

REACTOR CONTAINMENT BUILDING
INTEGRATED LEAKAGE RATE TEST

TYPES A, B, AND C
PERIODIC TESTS FOR
MAY 1983 TO MAY 1985

NEW YORK POWER AUTHORITY
JAMES A. FITZPATRICK NUCLEAR POWER PLANT
DOCKET NO. 50-333

Prepared by
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TABLE OF CONTENTS

| <u>Section</u> | <u>Title</u> | <u>Page</u> |
|----------------|--|-------------|
| | LIST OF ATTACHMENTS | iii |
| | REFERENCES | v |
| 1 | PURPOSE | 1-1 |
| 2 | SUMMARY | 2-1 |
| | 2.1 TYPE A TEST | 2-1 |
| | 2.1.1 Test Summary | 2-1 |
| | 2.1.2 Conclusion | 2-2 |
| | 2.2 LOCAL LEAKAGE RATE TESTS (TYPES B AND C) | 2-3 |
| 3 | TYPE A TEST | 3.1-1 |
| | 3.1 EDITED LOG OF EVENTS | 3.1-1 |
| | 3.2 GENERAL TEST DESCRIPTION | 3.2-1 |
| | 3.2.1 Prerequisites | 3.2-1 |
| | 3.2.2 Equipment and Instrumentation | 3.2-1 |
| | 3.2.3 Data Acquisition System | 3.2-2 |
| | 3.2.4 Data Resolution System | 3.2-2 |
| | 3.3 TEST RESULTS | 3.3-1 |
| | 3.3.1 Presentation of Test Results | 3.3-1 |
| | 3.3.2 60 psia PCILRT Results | 3.3-2 |
| | 3.3.3 Supplemental Test Results | 3.3-2 |
| 4 | LOCAL LEAKAGE RATE TESTS (TYPES B AND C) | 4-1 |

LIST OF ATTACHMENTS

| <u>Attachment</u> | <u>Title</u> |
|-------------------|--|
| 2.1A | Graph 1 - Total Mass vs. Time |
| 3.2A | Site Meteorology |
| 3.2B | Temporary Piping Leakage Rate Analyzer (LRA) System No. 16-1 |
| 3.2C | Permanent Piping Leakage Rate Analyzer (LRA) System No. 16-1 |
| 3.2D | Instrumentation |
| 3.2E | LRA System No. 16-1, PCILRT Temperature Detector Locations |
| 3.2F | LRA System No. 16-1, PCILRT Moisture Detector Locations |
| 3.2G | Temporary Piping Superimposed Leakage Verification Test (CAD) System No. 27 |
| 3.3A | Primary Containment Integrated Leakage Rate Test (PCILRT) - Input Variables, from 1630 on 5-13-85 to 1630 on 5-14-85. |
| 3.3B | Primary Containment Integrated Leakage Rate Test (PCILRT) - Absolute Test Method, Mass Point Analysis Test Results, from 1630 on 5-13-85 to 1630 on 5-14-85. |
| 3.3C | Primary Containment Integrated Leakage Rate Test (PCILRT) - Initialization and Control Variables, from 1630 on 5-13-85 to 1630 on 5-14-85. |
| 3.3D | Type C Penetration Leakage to be Added to Calculated PCILRT Leakage Rate |
| 3.3E | Graph 2 - Primary Containment Leakage Rate and UCL vs. Time |
| 3.3F | Graph 3 - Primary Containment Air Mass vs. Time |
| 3.3G | Superimposed Leakage Verification Test - Input Variables, from 1730 on 5-14-85 to 2130 on 5-14-85. |
| 3.3H | Superimposed Leakage Verification Test - Absolute Test Method, Mass Point Analysis Test Results, from 1730 on 5-14-85 to 2130 on 5-14-85. |

LIST OF ATTACHMENTS (Cont.)

| <u>Attachment</u> | <u>Title</u> |
|-------------------|--|
| 4A | 1985 Types B and C Data Summary |
| 4B | 1983 Types B and C Data Summary |
| 4C | 1983/1985 Primary Containment Boundary Modifications |

REFERENCES

1. 10CFR50, Appendix J, Primary Reactor Containment Leakage Testing For Water-Cooled Power Reactors, October 22, 1980.
2. F-ST-39F, Type "A" Test (60 PSIA) Primary Containment Integrated Leak Rate Test.
3. ANSI N45.4, American National Standard Leakage - Rate Testing of Containment Structures For Nuclear Reactors, March 16, 1972.
4. ANSI/ANS-56.8, Containment System Leakage Testing Requirements, February 19, 1981¹.

¹This document used only as a guideline and any reference to said document in no way implies compliance.

SECTION 1

PURPOSE

The purpose of this report is to present a description and analysis of the May 1985 Periodic Type A Primary Containment Integrated Leakage Rate Test (PCILRT) and a summary of the last two periodic Type B and C tests conducted since May 1983 at the James A. FitzPatrick Nuclear Power Plant (JAFNPP). JAFNPP is owned and operated by the New York Power Authority (NYPA).

Stone & Webster Engineering Corporation (SWEC) provided engineering consultation services to NYPA during the performance of this test.

This report is submitted as required by 10CFR50, Appendix J, Paragraph V.B.

SECTION 2

SUMMARY

2.1 Type A Test

2.1.1 Test Summary

On May 13, 1985, pressurization was started at 0330 hours. A fairly constant rate of 6.8 psig per hour was established. Equipment problems with 16-FCV-101 (see Attachment 3.2C) interrupted primary containment pressurization at 0615 hours. Flow was reestablished through bypass valve LRA-3 at 0620 hours with a fairly constant rate of 7.0 psig per hour. At 0815 hours, 16-FCV-101 was placed back in service with a fairly constant pressurization rate of 4.2 psig per hour being maintained throughout the remainder of the pressurization period.

Primary containment pressurization was secured at 1230 hours on May 13, 1985, with a peak instantaneous pressure of 60.33 psia. During the pressurization period both drywell vent fans (68-FN-4D and 68-FN-2D) tripped on high current overload. At approximately 1630 hours, the average hourly drywell and torus temperature satisfied the procedural thermal stabilization criterion.

An extensive investigation of all penetration areas was conducted. This search revealed minor packing leaks on several valves, the most significant on 27-AOV-101B.

During the 24 hour test period from 1630 hours on May 13, 1985 to 1630 hours on May 14, 1985, a steady mass increase of about 7.2 lbm per hour was observed (Attachment 2.1A). This mass increase was initially attributed to the difference in torus water and air temperatures, but was later attributed to an increasing torus water level of approximately 5 gpm and an increasing drywell equipment sump water level of approximately 0.5 gpm.

With the calculated mass adjusted for the torus water inleakage, a stable mass loss of about 7.1 lbm per hour was observed. This rate was below the procedural acceptance criteria rate of 0.375%/day (13 lbm per hour).

The Type A PCILRT was successfully completed at 1630 hours on May 14, 1985 with a total Type A leakage of 0.281214%/day. A superimposed leakage verification test was successfully completed from 1730 to 2130 hours on May 14, 1985.

In accordance with the U.S. Nuclear Regulatory Commission's (USNRC) request, an investigation of certain pathways was conducted in order to identify the source of torus water inleakage. For example the condensate transfer supply ("Keep Full") to the Residual Heat Removal (RHR) System was isolated. Also, 10-RV-41B was gagged since it was suspected to be leaking (warm tail pipe) back to the torus. The containment mass and the torus water level rate of change were monitored during this investigation. No significant change in the torus water level inleakage rate was detected during the investigation.

Drywell equipment sump cooling water was also isolated prior to the test since it was suspected that it had been leaking into the Drywell Equipment Sump. This also did not prove to be a water inleakage source, as the level still increased during the Type A test (see Section 3.3.2.d for the correction).

Depressurization of the primary containment began at 0200 hours on May 15, 1985 with a drywell pressure of about 60.2 psia and was completed at 0845 hours.

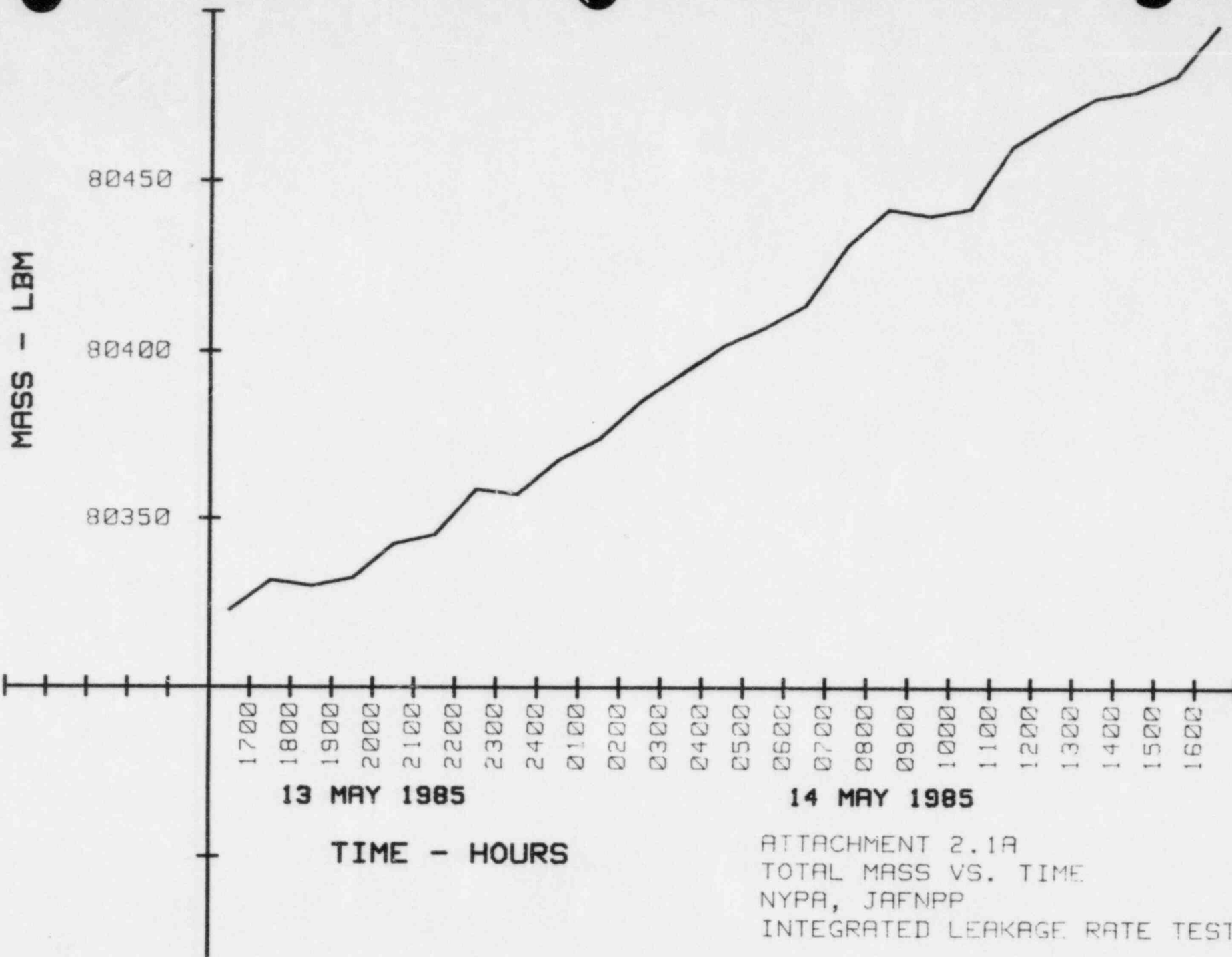
2.1.2 Conclusion

- a. The calculated air mass, when adjusted for the torus water inleakage, results in a leakage rate well within the procedural acceptance criteria. Although the source of the torus water inleakage could not be identified, it was the cause of the increasing air mass. As shown in Attachment 2.1A, the water level rate of increase was uniform throughout the Type A test period.

2.2 LOCAL LEAKAGE RATE TESTS (Types B and C)

The Local Leakage Rate Tests (LLRTs) of containment isolation valves and other primary containment penetrations were performed by the methods described in the plant surveillance procedure No. F-ST-39B, "Type 'B' and 'C' LLRT of Containment Penetrations."

Data for the two surveillance periods (1983 and 1985) of LLRTs performed since the last Type A Test in accordance with Appendix J, 10CFR50, Paragraph V.B., is summarized in Section 4 of this report.



SECTION 3

TYPE A TEST

3.1 EDITED LOG OF EVENTS

This log was edited from the Official PCILRT Log of Events, Shift Supervisor's Log, Nuclear Control Room Operator's Log, and Auxiliary Operator C's Log.

May 10, 1985

At 0800 hours, the valve lineups were started for the PCILRT.

May 11, 1985

At 2300 hours, used 06-LI-94C instead of 06-LI-94B as control room reactor vessel level indicator backup.

May 12, 1985

At 0001 hours, commenced processing torus water in order to meet 0.0 to -1.5 in.

At 0400 hours, successfully completed the local leakage rate test on the drywell head.

At 0500 hours, the primary containment inspection was completed.

At 1700 hours, observed a drywell equipment sump inleakage of approximately 0.5 gpm. Isolated drywell sump cooler and drywell cooler "A" to determine if the drywell sump cooler was the source of leakage.

At 2315 hours, successfully completed the local leakage rate test on the personnel hatch.

May 13, 1985

At 0215 hours, completed all PCILRT prerequisites.

At 0330 hours, commenced primary containment pressurization in accordance with surveillance procedure No. F-ST-39F entitled "Type A Test (60 psia) Primary Containment Integrated Leak Rate Test."

At 0615 hours, 16-FCV-101 closed.

At 0620 hours, opened bypass valve LRA-3.

At 0815 hours, 16-FCV-101 placed back in service.

At 0845 hours, drywell vent fan 68-FN-4D tripped on high current overload.

At 1015 hours, drywell vent fan 68-FN-2D tripped on high current overload.

At 1050 hours, isolated "Keep Full" to standby loop of RHR (A side). Torus water level pumped down from -0.72 to -1.03.

At 1230 hours, with the drywell pressure at 60.3 psia (instantaneous computer reading), the pressurization equipment was isolated and secured. The minimum 4-hour stabilization period began.

At 1515 hours, extensive search for leakage paths completed. This search revealed minor packing leaks on several valves, the most significant on 27-AOV-101B.

At 1610 hours, pumped down drywell equipment sump.

At 1630 hours, the temperature stabilization criterion was satisfied and the PCILRT was started.

May 14, 1985

At 0215 hours, investigated all possible sources of inleakage to the drywell. None were found.

At 0830 hours, torus water level increased 0.90 in. in 16 hours.

At 1630 hours, the PCILRT test period was completed, and preparation for the superimposed leakage verification test began.

At 1700 hours, the superimposed leakage verification test stabilization period was initiated with an imposed leakage of approximately 5375 SCFD.

At 1730 hours, began the superimposed leakage verification test period.

At 2130 hours, the superimposed leakage verification test was completed.

At 2300 hours, gagged 10-RV-41B to determine if this was the source of torus water inleakage.

May 15, 1985

At 0200 hours, the packing on 27-AOV-101B was adjusted. The PCILRT, the verification test, and the torus water inleakage investigation were documented as complete. The depressurization of the primary containment was started.

At 0845 hours, depressurization of the primary containment was completed.

3.2 GENERAL TEST DESCRIPTION

3.2.1 Prerequisites

In accordance with the James A. FitzPatrick PCILRT Procedure F-ST-39F (Reference 2), the following is a listing of the pertinent prerequisites completed and documented prior to primary containment pressurization:

- a. Site meteorological data recorded at least three days prior to and during the performance of the PCILRT (Attachment 3.2A).
- b. All required test instrumentation cleaned, calibrated within 6 months of the test, and placed in service.
- c. All required Types B and C leakage rate testing completed.
- d. Satisfactory inspection of accessible interior and exterior surfaces of the primary containment structures and components completed.
- e. Temporary air compressors and test skid ready for use as the pressurization source.
- f. Two drywell ventilation fans adjusted for continuous operation at test pressure (45 psig), and their associated dampers blocked in the open position.
- g. All computer software used for test calculations tested and operational.
- h. Valves lined up and tagged in accordance with the Valve Line-Up List.
- i. Water levels recorded for the suppression pool, reactor vessel, drywell equipment sump, and drywell floor drain sump.
- j. Controlled Work Area Plan in effect.
- k. An Official Log of Events located in the Control Room and maintained by the Test Director.

3.2.2 Equipment and Instrumentation

Pressurization of the primary containment was achieved by the utilization of a temporary system consisting of two parallel compressor trains. Each train consisted of two air compressors which were manifolded through an in-line water cooled heat exchanger and refrigerant air dryer (Attachment 3.2B). The discharge of the temporary system was routed to the primary containment via the drywell spray portion of the RHR System (Attachment 3.2C). The system included adequate instrumentation and valving to maintain proper monitoring and control of the compressed air quality throughout the pressurization sequence. The total capacity of the pressurization system was 3,600 cubic feet per minute.

The various containment parameters required to calculate containment leakage during the test were monitored by the leakage monitoring system instrumentation. The instrumentation consisted of multiple resistance temperature detectors (RTDs), moisture detectors (dewcells), and absolute pressure quartz manometers for both the drywell and torus. Pertinent data for the test instrumentation is listed in Attachment 3.2D. The general locations of the temperature and moisture sensors, including applicable test zones, are shown in Attachments 3.2E and 3.2F.

A mass flow meter was used to perform the superimposed leakage verification test (Attachment 3.2G). All test instrumentation with the exception of that used for the superimposed leakage verification test was monitored by the plant process computer for data acquisition.

3.2.3 Data Acquisition System

The James A. FitzPatrick plant process computer system (PPCS) performs reactor core calculations and provides the plant operator with current core operating data. The PPCS also scans, calculates, stores, logs, and alarms information which has been collected for the plant operation.

The PPCS analog scan package reads all the analog inputs in a pre-established manner, converts these readings into engineering units, and then stores these values into predefined locations for use by the plant operators and by the plant application programs.

For the PCILRT, the function of the PPCS is to provide and transmit at five minute intervals sufficient sensor and zone pair information for input to a remote AT&T 3B2/300 computer (PCILRT computer) PCILRT calculation program. The PPCS PCILRT sensor program converts binary-coded decimal digital information from each manometer to an analog value.

For the PCILRT, the plant computer monitored the following instrumentation:

| <u>Type</u> | <u>Scan Rate (sec)</u> |
|-----------------------|------------------------|
| 18 RTDs | 60 |
| 6 Dewcells | 60 |
| 4 Absolute Manometers | 60 |

3.2.4 Data Resolution System

Periodically, during the PCILRT test period, leakage rate trends were monitored from data obtained from the plant process computer. The PCILRT computer program converts the dewcell equilibrium temperature to dewpoint temperature, and calculates a zone pair average (see Attachment 3.2E and 3.2F). This data along with the instantaneous sensor values and the difference between the two averaged sensor values for each zone are logged on the utility typer every 10 minutes.

After the appropriate data had been acquired and averaged utilizing the PCILRT computer system, the results were inputted for leakage rate calculations, utilizing the Absolute Method of Mass Point Analysis.

Absolute Method of Mass Point Analysis

The Absolute Method of Mass Point Analysis consists of calculating air masses within the containment structure over the test period from pressure, temperature, and dewpoint observations made during the PCILRT. The air masses are computed using the ideal gas law as follows:

$$\text{Mass} = \frac{144V(P-P_v)}{RT} \quad (\text{Eq. 1})$$

where:

- M = air mass, lbm
- P = total pressure, psia
- P_v = average vapor pressure, psia
- R = 53.35 ft-lbf/lbm°R (for air)
- T = average containment temperature, °R
- V = containment free volume, ft³

There are two containments: torus (suppression chamber) and drywell. The masses for each containment are computed separately and added together. The leakage rate is then determined by plotting the total air mass as a function of time, using a least-squares fit to determine the slope, $A = dM/dT$. The leakage rate is expressed as a percentage of the air mass lost in 24 hours or symbolically:

$$\text{Leakage Rate} = A/B(-2400) \quad (\text{Eq. 2})$$

where A is the slope of the least-squares curve and B is the y-intercept. The sign convention is such that the leakage out of containment is positive and the units are in percent/day.

A 95 percent confidence interval is calculated using a Students T distribution. The sum of the leakage rate and the 95 percent confidence interval is the upper confidence limit (UCL). The measured leakage rate may be described as 95 percent accurate to within the value of the UCL.

ATTACHMENT 3.2A

SITE METEOROLOGY

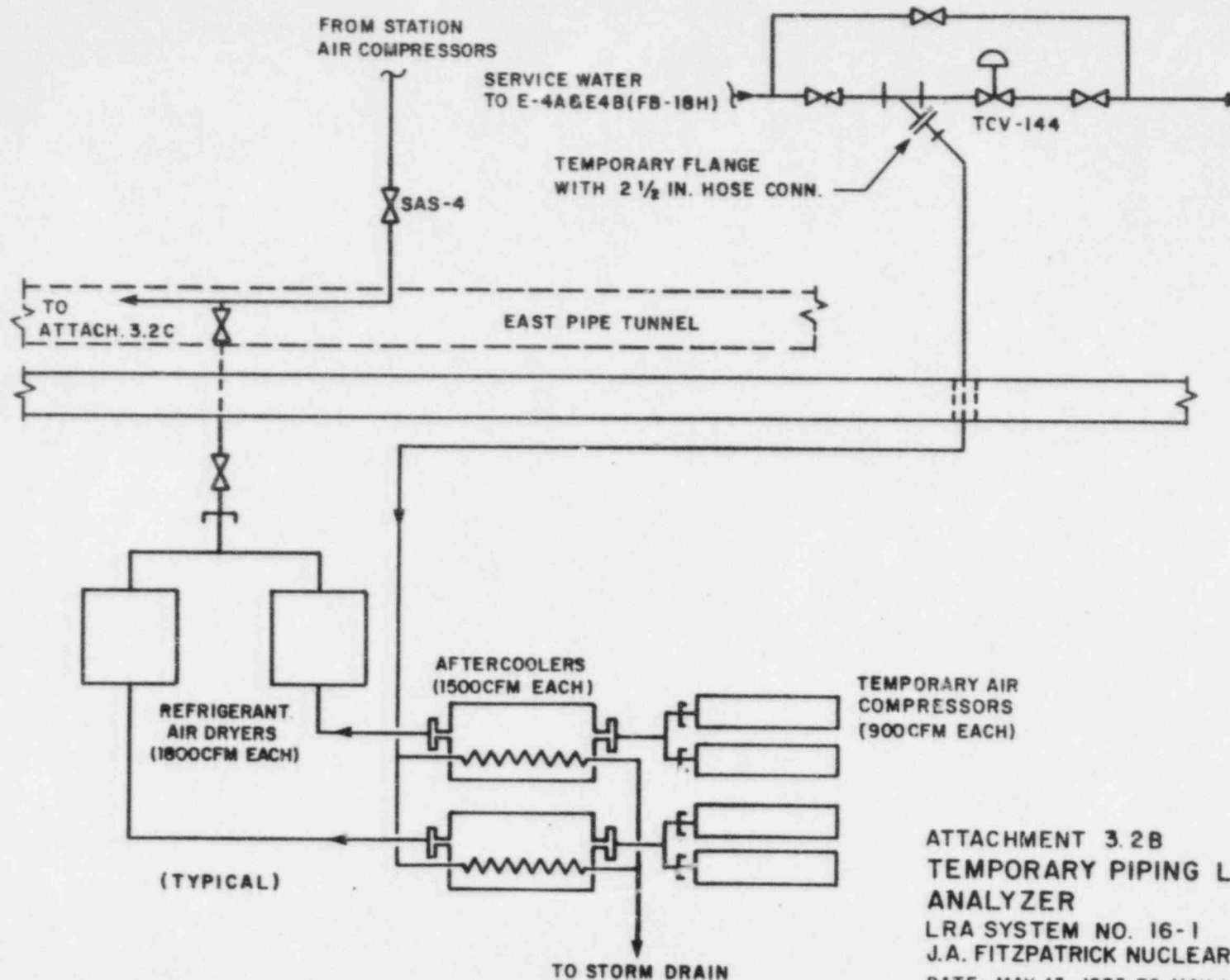
| Date | Time | Temperature Ambient, °F | Barometric Pressure, in. Hg | Wind Velocity, mph | Wind Direction | Dew Point Temperature °F | Reactor Bldg. Temperature °F |
|-------------------------------------|------|-------------------------------|-----------------------------------|--------------------------|-------------------|--------------------------------|------------------------------------|
| 5/9/85 | 1500 | 64.3 | 29.87 | 7.0 | 232.9° (SW) | 21.2 | 68 |
| | 2300 | 65.3 | 29.79 | 8.1 | 183.3 | 35.0 | 75 |
| 5/10/85 | 0700 | 65.2 | 29.75 | 11.2 | 197.6 | 38.6 | 73 |
| | 1500 | 62.8 | 29.71 | 12.4 | 244.8 | 21.4 | 69 |
| | 2300 | 71.0 | 29.72 | 10.3 | 224.9 | 19.4 | 78 |
| 5/11/85 | 0700 | 65.0 | 29.77 | 6.1 | 206.8 | 23.7 | 70 |
| | 1500 | 69.7 | 29.78 | 3.4 | 34.2 | 21.4 | 72 |
| | 2300 | 68.5 | 29.73 | 4.1 | 95.7 | 15.4 | 74 |
| 5/12/85 | 0700 | 66.8 | 29.71 | 7.9 | 134.5 | 16.6 | 71 |
| | 1500 | 65.4 | 29.66 | 3.4 | 285.4 | 57.7 | 72 |
| | 2300 | N/A | N/A | N/A | N/A | N/A | 72 |
| 5/13/85 0330 - Start Pressurization | | | | | | | |
| | 0400 | N/A | N/A | N/A | N/A | N/A | N/A |
| | 0500 | N/A | N/A | N/A | N/A | N/A | N/A |
| | 0600 | N/A | N/A | N/A | N/A | N/A | N/A |
| | 0700 | N/A | N/A | N/A | N/A | N/A | 70 |
| | 0800 | 70.5 | 29.64 | 9.3 | 228.4 | 22.6 | N/A |
| | 0900 | 69.2 | 29.65 | 12.8 | 240.0 | 15.3 | N/A |
| | 1000 | 62.7 | 29.66 | 14.0 | 247.1 | 14.5 | N/A |
| | 1100 | 54.6 | 29.67 | 12.1 | 251.7 | 22.0 | N/A |
| | 1200 | 53.0 | 29.66 | 13.2 | 247.8 | 26.1 | N/A |

ATTACHMENT 3.2A (Cont)

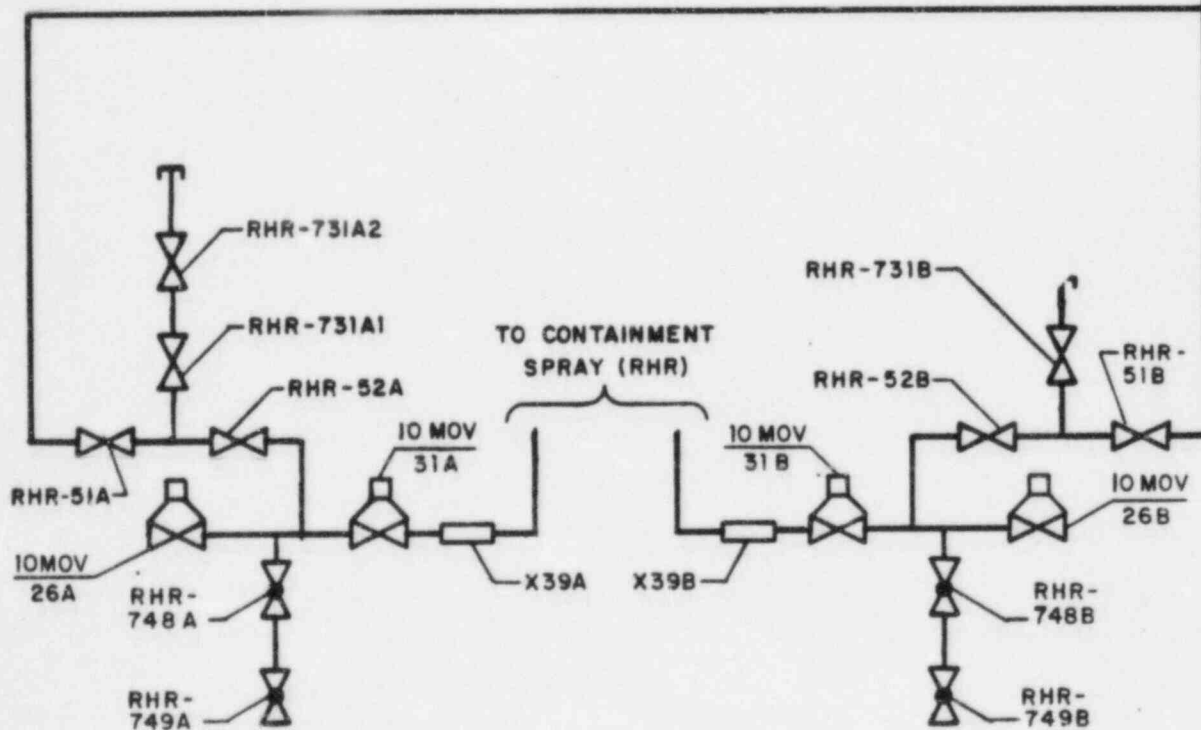
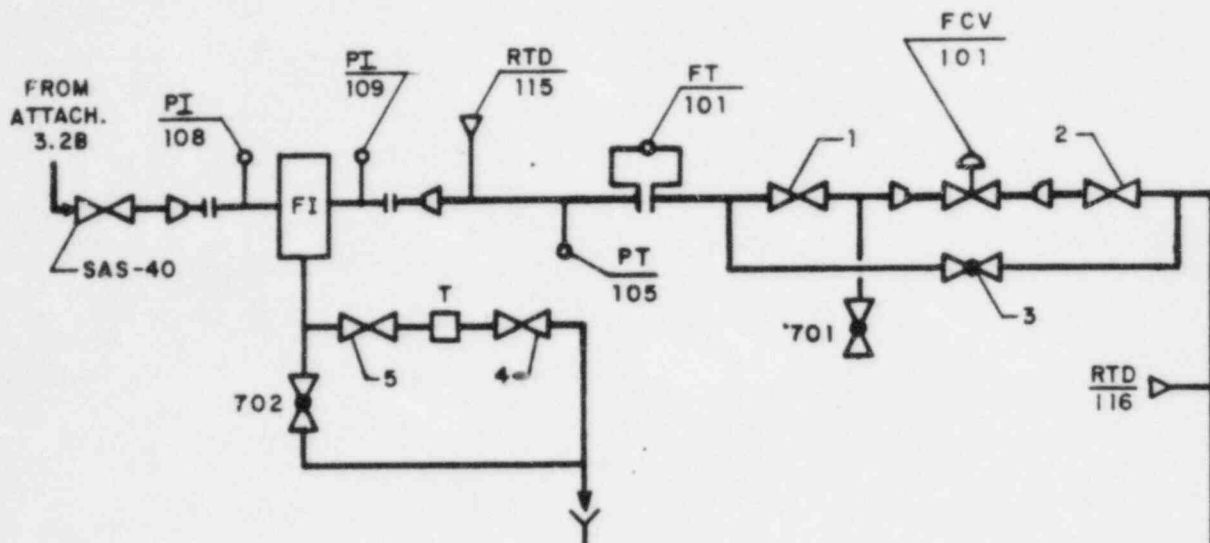
| <u>Date</u> | <u>Time</u> | <u>Temperature Ambient, °F</u> | <u>Barometric Pressure, in. Hg</u> | <u>Wind Velocity, mph</u> | <u>Wind Direction</u> | <u>Dew Point Temperature °F</u> | <u>Reactor Bldg. Temperature °F</u> |
|-------------|-------------|--|--|-----------------------------------|---------------------------|---|---|
| 5/13/85 | 1300 | 52.2 | 29.67 | 12.6 | 250.4 | 24.0 | N/A |
| | 1400 | 56.0 | 29.67 | 13.6 | 257.9 | 22.0 | N/A |
| | 1500 | 56.9 | 29.67 | 12.3 | 247.2 | 27.5 | 69 |
| | 1600 | 57.9 | 29.67 | 13.3 | 247.7 | 25.1 | 68 |
| | 1630 | - Start PCILRT | | | | | |
| | 1700 | 56.0 | 29.66 | 12.6 | 249.4 | 22.0 | 70 |
| | 1800 | 54.5 | 29.67 | 12.4 | 249.7 | 18.8 | 69 |
| | 1900 | 53.6 | 29.67 | 13.1 | 248.3 | 17.1 | 70 |
| | 2000 | 52.6 | 29.68 | 12.6 | 247.5 | 16.0 | 70 |
| | 2100 | 52.1 | 29.70 | 12.9 | 247.5 | 16.7 | 70 |
| | 2200 | 51.3 | 29.70 | 11.2 | 260.1 | 21.4 | 70 |
| | 2300 | 52.7 | 29.71 | 10.2 | 241.7 | 26.9 | 70 |
| | 2400 | 52.1 | 29.73 | 12.0 | 242.5 | 22.8 | 70 |
| 5/14/85 | 0100 | 50.5 | 29.75 | 11.2 | 242.8 | 21.1 | 70 |
| | 0200 | 48.7 | 29.75 | 10.0 | 252.6 | 19.5 | 70 |
| | 0300 | 49.7 | 29.75 | 6.8 | 239.2 | 18.1 | 70 |
| | 0400 | 50.4 | 29.74 | 5.3 | 228.5 | 16.3 | 69 |
| | 0500 | 49.9 | 29.76 | 7.5 | 238.3 | 16.3 | 69 |
| | 0600 | 48.6 | 29.77 | 9.0 | 241.9 | 16.2 | 69 |
| | 0700 | 48.8 | 29.80 | 9.0 | 243.2 | 15.2 | 69 |
| | 0800 | 49.0 | 29.82 | 11.0 | 246.0 | 13.3 | 69 |
| | 0900 | 47.7 | 29.83 | 10.8 | 288.5 | 13.1 | 69 |
| | 1000 | 47.5 | 29.85 | 9.9 | 333.5 | N/A | 70 |
| | 1100 | 46.8 | 29.86 | 9.9 | 348.5 | N/A | 70 |
| | 1200 | 47.1 | 29.87 | 5.2 | 357.1 | N/A | 69 |
| | 1300 | N/A | N/A | N/A | N/A | N/A | 69 |
| | 1400 | N/A | N/A | N/A | N/A | N/A | 69 |
| | 1500 | 52.6 | 29.89 | 5.0 | 303.3 | 45.5 | 69 |
| | 1600 | 53.7 | 29.89 | 5.4 | 6.4 | 45.6 | 69 |
| | 1630 | - Complete PCILRT | | | | | |

NOTE:

N/A - Site Meteorology Data Computer Inoperable.



ATTACHMENT 3.2B
 TEMPORARY PIPING LEAK RATE
 ANALYZER
 LRA SYSTEM NO. 16-1
 J.A. FITZPATRICK NUCLEAR POWER PLANT
 DATE: MAY 13, 1985 TO MAY 14, 1985



NOTE:

ALL MANUAL VALVES ARE PREFIXED
WITH LRA, WHICH IS LEAK RATE
ANALYZER SYSTEM NO. 16-1, EXCEPT
AS NOTED.

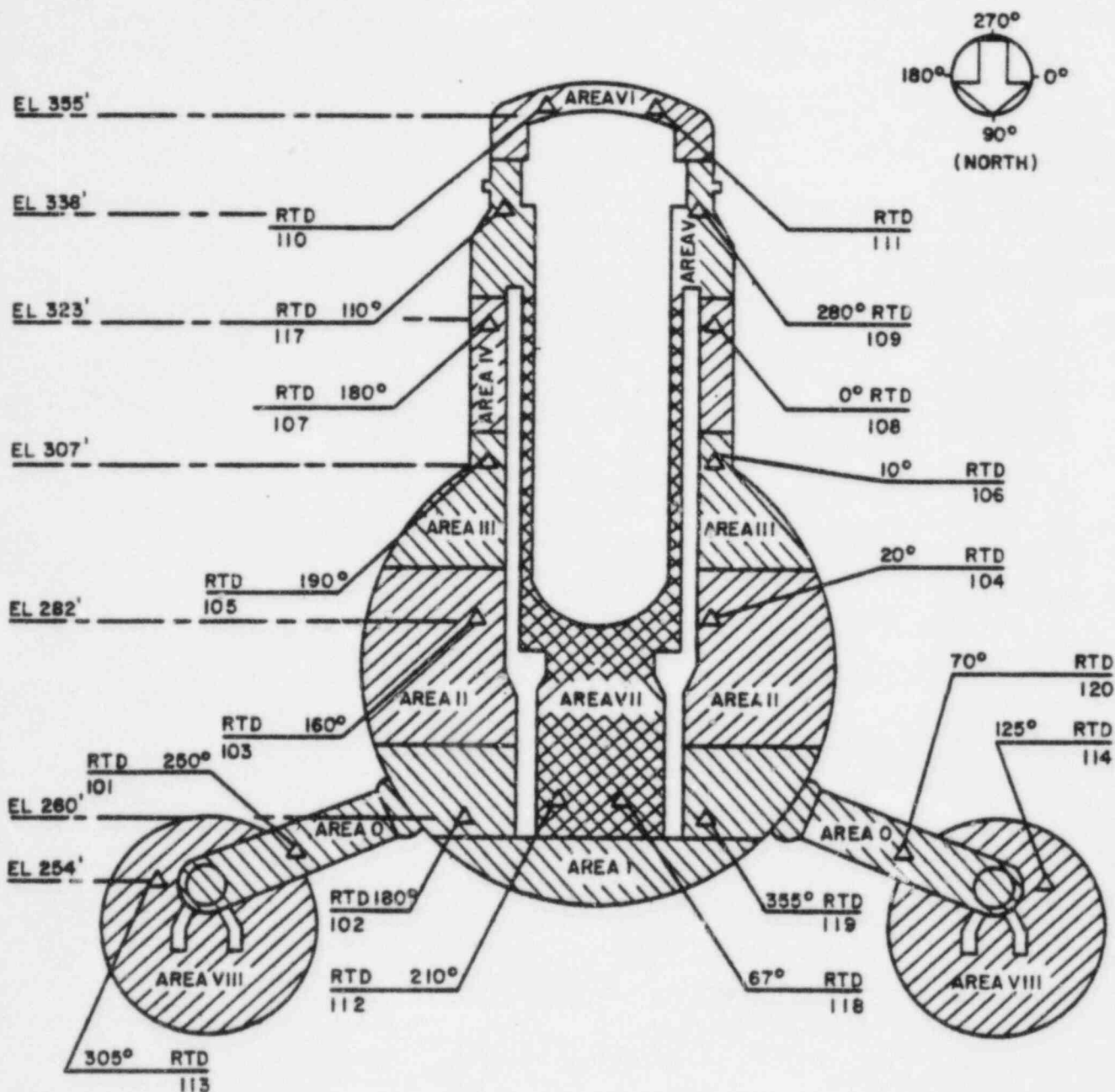
**ATTACHMENT 3.2C
PERMANENT PIPING LEAK RATE
ANALYZER**

LRA SYSTEM NO. 16-1
J.A. FITZPATRICK NUCLEAR POWER PLANT
DATE: MAY 13, 1985 TO MAY 14, 1985

ATTACHMENT 3.2D

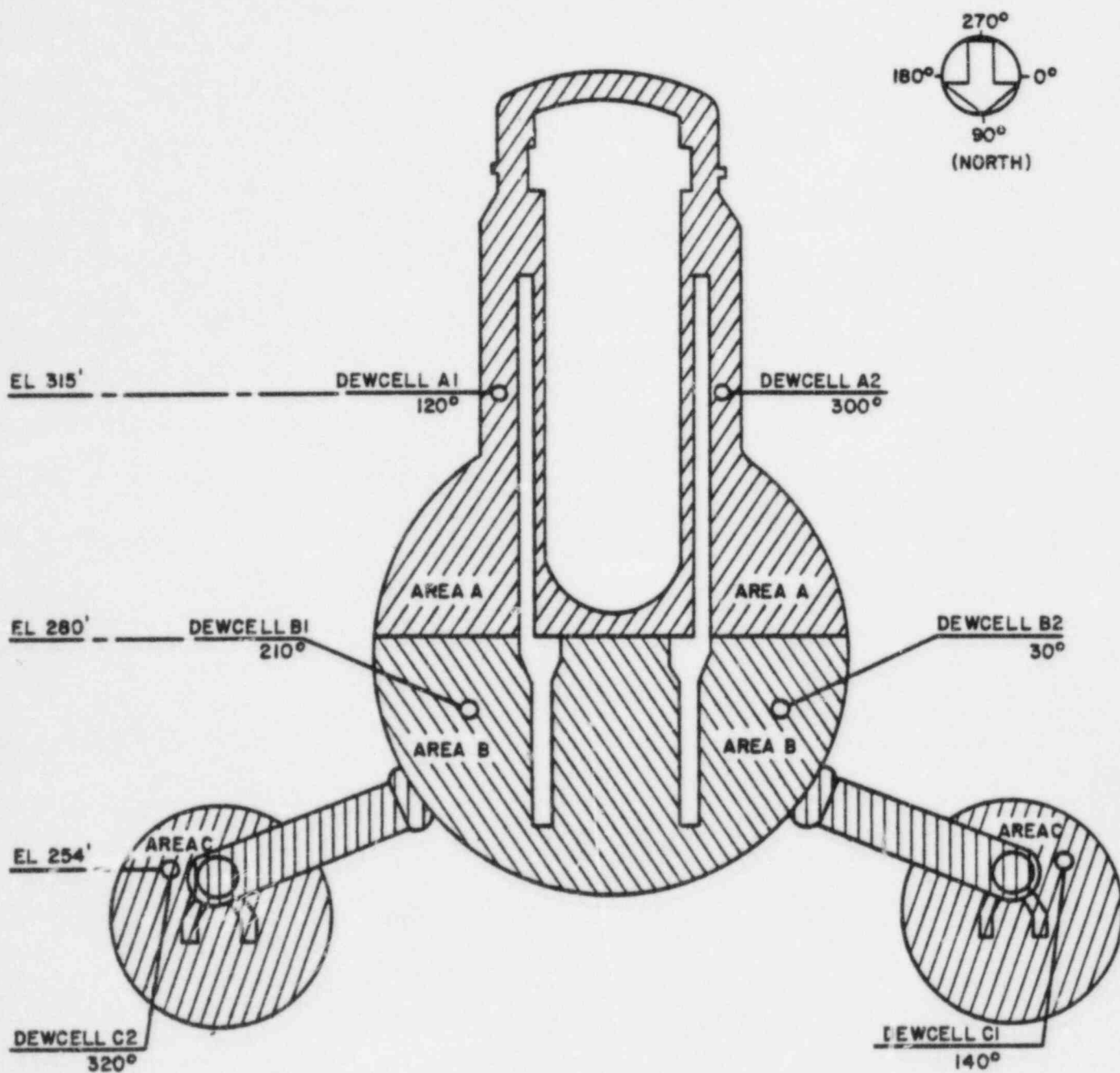
INSTRUMENTATION

| <u>Instrument</u> | <u>Weight Factor</u> | <u>Computer Point</u> | <u>Range</u> | <u>Zone</u> | <u>Accuracy</u> |
|--|--------------------------|---------------------------|---------------|-------------|-----------------|
| <u>A. Temperature</u> | | | | | |
| 16-1-RTD-101 | 0.056755 | M103 | 0°-300°F | 0 | ±1.0°F |
| 16-1-RTD-120 | 0.056755 | M116 | 0°-300°F | 0 | ±1.0°F |
| 16-1-RTD-102 | 0.082510 | M084 | 0°-300°F | 1 | ±1.0°F |
| 16-1-RTD-119 | 0.082510 | M115 | 0°-300°F | 1 | ±1.0°F |
| 16-1-RTD-103 | 0.178020 | M085 | 0°-300°F | 2 | ±1.0°F |
| 16-1-RTD-104 | 0.178020 | M086 | 0°-300°F | 2 | ±1.0°F |
| 16-1-RTD-105 | 0.065685 | M087 | 0°-300°F | 3 | ±1.0°F |
| 16-1-RTD-106 | 0.065685 | M088 | 0°-300°F | 3 | ±1.0°F |
| 16-1-RTD-107 | 0.023505 | M089 | 0°-300°F | 4 | ±1.0°F |
| 16-1-RTD-108 | 0.023505 | M090 | 0°-300°F | 4 | ±1.0°F |
| 16-1-RTD-109 | 0.026685 | M091 | 0°-300°F | 5 | ±1.0°F |
| 16-1-RTD-117 | 0.026685 | M113 | 0°-300°F | 5 | ±1.0°F |
| 16-1-RTD-110 | 0.035765 | M092 | 0°-300°F | 6 | ±1.0°F |
| 16-1-RTD-111 | 0.035765 | M093 | 0°-300°F | 6 | ±1.0°F |
| 16-1-RTD-112 | 0.031075 | M094 | 0°-300°F | 7 | ±1.0°F |
| 16-1-RTD-118 | 0.031075 | M114 | 0°-300°F | 7 | ±1.0°F |
| 16-1-RTD-113 | 0.500000 | M095 | 0°-300°F | 8 | ±1.0°F |
| 16-1-RTD-114 | 0.500000 | M102 | 0°-300°F | 8 | ±1.0°F |
| <u>B. Pressure</u> | | | | | |
| 16-1-PIT-101 | 0.50 | M096 | 0-100 psia | Drywell | ±0.02% |
| 16-1-PIT-102 | 0.50 | M097 | 0-100 psia | Drywell | ±0.02% |
| 16-1-PIT-103 | 0.50 | M098 | 0-100 psia | Torus | ±0.02% |
| 16-1-PIT-104 | 0.50 | M099 | 0-100 psia | Torus | ±0.02% |
| <u>C. Dewpoint</u> | | | | | |
| 16-1-DC-A1 | 0.50 | T062 | 38.5°-118.5°F | A | ±1°-2°F |
| 16-1-DC-A2 | 0.50 | T063 | 38.5°-118.5°F | A | ±1°-2°F |
| 16-1-DC-B1 | 0.50 | T064 | 38.5°-118.5°F | B | ±1°-2°F |
| 16-1-DC-B2 | 0.50 | T065 | 38.5°-118.5°F | B | ±1°-2°F |
| 16-1-DC-C1 | 0.50 | T066 | 38.5°-118.5°F | C | ±1°-2°F |
| 16-1-DC-C2 | 0.50 | T067 | 38.5°-118.5°F | C | ±1°-2°F |
| <u>D. Superimposed Leakage Verification Test Flow Instrument</u> | | | | | |
| Mass Flow Meter | N/A | N/A | 0-150 SLPM | N/A | ±2% F.S. |



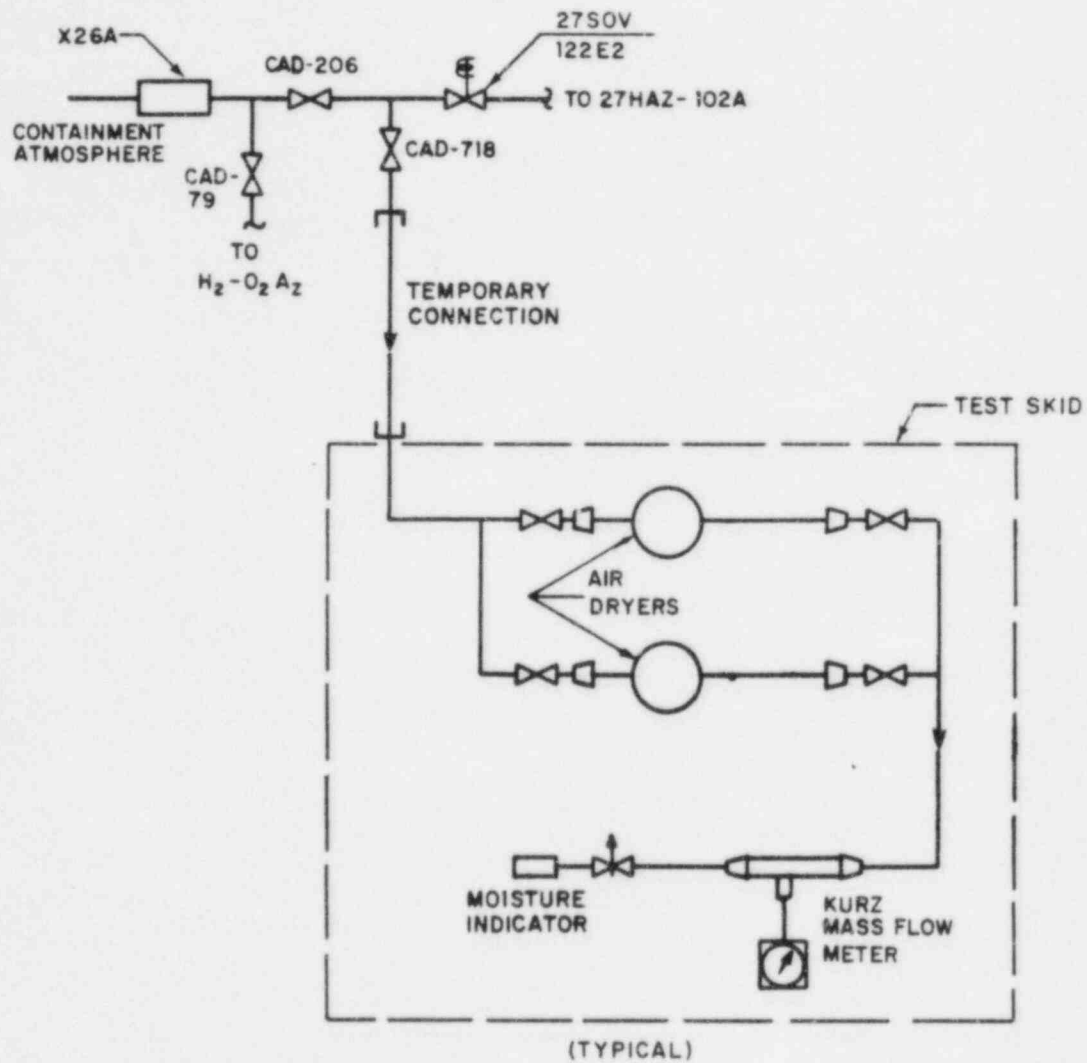
NOTE
RTD ELEVATIONS AND AZIMUTH
POSITIONS ARE APPROXIMATE

ATTACHMENT 3.2E
PCILRT TEMPERATURE DETECTOR
LOCATIONS
LRA SYSTEM NO. 16-1
J.A. FITZPATRICK NUCLEAR POWER PLANT
DATE: MAY 13, 1985 TO MAY 14, 1985



NOTE
MOISTURE DETECTOR ELEVATIONS
AND AZIMUTH POSITIONS ARE
APPROXIMATE.

ATTACHMENT 3.2F
PCILRT MOISTURE DETECTOR
LOCATIONS
LRA SYSTEM NO. 16-1
J.A. FITZPATRICK NUCLEAR POWER PLANT
DATE: MAY 13, 1985 TO MAY 14, 1985



ATTACHMENT 3.2G
 TEMPORARY PIPING SUPERIMPOSED
 LEAKAGE VERIFICATION TEST
 CAD SYSTEM NO. 27
 J.A. FITZPATRICK NUCLEAR POWER PLANT
 DATE: MAY 13, 1985 TO MAY 14, 1985

3.3 TEST RESULTS

3.3.1 Presentation of Test Results

The test data for the period of 1630 hours on May 13, 1985 through 1630 on May 14, 1985 were analyzed for the final test results using NYPA's AT&T 3B2/300 PCILRT computer program. The reduced input data and test results obtained by the PCILRT computer program are contained in Attachments 3.3A through 3.3C. Primary containment air mass was adjusted for the continuous torus water inleakage.

Two representative graphs (Attachments 3.3E and 3.3F) are provided showing the following quantities vs time:

1. Primary Containment Leakage Rate and UCL
2. Primary Containment Air Mass

The Absolute Test Method - Mass Point Analysis calculated test results are well below the procedural acceptance criteria of 0.375 percent/day. These test results include corrections for water levels and Type C leakage penalties (Section 3.3.2).

The Type A test instrumentation was verified during the supplemental test which used the superimposed leakage verification test method. The calculated test results using the PCILRT computer program were acceptable, as shown in Section 3.3.3. The reduced input data and test results obtained by the PCILRT computer program are contained in Attachments 3.3G and 3.3H.

3.3.2 60-psia PCILRT Results

The 60-psia PCILRT was conducted in accordance with Section VII.3 of surveillance procedure No. F-ST-39F. The results for the PCILRT is shown below.

| | | |
|----|--|----------|
| a. | Lam, leakage rate calculated (percent/day) | 0.203447 |
| b. | 95 percent confidence level (percent/day) | 0.007808 |
| c. | UCL, leakage rate with 95 percent confidence level (percent/day) | 0.211255 |
| d. | Corrections due to water level (percent/day) | |
| | Torus (adjusted) | 0.000000 |
| | Reactor Vessel | 0.000692 |
| | Drywell Equipment Sump | 0.027695 |
| | Drywell Floor Sump | 0.000000 |
| | Total | 0.028387 |
| e. | Correction for Type C leakage (percent/day) (See Attachment 3.3D) | 0.041572 |
| f. | Total reported Type A leakage rate (percent/day) | 0.281214 |

Results were within the acceptable limits of 0.75 La or 0.375 percent/day.

3.3.3 Supplemental Test Results

The Supplemental Verification Test was performed using the Superimposed Leakage Verification Test Method in accordance with Section VII.4 of surveillance procedure No. F-ST-39F. The results for the superimposed leakage verification test is shown below.

- a. Average Flow
 - i. Average flow in 4 hours = 223.9583 scfh
 - or $L_o = 0.489579\%/day$
- b. Composite Leakage, L_c
 - i. $L_c = 0.761626\%/day$
- c. Leakage rate from 24 hour PCILRT, L_{am}
 - i. $L_{am} = 0.203447\%/day$

d. $L_{am} + L_o - 0.25 L_a \leq L_c \leq L_{am} + L_o + 0.25 L_a$

i. $0.203447 + 0.489579 - 0.125 = 0.568026$

ii. $0.203447 + 0.489579 + 0.125 = 0.818026$

$$0.568026 \leq 0.761626 \leq 0.818026$$

The composite leakage rate is within the limits for the period of 1730 to 2130 hours on May 14, 1985.

ATTACHMENT 3.3A

PRIMARY CONTAINMENT INTEGRATED LEAKAGE RATE TEST
 NYPA JAMES A. FITZPATRICK NUCLEAR POWER PLANT
 FROM 1630 ON MAY 13, 1985 TO 1630 ON May 14, 1985

INPUT VARIABLES

| Time Hr | Drywell | | | | Torus | | | |
|------------|--------------|-------------------|----------------|-------------------|--------------|-------------------|----------------|-------------------|
| | Temp Degr | Abs Press Psia | Dew Pt Degr | Vap Press Psia | Temp Degr | Abs Press Psia | Dew Pt Degr | Vap Press Psia |
| 1630 | 89.274 | 60.146 | 75.575 | 0.438 | 75.133 | 60.244 | 73.424 | 0.408 |
| 1730 | 89.342 | 60.142 | 76.005 | 0.444 | 74.790 | 60.241 | 73.234 | 0.405 |
| 1830 | 89.353 | 60.136 | 76.316 | 0.449 | 74.653 | 60.235 | 72.995 | 0.402 |
| 1930 | 89.398 | 60.136 | 76.699 | 0.455 | 74.516 | 60.235 | 72.804 | 0.399 |
| 2030 | 89.482 | 60.136 | 76.913 | 0.458 | 74.242 | 60.235 | 72.613 | 0.397 |
| 2130 | 89.572 | 60.138 | 77.201 | 0.462 | 74.104 | 60.238 | 72.470 | 0.395 |
| 2230 | 89.556 | 60.142 | 77.439 | 0.466 | 73.966 | 60.241 | 72.326 | 0.393 |
| 2330 | 89.593 | 60.144 | 77.655 | 0.469 | 73.966 | 60.244 | 72.231 | 0.391 |
| 0030 | 89.595 | 60.147 | 77.822 | 0.472 | 73.830 | 60.245 | 72.183 | 0.391 |
| 0130 | 89.619 | 60.150 | 77.966 | 0.474 | 73.762 | 60.249 | 72.040 | 0.389 |
| 0230 | 89.621 | 60.155 | 78.037 | 0.475 | 73.693 | 60.255 | 71.992 | 0.388 |
| 0330 | 89.623 | 60.158 | 78.110 | 0.476 | 73.624 | 60.258 | 71.896 | 0.387 |
| 0430 | 89.626 | 60.161 | 78.109 | 0.476 | 73.555 | 60.261 | 71.896 | 0.387 |
| 0530 | 89.666 | 60.168 | 78.205 | 0.478 | 73.555 | 60.268 | 71.849 | 0.386 |
| 0630 | 89.674 | 60.165 | 78.133 | 0.477 | 73.418 | 60.267 | 71.801 | 0.386 |
| 0730 | 89.655 | 60.175 | 78.229 | 0.478 | 73.350 | 60.275 | 71.801 | 0.386 |
| 0830 | 89.662 | 60.183 | 78.229 | 0.478 | 73.350 | 60.283 | 71.706 | 0.385 |
| 0930 | 89.682 | 60.186 | 78.181 | 0.477 | 73.418 | 60.286 | 71.753 | 0.385 |
| 1030 | 89.654 | 60.186 | 78.229 | 0.478 | 73.418 | 60.286 | 71.706 | 0.385 |
| 1130 | 89.663 | 60.200 | 78.253 | 0.479 | 73.418 | 60.300 | 71.658 | 0.384 |
| 1230 | 89.672 | 60.199 | 78.205 | 0.478 | 73.282 | 60.299 | 71.658 | 0.384 |
| 1330 | 89.612 | 60.201 | 78.277 | 0.479 | 73.282 | 60.301 | 71.658 | 0.384 |
| 1430 | 89.589 | 60.204 | 78.253 | 0.479 | 73.350 | 60.305 | 71.706 | 0.385 |
| 1530 | 89.592 | 60.207 | 78.229 | 0.478 | 73.350 | 60.308 | 71.610 | 0.383 |
| 1630 | 89.586 | 60.215 | 78.277 | 0.479 | 73.282 | 60.315 | 71.658 | 0.384 |

ATTACHMENT 3.3A (Cont)

| <u>Initialization</u> | <u>Drywell</u> | <u>Torus</u> |
|-----------------------|----------------|--------------|
| Abs Press | 60.146 | 60.244 |
| Vap Press | 0.438 | 0.408 |
| Temp | 89.274 | 75.133 |
| Volume | 154476 | 115800 |

ATTACHMENT 3.3B

PRIMARY CONTAINMENT INTEGRATED LEAKAGE RATE TEST
 NYPA JAMES A. FITZPATRICK NUCLEAR POWER PLANT
 FROM 1630 ON MAY 13, 1985 TO 1630 ON MAY 14, 1985

ABSOLUTE TEST METHOD, MASS POINT ANALYSIS TEST RESULTS

| Time Hrs | Air Mass Pounds | (Adjusted) Air Mass Pounds | Leakage Rate Pct/Day | 95 Pct Conf Pct/Day | UCL |
|-------------|--------------------|----------------------------------|-------------------------|------------------------|----------|
| 0.000 | 80322.69 | 80322.69 | 0.000000 | 0.000000 | 0.000000 |
| 1.000 | 80331.16 | 80316.88 | 0.000000 | 0.000000 | 0.000000 |
| 2.000 | 80329.91 | 80301.35 | .318808 | .717293 | 1.036101 |
| 3.000 | 80332.36 | 80289.52 | .343724 | .118156 | .461880 |
| 4.000 | 80342.45 | 80285.33 | .305006 | .075838 | .380844 |
| 5.000 | 80345.13 | 80273.73 | .299885 | .045391 | .345276 |
| 6.000 | 80358.22 | 80272.54 | .269740 | .046376 | .316116 |
| 7.000 | 80356.73 | 80256.77 | .273965 | .033670 | .307635 |
| 8.000 | 80367.02 | 80252.78 | .265623 | .027017 | .292641 |
| 9.000 | 80374.05 | 80245.53 | .258705 | .022421 | .281126 |
| 10.000 | 80384.84 | 80242.04 | .247914 | .021359 | .269273 |
| 11.000 | 80392.48 | 80235.40 | .239785 | .019523 | .259309 |
| 12.000 | 80401.03 | 80229.67 | .232613 | .017963 | .250575 |
| 13.000 | 80406.44 | 80220.80 | .229031 | .015705 | .244735 |
| 14.000 | 80413.25 | 80213.33 | .226557 | .013749 | .240306 |
| 15.000 | 80430.96 | 80216.76 | .217646 | .015006 | .232652 |
| 16.000 | 80441.23 | 80212.75 | .209614 | .015481 | .225095 |
| 17.000 | 80439.32 | 80196.56 | .208786 | .013724 | .222510 |
| 18.000 | 80441.17 | 80184.13 | .210759 | .012391 | .223150 |
| 19.000 | 80460.30 | 80188.98 | .207119 | .011696 | .218815 |
| 20.000 | 80467.05 | 80181.45 | .204656 | .010832 | .215489 |
| 21.000 | 80474.53 | 80174.65 | .202790 | .009995 | .212785 |
| 22.000 | 80476.25 | 80162.09 | .203244 | .009114 | .212358 |
| 23.000 | 80480.70 | 80152.26 | .204498 | .008428 | .212926 |
| 24.000 | 80495.49 | 80152.77 | .203447 | .007808 | .211255 |

ATTACHMENT 3.3C

PRIMARY CONTAINMENT INTEGRATED LEAKAGE RATE TEST
NYPA JAMES A. FITZPATRICK NUCLEAR POWER PLANT
FROM 1630 ON MAY 13, 1985 TO 1630 ON MAY 14, 1985

INITIALIZATION AND CONTROL VARIABLES

Weighting Factors for Temperature and Dew Point Averaging

| <u>Zone 0</u> | <u>Zone 1</u> | <u>Zone 2</u> | <u>Zone 3</u> | <u>Zone 4</u> | <u>Zone 5</u> | <u>Zone 6</u> | <u>Zone 7</u> | <u>Zone 8</u> | <u>Zone A</u> | <u>Zone B</u> | <u>Zone C</u> |
|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| 0.11351 | 0.16502 | 0.35604 | 0.13137 | 0.04701 | 0.05337 | 0.07153 | 0.06215 | 1.00000 | 0.50000 | 0.50000 | 1.00000 |

Polynomial Coefficients for Vapor Pressure Conversion

0.919818D-14 0.172223D-10 0.105015D-08 0.349876D-06 0.179585D-04 0.112199D-02 0.211397D-01

STUDENT'S T CONSTANTS

1.95996 2.37226 2.82250

ATTACHMENT 3.3D

TYPE C PENETRATION LEAKAGE TO BE ADDED TO CALCULATED PCILRT LEAKAGE RATE

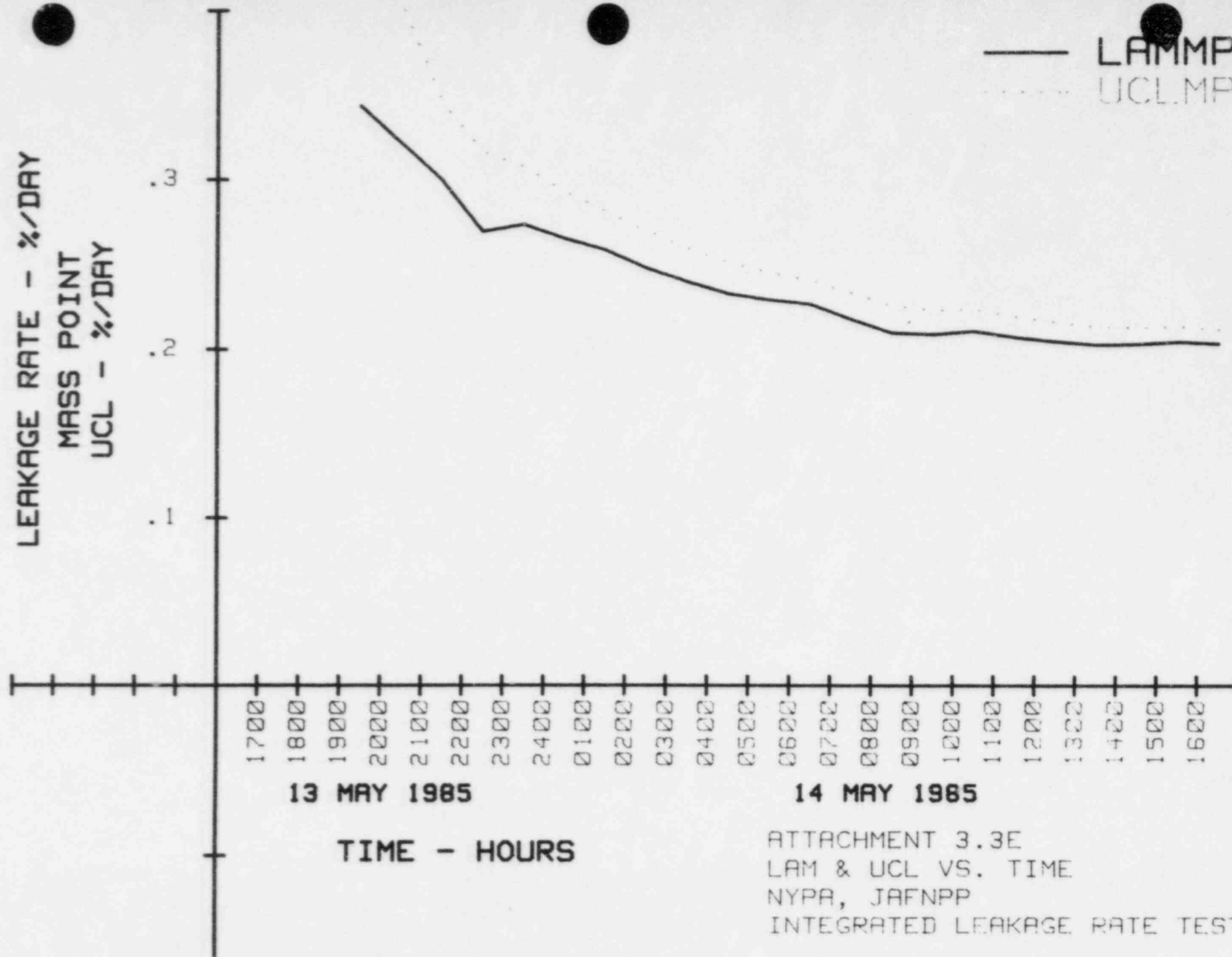
1. Penetrations to be penalized from initial valve line-up (see Types B and C data):

| <u>Penetration</u> | <u>Description</u> | <u>Leakage (SCFD)</u> |
|--------------------|---------------------------|---------------------------|
| X-9A | "A" Feedwater Line | 184.20 |
| X-9B | "B" Feedwater Line | 221.40 |
| X-14 | RWCU Supply | 13.54 |
| X-23 | Drywell Cooling Equipment | 30.44 |
| X-24 | Drywell Cooling Equipment | 6.71 |

| | |
|---------------------|----------|
| Total (percent/day) | 0.041572 |
|---------------------|----------|

LEAKAGE RATE - %/DAY
MASS POINT
UCL - %/DAY

— LAMMP
..... UCLMP



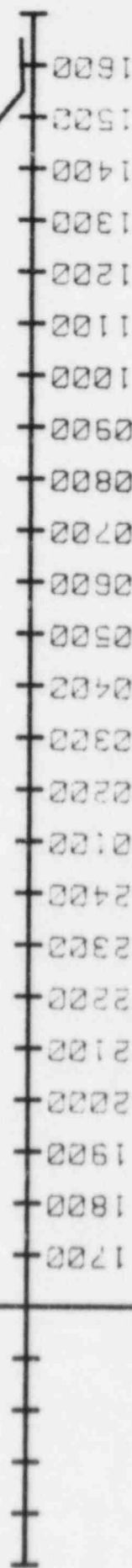
ATTACHMENT 3.3E
LAM & UCL VS. TIME
NYPA, JAFNPP
INTEGRATED LEAKAGE RATE TEST

MASS - LBM

80300

80250

80200



13 MAY 1985

14 MAY 1985

TIME - HOURS

ATTACHMENT 3.3F

MASS VS. TIME

NYPA, JAFNPP

INTEGRATED LEAKAGE RATE TEST

ATTACHMENT 3.3G

PRIMARY CONTAINMENT INTEGRATED LEAKAGE RATE TEST
 SUPERIMPOSED LEAKAGE VERIFICATION TEST
 NYPA JAMES A. FITZPATRICK NUCLEAR POWER PLANT
 FROM 1730 ON MAY 14, 1985 TO 2130 ON MAY 14, 1985

Input Variables

| Time Hr | Temp Degr | Drywell | | | Temp Degr | Torus | | |
|------------|--------------|-------------------|----------------|-------------------|--------------|-------------------|----------------|-------------------|
| | | Abs Press Psia | Dew Pt Degr | Vap Press Psia | | Abs Press Psia | Dew Pt Degr | Vap Press Psia |
| 1730 | 89.601 | 60.191 | 78.253 | 0.479 | 73.282 | 60.292 | 71.658 | 0.384 |
| 1750 | 89.554 | 60.186 | 78.276 | 0.479 | 73.350 | 60.286 | 71.610 | 0.383 |
| 1810 | 89.582 | 60.186 | 78.277 | 0.479 | 73.282 | 60.286 | 71.610 | 0.383 |
| 1830 | 89.627 | 60.182 | 78.253 | 0.479 | 73.213 | 60.283 | 71.610 | 0.383 |
| 1850 | 89.607 | 60.179 | 78.301 | 0.479 | 73.350 | 60.281 | 71.658 | 0.384 |
| 1910 | 89.592 | 60.177 | 78.276 | 0.479 | 73.282 | 60.278 | 71.610 | 0.383 |
| 1930 | 89.592 | 60.174 | 78.277 | 0.479 | 73.350 | 60.274 | 71.610 | 0.383 |
| 1950 | 89.600 | 60.171 | 78.325 | 0.480 | 73.282 | 60.272 | 71.610 | 0.383 |
| 2010 | 89.570 | 60.168 | 78.420 | 0.481 | 73.282 | 60.269 | 71.610 | 0.383 |
| 2030 | 89.613 | 60.165 | 78.276 | 0.479 | 73.213 | 60.265 | 71.610 | 0.383 |
| 2050 | 89.634 | 60.166 | 78.253 | 0.479 | 73.282 | 60.268 | 71.658 | 0.384 |
| 2110 | 89.626 | 60.163 | 78.348 | 0.480 | 73.350 | 60.264 | 71.658 | 0.384 |
| 2130 | 89.655 | 60.160 | 78.325 | 0.480 | 73.282 | 60.260 | 71.610 | 0.383 |

| <u>Initialization</u> | <u>Drywell</u> | <u>Torus</u> |
|-----------------------|----------------|--------------|
| Abs Press | 60.191 | 60.292 |
| Vap Press | 0.479 | 0.384 |
| Temp | 89.601 | 73.282 |
| Volume | 154476 | 115800 |

ATTACHMENT 3.3H
 PRIMARY CONTAINMENT INTEGRATED LEAKAGE RATE TEST
 SUPERIMPOSED LEAKAGE VERIFICATION TEST
 NYPA JAMES A. FITZPATRICK NUCLEAR POWER PLANT
 FROM 1730 ON MAY 14, 1985 TO 2130 ON May 14, 1985

ABSOLUTE TEST METHOD, MASS POINT ANALYSIS TEST RESULTS

| <u>Time Hrs</u> | <u>Air Mass Pounds</u> | <u>(Adjusted) Air Mass Pounds</u> | <u>Leakage Rate Pct/Day</u> | <u>95 Pct Conf Pct/Day</u> | <u>UCL</u> |
|---------------------|----------------------------|---|---------------------------------|--------------------------------|------------|
| 0.000 | 80462.26 | 80462.26 | 0.000000 | 0.000000 | 0.000000 |
| 0.333 | 80455.06 | 80450.30 | 0.000000 | 0.000000 | 0.000000 |
| 0.667 | 80456.20 | 80446.68 | .697084 | 1.843232 | 2.540316 |
| 1.000 | 80452.97 | 80438.69 | .665140 | .288623 | .953763 |
| 1.333 | 80441.54 | 80422.50 | .815458 | .244019 | 1.059477 |
| 1.667 | 80444.95 | 80421.15 | .759181 | .160372 | .919553 |
| 2.000 | 80435.02 | 80406.46 | .798572 | .116573 | .915145 |
| 2.333 | 80434.56 | 80401.24 | .787368 | .084730 | .872098 |
| 2.667 | 80431.91 | 80393.83 | .773855 | .065677 | .839532 |
| 3.000 | 80431.30 | 80388.46 | .750980 | .056990 | .807971 |
| 3.333 | 80426.50 | 80378.90 | .743252 | .046595 | .789847 |
| 3.667 | 80417.58 | 80365.22 | .757283 | .041050 | .798333 |
| 4.000 | 80415.28 | 80358.16 | .761626 | .034670 | .796296 |

SECTION 4

LOCAL LEAKAGE RATE TESTS (TYPES B AND C)

Attachments 4A and 4B, which follow, summarize the LLRT data which has been obtained from periodic testing performed since the February 1982 Type A Test. Pre-repaired data is provided for surveillance testing performed in 1985 and 1983. Values listed in both summaries are individual valve measurements, unless otherwise noted. Each penetration's leakage rate can be obtained from site reference material. These LLRTs were performed using "volumetric" leakage measuring equipment with a maximum range of 1,018 SCFD. No attempt to establish the actual leakage rate was made when the calibrated range of the test instrumentation was exceeded.

The acceptance criteria for Types B and C testing are in accordance with 10CFR50, Appendix J. The combined "as-left" leakage rate for all penetrations and valves subject to Types B and C tests shall be less than 0.6 La. The LLRTs performed in 1983 and 1985 were well below the acceptance criteria.

The data contained in this section are summarized below:

| <u>Attachment No.</u> | <u>Title</u> |
|-----------------------|---|
| 4A | 1985 LLRT Data (10-Year Plant Inservice Inspection) |
| 4B | 1983 LLRT Data (Refueling Outage) |
| 4C | Primary Containment Boundary Modifications |

ATTACHMENT 4A
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|--|----------------------|------------------------------------|---|--|---------------------|
| Drywell Stabilizer | | | | | |
| 0° (GE-90°) | B | "0" rings | 0.188 | 0.188 | |
| 45° (GE-135°) | B | "0" rings | 0.181 | 0.181 | |
| 90° (GE-180°) | B | "0" rings | 0.133 | 0.133 | |
| 135° (GE-225°) | B | "0" rings | 0.154 | 0.154 | |
| 180° (GE-270°) | B | "0" rings | 0.252 | 0.252 | |
| 225° (GE-315°) | B | "0" rings | 0.417 | 0.417 | |
| 270° (GE-0°) | B | "0" rings | 28.0 | <0.102 | 270° |
| 315° (GE-45°) | B | "0" rings | 0.155 | 0.155 | |
| Dry Well Head | B | "0" rings | 0.2886 | 0.2886 | |
| X-1A Equipment and Emergency Escape Hatch | B | "0" rings | 7.89 | 7.89 | |
| X-1B Equipment Hatch | B | "0" rings | 0.1404 | 0.1404 | |
| X-2A Personnel Access Hatch | B | "0" rings | 91.387 | 91.387 | |
| X-4 Drywell Head Manhole | B | "0" rings | 0.2886 | 0.2886 | |
| X-6 CRD Removal Hatch | B | "0" rings | <0.102 | <0.102 | |
| X-7A "A" Main Steam Line | C | 29-AOV-80A(IPC) 29-AOV-86A(OPC) | 0.298 (Combined) | 0.298 (Combined) | |
| X-7B "B" Main Steam Line | C | 29-AOV-80B(IPC) 29-AOV-86B(OPC) | >1018 (Combined) | 16.13 (Combined) | AOV-86B |
| X-7C "C" Main Steam Line | C | 29-AOV-80C(IPC) 29-AOV-86C(OPC) | 0.102 (Combined) | 0.102 (Combined) | |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|-----------------------------|------------------|--|--|--|---|
| X-7D "D" Main Steam Line | C | 29-AOV-80D(IPC) 29-AOV-86D(OPC) | 0.141 (Combined) | 0.141 (Combined) | |
| X-8 Condensate Drain | C | 29-MOV-74(IPC) 29-MOV-77(OPC) | 826.6 16.69 | <0.102 16.69 | MOV-74 ground bonnet mating surfaces and replaced gasket. |
| X-9A Feedwater | C | 34-FWS-28A(IPC) 13-MOV-21(OPC) 34-NRV-111A(OPC) RWC-62(OPC) | 0.520 (FWS-28A) 184.2 (MOV-21) (NRV-111A) 17.9 (RWC-62) | 0.520 (FWS-28A) 184.2 (MOV-21) (NRV-111A) 17.9 (RWC-62) | |
| X-9B Feedwater | C | 34-FWS-28B(IPC) 23-MOV-19(OPC) 34-NRV-111B(OPC) | 0.674 (FWS-28B) 343.5 (MOV-19) (NRV-111B) | 0.674 (FWS-28B) 221.4 (MOV-19) (NRV-111B) | NRV-1118 machined disc and seat. Replaced internals and adjusted valve. |
| X-10 Steam to RCIC Turbine | C | 13-MOV-16(IPC) 13-MOV-15(OPC) | >0.102 30.4 | <0.102 4.39 | MOV-15 lapped disc and seat and body/ bonnet tightened. |
| X-11 Steam to HPCI Turbine | C | 23-MOV-15(IPC) 23-MOV-16(OPC) 23-MOV-60(OPC) | 14.04 (Combined) | 14.04 (Combined) | |
| X-12 Shutdown Supply to RHR | C | 10-MOV-17(IPC) 10-MOV-18(OPC) | >1018 >1018 | 26.72 23.82 | MOV-17 lapped disc and seat replaced MOV-18 new installation |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|--|----------------------|--|--|---|--|
| X-13A RHR Return | C | 10-MOV-27A(OPC) 10-MOV-25A(OPC) | >1018 5.53 | 81.74 40.92 | MOV-27A repacked MOV-25A repacked |
| X-13B RHR Return | C | 10-MOV-27B(OPC) 10-MOV-25B(OPC) | 73.9 119.6 | 73.9 119.6 | |
| X-14 RWCU Supply to Recirculation Pumps | C | 12-MOV-15(IPC) 12-MOV-18(OPC) 12-MOV-80(OPC) | 71.26 (MOV-15) 13.54 (MOV-18) (MOV-80) | 9.75 (MOV-15) 13.54 (MOV-18) (MOV-80) | MOV-15 machined stem and wedge. Lapped wedge and seat. Replaced gasket and packing. |
| X-16A Core Spray Pump Discharge | C | 14-MOV-11A(OPC) 14-MOV-12A(OPC) | 0.102 0.231 | 0.102 0.231 | |
| X-16B Core Spray Pump Discharge | C | 14-MOV-11B(OPC) 14-MOV-12B(OPC) | 0.178 0.102 | 0.178 0.102 | |
| X-17 RPV Head Spray | C | 10-MOV-32(IPC) 10-MOV-33(OPC) | 0.855 15.06 | 0.855 15.06 | |
| X-18 Floor Sump Pump Discharge | C | 20-MOV-82(IPC) 20-AOV-83(OPC) | 1.74 19.95 | 1.74 19.95 | |
| X-19 Equipment Sump Pump Discharge | C | 20-MOV-94(IPC) 20-MOV-95(OPC) | >1018 269.0 | 18.9 1.53 | MOV-94 cleaned seat and disc. RDW-98A repacked lapped seat. |
| X-21 Service Air | C | 39-SAS-10(IPC) 39-SAS-9(OPC) | >1018 4.63 | 15.6 4.63 | SAS-10 lapped disc and seat, cleaned, new gasket. |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|--|------------------|--------------------------------|-------------------------------------|--------------------------------------|--|
| X-22 Instrument Air | C | IAS-22(IPC) | 0.242 | 0.242 | |
| | | IAS-21(OPC) | 0.102 | 0.102 | |
| | | IAS-23(OPC) | 0.102 | 0.102 | |
| X-23 Cooling Water Supply | C | 46-ESW-16B(OPC) | <0.102 | 3.48 | ESW-16B disassembled for drywell cooling. |
| | | 15-RBC-24A(OPC) | <0.102 | <0.102 | |
| | | 15-AOV-130A(OPC) | 30.44 | 30.44 | |
| X-24 Cooling Water Supply | C | 46-ESW-16A(OPC) | 65.05 | 6.71 | ESW-16A lapped disc and seat and cleaned valve internals. |
| | | 15-RBC-24B(OPC) | <0.102 | <0.102 | |
| | | 15-AOV-130B(OPC) | 13.89 | 13.89 | |
| X-25 Drywell Inerting and CAD and Purge X-71 | C | 27-AOV-111(OPC) | <0.102 (AOV-111) | <0.102 (AOV-111) | CV-68 lapped seat and replaced disc, spring, and gasket. AOV-131A replaced plug, stem, seat, and repacked. |
| | | 27-AOV-112(OPC) | (AOV-112) | (AOV-112) | |
| | | 27-AOV-131A(OPC) | >1018 (AOV-131A) | 9.37 (AOV-131A) | |
| | | CV-68(OPC) | (CV-68) | (CV-68) | |
| | | 27-AOV-131B(OPC) | 6.36 (AOV-131B) | 6.36 (AOV-131B) | |
| | | CV-69(OPC) | (CV-69) | (CV-69) | |
| X-26A Containment Atmospheric Sampling | C | 27-SOV-119F1(OPC) | 0.25 | 0.25 | SOV-120A cleaned replaced disc spring, body o-ring, piston ring. |
| | | 27-SOV-119F2(OPC) | 0.102 | 0.102 | |
| | | 27-SOV-120A(OPC) | 21.3 | <0.102 | |
| | | 27-SOV-120B(OPC) | 41.1 | <0.102 | |
| | | 27-SOV-120E1(OPC) | 0.102 | 0.102 | |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|--|------------------|--------------------------------|-------------------------------------|--------------------------------------|---------------------|
| | | 27-SOV-120E2(OPC) | 0.102 | 0.102 | SOV-120B cleaned |
| | | 27-SOV-122A(OPC) | >1018 | 0.102 | replaced disc |
| | | 27-SOV-122B(OPC) | 98.2 | <0.102 | spring, body |
| | | 27-SOV-122E1(OPC) | 1.67 | 1.67 | o-ring, piston |
| | | 27-SOV-122E2(OPC) | 0.386 | 0.386 | ring. |
| | | 27-SOV-121A(OPC) | 4.38 | 4.38 | SOV-122A cleaned |
| | | | | 0.119 | replaced disc |
| | | 27-SOV-121B(OPC) | 33.8 | | spring, body |
| | | | | | o-ring, piston |
| | | | | | ring. |
| | | | | | SOV-122B |
| | | | | | SOV-121B cleaned |
| | | | | | replaced disc |
| | | | | | spring, body |
| | | | | | o-ring, piston |
| | | | | | ring. |
| X-26A, X-26B Containment Vent and Purge | C | 27-AOV-113(OPC) | 7.35 (AOV-113) | 7.35 (AOV-113) | |
| | | 27-AOV-114(OPC) | (AOV-114) | (AOV-114) | |
| | | 27-MOV-113(OPC) | 0.179 (MOV-113) | 0.179 (MOV-113) | |
| | | 27-MOV-122(OPC) | (MOV-122) | (MOV-122) | |
| X-31Ac "A" Recirculation Pump Mini-Purge | C | 02-RWR-13A(IPC) | >1018 (RWR-13A) | 2.8 (RWR-13A) | RWR-13A lapped |
| | | 02-RWR-14A(IPC) | (RWR-14A) | (RWR-14A) | disc and seat. |
| | | 02-RWR-40A(OPC) | 11.2 (RWR-40A) | 11.2 (RWR-40A) | Cleaned valve |
| | | | (RWR-14A) | (RWR-14A) | internals and |
| | | | | | replaced spring |
| | | | | | and gasket. |
| X-31Ad Drywell Inert and Purge | C | 27-SOV-135A(OPC) | 2.85 | 11.04 | SOV-135A |
| | | 27-SOV-135B(OPC) | 328.3 | 11.4 | SOV-135B new |
| | | | | | plunger assembly |
| | | | | | viton disc, |
| | | | | | piston ring, |
| | | | | | body o-ring. |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|--|------------------|---|--|--|--|
| X-31Bc "B" Recirculation Pump Mini-Purge | C | 02-RWR-13B(IPC) 02-RWR-14B(IPC) 02-RWR-40B(OPC) | 79.9 (RWR-13B) (RWR-14B) 7.48 (RWR-40B) (RWR-14B) | 4.55 (RWR-13B) (RWR-13B) 7.48 (RWR-40B) (RWR-14B) | RWR-14B re-placed internals RWR-13B lapped disc and seat. Cleaned valve internals and replaced disc, spring, and gasket. |
| X-35A TIP Probe | C/B | Ball Valve (OPC) "O" ring (OPC) | 0.347 0.102 | 0.488 0.282 | X-35A disassembled for maintenance. |
| X-35B TIP Probe | C/B | Ball Valve (OPC) "O" ring (OPC) | 0.79 0.102 | 2.5 0.116 | X-35B disassembled for maintenance. |
| X-35C TIP Probe | C/B | Ball Valve (OPC) "O" ring (OPC) | 3.17 0.102 | <0.102 0.228 | X-35C disassembled for maintenance. Ball valve replaced. |
| X-35D TIP Probe | C/B | Ball Valve (OPC) "O" ring (OPC) | 0.401 0.102 | 0.79 2.74 | X-35D disassembled for maintenance. |
| X-35E TIP Purge | C/B | TP-1 (OPC) "O" ring (OPC) | 0.435 0.102 | 0.435 0.102 | |
| X-39A Containment Spray | C | 10-MOV-26A(OPC) 10-MOV-31A(OPC) | >101.8 (Combined) | 42.1 (Combined) | MOV-26A lapped wedge and seat. |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|-----------------------------------|----------------------|--|--|--|--|
| | | RHR-52A(OPC) | | | Replaced gasket and packing MOV-31A lapped wedge and seat, polished stem, repacked. |
| X-39B Containment Spray | C | 10-MOV-26B(OPC) 10-MOV-31B(OPC) RHR-52B(OPC) | 136.9 (Combined) | 41.3 (Combined) | MOV-26B lapped disc and seat and replaced gasket. |
| X-41 Recirculation Loop Sample | C | 02-AOV-39(IPC) RWR-255(IPC) 02-AOV-40(OPC) | 0.266 (AOV-39) (RWR-255) 0.109 (AOV-40) (RWR-255) | 0.266 (AOV-39) (RWR-255) 0.109 (AOV-40) (RWR-255) | |
| X-42 Standby Liquid Control | C | 11-SLC-17(IPC) 11-SLC-16(OPC) | 0.447 0.987 | 0.447 0.987 | |
| X-45 Leak Rate Analyzer | C | 16-1-AOV-101A(OPC) 16-1-AOV-101B(OPC) LRA-20(OPC) LRA-21(OPC) | 0.3415 (AOV-101A) (AOV-101B) <0.102 (LRA-20) (LRA-21) | 0.3415 (AOV-101A) (AOV-101B) <0.102 (LRA-20) (LRA-21) | |
| X-55B Drywell CAD Inert and Purge | C | 27-SOV-125A(OPC) 27-SOV-125B(OPC) | 1.068 >1018 | 1.068 0.364 | 27-SOV-125B installed new valve. |
| X-58B CAD System | C | 27-SOV-122F1(OPC) 27-SOV-122F2(OPC) | 0.251 0.1694 | 0.251 0.1694 | |
| X-58C CAD System | C | 27-SOV-120F1(OPC) 27-SOV-120F2(OPC) | 0.786 0.1501 | 0.786 0.1501 | |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|---|----------------------|--|---|--|---|
| X-58D CAD System | C | 27-SOV-123F1(OPC) 27-SOV-123F2(OPC) | <0.102 <0.102 | <0.102 <0.102 | |
| X-59 Drywell CAD Inert and Purge | C | 27-SOV-123A(OPC) 27-SOV-123B(OPC) 27-SOV-123E1(OPC) 27-SOV-123E2(OPC) | 101.8 357.0 0.102 0.923 | 0.102 0.923 | X-59; SOV-123A, 123B line cut and capped. |
| X-61 Breathing Air | C | BAS-5(IPC) BAS-4(OPC) | 16.38 125.21 | 16.38 0.72 | BAS-4 lapped disc and seat. |
| X-62 Drywell Cooling Return | C | RBC-26B(OPC) 15-AOV-131B(OPC) | 2.55 1.41 | 2.55 1.41 | |
| X-63 "B" Recirculation Pump MTR Cooling Supply | C | 15-RBC-21A(OPC) 46-ESW-15B(OPC) 15-AOV-132A(OPC) | 0.127 33.64 2.9 | 0.127 33.64 2.9 | |
| X-64 "A" Recirculation Pump MTR Cooling Return | C | 15-RBC-22A(OPC) 15-AOV-133A(OPC) | 6.7 0.81 | 6.7 0.81 | |
| X-65 Equipment Drain Pump Cooler Return | C | 15-RBC-33(OPC) 15-AOV-134A(OPC) | 4.95 6.3 | 4.95 6.3 | |
| X-66 "A" Drywell Cooler Assembly Return | C | 15-RBC-26A(OPC) 15-AOV-131A(OPC) | 207.0 9.92 | 9.0 9.92 | RBC-26A, lapped seat, disc, repacked. |
| X-67 "A" Recirculation Pump MTR Cooling Supply | C | 15-RBC-21B(OPC) 46-ESW-15B(OPC) 15-AOV-132B(OPC) | 0.102 0.102 0.324 | 0.102 0.102 0.324 | |
| X-68 "B" Recirculation Pump MTR Cooling Return | C | 15-RBC-22B(OPC) 15-AOV-133B(OPC) | 3.72 0.835 | 3.72 0.835 | |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|------------------------|----------------------|------------------------------------|---|--|---------------------|
| X-100A Elect | B | "0" rings | 0.525 | 0.525 | |
| X-100B Elect | B | "0" rings | 0.554 | 0.127 | X-100B Elect. |
| X-100C Elect | B | "0" rings | 0.242 | 0.242 | |
| X-100D Elect | B | "0" rings | 0.639 | 0.639 | |
| X-100F Elect | B | "0" rings | 0.2692 | 0.2692 | |
| X-100G Elect | B | "0" rings | 0.102 | 0.102 | |
| X-100K Elect | B | "0" rings | <0.102 | <0.102 | |
| X-101A Elect | B | "0" rings | 0.303 | 0.303 | |
| X-101B Elect | B | "0" rings | 0.453 | 0.453 | |
| X-101C Elect | B | "0" rings | 0.239 | 0.239 | |
| X-101D Elect | B | "0" rings | 0.171 | 0.171 | |
| X-101E Elect | B | "0" rings | 0.401 | 0.401 | |
| X-101F Elect | B | "0" rings | 0.1119 | 0.1119 | |
| X-103A Elect | B | "0" rings | 0.102 | 0.102 | |
| X-103B Elect | B | "0" rings | 0.102 | 0.102 | |
| X-104C Elect | B | "0" rings | 1.018 | 0.102 | X-104C Elect. |
| X-104D Elect | B | "0" rings | 0.102 | 0.102 | |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|------------------------|----------------------|------------------------------------|---|--|---------------------|
| X-104E Elect | B | "O" rings | 0.776 | 0.776 | |
| X-106A Elect | B | "O" rings | 0.948 | 0.102 | X-106A Elect. |
| X-106B Elect | B | "O" rings | 0.5614 | 0.5614 | |
| X-107 Elect | B | "O" rings | 0.102 | 0.102 | |
| X-108 Elect | B | "O" rings | 0.207 | 0.207 | |
| X-109 Elect | B | "O" rings | 0.489 | 0.489 | |
| X-110C Elect | B | "O" rings | 0.1628 | 0.1628 | |
| X-110D Elect | B | "O" rings | 0.1409 | 0.1409 | |
| X-111B Elect | B | "O" rings | 0.4591 | 0.1786 | X-111B Elect. |
| X-200A Torus Access | B | "O" rings | 0.1521 | 0.102 | X-200A |
| X-200B Torus Access | B | "O" rings | 0.3949 | 0.3949 | |
| X-200C Torus Access | B | "O" rings | 0.332 | 0.332 | |
| X-202BG Vacuum Breaker | C | 27-AOV-101B(OPC) | <0.102 (AOV-101B) | <0.102 (AOV-101B) | |
| | | VB-7(OPC) | (VB-7) | (VB-7) | |
| | | 27-AOV-101A(OPC) | 4.79 (AOV-101A) | 4.79 (AOV-101A) | |
| | | VB-6(OPC) | (VB-6) | (VB-6) | |
| X-202F Vacuum Breaker | B | "O" ring(VB-1) | 0.285 | 0.285 | |
| X-202G Vacuum Breaker | B | "O" ring(VB-2) | 0.210 | 0.102 | VB-2 |
| X-202H Vacuum Breaker | B | "O" ring(VB-3) | 0.1369 | 0.1369 | |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|---------------------------------------|------------------|--------------------------------|-------------------------------------|--------------------------------------|--|
| X-202I Vacuum Breaker | B | "O" ring(VB-4) | 0.1328 | 0.1328 | |
| X-202J Vacuum Breaker | B | "O" ring(VB-5) | 0.2397 | 0.2397 | |
| X-203A O ₂ Analyzer Sample | C | 27-SOV-119A(OPC) | 16.03 | 0.284 | SOV-119A cleaned new disc spring, body o-ring and piston ring. |
| | | 27-SOV-119B(OPC) | 0.1817 | 0.1817 | |
| | | 27-SOV-119E1(OPC) | 2.81 | 2.81 | |
| | | 27-SOV-119E2(OPC) | 0.1129 | 0.1129 | |
| X-203B O ₂ Analyzer Sample | C | 27-SOV-124A(OPC) | 7.5 | 7.5 | |
| | | 27-SOV-124B(OPC) | 0.228 | 0.228 | |
| | | 27-SOV-124E1(OPC) | 0.171 | 0.171 | |
| | | 27-SOV-124E2(OPC) | 0.35 | 0.35 | |
| | | 27-SOV-124F1(OPC) | 0.115 | 0.115 | |
| | | 27-SOV-124F2(OPC) | 0.378 | 0.378 | |
| X-205 Drywell Inert CAD and Purge | C | 27-AOV-117(OPC) | >1018 (AOV-117) | 0.338 (AOV-117) | AOV-117, 118 cleaned valve and installed new "T" ring and "O" ring |
| | | 27-AOV-118(OPC) | (AOV-118) | (AOV-118) | |
| | | 27-MOV-117(OPC) | 0.33 (MOV-117) | 0.33 (MOV-117) | |
| | | 27-MOV-123(OPC) | (MOV-123) | (MOV-123) | |
| X-211A Containment Spray | C | 10-MOV-34A(OPC) | >101.8 | 4.16 | MOV- |
| | | 10-MOV-38A(OPC) | (Combined) | (Combined) | |
| | | 10-MOV-39A(OPC) | | | |
| X-211B Containment Spray | C | 10-MOV-34B(OPC) | 153.7 | 96.15 | MOV-39B ground seat and disc. Cleaned valve internals and replaced gasket. |
| | | 10-MOV-38B(OPC) | (Combined) | (Combined) | |
| | | 10-MOV-39B(OPC) | | | |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|------------------------------------|------------------|--|--|---|--|
| X-212 RCIC Turbine Exhaust | C | RCIC-04(OPC) RCIC-05(OPC) 13-MOV-130(OPC) | >1018 >1018 0.2 | 38.17 52.93 0.2 | RCIC-04 lapped seat. RCIC-03 lapped wedge and seat. |
| X-214 HPCI Turbine Exhaust | C | 23-HPI-12(OPC) 23-HPI-65(OPC) | 96.6 >1018 | 96.35 88.51 | HPI-65 cleaned, new gasket. HPI-11 Cleaned ground seat, new gasket |
| X-217 HPCI Turbine Exhaust Vent | C | 23-MOV-59(OPC) 23-HPI-403(OPC) 23-HPI-402(OPC) | 9.45 (Combined) | 9.55 (Combined) | MOV-59 repacked. |
| X-218 Leak Rate Analyzer | C | LRA-13(OPC) LRA-14(OPC) AOV-102A(OPC) AOV-102B(OPC) | 0.203 (LRA-13) (LRA-14) 5.3 (AOV-102A) (AOV-102B) | 0.203 (LRA-13) (LRA-14) 5.3 (AOV-102A) (AOV-102B) | |
| X-220 Drywell CAD Inert and Purge | C | 27-AOV-132A(OPC) CV-67(OPC) 27-AOV-132B(OPC) CV-70(OPC) 27-AOV-115(OPC) 27-AOV-116(OPC) | 4.3 (AOV-132A) (CV-67) 0.116 (AOV-132B) (CV-70) >1018 (AOV-115) (AOV-116) | 4.3 (AOV-132A) (CV-67) 0.116 (AOV-132B) (CV-70) 1.84 (AOV-115) (AOV-116) | AOV-116 replaced operator pin. |
| X-221 Condensate from RCIC Turbine | C | 13-RCIC-07(OPC) 13-RCIC-08(OPC) | >101.8 >101.8 | 23.41 5.27 | RCIC-07 lapped piston and seat, installed new spring and gasket, and repacked valve. |

ATTACHMENT 4A (Cont.)
1985 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|------------------------|----------------------|------------------------------------|---|--|--|
| X-231A Elect | B | "O" rings | 0.597 | 0.597 | RCIC-08 lapped seat and re- placed gasket. |

ATTACHMENT 4B
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|--|----------------------|------------------------------------|---|--|---------------------|
| Drywell Stabilizer | | | | | |
| 0° (GE-90°) | B | "0" rings | 0.5003 | 0.5003 | |
| 45° (GE-135°) | B | "0" rings | 0.6153 | 0.6153 | |
| 90° (GE-180°) | B | "0" rings | 0.401 | 0.401 | |
| 135° (GE-225°) | E | "0" rings | 0.3206 | 0.3206 | |
| 180° (GE-270°) | B | "0" rings | 0.5156 | 0.5156 | |
| 225° (GE-315°) | B | "0" rings | 0.539 | 0.539 | |
| 270° (GE-0°) | B | "0" rings | 0.6036 | 0.6036 | |
| 315° (GE-45°) | B | "0" rings | 0.6153 | 0.6153 | |
| Dry Well Head | B | "0" rings | 0.102 | 0.102 | |
| X-1A Equipment and Emergency Escape Hatch | B | "0" rings | 1.593 | 1.593 | |
| X-1B Equipment Hatch | B | "0" rings | 0.2229 | 0.2229 | |
| X-2A Personnel Access Hatch | B | "0" rings | 42.25 | 42.25 | |
| X-4 Drywell Head Manhole | B | "0" rings | 0.2682 | 0.2682 | |
| X-6 CRD Removal Hatch | B | "0" rings | 0.2957 | 0.2957 | |
| X-7A "A" Main Steam Line | C | 29-AOV-80A(IPC) 29-AOV-86A(OPC) | 14.761 (Combined) | 14.761 (Combined) | |
| X-7B "B" Main Steam Line | C | 29-AOV-80B(IPC) 29-AOV-86B(OPC) | 20.36 914.164 | <0.102 <0.102 | |
| X-7C "C" Main Steam Line | C | 29-AOV-80C(IPC) 29-AOV-86C(OPC) | 18.4258 (Combined) | 18.4258 (Combined) | |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| Penetration No. | Type Test | Equipment/Valves Tested | Pre-Repair Leakage (scf/day) | Post-Repair Leakage (scf/day) | Repair/Notes |
|-----------------------------|-----------|--|---|---|--|
| X-7D "D" Main Steam Line | C | 29-AOV-80D(IPC) 29-AOV-86D(OPC) | >1018 <0.102 | 112.489 <0.102 | |
| X-8 Condensate Drain | C | 29-MOV-74(IPC) 29-MOV-77(OPC) | 2.825 5.0034 | 2.825 5.0034 | |
| X-9A Feedwater | C | 34-FWS-28A(IPC) 13-MOV-21(OPC) 34-NRV-111A(OPC) RWC-62(OPC) | >1018(FWS-28A) >1018(MOV-21) (NRV-111A) (RWC-62) | 12.826(FWS-28A) 147.61(MOV-21) (NRV-111A) (RWC-62) | FWS-28A cleaned valve, ground seat, and replaced disc. NRV-111A cleaned valve, ground seat and disc, cleaned operator shaft and cylinder, and replaced O-ring and gasket. |
| X-9B Feedwater | C | 34-FWS-28B(IPC) 23-MOV-19(OPC) 34-NRV-111B(OPC) | >1018(FWS-28B) >1018(MOV-19) (NRV-111B) | 6.275(FWS-28B) 32.5251(MOV-19) (NRV-111B) | FWS-28B cleaned valve, ground seat, and replaced disc. |
| X-10 Steam to RCIC Turbine | C | 13-MOV-16(IPC) 13-MOV-15(OPC) | <0.102 5.1205 | <0.102 5.1205 | |
| X-11 Steam to HPCI Turbine | C | 23-MOV-15(IPC) 23-MOV-16(OPC) 23-MOV-60(OPC) | >1018 (Combined) | 3.0947 (Combined) | MOV-16 repacked valve |
| X-12 Shutdown Supply to RHR | C | 10-MOV-17(IPC) 10-MOV-18(OPC) | 191.893 >1018 | 191.893 1.99 | MOV-18 replaced wedge, ground seats. |
| X-13A RHR Return | C | 10-MOV-27A(OPC) 10-MOV-25A(OPC) | 81.44 124.196 | 81.44 124.196 | |
| X-13B RHR Return | C | 10-MOV-27B(OPC) 10-MOV-25B(OPC) | 81.185 115.54 | 81.185 115.54 | |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| Penetration No. | Type Test | Equipment/Valves Tested | Pre-Repair Leakage (scf/day) | Post-Repair Leakage (scf/day) | Repair/Notes |
|--|--------------|--|---|---|---|
| X-14 RWCU Supply to Recirculation Pumps | C | 12-MOV-15(IPC) 12-MOV-18(OPC) 12-MOV-80(OPC) | 28.504(MOV-15) 6.342(MOV-18) (MOV-80) | 28.504(MOV-15) 6.342(MOV-18) (MOV-80) | |
| X-16A Core Spray Pump Discharge | C | 14-MOV-11A(OPC) 14-MOV-12A(OPC) | <1.02 29.165 | <1.02 29.165 | |
| X-16B Core Spray Pump Discharge | C | 14-MOV-11B(OPC) 14-MOV-12B(OPC) | 0.1822 3.3085 | 0.1822 3.3085 | |
| X-17 RPV Head Spray | C | 10-MOV-32(IPC) 10-MOV-33(OPC) | 30.2855 17.5605 | 30.2855 17.5605 | |
| X-18 Floor Sump Pump Discharge | C | 20-MOV-82(IPC) 20-AOV-83(OPC) | 0.803 3.28 | 0.803 3.28 | |
| X-19 Equipment Sump Pump Discharge | C | 20-MOV-94(IPC) 20-AOV-95(OPC) | >1018 >1018 | 1.04117 0.579 | MOV-94 ground seat, replaced wedge, and repacked with new rings. |
| X-21 Service Air | C | 39-SAS-10(IPC) 39-SAS-9(OPC) | >1018 <0.102 | 1.379 <0.102 | SAS-10 cleaned and lapped seat and disc, replaced gasket. SAS-11 inspected valve and lapped seat. |
| X-22 Instrument Air | C | IAS-22(IPC) IAS-21(OPC) IAS-23(OPC) | >1018 12.98 <0.102 | 21.429 12.98 <0.102 | IAS-22 ground and lapped seat, replaced gasket. |
| X-23 Cooling Water Supply | C | 46-ESW-16B(OPC) 15-RBC-24A(OPC) 15-AOV-130A(OPC) | <0.102 <0.102 39.3966 | <0.102 <0.102 39.3966 | AOV-130A new installation. |
| X-24 Cooling Water Supply | C | 46-ESW-16A(OPC) 15-RBC-24B(OPC) 15-AOV-130B(OPC) | >1018 <0.102 <0.102 | 2.1475 <0.102 <0.102 | AOV-130B new installation. ESW-16A ground disc and seat, new gasket. |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| Penetration No. | Type Test | Equipment/Valves Tested | Pre-Repair Leakage (scf/day) | Post-Repair Leakage (scf/day) | Repair/Notes |
|--|-----------|-------------------------|------------------------------|-------------------------------|--|
| X-25 Drywell Inerting and CAD and Purge X-71 | C | 27-AOV-111(OPC) | >1018(AOV-111) | 0.3547(AOV-111) | AOV-111, 112 cleaned valves, replaced T rings and O-rings. CV-68 machined plug seat, replaced spring, replaced gasket, ground seat. |
| | | 27-AOV-112(OPC) | (AOV-112) | (AOV-112) | |
| | | 27-AOV-131A(OPC) | >1018(AOV-131A) | 4.983(AOV-131A) | |
| | | CV-68(OPC) | (CV-68) | (CV-68) | |
| | | 27-AOV-131B(OPC) | 2.5094(AOV-131B) | 2.5094(AOV-131B) | |
| | | CV-69(OPC) | (CV-69) | (CV-69) | |
| X-26A Containment Atmospheric Sampling | C | 27-SOV-119F1(OPC) | <0.102 | <0.102 | SOV-119F1,F2 new installation. |
| | | 27-SOV-119F2(OPC) | <0.102 | <0.102 | |
| | | 27-SOV-120A(OPC) | 127.25 | <0.102 | |
| | | 27-SOV-120B(OPC) | 6.8613 | 6.8613 | SOV-120E1,E2 new installation. |
| | | 27-SOV-120E1(OPC) | <0.102 | <0.102 | |
| | | 27-SOV-120E2(OPC) | <0.102 | <0.102 | |
| | | 27-SOV-122A(OPC) | >1018 | <0.102 | SOV-122E1,E2 new installation. |
| | | 27-SOV-122B(OPC) | 2.2294 | 2.2294 | |
| | | 27-SOV-122E1(OPC) | <0.102 | <0.102 | |
| | | 27-SOV-122E2(OPC) | <0.102 | <0.102 | |
| | | 27-SOV-121A(OPC) | 4.072 | 4.02 | |
| | | 27-SOV-121B(OPC) | 9.6557 | 9.6557 | |
| X-26A, X-26B Containment Vent and Purge | C | 27-AOV-113(OPC) | 0.2428(AOV-113) | 0.2428(AOV-113) | |
| | | 27-AOV-114(OPC) | (AOV-114) | (AOV-114) | |
| | | 27-MOV-113(OPC) | 0.2718(MOV-113) | 0.2718(MOV-113) | |
| | | 27-MOV-122(OPC) | (MOV-122) | (MOV-122) | |
| X-31Ac "A" Recirculation Pump Mini-Purge | C | 02-RWR-13A(IPC) | >1018(RWR-13A) | 7.13(RWR-13A) | RWR-13A machined plug, lapped plug and seat, replaced gasket and spring. |
| | | 02-RWR-14A(IPC) | (RWR-14A) | (RWR-14A) | |
| | | 02-RWR-40A(OPC) | >1018(RWR-40A) | 13.28(RWR-40A) | |
| | | | (RWR-14A) | (RWR-14A) | |
| X-31Ad Drywell Inert and Purge | C | 27-SOV-135A(OPC) | 8.037 | 8.037 | SOV-135B cleaned valve, replaced viton plug, seat, piston rings, o-rings, piston, piston rod, connection link, plunger assembly, and disc. |
| | | 27-SOV-135B(OPC) | >1018 | 26.57 | |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|--|------------------|---|---|--|--|
| X-31Bc "B" Recirculation Pump Mini-Purge | C | 02-RWR-13B(IPC) 02-RWR-14B(IPC) 02-RWR-40B(OPC) | 30.133(RWR-13B) (RWR-14B) 34.256(RWR-40B) (RWR14B) | 30.133(RWR-13B) (RWR-14B) 34.256(RWR-40B) (RWR-14B) | |
| X-35A TIP Probe | C/B | Ball Valve (OPC) "O" ring (OPC) | 26.824 0.207 | 26.824 0.207 | |
| X-35E TIP Probe | C/B | Ball Valve (OPC) "O" ring (OPC) | 0.964 0.205 | 0.964 0.205 | |
| X-35C TIP Probe | C/B | Ball Valve (OPC) "O" ring (OPC) | 3.346 0.135 | 3.346 0.135 | |
| X-35D TIP Probe | C/B | Ball Valve (OPC) "O" ring (OPC) | 6.795 0.0208 | 6.795 0.0208 | |
| X-35E TIP Purge | C/B | TF-1 (OPC) "O" ring (OPC) | 1.006 0.132 | 1.006 0.132 | |
| X-36 CRD Return | C | CRD-113(IPC) CRD-110(OPC) | 70.14 >1018 | 1.5422 (Combined) | |
| X-39A Containment Spray | C | 10-MOV-26A(OPC) 10-MOV-31A(OPC) RHR-52A(OPC) | >1018 (Combined) | 1.5779 (Combined) | RHR-52A cut-out valve and replaced with new one. |
| X-39B Containment Spray | C | 10-MOV-26B(OPC) 10-MOV-31B(OPC) RHR-52B(OPC) | 533.941 (Combined) | 74.212 (Combined) | MOV-26B inspected valve operator, increased torque switch setting, machined rings, replaced wedge and rings. |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|-----------------------------------|----------------------|--|---|---|---|
| X-41 Recirculation Loop Sample | C | 02-AOV-39(IPC) RWR-255(IPC) 02-AOV-40(OPC) | >1018(AOV-39) (RWR-255) 2.036(AOV-40) (RWR-255) | 1.481(AOV-39) (RWR-255) 2.036(AOV-40) (RWR-255) | AOV-39 repacked valve, ground and lapped seat and plug. |
| X-42 Standby Liquid Control | C | 11-SLC-17(IPC) 11-SLC-16(OPC) | 2.652 44.792 | 2.652 39.85 | SLC-16 replaced gasket, plug, piston, disc, and spring. |
| X-45 Leak Rate Analyzer | C | 16-1-AOV-101A(OPC) 16-1-AOV-101B(OPC) LRA-20(OPC) LRA-21(OPC) | 0.789(AOV-101A) (AOV-101B) 0.1415(LRA-20) (LRA-21) | 0.789(AOV-101A) (AOV-101B) 0.1415(LRA-20) (LRA-21) | |
| X-55B Drywell CAD Inert and Purge | C | 27-SOV-125A(OPC) 27-SOV-125B(OPC) | 0.9625 1.3183 | 0.9625 1.3183 | |
| X-58B CAD System | C | 27-SOV-122F1(OPC) 27-SOV-122F2(OPC) | 4.698 0.1669 | 4.698 0.1669 | SOV-122F1,F2 new installation. |
| X-58C CAD System | C | 27-SOV-120F1(OPC) 27-SOV-120F2(OPC) | 0.3995 0.6542 | 0.3995 0.6542 | SOV-120F1,F2 new installation. |
| X-58D CAD System | C | 27-SOV-123F1(OPC) 27-SOV-123F2(OPC) | 0.4123 0.2647 | 0.4123 0.2647 | SOV-123F1,F2 new installation. |
| X-59 Drywell CAD Inert and Purge | C | 27-SOV-123A(OPC) 27-SOV-123B(OPC) 27-SOV-123E1(OPC) 27-SOV-123E2(OPC) | >1018 >1018 2.6977 <0.102 | 5.6499 <0.102 2.6977 <0.102 | SOV-123A,B cleaned valves, replaced seats, viton discs, springs, piston rings, and O-rings. SOV-123E1,E2 new installation. |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|---|----------------------|--|---|--|--|
| X-61 Breathing Air | C | BAS-5(IPC) BAS-4(OPC) | 413.817 119.615 | 13.743 6.785 | BAS-5 cleaned valve and polished disc. BAS-4 ground disc and seat. |
| X-62 Drywell Cooling Return | C | RBC-26B(OPC) 15-AOV-131B(OPC) | 36.85 13.794 | 36.85 13.794 | AOV-131B new installation. |
| X-63 "B" Recirculation Pump MTR Cooling Supply | C | 15-RBC-21A(OPC) 46-ESW-15B(OPC) 15-AOV-132A(OPC) | <0.102 12.5214 27.995 | <0.102 12.5214 27.995 | AOV-132A new installation. |
| X-64 "A" Recirculation Pump MTR Cooling Return | C | 15-RBC-22A(OPC) 15-AOV-133A(OPC) | 38.84 4.5351 | 38.84 4.5351 | AOV-133A new installation. |
| X-65 Equipment Drain Pump Cooler Return | C | 15-RBC-33(OPC) 15-AOV-134A(OPC) | 2.0156 2.1174 | 2.0156 2.1174 | AOV-134A new installation. |
| X-66 "A" Drywell Cooler Assembly Return | C | 15-RBC-26A(OPC) 15-AOV-131A(OPC) | <0.102 5.446 | <0.102 5.446 | AOV-131A new installation. |
| X-67 "A" Recirculation Pump MTR Cooling Supply | C | 15-RBC-21B(OPC) 46-ESW-15A(OPC) 15-AOV-132B(OPC) | <0.102 <0.102 <0.102 | <0.102 <0.102 <0.102 | AOV-132B new installation. |
| X-68 "B" Recirculation Pump MTR Cooling Return | C | 15-RBC-22B(OPC) 15-AOV-133B(C. ') | 560.41 19.8001 | 34.3575 19.8001 | RBC-22B cleaned valve, lapped disc and seat. AOV-133B new installation. |
| X-100A Elect | B | "O" rings | <0.102 | <0.102 | |
| X-100B Elect | B | "O" rings | <0.102 | <0.102 | |
| X-100C Elect | B | "O" rings | <0.102 | <0.102 | |
| X-100D Elect | B | "O" rings | 0.2769 | 0.2769 | |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|------------------------|----------------------|------------------------------------|---|--|---------------------|
| X-100F Elect | B | "0" rings | 0.1312 | 0.1312 | |
| X-100G Elect | B | "0" rings | <0.102 | <0.102 | |
| X-100K Elect | B | "0" rings | <0.102 | <0.102 | |
| X-101A Elect | B | "0" rings | <0.102 | <0.102 | |
| X-101B Elect | B | "0" rings | <0.102 | <0.102 | |
| X-101C Elect | B | "0" rings | <0.102 | <0.102 | |
| X-101D Elect | B | "0" rings | <0.102 | <0.102 | |
| X-101E Elect | B | "0" rings | <0.102 | <0.102 | |
| X-101F Elect | B | "0" rings | 0.1273 | 0.1273 | |
| X-103A Elect | B | "0" rings | <0.102 | <0.102 | |
| X-103B Elect | B | "0" rings | <0.102 | <0.102 | |
| X-104C Elect | B | "0" rings | <0.102 | <0.102 | |
| X-104D Elect | B | "0" rings | <0.102 | <0.102 | |
| X-104E Elect | B | "0" rings | <0.102 | <0.102 | |
| X-106A Elect | B | "0" rings | 0.5039 | 0.5039 | |
| X-106B Elect | B | "0" rings | <0.102 | <0.102 | |
| X-107 Elect | B | "0" rings | <0.102 | <0.102 | |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|------------------------|------------------|--|--|--|---------------------|
| X-108 Elect | B | "0" rings | <0.102 | <0.102 | |
| X-109 Elect | B | "0" rings | <0.102 | <0.102 | |
| X-110C Elect | B | "0" rings | <0.102 | <0.102 | |
| X-110D Elect | B | "0" rings | <0.102 | <0.102 | |
| X-111B Elect | B | "0" rings | <0.102 | <0.102 | |
| X-200A Torus Access | B | "0" rings | 0.3741 | 0.3741 | |
| X-200B Torus Access | B | "0" rings | 0.5415 | 0.5415 | |
| X-200C Torus Access | B | "0" rings | 0.3837 | 0.3837 | |
| X-202BG Vacuum Breaker | C | 27-AOV-101B(OPC) VB-7(OPC) 27-AOV-101A(OPC) VB-6(OPC) | 1.49(AOV-101B) (VB-7) 2.35(AOV-101A) (VB-6) | 1.49(AOV-101B) (VB-7) 2.35(AOV-101A) (VB-6) | |
| X-202F Vacuum Breaker | B | "0" ring(VB-1) | 0.214 | 0.214 | |
| X-202G Vacuum Breaker | B | "0" ring(VB-2) | 0.214 | 0.214 | |
| X-202H Vacuum Breaker | B | "0" ring(VB-3) | 0.216 | 0.216 | |
| X-202I Vacuum Breaker | B | "0" ring(VB-4) | 2.988 | 2.988 | |
| X-202J Vacuum Breaker | B | "0" ring(VB-5) | 0.247 | 0.247 | |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|---------------------------------------|----------------------|------------------------------------|---|--|--|
| X-203A O ₂ Analyzer Sample | C | 27-SOV-119A(OPC) | 3.242 | 3.242 | SOV-119E1,E2 new installation. |
| | | 27-SOV-119B(OPC) | 3.7528 | 3.7528 | |
| | | 27-SOV-119E1(OPC) | 0.779 | 0.779 | |
| | | 27-SOV-119E2(OPC) | 2.08 | 2.08 | |
| X-203B O ₂ Analyzer Sample | C | 27-SOV-124A(OPC) | 13.28 | 13.28 | SOV-124E1,E2 new installation. |
| | | 27-SOV-124B(OPC) | 0.2214 | 0.2214 | |
| | | 27-SOV-124E1(OPC) | 0.6103 | 0.6103 | |
| | | 27-SOV-124E2(OPC) | 0.2713 | 0.2713 | |
| | | 27-SOV-124F1(OPC) | 0.2779 | 0.2779 | SOV-124F1,F2 new installation. |
| | | 27-SOV-124F2(OPC) | 0.6886 | 0.6886 | |
| X-205 Drywell Inert CAD and Purge | C | 27-AOV-117(OPC) | 330.85(AOV-117) | 52.1725(AOV-117) | AOV-117 replaced T-ring and O-ring. |
| | | 27-AOV-118(OPC) | (AOV-118) | (AOV-118) | |
| | | 27-MOV-117(OPC) | 0.2886(MOV-117) | 0.2886(MOV-117) | |
| | | 27-MOV-123(OPC) | (MOV-123) | (MOV-123) | |
| X-211A Containment Spray | C | 10-MOV-34A(OPC) | 107.399 | 107.399 | |
| | | 10-MOV-38A(OPC) | (Combined) | (Combined) | |
| | | 10-MOV-39A(OPC) | | | |
| X-211B Containment Spray | C | 10-MOV-34B(OPC) | 53.5468 | 53.5468 | |
| | | 10-MOV-38B(OPC) | (Combined) | (Combined) | |
| | | 10-MOV-39B(OPC) | | | |
| X-212 RCIC Turbine Exhaust | C | RCIC-04(OPC) | >1018 | 44.7106 | RCIC-04 machined back seat surface, seat ring, and disc. |
| | | RCIC-05(OPC) | >1018 | 44.1812 | |
| | | 13-MOV-130(OPC) | 6.885 | 6.885 | |
| X-214 HPCI Turbine Exhaust | C | 23-HPI-12(OPC) | >1018 | 101.545 | HPI-65 cleaned valve, machined and ground back seat surface, seat, disc, disc swing arm, and replaced gaskets. HPI-12 cleaned valve, machined disc, ground seat, replaced gasket. |
| | | 23-HPI-65(OPC) | >1018 | 44.842 | |

ATTACHMENT 4B (Cont.)
1983 LOCAL LEAKAGE RATE TEST PENETRATION DATA

| <u>Penetration No.</u> | <u>Type Test</u> | <u>Equipment/Valves Tested</u> | <u>Pre-Repair Leakage (scf/day)</u> | <u>Post-Repair Leakage (scf/day)</u> | <u>Repair/Notes</u> |
|------------------------------------|------------------|--|---|--|--|
| X-217 HPCI Turbine Exhaust Vent | C | 23-MOV-59(OPC) 23-HPI-403(OPC) 23-HPI-402(OPC) | 19.2402 (Combined) | 19.2402 (Combined) | |
| X-218 Leak Rate Analyzer | C | LRA-13(OPC) LRA-14(OPC) AOV-102A(OPC) AOV-102B(OPC) | 0.3277(LRA-13) (LRA-14) 0.3064(AOV-102A) (AOV-102B) | 0.3277(LRA-13) (LRA-14) 0.3064(AOV-102A) (AOV-102B) | |
| X-220 Drywell CAD Inert and Purge | C | 27-AOV-132A(OPC) CV-67(OPC) 27-AOV-132B(OPC) CV-70(OPC) 27-AOV-115(OPC) 27-AOV-116(OPC) | 2.789(AOV-132A) (CV-67) 55.1756(AOV-132B) (CV-70) >1018(AOV-115) (AOV-116) | 2.789(AOV-132A) (CV-67) 55.1756(AOV-132B) (CV-70) 4.0618(AOV-115) (AOV-116) | AOV-115,116 cleaned valves, replaced T-rings and O-rings. |
| X-221 Condensate from RCIC Turbine | C | 13-RCIC-07(OPC) 13-RCIC-08(OPC) | >1018 >1018 | 2.8605 2.7587 | RCIC-07,08 cleaned valves, ground and lapped plugs, seats, pistons, replaced flex gaskets and springs. |
| X-231A Elect | B | "O" rings | 0.3823 | 0.3823 | |

ATTACHMENT 4C

PRIMARY CONTAINMENT BOUNDARY MODIFICATIONS

The following JAFNPP primary containment boundaries were modified during the 1983 and 1985 outages.

1. Penetrations modified to provide taps for the H₂ Monitoring System:

- a. X-26A SOV-120E1, SOV-120E2, SOV-119F1, SOV-119F2, SOV-122E1, and SOV-122E2 were tied in. Manual valves (CAD-204, CAD-205, and CAD-206) are open and associated caps removed.
- b. X-58B SOV-122F1 and SOV-122F2 were tied in. Manual valve (CAD-214) is open and associated cap removed.
- c. X-58C SOV-120F1 and SOV-120F2 were tied in. Manual valve (CAD-215) is open and associated cap removed.
- d. X-58D SOV-123F1 and SOV-123F2 were tied in. Manual valve (CAD-216) is open and associated cap removed.
- e. X-59 SOV-123E1 and SOV-123E2 were tied in. Manual valve (CAD-207) is open and associated cap removed.
- f. X-203A SOV-119E1 and SOV-119E2 were tied in. Manual valve (CAD-201) is open and associated cap removed.
- g. X-203B SOV-124E1, SOV-124E2, SOV-124F1, and SOV-124F2 were tied in. Manual valves (CAD-202 and CAD-203) are open and associated caps removed.

2. Reactor Building Cooling Water containment isolation valves added:

- a. X-23 AOV-130A was added.
- b. X-24 AOV-130B was added.
- c. X-62 AOV-131B was added.
- d. X-63 AOV-132A was added.
- e. X-64 AOV-133A was added.
- f. X-65 AOV-134A was added.
- g. X-66 AOV-131A was added.
- h. X-67 AOV-132B was added.
- j. X-68 AOV-133B was added.

ATTACHMENT 4C (Cont.)

PRIMARY CONTAINMENT BOUNDARY MODIFICATIONS

3. MOV-18 was replaced and relocated on Penetration X-12.
4. Penetration X-36 CRD return line was cut and capped.
5. Penetration X-59 line containing valves SOV-123A,B was cut and capped.