
| 2101001 | 01000 | 4 | | | | | | | | |
| 2102701 | 00000 | 4 | | | | | | | | |
| 2101101 | 100100 | 3 | | | | | | | | |
| 2101201 | 0 | 15201400. | 1227290. | 2455030. | .00000000 | 0.0 | | | 1 | |
| 2101202 | 0 | 15204900. | 1227290. | 2454940. | .00000000 | 0.0 | | | 2 | |
| 2101203 | 0 | 15213600. | 1227290. | 2454730. | .00000000 | 0.0 | | | 3 | |

| | | | | | | | | | | |
|---|-----------|-----------|-----------|----------|-----------|------------|--|--|--|---|
| 2101204 | 0 | 15221100. | 1227290. | 2454550. | .00000000 | 0.0 | | | | 4 |
| 2101300 | 0 | | | | | | | | | |
| 2101301 | 3.2693 | 3.5236 | 0.0 | 1 | | | | | | |
| 2101302 | 3.2693 | 3.5236 | 0.0 | 2 | | | | | | |
| 2101303 | 3.2692 | 3.5234 | 0.0 | 3 | | | | | | |
| 2101401 | 0.102 | 0.0 | 1.0 | 1.0 | 1 | | | | | |
| 2101402 | 0.102 | 0.0 | 1.0 | 1.0 | 2 | | | | | |
| 2101403 | 0.102 | 0.0 | 1.0 | 1.0 | 3 | | | | | |
| * junction - inlet annulus to downcomer intact side | | | | | | | | | | |
| 2150000 | inan2dci | sngljun | | | | | | | | |
| 2150101 | 210010000 | 222000000 | 0.0709408 | 0.0000 | 0.0000 | 100100 | | | | |
| 2150110 | 0.102 | 0.0 | 1.0 | 1.0 | | | | | | |
| 2150201 | 0 | 2.5365 | 5.1650 | 0.0 | | | | | | |
| * lower plenum top volume | | | | | | | | | | |
| 2220000 | lwrpiti | branch | | | | | | | | |
| 2220001 | 2 | | | | | | | | | |
| 2220101 | 0. | 0.3533183 | 0.2592277 | 0. | -90. | -0.3533183 | | | | |
| 2220102 | 3.81-6 | 0.0 | 01000 | | | | | | | |
| 2220200 | 0 | 1.52253+7 | 1227290. | 2454450. | 0.0 | | | | | |
| 2221101 | 222010000 | 220000000 | 0.0 | 0.005 | 0.005 | 0000 | | | | |
| 2222101 | 222000000 | 225000000 | 0.1499 | 1.5 | 1.5 | 0000 | | | | |
| 2221201 | 7.17715-7 | 7.17715-7 | 0. | | | | | | | |
| 2222201 | 2.1854000 | 2.4112000 | 0. | | | | | | | |
| * lower plenum bottom volume | | | | | | | | | | |
| 2200000 | lowplbv | snglvol | | | | | | | | |
| 2200101 | 0. | 0.3741720 | 0.29656 | 0.0 | -90. | -0.3741720 | | | | |
| 2200102 | 0. | 0.0 | 01000 | | | | | | | |
| 2200200 | 0 | 1.51655+7 | 1408220. | 2455830. | 0.0 | | | | | |
| * lower core support structure | | | | | | | | | | |
| 2250000 | lcoresup | branch | | | | | | | | |
| 2250001 | 3 | 0 | | | | | | | | |
| 2250101 | 0.2832456 | 0.5709989 | 0.0 | 0.0 | 90.0 | 0.5709989 | | | | |
| 2250102 | 3.81-6 | 0.095 | 01000 | | | | | | | |
| 2250200 | 0 | 1.50018+7 | 1230920. | 2459750. | 0.0 | | | | | |
| 2251101 | 225010000 | 230000000 | 9.4301-2 | 1.5 | 1.5 | 0000 | | | | |
| 2252101 | 225010000 | 231000000 | 1.9099-2 | 1.5 | 1.5 | 0000 | | | | |
| 2253101 | 225010000 | 235000000 | 0.0 | 12. | 12. | 0000 | | | | |
| 2251201 | 0.5923840 | 0.5923840 | 0.0 | | | | | | | |
| 2252201 | 1.5174900 | 1.5174900 | 0.0 | | | | | | | |
| 2253201 | 0.3590500 | 0.3590500 | 0.0 | | | | | | | |
| 2251110 | 0.095 | 0. | 1. | 1. | | | | | | |

| | | | | | | | | | |
|------------------------------|-----------|-----------|----------|----------|-----------|-----|----|--|--|
| 2252110 | 0.095 | 0. | 1. | 1. | | | | | |
| 2253110 | 0.095 | 0. | 1. | 1. | | | | | |
| * active core (average core) | | | | | | | | | |
| 2300000 | avgcore | pipe | | | | | | | |
| 2300001 | 12 | | | | | | | | |
| 2300101 | 0.152397 | 2 | | | | | | | |
| 2300102 | 0.142439 | 4 | | | | | | | |
| 2300103 | 0.143852 | 6 | | | | | | | |
| 2300104 | 0.142604 | 8 | | | | | | | |
| 2300105 | 0.142578 | 10 | | | | | | | |
| 2300106 | 0.147386 | 12 | | | | | | | |
| 2300201 | 0.141784 | 3 | | | | | | | |
| 2300202 | 0.119747 | 4 | | | | | | | |
| 2300203 | 0.141784 | 7 | | | | | | | |
| 2300204 | 0.119747 | 8 | | | | | | | |
| 2300205 | 0.141784 | 11 | | | | | | | |
| 2300301 | 0.1397017 | 12 | | | | | | | |
| 2300401 | 0.0 | 12 | | | | | | | |
| 2300501 | 0.0 | 12 | | | | | | | |
| 2300601 | 90.0 | 12 | | | | | | | |
| 2300801 | 1.27-7 | 0.012 | 12 | | | | | | |
| 2300901 | 0.0 | 0.0 | 3 | | | | | | |
| 2300902 | 0.66 | 0.66 | 4 | | | | | | |
| 2300903 | 0.0 | 0.0 | 7 | | | | | | |
| 2300904 | 0.66 | 0.66 | 8 | | | | | | |
| 2300905 | 0.0 | 0.0 | 11 | | | | | | |
| 2301001 | 01000 | 12 | | | | | | | |
| 2301101 | 0000 | 11 | | | | | | | |
| 2301201 | 0 | 15048500. | 1263450. | 2459550. | .00000000 | 0.0 | 02 | | |
| 2301202 | 0 | 15045400. | 1309480. | 2459550. | .00000000 | 0.0 | 04 | | |
| 2301203 | 0 | 15042500. | 1357660. | 2459550. | .00000000 | 0.0 | 05 | | |
| 2301204 | 0 | 15040100. | 1394080. | 2459550. | .00000000 | 0.0 | 06 | | |
| 2301205 | 0 | 15037200. | 1417170. | 2459550. | .00000000 | 0.0 | 10 | | |
| 2301206 | 0 | 15034300. | 1424460. | 2459550. | .00000000 | 0.0 | 12 | | |
| 2301300 | 0 | | | | | | | | |
| 2301301 | 1.4679000 | 1.4679000 | 0.0 | 02 | | | | | |
| 2301302 | 1.7789000 | 1.7789000 | 0.0 | 04 | | | | | |
| 2301303 | 1.5425000 | 1.5425000 | 0.0 | 06 | | | | | |
| 2301304 | 1.8668000 | 1.8668000 | 0.0 | 08 | | | | | |
| 2301305 | 1.5994000 | 1.5994000 | 0.0 | 11 | | | | | |
| 2301401 | 0.012 | 0. | 1. | 1. | 1 | | | | |
| 2301402 | 0.012 | 0. | 1. | 1. | 2 | | | | |
| 2301403 | 0.012 | 0. | 1. | 1. | 3 | | | | |
| 2301404 | 0.012 | 0. | 1. | 1. | 4 | | | | |
| 2301405 | 0.012 | 0. | 1. | 1. | 5 | | | | |
| 2301406 | 0.012 | 0. | 1. | 1. | 6 | | | | |
| 2301407 | 0.012 | 0. | 1. | 1. | 7 | | | | |

| | | | | | | | | | |
|---------------------|-----------|-----------|----------|----------|-----------|-----|----|--|--|
| 2301408 | 0.012 | 0. | 1. | 1. | 8 | | | | |
| 2301409 | 0.012 | 0. | 1. | 1. | 9 | | | | |
| 2301410 | 0.012 | 0. | 1. | 1. | 10 | | | | |
| 2301411 | 0.012 | 0. | 1. | 1. | 11 | | | | |
| * active core (hot) | | | | | | | | | |
| 2310000 | hotcore | pipe | | | | | | | |
| 2310001 | 12 | | | | | | | | |
| 2310101 | 3.08652-2 | 2 | | | | | | | |
| 2310102 | 2.88483-2 | 4 | | | | | | | |
| 2310103 | 2.91345-2 | 6 | | | | | | | |
| 2310104 | 2.88819-2 | 8 | | | | | | | |
| 2310105 | 2.88766-2 | 10 | | | | | | | |
| 2310106 | 2.98503-2 | 12 | | | | | | | |
| 2310201 | 2.87158-2 | 3 | | | | | | | |
| 2310202 | 2.42526-2 | 4 | | | | | | | |
| 2310203 | 2.87158-2 | 7 | | | | | | | |
| 2310204 | 2.42526-2 | 8 | | | | | | | |
| 2310205 | 2.87158-2 | 11 | | | | | | | |
| 2310301 | 0.1397017 | 12 | | | | | | | |
| 2310401 | 0 | 12 | | | | | | | |
| 2310501 | 0.0 | 12 | | | | | | | |
| 2310601 | 90.0 | 12 | | | | | | | |
| 2310801 | 1.27-7 | 0.012 | 12 | | | | | | |
| 2310901 | 0.0 | 0.0 | 3 | | | | | | |
| 2310902 | 0.66 | 0.66 | 4 | | | | | | |
| 2310903 | 0.0 | 0.0 | 7 | | | | | | |
| 2310904 | 0.66 | 0.66 | 8 | | | | | | |
| 2310905 | 0.0 | 0.0 | 11 | | | | | | |
| 2311001 | 01000 | 12 | | | | | | | |
| 2311101 | 0000 | 11 | | | | | | | |
| 2311201 | 0 | 15048500. | 1263450. | 2459550. | .00000000 | 0.0 | 02 | | |
| 2311202 | 0 | 15045400. | 1309480. | 2459550. | .00000000 | 0.0 | 04 | | |
| 2311203 | 0 | 15042500. | 1357660. | 2459550. | .00000000 | 0.0 | 05 | | |
| 2311204 | 0 | 15040100. | 1394080. | 2459550. | .00000000 | 0.0 | 06 | | |
| 2311205 | 0 | 15037200. | 1417170. | 2459550. | .00000000 | 0.0 | 10 | | |
| 2311206 | 0 | 15034300. | 1424460. | 2459550. | .00000000 | 0.0 | 12 | | |
| 2311300 | 0 | | | | | | | | |
| 2311301 | 1.4679000 | 1.4679000 | 0.0 | 02 | | | | | |
| 2311302 | 1.7789000 | 1.7789000 | 0.0 | 04 | | | | | |
| 2311303 | 1.5425000 | 1.5425000 | 0.0 | 06 | | | | | |
| 2311304 | 1.8668000 | 1.8668000 | 0.0 | 08 | | | | | |
| 2311305 | 1.5994000 | 1.5994000 | 0.0 | 11 | | | | | |
| 2311401 | 0.012 | 0. | 1. | 1. | 1 | | | | |
| 2311402 | 0.012 | 0. | 1. | 1. | 2 | | | | |
| 2311403 | 0.012 | 0. | 1. | 1. | 3 | | | | |
| 2311404 | 0.012 | 0. | 1. | 1. | 4 | | | | |
| 2311405 | 0.012 | 0. | 1. | 1. | 5 | | | | |

| | | | | | |
|---------|-------|----|----|----|----|
| 2311406 | 0.012 | 0. | 1. | 1. | 6 |
| 2311407 | 0.012 | 0. | 1. | 1. | 7 |
| 2311408 | 0.012 | 0. | 1. | 1. | 8 |
| 2311409 | 0.012 | 0. | 1. | 1. | 9 |
| 2311410 | 0.012 | 0. | 1. | 1. | 10 |
| 2311411 | 0.012 | 0. | 1. | 1. | 11 |

* core bypass volume (4 Prozent)

| | | | | | |
|---------|-----------|-----------|----------|----------|-----------|
| 2350000 | corebyps | pipe | | | |
| 2350001 | 3 | | | | |
| 2350101 | 0.0129428 | 3 | | | |
| 2350201 | 0.0 | 2 | | | |
| 2350301 | 0.5588068 | 3 | | | |
| 2350401 | 0.0 | 3 | | | |
| 2350501 | 0.0 | 3 | | | |
| 2350601 | 90.0 | 3 | | | |
| 2350801 | 3.81-6 | 0.003 | 3 | | |
| 2350901 | 0.0 | 0.0 | 2 | | |
| 2351001 | 01000 | 3 | | | |
| 2351101 | 0000 | 2 | | | |
| 2351201 | 0 | 1.49951+7 | 1230900. | 2460030. | 0.0 0.0 1 |
| 2351202 | 0 | 1.49899+7 | 1230870. | 2460150. | 0.0 0.0 2 |
| 2351203 | 0 | 1.49846+7 | 1230840. | 2460270. | 0.0 0.0 3 |
| 2351300 | 0 | | | | |
| 2351301 | 0.6985700 | 0.7893400 | 0.0 | 1 | |
| 2351302 | 0.6985700 | 0.7893600 | 0.0 | 2 | |
| 2351401 | 0.002 | 0. | 1. | 1. | 1 |
| 2351402 | 0.003 | 0. | 1. | 1. | 2 |

* upper end boxes and support structure

| | | | | | |
|---------|-----------|-----------|----------|----------|----------------|
| 2400000 | uprendbx | branch | | | |
| 2400001 | 3 | 0 | | | |
| 2400101 | 0.2423341 | 0.5867979 | 0.0 | 0.0 | 90.0 0.5867979 |
| 2400102 | 3.81-6 | 0.145 | 01000 | | |
| 2400200 | 0 | 1.49777+7 | 1423500. | 2460430. | 0.0 |
| 2401101 | 230010000 | 240000000 | 9.2971-2 | 1.5 | 1.5 100000 |
| 2402101 | 231010000 | 240000000 | 1.8829-2 | 1.5 | 1.5 100000 |
| 2403101 | 235010000 | 240000000 | 0.0 | 12. | 12. 100000 |
| 2401201 | 0.5486000 | 0.5484000 | 0.0 | | |
| 2402201 | 1.5486000 | 1.5484000 | 0.0 | | |
| 2403201 | 0.4357900 | 0.4357900 | 0.0 | | |
| 2401110 | 0.012 | 0. | 1. | 1. | |
| 2402110 | 0.012 | 0. | 1. | 1. | |
| 2403110 | 0.003 | 0. | 1. | 1. | |

* upper core support structure - cross flow region

| | | | | | |
|---------|-----------|-----------|-----------|----------|----------------|
| 2450000 | uprcrsup | branch | | | |
| 2450001 | 2 | 0 | | | |
| 2450101 | 0.0 | 0.4933248 | 0.1280806 | 0.0 | 90.0 0.4933248 |
| 2450102 | 3.81-6 | 0.145 | 01000 | | |
| 2450200 | 0 | 1.51905+7 | 1420710. | 2455290. | 0.0 |
| 2451101 | 240010000 | 245000000 | 0.0 | 0.0 | 0.0 100000 |
| 2452101 | 245010000 | 251000000 | 0.0 | 0.0 | 0.0 100000 |
| 2451201 | 1.4917000 | 1.6814000 | 0.0 | | |
| 2452201 | 2.34575-6 | 2.34579-6 | 0.0 | | |
| 2451110 | 0.145 | 0. | 1. | 1. | |
| 2452110 | 0.145 | 0. | 1. | 1. | |

* upper flow skirt region

| | | | | | |
|---------|-----------|-----------|----------|----------|----------------|
| 2500000 | uflwskrt | branch | | | |
| 2500001 | 1 | 0 | | | |
| 2500101 | 0.1547532 | 0.7850547 | 0.0 | 0.0 | 90.0 0.7850547 |
| 2500102 | 3.81-6 | 0.131 | 01000 | | |
| 2500200 | 0 | 1.51850+7 | 1420710. | 2455420. | 0.0 |
| 2501101 | 245010000 | 250000000 | 0.0 | 0.0 | 0.0 100000 |
| 2501201 | 2.3359000 | 2.5642000 | 0.0 | | |
| 2501110 | 0.145 | 0. | 1. | 1. | |

* dead end of fuel modules

| | | | | | |
|---------|----------|-----------|-----------|----------|----------------|
| 2510000 | deftlmod | snglvol | | | |
| 2510101 | 0.0 | 0.7844123 | 0.1154214 | 0.0 | 90.0 0.7844123 |
| 2510102 | 3.81-6 | 0.214 | 01000 | | |
| 2510200 | 0 | 1.51872+7 | 1590340. | 2455370. | 0.0 |

* upper head

| | | | | | |
|---------|-----------|-----------|----------|----------|----------------|
| 2520000 | uprhead | branch | | | |
| 2520001 | 2 | 0 | | | |
| 2520101 | 0.2622585 | 0.2869580 | 0.0 | 0.0 | 90.0 0.2869580 |
| 2520102 | 3.81-6 | 0.0 | 01000 | | |
| 2520200 | 0 | 1.51825+7 | 1415050. | 2455490. | 0.0 |
| 2521101 | 250010000 | 252000000 | 0.0 | 0.096 | 0.006 100000 |
| 2522101 | 202000000 | 252010000 | 0.0 | 0.90+4 | 0.90+4 0003 |
| 2521201 | 2.3359000 | 2.5642000 | 0.0 | | |
| 2522201 | 0.053 | 0.053 | 0.0 | | |
| 2521110 | 0.131 | 0. | 1. | 1. | |
| 2522110 | 0.172 | 0. | 1. | 1. | |

* upper plenum bottom volume

| | | | | | |
|---------|-----------|-----------|-----|-----|----------------|
| 2550000 | uprplbot | branch | | | |
| 2550001 | 2 | 0 | | | |
| 2550101 | 0.2622585 | 0.6312304 | 0.0 | 0.0 | 90.0 0.6312304 |


```

2550102 3.81-6 0.0 01000
2550200 0 1.51822+7 1539710. 2455490 0.0
2551101 250010000 255000000 0.0 0.006 0.006 100000
2552101 255910000 260000000 0.0 0.03 0.03 100000
2551201 2.16560-5 2.16570-5 0.0
2552201 1.21306-5 0.1789200 0.0
2551110 0.131 0. 1. 1.
*-----|-----|-----|-----|-----|-----|-----|-----|
* upper plenum top volume
*-----|-----|-----|-----|-----|-----|-----|-----|
2600000 uprpltop snglvol
2600101 0.0 0.7747094 0.1914909 0.0 90.0 0.7747094
2600102 3.81-6 0.0 01000
2600200 0 1.51787+7 1592880. 2455580. 0.38893
*-----|-----|-----|-----|-----|-----|-----|-----|
* inlet annulus upper volume intact side
*-----|-----|-----|-----|-----|-----|-----|-----|
2700000 inanupri annulus
2700001 1
2700101 0.1308530 1
2701601 0.0322690 1
2700301 0.1876129 1
2701801 0.7607831 1
2700401 0.0 1
2700501 0.0 1
2700601 90.0 1
2700801 3.81-6 0.172 1
2702301 3.81-6 0.172 1
2701001 01000 1
2702701 00000 1
2701201 0 15201400. 1227290. 2455030. 00000000 0.0 1
*-----|-----|-----|-----|-----|-----|-----|-----|
* junction - upper to lower inlet annulus intact side
*-----|-----|-----|-----|-----|-----|-----|-----|
2710000 inanmuin sngljun
2710101 272000000 270000000 0.129467 0.0000 0.0000 0100
2710110 0.172 0.0 1.0 1.0
2710201 0 .5 .5 0.0
*-----|-----|-----|-----|-----|-----|-----|-----|
* inlet annulus middle volume intact side
*-----|-----|-----|-----|-----|-----|-----|-----|
2720000 inanmidi annulus
2720001 1
2720101 0.1308530 1
2721601 0.0490510 1
2720301 0.2851823 1
2721801 0.7607787 1
2720401 0.0 1
2720501 0.0 1

```

```

2720601 -90.0 1
2720801 3.81-6 0.172 1
2722301 3.81-6 0.172 1
2721001 01000 1
2022701 00000 1
2721201 0 15201400. 1227290. 2455030. 0.0 0.0 1
*-----|-----|-----|-----|-----|-----|-----|-----|
* junction - middle to lower inlet annulus intact side
*-----|-----|-----|-----|-----|-----|-----|-----|
2750000 inanmlin sngljun
2750101 272010000 280000000 0.0709408 0.0 0.0 0100
2750110 0.172 0.0 1.0 1.0
2750201 0 0.5 0.5 0.0
*-----|-----|-----|-----|-----|-----|-----|-----|
* inlet annulus lower volume intact side
*-----|-----|-----|-----|-----|-----|-----|-----|
2800000 inanlwri annulus
2800001 4
2800101 0.0710000 1
2800102 0.0 4
2801601 0.0258470 1
2801602 0.1550460 2
2801603 0.1286870 3
2801604 0.1100840 4
2800201 0.0709408 3
2800301 0.2534239 1
2800302 1.5200561 2
2800303 1.2616333 3
2800304 1.0792591 4
2801801 0.6961386 1
2801802 1.0202559 2
2801803 0.9457054 3
2801804 0.8964118 4
2800401 0.0 1
2800402 0.1581866 2
2800403 0.1217000 3
2800404 0.0986806 4
2800501 0.0 4
2800601 -90.0 4
2800801 3.81-6 0.102 4
2802301 3.81-6 0.102 4
2800901 0.0 0.0 3
2801001 01000 4
2802701 00000 4
2801101 100100 3
2801201 0 15201400. 1227290. 2455030. 00000000 0.0 1
2801202 0 15204900. 1227290. 2454940. 00000000 0.0 2
2801203 0 15213600. 1227290. 2454730. 00000000 0.0 3
2801204 0 15221100. 1227290. 2454550. 00000000 0.0 4

```


| | | | | | | | |
|--|-----------|-----------|-----------|----------|----------|------|---|
| 3150901 | 4.0-5 | 0.0 | 8 | | | | |
| 3150901 | 0.93596 | 0.93596 | 1 | | | | |
| 3150902 | 2.0 | 2.0 | 2 | | | | |
| 3150903 | 0.5 | 0.5 | 3 | | | | |
| 3150904 | 2.0 | 2.0 | 4 | | | | |
| 3150905 | 0.23025 | 0.23025 | 5 | | | | |
| 3150906 | 2.534 | 2.534 | 6 | | | | |
| 3150907 | 5.069 | 5.069 | 7 | | | | |
| 3151001 | 01000 | | 8 | | | | |
| 3151101 | 0000 | | 7 | | | | |
| 3151201 | 0 | 1.51803+7 | 1237700. | 2456950. | 0.0 | 0.0 | 1 |
| 3151202 | 0 | 1.51715+7 | 1237700. | 2456950. | 0.0 | 0.0 | 2 |
| 3151203 | 0 | 1.51636+7 | 1237700. | 2456950. | 0.0 | 0.0 | 3 |
| 3151204 | 0 | 1.51628+7 | 1237700. | 2486950. | 0.0 | 0.0 | 4 |
| 3151205 | 0 | 1.51698+7 | 1237700. | 2456950. | 0.0 | 0.0 | 5 |
| 3151206 | 0 | 1.51809+7 | 1237700. | 2456950. | 0.0 | 0.0 | 6 |
| 3151207 | 0 | 1.51871+7 | 1237700. | 2456950. | 0.0 | 0.0 | 7 |
| 3151208 | 0 | 1.51848+7 | 1237700. | 2456950. | 0.0 | 0.0 | 8 |
| 3151300 | 0 | | | | | | |
| 3151301 | 0. | 0. | 0.0 | 7 | | | |
| * hot leg break valve | | | | | | | |
| 3170000 | hbreak | valve | | | | | |
| 3170101 | 315010000 | 700000000 | 8.3647-3 | 0.94883 | 0.94883 | 0100 | |
| 3170102 | 1.0 | 1.0 | | | | | |
| 3170201 | 0 | 0. | 0. | 0.0 | | | |
| 3170300 | trpviv | | | | | | |
| 3170301 | 510 | | | | | | |
| * reactor vessel nozzle - broken loop cold leg | | | | | | | |
| 3350000 | rvnblic | branch | | | | | |
| 3350001 | 2 | 0 | | | | | |
| 3350101 | 0.0 | 0.749305 | 0.047979 | 0.0 | 0.0 | 0.0 | |
| 3350102 | 4.0-5 | 0.0 | 01000 | | | | |
| 3350200 | 0 | 1.51935+7 | 1273905. | 2456950. | 0.0 | | |
| 3351101 | 272000000 | 335000000 | 0.064130 | 1.455594 | 0.812933 | 0002 | |
| 3352101 | 335010000 | 340000000 | 0.063426 | 0.1005 | 0.1005 | 0000 | |
| 3351201 | 0. | 0. | 0.0 | | | | |
| 3352201 | 0. | 0. | 0.0 | | | | |
| * cold leg pipe to reflood assist bypass tee | | | | | | | |
| 3400000 | clprabst | branch | | | | | |
| 3400001 | 1 | 0 | | | | | |
| 3400101 | 0.0 | 0.698336 | 0.0443927 | 0.0 | 0.0 | 0.0 | |
| 3400102 | 4.0-5 | 0.0 | 01000 | | | | |
| 3400200 | 0 | 1.51935+7 | 1273905. | 2456950. | 0.0 | | |

| | | | | | | | |
|--|-----------|-----------|-----------|----------|--------|------|--|
| 3401101 | 340010000 | 342000000 | 0.063426 | 0.1005 | 0.1005 | 0000 | |
| 3401201 | 0. | 0. | 0.0 | | | | |
| * broken loop cold leg rabs to dtt | | | | | | | |
| 3420000 | bic12dtt | branch | | | | | |
| 3420001 | 1 | 0 | | | | | |
| 3420101 | 0.0 | 0.5715069 | 0.0362484 | 0.0 | 0.0 | 0.0 | |
| 3420102 | 4.0-5 | 0.0 | 01000 | | | | |
| 3420200 | 0 | 1.51935+7 | 1273905. | 2456950. | 0.0 | | |
| 3421101 | 342000000 | 370000000 | 0.0388 | 0.84 | 0.84 | 0000 | |
| 3421201 | 0. | 0. | 0.0 | | | | |
| * broken loop cold leg dtt to break plane | | | | | | | |
| 3440000 | bic12brk | branch | | | | | |
| 3440001 | 1 | 0 | | | | | |
| 3440101 | 0.0 | 0.9286231 | 0.0310679 | 0.0 | 0.0 | 0.0 | |
| 3440102 | 4.0-5 | 0.0 | 01000 | | | | |
| 3440200 | 0 | 1.51935+7 | 1273905. | 2456950. | 0.0 | | |
| 3441101 | 342010000 | 344000000 | 0.0540157 | 6.545 | 14.05 | 0000 | |
| 3441201 | 0. | 0. | 0.0 | | | | |
| * cold leg break valve | | | | | | | |
| 3470000 | clbreak | valve | | | | | |
| 3470101 | 344010000 | 705000000 | 8.3647-3 | 0.415 | 0.415 | 0100 | |
| 3470102 | 1.0 | 1.0 | | | | | |
| 3470201 | 0 | 0. | 0. | 0.0 | | | |
| 3470300 | trpviv | | | | | | |
| 3470301 | 510 | | | | | | |
| * reflood assist bypass piping - cold leg side | | | | | | | |
| 3700000 | rabscl | pipe | | | | | |
| 3700001 | 3 | | | | | | |
| 3700101 | 0.0388 | 2 | | | | | |
| 3700102 | 0.0776 | 3 | | | | | |
| 3700201 | 0.0388 | 2 | | | | | |
| 3700301 | 0.0 | 3 | | | | | |
| 3700401 | 0.0279 | 1 | | | | | |
| 3700402 | 0.070 | 2 | | | | | |
| 3700403 | 0.1165 | 3 | | | | | |
| 3700601 | 90.0 | 1 | | | | | |
| 3700602 | 0.0 | 3 | | | | | |
| 3700701 | 0.64 | 1 | | | | | |
| 3700702 | 0.0 | 3 | | | | | |
| 3700801 | 4.0-5 | 0.0 | 3 | | | | |
| 3700901 | 0.28 | 0.28 | 1 | | | | |


```

* surge line pcs side
4000000 srglnpcs branch
4000001 2
4000101 1.44561-3 2.30 0.0 0.0 90.0 0.54
4000102 2.3622-5 0.0 01000
4000200 0 1.51639+7 1411430 2455940. 0.0
4001101 107000000 400000000 1.44561-3 3.9 3.9 9002
4002101 400010000 405000000 1.44561-3 2.85 2.85 1000
4001201 -5.33782-3 -5 33797-3 0.0
4002201 -5.33967-3 -5.57944-3 0.0
* pressurizer surge lin
* pressurizer surge line
4050000 srglnprzr pipe
4050001 2
4050101 1.44561-3 2
4050201 1.44561-3 1
4050301 2.30 2
4050401 0.0 2
4050601 90.0 2
4050701 0.30 2
4050801 2.3622-5 0.0 2
4050901 2.85 2.85 1
4051001 01000 2
4051101 1000 1
4051201 0 1.51610+7 1410220. 2456010. 0.0 0.0 1
4051202 0 1.51589+7 1409520. 2456060. 0.0 0.0 2
4051300 0
4051301 -5.34077-3 -5.58056-3 0.0 1
* pressurizer surge line
4100000 srgline sngljun
4100101 405010000 415000000 1.44561-3 0.42 1.00 1000
4100201 0 -5.34114-2 -5.58095-2 0.0
* pressurizer vesse
4150000 przvesse pipe
4150001 12
4150101 0.0 4
4150102 0.5653 10
4150103 0.0 12
4150201 0.0 11
4150301 0.09075 2
4150302 0.0762 4
4150303 0.19835 6
4150304 0.26445 8

```

```

3700902 0.84 2
3701001 01000 3
3701101 0000 2
3701201 0 1.51912+7 1227350. 2456950. 0.0 0.0 1
3701202 0 1.51889+7 1227350. 2456950. 0.0 0.0 2
3701203 0 1.51889+7 1227350. 2456950. 0.0 0.0 3
3701300 0
3701301 0. 0. 0.0 2
* reflod assist bypass valve
3750000 rabsvalv valve
3750101 370010000 380000000 0.0 6.5044 0.90+4 1100
3750201 0 .05011390 .05011390 0.0
3750300 trpvlv
3750301 681
* reflod assist bypass piping - hot leg side
3800000 rabsht pipe
3800001 3
3800101 0.0776 1
3800102 0.0388 3
3800201 0.0388 2
3800301 0.0 3
3800401 0.0915 1
3800402 0.048 2
3800403 0.0489 3
3800601 0.0 1
3800602 -90.0 2
3800603 0.0 3
3800701 0.0 1
3800702 -0.64 2
3800703 0.0 3
3800801 4.0-5 0.0 3
3800901 0.84 1
3800902 0.28 2
3801001 01000 3
3801101 0900 2
3801201 0 1.51783+7 1227350. 2456950. 0.0 0.0 1
3801202 0 1.51804+7 1227350. 2456950. 0.0 0.0 2
3801203 0 1.51825+7 1227350. 2456950. 0.0 0.0 3
3801300 0
3801301 0. 0. 0.0 2
* pressurizer [400]

```



```

*-----1-----1-----1-----1-----1-----1-----1-----
5400000 cv-p4-10 valve
5400101 530010000 541000000 0.0047772 0.0 0.0 1100
5400201 0 18.813000 19.188000 0.0
5400300 mtrvlv
5400301 687 688 0.05 0.64829 540
20254000 normarea
20254001 0.0 0.0
20254002 9.25-4 9.25-4
20254003 1.0 1.0
*-----1-----1-----1-----1-----1-----1-----1-----
* pipe downstream of steam control valve
*-----1-----1-----1-----1-----1-----1-----1-----
5410000 condinlt branch
5410001 1 0
5410101 0.06557 54.44 0.0 0.0 0.0 0.0
5410102 4.-5 0.0 01000
5410200 0 2077680. 915077. 2597730. 1.0
5411101 541010000 542000000 0.0 0.0 0.0 0100
5411201 10.486000 32.894000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* air cooled condenser
*-----1-----1-----1-----1-----1-----1-----1-----
5420000 condense tmdpvvl
5420101 0.21677 17.67 0.0 0.0 0.0 0.0
5420102 4.-5 0.02 00000
5420200 2
5420207 0.0 2.069+6 1.0
*-----1-----1-----1-----1-----1-----1-----1-----
* simplified feed system
*-----1-----1-----1-----1-----1-----1-----1-----
* feed storage tank
*-----1-----1-----1-----1-----1-----1-----1-----
5650000 feedtnk tmdpvvl
5650101 29.81 3.048 0.0 0.0 0.0 0.0
5650102 4.-5 0.0 00000
5650200 3 0
5650201 0.0 7.6+6 477.6 * TC = 555.8
*-----1-----1-----1-----1-----1-----1-----1-----
* feed water
*-----1-----1-----1-----1-----1-----1-----1-----
5660000 feed tmdpvvl
5660101 565000000 508000000 0.05
5660200 1 0 cntrlvar 912
5660201 -100.0 19.017 0.0 0.0
5660202 -1.0 0.0 0.0 0.0
5660203 0.0 0.0 0.0 0.0
5660204 50.0 50.0 0.0 0.0
*

```

```

20591100 sglvlerr sum 1.0 0.0 1
20591101 3.1293 -1.0 cntrlvar 1
20591200 feedflow sum 1.0 0.0 1
20591201 0.0 1.0 mflowj 540000000
20591202 48.4 cntrlvar 911
*-----1-----1-----1-----1-----1-----1-----1-----
*
* ecc system [600]
*
*-----1-----1-----1-----1-----1-----1-----1-----
* eccs header to pcs
*-----1-----1-----1-----1-----1-----1-----1-----
6050000 eccshead snglvvl
6050101 5.9896-3 1.0 0.0 0.0 90.0 1.0
6050102 4.0-5 0.0 01000
6050200 0 1.52222+7 1227290. 2454520. 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* accumulator valve
*-----1-----1-----1-----1-----1-----1-----1-----
6100000 accumvlv valve
6100101 615010000 605000000 5.9896-3 6.278 6.278 1100
6100201 0 0. 0. 0.
6100300 trpvvl
6100301 682
*-----1-----1-----1-----1-----1-----1-----1-----
* accumulator pipe
*-----1-----1-----1-----1-----1-----1-----1-----
6150000 accpipe snglvvl
6150101 0.0 25.997165 0.3327 0.0 0.0 0.0
6150102 4.0-5 0.0 01000
6150200 0 4.11+6 120491.12 2600476. 0.
*-----1-----1-----1-----1-----1-----1-----1-----
* accumulator vessel
*-----1-----1-----1-----1-----1-----1-----1-----
6200000 accumula accum
6200101 1.254 1.4151 0.0 0.0 90.0 1.4151
6200102 4.0-5 0.0 00000
6200200 4.11+6 302.0
6201101 615000000 8.2132-3 40. 40. 00000
6202200 1.315 0.0 3.3266 0.8 0.04445 1 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* bwst lpis
*-----1-----1-----1-----1-----1-----1-----1-----
6250000 bwstlpis tmdpvvl
6250101 20.44 5.0 0.0 0.0 90.0 5.0
6250102 4.0-5 0.0 00000
6250200 3
6250201 0.0 1.0+5 305.0

```

```

* low pressure injection system
*
6300000 hpis tmdj tun
6300101 625000000 605000000 5.9896-3
6300200 1 516 p 605010000
6300201 -1.0 0.0 0.0
6300202 0.0 0.0 0.0
6300203 8.483+4 7.045 0.0
6300204 4.297+5 6.091 0.0
6300205 7.745+5 5.045 0.0
6300206 9.448+5 4.313 0.0
6300207 1.119+6 3.454 0.0
6300208 1.186+6 3.173 0.0
6300209 1.257+6 2.673 0.0
6300210 1.326+6 2.159 0.0
6300211 1.395+6 1.536 0.0
6300212 1.464+6 0.7182 0.0
6300213 1.517+6 0.0 0.0
*
* bwt hpis
*
6350000 bwt hpis tmdpvol
6350101 20.44 5.0 0.0 90.0 5.0
6350102 4.0-5 0.0 00000
6350200 3
6350201 0.0 1.0+5 305.0
*
* high pressure injection system
*
6400000 hpis tmdpjun
6400101 635000000 605000000 5.9896-3
6400200 1 513 p 605010000
6400201 -1.0 0.0 0.0
6400202 0.0 .75687272 0.0
6400203 7.72514+6 .75687272 0.0
6400204 8.3597+6 .31536281 0.0
6400205 17.2436+6 .31536281 0.0
*
* containment
*
* containment broken loop hot leg
*
7000000 contblhl tmdpvol
700101 0.0 1.0 0.1 0.0 0.0
7000102 0.0 0.0 00000
7000200 2 510

```

```

7050201 -1.0 106538. 1.0
7000202 0.0 106538. 1.0
7000203 0.278 108155. 1.0
7000204 0.578 181026. 1.0
7000205 1.078 207760. 1.0
7000206 2.078 186200. 1.0
7000207 10.078 251526. 1.0
7000208 20.378 311353. 1.0
7000209 30.378 284404. 1.0
7000210 40.378 266941. 1.0
7000211 50.378 253142. 1.0
7000212 57.278 253142. 1.0
7000213 65.078 300896. 1.0
7000214 75.978 312754. 1.0
7000215 1.45 100000. 1.0
*
* containment broken loop cold leg
*
7050000 contblcl tmdpvol
7050101 0.0 1.0 0.1 0.0 0.0
7050102 0.0 0.0 00000
7050200 2 510
7050201 -1.0 106538. 1.0
7050202 0.0 106538. 1.0
7050203 0.278 108155. 1.0
7050204 0.578 181026. 1.0
7050205 1.078 207760. 1.0
7050206 2.078 186200. 1.0
7050207 .3.078 251526. 1.0
7050208 20.378 311353. 1.0
7050209 30.378 284404. 1.0
7050210 40.378 266941. 1.0
7050211 50.378 253142. 1.0
7050212 57.278 253142. 1.0
7050213 65.078 300896. 1.0
7050214 75.978 312754. 1.0
7050215 1.45 100000. 1.0
*
* reactor vessel heat structures
*
* active core
*
station 116.91 to 182.94
*
peripheral fuel modules
*
12300000 12 10 2 1 0.0 555 1 8

```



```

20500211      0.0975 voidf 415110000
20500212      0.0975 voidf 415120000
20500213      0.19835 voidf 420010000
20500214      0.19835 voidf 420020000
-----|-----|-----|-----|-----|-----|
* 004 accumulator level
-----|-----|-----|-----|-----|-----|
20500400 accmlvl      integral -4.7764-3 2.1 0
20500401 velfj      610000000
-----|-----|-----|-----|-----|-----|
* 007 reactor vessel downcomer level intact side
-----|-----|-----|-----|-----|-----|
20500700 rvdclvl      sum      1.      5.3137665 0
20500701 0.0      0.1876129 voidf 200010000
20500702      0.2851823 voidf 202010000
20500703      0.2525361 voidf 210010000
20500704      1.5200561 voidf 210020000
20500705      1.2616633 voidf 210030000
20500706      1.0792591 voidf 210040000
20500707      0.3533183 voidf 222010000
20500708      0.3741720 voidf 220010000
-----|-----|-----|-----|-----|-----|
20500800 rvdclvl      sum      1.      5.3137665 0
20500801 0.0      0.1876129 voidf 270010000
20500802      0.2851823 voidf 272010000
20500803      0.2525361 voidf 280010000
20500804      1.5200561 voidf 280020000
20500805      1.2616333 voidf 280030000
20500806      1.0792591 voidf 280040000
20500807      0.3533183 voidf 222010000
20500808      0.3741720 voidf 220010000
-----|-----|-----|-----|-----|-----|
* 230 level average channel
-----|-----|-----|-----|-----|-----|
20523000 "lvl avg"      sum      1.0      2.975010 0
20523001 0.0      0.1397017 voidf 230010000
20523002      0.1397017 voidf 230020000
20523003      0.1397017 voidf 230030000
20523004      0.1397017 voidf 230040000
20523005      0.1397017 voidf 230050000
20523006      0.1397017 voidf 230060000
20523007      0.1397017 voidf 230070000
20523008      0.1397017 voidf 230080000
20523009      0.1397017 voidf 230090000
20523010      0.1397017 voidf 230100000
20523011      0.1397017 voidf 230110000
20523012      0.1397017 voidf 230120000
*20523013      0.3742720 voidf 220010000
*20523014      0.3533183 voidf 222010000

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*20523015      0.5709989 voidf 225010000
-----|-----|-----|-----|-----|-----|
* 231 level hot channel
-----|-----|-----|-----|-----|-----|
20523100 "lvl hot"      sum      1.0      2.975010 0
20523101 0.0      0.1397017 voidf 231010000
20523102      0.1397017 voidf 231020000
20523103      0.1397017 voidf 231030000
20523104      0.1397017 voidf 231040000
20523105      0.1397017 voidf 231050000
20523106      0.1397017 voidf 231060000
20523107      0.1397017 voidf 231070000
20523108      0.1397017 voidf 231080000
20523109      0.1397017 voidf 231090000
20523110      0.1397017 voidf 231100000
20523111      0.1397017 voidf 231110000
20523112      0.1397017 voidf 231120000
*20523113      0.3742720 voidf 220010000
*20523114      0.3533183 voidf 222010000
*20523115      0.5709989 voidf 225010000
-----|-----|-----|-----|-----|-----|
* 090 thermal power - average
-----|-----|-----|-----|-----|-----|
20509000 "pow-avg"      sum      1.      3.57765+7 0
20509001 0.0      1.      q      230010000
20509002      1.      q      230020000
20509003      1.      q      230030000
20509004      1.      q      230040000
20509005      1.      q      230050000
20509006      1.      q      230060000
20509007      1.      q      230070000
20509008      1.      q      230080000
20509009      1.      q      230090000
20509010      1.      q      230100000
20509011      1.      q      230110000
20509012      1.      q      230120000
-----|-----|-----|-----|-----|-----|
* 091 thermal power - hot
-----|-----|-----|-----|-----|-----|
20509100 "pow-hot"      sum      1.      0.91253+7 0
20509101 0.0      1.      q      231010000
20509102      1.      q      231020000
20509103      1.      q      231030000
20509104      1.      q      231040000
20509105      1.      q      231050000
20509106      1.      q      231060000
20509107      1.      q      231070000
20509108      1.      q      231080000
20509109      1.      q      231090000

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* 096 structure downcomer broken loop
-----|-----|-----|-----|-----|
20509600 "hc brkl"          sum      1.      2181.7821 0
20509601 0.0          1.0      q      270010000
20509602          1.0      q      272010000
20509603          1.0      q      280010000
20509604          1.0      q      280020000
20509605          1.0      q      280030000
20509606          1.0      q      280040000
-----|-----|-----|-----|-----|
* 097 structure core barrel
-----|-----|-----|-----|-----|
20509700 "hc core"          sum      1.      259.08643 0
20509701 0.0          1.0      q      220010000
20509702          1.0      q      222010000
20509703          1.0      q      225010000
-----|-----|-----|-----|-----|
* 098 structure total
-----|-----|-----|-----|-----|
20509800 heatcap          sum      1.      4382.7578 0
20509801 0.0          1.0      cntrlvar 95
20509802          1.0      cntrlvar 96
20509803          1.0      cntrlvar 97
-----|-----|-----|-----|-----|
*
*
-----|-----|-----|-----|-----|
* 510 - 520 trip-sets
*
* 510 blow-down valves
-----|-----|-----|-----|-----|
20551000 blowdown          tripunit 1.      0.      0
20551001 510
-----|-----|-----|-----|-----|
* 511 power scram
-----|-----|-----|-----|-----|
20551100 powerscr          tripunit 1.      0.      0
20551101 511
-----|-----|-----|-----|-----|
* 512 pump trip
-----|-----|-----|-----|-----|
20551200 pumptrip          tripunit 1.      0.      0
20551201 512
-----|-----|-----|-----|-----|
* 513 hpis trip
-----|-----|-----|-----|-----|
20551300 hpistrip          tripunit 1.      0.      0
20551301 513
-----|-----|-----|-----|-----|

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* 536 lpis trip
-----|-----|-----|-----|-----|
20553600 lpistrip          tripunit 1.      0.      0
20553601 516
-----|-----|-----|-----|-----|
* 524 accumulator valve
-----|-----|-----|-----|-----|
20552400 accumulv          tripunit 1.      0.      0
20552401 682
-----|-----|-----|-----|-----|
* 514 eccs
-----|-----|-----|-----|-----|
*20551400 eccs          sum      1.      0.      0
*20551401 0.0          .3      cntrlvar 523
*20551402          .7      cntrlvar 524
-----|-----|-----|-----|-----|
* 516 steam valve
-----|-----|-----|-----|-----|
20552600 steamvop          tripunit 1.      0.      0
20552601 685
20552700 steamvci          tripunit -1.      0.      0
20552701 686
20551600 steamvivi          sum      1.      0.      0
20551601 0.0          1.0      cntrlvar 526
20551602          1.0      cntrlvar 527
-----|-----|-----|-----|-----|
*
*
-----|-----|-----|-----|-----|
* 401 - 408 mass flux, momentum flux of 225-01
*
-----|-----|-----|-----|-----|
* .01 absolute of velfj 225010000
-----|-----|-----|-----|-----|
20540100 avl22501          stdfnctn 1.      0.      1
20540101          abs      velfj      225010000
-----|-----|-----|-----|-----|
* 402 absolute of velfj 225010000
-----|-----|-----|-----|-----|
20540200 avg22501          stdfnctn 1.      0.      1
20540201          abs      velgj      225010000
-----|-----|-----|-----|-----|
* 403 liquid mass flux of junction 225010000
-----|-----|-----|-----|-----|
20540300 mfl22501          mult      1.      0.      1
20540301 voidfj      225010000 rhofj      225010000
20540302 velfj      225010000

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*-----|-----|-----|-----|-----|-----|
* 404 void mass flux of junction 225010000
*-----|-----|-----|-----|-----|-----|
20540400 mfg22501      mult 1.      0.      1
20540401 voidgj      225010000 rhogj 225010000
20540402 velgj      225010000
*-----|-----|-----|-----|-----|-----|
* 405 mass flux of junction 225010000
*-----|-----|-----|-----|-----|-----|
20540500 mf22501      sum 1.      0.      1
20540501      0.0      1.0      cntrlvar 403
20540502      1.0      cntrlvar 404
*-----|-----|-----|-----|-----|-----|
* 406 liquid phase momentum flux of junction 225010000
*-----|-----|-----|-----|-----|-----|
20540600 mml22501      mult 1.      0.      1
20540601 cntrlvar 401      cntrlvar 403
*-----|-----|-----|-----|-----|-----|
* 407 void phase momentum flux of junction 225010000
*-----|-----|-----|-----|-----|-----|
20540700 mmg22501      mult 1.      0.      1
20540701 cntrlvar 402      cntrlvar 404
*-----|-----|-----|-----|-----|-----|
* 408 momentum flux of junction 225010000
*-----|-----|-----|-----|-----|-----|
20540800 mmf22501      sum 1.      0.      1
20540801      0.0      1.0      cntrlvar 406
20540802      1.0      cntrlvar 407
*-----|-----|-----|-----|-----|-----|
*
* 411 - 418 mass flux, momentum flux of 225-02
*
*-----|-----|-----|-----|-----|-----|
* 411 absolute of velfj 225020000
*-----|-----|-----|-----|-----|-----|
20541100 avl22502      stdfnctn 1.      0.      1
20541101      abs      velfj 225020000
*-----|-----|-----|-----|-----|-----|
* 412 absolute of velfj 225020000
*-----|-----|-----|-----|-----|-----|
20541200 avg22502      stdfnctn 1.      0.      1
20541201      abs      velgj 225020000
*-----|-----|-----|-----|-----|-----|
* 413 liquid mass flux of junction 225020000
*-----|-----|-----|-----|-----|-----|
20541300 mfl22502      mult 1.      0.      1
20541301 voidfj      225020000 rhofj 225020000
20541302 velfj      225020000
*-----|-----|-----|-----|-----|-----|

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* 414 void mass flux of junction 225020000
*-----|-----|-----|-----|-----|-----|
20541400 mfg22502      mult 1.      0.      1
20541401 voidgj      225020000 rhogj 225020000
20541402 velgj      225020000
*-----|-----|-----|-----|-----|-----|
* 415 mass flux of junction 225020000
*-----|-----|-----|-----|-----|-----|
20541500 mf22502      sum 1.      0.      1
20541501      0.0      1.0      cntrlvar 413
20541502      1.0      cntrlvar 414
*-----|-----|-----|-----|-----|-----|
* 416 liquid phase momentum flux of junction 225020000
*-----|-----|-----|-----|-----|-----|
20541600 mml22502      mult 1.      0.      1
20541601 cntrlvar 411      cntrlvar 413
*-----|-----|-----|-----|-----|-----|
* 417 void phase momentum flux of junction 225020000
*-----|-----|-----|-----|-----|-----|
20541700 mmg22502      mult 1.      0.      1
20541701 cntrlvar 412      cntrlvar 414
*-----|-----|-----|-----|-----|-----|
* 418 momentum flux of junction 225020000
*-----|-----|-----|-----|-----|-----|
20541800 mmf22502      sum 1.      0.      1
20541801      0.0      1.0      cntrlvar 416
20541802      1.0      cntrlvar 417
*-----|-----|-----|-----|-----|-----|
*
* 421 - 428 mass flux, momentum flux of 240-01
*
*-----|-----|-----|-----|-----|-----|
* 421 absolute of velfj 240010000
*-----|-----|-----|-----|-----|-----|
20542100 avl24001      stdfnctn 1.      0.      1
20542101      abs      velfj 240010000
*-----|-----|-----|-----|-----|-----|
* 422 absolute of velfj 240010000
*-----|-----|-----|-----|-----|-----|
20542200 avg24001      stdfnctn 1.      0.      1
20542201      abs      velgj 240010000
*-----|-----|-----|-----|-----|-----|
* 423 liquid mass flux of junction 240010000
*-----|-----|-----|-----|-----|-----|
20542300 mfl24001      mult 1.      0.      1
20542301 voidfj      240010000 rhofj 240010000
20542302 velfj      240010000
*-----|-----|-----|-----|-----|-----|
* 424 void mass flux of junction 240010000

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*-----1-----1-----1-----1-----1-----1-----
20542400 mfg24001          mult 1. 0. 1
20542401 voidgj          240010000 rhogj 240010000
20542402 velgj          240010000
*-----1-----1-----1-----1-----1-----1-----
* 425 mass flux of junction 240010000
*-----1-----1-----1-----1-----1-----1-----
20542500 mf24001          sum 1. 0. 1
20542501          0.0 1.0 cntrlvar 423
20542502          1.0 cntrlvar 424
*-----1-----1-----1-----1-----1-----1-----
* 426 liquid phase momentum flux of junction 240010000
*-----1-----1-----1-----1-----1-----1-----
20542600 mml24001          mult 1. 0. 1
20542601 cntrlvar 421 cntrlvar 423
*-----1-----1-----1-----1-----1-----1-----
* 427 void phase momentum flux of junction 240010000
*-----1-----1-----1-----1-----1-----1-----
20542700 mmg24001          mult 1. 0. 1
20542701 cntrlvar 422 cntrlvar 424
*-----1-----1-----1-----1-----1-----1-----
* 428 momentum flux of junction 240010000
*-----1-----1-----1-----1-----1-----1-----
20542800 mmf24001          sum 1. 0. 1
20542801          0.0 1.0 cntrlvar 426
20542802          1.0 cntrlvar 427
*-----1-----1-----1-----1-----1-----1-----
*
* 431 - 438 mass flux, momentum flux of 240-02
*
*-----1-----1-----1-----1-----1-----1-----
* 431 absolute of velfj 240020000
*-----1-----1-----1-----1-----1-----1-----
20543100 avl24002          stdfnctn 1. 0. 1
20543101          abs velfj 240020000
*-----1-----1-----1-----1-----1-----1-----
* 432 absolute of velfj 240020000
*-----1-----1-----1-----1-----1-----1-----
20543200 avg24002          stdfnctn 1. 0. 1
20543201          abs velgj 240020000
*-----1-----1-----1-----1-----1-----1-----
* 433 liquid mass flux of junction 240020000
*-----1-----1-----1-----1-----1-----1-----
20543300 mfl24002          mult 1. 0. 1
20543301 voidfj          240020000 rhofj 240020000
20543302 velfj          240020000
*-----1-----1-----1-----1-----1-----1-----
* 434 void mass flux of junction 240020000
*-----1-----1-----1-----1-----1-----1-----

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20543400 mfg24002          mult 1. 0. 1
20543401 voidgj          240020000 rhogj 240020000
20543402 velgj          240020000
*-----1-----1-----1-----1-----1-----1-----
* 435 mass flux of junction 240020000
*-----1-----1-----1-----1-----1-----1-----
20543500 mf24002          sum 1. 0. 1
20543501          0.0 1.0 cntrlvar 433
20543502          1.0 cntrlvar 434
*-----1-----1-----1-----1-----1-----1-----
* 436 liquid phase momentum flux of junction 240020000
*-----1-----1-----1-----1-----1-----1-----
20543600 mml24002          mult 1. 0. 1
20543601 cntrlvar 431 cntrlvar 433
*-----1-----1-----1-----1-----1-----1-----
* 437 void phase momentum flux of junction 240020000
*-----1-----1-----1-----1-----1-----1-----
20543700 mmg24002          mult 1. 0. 1
20543701 cntrlvar 432 cntrlvar 434
*-----1-----1-----1-----1-----1-----1-----
* 438 momentum flux of junction 240020000
*-----1-----1-----1-----1-----1-----1-----
20543800 mmf24002          sum 1. 0. 1
20543801          0.0 1.0 cntrlvar 436
20543802          1.0 cntrlvar 437
*-----1-----1-----1-----1-----1-----1-----
*
* 441 - 448 mass flux, momentum flux of 231-05
*
*-----1-----1-----1-----1-----1-----1-----
* 441 absolute of velfj 231050000
*-----1-----1-----1-----1-----1-----1-----
20544100 avl23105          stdfnctn 1. 0. 1
20544101          abs velfj 231050000
*-----1-----1-----1-----1-----1-----1-----
* 442 absolute of velfj 231050000
*-----1-----1-----1-----1-----1-----1-----
20544200 avg23105          stdfnctn 1. 0. 1
20544201          abs velgj 231050000
*-----1-----1-----1-----1-----1-----1-----
* 443 liquid mass flux of junction 231050000
*-----1-----1-----1-----1-----1-----1-----
20544300 mfl23105          mult 1. 0. 1
20544301 voidfj          231050000 rhofj 231050000
20544302 velfj          231050000
*-----1-----1-----1-----1-----1-----1-----
* 444 void mass flux of junction 231050000
*-----1-----1-----1-----1-----1-----1-----
20544400 mfg23105          mult 1. 0. 1

```


| | | |
|--------------------|--------------|--------------|
| 1351304 | -4.068300-01 | 1.624000+00 |
| 1351305 | -2.001710-01 | 1.470500+00 |
| 1351306 | 0.000000+00 | 1.403600+00 |
| * head curve no. 4 | | |
| 1351400 | 1 | 4 |
| 1351401 | -1.000000+00 | 2.472200+00 |
| 1351402 | -8.229700-01 | 1.996800+00 |
| 1351403 | -6.333200-01 | 1.589700+00 |
| 1351404 | -4.553400-01 | 1.327900+00 |
| 1351405 | -2.710900-01 | 1.194900+00 |
| 1351406 | -1.771600-01 | 1.060500+00 |
| 1351407 | -9.073000-02 | 1.015600+00 |
| 1351408 | 0.000000+00 | 9.342790-01 |
| * head curve no. 5 | | |
| 1351500 | 1 | 5 |
| 1351501 | 0.000000+00 | 2.500000-01 |
| 1351502 | 2.000000-01 | 2.800000-01 |
| 1351503 | 4.000000-01 | 3.400000-01 |
| 1351504 | 4.118000-01 | 2.768000-01 |
| 1351505 | 5.976300-01 | 4.584000-01 |
| 1351506 | 7.934670-01 | 6.992000-01 |
| 1351507 | 1.000000+00 | 1.000000+00 |
| * had curve no. 6 | | |
| 1351600 | 1 | 6 |
| 1351601 | 0.000000+00 | 9.342790-01 |
| 1351602 | 9.109900-02 | 9.229000-01 |
| 1351603 | 1.865090-01 | 8.963000-01 |
| 1351604 | 2.717620-01 | 8.750000-01 |
| 1351605 | 4.558720-01 | 8.433000-01 |
| 1351606 | 5.744060-01 | 8.355000-01 |
| 1351607 | 7.405760-01 | 8.466000-01 |
| 1351608 | 7.666190-01 | 8.469000-01 |
| 1351609 | 8.714710-01 | 8.838000-01 |
| 1351610 | 1.000000+00 | 1.000000+00 |
| * head curve no. 7 | | |
| 1351700 | 1 | 7 |
| 1351701 | -1.000000+00 | -1.000000+00 |
| 1351702 | -8.000000-01 | -6.300000-01 |
| 1351703 | -6.000000-01 | -3.000000-01 |
| 1351704 | -4.000000-01 | -5.000000-02 |
| 1351705 | -2.000000-01 | 1.500000-01 |

| | | |
|----------------------------|--------------|--------------|
| 1351706 | 0.000000+00 | 2.500000-01 |
| * head curve no. 8 | | |
| 1351800 | 1 | 8 |
| 1351801 | -1.000000+00 | -1.000000+00 |
| 1351802 | -8.000000-01 | -9.700000-01 |
| 1351803 | -6.000000-01 | -9.500000-01 |
| 1351804 | -4.000000-01 | -8.800000-01 |
| 1351805 | -2.000000-01 | -8.000000-01 |
| 1351806 | 0.000000+00 | -6.700000-01 |
| * single phase torque data | | |
| * torque curve no. 1 | | |
| 1351900 | 2 | 1 |
| 1351901 | 0.000000+00 | 6.032000-01 |
| 1351902 | 1.930000-01 | 6.325000-01 |
| 1351903 | 3.930000-01 | 7.369000-01 |
| 1351904 | 5.955200-01 | 8.331000-01 |
| 1351905 | 7.978200-01 | 9.229000-01 |
| 1351906 | 1.000000+00 | 1.000000+00 |
| * torque curve no. 2 | | |
| 1352000 | 2 | 2 |
| 1352001 | 0.000000+00 | -6.700000-01 |
| 1352002 | 4.000000-01 | -2.500000-01 |
| 1352003 | 5.000000-01 | 1.500000-01 |
| 1352004 | 7.372550-01 | 5.265860-01 |
| 1352005 | 7.680490-01 | 6.065940-01 |
| 1352006 | 8.672300-01 | 7.436600-01 |
| 1352007 | 1.000000+00 | 1.000000+00 |
| * torque curve no. 3 | | |
| 1352100 | 2 | 3 |
| 1352101 | -1.000000+00 | 1.984300+00 |
| 1352102 | -8.009600-01 | 1.394000+00 |
| 1352103 | -6.063800-01 | 1.097500+00 |
| 1352104 | -4.068600-01 | 8.220000-01 |
| 1352105 | -1.992800-01 | 6.648000-01 |
| 1352106 | 0.000000+00 | 6.032000-01 |
| * torque curve no. 4 | | |
| 1352200 | 2 | 4 |
| 1352201 | -1.000000+00 | 1.984300+00 |

| | | |
|--------------------|--------------|--------------|
| 1354302 | -9.000000-01 | -1.240000+00 |
| 1354303 | -8.000000-01 | -1.770000+00 |
| 1354304 | -7.000000-01 | -2.360000+00 |
| 1354305 | -6.000000-01 | -2.790000+00 |
| 1354306 | -5.000000-01 | -2.910000+00 |
| 1354307 | -4.000000-01 | -2.670000+00 |
| 1354308 | -2.500000-01 | -1.690000+00 |
| 1354309 | -1.000000-01 | -5.000000-01 |
| 1354310 | 0.000000+00 | 0.000000+00 |
| * head curve no. 4 | | |
| 1354400 | 1 | 4 |
| 1354401 | -1.000000+00 | -1.160000+00 |
| 1354402 | -9.000000-01 | -7.800000-01 |
| 1354403 | -8.000000-01 | -5.000000-01 |
| 1354404 | -7.000000-01 | -3.100000-01 |
| 1354405 | -6.000000-01 | -1.700000-01 |
| 1354406 | -5.000000-01 | -8.000000-02 |
| 1354407 | -3.500000-01 | 0.000000+00 |
| 1354408 | -2.000000-01 | 5.000000-02 |
| 1354409 | -1.000000-01 | 8.000000-02 |
| 1354410 | 0.000000+00 | 1.100000-01 |
| * head curve no. 5 | | |
| 1354500 | 1 | 5 |
| 1354501 | 0.000000+00 | 0.000000+00 |
| 1354502 | 2.000000-01 | -3.400000-01 |
| 1354503 | 4.000000-01 | -6.500000-01 |
| 1354504 | 6.000000-01 | -9.300000-01 |
| 1354505 | 8.000000-01 | -1.190000+00 |
| 1354506 | 1.000000+00 | -1.470000+00 |
| * head curve no. 6 | | |
| 1354600 | 1 | 6 |
| 1354601 | 0.000000+00 | 1.100000-01 |
| 1354602 | 1.000000-01 | 1.300000-01 |
| 1354603 | 2.500000-01 | 1.500000-01 |
| 1354604 | 4.000000-01 | 1.300000-01 |
| 1354605 | 5.000000-01 | 7.000000-02 |
| 1354606 | 6.000000-01 | -4.000000-02 |
| 1354607 | 7.000000-01 | -2.300000-01 |
| 1354608 | 8.000000-01 | -5.100000-01 |
| 1354609 | 9.000000-01 | -9.100000-01 |
| 1354610 | 1.000000+00 | -1.470000+00 |
| * head curve no. 7 | | |

| | | |
|----------------------|--------------|--------------|
| 1354700 | 1 | 7 |
| 1354701 | -1.000000+00 | 0.000000+00 |
| 1354702 | 0.000000+00 | 0.000000+00 |
| * head curve no. 8 | | |
| 1354800 | 1 | 8 |
| 1354801 | -1.000000+00 | 0.000000+00 |
| 1354802 | 0.000000+00 | 0.000000+00 |
| * torque curve no. 1 | | |
| 1354900 | 2 | 1 |
| 1354901 | 0.000000+00 | 1.000000+00 |
| 1354906 | 1.000000+00 | 1.000000+00 |
| * torque curve no. 2 | | |
| 1355000 | 2 | 2 |
| 1355001 | 0.000000+00 | 1.000000+00 |
| 1355007 | 1.000000+00 | 1.000000+00 |
| * torque curve no. 3 | | |
| 1355100 | 2 | 3 |
| 1355101 | -1.000000+00 | 1.984300+00 |
| 1355102 | -8.009600-01 | 1.394000+00 |
| 1355103 | -6.063800-01 | 1.097500+00 |
| 1355104 | -4.068600-01 | 8.220000-01 |
| 1355105 | -1.992800-01 | 6.648000-01 |
| 1355106 | 0.000000+00 | 6.032000-01 |
| * torque curve no. 4 | | |
| 1355200 | 2 | 4 |
| 1355201 | -1.000000+00 | 1.984300+00 |
| 1355202 | -8.223400-01 | 1.830800+00 |
| 1355203 | -6.337100-01 | 1.682400+00 |
| 1355204 | -4.585300-01 | 1.557000+00 |
| 1355205 | -2.670230-01 | 1.436200+00 |
| 1355206 | -1.761070-01 | 1.387900+00 |
| 1355207 | -8.931000-02 | 1.348100+00 |
| 1355208 | 0.000000+00 | 1.233610+00 |
| * torque curve no. 5 | | |
| 1355300 | 2 | 5 |
| 1355301 | 0.000000+00 | -4.500000-01 |


```

9900101 1.0 1.0 0.0 0.0 0.0 0.0 0.0
9900102 4.0-5 0.0 0.0 0.0 0.0 0.0
9900200 3
9900201 0.0 1.44+7 559.2
* letdown valve
*
9950000 ltdnvlv valve
9950101 185000000 990000000 2.5-5 0.0 0.0 0.0 0100
9950201 0 0.0 0.0 0.0
9950300 srvvlv
9950301 999
20299900 normarea
20299901 0.0 0.0
20299902 0.0001 0.0
20299903 1.0 1.0
* letdown valve position calculator
*
20590660 ltdnwn sum -7.7 0.0 1
+ 3 0.0 1.0
20590661 1.04 -1.0 cntrlvar 2
*
* steam valve controller
*
* changes to steam valve
*
5400000 cv-p4-10 valve
5400101 530010000 541000000 0.0047772 0.0 0.0 0.0 1100
5400201 0 17.80400 17.80400 0.0
5400300 srvvlv
5400301 910 540
20254000 normarea
20254001 0.0 0.0
20254002 1.0-4 0
20254003 1.0 1.0
* compute delta t error
*
20590700 deltat sum 1.0 0.0 1
20590701 555.9 -1. temp 185010000
* filter delta t through deadband
*
20590800 deadband function 1.0 0.0 1
20590801 cntrlvar 907
20290800 reac-t

```

```

20290801 -100.
20290802 -0.1
20290803 -0.1 0.0
20290804 0.1 0.0
20290805 0.1 0.1
20290806 100.
* integrate delta t error
*
20590900 int-dt integral 1.0 0.0 1
20590901 cntrlvar 908
* steam valve position calculator
*
20591000 tcontrol sum 1.0 0.65 0.50405 0
+ 3 0.40 0.40
20591001 0.50405 cntrlvar 908
20591002 -0.0059 cntrlvar 909
* end of input

```



```

*-----1-----1-----1-----1-----1-----1-----
* head curve no. 8
*-----1-----1-----1-----1-----1-----1-----
1351800  1          8
1351801 -1.000000+00 -1.000000+00
1351802 -8.000000-01 -9.700000-01
1351803 -6.000000-01 -9.500000-01
1351804 -4.000000-01 -8.800000-01
1351805 -2.000000-01 -8.000000-01
1351806  0.000000+00 -6.700000-01
*-----1-----1-----1-----1-----1-----1-----
* single phase torque data
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 1
*-----1-----1-----1-----1-----1-----1-----
1351900  2          1
1351901  0.000000+00  6.032000-01
1351902  1.930000-01  6.325000-01
1351903  0.930000-01  7.369000-01
1351904  5.935200-01  8.331000-01
1351905  7.978200-01  9.229000-01
1351906  1.000000+00  1.000900+00
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 2
*-----1-----1-----1-----1-----1-----1-----
1352000  2          2
1352001  0.000000+00 -6.700000-01
1352002  4.000000-01 -2.500000-01
1352003  5.000000-01  1.500000-01
1352004  7.372550-01  5.265860-01
1352005  7.680490-01  6.065940-01
1352006  8.672300-01  7.436600-01
1352007  1.000000+00  1.000000+00
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 3
*-----1-----1-----1-----1-----1-----1-----
1352100  2          3
1352101 -1.000000+00  1.984300+00
1352102 -8.009600-01  1.394000+00
1352103 -6.063800-01  1.097500+00
1352104 -4.068500-01  8.220000-01
1352105 -1.992800-01  6.648000-01
1352106  0.000000+00  6.032000-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 4
*-----1-----1-----1-----1-----1-----1-----
1352200  2          4
1352201 -1.000000+00  1.984300+00
1352202 -8.223400-01  1.830800+00

```

```

1352203 -6.337100-01  1.682400+00
1352204 -4.585300-01  1.557000+00
1352205 -2.670230-01  1.436200+00
1352206 -1.761070-01  1.387900+00
1352207 -8.931000-02  1.348100+00
1352208  0.000000+00  1.233610+00
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 5
*-----1-----1-----1-----1-----1-----1-----
1352300  2          5
1352301  0.000000+00 -4.500000-01
1352302  4.000000-01 -2.500000-01
1352303  5.000000-01  0.000000+00
1352304  1.000000+00  3.569000-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 6
*-----1-----1-----1-----1-----1-----1-----
1352400  2          6
1352401  0.000000+00  1.233610+00
1352402  9.064300-02  1.196500+00
1352403  1.885690-01  1.109600+00
1352404  2.734700-01  1.041600+00
1352405  4.586690-01  8.958000-01
1352406  5.744800-01  7.807000-01
1352407  7.381600-01  6.134000-01
1352408  7.685200-01  5.849000-01
1352409  8.700570-01  4.877000-01
1352410  1.000000+00  3.569000-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 7
*-----1-----1-----1-----1-----1-----1-----
1352500  2          7
1352501 -1.000000+00 -1.000000+00
1352502 -3.000000-01 -9.000000-01
1352503 -1.000000-01 -5.000000-01
1352504  0.000000+00 -4.500000-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 8
*-----1-----1-----1-----1-----1-----1-----
1352600  2          8
1352601 -1.000000+00 -1.000000+00
1352602 -2.500000-01 -9.000000-01
1352603 -8.000000-02 -8.000000-01
1352604  0.000000+00 -6.700000-01
*-----1-----1-----1-----1-----1-----1-----
* two - phase multiplier data from 13-6 test data
*-----1-----1-----1-----1-----1-----1-----
* head curve
*-----1-----1-----1-----1-----1-----1-----

```



```

*-----|-----|-----|-----|-----|-----|-----|
5400000 cv-p4-10 valve
5400101 530010000 541000000 0.0047772 0.0 0.0 1100
5400201 0 19.14 19.55 0.0
5400300 mtrvlv
5400301 687 688 0.05 0.41617 540
20254000 normarea
20254001 0.0
20254002 9.25-4 9.25-4
20254003 1.0 1.0
20590800 deadband delete
20590900 int-dt delete
20591000 tcontrol delete
20591100 sgvlerr delete
20591200 feedflow delete
*-----|-----|-----|-----|-----|-----|-----|
* change input for feed water system
*-----|-----|-----|-----|-----|-----|-----|
5660000 feed tmdpjun
5660101 565000000 508000000 0.05
5660200 1 511
5660202 0.0 24.32 0.0 0.0
5660203 0.5 2.06 0.0 0.0
5660204 1.0 1.00 0.0 0.0
5660205 1.5 0.61 0.0 0.0
5660206 1.46 0.50 0.0 0.0
*-----|-----|-----|-----|-----|-----|-----|
* 074 mass loss through x-flow junction
*-----|-----|-----|-----|-----|-----|-----|
20507400 lossxj
20507401 mflowj 290000000
* end of input

```


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S. Smith, NRC Project Manager

11. ABSTRACT (200 words or less)

The LOFT experiment LP-02-6 was simulated using the RELAP5/MOD3.2 code to assess its capability to predict the thermal-hydraulic phenomena in LBLOCA of the PWR. The reactor vessel was modeled with two core channels and split downcomer for a base calculation. The results of the base calculation show that the code can not predict the early bottom-up quenching which is a distinguished phenomenon of the experiment LP-02-6, mainly due to the deficiency of break flow model.

The discharge coefficient sensitivity study was performed to show that the calculated subcooled break flow which might significantly affect the early bottom-up quenching is dependent on the coefficient. More detailed modeling of the cross flow in the split downcomer was performed, but, resulted in little improvement on the predictability of bottom-up quenching. Additional calculation using the RELAP5/MOD3.1 instead of RELAP5/MOD3.2 showed that there is no large difference between the versions in the simulation of LBLOCA.

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