JUSTIFICATION/ANALYSIS

Project No.: 7390-00 Volume: EQ-FSV14 CQD File No.: 027095 Rev. 00: Date 01/29/86

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ANALYSIS & CONCLUSIONS SECTION

Table of Contents

Table of concentry	Page
	-C3-
Objective	C3
References	CA
Assumptions	CA
Equipment Description	C4
Performance Requirements/Acceptance Criteria	CS
Service Conditions	CS
Method of Qualification	C5
DBE Conditions	C7
Similarity Analysis	C7
DBE/Post-DBE Qualification	C8
Thermal Aging Analysis	C13
Cyclic Aging	C15
Accuracy Calculations	C16
Padiation Aging Analysis	C17
Submargance	C17
Submergence	C17
Synergism	C17
Humidity	C17
Chemical Spray	C18
Disposition of Anomalies	C18
Response to IE Builetins/Notices	C19
Maintenance/Surveillance Reduirements	C19
Conclusions	C20
Appendix I	620

CQD No.: 027095 Rev.: 00 Project No.: 7390-00

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Volume No.: EQ-FSV14

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1.0 OBJECTIVE

The purpose of this report is to analyze the subject safety-related equipment for the effect of normal service time/temperature aging, identify age susceptible materials used in the equipment, demonstrate operability of the safety-related equipment during and after a Design Basis Event (DBE), and establish a maintenance and surveillance program. The aging analysis will be performed per DOR Guidelines of IE Bulletin 79-01B.

2.0 REFERENCES

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- Wyle Report #57705-7, Aging analysis of Square 'D' pressure switch and temperature switch models 9012 and 9025 used in Public Service Co. of Colorado's Fort St. Vrain Nuclear Power Plant, Rev. A, dated 11/22/85.
- 2. Wyle Report #58084-2, steam line rupture (SLR) qualification test on pressure differential switch, part #ACW31538B9G1 Class 9012, Serial #271 for General Atomic Company (GAC), dated 8/10/76.
- Wyle Report #57504-10, SLR qualification test on temperature switch Type BCW-42, Class 9025, Form LA16 for GAC, dated 9/14/76.
- CQD File #022959, Rev. 00, "Fort St. Vrain 35 Year Temperature Histogram for Normal Plant Conditions".
- CQD File #027090, "Version IV of DBE Temperature/Humidity Profiles for Reactor and Turbine Buildings" (Preliminary).
- Southwest Research Institute Document #06-6073-TR66, dated 11/84, "Nuclear Component Qualification Test Report Square D 9012-ACW-25 Pressure Switch".
- SWRI Document #06-6073-TR116, dated 11/84, "Nuclear Component Qualification Test Report Square D 9025-BCW-45 Temperature Switch".

8. Durez Bulletin #328.

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	9. "I At Ir	Design Guide for tomics Internati nternational, Do	Reactor Co onal, Divis cument #AI-	ver Gas Elast ion of Rockwe AEC-13145.	omer Seals", 11
	10. Pa	arker O-Ring Han	dbook, date	d 3/82.	
	11. PS Er	SC letter #NDG-8 nvironmental Qua	6-0108 date lification	d 1/23/86 tra Master Equipm	nsmitting ent List.
	12. So	quare D Company lass 9012.	Catalog Sec	tion dated 1/	82,
	13. Sc	quare D Company lass 9025.	Catalog Sec	tion dated 1/	81,
	14. Er Or	ngineering Evalu perating Cycles	ation of Fo #EE-EQ-002,	rt St. Vrain Rev. A, date	Component d 8/21/85.
3.0	ASSUMP	TIONS			
	1. Me ti pi	etals are insens herefore due to roperties are no	itive to en their high t age sensi	vironmental e heat resistan tive.	ffects and ce
	2. No	o internal heat peration is expe	rise above cted (delta	the ambient $d = 0$.	ue to switch
4.0	EQUIPM	ENT DESCRIPTION			
	The sul pressu models	bject of this an re switches. Th and tag numbers	alysis is S e following taken from	quare D tempe is the list Reference 11	rature and of switch :
Tag No.	It	em Description	Manufactu	rer/Model #	Location
PS-8208	B Pr	essure Switch	Square	D/9012-ACW-25	TB2
PS-821	\$		н	9012-ACW-25	TB 2
PS-822				9012-ACW-28	TB2
PC-922	2			9012-ACW-28	TB2
10-0221					
PS-824	7			9012-ACW-25	TB2

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Proj. No. 7390-00	Equip No. See Tab D	Approved by		Data

Tag No.	Item Description	Manufacturer/Model #	Location	
TS-8208	Temperature Switch	Square D/9025-BCW-42	TB 2	
TS-8214		9025-BCW-42	TB 2	
TS-8218	Temperature Switch	Square D/9025-BCW-64	TB 2	
TS-8219		9025-BCW-64	TB 2	
TS-8236		" 9025-BCW-43	TB 2	
TS-8237		" 9025-BCW-43	TB2	
TS-8245		" 9025-BCW-43	TB 2	
TS-8246		• 9025-BCW-42	TB 2	

5.0 PERFORMANCE REQUIREMENTS/ACCEPTANCE CRITERIA

A pre-operational test, operational test during the DBE test, and post-operational test were performed per GAC Specification 93-I-530 to monitor the performance requirements. The tests were conducted as described in References 2 & 3, Page 2. The test specimen operated at all times per GAC Specification 93-I-530 (References 2&3, Pages 3 & 4). Setpoint deviations during the test are evaluated later in Tab C.

6.0 SERVICE CONDITIONS

The subject pressure and temperature switches are located in environmental zone TB2. The time/temperature histogram per Reference 4 for the normal service conditions of Zone TB2 is provided below:

Temperature (^O F)	Duration (days)
105	2723 Period I
95	2756 Period I
105	5040 Period II
95	2160 Period II

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7.0 METHOD OF QUALIFICATION

The Square D pressure and temperature switches are qualified to 79-01B requirements. Therefore, the qualification for thermal aging is done by analysis. The DBE qualification is performed by a combination of type testing and analysis.

- 7.1 Service Life Evaluation
 - All non-metallics that are subject to temperature aging were identified.
 - Utilizing the minimum activation energy value (eV), the amount of required aging at a 105°F reference temperature was calculated based upon the 35 year plant requirements (Reference 4).
 - The life consumed for the entire 30 day DBE/post-DBE period is calculated based on the 105°F reference temperature and added to the results obtained in Step 2 above.
 - 4. Utilizing aging test data (References 6 & 7) the qualified life is calculated at a 105°F reference temperature and compared to the results obtained in Step 3 above.
- 7.2 DBE/Post-DBE Evaluation

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- High temperature peaks postulated for the plant DBE are enveloped by the test with significant margin.
- Operability for the duration of the SLR test was demonstrated by successful functional testing during the DBE simulation and post-DBE functional testing.
- Qualification after the termination of the SLR test is demonstrated by analysis of thematerials and their specific properties relative to their contribution to switch operation.

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Proj. No. 7390-00	iquip No. See Tab D	Approved by	Alter John	Dete

4. The thermal stress induced during the entire DBE at a reference temperature of 105°F is calculated in Appendix I to verify that the total thermal stress induced during the entire DBE/post-DBE is a fraction of the gualified life.

8.0 DBE CONDITIONS

Per Reference 5, the following are the DBE conditions (combined line break profile) for the Square D temperature and pressure switches:

Temperature (^O F)	Duration (minutes)
100-200	0.03
200-300	0.07
300-330	0.05
360-360	0.10
330-300	0.05
300-160	0.70
160-170	0.50
170-170	1.40
170-185	4.60
185-195	9.50
195-170	53.0
170-150	50.0
150-120	380.0
120-120	42700.0

Total 30 days

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9.0 SIMILARITY ANALYSIS

Square D temperature switch Model 9025 and pressure switch Model 9012 (which were DBE tested) are similiar to the Square D temperature and pressure switches installed at the Fort St. Vrain Plant, since the tested and installed switches are the same model with the same materials of construction. Furthermore, the materials application for both the Square D temperature and pressure switches is the same even though the model numbers are different. The following are the non-metallic materials in the Model 9025 Square D temperature switch and the Model 9012 pressure switch:

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SARGENT & LUNDY	Square D Pressure X Selety-Related	& Temp. Switches	Rev. 00	Date
Client Public Service	e Co. of Colorado	Prepared by		Dete
Project Fort St. Vrain	1	Reviewed by		Date
Proj. No. 7390-00	iquip No. See Tab D	Approved by	and the set	Dete

Snap switch insulator - Phenolic Gasket - Silicone Rubber

The remaining parts of the temperature and pressure switches are metallic and, therefore, are not age sensitive.

- 10.0 DBE/POST-DBE QUALIFICATION
 - 10.1 DBE

The test specimen was subjected to a 30 minute DBE test. Qualification for the DBE will be justified by performing a comparison of the tested and plant profiles. The plant and tested DBE profiles are shown in Figures 1 & 2. The test specimens were subjected to SLR testing, per Reference 2, Figure 2, Page 17 and References 3, Figure 2, Page 16 as follows:

 Test Profile for Pressure Switch Model 9012 (Reference 2, Page 17)

Temperature (^O F)	Duration (Minutes)
110-440	1
440-504	1
504-515	1
515-504	1
504-311	1
311-310	8
310-264	7
264-252	10

 Test Profile for Temperature Switch Model #9025 (Reference 3, Page 16)

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Client Public Service	Co. of Colorado	Prepared by		Date
Project Fort St. Vrain		Reviewed by		Date
Proj. No. 7390-00	iquip No. See Tab D	Approved by		Deta

Temperature (^O F)	Duration (Minutes)
185-470	1
470-516	1
516-526	1
526-504	1
504-330	1
330-328	1
328-328	4
328-316	2
316-304	2
304-284	2
284-270	4
270-240	10

Referring to Figures 1 & 2 which graphically depict both the tested and the plant DBE profiles it can be seen that for the first 30 minutes the tested peak temperature (approx. 520°F) envelopes the plant peak temperature of (approx. 360°F) with significant margin. The tested peak temperature duration at 520°F also envelopes the plant peak temperature duration at 360°F. Although a mismatch in rise times exists between the plant and tested profiles for the initial transient, which can be attributed to test facility limitations, this mismatch can be considered negligible based on the following justification:

- The tested switches were wrapped with 3 inches of insulation. The plant switches are required to be wrapped with 3 inches of insulation per Tab E.
- Switch internals that are housed in a NEMA type 13 enclosure, wrapped in 3 inches of insulation, cannot be significantly affected by the short duration accident peak temperature.
- 3. The switch internal temperature rise would be higher due to a 44 second temperature rise to 520°F. (tested) than a 9 second rise to 360°F (plant).



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Client Public Service Co. of Colorado Project Fort St. Vrain		Prepared by	Data
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 The switch internal temperature would rise more due to the test duration at 520°F than the 6 second plant duration at 360°F.

Considering the construction of the temperature and pressure switches, the non-metallic internals, i.e. phenolic and silicone rubber that are housed in a NEMA type 13 enclosure, the thermal conditions imposed by the tested profile are more severe than those that would be imposed by the plant profile.

Therefore, based on the above discussion, it is concluded that the thermal stress experienced by the tested switches is more severe than the thermal stress the switches would see during the initial plant transient despite the mismatch in rise times. This is documented in Sargent & Lundy CQD File #027843 and is available for audit purposes.

Discussion of the post-DBE including material analysis follows:

10.2 POST-DBE QUALIFICATION

Per the manufacturers' published data (References 12 & 13), the switches are designed for a continuous ambient temperature of 185°F. The maximum post-DBE temperature (decaying to ambient) postulated for the plant is 185°F. Furthermore, the Square D pressure and temperature switches have successfully performed their saftey function at the 5, 15 and 25 minute intervals during the DBE and post-DBE (References 2 & 3). Operability after the DBE is demonstrated by the post-DBE functional test. In addition, research of the phenolics listed in the EPRI material data base has revealed a minimum continuous threshold temperature of 143°C (289°F), irrespective of the phenolic's failure mode (Reference 8). The phenolic material which is used as an insulator in the Square D switches has a corresponding failure mode attributed to a loss of flexural strength for it's specific application. Thirty (30) minutes into the DBE, the phenolics are not thermally stressed since the maximum temperature after 30 minutes into the DBE is 190°F which is siginificantly less than the 289°F minimum continous threshold temperature stated above. Since it has been demonstrated that the

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Client Public Service Co. of Colorado		Prepared by		Date
Project Fort St. Vrain		Reviewed by		Dete
Proj. No. 7390-00	Equip No. See Tab D	Approved by		Dete

properties of phenolics do not change at 289°F or below, which envelopes the post-DBE requirements of the plant, it is concluded that the phenolics will maintain their physical properties during the entire 30 day DBE/post-DBE.

In an application, similar to that for the switches, the silicone rubber maintained its 90% compression set even after exposure to a temperature of 505°F (Reference 9). Further evidence of silicone rubber's ability to retain its retention property as a static seal is provided by Parker Seal This material resists 700°F temperatures Company. for short periods and would maintain the desired material property (compression set) for 1,000 hours at 450°F (Reference 10, Page A3-36). Therefore, based upon the above and the knowledge that the silicone rubber is held in compression, it is also concluded that the silicone rubber will maintain its physical properties during the entire 30 day DBE/post-DBE.

Demonstration of the switches capability to perform their intended safety function for the post-DBE is supported by References 6 & 7. In these references both the Square D temperature and pressure switches were aged at $125^{\circ}C$ ($257^{\circ}F$) for 108 continuous days. After this thermal aging period, operability was verified. This more than adequately envelopes the plant post-DBE requirements (time and temperature).

Based upon the above discussion, it is concluded that during the 30 day DBE/post-DBE period, the change in physical properties for the non-metallics is negligible. The switches are capable of performing the intended safety function during the entire 30 day DBE/post-DBE period.

11.0 THERMAL AGING ANALYSIS

The Arrhenius model is utilized in the evaluation of the switch's service life. The service temperature during normal operation of the plant varies between 95°F and 105°F in the turbine building. The Arrhenius parameters provided in Table 1, Page 7, Reference 1 will be used to

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SARGENT & LUNDY	Cola For Environmenta	A Temp, Switches	Calc. No. CQD-027095
CHICAGO	X Safety-Related	Non-Sefety-Related	Page C14 of
Client Public Service Co. of Colorado Prepared by		Dete	
Project Fort St. Vrain		Reviewed by	Data
Proj. No. 7390-00	iquip No. See Tab D	Approved by	Ceta

determine the qualified life of the non-metallic materials of the Square D temperature and pressure switches. Arrhenius parameters used for the following non-metallic materials in the subject switches are:

1.	Phenolic ($\emptyset = 0.64 \text{ ev}$)	S = 7396.48	S = Slope
	(Snap Switch Insulator)	I = -8.96	I = Intercept
2.	Silicone Rubber ($\emptyset = 0.86 \text{ eV}$)	S = 9987.54	Ø = Activation
	(gasket)	I = -18.39	Energy (eV)

Utilizing of the Arrhenius equation in the following form:

$$t_{AG} = t_{SER} \exp \left[\frac{g}{\kappa} \left(\frac{1}{T_{AG}} - \frac{1}{T_{SER}}\right)\right]$$

Where:

 t_{AG} = time of aging in hours t_{SER} = time of service in hours T_{AG} = Temperature of aging in degrees Kelvin T_{SER} = Service temperature in degrees Kelvin. \emptyset = Activation Energy (eV) k = Boltzmann's constant = 8.617 x 10⁻⁵ eV/°K

Therefore, the qualified life can now be determined for the phenolic in the subject switches. If the qualified life of the phenolic is greater than 35 years in the TB2 zone, then the silicone rubber is likewise qualified for at least that period since the phenolic is the weak link material, i.e., lowest eV value.

11.1 Required Aging at 105°F Reference Temperature for the 35 Year Plant Life (Reference 4)

> As indicated in Section 6.0 of Tab C, the TB2 environmental zone has the following time/temperature histogram during the plant 35 year service life:

Temperature (^O F)	Total Duration (days)
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105	7,763
95	4,916

For the phenolic, the required equivalent aging at 105°F for satisfying the plants' 35 year histogram is as follows:

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Client Public Service Co. of Colorado		Prepared by	Dete
Project Fort St. Vrain Reviewed by			Date
Proj. No. 7390-00	iquip No. See Tab D	Approved by	Dete

The equivalent duration for the Phase I period (i.e., from January 1, 1974 to December 31, 1988 at 105^oF is given by:

 $\frac{2723+2756 \times \exp \left[\frac{0.64\times10^5}{8.617} \left(\frac{1}{313.555} - \frac{1}{308}\right)\right]}{365.25}$ = 12.38 years at 105°F

Similarly, the equivalent duration for the Phase II period (i.e., from January 1 1989 to September 17, 2008) at 105°F is given by:



= 17.66 years at $105^{\circ}F$

Therefore, the total required aging of the phenolic is:

12.38 + 17.66 = 30.04 years at $105^{\circ}F$

11.2 Equivalent Time Demonstrated by Thermal Aging

Per References 6 & 7, a Square D pressure and temperature switch were each aged at 125°C (257°F) for 108 days. Shown below is the equivelency of this aging period at 105°F using the Arrhenius methodology:

Phenolic - (Life Consumed in 30 day DBE/post-DBE = 0.16 years at 105°F per Appendix I)

Actual Aging = $\frac{108 \times \exp \left[\frac{0.64 \times 10^5}{8.617} \left(\frac{1}{313.555} - \frac{1}{398}\right)\right]}{365.25}$

= 45.03 years at 105°F

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The 35 year plant life (TB2 zone) plus the 30 day DBE/post-DBE consume a total of 30.04 years + 0.16 years = 30.20 years at 105°F. Since the thermal aging temperature of 125°C for 108 days equates to 45.03 years at 105°F, the combined plant normal service conditions plus 30 day DBE/post-DEE period aging requirements are enveloped.

12.0 CYCLIC AGING

Per Reference 14, the maximum cyclic requirements for both 9012 and 9025 switches is 2191 during the 35 year service life. A total of 6210 cycles of operation under inductive loading conditions was performed on both the 9012 and 9025 switches. The test items functioned normally at the conclusion of the operational aging (References 6 & 7). Therefore the tested conditions envelope the plant requirements.

13.0 ACCURACY CALCULATIONS

 9012 Pressure Switch (Reference 2, Page 13) The set point pressure for "open" position was = 5.6 psi. The maximum deviation ouring DBE and post-test operation check was - 0.4 psi.

So the percentage deviation fc = "open" position for DBE was = $-0.4 \times 100 = -7.24$ % 5.6

Similarly for "close" position the percentage deviation for the DBE was = $-0.3 \times 100 = -5$ 3.0

So the deviations in the setting pressure during the DBE are as follows:

Open + 0 - 7.14% Close + 0 - 6%

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SARGENT&LUNDY	Square D Pressure	& Temp. Switches	Rev. 00	Dete
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Client Public Service Co. of Colorado Propered by		Prepared by		Data
Project Fort St. Vrain		Reviewed by		Data
Proj. No. 7390-00	iquip No. See Tab D	Approved by		Deta

2. 9025 Temperature Switch (See Reference 3, Page 13) The set point temperature for "open" position was = 206.67°F (average). The maximum deviation during DBE and post-test operation check was + 10.33°F and - 6.0°F.

So the percentage deviation for "open" position for DBE was

= + $\frac{10.33 \times 100}{206.67}$ and - $\frac{6 \times 100}{206.67}$ i.e. + 5% and - 3%

The set point temperature for "close" position was $177.33^{\circ}F$ (average). Similarly for "close" position the percentage deviation for the DBE was $+ 0.66^{\circ}Fx100$ and $- 2.66^{\circ}Fx100$ i.e. +0.5% and -1.5% 177.33

So the deviations in the setting temperature during the DBE are as follows:

Open + 5% - 3% Close = + 0.5% - 1.5%

The above deviations during DBE shall be incorporated into the normal calibration procedures for Fort St. Vrain. See Tab E.

14.0 RADIATION AGING ANALYSIS

The process fluid (steam or feedwater) is not contaminated, and therefore, no radiological concerns are directly associated with the DBE. Design Basis Accident No. 1, "Permanent Loss of Forced Circulation", discussed in the Appendix D of the FSAR, provides the worst case radiological conditions, but the overall radiological concerns are minimal, and accumulated doses (less than 1000 rads, TID) would have no operational effect on the equipment.

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Client Public Service Co. of Colorado Prepared by		Prepared by	Dete
Project Fort St. Vrain	n	Reviewed by	Date
Proj. No. 7390-00	iquip No. See Tab D	Approved by	Dete

15.0 SUBMERGENCE

All switches are above the turbine building Flood level. Therefore submergence is not applicable.

16.0 SYNERGISM

No synergistic effects are presently known to exist for the non-metallic materials of construction of the Square D temperature and pressure switches.

17.0 HUMIDITY

During the DBE, the humidity level can reach 100%. In order to maintain the qualification of the switches, a qualified seal at the conduit entrance is required. See Tab E.

18.0 CHEMICAL SPRAY

Chemical spray is not utilized at Fort St. Vrain.

19.0 DISPOSITION OF ANOMALIES

- Per Reference 2, the chamber pressure was monitored during the test and was found to be within + 0.5 psi limits. This was considered satisfactory and was waived by GAC personnel as a continuing system requirement.
- Per Reference 3, the following deviations were identified:
 - a) During the visual inspection, it was noted that the specimen part number was BCW42, Class 9025, Form LA16 instead of BCW43 as listed in Paragraph 5.1 of GAC Specification 93-I-530.

Both the part number BCW42 and BCW43 are similar, having the same materials of construction and therefore this deviation is insignificant.

b) The deviation mentioned on Page 22 of Reference 3 concerning the wrapping of the specimen with 3 inches of fiber glass insulation is considered a test set-up anomaly. The probe capillary tubing and specimen was wrapped with 3 inches of fiber

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20.0	The Squ temperative the test during switch which h after est Since to less se anomaly 9025 Sc RESPONS Not app	inches) between rupture simulation are D switches will ature of 360°F for it specimen was exp the DBE simulation (9012 and 9025 Squ ad no such wrappin exposure to acciden the plant peak accident the plant peak accident vere than the test vis judged not to guare D temperature SE TO IE BULLETINS, plicable, since no	the specimen and th lon entrance. Il be exposed only t 6 seconds during th bosed to temperature h. The 9012 Square hare D have the same of has successfully it temperatures abov ident temperature is ted peak DBE tempera impact the qualific e switches. /NOTICES IE Bulletins have b	e stream- o a peak e DBE whe s above S D pressur material operated e 500°F. signific ture, thi ation of	-line ereas 500°F re ls) even cantly is the
21.0	date.	NANCE/SUBVETLLANCE	REQUIREMENTS		
21.0	1. 1	The set point devia DBE test must be in calibration procedu	ations that occurred ncorporated in to th ures. See Tab E.	during t e normal	the plant
	2. 1	All the Square D so qualified seal at	witches must be seal the conduit entrance	ed with a	ab E.
	3.	The 9012 pressure is witches must be wighted by a second strain of the second strain of the second strain second s	switches and 9025 te rapped with 3 inches nd sealed with fiber	of fiber glass re	sin.
22.0	CONCLUS	SIONS			
	The sul (Models Nuclear Bullet: DBE pro	oject Square D tem 9012 and 9025) is Power Plant are in 79-01B requirem ovided the mainten "E" are implement	perature and pressur nstalled at PSC's Fo qualified to DOR Gui ents for 35 years pl ance and surveillance ed.	e switche ort St. V delines o us DBE/po e require	es rain of IE ost- ements

S - wert

Form GO 3 06.1 Rev. 2

	Cala For Environment	al Qualification of	Cale. No. CQD-027
SARGENT&LUNDY	Square D Pressure	& Temp. Switches	Rev. 00 Date
CHICAGO	X Safety-Related	Non-Selety-Related	Page C20 of
Clant Public Service Co. of Colorado		Prepared by	Date
Project Fort St. Vrain		Reviewed by	Dete
Proj. No. 7390-00	coup No. See Tab D	Approved by	Deta

APPENDIX I

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	Cola For Environmenta	al Qualification of	Celc. No.	CQD-02709
SARGENT & LUNDY	Square D Pressure	& Temp. Switches	Rev. 00	Date
	X Sefety-Related	Non-Safety-Related	Page C21	et
Client Public Service Co. of Colorado		Prepared by		Date
Project Fort St. Vrain		Reviewed by		Date
Proj. No. 7390-00 zquip. No. See Tab D Approved by				Dete

PURPOSE:

The purpose of this appendix is to calculate the equivalent durations at the normal operating conditions for different materials for the entire 30 day DBE/post-DBE.

CALCULATION AND RESULTS

The thermal calculations are based upon the Arrhenius methodology namely,

$$\frac{1}{k} = \frac{1}{T_{EO}} = \frac{1}{T_{DBE}}$$

 $t_{EO} = t_{DBE}e$

where

T_{EQ} = Reference temperature in ^OK T_{DBE} = DBE temperature in ^OK t_{EQ} = Equivalent duration t_{DBE} = DBE duration Ø = Limiting activation energy (eV) K = Boltzmann's Constant (8.617x10⁻⁵ eV/^OK)

S were

ENTER K.F. OR C FOR TEMPERATURE UNITS XE ENTER S.M.H.D. OR Y FOR DURATION UNITS >M IS IT A RAMP? (Y/N) YC ENTER SPLIT-UP FACTOR (DEFAULT IS 1000) \$9999 ENTER AGING TEMPERATURE >105 ENTER ACTIVATION ENERGY VALUE >0.64 ENTER BEGINNING TEMP., ENDING TEMP., DURATION ENTER END WHEN COMPLETE >100,200,0.03 >200.300.0.07 >300,330.0.05 >330.300.0.05 >360,360,.0=<01>0=<0>'X >360,360,0.10 >300,160.0.70 >160.170.0.50 >170,170,1.40 >170,185,4.60 >185,195,9.50 >195.170.53.00 >170,150,50.00 >150.120.380.0 >120,120,42700 END

EQUIVALENT DURATION AT 105.00F IS 82023.67 MINUTES

ENTER M FOR MENU PRINT-OUT OR ENTER ACTIVITY NUMBER

>M

ENTER ACTIVITY NUMBER 1) DEFINE PROFILE TYPE 6) BEFINE ACTIVATION ANERGY RUN ID : UAKB DATE : 01/13 Page C22

- Calculation for phenolic for the entire 30-day plant DBE.
- The equivalent number of years at 105°F for the entire 30-day plant DBE is 0.16 yrs.

Page C23

@XQT OPS\$*095ABSOLUTES.AGE095249101 ENTER PROJECT NUMBER >739000 PROJ. NO. : 739000 PROG. NO. : 09.5.249-1.01 .../86

ENTER K.F. OR C FOR TEMPERATURE UNITS >F ENTER S.M.H.D. OR Y FOR DURATION UNITS >M IS IT A RAMP? (Y/N) >Y ENTER SPLIT-UP FACTOR (DEFAULT IS 1000) >9999 ENTER AGING TEMPERATURE >105 ENTER ACTIVATION ENERGY VALUE >0.86 ENTER BEGINNING TEMP., ENDING TEMP., DURATION ENTER END WHEN COMPLETE >100.200.0.03 >200,300,0.07 >300.330.0.05 >360,360,0.10 >330,300.0.05 >300,160,0.70 >160,170,0.50 >170.170.1.40 >170,185,4.60 >185,195,9.50 >195,170,53.00 >170,150,50.00 >150,120,380.00 >120,120,42700 * >END X END

RUN ID : DAKB DATE : 01/14

14.

-)

 Calculation for silicone rubber for the entire 30-day plant DBE.

Aunt

 The equivalent number of years at 105°F for the entire 30-day plant DBE is 0.20 yrs.

EQUIVALENT DURATION AT 105.00F IS 106628.2 MINUTES

>195,192,13.0 >END

A. witt

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EQUIVALENT DURATION AT 105.00F IS 933.7639 MINUTES

ENTER M FOR MENU PRINT-OUT OR ENTER ACTIVITY NUMBER

>9

CURRENT AGING TEMPERATURE = 105.00F CURRENT ACTIVATION ENERGY = .64 CURRENT SPLIT-UP FACTOR = 9999 TIME UNIT IS MINUTES

ENTER N FOR MENU PRINT-OUT OR ENTER ACTIVITY NUMBER

10

>005KIP 30 >0FIN *TERMINAL INACTIVE* >00TERM Page C24

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