MONTICELLO NUCLEAR GENERATING PLANT
DOCKET NO. 50-263 LICENSE NOS. DPR-22

ASME CODE SECTION XI INSERVICE INSPECTION AND TESTING PROGRAM

AND

INFORMATION REQUIRED FOR NRC REVIEW OF REQUESTS FOR RELIEF FROM ASME CODE SECTION XI REQUIREMENTS

SUBMITTED: March 15, 1978

REVISED: Revision 1

August 28, 1978

Revision 2 January 5, 1979

Revision 3 February 26, 1979

Revision 4 July 27, 1979

Revision 5 March 5, 1980

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This report contains a description of our proposed program of inservice inspection and testing of components of the Monticello Nuclear Generating Plant. This program conforms to the requirements of 10 CFR 50, Section 50.55a(g).

The information presented in this section follows the recommendations contained in a letter dated November 24, 1976 from Mr D L Ziemann, Chief, Operating Reactors Branch #2, Division of Operating Reactors, USNRC, and in a letter dated January 16, 1978 from Mr D K Davis, Acting Chief, Operating Reactors Branch #2. The program is updated as required by changes to Section 50.55a(g) published in the Federal Register on October 7, 1979.

Inservice inspection and testing requirements are updated at 120 month intervals to conform to the latest edition and addenda of Section XI of the ASME Code referenced in paragraph (b) of 10 CFR 50, Section 50.55a. This manual will be updated each time changes are made to the inservice inspection and testing program. Deviations from Code requirements are also documented for NRC Staff review in this manual.

The program description is arranged in the following manner:

Nondestructive Examination

Class 1	-	Section	1.1
Class 2	-	Section	1.2
Class 3	*	Section	1.3
Pressure Testing Program	-	Section	2
Inservice Tests of Pumps and Valves	-	Section	3
Deviations from Section XI Requirements	-	Sect ion	4

Proposed changes to the Technical Specifications which implement this program were submitted to the Commission on August 30, 1977. A summary of these proposed changes is contained in Section 5 of this report.

System drawings showing ASME Code classification boundaries are included in Section 6 of this report. These drawings are used to define pressure test boundaries and identify those Class 3 components subject to visual inspection as part of the nondestructive examination program.

ASME Section XI Nondestructive Examination Program - Class 1

ASME Code Edition and Addenda: 1974 Edition through and including Summer 1975 Addenda

Program Period: February 28, 1978 to June 30, 1981 (Third Inspection Period)

NOTES:

- 1. The following tables identify the specific Class I components and parts to be examined. These tables can be directly correlated with Table IWB-2500 and Table IWB-2600 of Section XI identify the examination method for each listed item. The inspections that were completed during period one and period two are identified in the tables, along with the running percent completed during each of these periods. No effort was made to retrofit items into the first two periods that were not previously required for examination. The tables show the amount of items required to be examined during period three and the corresponding percentage that will have been completed by the end of this period.
- 2. Repairs will be performed in accordance with the applicable requirements of the latest edition and addenda of the ASME Code, Section XI. However, if rules for a particular repair are not specified in Section XI, the original design specification and Construction Code of the component or system, or later editions of the Construction Code or ASME Code Section III, either in their entirety or portions thereof, may be used.

LEGEND

Examination method:

V - visual

U.T. - ultrasonic

R.T. - radiography

S - Serface examination, either liquid penetrant or magnetic particle

Inspection Period

ONE - June 30, 1971 to October 30, 1974

TWO - October 30, 1974 to February 28, 1978

THREE - February 28, 1978 to June 30, 1981

TEN TEAR INTERVAL INSPECTION SUMMARY

TABLE 1,1

PAGE 1 OF 8

MAJOR ITIM: REACTOR VESSEL

SUB	EXAM. CATE- CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF ITEM TO BE EXAMINED	TOTAL NO. PER ITEM	NDE METHOD	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING PERCENT	REMARKS
81.1	в-А	LONGITUDINAL AND CIRCUMFEREN-								RELIEF REQUEST NO. 15
		TIAL WELDS IN CORE REGION LONGITUDINAL WELDS		UT	VLAA-1 VLAA-2	WELDS ARE NOT ACCESSIBLE	× -	SHELL COURSE 1 75° SHELL COURSE 1 255°	-	(WELD LENCTHS = 11 FEET TOP 27" OF WELD SEAMS (SHELL COURSE 1) IN CORE REGION
					VLBA-1 VLBA-2	WELDS ARE NOT ACCESSIBLE		SHELL COURSE 2 450 SHELL COURSE 2 2250		BOTTOM 117" OF WELD SEAMS (SHELL COUPSES 2) IN CORE REGION
-		CIRCUMFERENTIAL WELDS	1	UT	VCBA-2	WELD IS NOT ACCESSIBLE	-	SHELL COURSE 1 TO 2 ELEVATION 19'6"		(WELD LENGTH - 57 FEET)
11.2	B-8	LONGITUDINAL AND CIRCUMFERENTIAL WELDS IN SHELL (OTHER THAN THOSE OF CATEGORY B-A AND B-C) AND MERIDIONAL AND CIRCUMFERENTIAL SEAM WELDS IN BOTTOM HEAD AND CLOSURE HEAD (OTHER THAN THOSE OF CATEGORY B-C)								
		SHELL LONGITUDINAL WELDS	6	UT	VLAA-1 VLAA-2	WELDS ARE NOT ACCESSIBLE	-	SHELL COURSE 1 75° SHELL COURSE 1 255°	-	(WELD LENGTHS = 11 FEE RELIEF REQUEST NO. 15
					VLCB-1 VLCB-2	RELIEF REQ'T NO. 16		SHELL COURSE 3 1050 SHELL COURSE 3 2850	-	RELIEF REQUEST NO. 16
					VLDB-1	(24" EXAMINED) (NONE) 33" 190%	ONE TWO THREE	SHELL COURSE 4 100°	(187)	only 57" (43%) OF EACH WELD SEAM, VLDR-1 AND VLDB-2, ARE EXTERNALLY ACCESSIBLE
					VLb8-2	(NONE) (57" EXAMIRED) NONE	ONE TWO THREE	SHELL COUPSE 4 330°	(0) (43%) 43%	
										RELIEF REQUEST NO. 16
					VLBA-1 VLBA-2	RELIEF REQ'T NO.16 RELIEF REQ'T NO.16		SHELL COURSE 2 45° SHELL COURSE 2 225°	1 2	TOP 15" OF WELD SEAMS NOT IN CORE RECION

NORTHERN STATES POWER CO. MONTICULIO NUCLEAR GENERATING PLANT

THE YEAR INTERVAL INSPECTION SUMMARY

TABLE 1,1

PAGE 2 OF 8

MAJOR ITEM: REACTOR VESSEL

SUB	EXAM. CATE- CORY	AND DESCRIPTION OF LITEM TO BE EXAMINED	NO. PER TEEM	NDE METHODS	TOENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	PERCENT	REMARKS
81.2	B-B	(CONTINUED)								
		CIRCUMPERENTIAL WELDS	3	ur	∀CHB-1	WELD IS NOT ACCESSIBLE		BOTTOM HEAD TO COURSE 1 ELEVATION 8*7"	-	RELIEF REQUEST NO. 15
					VCBB~3	WELD IS NOT ACCESSIBLE	-	SHELL COURSE 2 TO 3 ELEVATION 30'6"	-	RELIEF REQUEST NO. 15
1					vcss-4	RELIEF REQ'T NO. 16	-	SHELL COURSE 3 TO 4 ELEVATION 41'6"	-	RELIEF REQUEST NO. 16
		CLOSURE HEAD								
		MERIDIONAL WELDS	6	vr	HMCB-1 HMCB-2	(1½ FEET EXAMINED) (1½ FEET EXAMINED)	ONE	CLOSURE HEAD 30° CLOSURE HEAD 90°	(7)	(WELD LENGTHS = 7 FEET
					HMCB-1	(7 FEET EXAMINED)	TMO	CLOSURE HEAD 30°	(57)	
	-				HMCB-3 HMCB-5	(7 FEET EXAMINED) (7 FEET EXAMINED)		CLOSURE HEAD 150° CLOSURE HEAD 270°		
					HMCB-4 HMCB-6	7 FEET 100% 7 FEET 100%	THREE	CLOSURE HEAD 210° CLOSURE HEAD 330°	87	
	-	CIRCUMFERENTIAL WELD	1	UT	нссв-2	(NONE) (25 FEET EXAMINED) NONE	ONE TWO THREE	DOLLAR PLATE WELD	(100%) 100	(WELD LENGTH = 25 FEET
	- 1	BOTTOM HEAD			FIGURE 5					
		MERIDIONAL WELDS		UŢ	HMAB-1 HMAB-2 HMAB-3 HMAB-4 HMAB-5 HMAB-6 HMAB-7 HMAB-8	WELDS ARE NOT ACCESSIBLE		BOTTOM HEAD 00 450 900 1350 1800 2250 2700 3150		RELIEF REQUEST NO. 16
-	-	MERICNAL WELDS THROUGH DOLLAR PLATE ASSEMBLY	2	£3.	HMAB-9 HMAB-10	WELDS ARE NOT ACCESSIBLE		воттом неар 12 ⁰ 195 ⁰	-	RELIEF REQUEST NO. 16

8/28/78

NORTHERN STATES POWER CO.

TEN PEAR INTERNAL INSPECTION SUMMAN

TABLE 1.1

MAJOR ITEM: REACTOR VESSTA.

REFERENCE		(WELD LENGTH = 64 FEET)	(WELD LENGTH = 57 FEET)	EXMINATION FROM PLANCE SURFACE.	(SELD LEMCTH = 57 FEET)					RELIEF REQUEST NO. 15				
RUNNING		S2 S2		(337.) (677.) 17067.	(332)	Į.		(33)		ı		(25%) 75% (50%) 100%	(252.) (502.) (752.) 1007.	
LOCATION OR SYSTEM NUMBER		0° TO 18°		STUD HOLE NO. 64 TO 21 STUD HOLE NO. 21 TO 43 STUD HOLE NO. 43 TO 64	STUD HOLE NO. 64 TG 22 STUD HOLE NO. 21 TO 1 AND NO. 36 TO 43			CLOSURE HEAD TDC CLOSURE HEAD 900 CLOSURE HEAD 1800		BOTTOM HEAD 350°		SHELL COURSE 4 72° SHELL COURSE 4 108° SHELL COURSE 4 252° SHELL COURSE 4 288°	SHELL CORRSE 3 45° SHELL CORRSE 3 135° SHELL CORRSE 3 225° SHELL COURSE 3 315°	
INSPEC- TION PERIOD		ORE TWO THREF		CME TWO THREE	TWO	THE CANADA		ONE		1740		ONE THREE TMO THREE	ONE TMO THREE	
EXAMENATION AMOUNT AND EXTENT		(2.2 FT EXAMENED) 2.2 FEET 100%		(19.4 FT EXAMINED) (19.4 FT EXAMINED) 18.8 FEET 1007	FT EXAMI	1000		(CXAMINED) (CXAMINED) 1 WELD 1007		TO THE EXTENT POSSIBLE		(ESAMINED) I WELD 100% (ESAMINED) I WELD 100%	(EMMINED) (EMMINED) (EMMINED) I WELD 1902	
IMPATIFICATION		HCAB-1		VCBC-5	HCCC-1	FIGURE 4		HVAD-1 RBDF-1 HSBD-1		CPAD-1		MSR0-1 MSR0-1 MSR0-1 MSR0-1	FWAD-1 FWED-1 FWCD-1 FWED-1	
NETHORS		E		ģ	B	1		555		Б		E .	E	
NO.PER		-		**	-	29						4	-3	
CAMPONENT OR SYSTEM, AND DESCRIPTION OF LITH TO BE EXAMINED	(CONTINUED)	C COMPERENTIAL WELD (P. LAR PLATE)	VESSEL-TO-FIANCE AND HEAD-TO-FIANCE CIRCUMFERENTIAL WELDS	VESSEL-TO-FLANGE	HEAD-TO-FLANGE	PRIMARY MOZZLE-TO-VESSEL WELDS AND NOZZLE INSIDE RADIUSED SECTION	CLOSURE HEAD	HEAD VENT (N7) HEAD SPEAY (N6A) HEAD SPARE (N6B)	BOTTON BEAD	STANDBY LIQUID CONTROL (NIO)	VESSEL SHELL	MAIN STEAN A (N3A) MAIN STEAN B (N3B) MAIN STEAN C (N3C) NAIN STEAN D (N3C)	FEEDWATER A (NGA) FEEDWATER B (NGB) FEEDWATER C (NGC) FEEDWATER D (NGD)	
EXAM.	_		9 P			8-8								
SUB	81.2		81.3		THE RESIDENCE	81.4		e estan management	-					

NORTHERN STATES POWER CD. MONTICELLO NUCLEAR GENERATING PLANT

TEN TEAR INTERVAL INSPECTION SUMMARS

TABLE 1.1

PAGE 4 OF 8

MAJOR ITEM: REACTOR VESSEL

SUB FTEM	EXAM. CATE- CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF LITM TO BE EXAMINED	TOTAL NO.PER ITEM	NDE METHODS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING PERCENT	REMARKS
81.4	8-0	(CONTINUED)							-	**************************************
		VESSEL SHELL						The state of		
		CORE SPRAY A (NSA) CORE SPRAY B (NSB)	2	Ur.	CSAD-1 CSBD-1	(EXAMINED) (EXAMINED)	THREE TWO	SHELL COURSE 3 90° SHELL COURSE 3 270°	100 (50)	
		CONTROL ROD HYDRAULIC RETURN (N9)	1	UI	CRAD-1	(EXAMINED)	ONEATWO	SHELL COURSE 3 650	(100)	
		RECIRCULATION OUTLET A (NIA)	2	ur	RCAD-1	(EXAMINED)	ONE	SHELL COURSE 1 00	(100)	
		RECIRCULATION OUTLET B (NIB)			RCBD-1	(EXAMINED) 1 WELD 100%	ONE	SHELL COURSE 1 180°	(100) 100	RESCHEDULED FOR EXAMINA- TION
- 1		RECIRCULATION INLET NOZZLES	10	UT						
		INLET A (N2A) INLET D (N2D) INLET J (N2J)			RRAD-1 RRDD-1 RRID-1	(EXAMINED) (EXAMINED) (EXAMINED)	ONE ONE ONE	SHELL COURSE 1 30° SHELL COURSE 1 120° SHELL COURSE 1 300°	(10) (20) (30)	
		INLET C (N2C) INLET E (N2E) INLET G (N2G)			RRCD-1 RRED-1 RRGD-1	(EXAMINED) (EXAMINED) (EXAMINED)	TWO TWO TWO	SHELL COURSE 1 90° SHELL COURSE 1 150° SHELL COURSE 1 240°	(40) (50) (60)	
	And in case of the last of the	INLET B (N2B) INLET F (N2F) INLET H (N2H) INLET K (N2K)			RRBD-1 RRFD-1 RRHD-1 RRKD-1	1 WELD 1007, 1 WELD 1007, 1 WELD 1007, 1 WELD 1007,	THREE THREE THREE THREE	SHELL COURSE 1 60° SHELL COURSE 1 210° SHELL COURSE 1 270° SHELL COURSE 1 330°	70 80 90 100	
-	-	JET PUMP INSTRUMENT NOZZLE	2	UT						
		NOZZLE A (NRA)			JPAD-1	(EXAMINET)	ONE	SHELL COURSE 1 60°	(50)	
		NOZZŁE B (N8B)			JPSb-1	I WELD 100%	THREE	SHELL COURSE 1 240°	100	
81.5	B-E	VESSEL PENETRATIONS, INCLUD- ING OCTROL ROD DRIVE AND INSTRUMENTATION PENETRATIONS								
		CONTROL ROD DRIVE PENETRATIONS	121	V	FIGURE 1	RELIEF REQ'I NO. 17	- 1	UNDER REACTOR VESSEL BOTTOM READ	-	RELIEF REQUEST NO. 17

NORTHERN STATES POWER CO. MONTICELLO MIKLEAR GENERATING PLANT

TEN TEAR INTERVAL INSPECTION SUMMAS.

TABLE 1.1

PAGE 5 OF 8

MAJOR ITEM: REACTOR VESSEL

REACTOR VESSEL CLOSURE HEAD FLANCE LEARAGE SENSORS 2	SUR ETEM	CATE- CORY	AND DESCRIPTION OF LITEM TO BE EXAMINED	TOTAL NO.PER ITEM	NDE METHODS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING PERCENT	RIMARKS
PENETRATIONS NOZZLE NIIA	81.5	B-E	(CONTINUED)								
NOZZIE N12B				4	٧	FIGURE 4	1 WELD 100%	THREE		25	
REACTOR VESSEL CLOSURE HEAD FIANCE LEARAGE SENSORS 2	Male school of the second second second		NOZZLE N11B NOZZLE N12A			VIBE-1 VICE-1			SHELL COURSE 4 220° SHELL COURSE 3 40°		
CLOSURE HEAD FLANGE LEAKAGE SENSORS 2 V NOZZLE N13 NOZZLE N13 NOZZLE N14 NOZZLE N15 NOZZLE-TO-SAFE END WELDS CLOSURE HEAD HEAD SPRAY (BGA) HEAD SPRAY (BGA) HEAD SPRAY (BGA) HEAD SPRAY (BGB) 1 PT-UT				1	٧	HDAE-1	RELIEF REQ'T NO. 17		BOTTOM HEAD		RELIEF REQUEST NO. 17
B1.6 B-F NOZZLE-TO-SAFE END WELDS CLOSURE HEAD CLOSURE HEAD HEAD SPRAY (NoA) HEAD SPRAY (NoA) HEAD SPRAY (NoA) HEAD SPRAY (NoB) HEAD SPRAY (NoB) BOTTOM HEAD STANDBY LIQUID CONTROL (NID) VESSEL SHELL CORE SPRAY A (NSA) CORE SPRAY A (NSA) CORE SPRAY B (NSB) CONTROL ROD HYDRAULIC RETURN (N9) 1 PT-UT CRAF-2 (EXAMINED) ONE CLOSURE HEAD TDC CLOSURE HEAD TDC CLOSURE HEAD 180° (61) CLOSURE HEAD 180° (62) CLOSURE HEAD 180° (63) THREE CLOSURE HEAD 180° (64) CLOSURE HEAD 180° (64) THREE CLOSURE HEAD 180° (65) THREE CLOSURE HEAD 180° (65) THREE CLOSURE HEAD 180° (65) THREE CLOSURE HEAD TDC CLOSURE HEAD 180° (65) THREE CLOSURE HEAD 180° (65) THREE CLOSURE HEAD TDC CLOSURE HEAD 180° (65) THREE CLOSURE HEAD 180° (65) THREE CLOSURE HEAD TDC CLOSURE HEAD 180° (65) THREE CLOSURE HEAD TDC CLOSURE HEAD 180° (65) THREE CLOSURE HEAD 180° (65) THREE CLOSURE HEAD TDC CLOSURE HEAD 180° (65) THREE CLOSURE HEAD 180° (65) THREE CLOSURE HEAD TDC CLOSURE HEAD TDC CLOSURE HEAD 180° (65) THREE CLOSURE HEAD TDC CLOSURE HE			CLOSURE HEAD	2	y						
CLOSURE HEAD HEAD VENT (N7) HEAD SPRAY (N6A) HEAD SPRAY (N6A) BOTTOM HEAD STANDBY LIQUID CONTROL (N10) VESSEL SHELL CORE SPRAY B (N5B) CONTROL ROD HYDRAULIC RETURN (N9) LEVAMOR AND							RELIEF REQ'T NO. 18				RELIEF REQUEST NO. 18
HEAD VENT (N7) HEAD SPRAY (N6A) HEAD SPRAY (N6A) HEAD SPARE (N6B) BOTTOM HEAD STANDBY LIQUID CONTROL (N10) VESSEL SHELL CORE SPRAY A (N5A) CORE SPRAY B (N5B) CONTROL ROD HYDRAULIC RETURN (N9) PT-UT HVAF-2 RHDF-2 REXAMINED REXAMINED REPLACED SITH CAP 1° REXAMINED REPLACED SITH CAP 1°	B1.6	В-Г	NOZZLE-TO-SAFE END WELDS	(19)							
HEAD SPRAY (N6A)		- 1	CLOSURE HEAD								
STANDBY LIQUID 1 PT-UT CPAF-2 PARTIALLY ACCESSIBLE BOTTOM HEAD 350° 100 RELIEF REQUEST NO. IS VESSEL SHELL CORE SPRAY A (NSA) 2 PT-UT CSAF-2 (EXAMINED) TWO SHELL COURSE 3 90° (50) CORE SPRAY B (NSB) 1 PT-UT CRAF-2 (EXAMINED) TWO SHELL COURSE 3 270° (100) CONTROL ROD 1 PT-UT CRAF-2 (EXAMINED) TWO BASELINE (100) REPLACED WITH CAF 1° HYDRAULIC RETURN (N9)			HEAD SPRAY (N6A)	1 1	PT-UT	RHDF-2	(EXAMINED)	CNE	CLOSURE HEAD 900	(67)	
CONTROL (N10) VESSEL SHELL. CORE SPRAY A (N5A) CORE SPRAY B (N5B) CONTROL ROD HYDRAULIC RETURN (N9) ACCESSIBLE LEXAMINED TWO SHELL COURSE 3 90° (50) SHE'LL COURSE 3 270° (100)			BOTTOM HEAD								
CORE SPRAY A (NSA) 2 PT-UI CSAF-2 (EXAMINED) TWO SHELL COURSE 3 90° (50) CORE SPRAY B (NSB) 1 PT-UI CRAF-2 (EXAMINED) TWO SHELL COURSE 3 270° (100) CONTROL ROD 1 PT-UI CRAF-2 (EXAMINED) TWO BASELINE (100) REPLACED WITH CAP 1° (100)				1	PT-UT	CPAF-2	a contract of the contract of	THREE	BOTTOM HEAD 350°	100	RELIEF REQUEST NO. 19
CORE SPRAY B (N5B) CSBF-2 (EXAMINED) TWO SHELL COURSE 3 270° (100) CONTROL ROD HYDRAULIC RETURN (N9) CSBF-2 (EXAMINED) TWO BASELINE (100) REPLACED WITH CAP 1°	- 1		VESSEL SHELL								
HYDRAULIC RETURN (N9)				2	PT-UT	The state of the s		501.0			
1 MELD 1001 THREE SHELL COURSE 3 65° 1001				-1	PT-UT	CRAF-2	(EXAMINED)	TWO	BASELINE	(100)	REPLACED WITH CAP 1077
							1 WELD 1001	THREE	SHELL COURSE 3 65°	100%	

NORTHERN STATES POWER CO. MONTICELLO NUCLEAR GENERATING PLANT

TEN TEAR INTERVAL INSPECTION SUMMARY

TABLE 1.1

PAGE 6 OF 8

MAJOR ITEM: REACTOR VESSEL

SUR ITEM	EXAM. CATE- CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF LITEM TO BE EXAMINED	TOTAL NO. PER LITEM	NDE METHODS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING PERCENT	REMARKS
81.6	B-F	(CONTINUED)								
		VESSEL SHELL			1.					
		RECTROULATION	2	PT-UT	RCAF-2	(EXAMINED)	ONE	SHELL COURSE 1 60	(50)	BOTH SAFE END WELDS (A6B) WERE EXAMENED
		OUTLET A (NIA) RECIRCULATION			RCBF-2	(EXAMINED) I WELD 100%	ONE	SHELL COURSE 1. 180°	(100) 100	DURING PERIOD ONE PER PLANT TECH, SPEC,
		OUTLET 8 (N1B)				1 WELD 400%	THEFE		100	FUNIT TERM, STACE
		RECIRCULATION INLET	(10)	FT-UI						
		ENLET A (N2A)			RRAF-2	(EXAMINED)	ONE	SHELL COURSE 1 30°	(10)	
		INLET D (N2D)			RRDF-2	(EXAMENED)	ONE	SHELL COURSE I 1200	(20)	
		INLET J (N2J)			RRJF-2	(EXAMINED)	ONE	SHELL COURSE 1 300°	(30)	
		INLET C (N2C)			RRCF-2	(EXAMINED)	TWO	SRELL COURSE 1 90°	(40)	
		INLET E (N2E)			RREF-2	(EXAMINED)	TWO	SHELL COURSE I 150°	(50)	
		INLET G (N2G)	1 1		RRGF-2	(EXAMINED)	TWO	SHELL COURSE 1 240°	(60)	
		INLET B (NZB)			RRBF-2	1 WELD 100%	THREE	SHELL COURSE 1 60°	70	
	1	INLET F (N2F)			RRFT-Z	1 WELD 100%	THREE	SHELL COURSE 1 2100	80	
	- 1	INLET H (N2H)			RRHF-2	1 WELD 100%	THREE	SHELL COURSE 1 2700	90	
		INLET K (NZK)			RRKF-2	1 WELD 100%	THREE	SHELL COURSE 1 330°	100	
		JET PUMP INSTRUMENTATION	2	PT-UT						
		NOZZLE A (NBA)			JPAF-2	(EXAMINED)	ONE	SHELL COURSE 1 60°	(50)	
		NOZZLE B (N8B)	1 1		JPBF-2	1 WELD 100%	THREE	SHELL COURSE 1 2400	100	
		INSTRUMENTATION LINES	4	PT-UT						
					VIAF-2	1 WELD 100%	THERES	SHELL COURSE 4 400	25	
		NOZZLE A (N11A) NOZZLE B (N11B)			VIRF-2	1 WELD 100%	THREE	SHELL COURSE 4 220°	50	
		NOZZLE C (NIZA)			VICE-2	1 WELD 100%	THREE	SHELL COURSE 3 40°	75	
		NOZZŁE D (N128)			VIDF-2	1 WELD 100%	THREE	SHELL COURSE 3 2200	100	
B1.7		CLOSURE STUDS AND NUTS	64		FIGURE 3					
6 BL.8 B	F-1	INPLACE		UT		(23 EXAMINED)	OME		(36)	
		or				(23 EXAMINED)	TMO		(72)	
8-	-G-2	WHEN REMOVED		SURFACE 6 UT		23 STUDS 1007.	THREE		100	
	1									

2 25

2 26/79

NORTHERN STATES POWER (D).
NORTHGELLO NIKLEAR GENERATING PLANT

THE PERMENT PROPERTY IN SUMMAY

TABLE 1.1 PAGE 7 OF 8

NAJOR ITIM: PLACTOR VESSEL

-		-	and severate sea	Orașie official and an orași		Contractor de servi	. etc. d. and constitution	erri menggan	STATEMENT OF S	Comments of the second section of the second
RIMMIKS		BUSHINGS COINCIDENT WITH STUD REMOVAL AND LIGARINT EXAM				OMIN TWO AREAS OF THE WELD ARE ACCESSIBLE	RELIEF REQUEST NO. 15	RELIEF FEQUEST NO. 20		THOM WITH BL.16
RUNNUNG	(37)	C100 C100 100 100 100		861		88			1	8
LOCATION OR SYSTEM NEMBER	STUD HOLE 1 THRU 22 STUD HOLE 21 THRU 43 STUD HOLE 43 THRU 64	REMOVED FROM VESSEL.		CLOSURE HEAD TDC CLOSURE HEAD 90° CLOSURE HEAD 180°		BOTTON HEAD-OPENINGS 1207 THRU BIOLOGICAL SHLD 3007	SHELL COURSE 4 AT 00, 900, 1800, AND 2700			
THON PERIOD	OME TWO THREE	OME TAYO THREE		THREE THREE THREE		THREE	THREE	THREE	THREE	THREE
EXAMENATION AMENAT AND EXTENT	(24 EXAMINED) (23 EXAMINE) 21 EXAMINE	(64 EXAMINED) (64 EXAMINED) 64 PAIRS 100%		8 BOLTS 1007, 8 BOLTS 1007, 8 BOLTS 1007,		(5'8" EXAMINED) ≈ 5' 100%	ACCESSIBLE AREAS	2-36 IN ² PATCHES	2-36 IN ² PATCHES	SPACE ABOVE AND VISUALLY ACCESSI- BELOW THE BEAC- IS CORE THAT IS NADE ACCESS- INLE FOR EXAM- INATION BY THE REAVAL OF COM- OMERAL REFUEL- INC OUTAGE.
IDENTIFICATION	FIGHE 3	MASHER PAIRS BUSHINGS (REMARKS)				HCAH-2	RPV LUCS	RELIEF REQUEST NO. 20		SPACE ABOVE AND VISUALLY ACCESS TOR CORE THAT IS NADE ACCESS- INLE FOR EXAM- INATION BY THE PROPREYED OF COM- PONEWES DURING THE OUTAGE.
NOE	111	> >	>			In	6/3	14-7	>	>-
NO. PER TITEM	299	7 9 9		00.00.00		e-i	4	6 PATCHES	6 PATCHES	1
COMPONENT OR SYSTEM, AND DESCRIPTION OF LITEM TO BE EXMINED	SITO HOLES	CLOSURE WASHERS AND BUSHINGS	PRESSURE RETAINING BOLLING	HEAD VENT (N7) HEAD SPRAY (N6A) HEAD SPARE (N6B)	INTEGRALLY WELDED VESSEL SUPPORTS	SUPPORT SKIRT	VESSEL STABILIZER LUCS	CLOSURE HEAD CLADDING	VESSEL CLADDING	VESSEL INTERIOR
CATE.	DOWN TOTAL PROPERTY.	B1.10 B-C-1	B1.11 B-C-2		B-48			81.12 8-1-1	8-1-1	
SUR METT	81.9	81.10	81.11		HE. L			81.13	81.14	or and a second

NORTHERN STATES POWER CO. MUNITICELLO MUNICAR GENERATING PLANT

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE 1.1

PAGE 8 OF 8

MAJOR ITEM: REACTOR VESSEL

SUB EXAM. CATE. GARY	COMPONENT OR SYSTEM, AND DESCRIPTION OF TIEM TO BE EXAMENED	TOTAL NO. PER LTEM	NDE METHORS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING	
B1,16,8-N-2	INTERIOR ATTACHMENTS AND CORE SUPPORT STRUCTURES		V	ATTACHMENTS AND CORE SUPPORT STRUCTURES	VISUALLY ACCESSI- BLE ATTACHMENTS AND SUPPORTS	THREE		100	PERFORMED IN CONJUNC- TION WITH B1,15
81.17 8-N-3	CORE SUPPORT STRUCTURES	-	-					-	NOT APPLICABLE TO BOILING WATER REACTORS
81.18 8-0	CONTROL ROD DRIVE HOUSING	121	UT	HOUSING WELDS FICURE 1	3 WELDS 100%	THREE	UNDER VESSEL	10	24 PERIPHERAL HOUSINGS
81.19 8-P	EXEMPTED COMPONENTS								
	CLOSURE MEAD FLANGE SENSORS		V	VFAE-1 VFBE-1	REMARKS REMARKS	THREE	VESSEL FLANCE 0° VESSEL FLANCE 6°		HYDROSTATICALLY PRESSURE TESTED TO INA-5000 AND INB-5000 AT END OF TEN YEAR PERIOD PLUS SYSTEM LEAKAGE EXAM EACH SCHED- ULED REFUELING OUTAGE. NOTE 81.5

WARTICELLO MALEAR GENERATIVE PLANT

"EN EAST THTERNAL INSPECTION SUMMAN

TABLE 1.2 PAGE 1 OF 1

PRESSURIZER

MAJOR ITEM:

. 1	-	
and the second s	REMARKS	NOT APPLICABLE DUE TO THE DESIGN OF THIS PLANT.
	REMINIM	
	EDCATTON OR SYSTEM NUMBER	
-	ENSPBC TTON PERIOD	ì .
	EXAMENATION AMXINT AND EXTENT	
Section Commercial and Assessment Commercial Sections (Commercial Commercial	METHOD INSTITUTION	SS
-	NO.PER TIEM	
And the second s	COMPONENT OR SYSTEM, AND DESCRIPTION OF THEM TO BE, EXAMINED	FR ESS 520 R ESS
-	COTTE COM	
1	BE.	C
	SUB NOTES	

MANTIGELLO MINIEAR GENERATING PLANT

MENTICALLO METLAR GRABATINE PLANT
"EN FRAG LUTERVAL INSPECTION SUMMARY

MAJOR ITEM: HEAT EXCHANGERS AND STEAM

TARLE 1.3

	DESCRIPTION OF STREET	
CENERA TORS	REMARKS	NOT APPLICABLE DUE TO UNE DESIGN OF THIS PLANT.
0	RUNNING	
the second name and other desired to the second	LIXATION OR SYSTEM MIMBUR	
-	INSPEC- TION PURIOD	
Street, or other Designation of the last o	EXAMENATION AMOUNT AND EXTENT	
-	NETHORS IDENTIFICATION	PENARKS
-	METHORS	
The same of the same of	NO. PER TITIN	
The second secon	COMPONENT OR SYSTEM, AND DESCRIPTION OF LITHE TO BE EXMINED.	GENERA IORS GENERA IORS
-	EXAM. CATE.	
-	SUB MITH	

NORTHERN STATES POWER CO. MONTICELLO NUCLEAR GENERATING PLANT

TEN FEAR INTERPAL INSPECTION SUMMARY

TABLE 1,4

PAGE 1 OF 17

MAJOR ITEM: PIPING PRESSURE BOUNDARY

SUB TTEM	EXAM. CATE- CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF ITEM TO BE EXAMINED	TOTAL NO. PER TITM	NDE METHODS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING PERCENT	REMARKS
14.1	B-F	SAFE-END TO PIPING AND SAFE- END IN BRANCH PIPING WELDS								RELIEF REQUEST NO. 21
-		CORE SPRAY A	3	PT-UT	BUTTWELDS 8" ISI-6A	(1 WELF EXAMINED) (2 WELF:S EXAMINED) NONE.	ONE TWO THREE	DRYWELL IW7-8"EF	(33) (100) 100	AS THE RESULT OF AUG- MENTED INSPECTIONS, THESE 3 WELDS WERE EXAMINED THREE TIMES DURING PERIOD TWO.
		CORE SPRAY B	3	PT-UT	BUTIWELDS 8" ISI-6B	(NONE) (3 WELDS EXAMINED) NONE	ONE TWO THREE	DRYWELL TWII-8"EF	(100) 100	AS THE RESULT OF AUG- MENTED INSPECTIONS, THESE 3 WELDS WERE EXAMINED THREE TIMES DURING PERIOD TWO.
		HIGH PRESSURE COOLANT INJECTION - STEAM	2	PT-UT	BUTTWELDS 8" ISI-7	(NONE) (NONE) 2 WELDS 100%	ONE TWO THREE	DRYWELL PS18-8"ED	100	
		REACTOR WATER CLEANUP	1	PT-UT	BUTTWELD 4" ISL-9	(NONE) (1 WELD EXAMINED) NONE	ONE TWO THREE	DRYWELL REW3-4"EF	(100) 100	AS THE RESUL: OF AUG- MENTED INSPECTIONS, TO WELD WAS EXAMINED TWIC DURING PERIOD TWO.
		RZSIDUA'. HEAT REMOVAL REW-10	1	PT-UT	BUTTWELD 18" ISI-IIA	(1 WELD EXAMINED) (REMARKS) NONE	ONE TWO THREE	DRYWELL REWIO-18"ED	(100) (100) 100	AS THE RESULT OF AUG- MENTED INSPECTIONS, TO WELD WAS EXAMINED AGAI IN PERIOD TWO.
		RESIDUAL HEAT REMOVAL TW20	3	PT-UT	BUTTWELDS 16" 1SI-11B	(NONE) (1 WELD EXAMENED) 2 WELD 1007	ONE TWO THREE	TW20-16"DB	(33) 100	
	-	RESIDUAL HEAT REMOVAL TW30	3	PT-UT	BUTTWELDS 16" ISI-11C	(2 WELDS EXAMINED) (1 WELD EXAMINED) 1 WELD 100%	ONE TWO THINKE	TW30-16"DB	(67) (100) 100	(All and a second secon
4.2	B-G-1	PRESSURE-RETAINING BOLTS AND STUDS	NONE							NO ITEMS TO B-G-1
-		(2 INCH AND LARGER/DIA.)								

24.44

8/28/78

MONTHERN STATES POMER CO.
MONTHERLIA MATERIA GENERATING PLANT

TEN FEAR INTERVAL INSPECTION SLAMASY

FABI: 1.4

MAJOR ITEM: PIPING PRESSURE ROBINDARY

REMRES	RELIEF REQUEST NO. 21	MINISHER OF ONE FOOT OF LONGITUDINAL WELD EACH DIRECTION IN CONJUNC- TION WITH CIRCUMPEREN, TIAL WELD SCHEDULED, MIEN AFFLICABLE								
RUNNING	REL	MINES LONGI DIREC TION TIAL WHEN	(29)	(50)	(23)	(67.) (67.) 67.	(37)	(67)	(21.) (29.) 38	
LOCATION OR BYSTEM NIMBER			DEVWELL PSI-18"ED	DRYWELL PSI-6"ED	DRYMELL PS2-L8"ED	DRYMELE PSZ-6"ED	03.81-18d TTBMEBO	DRYINGLA. PS3-6"ED	DRYMELL PS4-18"ED	
INSPEC- TION PIRIOD			ONE TWO THREE	OME TWO THINKE	ONE	ONE TWO THREE	THREE THREE	CRRE TAUD THITTEE	ONE TWO THREE	
EXAMENATION AMOUNT AND EXTENT		AS REQUIRED	4 WELDS EXAMINED) 2 VELDS EVANINED)	(3 WELD: EXAMINED) (No.T.) 1 WELD 1: VZ	(5 WELDS EXAMLYED) (2 WELDS EXAMEND) 3 WELDS 100%	(2 WELDS EXAMINED) (NOWE) (NOWE)	(8 MELDS EXAMINED) (2 WELDS EXAMINED) 3 WELDS 100%	(2 WELDS EXAMINED) (NONE) NONE	(5 WELDS EXAMINED) (2 WELDS EXAMINED) 2 WELDS 100%	
NETROIS IDENTIFICATION		REMARKS	BUTTVELDS 18" LSI-1	8UTTWELDS 6" ? <t-1< td=""><td>BUTTWELDS 18" ISI-2</td><td>8UTTWEEDS 6" 1S1-2</td><td>BUTTWELDS 18" IS1-3</td><td>80111VEL08 6" 151-3</td><td>BUTTMELISS 18" ISL-4</td><td></td></t-1<>	BUTTWELDS 18" ISI-2	8UTTWEEDS 6" 1S1-2	BUTTWELDS 18" IS1-3	80111VEL08 6" 151-3	BUTTMELISS 18" ISL-4	
NDE M.THOLES		t	Ė	Б	5	Б	5	5	Mr.	
NO. PGR ITEM		KENARKS	52	9	56	m	23	m	572	
COMPONENT OR SYSTEM, AND DESCRIPTION OF LITER TO BE EXMINED	CIRCUMERENTIAL AND LONGITUDE-	LONGITUDINAL WELDS	CIRCUMPERENTIAL WELDS MAIN STEAM A		MAIN STEAM B		MAIN STEAM C		MATS STEAM D	
EXAM. CATE- GOIN	7									
ES MALE	84.5					Principal State of the State of				

MEDITER STATES POWER (D), MENTICELLO MICLEAR GENERATINE PLANT

"I'N SAR INTERNAL PROPERTY NA SUMMAN

TABLE 1.4

ARR 1754 PIPTER PROCESSES SCHOOL

REMARKS									AS THE RESULT OF AUG- MENTED DISPECTIONS, 2 OF THE 5 VELOS EXAMINED IN PERIOD ONE NERE RE- EXAMINED THOE ITYES IN FERIOR TAO, IN ADDI- ILON, 5 OF THE NELDS EXAMINED IN PERIOS NERE FACH EXAMINED DIRECTIONS, OFFICE THAT
RUNNING		89 8	€ <u>6</u> 8	(30)	(3.6) ×	(33)	€£8	() () ×	(51)
LOCATION OR SYSTEM MINGER		Ja.,9-554 Tianasi	DRINGEL FWZB-10"EB	DRYWELL FW28-10"ED	BRYAIGL, FAZ8-14"ED	DESCRIPE EWZA-10"ED	DEWELL FWZA-10"ED	DREWELL PAZA-14"ED	Derwell, tw7-6"EF
INSPEC- TION PURIOR		ONE THESE	ONE THE	ONE TMACK	TWO TWEE	ONE TWO THOREE	COUT. TAYO THREE	COLUMN TANO	Char Tances Tances
EXAMINATION AMENING AND EXTENT		(3 WELDS EXAMINED) (3 WELD EXAMINED) 1 WELD 1007,	(1 WELD EXAMEND) (1 WELD EXAMEND) I WELD 1007,	(3 WKLDS EXAMINED) 1 WKLD 100%	(5 WELDS EXAMINED) (1 WELDS EXAMINED) 1 WELD 100%	(2 WELDS EXAMINED) I WELD 1007,	(1 WELD EXAMINED) (1 WELD EXAMINED) 1 WELD 100%	(5 MELDS EXAMPRED) (1 MELD EXAMPRED) 1 MELD 1003.	(5 WELDS EVANINED) 1 WELD 1907,
NIE DENTIFICATION		SHITWELDS 6" 1SI-4	8077WELDS 10" 151-5A	HUTTAREDS 10" 151-5A	BUTTWELDS 14" 151-5A	BUTTMELDS 10" 151-58	PUTTNETERS 10" 151-58	84, TTMELDS 14" 151-58	BUTTARIOS 8" ISI-6A
NETHOPS		12	E	É	5	5	Б	E	5
ND. PER		4	12	01	12	01	22	22	42
COMPONENT OR SYSTEM, AND DESCRIPTION OF LITH TO BE EXMINED	(CONTINUED)	MAIN STEAM D	PEEDWATER A	FIEDWATER 8	PEEDMATER A	PEERWATER C	FEEDWATER 0	FEEDWATER D	CORE SPRAY A
CATT- CATT-	8-3					*****************			
RE MET	84.5		-						

NORTHERN STATES POWER CO.

THE EAST THICKNEY THEFFETT IN SUMMERS

TAME 4 OF 17

MAKUR LIEST: PIEING PRESSTRE SCHEDARY

REMARKS	AS THE RESULT OF AGG- NENTED INSPECTION, 2 OF THE 4 WELLS EXAMINED IN PERIOD ONE MEDE RE- EXAMINED THREE INNES IN PERIOD TWO. IT ADDI- TION, 5 OF THE WELLDS EXAMINED IN PERIOD TWO WERE EACH EXAMINED THREE INNES DURING THAT		AS THE RESULT OF AUG- MENTED INSPECTIONS, 2 VELUS WENT EXMINED TATES IN PERIOD TWO.					
RUNNUNG	888	868 868	- 69	888	888	(190)	(%) (%)	
EDCATION OR SYS' A NAMER	WAULT TRIE-8"EF	STEAM CHASE PSIS-8"ED	Devisell, REK3-4"EF	di,81-01628 TIMOS	DEVELL TAZO-16"06	DEVMELL TAZO-16"UR	0875ELL 2830-16"78	
TYSPEC. TYON PURIOD	CONE TRAD THINEE	7500 7500 7405	DMC THREE,	ONE TWO THREE	ONE THO THUSE	ONE THREE	00E 770 700	
EXMENSITION AMOUNT AND EXTENT	(4 WELDS EXAMINED) (5 WELD (005)	(4 WELDS EXACTORED) (1 WELD EXAMINED) I WELD 100%	(5 VELOS EXAMDES) 2 VELOS EXAMDES)	(I WELD EXAMINED) (7 WELDS EXAMINED) 2 WELDS EVANIMED)	(3 WELD EXAMINED) 2 WELDS 190%	(2 WELLOS EXAMINED) NOME	(8 VELDS EXAMINED) (NONE) 2 VELDS 1000,	
MUE IDENTIFICATION	887774EE,05 8** 151-6A	BUTTMELDS 8" IS1-7	80 TWELDS 8" 151-9	SUTTWELDS 18" 1ST-11A	BUTTWELDS 16" 1ST-118	BILTMELIS 18" 151-119	SUTTNELDS 16" 151-11C	
MEMORE	t	E	14	E	5	b	B	
NO. PER ITEM	ź	16	14	20	61	41	50	
COMPONENT OR SYSTEM, AND DESCRIPTION OF LITEM TO BE EXMINED	(CORT INDED)	HICH PRESSURE COULANT INJECTION - STEAM	REACTOR MATER CLEANUR	RESIDIAL HEAT REMOVAL RESIDIA	RESIDUAL REAT REMOVAL TW20		RESIDUAL BEAT RESONAL 1830	
CATE-	7							
SUB	5			7.5				

MONTHERN STATES FOWER (D).
MONTHCELLO MINIERE GANEMATINE, PLANT

The read full Boat Inspection Science.

TABLE 1.A

NAJOR 112M: PIPUM PRESSURE BOUNDARY

REMARKS	Act to consistence or cold-	AS A RESULT OF AUG- MENTED INSPECTIONS, TREES IND VELDS MENE EXAMINED INICE IT PER- 150 INO.						PERCENTAGE OWERED BY RECIRC, A (REWZ8-4)	LIDES REPSACED IN PER- IOD TWO AND A COMPLETE BASELINE WAS PURPOUSED, AFTER TWO VEARS SERVICE 100°C, (19 NELDS) WAS EXAMINED.	
FEBRUSE		(100)	884	(113)	8. 13. 13.	100	68a	111	(100)	\$.En
LOCATION OR SYSTEM NUMBER		DRYWELL TH30-16"98	SEPARIA DES6-4"ED	43.15-1.154 TIMAN	DRYMELL REWLIN-28"	SRYKELL REMZ6-4"	287WELL REWLIS-28"	DRYMEEL RENZZ-4"	DRYATEL REAZE-4"	NEYMELL RESSE-22"
INSPEC- TION PERIOD	-2000	THO	ONE TAO THREE	COUE TAND THINKEE	CME TAO THREE	CNUE	ONE TAO TURKE	CME. ZMO. THREE	ONE TWO THREE	ONE TWO THERE
EXMENATION AMOUNT AND EXTENT	-	(2 MELLOS ENAMINED) MONEE	(4 vel.bs examines) 2 vel.bs examines)	(2 WELDS EXAMINYD) Z WELDS 100%	(1 VELD EXAMINED) 2 VELDS EXAMINED) 2 VELDS 1997,	(NONE) (NONE) 1 WELD 1007	(1 WELD EXAMINED) 2 WELD EXAMINED) 2 WELDS 1007,	(NONE.) (NONE.)	(1007, EAMINED) 4 WELDS (1007)	(1 WILD EXMINED) (1 WELD EXMINED) 3 WELRS 1003,
NURE URENTIFICATION	DELECTION NO.	181 - 11C	SUTDELIS 4° 1SI-110	BUTTSELIS 3* ISI-12	80TGWELDS 28" 151-13A	BUTTMELD 4" ISI-13A	8UTTMELDS 28" 1ST-138	8017MELD 4" 1S1-138	98T7MELDS q= 181-1348 & 181-1388	SECTIVIZES 22" 154-130 & 151-130
METHODS	ı		ŧ.	Ė	5	E	Б	li .	5	Banda
NO. PER TITM		4	5	100 200	£		2	-	50	1
CONFORMENT OR SYSTEM, AND DESCRIPTION OF LIEM TO BE, EXAMINED	(CONCENERS)	TUBO PENUL PENUL PENUNAL	RESIDUAL HEAT REMOVAL TW36	REACTOR OBEE INJECTION . COMMANT - STEAM	RECIRCULATION A		RECIRCILATION 9		RECIRCHATION BY-PASS	RECIRCULATION MANIFOLD (AGE)
SUB EXAM.	PARTICULAR DE LA CONTRACTION D									

WARTHERN STATES POMER OD.

TO THE THIEBRAL INSPERSION SUBBANA

TABLE 1,4

MALOR IIIM: PIPING PRESSURE SOUNDARY

	T		montes / Designa	-	-	-	-	-			
REMARKS											
RUNNING		x + 10	(100)	- (2)	(23) (100) 190	<u> </u>	(100)	12	(100)	(25)	. 68
LOCATION OR SYSTEM NUMBER		DRYMELL REMISSIF	BETWELL REWIS-12"	DRYWELL REWIS-12"	BENEFIT REALT-IZE	DETWELL REWIS-12"	DRYWELL REW23-12**	DRYMETA, USN22-12**	DRYMELL REWZ1-12**	SENTERS REMZO-124	DRYNELL REWIS-12"
INSTEC- TION PERIOD		CNE No Dece	ONE TWO JHKEE	UNE TANS THREE	ONE TAU	ONE TWO THREE	TAO TAO DIRECT	ONE TAO TUBEE	ONE TWO TSPEE	ONE TWO TRACE	ONE. TWO THREE
EXMENATION AMENAT AND EXTENT		(SECHE) (SECHE) 1 MELD 100%	(4 SELDS (30M(PED))	(NONE) (NONE) 1 WELD 1002	(1 WELD EXAMINED) (3 WELDS EXAMINED) NOME	(1 WELD EGAMENED) (2009E.) 1 WELD 1003	(1 VELLS EXAMINED) (3 VELLS EXAMINED) NOWE	(NONE) (NENE) 1 WELD 1007,	(4 WPLDS EXAMINED)	(1 WELD EXAMINED) (3 WELL EXAMINED) NAME	(4 WELDS EXAMENSED)
DENTIFICATION		SUTTWELDS 12" 151-13c	80TFWELDS 12" 15T-13C	BUTTAELIS 12" EST-13C	RETURNEDO: 12" IST-13C	NUTTACLOS 12" 151-13C	BUTTWELDS 12" 1ST-130	FUTTMELDS 127" EST-130	BUTTAELDS 12" 151-130	8077WG.96 12" 151-130	8077WELOS 12" 18F-130
METHON SE		5	E	Ė	ž.	þ	Ė	Ē.	Se Se	Ė	1
WO. PER		3		-3	<	d	3	2	-2	4	4
ONGWARN OR SYSTEM, AND RESCRIPTION OF LIBH TO BE EXMINED.	(CONTINUED)	RISER F	ALISON G	R1558 10	75 864864	PETSUS R.	RISER A	RISER B	0 88 88 88	RISSE D	66 64 65 75
CATE:	500 1 000		-						-		
SUB	5.4	161.1		-		************					

NORTHERN STATES POMEN (D). MC.TTGELLD MAZLEAR GENERATING PLANT "EN HEAR INTERNAL INSPECTION SUBMARK

PAGE 7 OF 17

MAJOR ITEM: PIPING PRESSURE BOUNDARY

	-	VALUE DOLLERS				et, manufacture ma		******		-
REMUSICS						PORTION OF SYSTEM IS INACCESSIBLE				
RUNNTING	,	100	190	(100)		1 (**	2		8	5
SYSTEM NUMBER		CLOSURE NEAD	CLOSURE HEAD	COURSE 1 60° & 240°		BOTTON HEAD	STEAM CHASE PSIS-3"ED		AUX, BLDC.	
TION	ONE	TWO	ONE TWO THREE	ONE: TWO THREE		ONE. TMO THREE	OME TWO THREE		ONE TMO THREE	ONE
EXAMENATION ANYMIT AND EXTENT		(NOSE) 1 WELD 1993.	(NONE) (NONE) 1 MELR 1001	(2 NELDS EXAMINED) (NOTS) (NOTE)		(NONE) (NONE) 3 WELDS 100%	(NONE) (NONE) I WELD 1007.		(1000E) (1000E) (100E)	(NONE) (NONE)
NE DAIN IDENTIFICATION	BUTTWELD		61-151 4" 151-15	81171451.b 4" 151-16		BUTTWELD 2" ISI-21	BUTTMELINS 3" ISI-23	-	BUTTWELDS 8" 1SI-24A	BHITTMELDS 8" 151.72"
NET TROTE	E		5	E		E	110		E	E C
NO.PER.			ed .	N		31	9		m	(6)
O'MENT OR SYSTEM, AND DESCRIPTION OF THM TO BE EXAMINED	(CONTINUED) HEAD SPARE		HEAD VENT	JET PUMP (NSA) INSTRIBERTATION (NSE)		REACTOR VESSEL BOTTOM HEAD DRAIN	MAIN STEAM CONDENSATE LEAK OFF	CRD SCRAM HEADER	CR026A-8"08 A 9"	# 80 EX
CATE- CATE-	-					**********				
SUB	84.5									

WINCHERN STATES POMER CO.
WINTIGELLO MINIEAR CENERATINE PLANT

PRESENTE NOTE THAT THE PROPERTY OF STREET

TABLE 1.4 PAGE 8 OF 17 MAJOR ITEM: PIPING PRESSURE BOHNDARY

pronuncia	-	nerodenius:	ADVINIT MANUFACTURE	Market was to be a second				-		-	. Named Production Colored	-
REMARKS									RELIEF RECORST NO. 21 LONGITUDINAL WELDS AS 84.5 COVERACE REQUIRE- MENTS	TO - 8" SPCI ISL-7	TO - 18" NER NEW 10 151-11A	
REMETRE		2	, , 2		1 . 12	1	=	2 8		(20)	Cto	
LUCATTON OR SYSTEM MINBER		AUX, BLIKG,	AUX. SUNC	AUX, SLOG.	AUX, BLMG,	AUX, BLDG.	AUX, BEDG.	AUX, SEDE, CRDI8-12"DE		DRYMELL PS2-18"ED	DIPSELL REGIM-ZH**	
INSPEC- THON PERIOD		THREE	ONE	OME TARKE	CNE TMO THREE	ONE TMO THREE	ONE TWO THREE	ONE TWO THREE		OF.	ii.	
EXMENATION ANOINT AND EXTENT		(SONE) 1 WELD 1007,	(300K) (300K) 1 MEN 1007	(NONE) (NONE) 1 WELD 1902	(NONE) (NONE) I VELD 1002	(PONE) (PONE) 1 WELD 19	(NONE) (NONE) 1 WELD 1007	(NORE) (NEED 100E)	"PUNNEDG PERCENT" ODVEPS ALL BRANCE CORNECTIONS	(I WELD EXAMINED)	(1 WEDD ENAMERED)	
IDENTIFICATION		4" 151-24A	BHTTWELDS 4" ISI-248	BUITMELDS 4" ISL-24A	80177451.05 4" 151-248	BUTTNELS 6" IST-26A	Surrharios 6" IST-248	RUTTMELDS 12" 151-24c	ACC AT THE PARTY OF THE PARTY O	WELD-MSB 3-22 (88* (51-2	MELD-RCAJ-7 (18" 151-138	
MITTER			E .	5	ii.	5	5	E		į.		
NO. PER ITEM	9		101	4	-2	6	2	24				
	7		ig .	1,	5	i _p	5	-	121	-		
or overseen the	(2011)		45	CPBI5A~4"08 3		CRD14A-6"795 A		SCRAM DISCHARGE VOLUME TANK	BRANCH PIPE CONNECTION WEIDS EXCESSING SIX INCH DIAMETER	MAIN STEAM B	RECTROTEATION A	
P CATE	THE REAL PROPERTY.								1 m			
SUS MELLI	84.5					15-5			9.4			

WINDLESS STATES POWER CO. MINITEDLE MINITED PLANT

TEN TEAR INTERNAL INSPECTION SUMMAGE

TABLE 1.4 PAGE 9 OF 17 NAJOR IIIM: PIPING PRESSURE SCHNEARY

- AMERICAN IN COLUMN	Ţ			-	-	-		-		COLUMN A PROPERTY	-	-
REMARKS REMARKS	FROM - 88R 1420 -		20						(00)		(40)	
SYSTEM MINBER	RENE 38-28"		DRYKELL RE432-22**	REW32-22**	RFM32-22**	REM 32-22**		R5x32-22**	DRYWELL REW32-22"	R5M32-22"	NEW 32 - 22**	
TACN TACN			TRKEE			1			25		1740	
EXAMENATION ANOMAL ANOM			1 WELD 1007.	1					(1 WELD EXAMINED)		(I WELD EXAMINED)	
VATE TRENTIFICATION	WELLD-SHB 1-1	151-138	WELD-RM.J-3 12" TSI-UK	WELD-RPAJ-5 12" ISI-13C	WELD-RWAJ-12 12** TS1-13C	RELD-PMA1-14 12" 151-13C		WELD-4583-14 12" (SI-130	WELD-RYB J-12 (12" 151-130	WELD-RMSJ-5 12" (SI-130	RELD-R983-3 (12"	
NET THE			Е					Ė				-
MO. PER			-		-	and		***	-	-		
AND RESCRIPTION OF TIEM TO BE EXAMINED	(CONTENDED) RECIRCHATION R	RECERCITATION MARENES A	RISEL F	RISER C	RISER J	RISER K	RECTREMENTATION MANIFOLD 8	RISER A	RISER B	RISER D	RISER E	
CATE CATE	-					-				************		
SUB	97.9				Andrew States	THE STATE OF THE S		A PROPERTY OF	-			

NORTHERN STATES POWER CO. MONTICELLO NOCLEAR GENERATING PLANT

TEN YEAR INSTRUME INSPECTION SUMMARY

TABLE 1.4

PAGE 10 OF 17

MAJOR ITEM: PIPING PRESSURE BOUNDARY

SUB TTIM	EXW. CATE- CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF LIEM TO BE EXAMINED	TOTAL NO. PER LIEM	NIX METHORS	IDENTIFICATION	EXAMENATION AMOUNT AND EXTENT	INSPEC- THON PERIOD	LOCATION OR SYSTEM NUMBER	RUNNENG PERCENT	REMARKS
84.7	8+J	BEANCH PIPE CONSECTION WELDS SIX INCH DIAMETER AND SMALLER								
		NAIN STEAM A	6	5	BRANCH WELDS 6" ISI-1	(3 WELDS EXAMINED) (1 WELD EXAMINED) 1 WELD 100%	ONE TWO THREE	DRYWELL PS1-18"ED	(50) (67) 83	
		PAIN STEAM B	3	S	BRANCH WELDS 6" ISI-Z	(7 WELDS EXAMENED) (NONE) NONE	ONE TWO THREE	DHYWELL PSZ-18"ED	(67) (67) 67	
		NAIN STEAM C	à	5	BRANCH WELDS 6" ISI-3	(2 WELDS EXAMINED) (NONE) 1 WELD 100%	OSE TWO THREE	DRYWELL PS3-18"ED	(50) (50) 75	
		NAIN STEAM D	6	S	BRANCH WELDS 6" ISI-4	(4 WELDS EXAMINED) (NORE) NONE	ONE TWO THREE	DRYWELL PS4-18"ED	(67) (67) 67	
		RECIPITATION A	i	8	BRANCH WELD 4" ISI-13A	(NONE) (2 WELDS EXAMINET, NONE	ONE TWO THREE	ORYWELL REWISA-28"	(67) 67	
		RECIRCULATION B	4	8	BRANCH WELD 4" ISI-138	(NONE) (3 WELDS EXAMINED) NONE	ONE TWO THREE	DRYWELL REWISE-28"	(75) 75	
		CRD SCRAM HEADER CRD 15-12" DB	3	5	BRANCH WELD 2" IST-24C	(NONE) (NONE) 1 WELD 100%	ONE TWO THREE	REACTOR BLDG CRD 18-2" DB	- - - - - 33	
14.8	8-3	SOCKET WELDS	111							
		MAIN STEAM A	H	5	SOCKET WELD 2" 151-1	(I WELD EXAMENED) (NONE) REMARKS*	ONE TWO THREE	PS15a-2"ED		PEXCLUDED FROM EXAM CAT- EGORY B-J REQUIREMENTS BY INB-1220(b)(1) AND
		MARK STEAM B	8	S	SOCKET WELDS 2" ISI-2	(1 WELD EXAMINED) (NONE) REMARKS*	ONE TWO	PS158-2"ED	(50) (50) 50	INCLUDED UNDER 84.11 OF THIS TABLE.
-		MAIN STEAM C	8	S	SOCKET WELD 2" IST-3	(1 WELD EXAMINED) (NONE) REMARKS*	ONE TWO THERE	PSISC-2"ED	(100) (100) 100	

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2 26 79

MONTHERN STATES POMER CO. MONTHCELLO NIKLEAR GENERATING PLANT

TEN TEAR INTERVAL INSPECTION SUMMARY.

TABLE 1.4

PAGE 11 OF 17

MAJOR ITEM: PIPING PRESSURE BOUNDARY

SIB	EXAM: CATE- CORY	OMPONENT OR SYSTEM, AND DESCRIPTION OF TIEM TO BE EXAMINED	TOTAL NO. PER ITEM	NDE. METHODS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING	REMARKS
84.8	B-J	(CONTINUED)								*EXCLUDED FROM EXAM CAT
		NAIN STEZM D	1	3	SOCKET WELD 2" ISI-4	(1 WELD EXAMINED) (NONE) REMARKS*	ONE TWO THREE	PS150-2"ED	(100) (100) 100	EGORY 8-J REQUIREMENTS BY IWB-1220(5)(1) AND INCLUDED UNDER 84.11 OF THIS TABLE.
		REACTOR WATER CLEAN UP	3	s	SOCKET WELD 2" 1SI-21	(NONE) (I WELD EXAMINED) NONE	ONE TWO THREE	REW31-2"ED REW3-4"EF	(33) 33	
		STANDBY LIQUID COTTROL	.15	S	SOCKET WELDS 1½" ISI-22	NONE (15 WELDS EXAMINED) 2 WELDS 1007.	ONE TWO THREE	CH2-15"EF, CH2-15"DC	(100) 190	
		RECIRCULATION A (DRAIN TO COS)	APPROX. 9 - 15	S	SOCKET WELDS	RELIEF REQUEST NO. 22		EEW28-2"EF	-	RELIEF REQUEST NO. 22
		RECIRCULATION E (DRAIN TO CEW)	APPROX. 9 - 15	S	SOCKET WELDS 2"	RELIEF REQUEST NO. 22	-	REW29-2"EF	-	RELIEF REQUEST NO. 22
		RECIRCULATION MANIFOLD A R TASS 2" OF MO2-65A	14	s	SOCKET WELDS 2" ISI-25	(NONE) (2 WELDS EXAMINED) 2 WELDS 1007,	ONE TWO THREE	VB5-2"DC	(14) 29	
		RECERCIFICATION MANIFOLD B BYPASS 2" OF MO2-65B	16	5	SOCKET WELDS 2" ISI-25	(NONE) (2 WELDS EXAMINED) 2 WELDS 100%	ONE TWO THREE	VB6-2"DC	(14) 29	
		CRD SCRAM HEADER DISCHARGES								
		A	3.	S	SOCKET WELDS 2" ISI-24C	(NONE) (NONE) 1 WELD 100%	ONE TWO THREE	CRD16A-2"DB	13	
			28	s	SOCKET WELDS 2" ISI-24C	(NONE) (NONE) 3 WELDS 100%	ONE TWO THREE	CRD168-2"DB	11	
		CRD SCRAM HEADER DRAIN	8	8	SOCKET WELDS 27 ISI-24C	(NONE) (NONE) 1 WELD 100%	ONE THREE	CRD18-2°D8	13	
		INSTRUMENT LINES	4	S	SOCKET WELDS 3" x 1\" 1S1-18, 19	(NONE) (NONE) NONE	ONE TWO THREE	15"-BC		INCLUDED UNDER 84.11 OF THIS TABLE

1+22

8/28/78

NORTHERN STATES POWER CO. MONETCELLO NUCLEAR GENERATING PLANT

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE 1.4

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MAJOR ITEM: PIPING PRESSURE BOUNDARY

FILM	EXAM. CATE- CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF THEM TO BE EXAMINED	TOTAL NO. PER TIEM	NTE METHORS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	EDCATION OR SYSTEM NUMBER	RUNNING PERCENT	REMARKS
84.9	1-1/-1	INTEGRALLY WELDED SUPPORTS								RELIEF REQUEST NO. 21
		MAIN STEAM A	3	117	WELDED SUPPORT 18" 1SI-1	(RONE) -(1 SUPPORT 100%) NONE	ONE TWO THREE	PS1-18"ED	(10)	STEAMLINES (18") COM- BINED FOR PERCENTAGE REQUIREMENT
		MAIN STEAM B	2 '	LETY"	WELDED SUPPORT 18" 1SI-2	(NONE) (NONE) NONE	ONE TWO THREE	PS2-18"ED	1	
		MAIN STEAM C	2	W.	WELDED SUPPORT 18" 1SI-3	(NONE) (NONE) I SUPPORT 100%	ONE. TWO THREE	PS3-18"ED	(20)	
		MAIN STEAM D	3	W.	WELDED SUPPORT 19" ISI-4	(NONE) (NONE) 1 SUPPORT 1002	ONE TWO THREE	PS%-18**CD	30	
		FEEDWATER A	2	संर	WELDED SUPPORT 10" 151-5A	(1 EXAMINED) (NONE) NONE	ONE TWO THREE	FW28-10"ED	(16)	FEEDWATER 10" COMBINED FOR PERCENTAGE REQUIRE MENT
		FEEDWATER B	1	175	WELDED SUPPORT 10" ISI-5A	(NONE) (NONE) NONE	ONE. TWO THREE	FW28-10"ED		
		PEEDWATER C		100	GELDED SUPPORT 10" 1ST-58	(NONE) (NONE) NONE	OME TWO THREE	FW2A-10"ED		
		FEEDWATER D	2	377	GELDED SUPPORT 10" 1SI-5B	(I EXAMINED) (NONE) NONE	ONE. TWO THREE	FW2A-10"ED	(33)	
		PEEDMATÉR A		107	WELDED SPYWORT 15" ISI-5A	FLEXAMINED +0023 (NONE) NONE	ONE TWO THREE	FW28-14"ED	(25)	
		FEEDWATER D	2.	52	WELLED SUPPORT 14" 151-58	(NONE) (NONE) NONE	ONE TWO THREE	FW2A-14°ED		FEEDWATER 14" COMBINES FOR PERCENTAGE REQUIRE MENT
		NIGH PRESSURE CONLANT DESCRION	3	171	WELDED SUPPORT 8" 151-7	(NONE). (NONE). + SUPPORT_1007.	ONE	metal across	1	

MORTHERN STATES POWER CO. MONTTOELLO MECLEAR GENERATING PLANT TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE 1.4

PAGE 13 OF 17

MAJOR ITHM: PIPING PRESSURE BOUNDARY

SAM EXAM	COMPONENT OR SYSTEM, AND RESCRIPTION OF ITHM TO RE EXAMINED (CONTLINED) REACTOR WATER CLEAN OF RESCRIPTION OF	T WELL! WEALTON TYLOIL	an an Nice	of an assessment control of the state of the	MELDED SUPPORT 4.º 121-9 MELDED SUPPORT (4.º 1751-9	FICATION EXAMPLES 5 SUPPORT 1 SUP	D SUPPORT (NONE) D SUPPORT (NONE) 1 SUPPORT (NONE) 1 SUPPORT (NONE)	B SUPPORT (NONE) B SUPPORT (NONE) I SUPPORT (NONE)
	RESIDIAL HEAT REMOVAL TWOS REACTOR CORE ENJECTION COOLLAST - STEAR	м	9 9	ACLASD SUPPORT 4" ISI-11D ACLASD SUPPORT 3" ISI-12	PORT	PORT (NONE) (NONE) REMAJES* PORT (NONE) NONE)	THE THE PERSON AND TH	(NONE) (NONE) REMARKS* (NONE) (NONE)
	RESIDUAL HEAT REMOVAL REWIO	12	a	WELDED SUPPORT	9	2.001 DAVAGES I CRUDE)		2,001 DROMETS (CRONE) (SNON)
	RESIDEAL HEAT REWWAL	(a)	- 5	ISI-118		et (1 EXAMINED) (NAME) NOME	٥	(1 EXAMINED) (NAME)
	RESTRUAL HEAT REMOVAL	G.	S	181-11C 16"	- 14	(1 EXAMEND) (BONE) NORE	2	(A EXAMEND) (BONE) NORE
	RECIRCULATION A	=======================================	ą	TST-13A	- 3	(1 EXAMINEN) 2 SUPFORT 100T		(MONE) (1 EXAMINEN) 2 SUPPORT 1907
	RECIRCULATION B	=	ā	HELDED SUPPORT 28" ISI-138	ã	CT (NOME) (1 EXAMINE) 2 SUPPORTS (00%	THE R. P. LEWIS CO., LANSING, MICH.	(NOME) (1 EXAMINED) 2 SUPPORTS LOOK
	RECIRCULATION MANIFOLD (A69	A(3) In	- 4	WEILER SUPPOR 22"-130 & ISI-130 &		EZ (NONE) (1 EKANINED) 2 SUPPORTS 1502		(1 EXAMINE) 2 SUPPORTS 1502
23 - 12 H-F-2	NAIN STEAM A		4	12-15.1 		(3 EXAMENEY) (NUME)	CHUSE THOSE CHUSE	EXAMENED) (NURE) NURE

NORTHERN STATES POMER CO. MORTHERLIO NUCLEAR GENERATING PLANT

ANYMMEN NOILDEACHT TWARBINE BYEA NET

											84,10	
											17-X-2	CATE
RESIDUAL HEAT REMOVAL	PEACTOR WATER CHEAR OF	COSE SPRAY B	CORE SPRAY A	PEEDWATER D	PERSONATER D	FESSWATER A	FESTMINTER A	MAIN STEAM D	MAIN STEAM C	MAIN STEAM B	(CONCLINION) (CONCLINION)	AND DESCRIPTION OF
P	19	14	10	14	u	14	W	i,ni		12	жи	NO. PEN
- 4	45	c	4	d	4	a	<	40	4	s		MUNICAN
SUPPORT	121-9 24 2097/027	SUPPORT 8"	SUPPORT 8"	151-58 151-58	SUPPORT 10"	PC-1ST 17a DROMAINS	VS-ISI 101 SERMAINS	SUPPORTS 18" 181-4	SEPPORTS 18"	SUPPORTS 18" TSI-2		MOLLYCHILMHIT
(NOME) (2 EXAMINED) 2 SUPPORTS 1097	(NONE) (1 EXAMINED) 1 SUPPORT 100%	(NOME) (1 EXAMINED) 1 SUPPOPUL 1007	(2 EXAMINED) (NONE) NONE	(2 EXAMINED) (NONE) NONE	(3 EXAMINED) (MONE) 1 SHFPORT 100Z	(2 EXAMINED) (NONE) 1 SUPPORT 1007.	(3 EXAMENED) (NONE) Note:	(2 EXAMINED) (1 EXAMINED) 1 SHEPOST 100%	(2 EXAMINED) (NORE) NORE	(2 EXAMINED) (NONE) 2 SUPPORTS 100%	SALVELLY COST LANGUAGE	NOTANI PARTA
COMI	ASSISTANCE OF THE STREET	SESSELL OWL BAD	ONE	STRING OPEL	SERRIL OPL SEC	SZBHIL OML SRO	ONE ONE SNO	JANEE OME. JANO	ONE TWO SANO	CML	DEBUGE	THON
45.81-01.838 03.81-01.838	44,0-1.83i	43.8-11AL	33.8-fM	F#2A-14*ED	DETWELL FW2A-16"ED	DEVWELL FW28-14"ED	FW28-10"ED	DEFLELL PS4-18"ED	PS3-18"ED	DRYNELL PS2-18"ED	SCHOOL SELECTION	LOCATION OR
(50)	100 ·	100	(100) (100)	(100) (100)	(100) (100)	(100)	(100) (100)	(67) (100) 100	(100) (100)	001 (100) (100)		PERCENTIN
												REMARKS

MAJOR ITEM: PIPING PRESSURE BOUNDARY

TABLE 1.4

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NORTHERN STATES POWER CO. NORTHERLIS MICHEAR GENERATING FLANT

TEN YEAR INTERVAL INSPECTION SUMMARY

HIGH EXAMINAT NO. PER METHERS (MECO)	HEAT REMOVAL 3 V SUPPORTS A 16"	REFERENCE AND PER METHERS IDENTIFICATION AND EXPENT AND	NT OR SYSTEM, ITEMAL NUE IDENTIFICATION EXAMINATION OF HITM NO.PER METHERS IDENTIFICATION AND EXTENT AND EXTENT SEPPORTS (ROME)	SAB CATE A CONTROL OF THE CONTROL OF	SES.		1 88 E S	REA COO	WES COO	97.*1 RES SEC CAO				
2 4 SUPPORTS 151-11C 151-11C	116 ^α V SUPPORTS 151-11C 2	116" (1 EXAMINED) 11S1-118 2 SUPPORTS 1002 Ψ SUPPORTS (NONE) 116" (NONE) 11S1-11C 2 SUPPORTS 1002	16" (1 EXAMINED) 1S1-118 2 SUPPORTS 100% Ψ SUPPORTS (NONE) 16" (NONE) 1S1-11C 2 SUPPORTS 100%	RESIDUAL BEAT REMOVAL	TW20	RESIDUAL HEAT REMINAL.		REACTOR CORE INJECTION COORLARY - STEAM	REACTOR CORE INJECTION COOLANT - STEAM RECIRCULATION A	REACTOR CORE INJECTION COOLANY - STEAM RECIRCULATION A RECIRCULATION B	REACIDE CORE INJECTION COOLANY - STEAM RECIRCULATION A RECIRCULATION BY-PASS (A & B)	REACTOR CORE INJECTION COOLANY - STEAM RECIRCULATION BY-PASS (A & B) RECIRCULATION BY-PASS (A & B) RECIRCULATION BANIFOLD A RECIRCULATION BANIFOLD A	REACION CONE INJECTION CONLANT - STEAM RECIRCULATION BY-PASS (A & B) RECIRCULATION MANIFOLD A & BYPASS LINE 2" RECIRCULATION MANIFOLD B RECIRCULATION MANIFOLD B	REACION CONE INJECTION CONLANT - STEAM RECIRCULATION BY-PASS (A & B) RECIRCULATION MANIFOLD A & BYPASS LINE 2" RECIRCULATION MANIFOLD B RECIRCULATION RISERS MANIFOLD A
	SUPPORTS 151-11C SUPPORTS 157-11C SUPPORTS 3" 151-12	16"	16"			14	10		10	5 5	2 10 10			
	SUPPORTS 16" 151-118 SUPPORTS 16" 151-11C SUPPORTS 151-12 SUPPORTS 28"	SUPPORTS	SUPPORTS	-	-41	4	<	<		<	< <	< < <	< < < <	4 4 4 4 4
	THE RESIDENCE AND ASSESSMENT OF THE PARTY OF	EXAMINATION ANDIOT AND EXTENT (NONE) (1 EXAMINED) 2 SUPPORTS 100% (NONE) (1 EXAMINED) 1 SUPPORT 100% (NONE) (1 EXAMINED) 1 SUPPORT 100% (NONE) (3 EXAMINED) 7 SHPPORTS 100%	EXAMINATION THOW AND EXTENT PERIOD (NORE) ONE (LEXAMINED) TWO 2 SUPPORTS 100% THREE (NORE) ONE (NORE) THREE (NORE) THREE (NORE) THREE (NORE) THREE (LEXAMINED) THREE (LEXAMINED) THREE (SUPPORT 100% THREE (SUPPORT 100% THREE) THREE		SUPPORTS 1151-118	SUPPORTS 16" 151-11C	SUPPORTS 3" 151-12	SUPPORTS 28" 151-13A		SUPPORTS 28" ISI-138	SUPPORTS 28" ISI-13B SUPPORTS 4" ISI-13AA 4 ISI-13BB	50 DE 3H SS 51	S1 10 00 34 50 41	O
		(33) 100 100 (50)		RIWARKS								(2°) BYPASS OF MO2-65A	(2°) BYPASS OF MO2-65A	(2") BYPASS OF MO2-65A

MAJOR ITEM:

TABLE 1.4

PAGE 15 OF 17

NORTHERN STATES POWER OD. MUNITICELLO NIXLEAR GENERATING PLANT

TEN TEAR INTERVAL INSPECTION SUMMARY

TABLE 1.4

PAGE 16 OF 17

MAJOR ITEM: PIPING PRESSURE BOUNDARY

SUB EXAM, CATE- CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF ITEM TO BE EXAMINED	TOTAL NO. PER ITEM	NEE METHORS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING PERCENT	REMARKS
4,10 5-K-2	(CONTINUED)								
	CRÓ SCRAM HEADER A	4 4 3 3	A. A.	SUPPORTS 8" 4" 6" 4" ISI-24A	1 SUPPORT 100% 1 SUPPORT 100% 1 SUPPORT 100% 1 SUPPORT 100%	REMARKS THREE THREE THREE THREE	CRD26A-8"1B CRD13A-4"DB CRD14A-6"DB CRD15A-4"D8	25 25 33 33	EXAMINATIONS NOT REQUIRED DURING PERIOD ONE AND TWO.
	CRD SCRAM HEADER B	4 4 3 4	9 9 9	SUPPORTS 8" 4" 6" 4" ISI-248	1 SUPPORT 100% 1 SUPPORT 100% 1 SUPPORT 100% 1 SUPPORT 100%	REMARKS THREE THREE THREE THREE	CED268-8"DB CED13B-4"DB CED14B-6"DB CED15B-4"DB	25 25 33 25	EXAMINATIONS NOT REQUIRED DURING PERIOD ONE AND TWO.
4.11 B-P	EXEMPTED COMPONENTS		- 1						
	HYDROSTATICALLY PRESSURE TELT- ED TO IMA-5000 AND IMB-5000 AT END OF TEN YEAR INTERVAL PLUS SYSTEM LEAKAGE EXAM EACH SCHEDWLED REFUELING OUTAGE	-	v	COMPONENTS	EXAMINED TO EVA-5000 AND EWB-5000	-	PRIMARY SYSTEM LINES THAT ARE EXEMPTED BY EWB-1220(b)		
	VENT LINE					-	V15-1"ED		P 6 ID M-115
	INSTRUMENT LINES					-	I"DC NIIA, NIIB, NIZA, NIZB		M-117
							FROM 1"DC RECIRCULATION RISERS		H-117
						-	FROM 1"EF REW28-2" & REW29-2"		M-117
	CONTROL ROD DRIVE SYSTEM					-	I" LINES FROM CRD HYDRAULIC UNITS		M-119
	STANDBY LIQUED CONTROL			4.04			1" LINES FROM LIQUID CONTROL N-10		M-116
	THER COMPONENTS						LINES AS REQUESTED FOR BELIEF AND LINES AS INDICATED BY IWB-1220 EXCLUSIONS		

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8/28/78

WINTERS STATES POMER CO.

COMMENTS NOTESTAND PROBLEMS NO. 52.

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PAGE 17 OF

17

TABLE

1.4

SJB 1700 84.12	SUB EXAM. FINDN OVIE. FINDN OVER. A. 12 8-6-2	PRESSURE-RETAINING BOLING PRESSURE-RETAINING BOLING	MENT ON TYBOL	NDE	MOLECULE SERVICEM NO.	AM E	EXAMENATION AND EXTENT	OOTHER DELICE ONLY DAWN	NAME AND ADDRESS OF THE OWNER, TH
		MAIN STEAM A	į.	<	SLEND FLANCE 6" ISI-1	(EXAMINED) 4 FLANCES LOGZ	9	233161 20 ONL 2080	2
		MAIN STEAM B	-	<	BLIND FLANCE 6" 151-2	I FLANCE 109Z (1 EXAMINED)		SERVE ONL SERVE	
		MAIN STEAM C	н	<	SLIND FLANCE 6" IS1-3	(BONE) (1 EXAMINED) 1 FLANCE 100Z		STANT.	THREE DRYNELL PS3-18"ED THREE DRYNEL PS3-18"ED
		MADE STEAM D	ž-	< :	BLDED FLANCE 6"	(4 EXAMINED) 4 ELANGES 1003	20	MAC	
		RESIDUAL HEAT REMOVAL	152	<	FIANCE/SPOR, 4" ISI-IID	(NONE) (Z EXAMINED) 2 FLANCES 100%	3	ONE ZAND	3
		RECINCULATION A	3-1	4	121-131 1" 339874 08178	(BONE) (BONE)	P1	THREE TWO	
		RECINCULATION B	100	<	BLIND FLANGE 4" 151-138	(NONE) (NONE)		OWE	
		RECERCULATION SYPASS LINE A		<	BAHAD FLANGE A"	(1 EXAMINED)		ONE	
		ESCINCULATION ESPIRES LINE B		<	BLEND FLANCE 4" ISI-13mb	(1 EXAMINE) 1 FLANCE 1002		33840. 3 663. 380	-

MENTICIALLO MECLIAR CORRATING PLANT

LEA LEASTH TRABLING BY A. N. S.

MAJOR ITEM: PUMP PRESSURE ROUNDARY

PAGE 1 OF 2

TABLE

85.6	85.5	85.4	2010		85.3	85.2				Married Speciment	85 E	MELL! BUS
85.6 B-L-1	85.5 B-R-2	B5,4 B-K-1			B-C-1	8-6-1				1	8-0-1	CATE:
PINE CASING WELDS	JUPPORT COMPONENTS	INTEGRALLY WELLED SUPPORTS	POMP A OR B	SECIRCHATION FLANCE BOLIS	(2 INCH AND LANGER DIA.)	PRESSURE-RETAINING BOLTS AND STUDY, WHEN REMOVED	PUNP B	PONE A	RECIRCULATION FLANCE BOLIS	(2 INCH AND LARGER DIA.)	PRESSURE-RETAINING BOLTS AND STUDS, IN PLACE	THE TO BE EXMINED AND DESCRIPTION OF AND DESCRIPTION OF
ZNON		,	16				25	5				NO. PER
			TT S-V				19-51 18-51	n-h				METHORS
	REMARKS	REMARKS	P-200A /P-200B 2.75" X 19.25" ISI-13A /13B				P-2008 2,75" X 19,25" ISI-138	P-200A 2.75" X 19.25" ISI-13A				IDENTIFICATION
			(NCME) (NCME) 16 BOLTS (1-16) NOTE B5.7				(1-16 EXAMINED) (1-9 EXAMINED) 7 BOLTS (10-16)	(1-16 EXAMINED) (1-10 EXAMINED) 6 BOLTS (11-16) NOTE 35.2				EXAMENATION INCOME
		1	THREE THREE	(Alexander			JASSHI OME JANO	ZHREE OME 380				TION
			RECURCULATION LOOP ASB				LOOP B, RECIRCULATION	LOOP A, RECIRCULATION				SYSTEM NUMBER
	ı	ı	100				(100) (136) 43	(100) (163) 37				RUNNING
000 to 400 to 500 to	INCLUDED IN 84.10 OF TABLE 1.4	TABLE 1,4	HEEN PUMP IS DISASSEMBLED (RELIEP REQ NO. 41	A SQUARE SANS							RELIEF REQUEST NO. 24	REMARKS

MONTICELLO MOCLEAR CENERATING PLANT

TEN YEAR INTERVAL INSPECTION SUMMARY

MAJOR ITEM: PUMP PRE SIRE BOUNDARY

TABLE

1.5

		Albane Marino		24	15 55		er yakeer	50	138
			-	55.9	15.8		-	35.7 6	WELL BES
				8-0-2		-		E-L-2	CORP.
Pings 8	Y dead	RECIRCULATION CLAND BOLTS	(LESS THAN 2 DICH DIA.)	PRESSURE-RETAINING BOLTING	EXEMPTED COMPONENTS	PISSP A or B	RECTRONATION	PER CASINES	THE TO BE EXAMINED AND DESCRIPTION OF COMPANY OF COMPAN
10	10		*******			pie			WELL!
a	<				,	<			SICHER
P-2008 1,375" DIA. 1SI-138	P-20GA 1.375" DIA. ISI-13A				REMARKS	P-200A/F-200B INTERIOS - ISI-13A/13B			IDENTIFICATION
(10 EXAMINED) (10 EXAMINED)	(10 EXAMINED) (10 EXAMINED)					(NONE) (NONE) 1 PUNE 100% 1NTERIOR SHRVACE NOTE B5.2			EXAMINATION AND MICHAEL AND
338HIL DAG JAGO	THAT OWE					ARREA ONL RO			THON PERMIT
LOOP B, RECIBOUATION	LOOP A, RECERCILATION					RECIRCULATION A OF B			SYSTEM NUMBER
(100) (200)	(100) (200) 100					100			PERCENT
	VISUAL EMAMS FOR PERIOD ONE AND TWO INCLUDED VGLUMETRIC FOR GLAND ROLIS, PURP A AND B.		CLAND SOLIS, FUMP A	PERIOD I REPLACED ALL	INCLUDED IN SYSTEMS LISTED IN 84.11 OF TABLE 1.4	*WHEN PUMP IS DISASSIMBLED (RELIEF REQUEST NO. 41)			REMARKS

NORTHERN STATES POWER (D. MONTICELLO NIKLEAR GENERATING PLANT

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE 1.6

PAGE 1 OF 6

MAJOR ITEM: VALVE PRESSURE BOUNDARY

ONENT OR SYSTEM, DESCRIPTION OF TO BE EXAMINED	TOTAL NO. PER ITEM	NITE METHORS	IDENTIFICATION	EXAMENATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING	REMARKS
RETAINING BOLTS AND PLACE								RELIEF REQUEST NO. 24
AND LARGER DIA.)			TYPE NO.					
A MOITAIN	24	V-UT	GATE MO2-53A 2" x 15.5" ISI-13A	(NONE) (1-12 EXAMINED) 12 BOLTS (13-24) NOTE 86,2	ONE TWO THREE	DRYWELL REW13A-28"	(50) 100	
	24	V-UT	GATE MO2-43A 2" X 15.5" ISI-13A	(NONE) (1-12 EXAMINED) 12 BOLTS (13-24)	ONE TWO THREE	DRYWELL REW13A-28"	(50) 100	
TATION B	24	V-UT	CATE M02-53B 2" X 15.5" ISI-138	(NONE) (1-12 EXAMINED) 12 BOLTS (13-24)	ONE TWO THREE	DRY IL REW138-28"	(50) 100	
	24	V-UT	GATE M02-438 2" X 15.5" ISI-138	(NONE) (1-12 EXAMINED) 12 BOL "S (13-24)	ONE TWO THREE	DRYWELL REWI3B-28"	(50) 100	
RETAINING BOLTS AND HEN REMOVED								
AND LARGER DIA.)			1245					
DIATION GATE VALVES	24	V-S UT	GATE VALVES 2" x 15.5"	(NONE) (NONE)	ONE			
3A 33B 31B			ISI-13A /138	24 BOLTS (1-24) NOTE B6.7		RECIRCULATION LOOP A & B	100	WHEN VALVES DISASSEM- BLED (RELIEF REQ NO. 42
LY WELDED SUPPORTS	-		REMARKS				-	SUPPORTS ARE LISTED UNDER 84.9 OF TABLE 1.
COMPONENTS	-	-	REMARKS	3 34	-		-	SUPPORTS ARE LISTED UNDER 84.10 OF TABLE 1.
DY WELDS	NONE							
DY WELDS		NONE	NONE	NONE	NONE	NONE	NONE	NONE

NORTHERN STATES POWER CO.

MONITICELLO
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TABLE 1.6

PAGE 2 OF 6

MOUGH FIEM: VALVE PRESSURE BOUNDARY

6 9	10181	Yes					. 21	-1			THE RESIDENCE			
								-					86.7	MED!
							-					THE RESERVE	B-M-2	CATE-
CHECK NALVE	ROCKWELL		ATMOOD MORRILL CHECK VALVE	CHECK SATAR VACABOR				RELIEF VALVES				CLOSE VALVE CLOSE VALVE CLOSE VALVE CLOSE VALVE CLOSE VALVE CLOSE VALVE CLOSE VALVE CLOSE VALVE CLOSE VALVE CLOSE VALVE	VALUE BUDGES	GRUMNES SE OL MELL TO NEEDEN OF TOWNS SEED OF SEEDING
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VL.1 - 510V	A014-138	A010-46A	FW-97-1 FW-94-1 A010-468	FN-91-2 FN-94-2	842-71B 842-71F	RV2-71C RV2-71H	8V2-718 8V2-70G	RV2-71A RV2-71E	A02-80b A02-86b	A02-80C A02-86C	A02-808 A02-868	A02-80A A02-86A		IBENTIFICATION
	- KANINE THE INTER-		EXAMINE THE INTER-	NALS OF ONE VATVE.				EXAMINE THE INTER-				EXAMINE THE INTER-		WOLLY WAS EXISTED AND WAS AND
-	19812		THREE	THREE				THREE				THREE		NOTE:
AND STANKS	CORE SPRAY A	NAME - MAN	FEEDSATER B FW2A-14"ED RHR - TW2O TW2O-16"DB	FEEDWATER A	MAIN STEAM D PS4-6"ED	MAIN STEAM C	MAIN STEAM B	MAIN STEAM A PS1-6"ED	MAIN STEAM D PS4-18-ED	MAIN STEAM C	MAIN STEAM B PSZ-18-ED	MAIN STEAM A		SYSTEM NAMBER
100	š	*******	18	100				100				100		PERCENT N
							PLANTS OFTION.	WALVE LOCATIONS, NEMBERING AND ANOUNT						REMARKS

NORTHERN STATES POWER CO.

MONTICELLO

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE 1.6

PAGE 3 OF 6

MAJOR ITEM: VALVE PRESSURE BOUNDARY

SUB ITEM	EXAM. CATE- GORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF ITEM TO BE EXAMENED	TUTAL NO. PER ITEM	NDE METHORS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING PERCENT	REMARKS
B6.7	B-H-2	(CONTINUED)								
		ANCHOR GATE VALVE	15	V	POS-1758 NO-1754	EXAMINE THE INTER- NALS OF ONE VALVE	THREE	CORE SPRAY A TW7-8"EF	100	
					POS-1757 MO-1753			CORE SPRAY B TW11-8"EF		
					М0-2034 М0-2035			HPCI - STM. PS18-8"ED		
					M0-2029 M0-2030 P0S-2028			RHR - REWIO REWIO-18"ED		
					PV-98-2			FEEDWATER A FW2B-14"ED		
					FW-98-1			FEEDWATER B FW2A-14"ED		
					POS-2019 MO-2015			RHE - TW20 TW20-16"DB		
					POS-2018 MO-2014			RHR - TW30 TW30-16"DB		
		CRANE CHAPMAN GATE VALVE	6	v	M02-65A M02-65B	EXAMINE THE INTER- NALS OF ONE VALVE.	* THREE	RECIRCULATION REW32-22"	100	*WHEN VALVES ARE DISASSEMBLED (RELIEF REQUEST NO. 42
					M02-53A M02-43A M02-53B M02-43B			RECIRCULATION A REW13A-28" RECIRCULATION B REW13B-28"		
16.8	в-Р	EXEMPTED COMPONENTS	-		REMARK		- 1		-	INCLUDED IN 84.11 AT TABLE 1.4
16.9	8-G-2	PRESSURE-RETAINING BOLTING (LESS THAN 2 INCH DIA.)			VALVE TYPE NO.					
		MAIN STEAM A	2	v		(100% EXAMINED)	ONE.		(50)	
					A02-86A	100%	THREE	PS1-18"ED	100	

1 +33

3/5/80

MONTHERN STATES POMER (D). MONTH CELLO MINILEAR CENERATING PLANT

TEN TEAR INTERVAL INSPECTION SUMMANY

TABLE 1.6

PAGE 4 OF 6

MAJOR ITEM: VALUE PRESSURE BOUNDARY

FIEM CATE- GORY	AND DESCRIPTION OF TIEM TO BE EXAMINED	NO. PER TTIM	NTE METHODS	IDENTIFICATION	EXAMINATION AMOUNT AND EXTENT	INSPEC- TION PERIOD	LOCATION OR SYSTEM NUMBER	RUNNING PERCENT	REMARK"
5-0-2	(CONTINUED)					A AMARICA			
	MAIN STEAM B	2	V	GLORE A02-808 A02-868 ISI-2	The second secon	TWO. THREE	PSZ-18"ED	(50) 100	
	MAIN STEAM C	ž	ν.	CLOBE A02-86C A02-80C ISI-3	(196% EXAMINED) 100%	TWO THREE	PS3-18"ED	(50) 100	
	MAIN STEAM D	2	¥	GLOSE A02-80D AC2-86D	(100% EXAMINED) 100%	THREE	PS4-18"ED	(50) 100	
	NAIN STEAM A	2	¥		(100% EXAMINED) 100%	THPEE	PS1-6"ED	(50) 100	
	MAIN STEAM B	2	V	RELIEF RV2-715 RV2-7186G ISI-2	(100% EXAMINED) 100%	ONE THREE	PS2-6"ED	(50) 100	
	MAIN STEAM C	2	V	RELIEF RV2-71C RV2-71H LSI-3	(100% EXAMINED) 100%	ONE	PS3-6"ED	(50) 100	
	MAIN STEAM D	2	V	RELIEF RV2-71F RV2-71D 151-4	(100% EXAMINED) 100%	ONE TUREE	PS4-6"ED	(50) 100	
	FEEDMATER A	3	¥		(100% EXAMINED) (100% F.AMINED) 100%	ONE ONE THREE	FW28-14"ED	(67) 100	
	FREDMATER B	3	¥	CHECK FW-94-1	(100% EXAMINED) (100% EXAMINED) 100%	TWO TWO THREE	FW28-14"ED	(67) 100	
	HICH PRESSURE COOLANT INJECTION - STEAM	2	2	GATE MO-2034 MO-2035	(100% EXAMINED) 100%	THREE	PS18-8"ED	(50)	

E426/78

NAMINERO STATES POMER CO.
NAMINETO STATES POMER CO.

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MELLI	86.9									-
AMIN'S BIND WING	-									
ONDERED OR SYSTEM,	(CONTINUED)	CORE SPRAY A	CORE SPRAS B	REACTOR WATER CLEAN UP	RESIDUAL HEAT REMOVAL REWIO	RESIDUAL HEAT REMOVAL TW20	RESIDUAL HEAT REMOVAL TW30	TAP SKRE LYSH TWINGSER	REACTOR CORE INJECTION	EYEASS
MELLI		w	W	Ę.	(a)	Lei	la)	13	14)
NUC SIN		e ₅	*	10	4	4	<	45		×
METHOR IDENTIFICATION		GATE NO-1754 CHECK A014-138 GATE POS-1758 ISI-6A	CATE MO-1753 CHECK A014-13A CATE POS-1757 ISI-68	GATE MO-2398 GATE MC-1 GATE MO-2397 ISI-9	GATE POS-2028 GATE MO-2030 GATE MO-2029 IST-11A	GATE POS-2019 CHECK A010-468 GATE MO-2015 ISI-118	GATE MO-2014 GATE POS-2018 CHECK A010-46A ISI-11C	CHECK 1918-21 CATE 190-2027 ISI-7/10	GATE NO-2076 NO-2075 ISI-12	CATE MOZ-54A
EXAMINATION EXAMINATION INCOME.		(100% EXAMINED) (100% EXAMINED)	(100% ESAMDRED) 100% 100%	2001 (CBNINVE 2001) (CBNINVE 2001)	(100% EXAMINED) (100% EXAMINED) 100%	(100% EXAMINED) (100% EXAMINED)	(100% EXAMINED) (100% EXAMINED) 100%	Z001 (2001 EXAMINED)	(100% EXAMINED) 100%	(1962 EXAMINED)
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TOCATION OR		747-8"EF	TV11-8"EF	RENG-4"EF	REW10-18"ED	7W20-16"DB	TW30-16°DB	TW36-4"ED	PS17-3"ED	RE#24-4"
PUNNING		(67) 100	100	(67) 100	(67) 100	(67) 100	(67) 100	100	100	(100)
REMARKS										

MAJOR ITEM: VALVE PRESSURE BUNDARY

PAGE 5 OF 6

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TABLE 1.6

MONTHOPIA STATES FOWER CO.

TEN TEAT INTERVAL INSPECTION SUMMARY

PAGE 6 OF 6

MAJOR ITEM: VALVE PRESCREE SOUNDARY

			Transport Statement	-						86.9	MGDTI
										N-G-2	DANK DANK
	CHO SCRAM HEADER DRAIN LINE	RECIBERATION B.	RECERTIFATION A DRAIN LIME	DRAIN STEAM	STANDBY LIQUED	BOTTOM HEAD DRAIP	MANIFOLD B	RECERCIFATION MANIFOLD A	RECIRCULATION S BYPASS	(CONTINUED)	COMPONENT ON SYSTEM, AND DESCRIPTION OF
	ler .	fa.	19	14	ы	14	14	2	14		MULLI MULLI WILLI
			-	45	4	- <	- <				AICHLEM HEN
	DIAPBRAN 181-24C	CLOBE XR-6-2 CLOBE XR-7-2	CLOBE XR-6-1	CATE NO-2373 CATE NO-2374 ISI-23	GATE XP-7 OHEOX XP-8 OHEOX XP-6 ISI-22	CLOBE XDV-4	CATE MO2-668 MO2-658 ISI-130	GATE H02-65A H02-66A 1S1-13C	CATE NO2-548 ISI-1388		IDENTIFICATION
				ONE VALVE 100%	ONE VALVE 100%		2001 (1002 2001)	2001 (USKINEXE 2001)	2001		INSLICE GIVE LANGING NO. LINEWING.
				OMI	ZUMET	1	JYSHEE ON2	338EL 06U	TABEL		THON THON
	CRB1 8-2"D8	RE#29-2	EDI28-2	PS15-3-ED	CH2-15-DC	REK31-2"ED	2 DICH BYPASS OFF REW32-22"	2 INCH SYPASS OFF BEN32-22"	REN25-4"		LOCATION OR
The control of the co		1 1	1 1	(36)	116	,	(50)	100	100		RUNNIN
	HAD NOT BEEN REQUISED IN PREVIOUS IST PROGRAM	RELIEF REDUEST NO. 22 VALVES ARE NORMALLY CLOSED.	RELIEF REQUEST NO. 22 VALVES ARE NORMALLY CLOSED.	HAD NOT BEEN REQUIRED IN PREVIOUS IST PROFRAM.	HAD NOT BEEN REQUIRED IN PREVIOUS IST PROCEAR.	HAD NOT BEEN REQUIRED IN PREVIOUS IST PROCEASE.					REMARKS

ASME Section XI Nondestructive Examination Program - Class 2

ASME Code Edition and Addenda: 1974 Edition through and including Summer 1975 Addenda

Program Period: February 28, 1978 to June 30, 1981 (Third Inspection Period)

NOTES:

- 1. The following tables identify the specific Class 2 components and parts to be examined. These tables can be directly correlated with Table IWC-2520 and Table IWC-2600 of Section XI and identify the examination method for each listed item. In period one and two, Class 2 components and parts were not required to be examined; because of this, the Class 2 inspection program will begin with period three. The tables identify the number of items required to be examined over a forty (40) year service lifetime, and the amount required for a ten (10) year inspection interval. The tables also show the amount of items required to be examined during period three (which is approximately 1/3 of that required for an inspection interval), and the percentage that will have been completed by the end of that period based on the 40 year requirements.
- 2. The scope of the inspection program for Class 2 components was based on the exemption criteria of IWC-1220.
- 3. In accordance with the requirements of IWC 2411 the nondestructive examinations were selected so that the total examinations completed over forty (40) years will be 100% of the required examinations of the systems or portions of the systems with a single stream or be equivalent to having performed 100% of the required examinations in one of the streams of a multiple stream system. The only exception is that the selection of pressure retaining bolting for valves was based on the type, manufacturer, and design of valve and not on the total number of certain size valve bonnet bolts per system.
- 4. Repairs will be performed in accordance with the applicable requirements of the latest edition and addenda of the ASME Code, Section XI. However, if rules for a particular repair are not specified in Section XI, the original design specification and Construction Code of the component or system, or later editions of the Construction Code or ASME Code Section III, either in their entirety or portions thereof, may be used.

LEGEND:

Examination method:

V - visual

U.T. - ultrasonic

R.T. - radiography

S - surface examination, either liquid penetrant or magentic particle

Inspection Period

ONE - June 30, 1971 to October 30, 1974

TWO - October 30, 1974 to February 28, 1978

THREE - February 28, 1978 to June 30, 1981

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				DOCATION
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MAJOR FIEM: PRESSURE VESSELS

PAGE 1 OF

TABLE 2.1

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EL 978' GPENET, XIOA EL 978' GPENET, XIOA	EL 913" TURES CHAMBER EL 905" RECI PURP ROOM EL 905" RECI PURP ROOM		EL 949' GPENET, X-11		EL 926" TORUS CHAMBER			PERIOD THREE STABTING DATE IS FEBRUARY 28, 1978 ELEVATIONS ARE CENERAL, ALL CATHORRES	MODATION
-CS PUNP 1B-		ISI-33 SINGLE STREAM -DISCHARGE-		ISI-32 SINGLE STREAM -IMLET-		STREAM -DISCHARGE-	(2) WHERE APPLICA- BLE, PERCENT INDI- CATES COMBINED PER- CENTAGE OF MULTIPLE STREAMS.	BELLIEF REQUEST NO. 21 (1) THER PERIOD PERCENT COLUMN IS 1/3 INTERVAL OF EXAMS PROJECTED INTO REQUIRED EXAM-DIANTON OF 40 YEAR EXAM COLUMN WAS NOWN IS HOUNDED OFF TO NEXT HIGHEST JOINT AMOUNT.	SXRMERR

NORTHERN STATES POMER CO. MONTTCELLO UNIT 1

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE		3,2,1		
PAGE	2	OF	3	

MAJOR ITEM: PIPING - CIRCUMFERENTIAL BUTT WELDS

SUB THM	CAM CATE- GORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF LITEM TO BE EXAMINED	NINE MEDIANIS	TOTAL ITEMS	ACCES- TRLE THMS	40 YR. AMOUNT	10 YR. AMOUNT	THIRD PERIOD AMOUNT	THIRD PERIOD	LOCATION	REMARKS
(2,1)	CHG	(COSTINUED)						ASSEST	PERCENT		-
		CORE SPRAY A 5 8 10"									
		W. 10 1 1 0 1 10									ISI-34 6 ISI-35
		TW7-10"GE A	UT	14	14	4.					MULTIPLE STREAM
- 1		TWL1-10"GE B	TE	10	10 .	2		1 2	17	EL 976' REACTOR EL 971' BLEG	-CS PUMP IA-
1	100									CL SCA DLIKE	CORE SPRAY A & B
2.1	C-C	CONTAINMENT PURGE									COMBINED
		CP1-18"HE A	177								151-38.
1						1				EL 925' @ PENET. X-26	MULTIFLE STREAM
		CP1-18"HE B	UT	3 7	3					TORUS CHAMBER	PURGE LINE
									- 1	EL 976' @ PENET, X-25 BWCU ROOM	A & B COMBINED 151-388
1.1	C+G	RHR SERVICE WATER								THE REAL PROPERTY.	MULTIPLE STREAM
		SW9-8"GE	177	47	47	24	6	2		REACTOR	151-39
1.1	C-F	CIRCUMPERENTIAL BUTT WELDS							8	EL933* BLDG	SINGLE STREAM
		The bear and the									RELIEF REQUEST NO.
1	C-F	MAIN STEAM A		1.1							ISI-26
1		PSI-18"ED	177								MULTIPLE STREAM
				16	16 -	4		1	6	EL 936' STEAM CHASE	
	C+2	MAIN STEAM B						(4)		(1978 BASTLINE)	
	100	PS2-18**ED									IS1-27 MOLTIPLE STREAM
	10.78	***************************************	UT	15	.15	4	1.1	1	13	EL 940' STEAM CHASE	THE REAL PROPERTY.
	C-F	MAIN STEAM C						(2)		(1978 BASELINE)	
1		2013 1 SHOW									ISI-28 MULTIPLE STREAM
		PS3-18"ED	EL.	16	16	4	1	-	-	EL 942* MOISTURE SEPRIR	CHAPTELL STREAM
- 1	C-F	MAIN STEAM D						(2)	- 1	(1978 BASELINE)	
		The Part of the Pa							- 1		ES1-29
- 1		PS4-18"ED	UT	16	16	4			- 1	EL 942' MOISTURE SEPRIR	MULTIPLE STREAM
-	C-F	SUPPLY TO STEAM						(2)	- 1	(1978 BASELINE)	
- 1		SEAL SYSTEM							1		
- 1		Inch I. & Hess		1							151-30
1	1	PS11-6"ED	UT	. 8	. 8	2	1		- 1	EL 940° MOISTURE SEPRIE	MULTIPLE STREAMS
		PS12-6"ED	BY	- 5	5			(1)	- 1	(1978 BASELINE)	
-		P513-6"ED	UT	5	5	1	1	1	17	EL 940° MOISTURE SERRIR	MULTIPLE STREAMS
		PS14-6"ED	UT	5		1					NULTIPLE STREAMS
1		(SIX INCH LINES COMBINED)		- 1	1		1	1	200		MULTIPLE STREAMS

+40

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MONTHURN STATES POWER CO. MONTHURLED UNIT 1

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE 2,2.1

PAGE 3 OF 3

MAJOR ITEM: PIPING - CIRCU GERENTIAL BUTT WELDS

SUB LIDM	EXAM CATE- CORY	OMPONENT OR SYSTEM, AND DESCRIPTION OF LITEM TO BE EXAMINED	NDE METHODS	TOTAL TIMS	ACCES- USLE LTEMS	40 YR. AMOUNT	10 YR. AMOUS:	THIRD PERIOD AMOUNT	THIRD PERIOD PERCENT	LOCATION	REMARKS
(2,1	C-F	(CONTINUED)									
		SUPPLY TO STEAM SEAL SYSTEM									ISI-30
	Ħ.	PS10-5" - PS7-10"ED PS7-8"ED	UT UT UT	18 1' 7	18 16 7	18 16 7	5 4 2	2	11 6	EL 940' MOISTURE SEPRIR EL 940' MOISTURE SEPRIR EL 940' MOISTURE SEPRIR	SINGLE STREAM SINGLE STREAM SINGLE STREAM
	C-F	HIGH PRESSURE CONTARY INJECTION - WATER SIDE									IS1-31 -DISCHARGE
	11.0	7W3-12"ED	ET	6	6	6	2			EL 933' STEAM CHASE	SINGLE STREAM
	C-F	FEEDGATER S				3.7.7				(TO) FW2B-14"ED	ISI-37
	111	FW28-14"ED	UT	3	3	1	-			EL 940' STEAM CHASE	MULTIPLE STREAM
		FEEDMATER A									IS1-37
		F#2A-14"ED	11.1	3	3	2			33	EL 940° STEAM CHASE	MULTIPLE STREAM FEEDWATER A & B COMBINED
	C-F	REACTOR WATER FROM SKIDMER SYSTEM						4-11-1			ISI-36
		REW11-8"HE	117	29	29	29	8	2	7	EL 1007* REACTOR BLDG © SKIDDER TANK	SINGLE STREAM
	6-8	MAIN STEAM EQUALIZING BEADER									181-40
ı	C-F	PS30-18"EDB	07	2*	21	21	6	2 (21)	10	ZL 940' MOISTURE SETETR (1978 BASELINE)	SINCLE STREAM
		10" DRIP LEC	111	2	2	. 2	2	(2)		(1978 BASELINE)	
									1		

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THERE ARE NO ITEMS WITH SEP. D FIT- TINGS REQUIRED FOR SCHEDULING.	SYRVMER

MAJOR ITEM: PIPIDG - LUNGITUDINA, WELD JOINTS IN FITTINGS

TABLE

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NORTHERN STATES POWER CO.

TEN YEAR INTERVAL INSPECTION SUMMARY

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	ACCES-
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	10 YR. AMOUNT
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THERE ARE NO TRANCH WELD JOINTS REQ'D FOR SCHEDILING	REMARKS

MAJOR ITEM: PIPING - BRANCH PIPE TO PIPE WELD JOINTS

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PAGE TABLE

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	02.4	MCLLI
	C-0	CATE-
	PRESSURE RETAINING BOLIUM	AND DESCRIPTION OF
	1	WELLOUS MOR
	REMARKS	SACLLI
		TENT
		40 YR. AMOUNT
		19 YR.
		PERIOD AMOUNT
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SURE-FETA IN ME SURE-FETA IN GENERAL SURE- BOLTING EXCEEDING I-ING IN DIAMETER REQUIRED FOR SCHED- ULING.	THERE ARE NO BEEC.	REMARKS

NORTHERN STATES POWER OD. MONTICELLO UNIT 1

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE 2.2.5

PAGE 1 OF 2

MAJOR ITEM: PIPING - INTEGRALLY WELDED SUPPORTS

SUB FTEM	CATE- CORY	OMPONENT OR SYSTEM, AND DESCRIPTION OF ITEM TO BE EXAMENED	NDE METHODS	TOTAL ITEMS	ACCES- TBLE TTEMS	40 YR. AMOUNT	10 YR.	THIRD PERIOD AMOUNT	THIRD PERIOD PERCINI	LOCATION	REMARKS
C2.5	C-E-I	INTEGRALLY WELDED SUPPORTS									
	C-E-1	MAIN STEAM A								MOISTURE SEPERATOR ROOM	ISI-26
		PS1-18"ED	S	1	1	100% PER	1	1	100	EL 938' @ MS STOP VALVE	
		MAIN STEAM B				INTERVAL.					151-27
	11.	PS2-18"ED	S	1	1-1	100% PER	-	-		EL 938' @ MS STOP VALVE	
		MAIN STEAM C				INTERVAL.					ISI-28
		PS3-18"ED	S	1	1	100% PER	-	-	-	EL 938' @ MS STOP VALVE	
		MAIN STEAM D				INTERVAL					ISI-29
		PS4-18"ED	S	1	1	100% PER	-	-	-	EL 938' @ MS STOP VALVE	MULTIPLE STREAMS
	C-E-1	SUPPLY TO STEAM SEAL SYSTEM				INTERVAL					18" LINES COMBINE
		PS14-6"ED	s	5.	1	100% PER	1			EL 940" @ PS 4-18"ED	ISI-30 MULTIPLE STREAM
	C-E-I	HIGH PRESSURE COOLANT INJECTION - WATER SIDE				INTERVAL			-		(SINGLE ITEM)
		TW3-12"ED	s	4	4	1,00% PER					
	C-E-1	HIGH PRESSURE COOLANT INJECTION - STEAM SIDE				INTERVAL	4	1	25	EL 915' HPCI PUMP ROOM EL 926' TORUS CHAMBER	ISI-31 SINGLE STREAM
		PS18-8"ED	s	7	2	100% PER	2			EL 945' STEAM CHASE	ISI-32
	C-E-I	HPCI - STEAM DISCHARGE				INTERVAL				EL 906" TORUS CHAMBER	SINGLE STREAM
		8SZ-16"16E	S	2	2	100% PER	2		50	EL 920' HPCI PUMP ROOM	181-33
	C-E-1	CORE SPRAY A				INTERVAL					SINGLE STEAM
		TW7-8"ED TW7-10"CE	S	2 3	2 3	100% PER	1 2	1 10-10		EL 978 RUCH BOOM	ISI-34
						INTE. TAL			50	EL 927 TORUS CHAMBER	MUSTIPLE STREAM

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NORTHERN STATES POWER CO. MONTICELLO UNIT 1

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE 2,2,5

PAGE 2 OF 2

MAJOR TIEM: PIPING - INTEGRALLY WELDED SUPPORTS

SUB TTEM	EXAM CATE: CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF ITEM TO BE EXAMINED	NDE METHOOS	TOTAL ITEMS	ACCES- IBLE ITEMS	40 YR. AMOUNT	10 YR. AMOUNT	THIRD PERIOD AMOUNT	THIRD PERIOD PERCENT	LOCATION	REMARKS
62.5	C-E-1	(CONTINUED)									
		CORE SPRAY B									
		TW11-8"ED TW11-10"CE	S	NONE.	-	100% PER	1		-	EL 950 REACTOR BLDG	181-35
		1911-10-05				INTERVAL				SU 230 REACTOR BLAS	MULTIPLE STREAM CORE SPRAY A & B COMBINED
	C-E-1	REACTOR WATER FRONT SKIMMER SYSTEM									
		REW 11-8"HE	S	- 5	5	100% PER INTERVAL	. 5	2	40	EL 1005' @ SKIMMER TANK EL 998' REACTOR BLDG	ISI-36 SINGLE STREAM
	C-8-1	FHR SERVICE WATER									
		SW9-8"CE	(5)	2	2	100% PER INTERVAL	2			EL 928 AUX BLDG EL 920 AUX BLDG	ISI-39 SINGLE STREAM
									-		

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8/28/78

MONTICELLO UNIT 1 HEN YEAR INTERNAL INSPECTION SUMMAN

CZ.6 C	C-E-2	COMPONENT OR SYSTEM, AND DESCRIPTION OF ITEM TO BE EXAMBLED SUPPORT COMPONENTS	METHORS	SPELLI	I I I I I I I I I I I I I I I I I I I	40 YR. AMOUNT	10 YR. AMOUNT	PERIOD	PERCENT	MESON PROPERTY.
and the state of t	CE-2	SUPPORT COMPONENTS NAIN STEAM A								
O'ACLESSON.	THE REAL PROPERTY.	FS1-18"ED	۷.	•	25	1002 PER	2		,	1 20
	-	MAIN STEAM B				INTERVAL		W.	No.	
		PS2-18"ED	V	D)	6	100% FER	jet	Total Service		1
		MAIN STEAM C				INTERVAL		Carrier Street		
		PS3-18"	V	6	ō	100% PER		3-4		MCMA ACM
		KAIN STEAM D				TVARRIEL		Terror	THE STATE OF THE S	
		PS4-18"ED	٧	g.	6	100% PER INTERVAL		6.3	2	
9	982	SUPPLY TO STEAM SEAL SYSTEM	******					- Kenraja ini	olenoga, im	
AND A COMPANY PLANSAGE	THE REAL PROPERTY.	PS11-6"ED	ď	i,ui	ω	100% PER INTERVAL		-	-	
MANAGEMENT COM		PS12-4,"20	<	1	ы	INTERVAL				****
	Office Statement and	63.,9- ISA	×	N	2	100% PER INTERVAL		14	1-11	
		PS_4-6"ED	~	43	2	1901 PER INTERVAL				
		PS 7-10"ED	V	9	9	TVAMAINI ESA 2001		0	22	
ORONON SUN FOR ARCHITECTURE		757~8" ED	<	2	1-2	1001 PER INTERVAL		10	2	

MAJOR ITIM: PIPING - SUPPORT CONCURENTS

PAGE 1 09

TABLE

NORTHERN STATES POWER CO. MONTECELLO UNIT 1

TEN YEAR INTERVAL INSPECTION SEMMARY

TABLE 2.2.6

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MAJOR ITTM: PIPING - SUPPORT COMPONENTS

SUB	EXAM CATE- CORY	OMPONENT OR SYSTEM, AND DESCRIPTION OF LITEM TO BE EXAMINED	NDE METHODS	TOTAL TIMS	ACCES- TBLE THMS	40 YR. AMOUNT	10 YR. AMOUNT	THIRD PERIOD AMOUNT	THIRD PERIOD PERCENT	LOCATION	REMARKS
C2.6	C-E-2	RIGH PRESSURE COOLANT INJECTION - WATER SIDE									151-31
		TW3-12"ED	· 0	9	9	100% PER	9	3	33	EL 926'TORUS CHAMBER	SINGLE STREAM
	C-E-2	HIGH PRESSURE COOLANT INJECTION - STEAM SIDE				INTERVAL				EL 915'TORUS ROOM	ISI-32 - INLET-
		PS18-8"ED	V	13	13	100% PER INTERVAL	13	4	31	EL 943' STEAM CHASE EL 949' EL 906' HPCI PUMP ROOM EL 905' HPCI PUMP INLET	SINGLE STREAM
	C-E-2	HIGH PRESSURE COOLANT INJECTION - STEAM DISCH.									ISI-33 - DISCHARG SINGLE STREAM
		RS2-16"HE	V	. 6	6	1002 PER INTERVAL	- 6	2	33	EL 905' HPCI PUNT ROOM @ DISCHARGE	
	C-E-2	CORE SPRAY A & B									151-34 & 151-35
		TW7-10"GE A	v	3	3	100% PER	2	1	25	EL 955' REACTOR BLDG	MULTIPLE STREAM
		TW11-8"GE B	V	4	4	INTERVAL.	2		-	AND TOO MANAGEMENT AND AND ADDRESS OF THE PARTY OF THE PA	
		CORE SPRAY A & B									ISI-34 & TSI-35 MULTIPLE STREAM
		TW7-8"ED A	V	1	1	100% FER	2				CORE SPRAY
		TW11-8"ED B	V	2	2	INTERVAL		1	50	EL 971 REACTOR BLDG	A & B COMBINED
	C-E-2	REACTOR WATER FROM SKIMMER SYSTEM							i		SI-36 SINGLE STREAM
		6FW11-8"HE	v .	4	4	1001 PER INTERVAL	4	1	25	EL 998' REACTOR BLDG 0 SKIMMER TANK	
	C-E-2	CONTAINMENT PURGE A									151-383
		CP1-18"HE	v	2	. 2	100T PER		1	100	EL 925' TORUS CHAMBER	STREAM STREAM
		CONTAINMENT PURGE B				INTERVAL				(ATOP)	TSI-368
		CP2-18"HE	v	SONE		100% PER			-	EL 976' RWCD & PENET.25	MULTIPLE STREAM PURCE LINES COMMINGE

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NORTHERN STATES POMER CO. MONTECELLO UNIT 1

TEN YEAR INTERVAL INSPECTION SUMMA

TABLE 2.2.6
PAGE 3 OF 3

MAJOR ITEM: PIPING - SUPPORT COMPONENTS

SUB	EXAM CATE- CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF LITEM TO BE EXAMINED	NOE METHODS	TOTAL TIEMS	ACCES- TELE TIEMS	40 YR. AMOUNT	IO YR. AMOUNT	THIRD PERIOD AMOUNT	THIRD PERIOD PERCENT	LOCATION	REMARKS
C2.6	C-E-2	(CONTINUED)									
	C-E-2	RHR SERVICE WATER									
		SW9-8"GE	V	15	15	1001 PER INTERVAL	15	4	26	EL 920 REACTOR BLDG EL 931	ISI-39 SINGLE STREAM
	C-E-2	MAIN STEAM EQUALIZING HEADER									
		PS30-18"EDB	V	3	3	100% PER INTERVAL	3	1	33	EL 940' MOISTURE SEPARATOR ROOM	IS1-40 SINGLE STREAM
						- Company					
				- 1							

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NORTHERN STATES POWER (D. MONTICELLO UNIT 1

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE		2.3	
PAGE	1	OF	1

MAJOR ITEM: PUMPS

SITE	CATE- GORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF LIEM TO BE EXAMINED	NDE METHODS	TOTAL ITHMS	ACCES- IBLE ITHMS	40 YR. AMOUNT	10 YR. AMOUNT	THEED PERIOD AMOUNT	TE 'RD PERIOD PERCENT	LOCATION	REMARKS
63.1	C-G	PUMPS		REMARKS			-				THERE ARE NO ITEMS
C3.1	C-F	PUMP CASING WELDS		REMARKS		-	-	-	-		WITH SEAMED CASINGS,
63,2	6-9	PRESSURE RETAINING BOLTING									
		HIGH PRESSURE COOLANT INJECTION									ISI-32 AND ISI-33 RELIEF REQUEST NO. 24
	C-D	HPCI PUMP TURBINE CASING	V	REMARKS	-	100% PER INTERVAL	20	20	100	EL 906 HPCI PUMP ROOM	BOLTING/STUDS EX- CEEDING 1" DIAMETER
			UT	-	-	10% PER INTERVAL	2 (MIN)		-		-TOTALS- AS REQUIRED ON PUMP TURBINE CASING -
(3.3	C-E-I	INTEGRALLY WELDED SUPPORTS		REMARKS							THERE ARE NO ITEMS UNDER C3.3 - ALL WELDED SUPPORTS AT C2.5
£3.4	C-12	SUPPORT COMPONENTS		REMARKS					8		SUPPORT COMPONENTS UNDER C2.6
	- 1										

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NORTHERN STATES POWER CO. NORTHEELLO UNIT I

TEN YEAR INTERVAL INSPECTION SUMMARY

TABLE 2.4

PAGE 1 OF 1

MAJOR ITEM: VALVES

SUB THEM	EXAM CATE- CORY	COMPONENT OR SYSTEM, AND DESCRIPTION OF ITEM TO BE EXAMINED	NDE METHODS	TUTAL ITEMS	ACCES- IBLE ITEMS	40 YR. AMOUNT	10 YR.	THIRD PERIOD AMOUNT	THIRD PERIOD PERCENT	LOCATION	REMARKS
€6.1	€+G	VALVES	-	REMARKS	-		-	-	-	7	THERE ARE NO ITEMS
64.1	C-P	VALVE BODY WELDS		REMARKS	417	-	-	-	- 1		WITH SEAMED
C4.2	G=D	PRESSURE-RETAINING BOLTING									RELIEF REQUEST NO. 24 * VALVE BOLTING SCHEDULED BY VALVE RATHER THAN BOLT AMOUNT.
		MAIN STEAM	-	REMARKS	-	-	-	-	-		OUT OF CLASS 2 BOUNDARY
		STOP VALVE A	V	1	1	100% PER INTERVAL	1	1 1	100	MOISTURE SEPERATOR ROOM	MULTIPLE STREAM
		PSI-18"ED	P.E.					1	-	EL 938' SV-1	ISI-26
		STOP VALVE B	V	1	1			-	-	EL 938' SV-2	IS1-27
	17. 1	PS2-18"ED	UT			10 % PER INTERVAL	1	1	10		
		STOP VALVE C PS3-18"ED	n. A	1	1	LIVIENVAL				EL 938' SV-3	ISI-28
		STOP VALVE D PS4-18"ED	V.		1					EL 938' SV-4	ISI-29
		BYPASS				100% PER					
		CONTROL VALVE - 11	V			INTERVAL	1	1	100	EL 940' No.11	ISI-30
		CONTROL VALVE - 12	nı	1	1	10 % PER INTERVAL				EL 940' NO.12	
64.3	C-E-I	INTEGRALLY WELDED SUPPORTS		REMARKS					-		ALL WELDED SUPPORTS AT C2.5
C4.4	C-E-7	SUPPORT COMPONENTS	12.	REMARKS							SUPPORTS AT C2.5
	PE 1										
	W. 3			300							
								1			
	1										
	260							1			
								-			

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ASME Section XI Nondestructive Examination Program - Class 3

ASME Code Edition and Addenda: 1974 Edition through and including Summer 1975 Addenda

Program Period: February 28, 1978 to June 30, 1981 (Third Inspection Period)

NOTES:

- The classification diagrams* identify the systems that are required for examination in accordance with IWD-2000.
 During period one and period two, these examinations were not required, and no effort will be made to retrofit these examinations.
- 2. The scope of the inspection program for Class 3 components is based on the classification of the plant's inspection boundaries and exemptions as allowed for in IWD-2600 and IWD-5200. The inspection program will confort to IWD-2400 (Inspection Schedule), and will begin with period three of the first inspection interval.
- 3. Visual examination will be conducted for evidence of component leakage, structural distress, or corrosion when the system is undergoing either a system inservice test, component functional test, or a system pressure test.
- 4. Supports and hangers for components will be visually examined to detect any loss of support capability or evidence of inadequate restraint.
- 5. Repairs will be performed in accordance with the applicable requirements of the latest edition and addenda of the ASME Code, Section XI. However, if rules for a particular repair are not specified in Section XI, the original design specification and Construction Code of the component or system, or later editions of the Construction Code or ASME Code Section III, either in their encirety or portions thereof, may be used.

LEGEND

Inspection Period

ONE - June 30, 1971 to October 30, 1974 TWO - October 30, 1974 to February 28, 1978

TWDEF - February 28 1978 to Tune 30 1981

THREE - February 28, 1978 to June 30, 1981

^{*} Classification diagrams are included in Section 6 of this report.

ASME Section XI Pressure Testing Program

ASME Code Edition and Addenda: 1974 Edition through and including Summer 1975 Addenda.

Program Period: February 28, 1978 to June 30, 1981

The system Quality Group boundaries are shown on the figures in Section 6. These figures do not include small instrument, leak test, vent and drain lines.

APPLICABLE ASME CODE CLASS	TEST TYPE	TEST FREQUENCY	REQUEST FOR RELIEF
	Leakage	Refueling	30
1	Hydrostatic	10 years	30,36,38
2	Pressure	i0 years	30,31,36, 37,38
3	Pressure	10 years	30,36,37

SECTION 3 INSERVICE TESTING OF PUMPS AND VALVES

- A. Applicable ASME Code Edition and Addenda: 1974 Edition through and including Summer 1975 Addenda
- B. Program Period: October 28, 1979 to June 30, 1981

Key for 3.C Pump Testing Table

M = Monthly

NR = Not required (constant speed drive or fixed resistance system)

NA = Not applicable (sealed bearings)

RR = See request for relief

Key for 3.D Valve Testing Table

Q = Quarterly

NR = Not Required

RR = See request for relief

CSIQ = Cold Shutdown, not more often than quarterly.

IWV-3510 = In accordance with the requirements of

paragraph IWV-3510.

IWV-3610 = In accordance with the requirements of paragraph IWV-3610.

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Pump Description	ASME Code Class		7	est	Para	amet	er		Requests for Relief
		N	Pi	ΔΡ	Q	V	L/F	Tb	
11 Emergency Service Water	3	NR	RR	RR	RR	M	NA	RR	2 3 27
12 Emergency Service Water	3	NR		RR	PR	M		RR	2, 3, 27 2, 3, 27
11 Standby Liquid Control	2	NR	M	M	M	M	T	RR	7 3
12 Standby Liquid Control	2	NR	M	M	M	M	M	RR	7 3
Il Core Spray	2	NR	M	M	M	M	NA	RR	7 3
12 Core Spray	2	NR	M	M	M	M	NA	RR	2 3
ll Residual Heat Removal	2	NR	M	M	M	M	NA	RR	3 3
12 Residual Heat Removal	2	MR	M	M	M	M	NA	RR	3, 3
13 Residual Heat Removal	2	NE	M	M	M	M	NA	RR	2 3
14 Residual Heat Removal	2	NR	M	M	M	M	NA	RR	2 3
11 RHR Service Water	3	NR	RR	RA	M	M	NA	RR	1 2 3
12 RMR Service Water	3	NR	RR	RR	M	M	NA	PR	1 2 3
13 RIR Service Water	3	NR	RR	RR	M	M	NA	RR	1, 2, 3
14 RHR Service Water	3	NR	RR	RR	M	M	NA	RR	1 2 3
figh Pressure Coolant Injection	2	M	M	M	M	M	M	RR	2 3
Reactor Core Isolation Cooling	2	M	M	M	M	M	M	RR	57 7

System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
Main Steam	AO 2-80A	80-A	Main Steam Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	AO 2-80B	80-B	Main Steam Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	AO 2-80C	80-C	Main Steam Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	AO 2-80D	80-D	Main Steam Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	AO 2-86A	86-A	Main Steam Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	AO 2-86B	86-B	Main Steam Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	AO 2-86C	86-C	Main Steam Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	AO 2-86D	86-D	Main Steam Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	MO-2373	74	Steamline Drain Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	MO-2374	77	Steamline Drain Isolation	1	A	Q	Full Stroke-Time	28
Main Steam	RV-2-71A	RV-71-A	Main Steam Safety Relief	1	С	IWV-3510	Setpoint	
Main Steam	RV-2-71B	RV-71-B	Main Steam Safety Relief	1	C	IWV-3510	Setpoint	
Main Steam	RV-2-71C	RV-71-C	Main Steam Safety Relief	1	С	IWV-3510	Setpoint	
Main Steam Main	RV-2-71D	RV-71-D	Main Steam Safety Relief	1	С	IWV-3510	Setpoint	
Steam	RV-2-71E	None	Main Steam Safety Relief	1	С	1WV-3510	Setpoint	
Main Steam	RV-2-71F	None	Main Steam Safety Relief	1	C	IWV-3510	Setpoint	
Main Steam	RV-2-71G	None	Main Steam Safety Relief	1	С	IWV-3510	Setpoint	
Main Steam	RV-2-71H	None	Main Steam Safety Relief	1	C	IWV-3510	Setpoint	

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System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
FW	FW 91-1	27B	FW Inlet Check Valve	2	С	RR	RR	7
FW	FW 91-2	27A	FW Inlet Check Valve	2	С	RR	RR	7
FW	FW 94-1	96B	Outboard Isolation	1	A, C	RR	RR	8
FW	FW 94-2	96A	Outboard Isolation	1	А, С	RR	RR	8
FW	FW 97-1	28B	Inboard Isolation	1	A, C	RR	PR	8
FW	FW 97-2	28A	Inboard Isolation	1	A, C	RR	RR	8
FW	FW 98-1	29B	Feedwater Block Valve	1	Е	NR	Valve Lineup	
FW	FW 98-2	29A	Feedwater Block Valve	1	E	NR	Valve Lineup	
Recirc	CV-2790	39	Rx Water Sample Isolatio	n 2	A	Q	Full Stroke-Tin	e 10, 28
Recirc	CV-2791	40	Rx Water Sample Isolatio	n 2	A	Q	Full Stroke-Tim	e 10, 28
Recirc	MO-2-43A	43A	Recirc Suction	1	В	CSIQ	Full Stroke-Tin	e 28
Recirc	MO-2-43B	43B	Recirc Suction	1	В	CSIQ	Full Stroke-Tin	e 28
Recirc	MO-2-53A	53A	Recirc Discharge	1	В	CSIQ	Full Stroke-Tin	e 28
Recirc	MO-2-53B	53B	Recirc Discharge	1	В	CSIQ	Full Stroke-Tin	e 28
Recirc	MO-2-54A	54A	Recirc Disch. Bypass	1	В	Q	Full Stroke-Tin	e 28
Recirc	MO-2-541	54B	Recirc Disch. Bypass	1	В	Q	Full Stroke-Tim	e 28
Recirc	MO-2-65A	65B	Recirc Loop Crosstie	1	В	CSIQ	Full Stroke-Tin	e 28
Recirc	M)-2-65B	65A	Recirc Loop Crosstie	1	В	CSIQ	Full Stroke-Ti,	. 28

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Total and section of the section of	System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
-	Recirc	MO-2-66A	66B	Recirc Crosstie Bypass	1	В	CSIQ	Full Stroke Tim	e 28
	Recirc	MO-2-66B	66.4	Recirc Crosstie Bypass	1	В	CSIQ	Full Stroke-Tim	e 28
	Recirc		None	Block Valve on Upper Seal Leakoff	2	В	RR	Full Stroke-Tim	e 5,28
	Recirc		None	Block Valve on Upper Seal Leakoff	2	В	RR	Full Stroke-Tim	e 5,28
-	RHR	RV-1990	72A	Pump Suction Relief	2	С	IWV-3510	Setpoint	
	RIR	RV-1991	72B	Pump Suction Relief	2	С	IWV-3510	Setpoint	
	RIR	RV-1992	72C	Pump Suction Relief	2	C	IWV-3510	Setpoint	
	RHR	RV-1993	72D	Pump Suction Relief	2	С	IW-3510	Setpoint	
	RHR	RV-2004	35A	Pump Disck Relief	2	С	IWV-3510	Setpoint	TE
	RHR	RV-2005	35B	Pump Disch Relief	2	С	IWV-3510	Setpoint	
	RUR		None	Hx Shell Side Relief	2	С	IWV-3510	Setpoint	
	RHR		None	Hx Shell Side Relief	2	С	IWV-3510	Setpoint	
	RHR	AO-10-46	AO-46A	LPCI Loop Check	1	A, C	CSIQ	Exercise	
	RIR	AO-10-46	3 AO-46B	LPCI Loop Check	1	A, C	CSIQ	Exercise	
70		RHR-2-1	48A	NER Pump Discharge Check	2	C	Q	Exercise	Public 1
evis	RIR	RHR-2-2	48B	RHR Pump Discharge Check	2	C	Q	Exercise	
ion	RIR RIR	RHR-7-7	480	RHR Pump Discharge Check	2	С	Q	Exercise	
2	RIR	RHR-2-4	48D	RER Pump Discharge Check	2	С	Q	Exercise	

System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
RHR	RHR-21	29	Rx Head Clg Check	The state of the s	С	RR	RR	7
RHR	RFR-8-1	19A	RHR Min Flow Check	2	С	RR	RR	7
RHR	MO-1986	MO-13A	Torus Suction	2	Е	NR	Valve Lineup	
RHR	MO-1987	MO-13B	Torus Suction	2	Е	NR	Valve Lineup	
RHR	MO-1988	MO-15A	Shutdown Clg Suction	2	В	CSIQ	Full Stroke-Tim	e 28
RHR	MO-1989	MO-15B	Shutdown Clg Suction	2	В	CSIQ	Full Stroke-Tim	e 28
RHR	MO-2002	MO-65A	Hx Bypass	2	Е	NR	Valve Lineup	
RHR	MO-2003	MO-65B	Hx Bypass	2	Е	NR	Valve Li	
RIR	MO-2006	MO-39A	Disch to Torus	2	A	Q	Full St c'e-Tim	28
RHR	MO-2007	MO-39B	Disch to Torus	2	A	Q	Full Strok - Tam	e 28
RifR	MO-2008	MO-34A	Torus Clg Inlet	2	A	Q	Full Stroke-Tim	e 28
RHR	MO-2009	MO-34B	Torus Clg Inlet	2	A	Q	Full Stroke-Tim	28
RHR	MO-2010	MO-38A	Torus Spray	2	A	Q	Full Stroke-Tim	28
RHR	MO-2011	MO-38B	Torus Spray	2	A	Q	Full Stroke-Tim	28
RHR	MO-2012	MO-27A	LPCI Injection	2	В	Q	Full Stroke-Tim	e 28
RHR	MO-2013	MO-27B	LPCI Injection	2	В	Q	Full Stroke-Tim	28
RHR	MO-2014	MO-25A	LPCI Injection	1	A	Q	Full Stroke-Tim	28
RHR	MO-2015	MO-25B	LPCI Injection	1	A	Q	Full Stroke-Tim	28

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System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
RHR	MO-2020	MO-26A	Cont Spray Outboard Isolation	2	A	Q	Full Stroke-Tim	e 28
RHR	MO-2021	MO-26B	Cont Spray Outboard Isolation	2	A	Q	Full Stroke-Tim	e 28
RHR	MO-2022	MO-31A	Cont Spray Inner Isolation	2	A	Q	Full Stroke-Tim	e 28
RHR	MO-2023	MO-31B	Cont Spray Inner Isolation	2	A	Q	Full Stroke-Tim	e 28
RIR	MO-2026	MO-33	Head Spray Isolation	1	A	CSIQ	Full Stroke-Tim	e 28
RHR	MO-2027	MO-32	Head Spray Isolation	1	A	CSIQ	Full Stroke-Tim	e 28
RHR	MO-2029	MO-18	Shutdown Clg Isolation	1	A	CSIQ	Full Stroke-Tim	e 28
RIR	MO-2030	MO-17	Shutdown Clg Isolation	1	A	CSIQ	Full Stroke-Tim	e 28
RHR	MO-2033	MO-20	RIR Loop Crosstie	2	E	NR	Valve Lineup	
RHR	MO-2032	MO-57	Disch to Waste Surge	2	В	Q	Full Stroke-Tim	e 28
RHR	CV-1994	CV-153A	RHR Pump Min Flow	2	В	Q	Full Stroke-Tim	e 28
RHR	CV-1995	CV-153B	RHR Pump Min Flow	2	В	Q	Full Stroke-Tim	e 28
RHR	CV-1996	CV-153C	RHR Pump Min Flow	2	В	Q	Full Stroke-Tim	e 28
RHR	CV-1997	CV-153D	RHR Pump Min Flow	2	P	Q	Full Stroke-Tir	e 28
RHR	RV-2025	44	Head Spray Line Relief	2	C	1WV-3510	Setpoint	
RIR	RHR-8-2	19B	RMR Min Flow Check	2	С	RR	RR	7
RFR	RHR-SW-1	7 182	SW Imerg Supply to RIR	2	C	RR	KR .	11
PIR	RV-2031	40	RER Shutdown Clg Relief	2	<u></u>	TWV-3510	Setpoint	

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System	Valv. Number	FSAR Valve	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
RHR	RHR-6-1	81A	RIR Loop Block	1	E	NR	Valve Lineup	
RHR	RHR-6-2	81B	RHR Loop Block	1	E	NR	Valve Lineup	
RHR	RHR-1-1	152A	RHR Pump Suction Block	2	E	NR	Valve Lineup	
RHR	RHR-1-2	152B	RHR Pump Suction Block	2	E	NR	Valve Lineup	
RHR	RHR-1-3	152C	RHR Pump Suction Block	2	E	NR	Valve Lineup	
RHR	RHR-1-4	152D	RHR Pump Suction Block	2	Е	NR	Valve Lineup	
RIP	RHR-3-1	47A	RHR Pump Disch Block	2	E	NR	Valve Lineup	
RHR	RHR-3-2	47B	RIR Pump Disch Block	2	E	NR	Valve Lineup	
RHR	RHR-3-3	47C	RHR Pump Disch Block	2	E	NR	Valve Lineup	
RHR	RHR-3-4	47D	RHR Pump Disch Block	2	Е	NR	Valve Lineup	
KHR	RHR-18-1	30A	CST to RIR Block	2	E	NR	Valve Lineup	
RHR	RHR-18-2	30B	CST to RIR Block	2	Е	NR	Valve Lineup	
Core	AO-14-13A	AO-13A	Loop Inj. Check	1	Α, σ	CSIQ	Exercise	
Core	AO-14-13B		Loop Inj. Check	1	A, C	CSIQ	Exercise	
Spray Core Spray	MO-1753	MO-12A	Core Spray Injection	1	A	Q	Full Stroke-Tim	28
Spray Core Spray	MO-1754	MO-12B	Core Spray Injection	1	A	Q	Ful! Stroke-Tim	e 28
Core Spray	MO-1751	MO-11A	Core Spray Injection	2	B	Q	Full Stroke Tim	28
Core Spray	MO-1752	MO-11B	Core Spray Injection	2	В	Q	Full Stroke-Tim	e 28

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System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
ore prav	RV-1745	20A	Disch Line Relief	2	С	IW-3510	Setpoint	
ore pray	RV-1746	20B	Disch Line Relief	2	C	IWV-3510	Setpoint	
ore pray	CS-9-1	10A	Pump Disch Check	2	С	Q	Exercise	
ore	CS-9-2	10B	Pump Disch Check	2	С	Q	Exercise	
ore	MO-1741	7A	Core Spray Suction	2	В	Q	Full Stroke-Tim	28
lore pray	MO-1742	7B	Core spray Suction	2	В	Q	Full Stroke-Tim	28
lore Spr pray	CS-10-1	18A	Min Flow Block	2	Е	NR	Valve Lineup	
ore	CS-10-2	18B	Min Flow Block	2	Е	NR	Valve Lineup	
lore	MO-1749	MO-26A	Test Line to Torus	2	В	Q	Full Stroke-Tim	28
ore	MO-1750	MO-26B	Test Line to Torus	2	В	Q	Full Stroke-Tim	28
ore	CS-1-1	32A	Torus Suction Block	2	Е	NR	Valve Lineup	
ore	CS-1-2	32B	Torus Suction Block	2	Е	NR	Valve Lineup	
ore	CS-13-1	14A	Core Spray Block	1	Е	NR	Valve Lineup	
Core	CS-13-2	14B	Core Spray Block	1	E	NR	Valve Lineup	HEIZH
Core Spray	CS-3-1	8A	CST Suction Block	2	Е	NR	Valve Lineup	
lore Spray	CS-3-2	8B	CST Suction Block	2	E	NR	Valve Lineup	
IPCI I	RV-205€	66	Relief Valve	3	С	IW-3510	Setpoint	胡油艺
IPCI	HPCI-18	130	Clg Water Return Check	3	С	Q	Exercise	

	TEMPOR TO STANDARD TO THE	THE COLUMN	MILESTER CONTRACTOR OF THE					
	HPCI	MO-2068	MO-19	Pump Discharge Isol	2	В	Q	Full Stroke Time
	HPCI	AO-23-18	AO-18	Clg Wtr Disch Check	2	С	CSIQ	Exercise
	HPCI	MO-2071	MO-21	Test return to CST	2	В	Q	Full Stroke-Time
	HPCI	MO-2067	MD-20	Coolant Pump Disch.	2	В	Ç	Full Stroke-Time
	HPCI	CV-2065	41	Min Flow Bypass	2	В	Q	Full Stroke-Time
	HPCI	HPCI-42	62	Min Flow Bypass Check	9	c	RR	RR
	HPCI	RV-2064	34	Relief Valve	2	C	IWV-551	Setpoint
4	HPCI	HPCI-32	32	CST Suction Check	2	С	Q	Exercise
Ö	IPCI	MO-2063	MO-17	CST Suction	2	В	Q	Full Stroke Time
	HPCI	MO-2062	MO-57	Torus Suction	2	В	Q	Full Stroke-Time
	IPCI	HPCI-31	61	Torus Suction Check	2	С	RR	RR
	IFCI	MO-2061	MO-58	Torus Suction	2	В	Q	Full Stroke-Time
	HPCI	HPCI-33	33	Pump Suction Block	2	E .	NR	Valve Lineup
7.8	Inci	MO-2034	MO-15	Steam Supply Isolation	1	A	Q	Full Stroke-Time
7/27/79	HECI	MO-2035	MO-16	Steam Outboard Isolation	1		0	Full Stroke-Time
20.00		MO-2036	MO-14	Turbine Steam Supply	2	F .	Q	Full Stroke Time
	HPCI	HX)-7	HO	Turbine Stop Valve	2	P	Q	Full Stroke
	HPCI	110-8	110	Turbine Control Valve	2	8	Q	Full Stroke-Time

Applicable ASME Valve Code Class Catego

Test

Frequency

Category

Test

Request

For Relief

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FSAR

No.

Valve

Description

Valve

Number

System

	System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
	HPCI	PCV-3492	PCV-50	Cooling Water Supply Cont.	2	В	RR	RR	
	HPCI	HPCI-20	131	Cooling Water Return Check	2	С	Q	Exercise	
	IPCI	HPCI-14	56	Ex. Line Drain Pot Check	2	A, C	RR	RR	7
	HPCI	HPCI-15	45	Ex. Line Drain Pot Check	2	С	RR	RR	7
	HPCI	HPCI-9	65	Turbine Ex. Line Check	2	А, С	Q	Exercise	
	HPCI	HPCI-10	12	Ex. Line Stop Check	2	С	Q	Exercise	
	HPCI	HPCI-65	None	Vac. Bkr Check	2	С	RR	RR	7
3-11	HPCI	HPCI-71	None	Vac. Bkr Check	2	С	RR	RR	7
+	HPCI	PSD-2038	None	Ex. Line Rupture Disc	2	D	NR		
	RCIC	MO-2096	MO-2096	Cooling Nater to Cond.	2	В	Q	Full Stroke-Time	28
	RCIC	RV-2097	RV-2097	Relief Valve	3	С	IW-3510	Setpoint	
14.	RCIC	RCIC-14	None	Condenser Cond Pump Disc	2	С	Q	Exercise	
Rev 1/5	RCIC	RCIC-17	None	Vac Pump Disch Check	2	С	RR	RR	7
79	RCIC	RCIC-9	None	Turbine Exhaust Check	2	A,C	Q	Exercise	
on 2	RCIC	RCIC-10	None	Steam Exh Stop Check	2	С	Q	Exercise	
	RCIC	RCIC-57	None	Vac Brkr Check	2	С	RR	RR	7
	RCIC	RCIC-59	None	Vac Brkr Check	2	С	RR	RR	7
	RCIC	PSD-2089	PSD-2089	Rupture Disc	2	D	NR		

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System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
RCIC	MO-2075	MO-2075	Steam Supply Isolation	1	A	Q	Full Stroke-Time	28
PCIC	MO-2076	MO-2076	Steam Supply Isolation	·	A A	Q	Full Stroke-Time	28
RCIC	MD-2078	MO-2078	Steam Supply to Turbine	2	В	Q	Full Stroke-Time	28
PCIC	RCIC-7	None	Throttle Trip Valve	2	В	Q	Full Stroke	10
RCIC	HO	Nene	RCIC Governing	2	· B	RR	RR	
RCIC	PCV-2092	PCV-2092	Condenser Press Cont	2	В	RR	RR	
RCIC	RCIC-16	None	Vac Pump Disch Check	2	A, C	RR	RR	7
RCIC	MO-2100	MO-2100	Inboard Torus Suction	2	В	Q	Full Stroke-Time	28
ncic	RCIC-31	None	Check Valve to Torus	2	С	PR	RR	7
PCIC	MO-2101	MO-2101	Outboard Torus Suction	2	В	Q	Full Stroke-Time	28
PCIC	RCIC-41	None	Check Valve to CST	2	C	Q	Exercise	
RCIC	MO-2102	MO-2102	CST Suction	2	В	-0	Full Stroke-Time	28
RCIC	RV-2103	RV-2103	RCIC Section Line Relief	2	C -	IWV-351	Setpoint	
RCIC	CV-2104	CV-2104	Min Flow Bypass	2	B	Q	Full Stroke-Time	28
RCTC	RCIC-37	None	Min Flow Bypass Check	2	0	RR	RP	107 44
RCTC	MO-2106	MO-2106	Pump Discharge	2	B - 1	Q	Full Stroke-Time	28
RCIC	MO-2107	MO-2107	Pump Discharge	2	В .	Q	Full Stroke-Time	28
RCIC	AO-13-23	AO-13-22	Pump Disch Check	2	C.	CSIQ	Exercise	

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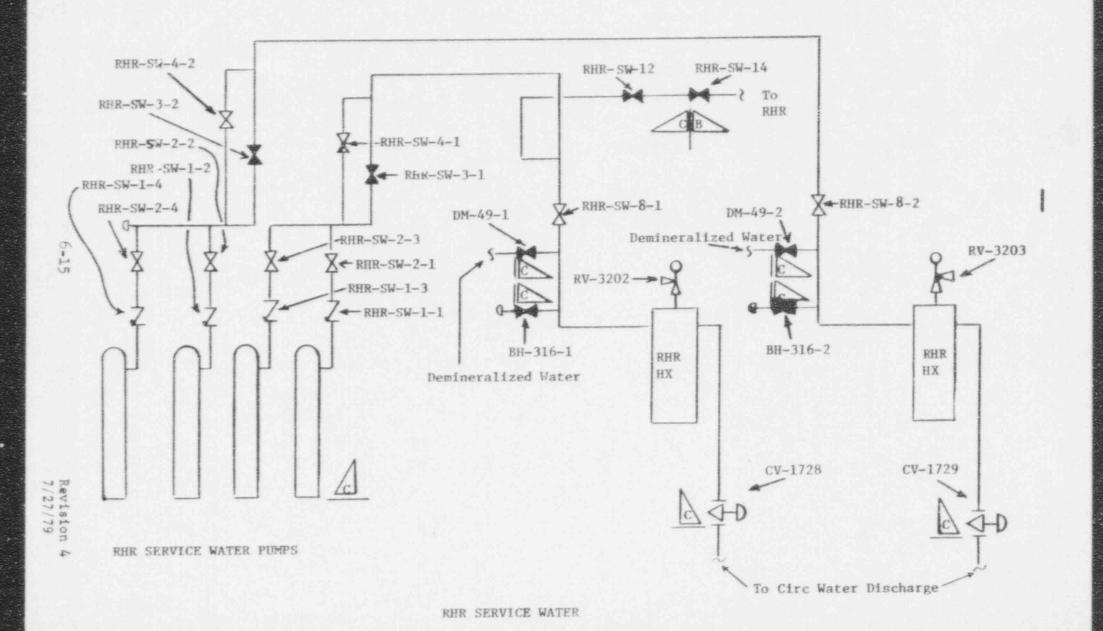
System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
RCIC	MO-2110	MO-2110	Test Return to Cond Stor	2	В	Q	Full Stroke-Time	28
RCIC	RCIC-32	None	Pump Suction Block	2	E	NR	Valve Lineup	
SBLC	XP-3-1	43A	Pump Disch Check	2	С	Q	Exercise	
SBLC	XP-3-2	43B	Pump Disch Check	2	С	Q	Exercise	
SBLC	XP-6	16	Outboard Isolation Check	1	A, C	RR	RR	13
SBLC	XP-7	17	Inboard Isolation Check	1	A, C	RR	RR	13
SBLC	RV-11-39A	39A	Relief Valve	2	С	IW-3510	Setpoint	
SBLC	RV-11-39B		Relief Valve	2	С	IW-3510	Setpoint	
SBLC	11-14A	14A	Explosive Actuated Valve	2	D	IWV-3610	Actuation	
SBLC	11-14B	14B	Explosive Actuated Valve	2	D	IWV-3610	Actuation	
SBLC	XP-17	41	Suction from Test Tank	2	Е	NR	Valve Lineup	
SBLC	XP-20	None	Suction Header Drain	2	Е	NR	Valve Lineup	
SBLC	DM-56	None	Demin Water to Suction	2	Е	NR	Valve Lineup	
SBLC	XP-13	26	Test Line Return	2	E	NR	Valve Lineup	
SBLC	XP-11-1	34	Pump Discharge Drain	2	Е	NR	Valve Lineup	
SBLC	XP-18	None	Poison Tank Drain	2	E	NR	Valve Lineup	
SBLC	XP-1	11	Poison Tank Outlet	2	Е	NR	. '> Lineup	
SBLC	XP-2-1	12A	Pump Suction Block	2	Е	NR	Valve Lineup	

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System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
SBLC	XP-2-2	12B	Pump Suction Block	2	Е	NR	Valve Lineup	
SBLC	XP-4-1	13A	Pump Disch Block	2	Е	NR	Valve Lineup	
SBLC	XP-4-2	13B	Pump Disch Block	2	Е	NR	Valve Lineup	
SRLC	XP-5	15	Injection Header Block	2	Е	NR	Valve Lineup	
SELC	XP-8	18	Injection Header Block	1	Е	NR	Valve Lineup	
CRD	CV-3-32A	CV-32A	Scram Disch Volume Vent	1	В	Q	Full Stroke-Time	28
CRD	CV-3-32B	CV-32B	Scram Disch Volume Vent	1	В	Q	Full Stroke-Time	28
CRD	CV-3-33	CV-33	Scram Disch Volume Drain	1	В	Q	Full Stroke-Time	28
CRD	RV-3-34	34	Scram Disch Volume Relief Valve	2	С	IWV-3510	Setpoint	
CRD	CRD-114	114	Scram Riser Check	2	С	RR	RR	9
CRD	CRD-115	115	Accumulator Charging Water Check	2	С	RR	RR	9
CRD	CRD-138	138	Cooling Water Check	2	С	RR	RR	9
CRD	CV-126	CV-126	Inlet Scram Valve	1	В	RR	RR	9
CRD	CV-127	CV-127	Outlet Scram Valve	2	В	RR	RR	9
RHR SW	CV-1728	CV-1728	RHR SW Control Valve3	3	В	Q	Full Stroke-Time	28
REIR SW	CV-1729	CV-1729	RHR SW Control Valve	3	В	Q	Full Stroke-Time	28
HR SW	RHR-SW 1-1	RHR-SW 1-1	RHR SW Pump Disch Check	3	С	0	Exercise	
UIR SW	RHR-SW 1-2	RHR-SW 1-2	RHR SW Pump Disch Check	3	С	Q	Exercise	

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System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
Emerg								
Serv Wtr Emerg	SW-103	None	E.S.W. Check Valve	1 3		RR	RR	-
Serv Wtr	SW-104	None	E.S.W. Check Valve	3	C	RR	RR	7
Emerg								T. P. L. P.
Serv Wtr	ESW-1-1	ESW-1-1	Promp Check Valve	3	C	Q	Exercise	
Emerg Serv Wtr	ESW-1-2	ESW-1-2	Pump Check Valve	3	C	0	Exercise	
Emerg			Description of the second second					7.17.2
Serv Wtr	SW-16	SW-16	E.S.W. Check Valve	3	C	RR	RR	/
Emerg Serv Wtr	SW-18	SW-18	E.S.W. Check Valve	3	C	RR	RR	7
Emerg								
Serv Wtr	AV-3155	AV-3155	Pump Disch Air Vent	3	C	Q	Exercise	
Emerg Serv Wtr	AV-3156	AV-3156	Pump Disch Air Vent	3	C	0	Exercise	
Emerg Serv Wtr	ESW- 3-1	ESW-3-1	Basket Strainer Bypass	3	Е	NR	Valve Lineup	
Emerg						The state of the s		
Serv Wtr Primary	ESW-3-2	ESW-3-2	Basket Strainer Bypass	3	E	NR	Valve Lineup	
Containm.	AO-2377	None	Cont. Purge Isolation	2	A	Q	Full Stroke-Time	
Primary								
Containm. Primary	AO-2378	None	Torus Purge Isolation	2	A	Q	Full Stroke-Time	28
Containm.	AO-2379	None	Torus Vac Bkr Isolation	2	A	0	Full Stroke-Time	28
Primary								20
Containm.	AO-2380	None	Torus Vac Ekr Isolation	2	A	Q	Full Stroke-Time	28
Primary Containm.	AO-2381	None	Drywell Purge Isolation	2	Α	Q	Full Stroke-Time	28
Primary Containm.	AO-2383	None	Torus Vent Isolation	2	A	0	Full Stroke-Time	28
Primary	NO-2303	NOTIC	10145 Vene 1501ac10n		7	Y	TOTAL DELONG THE	
Containm.	AO-2386	None	Drywell Vent Isolation	2	A	Q	Full Stroke-Time	28
Frimary Containm.	AO-2387	None	Drywell Vent Isolation	2	A	0	Full Stroke-Time	28

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System	Valve Number	Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
Primary	AC. 2004		Town Work Lasterin	1			Full Stroke-Time	28
Containm. Primary	AC-2896	None	Torus Vent Isolation Sec Cont to	6	Α	Q	ruli Stioke-Tune	
Containm.	DWV-8-1	None	Torus Vac Bkr	2	A, C	Q	Exercise	33
Primary Containm.	DWV-8-2	None	Sec Cont to Torus Vac Pkr		A, C	0	Exercise	33
Primary	DMA-0-7	None	TOTUS VAC : NI	4	A, C		LACICISC	
Containm.	CV-7436	None	N ₂ Pumpback Isolation	2	A	RR	RR	12, 28
Primary Containm.	CV-7437	None	N ₂ Pumpback Isolation		A	RR	RR	12, 28
Primary	CV-7437	NONE	Ny Fullipoack Isolacion	6	A	M	Liv.	22, 20
Containm.	CV-2384	None	Torus Vent Isolation	2	A	Q	Full Stroke-Time	28
Primary				THE THE				20
Containm.	CV-2385	None	Drywell Vent Isolation	2	A	Q	Full Stroke-Time	28
Primary Containm	CV-3267	None	Torus N ₂ Makeup Iso.	2	A	Q	Full Stroke-Time	28
Primary								-0
Containm.	CV-3268	None	Drywell N2 Makeup Iso.	2	A	Q	Full Stroke-Time	28
Primary Containm.	CV-3269	None	Cont N ₂ Makeup Iso	2	A	0	Full Stroke-Time	28
Primary			1					
Containm.	CV-3305	None	Drywell O2 Analy Iso	2	A	Q	Full Stroke-Time	28
Primary Containm.	CV-3306	None	Drywell O2 Analy Iso	2	A	0	Full Stroke-Time	28
Primary								- 0
Containm.	CV-3307	None	Drywell O2 Analy Iso	2	A	Q	Full Stroke-Time	28
Primary Containm.	CV-3308	None	Drywell O2 Analy Iso	2	Α	Q	Full Stroke-Time	28
Primary								
Containm.	CV-3309	None	Drywell O2 Analy Iso	2	A	Q	Full Stroke-Time	28
Primary Containm.	CV-3310	None	Drywell Oz Analy Iso	2	A	Q	Full Stroke-Time	28
Primary Containm.	CV-3311	None	Drywell O2 Analy Iso	2	A		Furl Stroke-Time	28
Primary	CV-3311	NOTIC	Diyweil Of Sunity 150				Tull Stroke-1186	20
Centainm.	CV-3312	None	Drywell 02 Analy Iso	2	A	Q	Full Stroke-Time	28

FSAR Valve

System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Te: 1 Frequency	Test	Request For Relief
Primary Containm.	CV-3313	None	Drywell O, Analy Iso	2	A	Q	Full Stroke-Time	28
Primary Containm.	CV-3314	None	Drywell O, Analy Iso	2	A	Q	Full Stroke-Time	28
Primary Containm.	CV-7440	None	Torus to Drywell N2 Iso	2	A	Q	Full Stroke-Time	28
Cond Serv System	DM-58	None	Drywell Demin Wtr Iso	2	А	RR	RR	12
RECCW	MO-1426	MO-1426	Drywell RBCCW Isolation	2 -	Α	CSIQ	Full Stroke-Tim	28
RBCCW	RBCC-15	None	Drywell RECCW Isolation	2	A, C	RR	RR	6
RWCU	MO-2397	MO-2397	Pump Suction Isolation	1	A	Q	Full Stroke-Time	28
RWCU	MO-2398	MG-2398	Pump Suction Isolation	1	A	Q	Full Stroke-Time	28
liquid Radwaste	AO-2541A	None	Drywell Floor Drn Smp Iso	2	HA I	Q	Full Stroke-Time	28
iquid Vadwaste	AO-2541B	None	Drywell Floor Drn Smp Iso	2	A	Q	Full Stroke-Time	28
iquid Nadwaste	AO-2561A	None	Drywell Equip Sump Iso	2	A	Q	Full Stroke-Time	28
iquid Madwaste	AO-2561B	None	Drywell Equip Sump Iso	2	A	Q	Full Stroke-Time	28
uel Pool	PC-20-1	None	Fuel Storage Pool Check	3	С	RR	RR	7
uel Pool lg & Clp	PC-20-2	None	Fuel Storage Pool Check	3	С	RR	RR	7
ir	CV-1478	CV-1478	Drywell Comp Air Iso	2	A	CSIQ	Full Stroke-Time	28
omp ir	CV-7956	None	Torus Inst Air Iso	2	A	Q	Full Stroke-Time	28
omp ir	AS-39	None	Service Air Iso	2	A	RR	RR	12

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System	Valve Number	FSAR Valve Number	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
TIP	TIP 1-1	None	#1 TIP Isolation Ball Valve	2	A	0	Full Stroke	28, 10
115	111 1-1	None	#2 TIP Isolation			- X	Full Stroke	
TIP	TIP 1-2	None	Ball Valve	2	A	Q	Time	28, 10
			#3 TIP Isolation				Full Stroke	20 10
TIP	TIP 1-3	None	Ball Valve	2	A	- Pw	Time	28, 10
	27D 2 1	M	#1 TIP Isolation		D	3610	Actuation	
TIP	TIP 2-1	None	Shear Valve	2	1.7	IRV	ACCUACION	
TIP	TIP 2-2	None	Shear Valve	2	D	3610	Actuation	
111	111 2 2	HONC	#3 TIP Isolat			IW		
TIP	TIP 2-3	None	Shear Valve	2	D	3610	Actuation	
			TIP System					
TIP	TIP 3	None	Purge Check	2	A, C	RR	RR	26
Main						CCTO	Full Stroke Time	28
Steam	FCV-7682	FCV 27	Recombiner Steam Supply	2	В	CS1Q	Full Stroke	20
Main Steam	CV-2369	17	Reactor Head Seal Leak-Off Valve	2	В	0	Time	28
Main	CV-2309	1/	Reactor Head Seal				Full Stroke	
Steam	CV-2370	18	Leak-Off Valve	2	В	Q	Time	28
Main			Reactor Head				Full Stroke	
Steam	CV-2371	20	Vent Valve	2	В	Q	Time	28
Main			Reactor Head				Full Stroke	20
Steam	CV-2372	21	Vent Valve	2	В	Q	Time	28
etir.	RHR-7	16	Crosstie Block	Z	E	NR	Valve Lineup	
EPC I	1PC1-7	None	Pump Cooling Water Block	2	E	NR	Valve Lineup	
IPC1	HPCI-60	None	Turbine Exhaust Vacuum Breaker	2	C	RR	RR	7

	Sy	stem	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
	RX	INST.	X-27A	None	Excess Flow Check Valve	1	А, С	RR	RR	39
	RX	INST.	X-27B	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	RX	INST.	X-27C	None	Excess Flow Check Valve	1	A,C	PR	RR	39
	RX	INST.	X-28A	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	RX	INST.	X-28B	None	Excess Flow Check Valve	1	А, С	RR	RR	39
	RX.	INST.	X-28C	None	Excess Flow Jheck Valve	1	А, С	RR	RR	39
	RX	INST.	X-28D	None	Excess Flow Check Valve	1	А, С	RR	RR	39
5-2	RX	INST.	X-28E	None	Excess Flow Check Valve	1	A,C	RR	RR	39
0	RX.	INST.	X-29A	None	Excess Flow Check Valve	1	А, С	RR	RP	39
	RX	INST.	X-29B	None	Excess Flow Check Valve	1	А, С	RR	RR	39
	RX	INST.	X-29C	None	Excess Flow Check Valve	1	A, 6	RR	RR	39
	RX.	INST.	X-29D	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	RX	INST.	X-31A	None	Excess Flow Check Valve	1	A, C	RR	PR	39
	RX	INST.	X-31B	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	RX	INST.	X-31D	None	Excess Flow Check Valve	1	А, С	RR	RR	39
- 4	RX.	INST.	X-31E	None	Excess Flow Check Valve	1	A, C	RR .	RR	39
	RX	INST.	X-31F	None	Excess Flow Check Valve	1	A, C	RR	RR	39

System	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
RX INST	. X-32A	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	. X-32B	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	. X-32D	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	. X-32E	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	. X-32F	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	. X-33A	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	. X-33B	None	Excess Flow Check Valve	1	А, С	RR	RR	39
RX INST	. X→33C	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	, X-33D	None	Excess Flow Check Valve	1	А, С	RR	RR	39
RX INST	. X-33E	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	. X-33F	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	X-40A-A	None	Excess Flow Check Valve	1	А, С	RR	RR	39
RX INST	. Х-40А-В	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	X-40A-C	None	Excess Flow Check Valve	1	A, C	RP.	ER	39
RX INST	. X-40A-D	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	. X-40A-E	None	Excess Flow Check Valve	1	А, С	RR	RR	39
RX INST	. X-40A-F	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX INST	X-40B-A	None	Excess Flow Check Valve	1	A, C	RR	RR	39

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Sy	rstem	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
RX	INST.	X-40B-B	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	INST.	X-40B-C	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	INST.		None	Excess Flow Check Valve	1	A, C	RR	RR	39
	INST.	X-40B-E	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	INST.	X-40B-F	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	INST.	X-40C-A	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	INST.	X-40C-B	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	INST.	X-40C-C	None	Excess Flow Check Valve	1	A, C	RR	RR	39
	INST.	X-40C-D	None	Excess Flow Check Valve	1	A, C	RR	RR	39
-	INST.	X-40C-E	None	Excess Flow Check Valve	1	A, C	RR	RR	39 -
1	(INST.	X-40C-F	None	Excess Flow Check Valve	1	А, С	RP.	RR	39
-	(INST.	X-40D-A	None	Excess Flow Check Valve	1	A, C	RR	RR	39
-	X INST.	X-40D-B	None	Excess Flow Check Valve	1	A, C	- RR	RR	39
-	X INST.	X-40D-C	None	Excess Flow Check Valve	1	A, C	RR	RR	39
1	INST.	X-40D-D	None	Excess Flow Check Valve	1	A, C	RR	RR	39
1	X INST.	X-40D-E	None	Excess Flow Check Valve	1	A, C	RR	T.R.	39
-	X INST.		None	Excess Flow Check Valve	1	A, C	RR	RR	39

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Sy	stem	Valve Number	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
RX	INST.	X-49A	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-49B	None	Excess Flow Check Valve	1	А, С	RR	RR	39
RX	INST.	X-49C	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-49D	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	IMST.	X-49E	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-49F	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-50A	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-503	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-50C	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-50D	None	Excess Flow Check Valve	1	A, C	RR	RR	39 -
RX	INST.	X-51A	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-51B	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-51C	None	Excess Flow Check Valve	1	A, C -	RR	RR	39
RX	INST.	X-51D	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX.	INST.	X-51E	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-51F	None	Excess Flow Check Valve	1	A, C	RR	RR	39
RX	INST.	X-52A	None	Excess Flow Check Valve	1	A, C	RR	RR	39

	System	Valve Numb	FSAR Valve No.	Description	Applicable ASME Code Class	Valve Category	Test Frequency	Test	Request For Relief
R	X INST.	X-52B	None	Excess Flow Check Valve	1	А, С	RR	RR	39
R	X INST.	X-52C	None	Excess Flow Check Valve	1	А, С	RR	RR	39
R	X INST.	X-52D	None	Excess Flow Check Valve	1	А, С	RR	RR	39
R	X INST.	X-52E	None	Excess Flow Check Valve	1	A, C	RR	RR	39
R	X INST.	X-52F	None	Excess Flow Check Valve	1	А, С	RR	RF.	39
R	X INST.	X-28F	None	Excess Flow Check Valve	2 .	А, С	RR	RR	40
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COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS
, 12, 13, 14 RHR ervice Water Pumps	Provide cooling water to the RHR heat exchangers.	3

Code Requirement

Inlet pressure and differential pressure will not be measured directly as required by IWP-3100 and IWP-4213.

Rasis

There is no installed instrumentation for directly measuring the inlet pressure and differential pressure of these pumps. These pumps are submerged and take suction several feet below the river level.

Alternate Testing

The river level elevation will be measured to determine the inlet pressure for these pumps. Differential pressure will be determined by taking the difference between the discharge pressure and calculated inlet pressure.

Scheduled for Implementation

2. Request for Relief

COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS
11, 12 Emergency Service Water	Provide cooling water to the emergency diesel generators and critical reactor building equipment.	3
11, 12 Standby Liquid Control	Provide a redundant means of reactor shutdown as a backup to the Control Rod Drive System.	2
11, 12 Core Spray	Provide cooling water to the reactor under emergency conditions.	2
11, 12, 13, 14 Residual Heat Removal	Provide cooling water to the reactor and to containment under accident conditions.	2
11, 12, 13, 14 RHR Service Water	Provide cooling water to the RHR heat exchangers.	3
High Pressure Coolant Injection	Provide cooling water to the reactor under emergency conditions.	2
Reactor Core Isolation Cooling	Provide cooling water to the reactor under emergency conditions.	2

Code Requirement

Pump bearing temperature will not be measured as required by IWP-3100 and IWP-4310.

Basis

There is no instrumentation installed to measure lube oil or bearing temperature. The use of external temperature measuring devices is not considered meaningful because of the environmental influence on these parameters.

2. REQUEST FOR RELIEF (Cont'd.)

Alternate Testing

The mechanical condition of the pump will be assessed by using vibration data.

Schedule for Implementation

COMPONENT	FUNCTION	APPLICABLE CODE CLASS
11, 12 Emergency Service Water Pumps	Provide cooling water to the emergency diesel generators and critical reactor building equipment.	3
11, 12 Standby Liquid Control Pumps	Provide a redundant means of reactor shutdown as a backup to the Control Rod Drive System.	2
11, 12 Core Spray Pumps	Provide cooling water to the reactor under emergency conditions.	• 2
11, 12, 13, 14 Residual Heat Removal Pumps	Provide cooling water to the reactor and to containment under accident conditions.	2
11, 12, 13, 14 RHR Service Water Pumps	Provide cooling water to the RHR heat exchangers.	3
High Pressure Cooling Injection	Provide cooling water to the reactor under emergency conditions.	2
Reactor Core Isolation Cooling	Provide cooling water to the reactor under emergency conditions.	2

Code Requirement

Displacement vibration amplitude will not be used to evaluate the condition of the pump as required by IWP-3110, 3210, 4500, 4510.

Basis

We prefer to measure vibration velocity due to its superiority in detecting wear and interior machine failure. Existing instrumentation reads out in velocity units.

Alternate Testing

Vibration velocity measurements will be used to evaluate the condition of the pump.

Schedule for Implementation

Deleted

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Component	Function	Applicable ASME Code Class	Valve Category
	Shutoff Recirc Pump #11 Upper Seal Flow When Pump is Shutdown	2	В
	Sutoff Recirc Pump #12 Upper Seal Flow When Pump is Shutdown	2	P

Code Requirement

These valves cannot be tested at the frequency required by IW-3410.

Basis

These valves are located inside primary containment which has an inerted atmosphere. The only way to verify valve stroke and measure stroke time is by direct observation of the valve stem.

Alternate Testing

These valves will be full stroked and timed during each refueling outage when the Containment is de-inerted and open for general access.

Schedule for Implementation

6. Request for Relief

Component	Function	Applicable ASME Code Class	Valve Category
RBCC-15	To provide containment isolation for the Reac or Building Closed Cooling water drywell inlet line.	2	A, C

Code Requirement

This valve will not be exercised as required by IW-3520.

Basis

There are no means provided for determining that the disc travels to the seat promptly on cessation or reversal of flow.

Alternate Testing

This line will be modified upon concurrence of the NRC to allow leak testing of this valve (see letter from L. O. Mayer to Victor Stello, subject, "Planned Modifications to Permit Testing to be Conducted in Accordance with 10CFR50, Appendix J", dated May 5, 1976). Proper seating of the valve disc will be verified during the leak rate test.

Schedule for Implementation

See Alternate Testing.

Component	Function	Applicable ASME Code class	Valve Category
SW-101	Prevent flow of emergency service water	3	С
SW-102	into the normal service water system when the emergency service water system	3	C
SW-103	is operating.	3	С
SW-104		3	С
ESW-4-1	Prevent reversal of flow into redundant	3	С
ESW-4-2	emergency service water line.	3	С
FW-91-1	Prevent reversal of flow into the	2	С
FW-91-2	feedwater system.	2	C
RHR 8-1	Prevent reversal of flow into RHR	2	С
RHR 8-2	Pump Discharge Line.	2	С
RHR-21	Prevent reversal of flow into Head Cooling line	1	C
HPCI-14	Prevent reversal of flow from	2	С
HPCI-15	Torus into HPCI System.	2	C
HPCI-42		2	C
HPCI-31	Prevent reversal of flow from HPCI System into Torus.	2	С
HPCI-65	Prevent HPCI Exhaust Steam flow to	2	С
HPCI-71	Torus Air Space.	2	C
RCIC-57	Prevent RCIC exhaust steam flow to	2	C
RCIC-59	Torus Air Space.	2	(
RCIC-37	Prevent Reversal of Flow from the	2	C
RCIC-16	Torus Into the RCIC System.	2	С
RCIC-17		2	С
RCIC-31	Prevent Reversal Flow of RCIC Flow to Torus.	2	C

Component	Function	Applicable ASME Code Class	Valve Category
SW-21-1	Prevent Reversal of Normal Cooling	3	С
SW-21-2	Flow Into the Service Water System.	3	С
SW-16	Prevent Reversal of Flow From	3	C
SW-18	Emergency Service Water System Into Service Water System.	3	С
PC-20-1	Prevent siphoning of Water From	3	С
PC-20-2	Fuel Storage Pool Into Fuel Pool Cleanup System.	3	С
HPCI-60	Turbine Steam Exhaust Vac Brkr	2	С

Code Requirement

These valves will not be tested as required by IWV-3520.

Rasis

There is no means available to verify that the disc travels promptly to the seat on cessation or reversal of flow for normally open valves or that the disc moves promptly away from the seat when the closing differential is removed and flow through the valve is initiated for normally closed valves.

Alternate Testing

The systems in which these valves are located will be functionally tested on a periodic basis to demonstrate proper operation.

Schedule For Implementation

NA

Component	Function	Applicable ASME Code Class	Valve Category
FW 94-1	To provide containment isolation for the feedwater injection lines.	1	A, C
FW 94-2		1	A, C
FW 97-1		1	A, C
FW 97-2		1	A, C

Code Requirement

These valves will not be exercised as required by IW-3520.

Rasis

There are three check valves in series in each of the feedwater injection lines. Verification that each valve disc travels to the seat promptly on cessation of flow cannot be completed by observing pressure indications. The valves cannot be directly observed and there is no instrumentation installed to monitor disc position.

Alternate Testing

Proper seating of the valve disc will be verified during the valve leak rate testing.

Schedule for Implementation

Component	Function	Applicable ASME Code Class	Valve Category	
CRD-114	Prevent scram discharge flow from flowing back into the CRD during a scram,	2	С	
CRD-115	Prevent scram accumulator pressure from discharging into CRD accumulator charging water circuit during a scram.	2	С	
CRD-138 Prevent scram accumulator pressure from discharging into CRD cooling water circuit during a scram.		2	С	
CV-126	Provide scram accumulator pressure to the bottom of the control rod drive piston during a scram.	1	В	
CV-127	Exhaust scram discharge water from the top of the control rod drive piston during a scram.	2	В	

Code Requirement

These valves will not be tested as required by IW-3410 and IW-3520.

Basis

The above listed valves are located on each of the 121 hydraulic control units. There is no practical method of testing these valves in accordance with Section XI requirements. There is no instrumentation installed to verify proper seating of the check valves and the control valves operate too rapidly to measure stroke time. Technical Specifications require all control rods to be scram tested once per operating cycle. These valves are all exercised one full cycle during a scram. Proper operation of these valves and the safety function of the control rod drive system are verified by the scram testing.

Alternate Testing

See Basis

Schedule For Implementation

8/28/78

10. REQUEST FOR RELIEF

Component	Function	Applicable ASME Code Class	Valve Category	
HO-7	Immediately stop the steam flow to the HPCI Turbine.	2	В	
RCIC-7	Immediately stop the steam flow to the RCIC Turbine.	2	В	
CV-2790	Drywell Isolation for reactor water sample	2	A	
CV-2791	line from recirculation Loop B.	2	A	
TIP 1-1		2	A	
TIP 1-2	Drywell isolation for TIP System.	2	A	
TIP 1-3		2	A	

Code Requirement

These valves will not be stroke timed as required by IW-3410.

Basis

These valves operate too fast to obtain meaningful stroke time.

Alternate Testing

These valves will be full stroked as required by IW-3410 and proper operation will be verified.

Schedule for Implementation

Component	Function	Applicable ASME Code Class	Valve Category
RHR SW-17	Prevent reversal of flow of RHR water into RHR Service Water System.	2	С

Code Requirement

This valve cannot be exercised as required by IWV-3520,

Basis

Exercising of this valve would require pumping river water into the RHR System.

Alternate Testing

None

Schedule for Implementation

NA

Component	Function	Applicable ASME Code Class	Valve Category
DM-58	Shutoff demineralized water to drywell.	2	А
AS-39	Shutoff service air to drywell.	2	A
CV-7436		2	A
CV-7437	Drywell Isolation for N ₂ pumpback system.	2	A

Code Requirement

These valves will not be tested as required by IW-3410.

Basis

These valves are located in systems or portions of systems that are presently out of service. They will be tested as required by IW-3410(f).

Alternate Testing

See Basis

Schedule For Implementation

May 31, 1978

Component	Function	Applicable ASME Code Class	Valve Category
XP-6	Prevent reversal of flow of reactor	1	A C
XP-7	water into SBLC System.	1	A C

Code Requirement

These valves will not be exercised at the frequency required by IWV-3520.

Basis

Exercising of these valves can only be accomplished by initiation of the SELC System, including actuation of an explosive valve, and pumping to the reactor vessel.

Alternate Testing

These valves will be exercised by initiation of the SBLC System, actuating an explosive valve and pumping demineralized water to the reactor vessel during each refueling outage.

Schedule For Implementation

Deleted Person

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COI	COMPONENT		CODE CLASS TABLE		CATEGORY
REJ	ACTOR VESSEL				
1)	Longitudinal and Circumferential Welds in Core Region	1	1.1	B1.1	B-A
2)		1	1.1	B1.2	B-B
3)	Nozzle-to-Vessel Welds and Inside Radius: Standby Liquid Control CPAD-1	1	1.1	B1.4	B-D

CODE REQUIREMENTS

- and 2) Volumetric examination of 10% of each longitudinal weld and 5% of each circumferential weld will not be performed as required by Exam Category B-A and B-B.
 - 3) Volumetric examination of nozzle-to-vessel weld and inside radius will not be performed as required by Exam Category B-D, however, an attempt will be made to volumetrically examine this weld and the inside radius to the extent possible.

BASIS

The design of the reactor internals and the external biological shield and vessel insulation prevents both internal and external access to these welds. It should be noted that the Monticello reactor vessel was fabricated and subjected to as-built inspection under very demanding specifications. Because the site was inaccessible to a river barge of the capacity necessary to transport a fully assembled vessel, the vessel was assembled at the site from shop-fabricated subassemblies. All requirements of Section III of the ASME Boiler and Pressure Vessel Code, 1965 Edition, including Addenda through Summer 1966, were satisfied just as if the vessel were shop fabricated. In addition, additional requirements more stringent than those required by the Code were applied by General Electric due to the unique circumstances surrounding the vessel fabrication. Refer to Volume VII of the Monticello Final Safety Analysis Report, "Reactor Pressure Vessel Design Seport," for details concerning vessel fabrication and inspection. In addition, it should be noted that based on analysis of the dosimeter removed from the reactor vessel, the maximum neutron fluence level at T/4 of the reactor vessel wall will be only 1.23 x 10¹⁸ not at the end of designed life (40 years). Based on the high quality level established for vessel fabrication and the relative low neutron fluence level at the vessel wall, the inability to examine these welds is not considered to have any significant decrease in safety.

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8/28/78

ALTERNATE

As the result of their inaccessibility, no examinations will be performed on these welds, other than the vessel pressure tests, and in the case of CPAD-1, examination will be to the extent possible.

SCHEDULE FOR IMPLEMENTATION

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COMPONENT	CODE	TABLE	ITEM	CATEGOR:
REACTOR VESSEL				
REACTOR VESSEL 1) Longitudinal and Circumferential Welds in Shell: VLCB-1, VLCB-2, VLBA-1, VLBA-2, and VCBB-4	1	1.1	B1.2	B-B

CODE REQUIREMENT

- 1) Volumetric examination of 10% of each longitudinal weld and 5% of each circumferential weld will not be performed as required by Exam Category B-B.
- 2) Volumetric examination of the vessel stabilizer lugs will not be performed as required by Exam Category B-H.

BASIS

The design of the biological shield and vessel insulation prevents external access to these welds. Internal access is available but surface preparation of the vessel cladding would be required to provide dependable ultrasonic results. Approximately 20 ft2 of cladding would need to be ground to permit the above examinations. Our experience indicates that even after hydro lancing the vessel wall, and the use of a concrete plug over the core and lead blankets on the wall for shielding, we could still expect personnel exposure to be in the 600-700 mr/hr range.

Based on the high quality level of the Monticello vessel and the relatively low neutron fluence level that the vessel wall will see during its service life (refer to Request for Relief No. 15), we do not believe that exposure to personnel is warranted for the preparation and the performance of these examinations. Especially, since there are vessel welds at much higher stress levels (such as the vessel and head flange welds, nozzle welds, and head welds) that are being examined at greater frequenca and, thus, their examination results should provide a sufficient means to measure the maintenance of veskel integrity.

It should also be noted that for the integrally welded stabilizer lugs (Item 2), they are part of a mechanical snubber system for seismic loading and have no support function. Therefore, the examination of these lug welds is probably not within the scope of Section XI inservice inspection requirements.

Revision 8/28/78

16. REQUEST FOR RELIEF (continued)

ALTERNATE

As the result of their inaccessibility, no examinations will be performed on these welds, other than the vessel pressure tests. However, an attempt will be made to examine the lug welds to the extent possible with a surface method.

SCHEDULE FOR IMPLEMENTATION

COMPONENT	CODE	TABLE	ITEM	CATEGOR
VESSEL PENETRATIONS				
Control Rod Drive and Bottom Head Drain	1	1.1	B1.5	B-E

CODE REQUIREMENT

The area surrounding each penetration cannot be visually examined for evidence of leakage during the vessel pressure test as required by Exam Category B-E.

BASIS

The design of the vessel, the biological shield, and vessel insulation prevents access to these areas that are directly adjacent to the vessel penetrations.

ALTERNATE

The areas below these penetrations will be visually examined for evidence of leakage during the vessel pressure test which will have a hold time of 4 hours.

SCHEDULE FOR IMPLEMENTATION

COMPONENT	CIASS	TABLE	ITEM	EXAM CATEGORY
REACTOR VESSEL				
Closure Head Flange Leakage Sensors (Nozzle N-13 and N-14)	1	1.1	B1.5	В-Е

CODE REQUIREMENT

The area surrounding these two penetrations will not be visually examined for evidence of leakage during the vessel pressure test as required by Exam Category B-E.

BASIS

These penetrations never see pressure during either operation or vessel pressure test, unless the vessel flange o-rings leak. Inspection during pressure testing therefore serves no purpose. In addition, the nozzle area alternate

The nozzles will be hydrostatically tested to insure seal integrity at or near the end of the inspection interval.

SCHEDULE FOR IMPLEMENTATION

COMPONENT	CODE	TABLE	ITEM	EXAM CATEGORY
REACTOR VESSEL			11369	
Standby Liquid Control Nozzle-to-Safe End Welds	1	1.1	B1.6	B-F

CODE REQUIREMENT

The ultrasonic examination, and possibly the liquid penetrant examination, cannot be performed for the total weld as required by Exam Category B-E.

BASIS

The design of the biological shield prevents access to the bottom portion of this weld for ultrasonic examination.

ALTERNATE

Effort will be made to ultrasonically examine as much of the weld as physically possible and to liquid penetrant examine the total weld, provided undue radiation exposure will not result to personnel.

SCHEDULE FOR IMPLEMENTATION

COMPONENT	CODE	TABLE	ITEM	EXAM CATEGORY
REACTOR VESSEL				
Closure Head Cladding	1	1.1	B1.13	B-I-1

CODE REQUIREMENT

The liquid penetrant examination of the closure head cladding will not be scheduled as required by Exam Category B-I-1.

BASIS

From our past experience in liquid penetrant examining the Monticello vessel cladding, we have discovered that the roughness of the closure head cladding results in considerable number of nonrelevant indications that required grinding to eliminate any possible masking effects. In addition, to assure success in the detection of tight cracks, the cladding has a need to be ground to eliminate the oxides and crud that develop during service.

The design stress analysis for the Monticello vessel did not take any credit for cladding thickness. The purpose of the cladding was to maintain water quality. It should be noted that many of the new HWR vessel designs have eliminated this cladding, and later editions of ASME Section XI Code has eliminated all requirements for the inspection of the closure head cladding.

ALTERNATE

Visual examination will be performed on the closure head cladding.

SCHEDULE FOR IMPLEMENTATION

COMPONENT	CODE	TABLE	ITEM	EXAM CATEGORY
Reactor Vessel Safe-end Welds	1	1.1	B1.6	B-F
Pipe Weld Inspection	1	1.4	B4.5	В-Ј
	1	1.4	B4.6	B-J
	1	1.4	B4.9	B-K
	1	1.4	B4.1	B-F
	2	2.2.1	C2.1	C-F
	2	2.2.1	C2.1	C-G

CODE REQUIREMENT

The ultrasonic examination method requirements (Appendix I of Section XI and Article 5 of Section V) of the Code Addenda in effect will not be used to govern the ultrasonic examination procedures for the inspection of pipe welds and welds of components fabricated from pipe components.

BASIS

The use of side drill holes (instead of slots) to establish a distance amplitude correction curve (DAC) for pipe weld inspections, as required by Appendix I of Section XI and Article 5 of Section V, results in an excessive instrument gain setting which greatly impairs the inspector's ability to detect and to interprete indications by producing a lower signal-to-noise ratio and reducing the range of useable DAC.

ALTERNATE

The rules of Appendix III, including Supplement 7, of the 1975 Winter and 1976 Summer Addenda to ASME Section XI Code will govern the ultrasonic examination method for the inspection of pipe welds and welds of components fabricated from pipe components.

SCHEDULE FOR IMPLEMENTATION

COMPONENT	CLASS	TABLE	ITEM	EXAM CATEGORY
Piping Socket Welds - Drain lines (REW28-2"-EF and REW29-2"-EF) of recirculation system A & B	1	1.4	B4.8	В-Ј
Valve Bonnet Briting - Valves XR-6-1, XR-7-1, XR-6-2, and XR-7-2	1	1.6	B6.9	B-G-2

CODE REQUIREMENT

The surface examination of the 2" socket welds and the visual examination of the valve bonnet bolting of these two drain lines were not scheduled for examination as required by Exam Category B-J and B-G-2, respectively.

BASIS

These two, 2-inch drain lines are reading in excess of 2R/hr. The location of these lines prevents the use of shighding or distance to provide any significant reduction in radiation exposure to personnel. We have estimated that exposure to inspection and insulating personnel would be in access of 1 man-rem for the excaination of approximately four socket welds and the bolting of four valves.

ALTERNATE

These lines would be examined in accordance with the requirements of Exam Category B-P, upstream from and including their first isolation valve.

SCHEDULE FOR IMPLEMENTATION

COMPONENT	CODE	TABLE	ITEM	EXAM CATEGORY
Non-Welded Piping and Valve Supports	1	1.4	84.10	B-K-2
	2	2.2	C2.6	C-E-2
	2	2.3	C3.4	C-E-2
	2	2.4	C4.4	C-E-2
	3	-	-	IWD-2600

CODE REQUIREMENT

Examination Category B-K-2 and C-E-2 requires all areas of the support component from the piping, valve, and pump attachment to and including the attachment to the supporting structure. Insulation will not be removed for visual examination of these support components.

BASIS

The general radiation background field for the inspection of Class 1 systems located within containment ranges from 30 to 400 mR and the Class 2 systems have permanent type of insulation (insulation not designed for removal and replacement).

It has been our experience that any loss of support capability or inadequate restraint can usually be detected through the inspection of the uninsulated portion of the support and the surrounding insulation. It is our contention that the removal and replacement of insulation for the sole purpose of inspecting Class 1 supports would result in undue radiation exposure to personnel without providing significant increase in safety. The governing Codes and Regulations used in the design and construction of those systems that are now classified as Class 2 and 3 did not require provisions for inspection access for these systems. Thus, it would be an undue burden without compensating increase in safety to require insulation removal for support inspection.

ALTERNATIVE

The insulation will be removed from a supported component for further inspections whenever an abnormality is detected that may have been a result of a loss of support capability or inadequate restraint.

SCHEDULE FOR IMPLEMENTATION

COMPONENT	CODE	TABLE	ITEM	EXAM CATEGORY
Pressure Boundary Bolts and Studs	1	1.5	B5.1	B-G-1 B-G-1
	1	1.5	B5.2	
	2	2.3	C3.2	C-D
	2	2.4	C4.2	C-D

CODE REQUIREMENT

Volumetric examination of bolts/studs will not have a DAC constructed (distance amplitude curve) as described in Article 5, Section V.

BASIS

The technique described in Section V is not as sensitive to detect surface defects as the presently applied technique using the basic back reflection method correlated with "as built/as installed" bolting sketch of the particular item being examined.

ALTERNATE

The items will be ultrasonically examined by longitudinal straight beam, utilizing the response from the back reflection of the bolt or stud being examined, evaluation criteria shall be per section XI, IWB-3000.

SCHEDULE FOR IMPLEMENTATION

All Class 2 Components	pressure retaining	2	
COMPONENT	FUNCTION	ASM Code Class	Vlv

CODE REQUIREMENT

The system pressure tests will not be distributed as required by IWC-2412.

BASIS

Scheduling system pressure tests in this manner is not practical as mechanisms are not available for isolation of the piping systems at the various boundaries created by the NDE exemption criteria. Consequently numerous redundant pressure tests will be performed which are not warranted considering the operational problems (system valve lineups, leak off or over-pressure protection, radiation exposure, generation of waste, etc.) involved. Additionally the majority of these systems are either normally pressurized or pressurized during the performance of a pump or valve functional test such that any system degradation would be immediately known.

ALTERNATE INSPECTION (TESTING)

All components will be pressure tested at or near the end of each inspection interval. This is consistant with proposed revisions (Winter 1976 Addenda) to ASME-XI, Subsection IWC and Section XI Subcommittee interpretation of Class 2 Pressure Test Requirements (attached).

SCHEDULE FOR IMPLEMENTATION



The American Society of Mechanical Engineers

United Engineering Center / 345 E. 47th St., New York, N.Y. 10017 / 212 644-7815

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CE RAWLINS W.R. SMITH, SE

WE SUMERS

The Hartford Steam Boiler Inspection and Insurance Company 56 Prospect Street Hartford, Connecticut 06102

Att: F. T. Duba

Subject: ASME File #BC-76-418

Section X1, Division 1, System Pressure Tests

Dear Mr. Duba:

Your inquiry of February 24, 1976 has been considered by the cognitant committee. We are responding to the following question:

QUESTION:

- 1. Are system leakage tests required for Class 2 and Class 3 systems?
- 2. Are system hydrostatic tests required for Class 2 and 3 systems?

REFLY:

- 1. System leakage tests are not required for Class 2 and 3 components.
- 2. System hydrostatic tests are required for Class 2 and 3 components at or near the end of each inspection interval. In addition, a system hydrostatic test is required on components which have been repaired by welding prior to returning the plant to service.

Very truly yours,

June Ling

Nuclear Engineding Administrator

JL:1c

RECEIVED ENGINETRING

11-3 0 19/6

E. L. KEMMLES "ira Presiden

FUNCTION	CODE CLASS	VALVE CATEGORY
Prevent reversal of flow in TIP purge line.	2	A, C
	Prevent reversal of flow	Prevent reversal of flow 2

Code Requirement

This valve cannot be exercised as required by IW-3520.

Basis

This is a normally open check valve that is in service during all modes of operation. In addition, there is no means available to verify that the disc travels promptly to the seat on cessation or reversal of flow.

Alternate Testing

Proper seating of the valve disc will be verified during the valve leak rate testing.

Schedule for Implementation

COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS
11,12 Emergency Service Water Pumps	Provide cooling water to the emergency diesel generators and critical reactor building equipment.	3

Code Requirement

Pump flowrate will not be measured to determine pump performance as required by IWP-3100.

Basis

There is no installed instrumentation for measuring the flowrate of these pumps. Flowrate varies due to the seasonal variations in cooling requirements m king it impractical to establish a reference value and acceptance criteria for this parameter.

Alternate Testing

The Emergency Service Water pumps will be tested to shutoff pressure. Pump differential pressure will be measured under these conditions.

Schedule for Implementation

January 1, 1979

COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS	VALVE CATEGORY
All power operated valves.		1, 2, 3	А, В

Code Requirement

The acceptance criteria for valve-stroke time as stated in IW-3410c)(3) will not be used.

Basis

Stroke time acceptance criteria outlined in IWV-3410 is general and is not based on system functional requirements and normal valve variability.

Alternate

Acceptance criteria for valve stroke times will be based on normal valve variability and on system functional requirements.

Schedule for Implementation

29. REQUEST FOR RELIEF
Deleted

Revision 2 1/5/79

COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS
All Class 1, 2 and 3 Components	Pressure Retaining	1, 2, 3

Code Requirements

The test pressure requirements of IWA-5000, IWB-5000, IWC-5000 and IWD-5000 will not be met on certain components.

Basis

The code does not recognize that non-isolable junctions of components with different design pressures or different ASME Classes exist (i.e., pump suction and discharge lines, piping upstream and downstream of restricting orifices, etc.). Pressurizing components to the requirements of the code may result in overpressurizing the non-isolable components.

Alternate Testing

Where these junctions exist, test pressure will be based on the component with the lowest test pressure requirement.

Schedule for Implementation

COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS
Head vent and leak test connections on Class 1 piping.	Provide connection for leak testing and for venting the reactor head.	2

Code Requirement

These lines will not be pressure tested in accordance with IMC-5210.

Basis

These lines are connected to Class 1 piping and are classified as Quality Group B lines (applicable ASME Code Class 2) due to line size only. These lines will be tested in accordance with Class 1 requirements (IWB-5000).

Alternate Testing

See Basis

Schedule for Implementation

MIQUEST FOR RELIEF

32.

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Revision 2 1/5/79

32. REQUEST FOR RELIEF
Deleted

Revision 2 1/5/79

Component	Function	Applicable ASME Code Class	Valve Category
DWV-8-1	Secondary containment to torus	2	A, C
DWV-8-2	vacuum breaker.	2	A, C

Code Requirement

These valves will not be exercised as required by IW-3520(b)(2).

Basis

Paragraph IW-3520 of Section XI, 1974 Edition with Addenda through and including Summer, 1975, does not recognize that the mechanical exerciser torque requirements do not apply to vacuum breakers, whereas the 1977 Edition Summer 1977 Addenda does recognize this fact.

Alternate Testing

These valves will be tested in accordance with Paragraph IW-3520 of Section XI, 1977 Edition Summer 1977 Addenda.

Schedule For Implementation

May 31, 1978

Deleted

34.

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Revision 3 2/26/79

Revision 8/28/78

35. REQUEST FOR RELIEF

COMPONENT	CLASS	TABLE	ITEM	EXAM CATEGORY
Reporting Requirements for Class 1 and Class 2 Components	1&2			

CODE REQUIREMENT

The filing of the inservice inspection reports for Class 1 and 2 components within ninety (90) days after completion of the inservice inspection with the regulatory authority (USNRC) will not be done as required by IWA-6220.

BASIS

Submital of the inservice inspection reports would be an addition to the already heavy reporting burden and would require positive reporting of successful completion of the hundreds of tests and examinations that are required every year on a nuclear plant.

ALTERNATE

All inspection and test records are available at the facility for inspection by the I & E regional inspectors. In addition, the inservice inspection examination summary report will be submitted following each outage in which inspections are conducted. Four copies will be sent to the Director, NRR, and two copies will be sent to the Region III office of Inspection and Enforcement.

SCHEDULE FOR IMPLEMENTATION

COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS
All Class 1, 2 and 3 Components	Pressure Retaining	1, 2, 3

Code Requirement

The hydrostatic test pressure and temperature will not be held for four (4) hours for exposed components, as required by IWA-5210.

Basis

It is unnecessary to maintain the pressure and temperature for four hours for areas of exposed pipe and components. Ten minutes is a sufficient period of time to determine if leaks are present in exposed areas.

Alternate Testing

The test pressure and temperature will be held for ten minutes for exposed areas and four hours for unexposed areas.

Schedule For Implementation

January 1, 1979

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COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS
All Class 2 and 3 Air and Nitrogen Systems	Pressure Retaining	2, 3

Code Requirement

The hydrostatic tests required by IWA-5000, IWC-5000 and IWD-5000 will not be performed using water as the test medium for certain systems.

Basis

The air and nitrogen systems were not designed for water service. Therefore, a hydrostatic test would be inappropriate.

Alternate Testing

These systems will undergo pneumatic tests.

Schedule For Implementation

January 1, 1979

COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS
All Class 1 and 2 Components	Pressure Retaining	1, 2

Code Requirement

The hydrostatic test temperature will not be greater than or equal to 100°F for austenitic stainless steel components as required by IWB-5222 and IWC-5220.

Basis

Austenitic stainless steels do not exhibit or undergo ductile-to-brittle transitions and the toughness remains essentially constant regardless of the temperature of the material. Therefore, heating the test medium to above 100°F for these components is unnecessary.

Alternate Testing

Austenitic stainless steel portions of lines will be tested at ambient temperature.

Schedule for Implementation

January 1, 1979

CODE RECUTREMENT

These valves will not be tested as required by IWV-3410 or IWV-3520.

BASIS

The Excess Flow Check Valves are located in sensing lines for the Plant Protection System and ECCS Instruments. Testing the check valves during operation is not practical since it would make the vital instrumentation inoperable. Cold shutdown testing is also impractical since it would require pressurizing the reactor vessel to operating pressure.

ALTERNATE TESTING

The Excess Flow Check Valves are tested each refueling outage when the vessel is pressurized to 1000 psig during the Reactor Vessel Hydro Test.

SCHEDULE FOR IMPLEMENTATION

This testing was implemented since initial plant startup as required by the original Technical Specifications.

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COMPONENT	FUNCTION	APPLICABLE ASME CODE CLASS	VALVE CATECORY
Excess Flow Check Valve X-28F	Minimize the Blowdown to the secondary containment in the event of an instrument line break and vessel head seal failure.	2	A, C

CODE REQUIREMENT

This valve will not be tested as required by IWV-3410 or IWV-3520.

BASIS

There is no way to test this valve except to remove it from the line since there is normally no pressure between the vessel head seals. Removal of the valve is extremely difficult because the piping is rigid and thread damage has resulted from previous attempts to remove the valve. A sensing line break would result in blowdown to the secondary containment only if the vessel head seal was leaking. The blowdown would be limited by the seal leak which would, in all probability, be less than the leakage allowed by the check valve. The probability of a line break and seal leak occurring to cause a significant blowdown is extremely small, therefore it is felt this valve should not be tested to avoid further thread damage to the piping.

ALTERNATE TESTING

None

SCHEDULE FOR IMPLEMENTATION

N/A

Component	Code	Table	Item	Exam Category
PUMP CASINGS RECIRCULATION PUMPS "A" AND "B"	1	1.5	B5.7	B-L-2

Code Requirement

The visual examination of the Recirculation Pumps internal pressure surfaces will not be scheduled as required by Exam Category B-L-2.

Basis

Disassembly of the recirculation pumps for the sole purpose of visual examination of the casing internal pressure surfaces requires many manhours from skilled maintenance personnel. Increased radiation exposures result from this activity. The probability of pump failure is increased by unnecessarily disassembling the units. Deferring the examination has no affect on integrity of the pumps.

Alternate

Recirculation Pump internal pressure surfaces will be visually examined when the pumps are disassembled for maintenance.

Schedule for Implementation

March 5, 1980

Component		Code	Table	Item	Exam Category
VALVE BODIES CRANE CHAPMAN GATE VAL RECIRCULATION VALVES	VES J 2-65A, MO 2-65B MO 2-53A, MO 2-43A MO 2-53B, MO 2-43B	1	1.6	В6.7	B-M-2

Code Requirement

The visual examination of the Recirculation Valves internal pressure surfaces will not be scheduled as required by Exam Category B-M-2.

Basis

Disassembly of the recirculation valves for the sole purpose of visual examination of the internal pressure surfaces requires many manhours from skilled maintenance personnel. Increased radiation exposures result from this activity. The probability of valve failure is increased by unnecessarily disassembling the units. Deferring the examination has no affect on the integrity of the valves.

Alternate

Recirculation Valve internal pressure surface will be visually examined when the pumps are disassembled for maintenance.

Schedule for Implementation

March 5, 1980

SECTION 5 PROPOSED TECHNICAL SPECIFICATION CHANGES

Reproduced in this section are the proposed Technical Specification changes included in Northern States Power Company's License Amendment Request dated August 30, 1977. These changes revise the surveillance requirements in the Technical Specifications to conform to 10 CFR 50, Section 50.55a(g).

Changes proposed in Northern States Power Company's License Amendment Request dated January 18, 1978 also appear here. These changes were submitted to incorporate a program of sugmented inservice inspection for piping susceptible to stress corrosion cracking.

3.4 STANDBY LIQUID CONTROL SYSTEM

Applicability:

Applies to the operating status of the standby liquid control system.

Objective:

To assure the availability of an independent reactivity control mechanism.

SPECIFICATION:

A. Normal Operation

- 1. The standby liquid control system shall be operable at all times when fuel is in the reactor and the reactor is not shutdown by control rods, except as specified in 3.4.B.
- Each standby liquid control system pump shall be capable of delivering 24 gpm against a reactor pressure of 1275 psig.
- The system pressure relief valves shall be operable with a setpoint between 1350 and 1450 psig.

4.0 SURVEILLANCE REQUIREMENTS

4.4 STANDBY LIQUID CONTROL SYSTEM

Applicability:

Applies to the periodic testing requirements for the standby liquid control system.

Objective:

To verify the operability of the standby liquid control system.

SPECIFICATION:

- A. The operability of the standby liquid control system shall be verified by performance of the following tests:
 - 1. At least once each operating cycle manually initiate one of the two standby liquid control systems and pump demineralized water into the reactor vessel. Both systems shall be tested and inspected in the course of two operating cycles.

2. Inservice inspection and testing of components shall be conducted in accordance with Specification 4.33.

B. Operation with Inoperable Components

From and after the date that a redundant component is made or found to be inoperable, Specification 3.4.A shall be considered fulfilled, provided that the component is returned to an operable condition within seven days.

B. Surveillance with Inoperable Components

When a component becomes inoperable, its redundant component shall be demonstrated to be operable immediately and daily thereafter.

C. Volume-Concentration Requirements

The liquid poison tank shall contain a boron bearing solution that satisfies the volume-concentration requirements of Figure 3.4.1 and at all times when the standby liquid poison system is required to be operable the temperature shall not be less than the solution temperature presented in Figure 3.4.2. In addition, the heat tracing on the pump suction lines shall be operable whenever the room temperature is less than the solution temperature presented in Figure 3.4.2.

C. The availability of the proper boron bearing solution shall be verified by performance of the following tests:

1. At least once per month -

Boron concentration shall be determined. In addition, the boron concentration shall be determined any time water or boron are added or if the solution temperature drops below the limits specified by Figure 3.4.2.

A. The design objective of the standby liquid control system is to provide the capability of bringing the reactor from full power to a cold, xenon-free shutdown assuming that none of the withdrawn control rods can be inserted. To meet this objective, the liquid control system is designed to inject a quantity of boron which produces a concentration of 900 ppm of boron in the reactor core in less than 125 minutes. 900 ppm boron concentration in the reactor core is required to bring the reactor from full power to a 3% Ak subcritical condition considering the hot to cold reactivity swing, xenon poisoning and an additional 25% boron concentration margin for possible imperfect mixing of the chemical solution in the reactor water and dilution from the water in the cooldown circuit. A minimum net quantity of 1400 gallons of solution having a 21.4% sodium pentaborate concentration is required to meet this shutdown requirement.

The time requirement (125 minutes) for insertion of the boron solution was selected to override the rate of reactivity insertion due to cooldown of the reactor following the xenon poison peak. The maximum net storage volume of the boron solution is 2895 gallons. (256 gallons are contained below the pump suction and, therefore, have not been used in the net quantities above.)

Boron concentration, solution temperature, and volume (including check of tank heater and pipe heat tracing system) are checked on a frequency to assure a high reliability of operation of the system should it ever be required. Experience with pump operability demonstrates that testing at a three-month interval is adequate to detect if failures have occurred.

Standby liquid control system components are inspected and tested in accordance with the requirements of 10 CFR 50, Section 50.55a(g). These requirements are delineated in Specification 4.13. This inspection and testing program, combined with the additional surveillance requirements contained in this section, provide a high degree of assurance that the standby liquid control system will perform as required when needed.

The relief valves in the standby liquid control system protect the system piping and positive displacement pumps which are nominally designed for 1500 psi from overpressure. The pressure relief valves discharge back to the standby liquid control solution tank.

4.0 SURVEILLANCE REQUIREMENTS

3.5 CORE AND CONTAINMENT COOLING SYSTEMS

Applicability:

Applies to the operational status of the emergency cooling systems.

Objective:

To insure adequate cooling capability for heat removal in the event of a loss of coolant accident or isolation from the normal reactor heat sink.

Specification:

Low Pressure Core Cooling Capability

A. Core Spray System

1. Except as specified in 3.5.A.2.,
3.5.A.3., and 3.5.A.5. below, both core
spray subsystems shall be operable whenever irradiated fuel is in the reactor
vessel and reactor coolant water temperature is greater than 212°F.

4.5 CORE AND CONTAINMENT COOLING SYSTEMS

Applicability:

Applies to periodic testing of the emergency cooling systems.

Objective:

To verify the operability of the emergency cooling systems.

Specification:

Low Pressure Core Cooling Capability

- A. Surveillance of the core spray system shall be performed as follows:
 - 1. Routine Testing
 - a. A simulated automatic actuation test shall be conducted each refueling outage.
 - b. Core spray header ap instrumentation shall be checked once each day, tested once each month, and calibrated once each 3-month period.

c. Inservice inspection and testing of components shall be conducted in accordance with Specification 4.13.

- 2. From and after the date that one of the core spray systems is made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding fifteen days unless such system is sooner made operable, provided that during such fifteen days all active components of the other core spray system and the LPCI mode of the RHR system and the diesel generators required for operation of such components (if no external source of power were available) shall be operable.
- From and after the date that both core spray systems are made or found to be inoperable for any reason, reactor

- 2. When it is determined that one core spray system is inoperable, the operable core spray system and the LPCI mode of the RHR system and the diesel generators required for operation of such components (if no external source of power were available) shall be demonstrated to be operable immediately. The operable core spray system shall be demonstrated to be operable daily thereafter.
- When it is determined that both core spray systems are inoperable, the LPCI mode of the RHR system and the

3.5/4.5

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operation is permissible only during the succeeding seven days unless at least one of such systems is sooner made operable, provided that during such seven days all active components of the LPCI mode of RHR system and the diesel generators required for operation of such components (if no external source of power were available) shall be operable.

- 4. Each core spray system shall be capable of delivering 3,020 gpm against a reactor pressure of 130 psig. If this rate of delivery requirement cannot be met, the system shall be considered inoperable.
- 5. If the requirements of 3.5.A.1 3 cannot be met, an orderly shutdown of the reactor will be initiated and the reactor water temperature shall be reduced to less than 212 of within C4 hours.

diesel generators required for operation of such components (if no external source of power were available) shall be demonstrated to be operable immediately and daily thereafter.

- B. Low Pressure Coolant Injection (LPCI) Subsystem (LPCI mode of RHR system)
 - Except as specified in 3.5.B.2 and 3.5.B.3 below, the LPCI shall be operable whenever irradiated fuel is in the reactor vessel and reactor coolant temperature is greater than 212°F.

2. From and after the date that one of the LPCI pumps or admission valves is made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding thirty days unless such pump or admission valve is sooner made operable, provided that during such thirty days the remaining active components of the LPCI and containment cooling subsystem and all active components of both core spray systems and the diesel generators required for operation of such components (if no external source of power were available) shall be operable.

- B. Surveillance of the Low Pressure Coolant Injection (LPCI) Subsystem (LPCI mode of RHR system) shall be performed as follows:
 - 1. Routine Testing
 - a. A simulated automatic actuation test shall be conducted each refueling cutage.
 - b. Inservice inspection and testing of components shall be conducted in accordance with Specification 4.13.
 - c. During each five year period, an air test shall be performed on the drywell spray headers and nozzles.
 - 2. When it is determined that one of the LPCI pumps is inoperable, the remaining active components of the LPCI and containment cooling subsystem, both core spray systems and the diesel generators required for operation of such components (if no external source of power were available) shall be demonstrated to be operable immediately and the operable LPCI pumps daily thereafter.

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- 3. From and after the date that two of the LPCI pumps or admission valves are made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding seven days unless such pumps or admission valves are made operable sooner, provided that during such seven days all active components of both core spray systems, the containment cooling subsystem (including 2 LPCI pumps) and the diesel generators required for operation of such components (if no external source of power were available) shall be demonstrated to be operable at least once each day.
- 4. A maximum of one drywell spray loop (containment cooling mode of RHR) may be inoperable for 30 days when the reactor water temperature is greater than 212°F. If the loop is not returned to service within 30 days, the orderly shutdown of the reactor will be initiated and the reactor water temperature shall be reduced to less than 212°F.
- 5. Each LPCI subsystem (RHR) pump shall be capable of delivering 4,000 gpm against a reactor pressure of 20 psig. If this

3. When it is determined that the LPCI subsystem is inoperable, both core spray systems, the containment cooling subsystem, and the diesel generators required for operation of such components (if no external source of power were available) shall be demonstrated to be operable immediately and daily thereafter.

4.0 SURVEILLANCE REQUIREMENTS

rate of telivery requirement cannot be met, the pump shall be considered inoperable.

6. If the requirements of 3.5.B.14 cannot be met, an orderly shutdown of the reactor will be initiated and the reactor water temperature shall be reduced to less than 212 bF within 24 hours.

Containment Cooling Capability

- C. Residual Heat Removal (RHR) Service Water System
 - 1. Except as specified in 3.5.0.2 and 3.5.0.3 below, both RHR service water system loops shall be operable whenever irradiated fuel is in the reactor vessel and reactor coolant temperature is greater than 212°F.
 - From and after the date that one of the RHR service water system pumps is ade or found to be inoperable for any reason,

Containment Cooling Capability

- C. Surveillance of the RHR service water system shall be performed as follows:
 - Inservice inspection and testing of components shall be conducted in accordance with Specification 4.13.

 When it is determined that one RHR service water pump is inoperable, the redundant components of the

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reactor operation is permissible only during the succeeding thirty days unless such pump is sooner made operable, provided that during such thirty days all other active components of the RHR service water system are operable.

- RHR service water systems is made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding seven days unless such system is sooner made operable, provided that during such seven days all active components of the operable RHR service water system shall be demonstrated to be operable at least once each day.
- 4. To be considered operable, a RHR service water pump shall be capable of delivering 3500 gpm against a head of 500 feet.
- 5. If the requirements of 3.5.C.1-3 cannot be met, an orderly shutdown of the reactor will be initiated and the reactor water temperature shall be reduced to less than 2120F within 24 hours.

remaining subsystem shall be demonstrated to be operable immediately and daily thereafter.

3. When one RHR service water system becomes inoperable, the operable system shall be demonstrated to be operable immediately and daily thereafter.

4.0 SURVEILLANCE REQUIREMENTS

High Pressure Core Cooling Capability

- D. High Pressure Coolant Injection (HPCI) System
 - Except as specified in 3.5.D.2 below, the HPCI system shall be operable whenever the reactor pressure is greater than 150 psig and irradiated fuel is in the reactor vessel.

2. From and after the date that the HPCI system is made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding seven days unless such system is sooner made operable, provided that during such seven days all of the Automatic Pressure Relief system, the RCIC system, both of the core spray systems, and the LPCI subsystem and containment cooling mode of the RHR system are operable.

High Pressure Core Cooling Capability

- D. Surveillance of HPCI System shall be performed as follows:
 - 1. Routine Testing
 - a. A simulated automatic actuation test shall be conducted each refueling outage.
 - b. Inservice inspection and testing of components shall be conducted in accordance with Specification 4.13.

When it is determined that HPCI system is inoperable, the RCIC system, the LPCI subsystem, and both of the core spray systems shall be demonstrated to be operable immediately.

- 3. To be considered operable, the HPCI system shall meet the following conditions:
 - a. The HPCI shall be capable of delivering 3,000 gpm into the reactor vessel for the reactor pressure range of 1120 psig to 150 psig.
 - b. The condensate storage tanks shall contain at least 75,000 gallons of condensate water.
 - c. The controls for automatic transfer of the HPCI pump suction from the condensate storage tank to the suppression chamber shall be operable.
- 4. If the requirements of 3.5.D.1-2 cannot be met, an orderly reactor shutdown shall be initiated immediately and the reactor pressure shall be reduced to 150 psig within 24 bours thereafter.

E. Automatic Pressure Relief System

- 1. Except as specified in 3.5.E.2 and 3.5.E.3 below, the entire automatic pressure relief system shall be operable at any time the reactor pressure is above 150 psig and irradiated fuel is in the reactor vessel.
- 2. From and after the date that one of the automatic pressure relief system valves is made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding seven days unless such valve is sooner made operable, provided that during such teven days both remaining automatic relief system valves and the HPCI system are operable.
- 3. From and after the date that more than one of the automatic pressure relief valves are made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding 24 hours unless repairs are made and provided that during such time the HPCI system is operable.
- 4. If the requirements of 3.5.5.1-3 cannot be met, an orderly reactor shutdown shall be initiated immediately and the reactor shall be reduced to 150 psig within 24 hours thereafter.

4.0 SURVEILLANCE REQUIREMENTS

- E. Surveillance of the Automatic Pressure Relief System shall be performed as follows:
 - 1. Routine Testing
 - a. A simulated automatic actuation test shall be conducted each operating cycle.
 - b. Once each operating cycle, valve operability shall be verified by cycling the valves and observing a compensating change in turbine bypass valve position.
 - c. Inservice inspection and testing of components shall be conducted in accordance with Specification 4.13.

 When it is determined that one or more automatic pressure relief valves of the Automatic Pressure Relief system is inoperable, the RPCI system shall be demonstrated to be operable immediately and weekly thereafter.

3.0 LIMITING COMDITIONS FOR OFERATION

F. Reactor Core Isolation Cooling System (RCIC)

- 1. Except as specified in 3.5.F.2 below, the RCIC system shall be operable whenever the reactor pressure is greater than 150 psig and irradiated fuel is in the reactor vessel.
 - a. To be considered operable, the RCIC system shall be capable of delivering 400 gpm into the reactor vessel.

- 2. From and after the date that the RCIC system is made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding 15 days unless such system is sooner made operable, provided that during such 15 days all active components of the HPCI system are operable.
- 3. If the requirements of 3.5.F.1 2 cannot be met, an orderly shutdown of the reactor shall be initiated immediately and the reactor pressure shall be reduced to 150 psig within 24 hours thereafter.

4.0 SURVEILLANCE REQUIREMENTS

F. Surveillance of Reactor Core Isolation Cooling System (RCIC)

Surveillance of the RCIC System shall be performed as follows:

1. Routine Testing

- a. A simulated automatic actuation test shall be conducted each refueling outage.
- b. Inservice inspectic, and testing of components shall be conducted in accordance with Epecification 4.13.

2. When it is determined that the RCIC system is inoperable, the HPCI system shall be demonstrated to be operable immediately and daily thereafter.

I. Recirculation System

- Except as specified in 3.5.1.2 below, whenever irradiated fuel is in the reactor, with reactor coolant temperature greater than 212°F and both reactor recirculation pumps operating, the recirculation system cross tie valve interlocks shall be operable.
- The recirculation system cross tie valve interlocks may be inoperable if at least one cross tie valve is maintained fully closed.
- Valves in the equalizer piping between the recirculation loops shall be closed. Reactor operation with one loop shall be limited to 24 hours.

I. Recirculation System

- Once per month, when irriated fuel is in the reactor with reactor coolent temperature greater than 212°F and both reactor recirculation pumps operating, the recirculation systym cross tie valve interlocks shall be demonstrated to be operable by verifying that the cros tie valves cannot be opened using the normal control switch.
- When a recirculation system cross tie valve interlock is inoperable, the position of at least one fully closed cross tie valve shall be recorded daily.
- Inservice inspection and testing of components shall be conducted in accordance with Specification 4.13.

Bases 4.5:

The testing interval for the core and containment cooling systems is based on a quantitative reliability analysis, judgment, and practicality. The core cooling systems have not been designed to be fully testable during operation. For example, the core spray final admission valves do not open until reactor pressure has fallen to 450 psig; thus, during operation even if high drywell pressure were simulated, the final valves would not open. In the case of the HPCI, automatic initiation during power operation would result in pumping cold water into the reactor vessel, which is not desirable.

The systems can be automatically actuated during a refueling outage and this will be done. To increase the availability of the individual components of the core and containment cooling systems, the components which make up the system, i.e., instrumentation, pumps, valve operators, etc., are tested more frequently. The instrumentation will initially be functionally tested once per month un. 1 a trend is established and thereafter according to Figure 4.1 (see Section 3.1/4.1) with an interval not greater than three months. Core and containment cooling system components are inspected and tested in accordance with the requirements of 10 CFR 50, Section 50.55a(g). These requirements are delineated in Specification 4.13. This inspection and testing program, combined with the additional surveillance requirements contained in this section, provide a high degree of assurance that the core and containment cooling systems will perform as required when needed.

With components or subsystems out-of-service, overall core and containment cooling reliability is maintained by demonstrating the operability of the remaining cooling equipment. The degree of operability to be demonstrated depends on the nature of the reason for the out-of-service equipment. For routine out-of-service periods caused by preventative maintenance, etc., the pump and valve operability checks will be performed to demonstrate operability of the remaining components. However, if a failure, design deficiency, etc., caused the out-of-service period, then the demonstration of operability should be thorough enough to assure that a similar problem does not exist on the remaining components. For example, if an out-of-service period were caused by failure of a pump to deliver rated capacity due to a design deficiency, the other pumps of this type might be subjected to a flow rate test in addition to the operability checks.

E. Safety/Relief Valves

- During power operating conditions and whenever reactor coolant pressure is greater than 110 psig and temperature is greater than 345°F:
 - a. The safety valve function (self-actuation) of seven safety/relief valves shall be operable.
 - b. The solenoid activated relief function (Automatic Pressure Relief) shall be operable as required by Specification 3.5.E.

E. Safety/Relief Valves

- The integrity of the safety/relief valve bellows shall be continuously monitored.
- The operability of the bellows monitoring system shall be demonstrated at least once every three months.
- Inservice inspection and testing of components shall be conducted in accordance with Specification 4.13.

3.0 LIMITING CONDITIONS FOR OPERATION

4.0 SURVEILLANCE REQUIREMENTS

F. deleted

G. Jet Pumps

Whenever the reactor is in the Startup or Run modes, all jet pumps shall be operable. If it is determined that a jet pump is inoperable, the plant shall be placed in a cold shutdown condition within 24 hours.

deleted

F.

G. Jet Pumps

Whenever there is recirculation flow with the reactor in the Startup or Run modes, jet pump operability shall be checked daily by verifying that all the following conditions do not occur simultaneously:

- 1. The two recirculation loop flows are unbalanced by 15% or more when the recirculation pumps are operating at the same speed.
- 2. The indicated value of core flow rate is 10% or more less than the value derived from loop flow measurements.

Bases Continued 3.6 and 4.6:

The safety/relief valves have two functions; i.e. power relief or self-actuated by high pressure. The solenoid actuated function (Automatic Pressure Relief) in which external instrumentation s'gnals of coincident high drywell pressure and low-low water level initiate opening of the valves. This function is discussed in Specification 3.5.E. In addition, the valves can be operated manually.

The safety function is performed by the same safety/relief valve with self-actuated integral bellows and pilot valve causing main valve operation. Article 9 of the ASME Pressure Vessel Code Section III Nuclear Vessels requires that these bellows be monitored for failure since this would defeat the safety function of the safety/relief valve.

It is realized that there is no way to repair or replace the bellows during operation and the plant must be shut down to do this. The thirty-day period to do this allows the operator flexibility to choose his time for shutdown; meanwhile, because of the redundancy present in the design and the continuing monitoring of the integrity of the other valves, the overpressure pressure protection has not been compromised. The auto-relief function would not be impaired by a failure of the bellows. However, the self-actuated overpressure safety function would be impaired by such a failure.

Provision also has been made to detect failure of the bellows monitoring system. Testing of this system quarterly provides assurance of bellows integrity.

When the setpoint is being bench checked, it is prudent to disassemble one of the safety/relief valves to examine for crud buildup, bending of certain actuator members or other signs of possible deterioration.

The program of safety/relief valve testing conforms to the requirements of 10 CFR 50, Section 50.55a(g). These requirements are delineated in Specification 4.13. This inspection and testing program, combined with the additional surveillance requirements contained in this section, provide a high degree of assurance that the safety/relief valves will perform as required when needed.

Bases Continued 3.6 and 4.6:

F. deleted

Bases Continued 3.6 and 4.6:

G. Jet pumps

Failure of a jet pump nozzle assembly hold down mechanism, nozzle assembly and/or riser, would increase the cross-sectional flow area for blowdown following the design basis double-ended line break. Therefore, if a failure occurred, repairs must be made.

The detection technique is as follows. With the two recirculation pumps balanced in speed to within + 5%, the flow rates in both recirculation loops will be verified by Control Room monitoring instruments. If the two flow rate values do not differ by more than 10%, riser and nozzle assembly integrity has been verified. If they do differ by 10% or more, the core flow rate measured by the jet pump diffuser differential pressure system must be checked against the core flow rate derived from the measured values of loop flow to core flow correlation. If the difference between measured and derived core flow rate is 10% or more (with the derived value higher) diffuser measurements will be taken to define the location within the vessel of failed jet pump nozzle (or riser) and the plant shut down for repairs. If the potential blowdown flow area is increased, the system resistance to the recirculation pump is also reduced; hence, the affected drive pump will "run out" to a substantially higher flow rate (approximately 115% to 120% for a single nozzle failure). If the two loops are balanced in flow at the same pump speed, the resistance characteristics cannot have changed. Any imbalance between drive loop flow rates would be indicated by the plant process instrumentation. In addition, the affected jet pump would provide a leakage path past the core thus reducing the core flow rate. The reverse flow through the inactive jet pump would still be indicated by a positive differential pressure but the net effect would be a slight decrease (3% to 6%) in the total core flow measured. This decrease, together with the loop flow increase, would result in a lack of correlation between measured and derived core flow rate. Finally, the affected jet pump diffuser differential pressure signal would be reduced because the backflow would be less than the normal forward flow.

A nozzle-riser system failure could also generate the coincident failure of a jet pump body; however, the converse is not true. The lack of any substantial stress in the jet pump body makes failure imp saible without an initial nozzle-riser system failure.

3.0 LIMITING CONDITIONS FOR OF PATION

- Pressure Suppression Chamber -Reactor Building Vacuum Breakers
 - a. Except as specified in 3.7.A.3.b below, two pressure suppression chamber-reactor building vacuum breakers shall be operable at all times when the primary containment integrity is required. The set point of the differential pressure instrumentation which actuates the pressure suppression chamber-reactor building vacuum breakers shall be 0.5 psi.
 - b. From and after the date that one of the pressure suppression chamber-reactor building vacuum breakers is made or found to be inoperable for any reason, reactor operation is permissible only during the succeeding seven days unless such vacuum breaker is sooner made operable. provided that the repair procedure does not violate primary containment integrity.

4.0 SURVEILLANCE REQUIREMENTS

- Pressure Suppression Chamber -Reactor Building Vacuum Breakers
 - a. The pressure suppression chamber-reactor building vacuum breakers and associated instrumentation including set point shall be checked for proper operation every three months.
 - b. Inservice inspection and testing of components shall be conducted in accordance with Specification 4.13.

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- d. The fuel cask or irradiated fuel is not being moved within the reactor building.
- D. Primary Containment Isolation Valves
 - During reactor power operating conditions, all isolation valves listed in Table 3.7.1 and all primary system instrument line flow check valves shall be operable except as specified in 3.7.D.2.
- D. Primary Containment Isolation Valves
 - The primary containment isolation valves surveillance shall be performed as follows:
 - a. At least once per operating cycle the operable isolation valves that are power operated and automatically initiated shall be tested for simulated automatic initiation and closure times.
 - b. Inservice inspection and testing of components shall be conducted in accordance with Specification 4.13.

- In the event any isolation valve specified in Table 3.7.1 becomes inoperable, reactor operation in the run mode may continue provided at least one valve in each line having an inoperable valve is closed.
- If Specification 3.7.D.1 and 3.7.D.2 cannot be met, initiate normal orderly shutdown and have reactor in the cold shutdown condition within 24 hours.

 Whenever an isolation valve listed in Table 3.7.1 is inoperable, the position of at least one fully closed valve in each line having an inoperable valve shall be recorded daily.

3.0 LIMITING CONDITIONS FOR OPERATION

3.13 INSERVICE INSPECTION AND TESTING

Applicability:

Applies to components which are part of the reactor coolant pressure boundary and their supports and other safety-related pressure vessels, piping, pumps, and valves.

Objective:

To assure the integrity of the reactor coolant pressure boundary and the operational readiness of safety-related pressure vessels, piping, pumps, and valves.

Specification:

A. Inservice Inspection

1. To be considered operable, Quality Group A, B, and C components shall satisfy the requirements contained in Section XI of the ASME Boiler and Pressure Vessel Code and applicable Addenda for continued service of ASME Code Class 1, 2, and 3 components, respectively, except where relief has been requested from the Commission pursuant to 10 CFR 50, Section 50.55a(g)(6)(i).

4.0 SURVEILLANCE REQUIREMENTS

4.13 INSERVICE INSPECTION AND TESTING

Applicability:

Applies to the periodic inspection and testing of components which are part of the reactor coolant pressure boundary and their supposes and other safetyrelated pressure vessels, piping, pumps, and valves.

Objective:

To verify the integrity of the reactor coolant pressure boundary and the operational readiness of safety-related pressure vessels, piping, pumps, and valves.

Specification:

A. Inservice Inspection

1. Inservice inspection of Quality
Group A, B, and C components shall
be performed in accordance with
the requirements for ASME Code Class
1, 2, and 3 components, respectively,
contained in Section XI of the ASME
Boiler and Pressure Vessel Code and
applicable Addenda as required by
10 CFR 50, Section 50.55a(g), except
where relief has been requested from
the Commission pursuant to 10 CFR 50,
Section 50.55a(g)(6)(i).

- 2. For Non-Conforming Lines which are not Service Sensitive, inspections required by 4.13.A.1 during the first 10-year inspection interval shall be completed by the end of the 1978 refueling outage. If these examinations reveal no incidence of stress corrosion cracking, the examination schedule may revert to that specified in 4.13.A.1.
- For Non-Conforming Lines which are Service Sensitive:
 - a. The welds and adjoining areas of bypass piping of the discharge valves in the main recirculation loops, and of the austenitic stainless steel reactor core spray piping up to and including the second isolation valve, shall be examined at each reactor refueling outage or at other scheduled or unscheduled plant cold shutdowns. Successive examinations need not be closer than six months apart. In the event three successive examinations find the piping free of unacceptable indications, the examination may be extended to each 36 month interval. plus or minus 12 months, coinciding with a refueling outage, and may be limited to one bypass pipe run and one reactor core spray pipe run.

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B. Inservice Testing of Pumps and Valves

1. To be considered operable, Quality Group A, B, and C pumps and valves shall satisfy the requirements contained in Section XI of the ASME Boiler and Pressure Vessel Code and applicable Addenda for operability of ASME Code Class 1, 2, and 3 pumps and valves, respectively, except where relief has been requested from the Commission pursuant to 10 CFR 50, Section 50.55a(g)(6)(1).

b. If Service Sensitive Lines other than those listed in 4.13. B. 3.a above are identified. the welds and adjoining areas of this piping shall be subjected to examination at each reactor refueling outage or at other scheduled or unscheduled plant cold shutdowns on a sampling basis. Successive examinations need not be closer than six months apart. If unacceptable flaw indications are detected in any branch run, the remaining branch runs with similar functions and configurations shall be examined. In the event three successive examinations find the piping free of unacceptable indications, the examination schedule may revert to that specified in 4.13.A.1 with the exception that all examinations normally completed over a ten-year interval shall be completed each 80-month period.

B. Inservice Testing of Pumps and Valves

A, B, and C pumps and valves shall be performed in accordance with the requirements for ASME Cole Class 1, 2, and 3 pumps and valves, respectively, contained in Section Xi of the ASME Boiler and Pressure Vessel Code and applicable Addenda as required by 10 CFR 50, Section 50.55a(g) except where relief has been required from the Commission pursuar to 10 CFR 50, Section 50.55a(g)(f',1).

Bases 3.13 and 4.13:

The inservice inspection and testing program conforms to the requirements of 10 CFR 50, Section 50.55a(g). Where practical, the inspection and testing of components classified into NRC Quality Groups A, B, and C will conform to the requirements for ASME Code Class 1, 2, and 3 components contained in Section XI of the ASME Boiler and Pressure Vessel Code.

Using Regulatory Guide 1.26, Revision 3, "Quality Group Classifications and Standards for Water, Steam, and Radioactive-Waste-Containing Components of Nuclear Power Plants," as a guide, all Monticello components have been classified into Quality Groups. This classification serves as the basis for determining which ASME Code Class inspection and testing requirements are applicable to a given component. 10 CFR 50, Section 50.55a(g) requires components which are part of the reactor coolant pressure boundary and their supports to meet the inservice inspection and testing requirements applicable to components classified as ASME Code Class 1. Other safety-related components must meet the inservice inspection and testing requirements applicable to components classified as ASME Code Class 2 or 3.

The inservice inspection program must be updated at 40 month intervals. The program for testing pumps and valves for operational readiness must be updated every 20 months. A description of the updated programs should be submitted to the NRC for review at least 90 days before the start of each period. A suggested format for this description is contained in Appendix A to reference (1).

The inservice inspection and testing program must, to the extent practical, comply with the requirements in editions and addenda to the ASME Code that are "in effect" no more than six months before the start of the period covered by the updated program. The term "in effect" means both having been published by the ASME, and having been referenced in paragraph (b) of 10 CFR 50, Section 50.55a. If a code required inspection or test is impractical, requests for deviations are submitted to the Commission in accordance with 10 CFR 50, Section 50.55a(g)(6)(i). The information specified in Appendix B to reference (1) should be submitted for each deviation requested. Deviation requests should, if possible, be submitted to the NRC for review at least 90 days tefore the start of each period. Deviations identified during an inspection reriod may be grouped and requested at the end of each calendar quarter. It is expected that a small number of deviations will be identified during the inspection period, particularily the first period when new inspection and testing techniques will be utilized. A requested deviation request may be considered acceptable to the Commission until a formal disapproval has been received.

3.13/4.13 BASES

Small, hairline cracks in austenitic stainless steel piping in BWR facilities has been observed on several occasions. Data indicates that Type 304 austenitic stainless steel piping in the reactor coolant pressure boundary of the boiling water reactor is susceptible to stress corrosion cracking. Such cracking is caused by a combination of significant amounts of oxygen in the coolant, high stresses, and some sensitization of metal adjacent to welds. Cracks have occurred in the heat affected zones adjacent to welds, but are not expected to occur outside these areas, provided the pipe material is properly annealed. Pipe runs containing stagnant or low velocity fluids have been observed to be more susceptible to stress corrosion cracking than pipes containing a continuously flowing fluid during plant operation. Bistorically, these cracks have been identified either by volumetric examination, by leak detection systems, or by visual inspection. Because of the inherent high material toughness of austenitic stainless steel piping, stress corrosion cracking is unlikely to cause a rapidly propagating failure resulting in a loss of coolant accident.

Although the probability that stress corrosion cracks will propagate far enough to create a significant safety hazard is slight, the presence of such cracks is undesirable. The following steps have been taken to minimize this problem:

- Where practical, pipe runs constructed of material susceptable to stress corrosion cracking and which contained stagnant or low velocity fluid have been replaced with materials not susceptable to cracking or they have been eliminated.
- The reactor coolant leakage detection technical specifications have been amended to enhance the ability to detect unidentified leakage that may include through-wall cracks.
- The program of inservice inspection has been augmented to increase the probability of crack detection in lines susceptable to stress corrosion cracking.

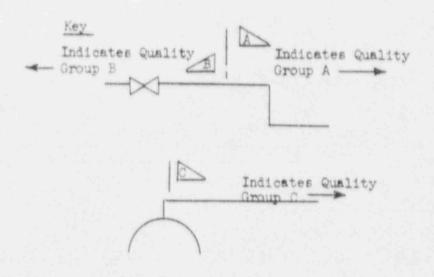
This program conforms to the Commission's guidelines for plants with operating licenses (crence 2).

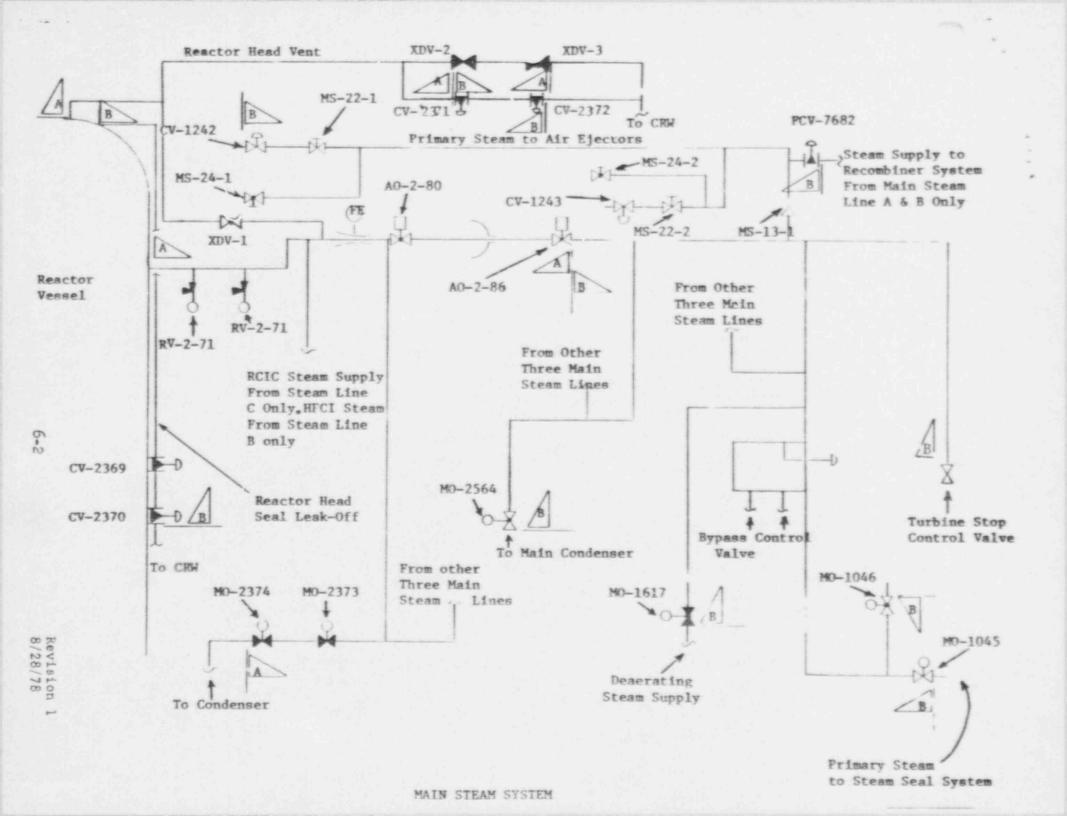
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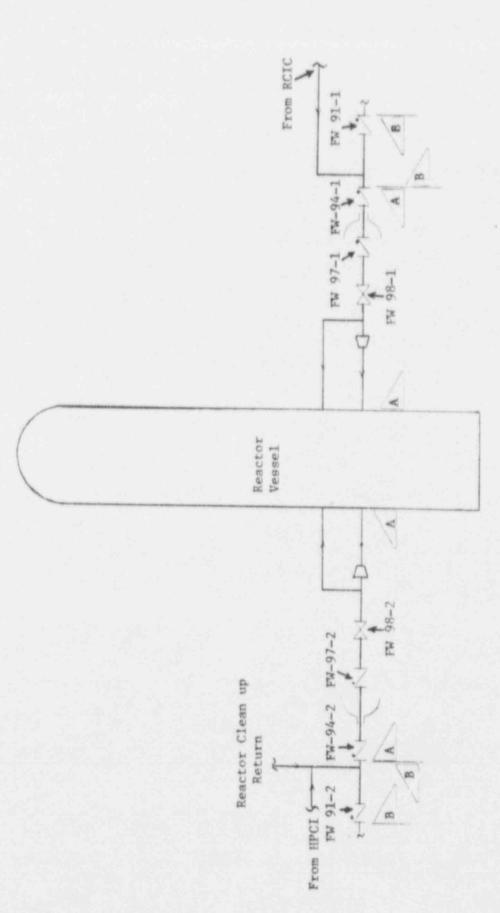
- 1. Letter from D. L. Ziemann, Chief, Operating Reactors Branch #2, USNRC, to L. O. Mayer, NSP, dated November 24, 1976.
- 2. NUREG-0313, "Technical Report on Material Selection and Processing Guidelines for BWR Coolant Pressure Boundary Piping," July, 1977.

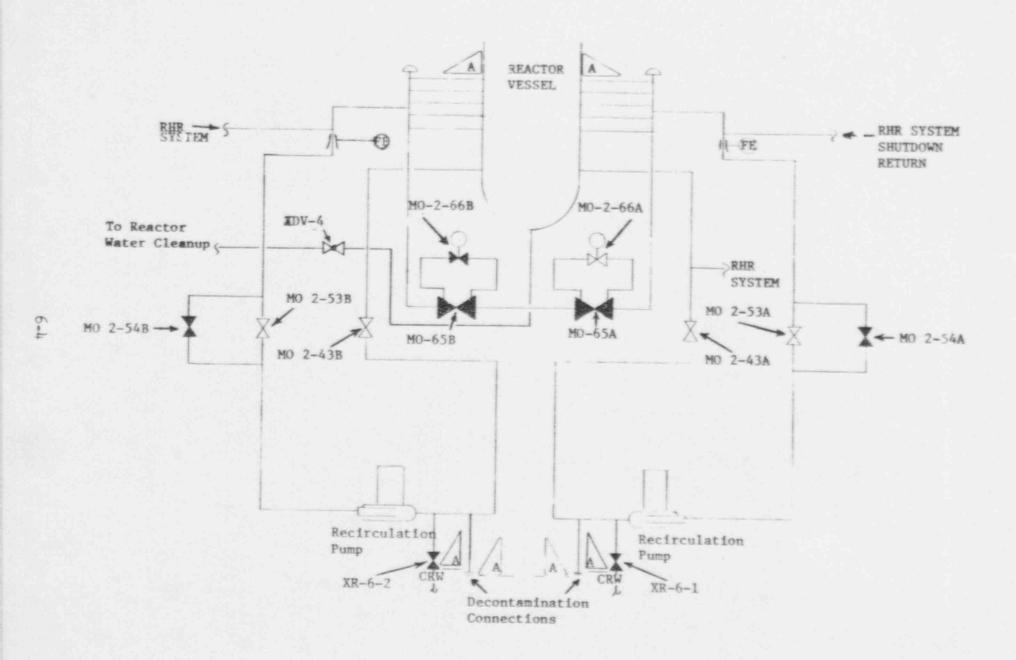
SECTION 6 QUALITY GROUP CLASSIFICATION DRAWINGS

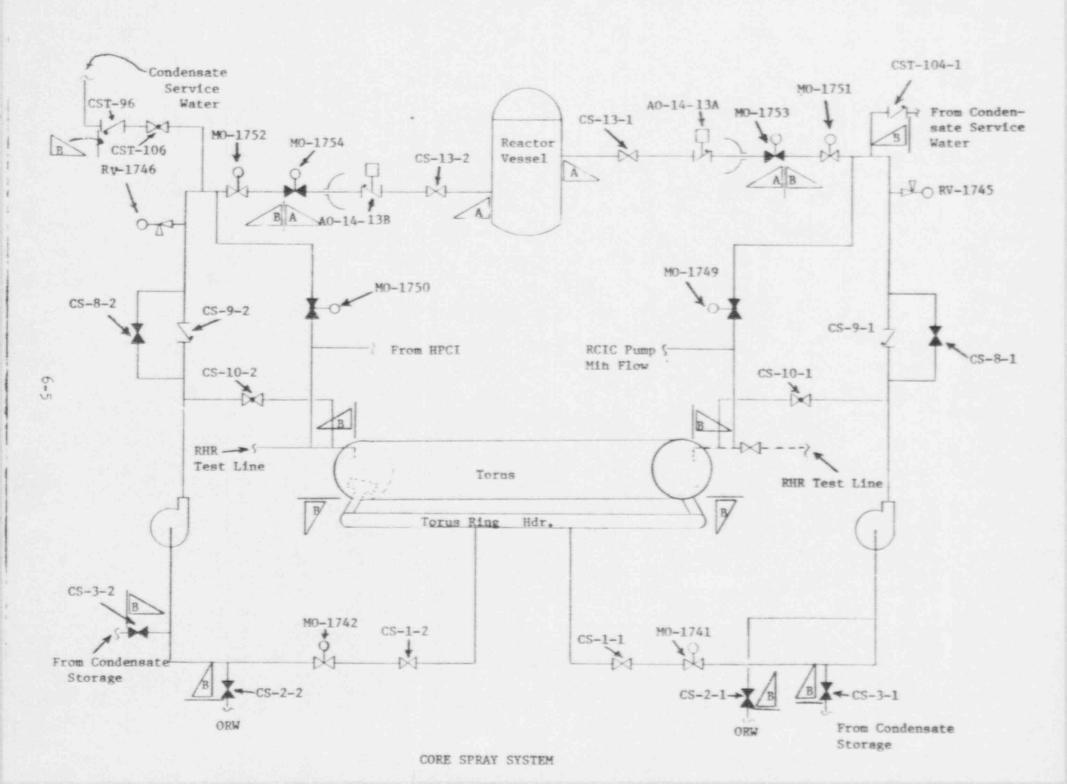
System	Page
Main Steam System Feedwater System	6+2
Reactor Recirculation System Core Spray System	6-4 6-5
Residual Heat Removal Syste Loop A Residual Heat Removal System Loop B	6-6
High Pressure Coolant Injection System (steam side)	6-7 6-8
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Primary Containment System Emergency Service Water	6-13 6-14
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Fuel Pool Cooling & Clean-up System	6-18
Compressed Air System Condensate Service System	6-18 6-18
Reactor Building Cooling Water System	0=19
Reactor Water Clean-up System Liquid Radwaste System	6-19 6-19
Traversing In-core Probe System	6+20
Excess Flow Check Valves	6-21

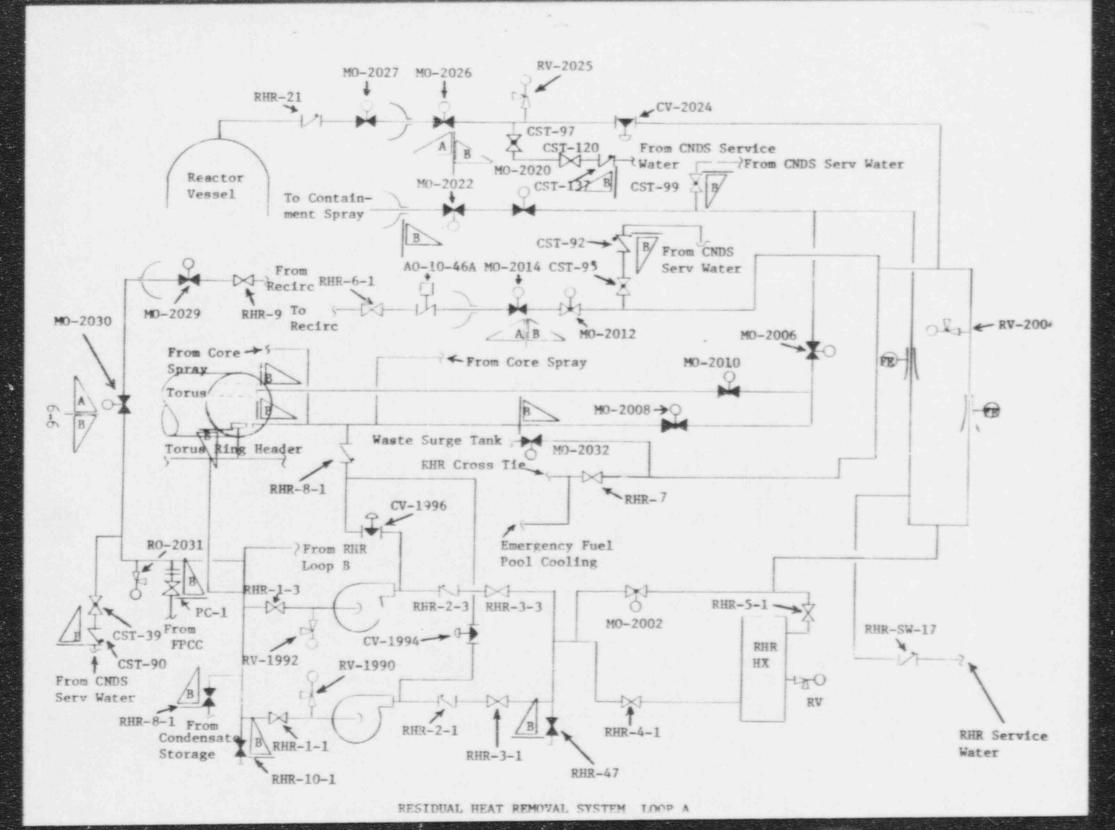


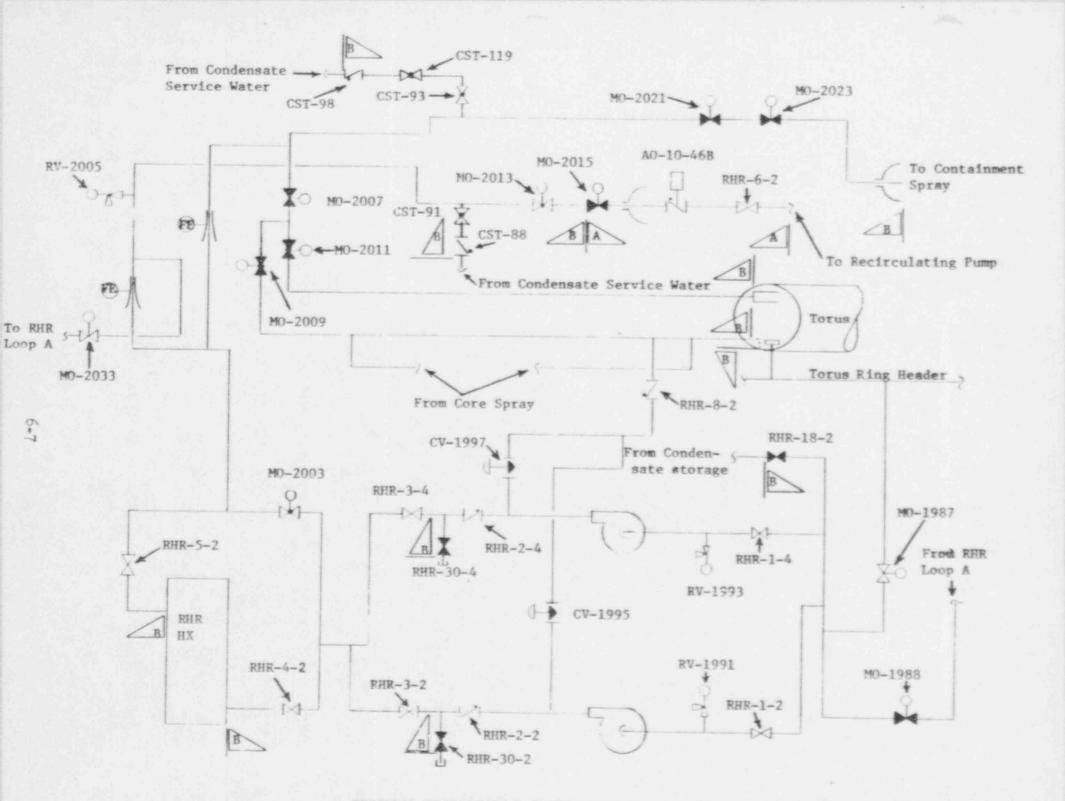


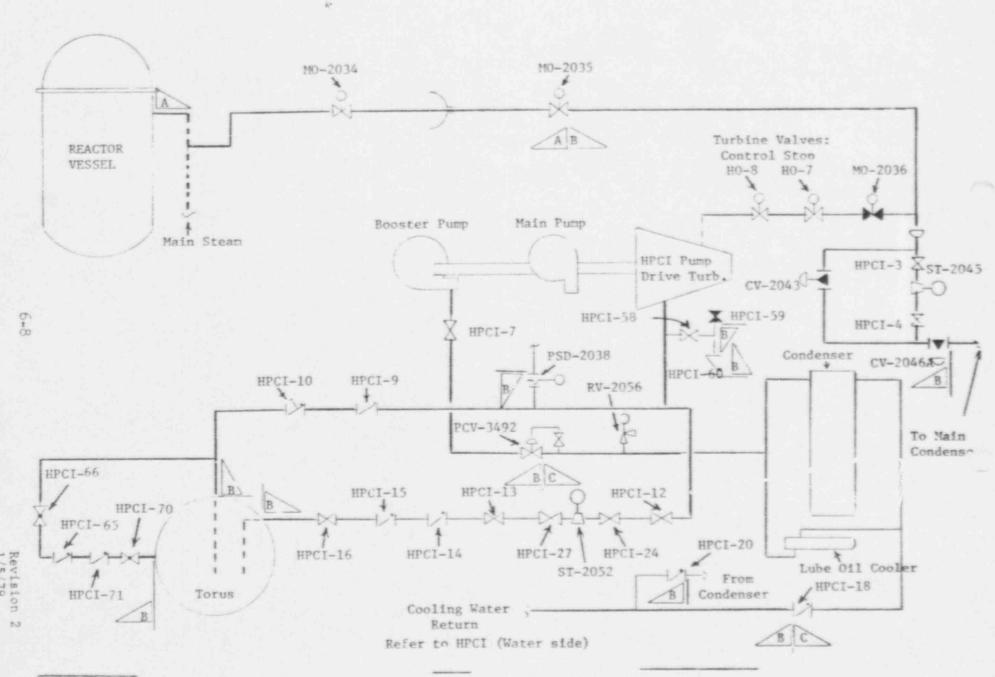


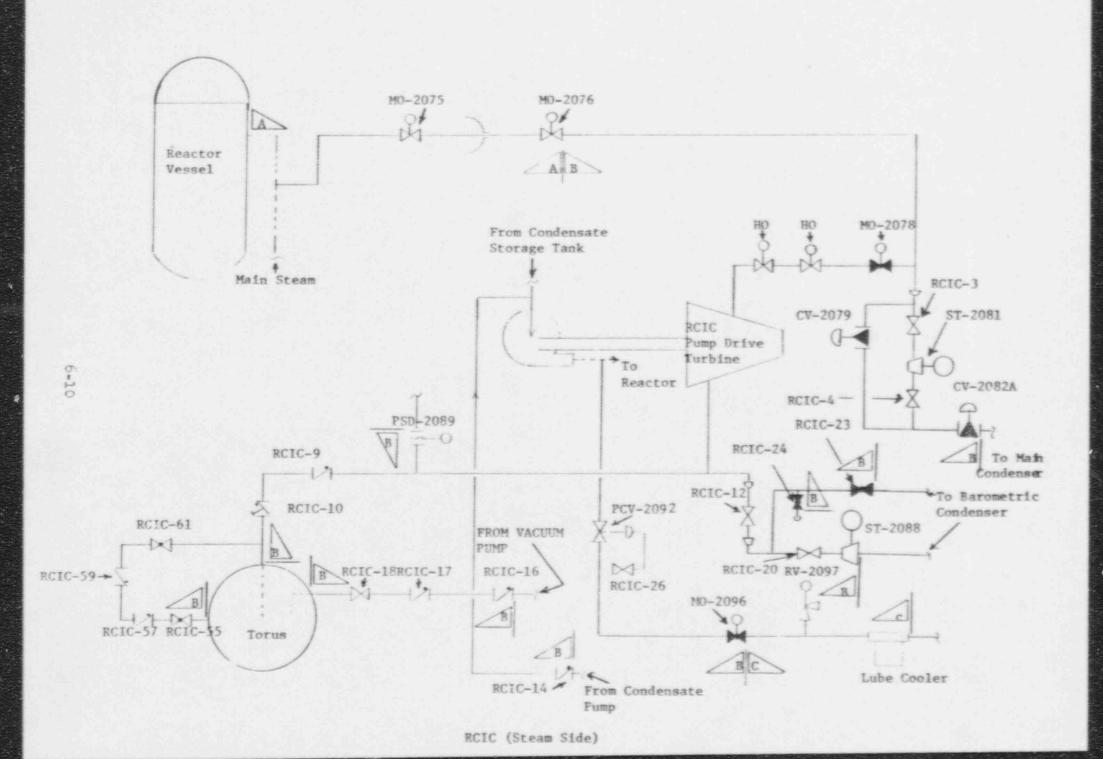




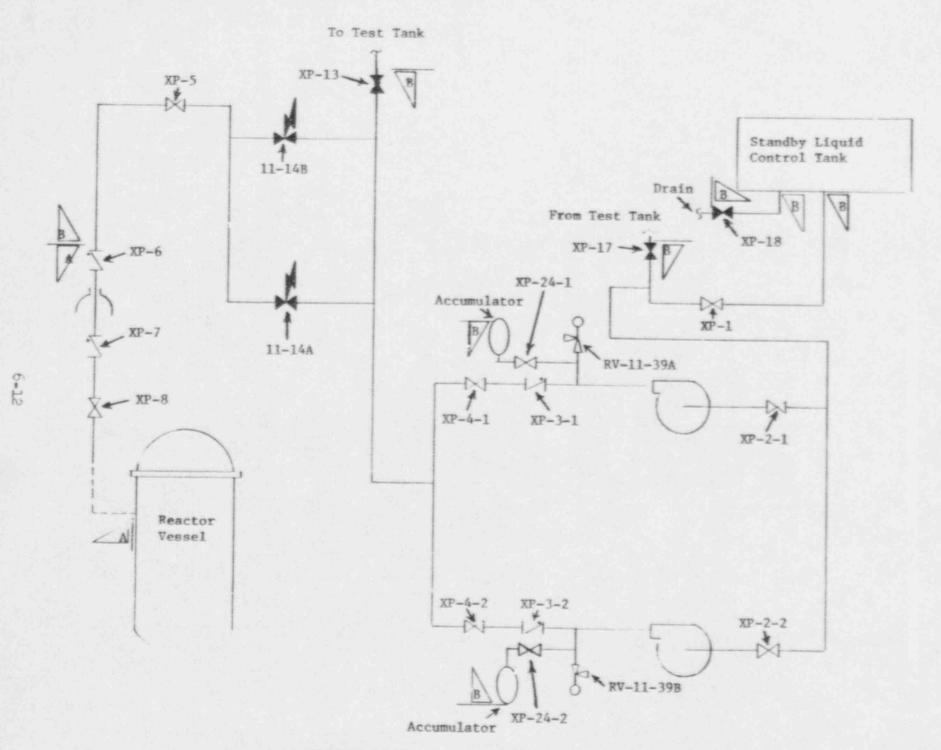


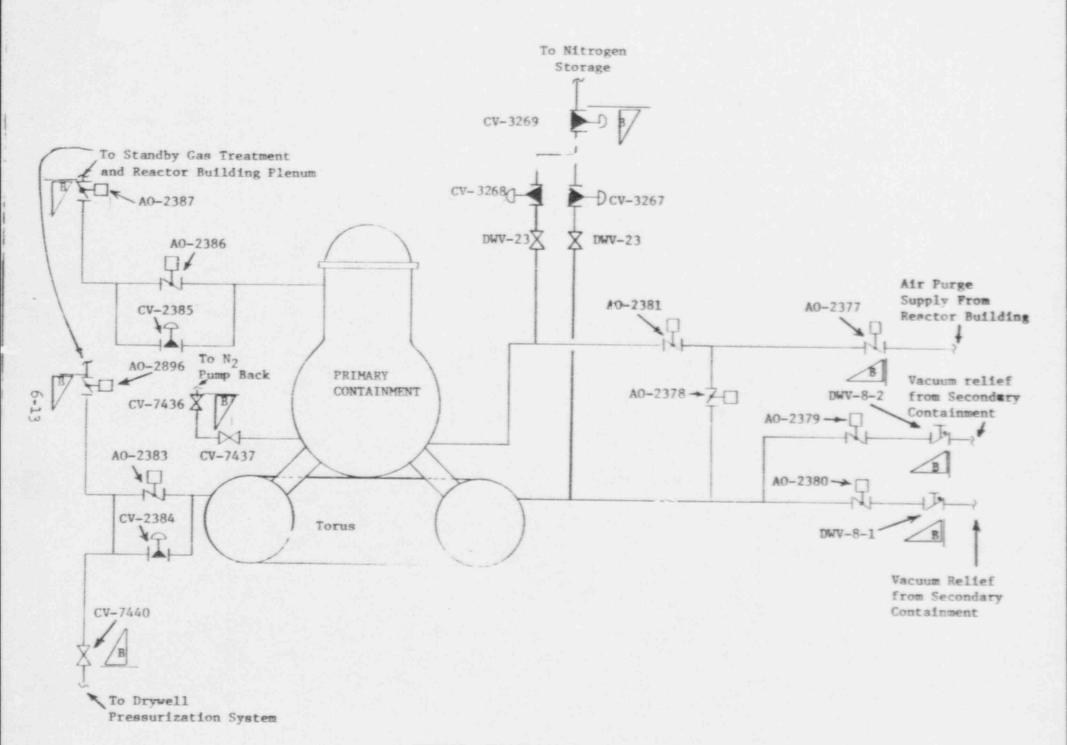


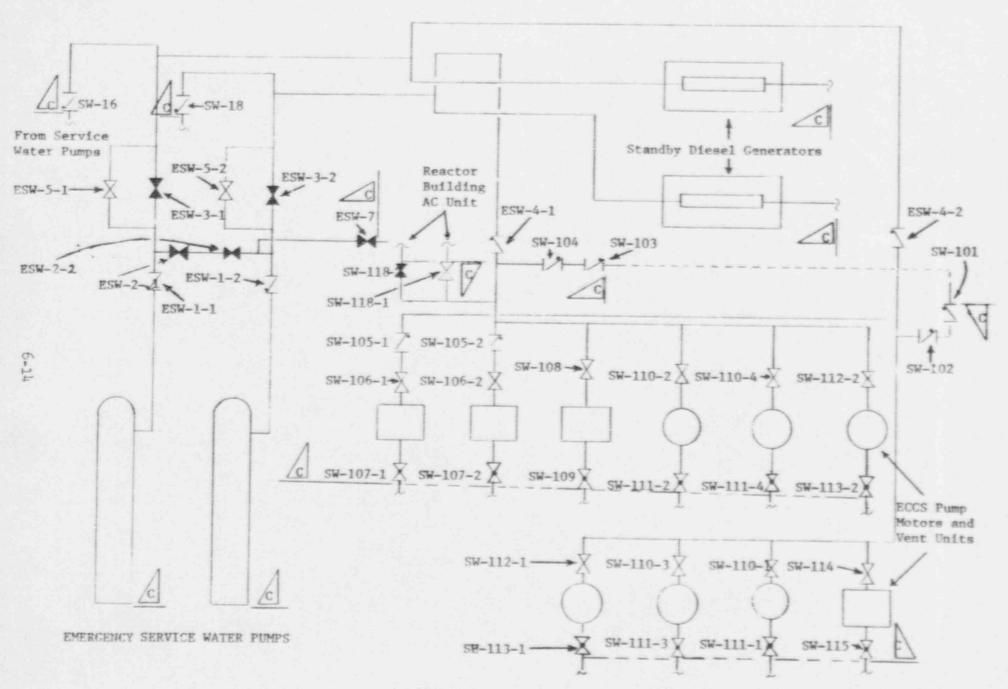




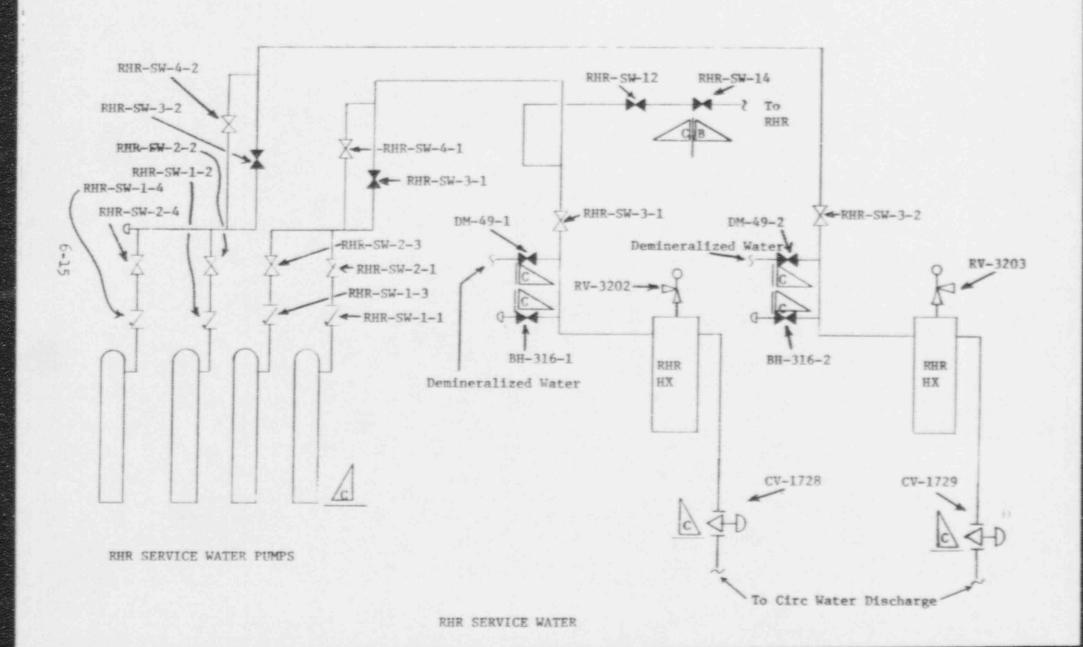
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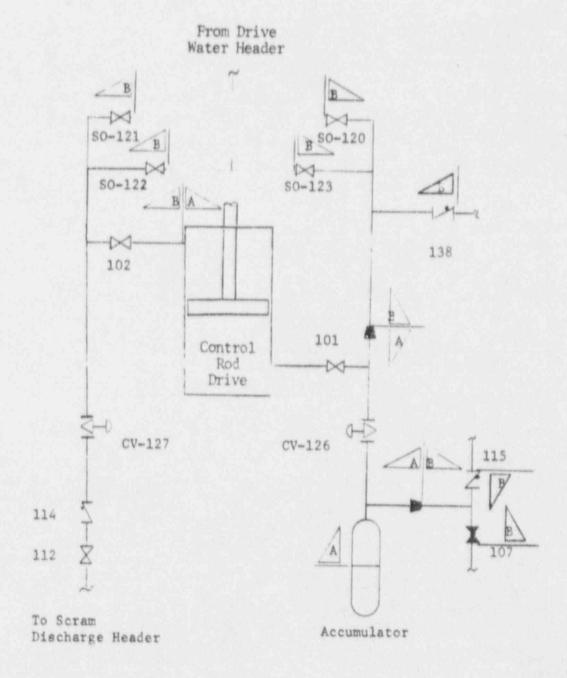


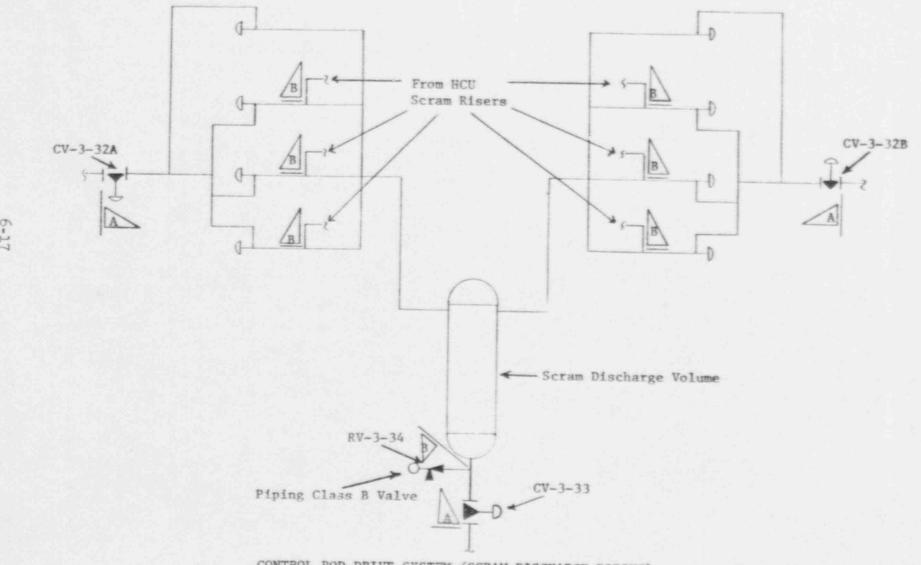


EMERGENCY SERVICE WATER

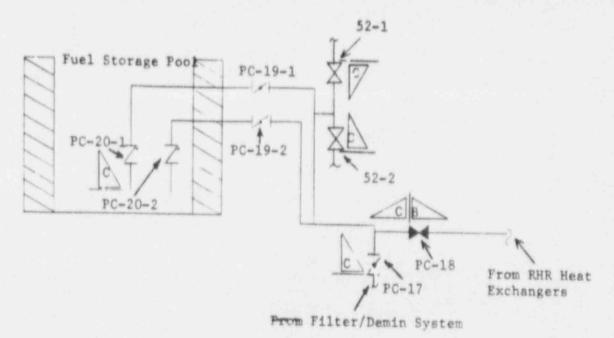


HYDRAULIC CONTROL UNIT (typical of 121)





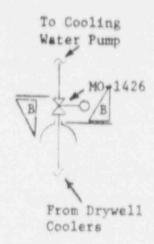
CONTROL ROD DRIVE SYSTEM (SCRAM DISCHARGE PIPING)

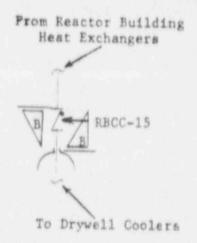


FUELPOOL COOLING & CLEAN-UP SYSTEM

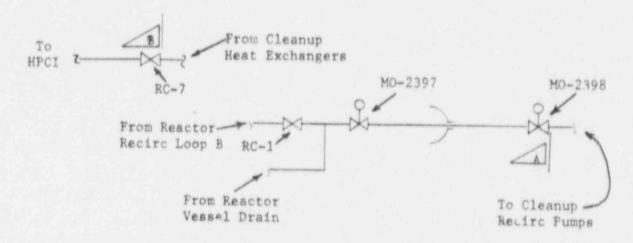
COMPRESSED AIR SYSTEM

CONDENSATE SERVICE SYSTEM

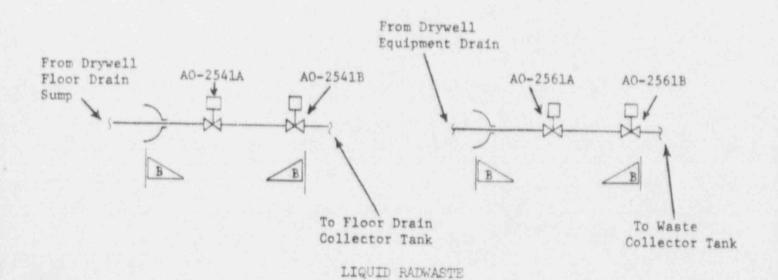


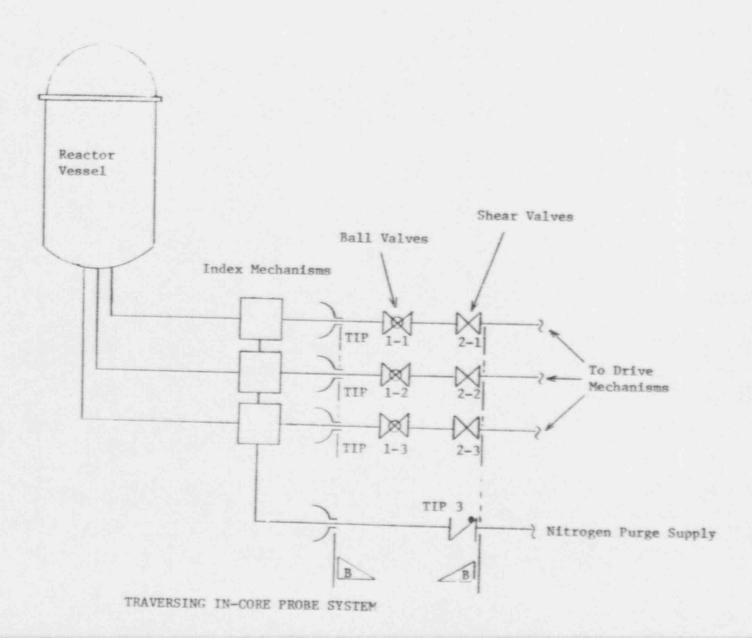


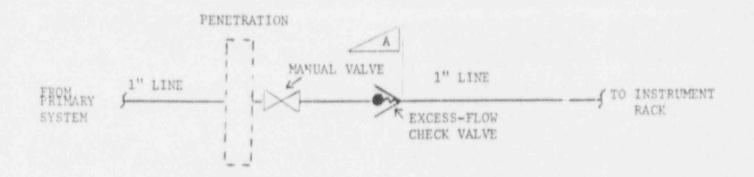
REACTOR BUILDING COOLING WATER SYSTEM



REACTOR WATER CLEAN-UP SYSTEM

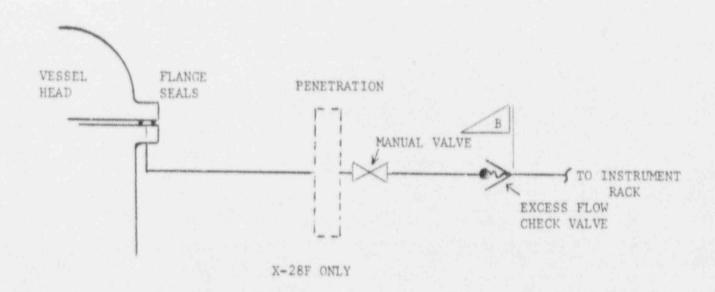






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TYPICAL OF X-27A THROUGH X-52F EXCEPT X-28F



EXCESS-FLOW CHECK VALVES