



IOWA METHODIST HOSPITAL

RAYMOND BLANK MEMORIAL HOSPITAL FOR CHILDREN
YOUNKER MEMORIAL REHABILITATION CENTER
HELEN POWELL CONVALESCENT CENTER

Area Code: 515
Telephone: 283-6212

1200 PLEASANT STREET
DES MOINES, IOWA 50308

December 5, 1974

4923

51891
Mr. Frank C. Davis
Material Branch
Directorate of Licensing
Atomic Energy Commission
Washington D.C. 20545

Dear Mr. Davis:

I am writing in response to your letter of October 29, 1974 for additional information for a cobalt-60 teletherapy license.

Attached to this letter is a copy of the calculations requested performed by our radiation physicist, Mr. Steven Babcock.

If additional information is necessary, please contact me.

Yours truly,

David S. Ramsey
Vice President & Administrator

DSR:rh

Enc.

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IOWA METHODIST HOSPITAL

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1200 PLEASANT STREET
DES MOINES, IOWA 50308

Department of Radiology

Area Code 515 283-6171

December 4, 1974

Enclosed is the extra information you requested. Your letter is enclosed.

The original shielding calculations could not be found. What has been done is a set of shielding calculations using NCRP No. 34 to show that the shielding is adequate. However, before the room is put into use a radiation survey will be done, to insure safe radiation levels in the adjacent areas.

The TV viewing system will be backed up by an alternate viewing system. The back-up shall consist of a lead window in the door and a curved mirror in the northwest corner of the room. With this, viewing of the patient can be maintained.

Steven M. Babcock

Steven M. Babcock,
Medical Physicist.

NCRP Report No. 34 - Medical X-ray and Gamma Ray Protection for energies up to 10 MEV - Structural Shielding Design and Evaluation - was used to find the required shielding. In particular, information in Appendices B, C and D was used.

The following values were used in the calculations.

$$\begin{aligned} W &= 40,000 \text{ R/week at 1 meter} \\ U &= 1 \\ T &= 1 \text{ except for ceiling } T = 1/16 \end{aligned}$$

The equations used were:

For scattered radiation

$$B_{sg} = \frac{P}{aWT} (d_{sec})^2 (d_{scat})^2$$

a - from Table B-2 NCRP 34

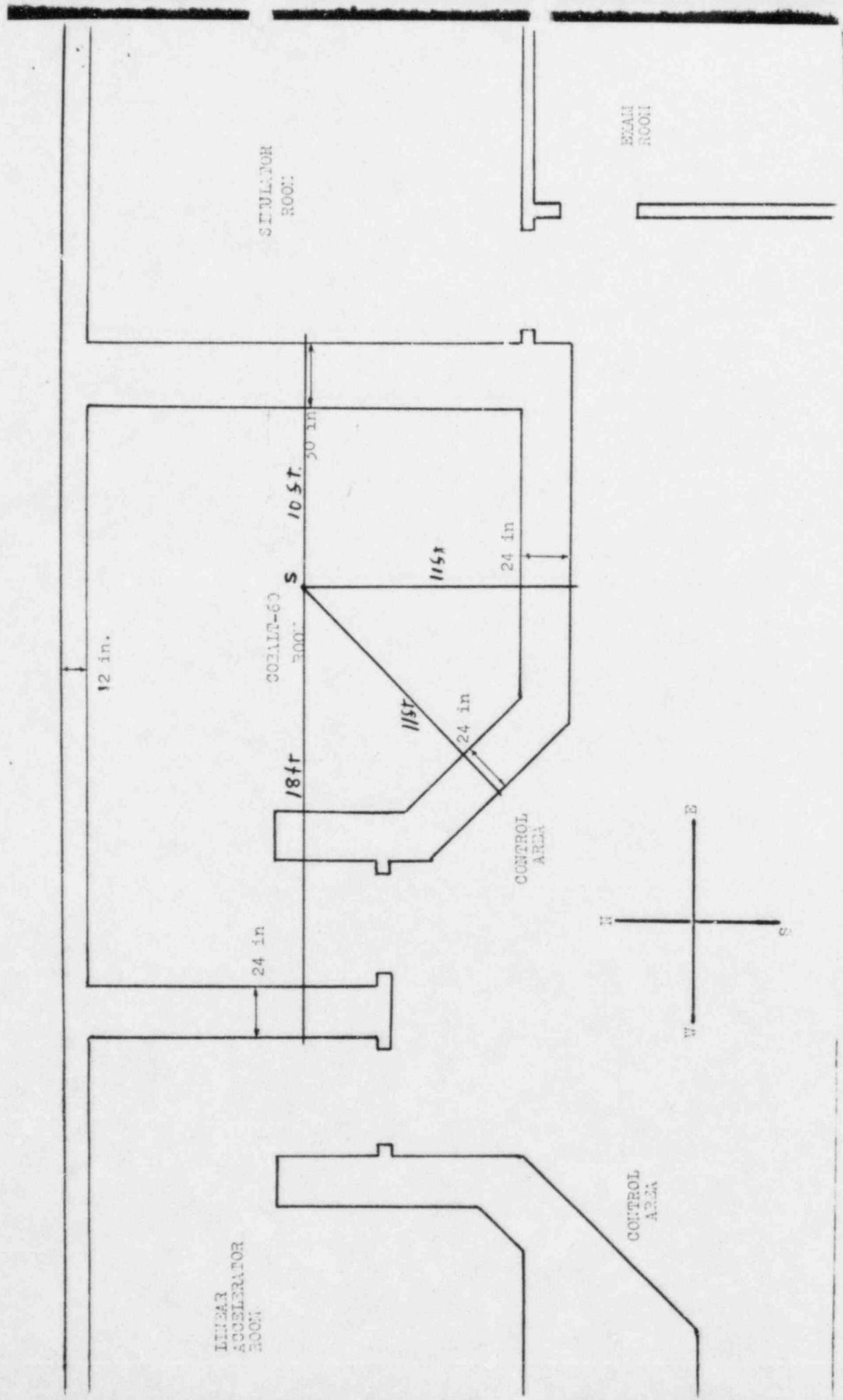
For leakage radiation

$$B_{Lg} = \frac{1000 P (d_{sec})^2}{WT}$$

$$\text{or } B_{Lg} = \frac{P (d_{sec})^2}{40}$$

S in the figure is the source location. Shielding calculations need only to be done along the four radii to walls in the figure plus to the ceiling. This being because the machine can only point at the floor on the north wall and these regions are unexcavated non-accessible areas for which shielding calculations need not be done. The radiation to walls under consideration is scattered or leakage. The area above the room is a non-controlled area; the rest are controlled areas. The distance to the south wall and to the control area is the same, hence their calculations are the same.

The door to the room is specified as having $1/4$ inch lead lining. The lead glass window will have $1/4$ inch lead equivalent.



South wall - Control area

$$d_{\text{sec}} = 11\text{ft.} = 3.35\text{m} \quad d_{\text{scat}} = .8\text{m}$$

Scattered

$$B_{\text{sg}} = \frac{(.1)(3.35)^2(.8)^2}{40a} = \frac{1.79 \times 10^{-2}}{a}$$

$$B_{\text{sg}} \text{ for } 30^\circ = 2.99 \times 10^{-3} \Rightarrow 22 \text{ in concrete}$$

$$\star B_{\text{sg}} \text{ for } 90^\circ = 2 \times 10^{-2} \Rightarrow 10 \text{ in concrete}$$

$$B_{\text{sg}} \text{ for } 135^\circ = 2.99 \times 10^{-2} \Rightarrow 7 \text{ in concrete}$$

Leakage

$$B_{\text{lg}} = \frac{.1(3.35)^2}{40} = 2.8 \times 10^{-2} \Rightarrow 14.5$$

The calculations require 17 inches of concrete. The wall has 24 inches

\star 90° scatter main contribution - shielding based on this

West Wall

$$d_{\text{sec}} = 18 \text{ ft} = 5.5 \text{ m}$$

$$d_{\text{coat}} = .8 \text{ m}$$

scattered

$$B_{\text{sg}} = \frac{(.1)(5.5)^2(.8)^2}{40} = \frac{4.84 \times 10^{-2}}{a}$$

$$B_{\text{sg}} \text{ for } 15^\circ = 8 \times 10^{-3} \Rightarrow 18 \text{ in concrete}$$

$$\star B_{\text{sg}} \text{ for } 90^\circ = 5.38 \times 10^{-2} \Rightarrow 8 \text{ in concrete}$$

$$B_{\text{sg}} \text{ for } 135^\circ = 8 \times 10^{-2} \Rightarrow 6 \text{ in concrete}$$

leakage

$$B_{\text{Lg}} = \frac{.1(5.5)^2}{40} = 7.56 \times 10^{-2} \Rightarrow 18 \text{ in concrete}$$

The calculations require 18 inches of concrete. The wall has 24 inches

\star 90° scatter main contribution - shielding based on this

East wall

$$d_{sec} = 10 \text{ feet} = 3.05 \text{ m}$$

$$d_{scat} = .8 \text{ m}$$

Scattered

$$B_{sg} = \frac{.1 (3.05)^2 (.8)^2}{40 \cdot a} = \frac{1.49 \times 10^{-2}}{a}$$

$$B_{sg} \text{ for } 30^\circ = 2.48 \times 10^{-3} \Rightarrow 22 \text{ in concrete}$$

$$* B_{sg} \text{ for } 90^\circ = 1.65 \times 10^{-2} \Rightarrow 12 \text{ in concrete}$$

$$B_{sg} \text{ for } 135^\circ = 2.48 \times 10^{-2} \Rightarrow 9 \text{ in concrete}$$

Leakage

$$B_{lg} = \frac{.1 (3.05)^2}{40} = 2.32 \times 10^{-2} \Rightarrow 15 \text{ in concrete}$$

The calculations require 18 inches of concrete. The wall has 30 inches.

* 90° scatter main contribution - shielding based on this.

Ceiling

The ceiling height is 9 feet and then there is 36 inches of concrete. The total distance to the room above is 12 feet or 3.66 meters. The source would be at most 2 meters off the floor. Thus $d_{\text{sc}} = 1.66$ meters. $d_{\text{scat}} = .8\text{m}$

Leakage

$$B_{Lg} = \frac{(1000)(.01)(1.66)^2}{40,000 \times \frac{1}{16}} = 1.1 \times 10^{-2} \Rightarrow 18 \text{ in concrete}$$

Scattered

$$B_{sg} = \frac{.01(.8)^2(1.66)^2}{40 \text{ a}} = \frac{4.4 \times 10^{-4}}{\text{a}}$$

$$* B_{sg} \text{ for } 135^\circ = 7.3 \times 10^{-4} \Rightarrow 18 \text{ in concrete}$$

The calculations require 27 inches of concrete. The ~~ceiling~~ ceiling has 36 inches

* 135° scatter only that reach it, for need back scattered radiation to hit ceiling.