### 5.5 Programs and Manuals

5.5.11	Safety Function Determination Program (SFDP) (continued)
	<ol> <li>A required system redundant to system(s) supported by the inoperable support system is also inoperable; or</li> </ol>
	<ol> <li>A required system redundant to system(s) in turn supported by the inoperable supported system is also inoperable; or</li> </ol>
	<ol> <li>A required system redundant to support system(s) for the supported systems (b.1) and (b.2) above is also inoperable.</li> </ol>
	c. The SFDP identifies where a loss of safety function exists. If a loss of safety function is determined to exist by this program, the appropriate Conditions and Required Actions of the LCO in which the loss of safety function exists are required to be entered.
5.5.12	Primary Containment Leakage Rate Testing Program
	A program shall be established to implement the leakage rate testing of the containment as required by 10 CFR 50.54(o) and 10 CFR 50, Appendix J, Option B, as modified by approved exemptions. This program shall be in accordance with the guidelines contained in Regulatory Guide 1.163, "Performance-Based Containment Leak- Test Program," dated September 1995 The peak calculated containment internal pressure for the design basis loss of coolant accident, P, is 49.1 psig.
	The maximum allowable primary containment leakage rate, L., at P., shall be 0.5% of primary containment air weight per day.
	Leakage Rate acceptance criteria are:
	a. Primary Containment leakage rate acceptance criterion is $\leq$ 1.0 L. During the first unit startup following testing in accordance with this program, the leakage rate acceptance criteria are $\leq$ 0.60 L. for the Type B and Type C tests and $\leq$ 0.75 L. for Type A tests;
	(continued)
	as modified by the following exception to NEI 94-01, Rev. 0, "Industry Guideline for Implementing Performance-Based Option of 10 CFR Part 50, Appendix J", Section 10.2:
	a. MSIV leakage is excluded from the combined total of 0.6 L <sub>a</sub> for the Type B and C tests
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## 5.5 Programs and Manuals

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5.5.12	Primary Containment Leakage Rate Testing Program (continued)
	b. Air lock testing acceptance criteria are:
Ş	<ol> <li>Overall air lock leakage rate is ≤ 9000 scc/min when tested at ≥ P</li> <li>The provisions of SR 3.0.2 do not apply to the test frequencies specified in the Primary Containment Leakage Rate Testing Program.</li> <li>The provisions of SR 3.0.3 are applicable to the Primary Containment Leakage Rate Testing Program.</li> </ol>
	c. MSIV leakage acceptance criteria are as specified in SR 3.6.1.3.14.

#### BASES

SURVEILLANCE REQUIREMENTS

### SR 3.6.1.1.1 (continued)

valve leakage (SR 3.6.1.3.14), does not necessarily result in a failure of this SR. The impact of the failure to meet these Sks must be evaluated against the Type A, B, and C acceptance criteria of the Primary Containment Leakage Rate Testing Program. As left leakage prior to the first startup after performing a required leakage test is required to be 0.51. For combined Type B and C leakage, and C 0.75 L for overall Type A leakage. At all other times between required leakage rate tests, the acceptance criteria is based on an overall type & leakage limit of  $\leq 1.0$  L. At  $\leq 1.0$  L, the offsite dose consequences are bounded by the assumptions of the safety analysis. The Frequency is required by the Primary Containment Leakage Rate Testing. Program.

#### SR 3.6.1.1.2

Maintaining the pressure suppression function of primary containment requires limiting the leakage from the drywell to the suppression chamber. Thus, if an event were to occur that pressurized the drywell, the steam would be directed through the downcomers into the suppression pool. This SR is a leak test that confirms that the bypass area between the drywell and the suppression chamber is less than or equivalent to a one-inch diameter hole (Ref. 4). This ensures that the leakage paths that would bypass the suppression pool are within allowable limits.

The leakage test is performed every 24 months. The 24 month Frequency was developed considering that component failures that might have affected this test are identified by other primary containment SRs. Two consecutive test failures, however, would indicate unexpected primary containment degradation; in this event, as the Note indicates, a test shall be performed at a Frequency of once every 12 months until two consecutive tests pass, at which time the 24 month test Frequency may be resumed.

(continued)

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Primary Containment B 3.6.1.1

BASES (continued)

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1.1.1.1.1

REFERENCES	1.	UFSAR, Section 14.6.3.
	2.	Letter G94-PEPR-183, Peach Bottom Improved Technical Specification Project Increased Drywell and Suppression Chamber Pressure Analytical Limits, from G.V. Kumar (GE) to A.A. Winter (PECO), August 23, 1994.
	3.	10 CFR 50, Appendix J, Option B.
	4.	Safety Evaluation by the Office of Nuclear Reactor Regulation Supporting Amendment Nos. 127 and 130 to Facility Operating License Nos. DPR-44 and DPR-56, dated February 18, 1988.
	5.	NEI 94-01, Revision 0, "Industry Guideline for Implementing Performance-Based Option of 10 CFR Part 50, Appendix J."
	6.	ANSI/ANS-56.8-1994, "Containment System Leakage Testing Requirements."

BASES

SURVEILLANCE

(continued)

This SR ensures that in case the non-safety grade instrument air system is unavailable, the SGIG System will perform its design function to supply nitrogen gas at the required pressure for valve operators and valve seals supported by the SGIG System. The 24 month Frequency was developed considering it is prudent that this Surveillance be performed only during a plant outage. Operating experience has shown that these components will usually pass this Surveillance when performed at the 24 month Frequency. Therefore, the Frequency was concluded to be acceptable from a reliability standpoint.

### SR 3.6.1.3.14

SR 3.6.1.3.13

The analyses in Reference | are based on leakage that is less than the specified leakage rate. Leakage through each MSIV must be  $\leq 11.5$  soft when tested at  $\geq P$ . (25 psig) (STATES This ensures that MSIV leakage is properly accounted for in determining the overall primary containment leakage rate. The Frequency is required by the Primary Containment Leakage ( Rate Testing Program.

### SR 3.6.1.3.15

Verifying the opening of each 6 inch and 18 inch primary containment purge valve and each 18 inch primary containment exhaust valve is restricted by a blocking device to less than or equal to the required maximum opening angle specified in the UFSAR (Ref. 4) is required to ensure that the valves can close under DBA conditions within the times in the analysis of Reference 1. If a LOCA occurs, the purge and exhaust valves must close to maintain primary containment leakage within the values assumed in the accident analysis. At other times pressurization concernaare not present, thus the purge and exhaust valves can be fully open. The 24 month Frequency is appropriate because the blocking devices may be removed during a refueling outage.

(continued)

The analyses in Reference 1 are based on treatment of MSIV leakage as a secondary containment bypass leakage, independent of a primary to secondary containment leakage analyzed at 1.27 L<sub>a</sub>. In the Reference 1 analysis all 4 steam lines are assumed to leak at the TS Limit. This ensures that MSIV leakage is properly accounted for in determining the overall impacts of primary containment leakage.

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# 5.5 Programs and Manuals

5.5.11	Safety Function Determination Program (SFDP) (continued)
	<ol> <li>A required system redundant to system(s) supported by the inoperable support system is also inoperable; or</li> </ol>
	<ol> <li>A required system redundant to system(s) in turn supported by the inoperable supported system is also inoperable; or</li> </ol>
	<ol> <li>A required system redundant to support system(s) for the supported systems (b.1) and (b.2) above is also inoperable.</li> </ol>
	c. The SFDP identifies where a loss of safety function exists. If a loss of safety function is determined to exist by this program, the appropriate Conditions and Required Actions of the LCO in which the loss of safety function exists are required to be entered.
5.5.12	Primary Containment Leakage Rate Testing Program
	A program shall be established to implement the leakage rate testing of the containment as required by 10 CFR 50.54(0) and 10 CFR 50, Appendix J, Option B, as modified by approved exemptions. This program shall be in accordance with the guidelines contained in Regulatory Guide 1.163, "Performance-Based Containment Leak- Test Program," dated September 1995,
	The peak calculated containment internal pressure for the design basis loss of coolant accident, P., is 49.1 psig.
	The maximum allowable primary containment leakage rate, L., at P. shall be 0.5% of primary containment air weight per day.
	Leakage Rate acceptance criteria are:
	a. Primary Containment leakage rate acceptance criterion is ≤ 1.0 L. During the first unit startup following testing in accordance with this program, the leakage rate acceptance criteria are ≤ 0.60 L, for the Type B and Type C tests and ≤ 0.75 L, for Type A tests;
	(continued)
	following exception to NEI 94-01. Rev. 0, "Industry Guideline for Implementing Performance-Based Option of 10 CFR Part 50, Appendix J", Section 10.2:
	a. MSIV leakage is excluded from the combined total of 0.6 L <sub>a</sub> for the Type B and C tests.
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## 5.5 Programs and Manuals

Primary Containment Leakage Rate Testing Program (continued) 5.5.12 Air lock testing acceptance criteria are: b. Overall air lock leakage rate is  $\leq$  9000 scc/min when 1) tes:ed at  $\geq P_*$ . The provisions of SR 3.0.2 do not apply to the test frequencies specified in the Primary Containment Leakage Rate Testing Program. The provisions of SR 3.0.3 are applicable to the Primary Containment Leakage Rate Testing Program. MSIV leakage acceptance criteria are as specified in SR 3.6.1.3.14. C.

BASES

# SURVEILLANCE <u>SR 3.6.1.1.1</u> (continued)

valve leakage (SR 3.6.1.3.14), does not necessarily result in a failure of this SR. The impact of the failure to meet these SRs must be evaluated against the Type A, B, and C acceptance criteria of the Primary Containment Leakage Rate Testing Program. As left leakage prior to the first startup after performing a required leakage test is required to be < 0.6 L, for combined Type B and C leakage, and < 0.75 L. for overall Type A leakage. At all other times between required leakage rate tests, the acceptance criteria is based on an overall Type A leakage limit of  $\leq 1.0$  L. At  $\leq 1.0$  L, the offsite dose consequences are bounded by the assumptions of the safety analysis. The Frequency is required by the Primary Containment Leakage Rate Testing Program.

### SR 3.6.1.1.2

Maintaining the pressure suppression function of primary containment requires limiting the leakage from the drywell to the suppression chamber. Thus, if an event were to occur that pressurized the drywell, the steam would be directed through the downcomers into the suppression pool. This SR is a leak test that confirms that the bypass area between the drywell and the suppression chamber is less than or equivalent to a one-inch diameter hole (Ref. 4). This ensures that the leakage paths that would bypass the suppression pool are within allowable limits.

The leakage test is performed every 24 months. The 24 month Frequency was developed considering that component failures that might have affected this test are identified by other primary containment SRs. Two consecutive test failures, however, would indicate unexpected primary containment degradation; in this event, as the Note indicates, a test shall be performed at a Frequency of once every 12 months until two consecutive tests pass, at which time the 24 month test Frequency may be resumed.

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BASES (continued)

REFERENCES	1.	UFSAR, Section (14.6.3. 14.9.)
	2.	Letter G94-PEPR-183. Peach Bottom Improved Technical Specification Project Increased Drywell and Suppression Chamber Pressure Analytical Limits, from G.V. Kumar (GE) to A.A. Winter (PFCO), August 23, 1994.
	3.	10 CFR 50, Appendix J, Option B.
	4.	Safety Evaluation by the Office of Nuclear Reactor Regulation Supporting Amendment Nos. 127 and 130 to Facility Operating License Nos. DPR-44 and DPR-56, dated February 18, 1988.
	5.	NEI 94-01, Revision 0, "Industry Guideline for Implementing Performance-Based Option of 10 CFR Part 50, Appendix J."
	6.	ANSI/ANS-56.8-1994, "Containment System Leakage Testing Requirements."

PCIVS 8 3.6.1.3

### SR 3.6.1.3.13

REQUIREMENTS (continued)

SURVEILLANCE

This SR ensures that in case the non-safety grade instrument air system is unavailable, the SGIG System will perform its design function to supply nitrogen gas at the required pressure for valve operators and valve seals supported by the SGIG System. The 24 month Frequency was developed considering it is prudent that this Surveillance be performed only during a plant outage. Operating experience has shown that these components will usually pass this Surveillance when performed at the 24 month Frequency. Therefore, the Frequency was concluded to be acceptable from a reliability standpoint.

### SR 3.6.1.3.14

The analyses in Reference 1 are based on leakage that is less than the specified leakage rate. Leakage through each MSIV must be  $\leq 11.5$  scfh when tested at  $\geq P$ . (25 psig). This ensures that MSIV leakage is properly accounted for in determining the overall primary containment leakage wate: The Frequency is required by the Primary Containment Leakage Rate Testing Program.

### GR 3.6.1.3.15

Verifying the opening of each 6 inch and 18 inch primary containment purge valve and each 18 inch primary containment exhaust valve is restricted by a blocking device to less than or equal to the required maximum opening angle specified in the UFSAR (Ref. 4) is required to ensure that the valves can close under DBA conditions within the times in the analysis of Reference 1. If a LOCA occurs, the purge and exhaust valves must close to maintain primary containment leakage within the values assumed in the accident analysis. At other times pressurization concerns are not present, thus the purge and exhaust valves can be fully open. The 24 month Frequency is appropriate because the blocking devices may be removed during a refueling outage.

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The analyses in Reference 1 are based on treatment of MSIV leakage as a secondary containment bypass leakage, independent of a primary to secondary containment leakage analyzed at 1.27 La. In the Reference 1 analysis all 4 steam lines are assumed to leak at the TS Limit. This ensures that MSIV leakage is properly accounted for in determining the overall impacts of primary containment leakage.

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