

February 10, 1988

Docket Nos. 50-266
and 50-301

DISTRIBUTION:

Docket Files

NRC & Local PDRs

PDIII-3 r/f

KPerkins

DWagner

OGC-WF1

EJordan

JPartlow

ACRS(10)

LICENSEE: WISCONSIN ELECTRIC POWER COMPANY

FACILITY: POINT BEACH NUCLEAR PLANT, UNITS 1 AND 2

SUBJECT: SUMMARY OF FEBRUARY 4, 1988 MEETING

At the request of the licensee, a meeting was held on February 4, 1988 in the Rockville, Maryland offices of the NRC to discuss the licensee's accident reanalysis to support increased allowable core peaking factors at Point Beach 1 and 2. A list of meeting attendees is included in Enclosure 1. The slides used during the presentation are included in Enclosure 2. These slides discuss the goals of the reanalysis effort, the strategy involved in achieving these goals and the potential Final Safety Analysis Report/Technical Specification changes resulting from the reanalysis.

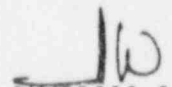
Original Signed By:

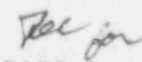
David H. Wagner, Project Manager
Project Directorate III-3
Division of Reactor Projects

Enclosures:
As stated

cc: See next page

Office: LA/PDIII-3
Surname: PKreutzer
Date: 02/11/88


PM/PDIII-3
DWagner/tg
02/10/88


PD/PDIII-3
KPerkins
02/10/88

8802230440 880210
PDR ADOCK 05000266
P PDR

Mr. C. W. Fay
Wisconsin Electric Power Company

Point Beach Nuclear Plant
Units 1 and 2

cc:
Mr. Bruce Churchill, Esq.
Shaw, Pittman, Potts and Trowbridge
2300 N Street, N.W.
Washington, DC 20037

Mr. James J. Zach, Manager
Point Beach Nuclear Plant
Wisconsin Electric Power Company
6610 Nuclear Road
Two Rivers, Wisconsin 54241

Town Chairman
Town of Two Creeks
Route 3
Two Rivers, Wisconsin 54241

Chairman
Public Service Commission
of Wisconsin
Hills Farms State Office Building
Madison, Wisconsin 53702

Regional Administrator, Region III
U.S. Nuclear Regulatory Commission
Office of Executive Director
for Operations
799 Roosevelt Road
Glen Ellyn, Illinois 60137

Resident Inspector's Office
U.S. Nuclear Regulatory Commission
6612 Nuclear Road
Two Rivers, Wisconsin 54241

ENCLOSURE 1

ACCIDENT REANALYSIS TO SUPPORT INCREASED ALLOWABLE CORE PEAKING
FACTORS AT POINT BEACH 1 AND 2

LIST OF ATTENDEES

NAME

AFFILIATION

David Wagner
Summer Sun
Lambros Lois
Y. Gene Hsui
Wayne Hodges
Randall Fieldhack
Harve Hanneman
Bob LaMuro
Janelle Ivey
Beth Hall

NRC
NRC
NRC
NRC
NRC
Wisconsin Electric (WE)
WE
Westinghouse (W)
W
W

NRC/WE/WESTINGHOUSE MEETING
ON
ACCIDENT REANALYSIS
TO SUPPORT
INCREASED ALLOWABLE CORE PEAKING FACTORS
AT
POINT BEACH NUCLEAR PLANT
UNITS 1 AND 2

February 4, 1988

Harv Hanneman (WE)

Bob LaMuro (W)

Randy Fieldhack (WE)

MEETING AGENDA
INCREASED ALLOWABLE CORE PEAKING FACTORS
POINT BEACH NUCLEAR PLANT, UNITS 1 AND 2

February 4, 1988

- | | |
|--|----------|
| I. Introduction/Schedule | WE |
| | |
| II. Non-LOCA Transients | |
| A. Scope of Analyses & Evaluations | <u>W</u> |
| B. Status of Generic WCAP Approval | NRC |
| 1. WCAP-11397 Revised Thermal Design
Procedure (RTDP) | |
| 2. WCAP-11394 WOG Dropped Rod Generic
Methodology | |
| | |
| III. Small-Break LOCA | |
| A. NOTRUMP Analysis | WE |
| B. Reanalysis Strategy | WE |
| | |
| IV. Possible Technical Specification/FSAR
Changes | WE |
| A. Increased Peaking Factors | |
| B. Part-length Hafnium Absorber Assemblies | |
| C. Thimble Plug Removal | |
| D. Increased Steam Generator Tube Plugging | |
| E. Enhanced OFA Fuel Features | |

PURPOSE OF MEETING

- o Present WE's Reasons, Strategy, and Schedule for Requesting a License Amendment to Increase Allowable Core Peaking Factors (F_Q and $F_{\Delta H}$) at Point Beach

- o Obtain Feedback from the NRC Staff on Strategy and Schedule so WE Can Proceed With Desired Fuel Cycle Design and Implementation (Unit 1, Cycle 17 - Spring 1989 Refueling)

- o Resolve Break-Spectrum Issue for Small-Break LOCA Analysis

ACCIDENT REANALYSIS AT INCREASED PEAKING FACTORS

GOALS:

- o Implement Low-Low Leakage Loading Pattern (L4P) Fuel Management Scheme with Part-Length Non-Burnable Absorbers in Peripheral Assemblies to Reduce Reactor Vessel Neutron Fluence
 - Enhance Ability for Additional Twenty (20) Years of Vessel Life
 - Address Current Reactor Vessel Safety Issues (PTS, Low Upper Shelf Material Toughness, Heatup and Cooldown Restrictions) and Uncertainty in Future NRC Requirements (e.g., Proposed Rev. 2 to R.G. 1.99)

- o Implement L4P and Enhanced OFA Fuel Features (e.g., Axial Blankets, High Burnup) to Reduce Fuel Cycle Costs

- o Improve Operational Flexibility
 - Removal of Thimble Plug Devices
 - Increased Steam Generator Tube Plugging

SCHEDULE:

Implement L4P Reload Designs As Follows:

- o Unit 1 - Spring 1989 (Order Fuel - April 1988)
- o Unit 2 - Fall 1989 (Order Fuel - September 1988)

INCREASED PEAKING FACTOR STRATEGY

- o Reanalyze Limiting Transients First (2/15/88)
 - Dropped RCCA ($F_{\Delta H}$)
 - Rod Ejection (F_Q)

- o Complete Reanalysis/Evaluation Effort for Remaining Accidents Including SBLOCA (6/30/88)

- o Coordinate with Upper Plenum Injection/Best-Estimate LOCA Analysis Project

- o Request License Amendment (i.e., Tech Spec Revision) to Allow Increased Peaking Factors (8/31/88):
 1. $F_{\Delta H} = 1.70$
 2. $F_Q = 2.50$
 3. Certain RPS Settings
 - Overtemperature ΔT
 - Overpower ΔT
 4. Control Rod and Power Distribution Limits
 5. DNB Safety Limit Curves
 6. Non-Burnable Absorber Assemblies

- o Reload Core 10CFR50.59 Safety Evaluation (April 1989)
 - Removal of Thimble Plug Devices
 - Insertion of Part-Length Non-Burnable Absorbers in Peripheral Fuel Assemblies

REQUIRED ANALYSES/EVALUATIONS FOR LICENSE AMENDMENT

- o LOCA Reanalysis at Higher F_Q of 2.50
 - Large Break - Best-Estimate WCOBRA/TRAC
 - Small Break - NOTRUMP

- o FSAR Chapter 14 Accident/Transient Reanalysis/Evaluations at Higher $F_{\Delta H}$ of 1.70 (Rod Ejection at F_Q of 2.50)
 - Revised Thermal Design Procedure (RTDP)
(WCAP-11397 Submitted 3/16/87)
 - WOG Dropped Rod Generic Methodology
(WCAP-11394 Submitted 5/22/87)
 - Operational Considerations - Maintain 2000 psia, Up to 14% SG Tube Plugging, Eliminate Thimble Plugs
 - OFA Fuel Enhancements - Higher Burnup, Axial Blanket, IFBAs, DFBN

POINT BEACH
INCREASED PEAKING FACTOR EFFORT
NON-LOCA CONSIDERATIONS

AREAS OF IMPACT

INCREASE IN ALLOWABLE $F \Delta H$

DNB - CRITERIA EVENTS

- o CORE LIMITS/SETPOINTS
- o FLOW TRANSIENTS
- o DROPPED ROD (WCAP 11394)

INCREASE IN ALLOWABLE F_Q

FUEL/CLAD TEMPERATURE CRITERIA EVENTS

THIMBLE PLUG REMOVAL

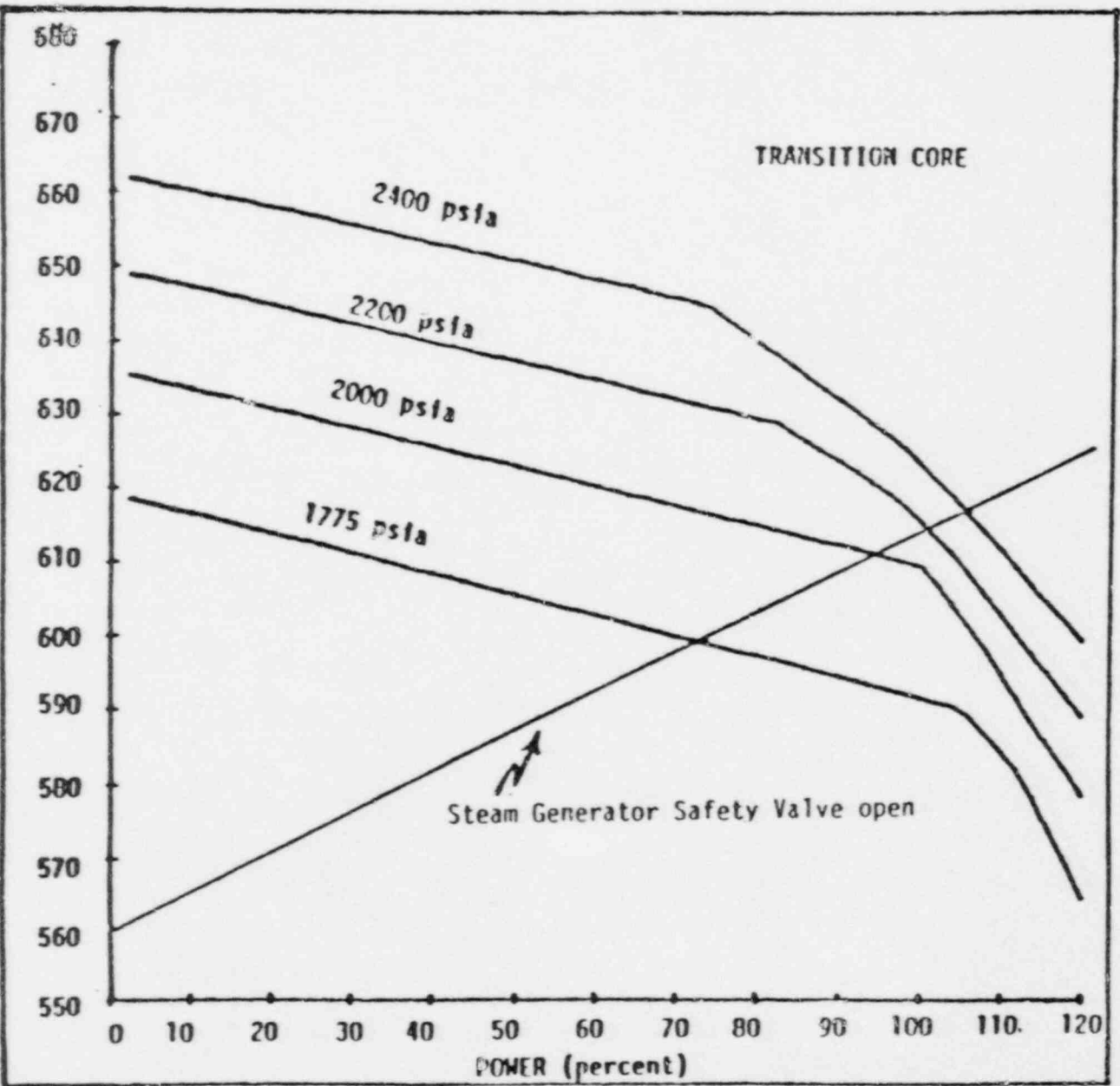
INCREASE CORE BYPASS FLOW

RTDP: REVISED THERMAL DESIGN PROCEDURE (WCAP 11397)

CORE LIMITS/SETPOINTS

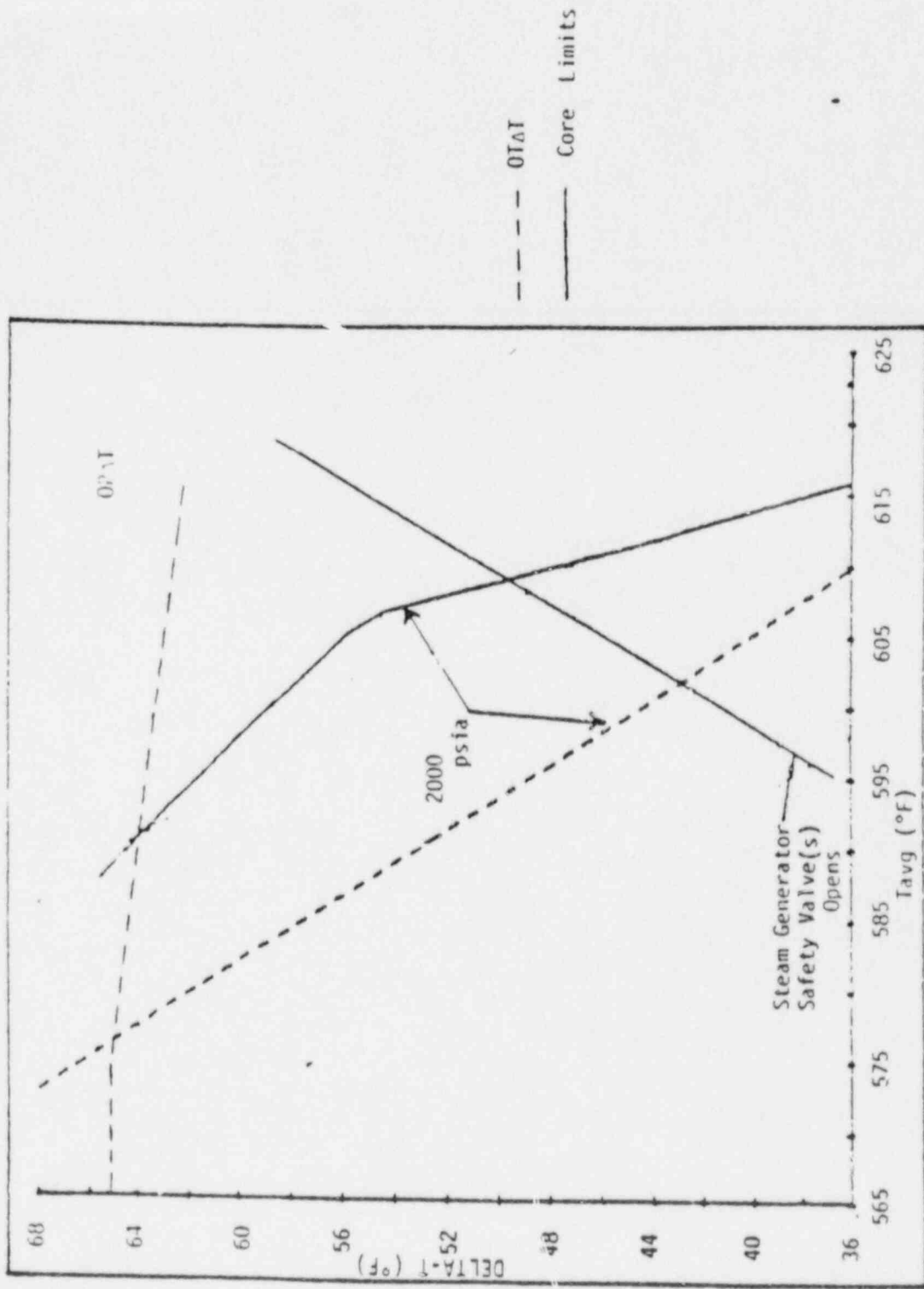
CORE DNB SAFETY LIMITS (TRANSITION CORE)
POINT BEACH UNITS 1 AND 2

Figure 15.2.1-1



T_{avg} - (°F)

FIGURE 14-1
 ILLUSTRATION OF OVERTEMPERATURE AND OVERPOWER ΔT PROTECTION



EVENTS REQUIRING NEW ANALYSIS FOR INCREASED PEAKING FACTORS

<u>EVENT</u>	<u>FSAR</u>	<u>Core Limits</u>	<u>FdH</u>	<u>Fg</u>	<u>Bypass</u>
OTDT/OPDT Setpoint Calculation		X			X
Rod Withdrawal at Power	14.1.2	X			
Rod Withdrawal from Subcritical	14.1.1		X		
Dropped Rod	14.1.3	X			
Boron Dilution at Power at Startup at Shutdown at Refueling	14.1.4	X			
Startup of an Inactive Loop	14.1.5				X
Reduction in Feedwater Enthalpy	14.1.6				
Excessive Load Increase	14.1.7	X			
Loss of Flow	14.1.8		X		
Locked Rotor	14.1.8		X		X
Loss of Load	14.1.9	X			
Loss of Normal Feedwater	14.1.10				X
Station Blackout	14.1.11				X
Steamline Break, Core Response	14.2.5				
, Containment Response	14.2.5				
Rod Ejection	14.2.6			X	

NOTRUMP ANALYSIS

o TMI Requirements

- NOTRUMP Description

WCAP - 10079-P-A, "NOTRUMP: A Nodal Transient
Small Break and General Network Code"

WCAP - 10054-P-A, "Westinghouse Small Break ECCS
Evaluation Model Using the NOTRUMP Code"

- Generic Study

WCAP - 11145-P-A, "Westinghouse Small Break LOCA
ECCS Evaluation Model Generic Study With The
NOTRUMP Code"

o Wisconsin Electric Status

GENERIC STUDY - WCAP-11145-P-A

Assumptions: 2-Loop Plant
Downflow Barrel-Baffle Configuration
0% Steam Generator Tube Plugging
1709 MWt Core Power
2.32 F_Q

<u>Results:</u>	Break Size (inches)	NOTRUMP (PCT)	WFLASH (PCT)
	3	NCU*	1132
	4	796	1713
	6	757	1547

* No Core Uncovery

WFLASH 74 EM

• Earlier Point Beach Analysis:

- Assumptions: Standard Fuel
1518 MWt Core Power
2.32 F_Q
Downflow Barrel-Baffle Configuration

- Results:	Break Size (Inches)	WFLASH (PCT)
	3	1469.
	4	1688.
	6	1167.

• Earlier Prairie Island Analysis:

- Assumptions: Standard Fuel
1709 MWt Core Power
2.32 F_Q
Downflow Barrel-Baffle Configuration

- Results:	Break Size (Inches)	WFLASH (PCT)
	3	1132.
	4	1713.
	6	1547.

WFLASH - OCT 75 EM

o Current Point Beach Analysis

- Assumptions: OFA Fuel
1518 MWt Core Power
2.32 F_Q
44F Steam Generators
Downflow Barrel-Baffle Configuration

- Results:	Break Size (Inches)	WFLASH (PCT)
	4	890.
	6	992.
	8	750.5

o Kori-1 Analysis

- Assumptions: OFA Fuel
1723.5 MWt Core Power
2.32 F_Q
Upflow Barrel-Baffle Configuration

- Results	Break Size (Inches)	WFLASH (PCT)
	4	1163.
	6	1375.
	8	1286.

o R.E. Ginna Analysis

- Assumptions: OFA Fuel
1520 MWt Core Power
2.32 F_Q
Downflow Barrel-Baffle Configuration

- Results:	Break Size (Inches)	WFLASH (PCT)
	4	976
	6	1092
	8	758

NOTRUMP

o Generic Analysis:

- Assumptions: 1709 MWt Core Power
2.32 F_Q
0% Steam Generator Tube Plugging
Downflow Barrel-Baffle Configuration

- Results	Break Size (Inches)	NOTRUMP (PCT)
	3	NCU*
	4	796.
	6	757.

o Prairie Island Analysis:

- Assumptions: 1650 MWt Core Power
2.5 F_Q
10% Steam Generator Tube Plugging
Downflow Barrel-Baffle Configuration
K(Z) Third Line Segment Removal

- Results:	Break Size (Inches)	NOTRUMP (PCT)
	3	NCU*
	4	1000.
	6	NCU*

*No Core Uncovery

COMPARISON OF POINT BEACH AND PRAIRIE ISLAND

NOTRUMP INPUT ASSUMPTIONS

POINT BEACH

1518 Mwt Core Power
2.50 F_Q
1.70 $F_{\Delta H}$
K(2) Third Line Removal
25% SGTP
Upflow Configuration

PRAIRIE ISLAND

1650 Mwt Core Power
2.50 F_Q
1.70 $F_{\Delta H}$
K(2) Third Line Removal
10% SGTP
Downflow Configuration

SBLOCA Reanalysis Strategy

- o Select Expected Limiting Break Size
 - 4" Cold Leg Break

- o Analyze This Break Using NOTRUMP

- o Evaluate For Acceptable Results
 - Criteria: 1. PCT \leq 1600^oF
 - 2. Core Uncovery

BASIS OF PCT CRITERION

A 1600°F PCT Cutoff Will:

- Ensure PCT for All Break Sizes Fall Below the 2200°F Limit:

Two-Loop Plant SBLOCA Analyses Results

Max. Δ PCT Between

<u>Model</u>	<u>Break Sizes</u>
WFLASH 74 EM	600°F
WFLASH 75 EM	340°F
NOTRUMP	40°F

- Prevent Any Significant Zirc-Water Reaction
- Ensure Significant Margin to the 2200°F Limit

POTENTIAL FSAR/TECH SPEC CHANGES

- o Increased Peaking Factors
 - Technical Specification Changes
 1. Core Safety Limits
 2. $OP\Delta T$, $OT\Delta T$
 3. Rod Insertion Limits
 4. F_Q , $F_{\Delta H}$
 5. Third Line Segments, $K(Z)$ Curve
 6. RAOC Band
 - Accident Analyses - Chapter 14 FSAR

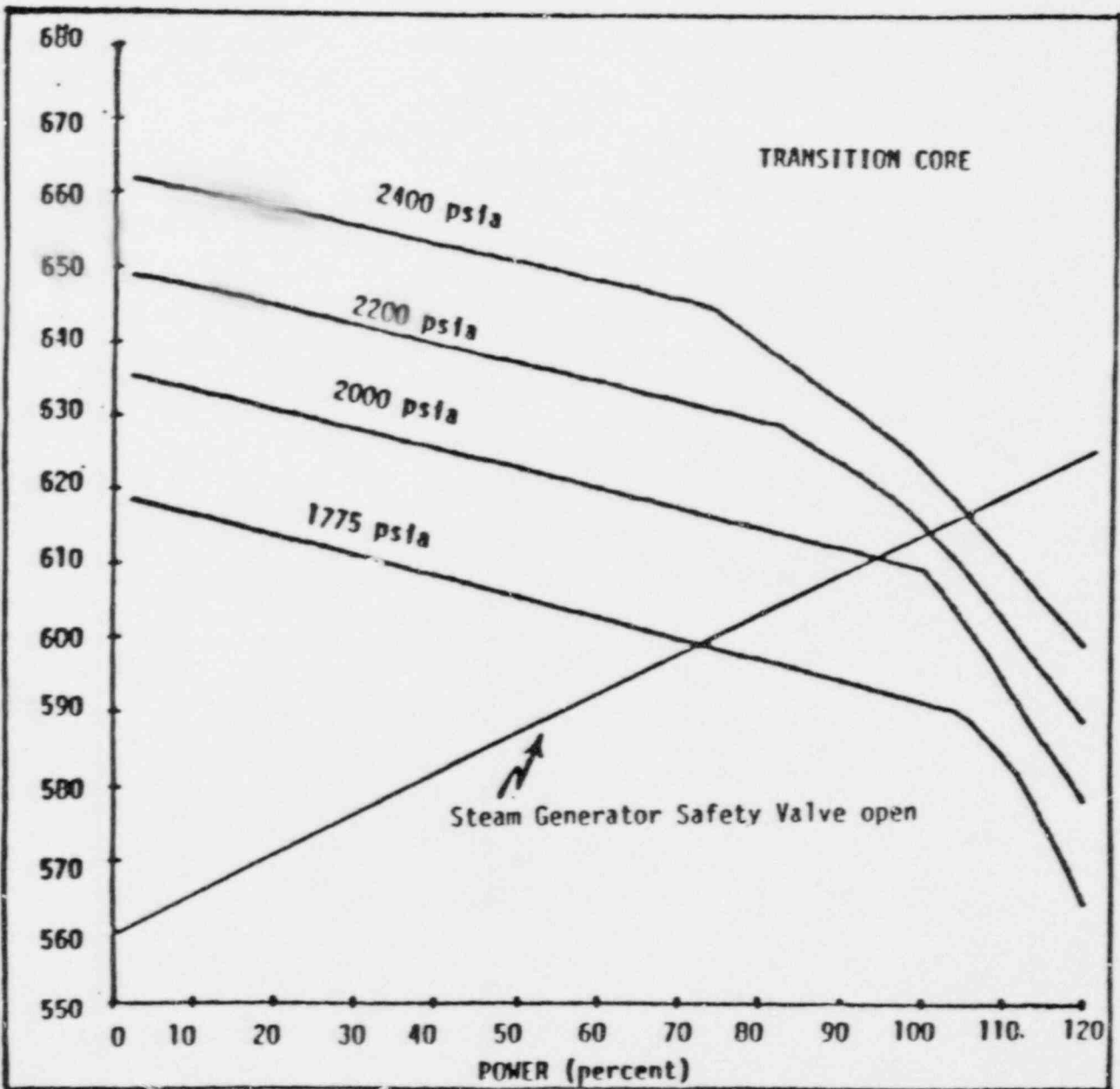
- o Part-Length Absorber Assemblies - Tech Spec Design Features

- o Thimble Plugs - FSAR Change

- o Increased Steam Generator Tube Plugging - Future License Amendment

- o Enhanced OFA Fuel Features
 - IFBA/Axial Blankets - Add to Tech Specs, FSAR
 - Debris Filter Bottom Nozzles - 10CFR50.59 Review
 - Removable Top Nozzles/Higher Burnup - 10CFR50.59 Review

$T_{avg} - (^{\circ}F)$



CORE DNB SAFETY LIMITS (TRANSITION CORE)
POINT BEACH UNITS 1 AND 2

Figure 15.2.1-1

FIGURE 14-1
 ILLUSTRATION OF CVERTEMPERATURE AND OVERPOWER AT PROTECTION

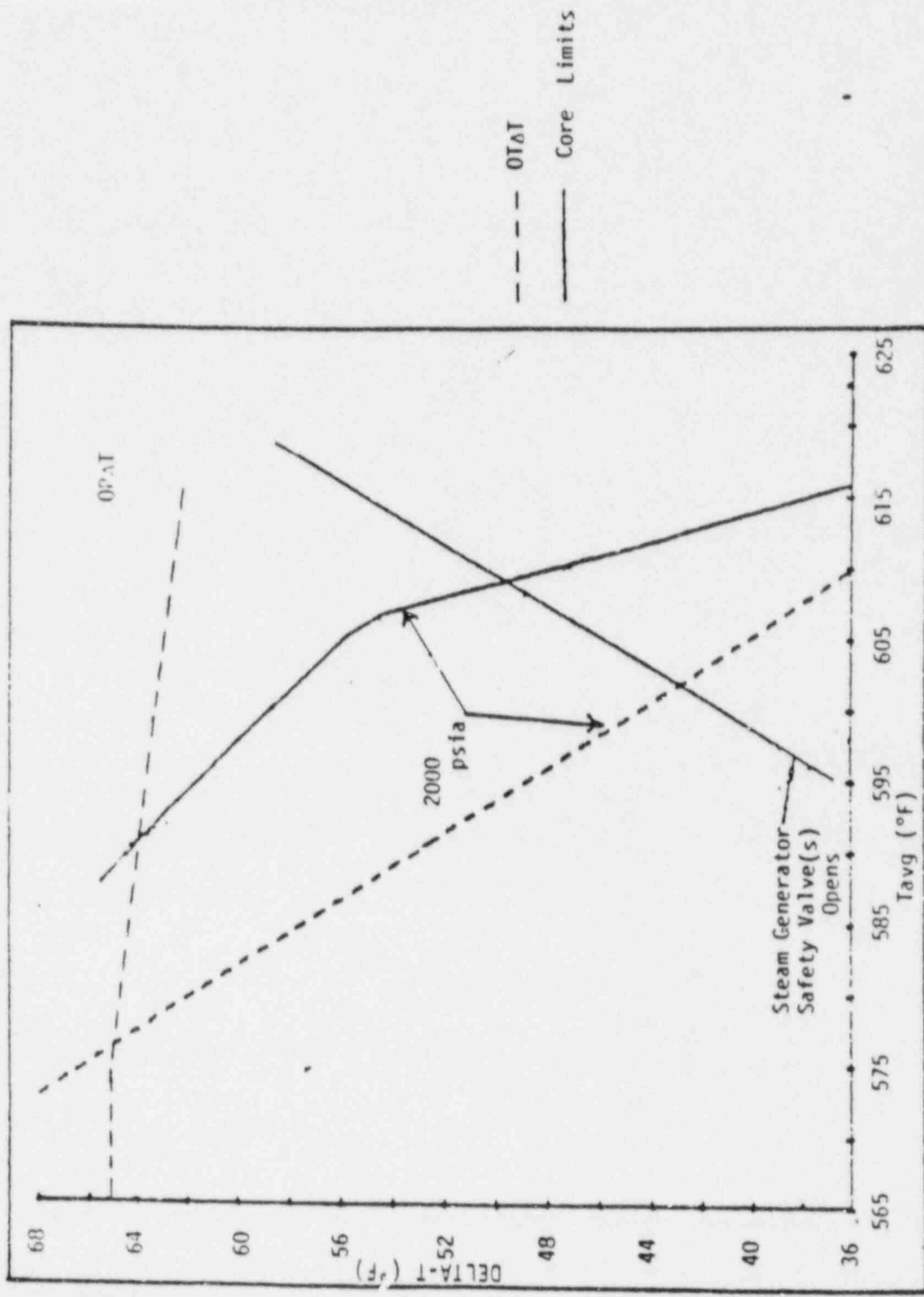
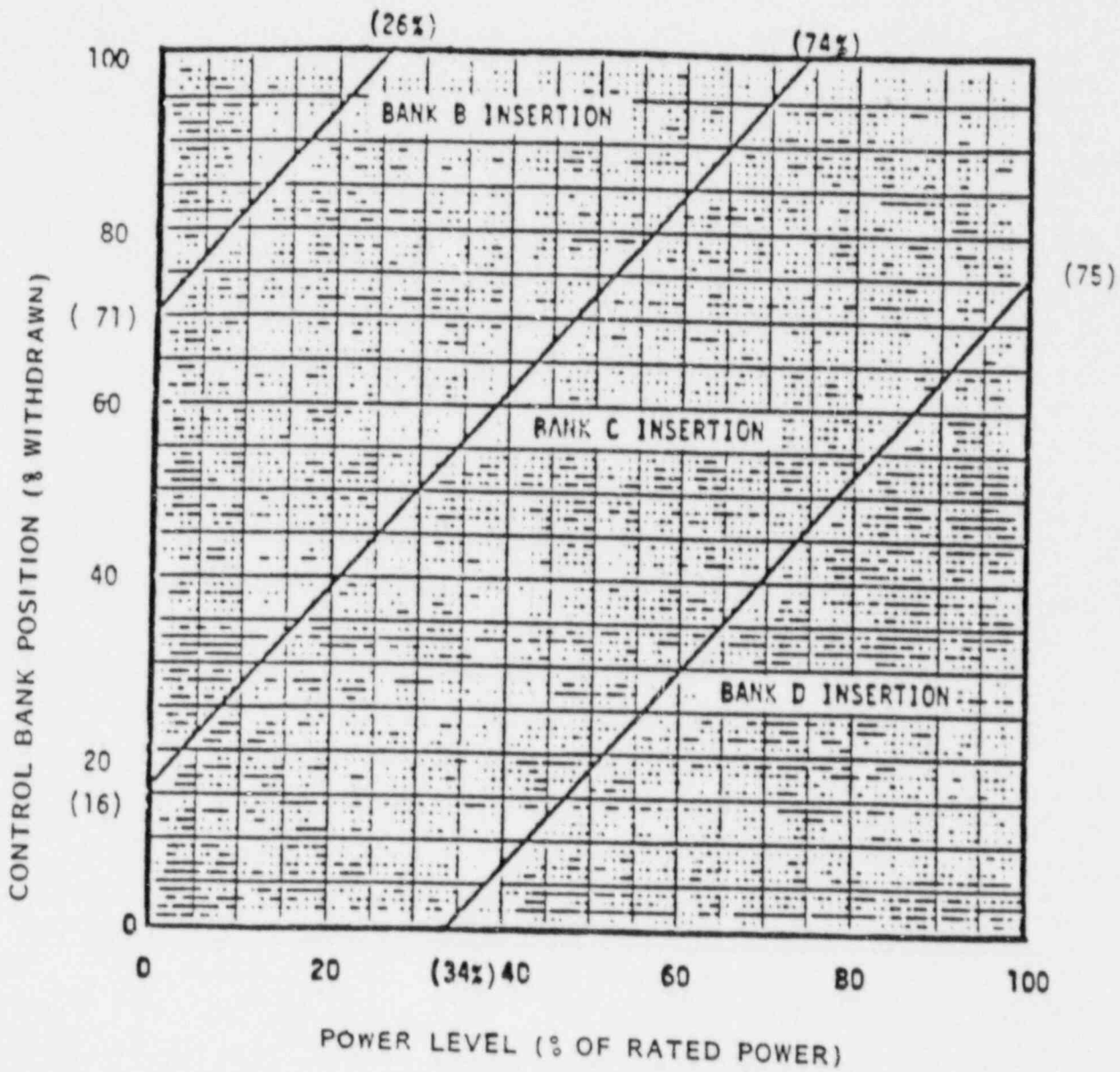


FIGURE 15.3.10-1
 CONTROL BANK INSERTION LIMITS
 POINT BEACH UNITS 1 AND 2



Unit 1 Amendment No. 86
 Unit 2 Amendment No. 90

May 22, 1985
 October 5, 1984

B. Power Distribution Limits

1. a. Except during low power physics tests, the hot channel factors defined in the basis must meet the following limits:

$$F_Q(Z) \leq \frac{(2.21)}{P} \times K(Z) \quad \text{for } P > 0.5$$

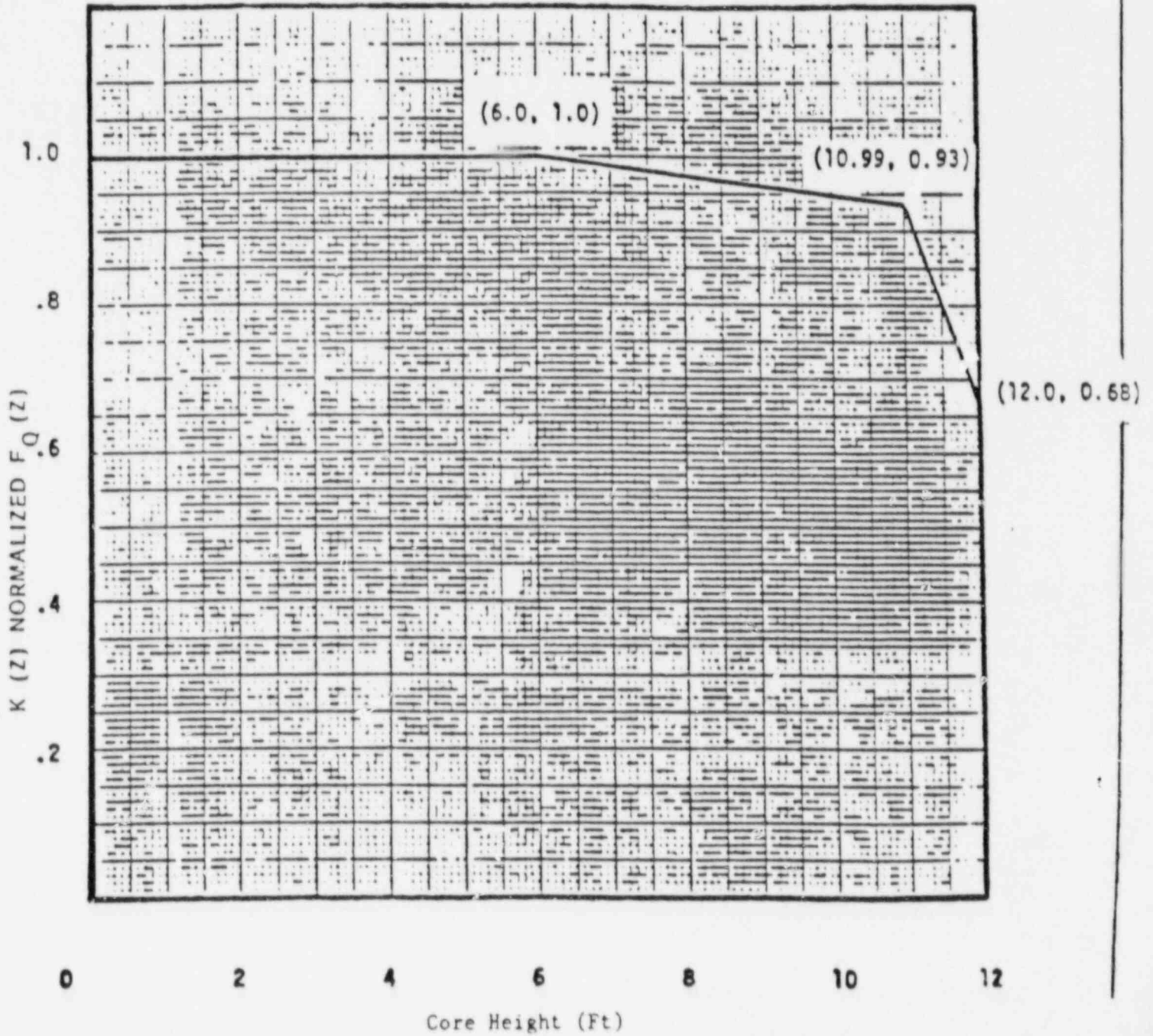
$$F_Q(Z) \leq 4.42 \times K(Z) \quad \text{for } P \leq 0.5$$

$$F_{\Delta H}^N < 1.58 \times [1 + 0.3 (1-P)]$$

Where P is the fraction of full power at which the core is operating, K(Z) is the function in Figure 15.3.10-3 and Z is the core height location of F_Q .

- b. Following a refueling shutdown prior to exceeding 90 percent of rated power and at effective full power monthly intervals thereafter, power distribution maps using the moveable incore detector system shall be made to confirm that the hot channel factor limits are satisfied. The measured hot channel factors shall be increased in the following way:
- (1) The measurement of total peaking factor, F_Q^{Meas} , shall be increased by three percent to account for manufacturing tolerances and further increased by five percent to account for measurement error.
 - (2) The measurement of enthalpy rise hot channel factor, $F_{\Delta H}^N$, shall be increased by four percent to account for measurement error.
- c. If a measured hot channel factor exceeds the full power limit of Specification 15.3.10.B.1.a, the reactor power and power range high setpoints shall be reduced until those limits are met. If subsequent flux mapping cannot, within 24 hours, demonstrate that the full power hot channel factor limits are met, the overpower

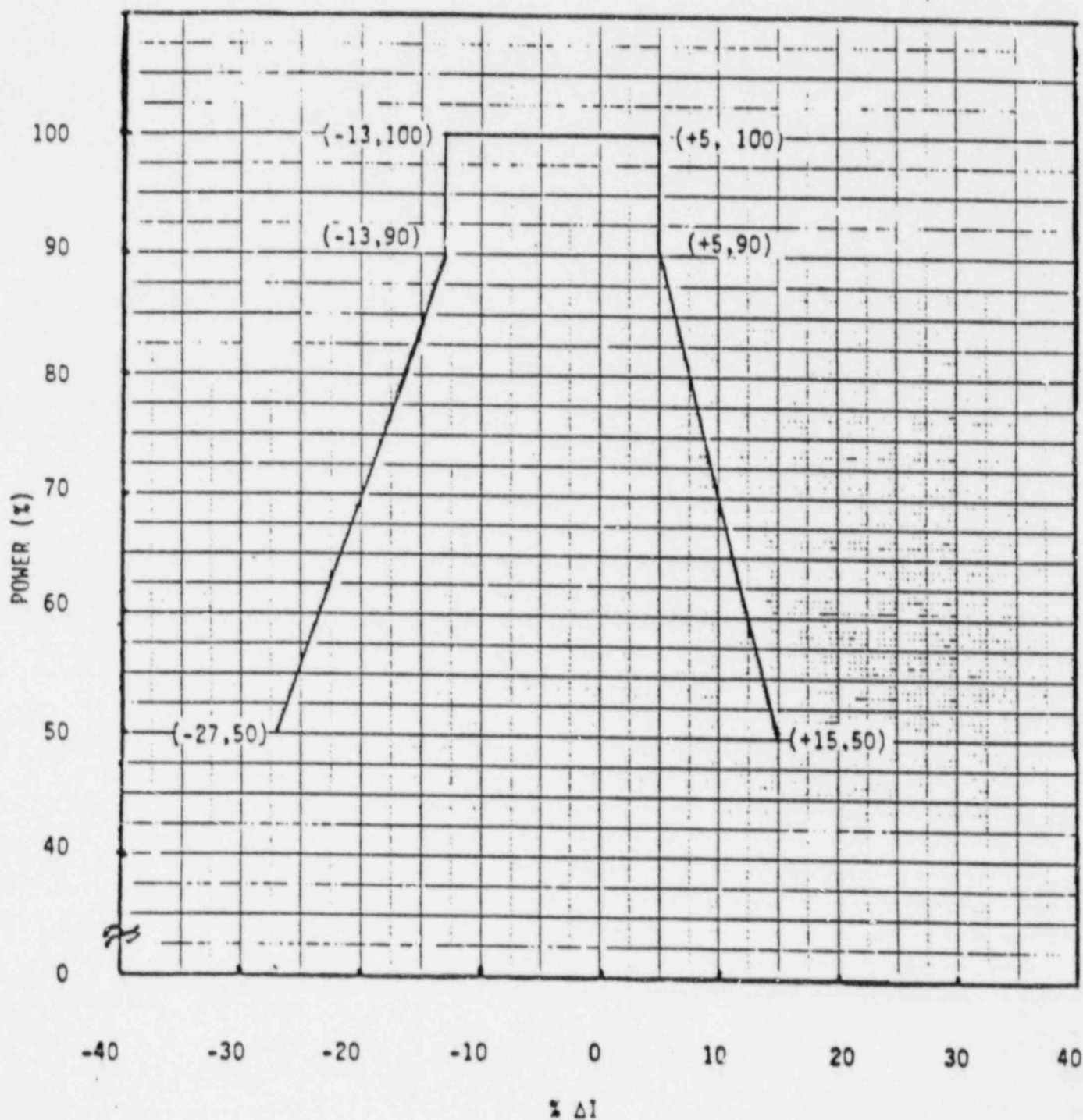
FIGURE 15.3.10-3
POINT BEACH UNITS 1 AND 2
HOT CHANNEL FACTOR NORMALIZED OPERATING ENVELOPE



Unit 1 Amendment No. 86
Unit 2 Amendment No. 90

May 22, 1985
October 5, 1984

FIGURE 15.3.10-4
 FLUX DIFFERENCE
 OPERATING ENVELOPE
 POINT BEACH UNITS 1 AND 2



Unit 1 Amendment 86
 Unit 2 Amendment 90

May 22, 1985
 October 5, 1984

E - POINT BEACH NUCLEAR PLANT, UNITS 1 AND 2

REVISION 7

'88 MAR '88 APR '88 MAY '88 JUN '88 JUL '88 AUG '88 SEP '88 OCT '88 NOV '88 DEC '88 JAN '89 FEB '89 MAR '89 APR '89 MAY '89 JUN '89

