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William J. Cahill, Jr. Group Vice President

December 14, 1992

U. S. Nuclear Regulatory Commission Attention: Document Control Desk Washington, DC 20555

SUBJECT: COMANCHE PEAK STEAM ELECTRIC STATION (CPSES)
DOCKET NOS. 50-446 AND 50-446

ADVANCE FSAR SUBMITTAL, FSAR SECTION 3.8, LOADINGS AND STRESSES IN CATEGORY I STRUCTURES

Gentlemen:

The attachment to this letter provides an advance CPSES FSAR submittal to facilitate NRC Staff review of the subject area in support of licensing Unit 2. The attachment is organized as follows:

- 1. A description/justification of each change.
- A copy of the revised FSAR pages (changes are indicated in the margin by a revision bar and *87*).

The attached material will be incorporated in CPSES FSAR Amendment 87 which is currently scheduled for December, 1992. If you have any questions regarding this submittal, please contact Mr. Carl Corbin at (214) 812-8859.

Sincerely,

William J. Cahill, Jr.

D. R. Woodlan

Docket Licensing Manager

CBC Attachment

c - Mr. J. L. Milhoan, Region IV
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Mr. T. A. Bergman, NRR
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AMENDMENT / REVISION 87 DETAILED DESCRIPTION

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Prefix Page (as amended)

Group Description

3.8-121

Clarifies the discussion (3.8.4.3.3(2)) of allowable increase in local strength capacities.

Clarification :

This change is consistent with a similar change submitted for Section 3.8.4.3.2(2) in FSAR Amendment 68. For load combination 2.5.2) of Section 3.8.4.3.3, local stresses caused by concentrated load Wt (design tornado load) may exceed the allowables when there is no loss of function of any safety-related system. This change is consistent with the wording in the Standard Review Plan (NUREG-0800).

Change Request Number : SA-92-825.1

Commitment Register Number : Related SER : 3.8.3 SSER : SER/SSER Impact : No

Table 3.8-1

See Sheet No(s):1, 2, 3 and 4
Corrects the summary of loading combinations and stresses at key locations in the Category I Structures (Table 3.8-1, "Summary Table for Category 'I' Structures").
Correction:

The table is revised to correct typographic errors and an error in calculating the allowable and actual stresses in Unit 1. The table is also updated with Unit 2 information. The changes have no impact on available margins of existing structures.

Change Request Number : SA-92-825.2

Commitment Register Number :

Related SER: 3.8 SSER: 23 3.8.3

SER/SSER Impact : No

0&R 130-45

Updates response to discuss the changes in design criteria of Unit 2 in contrast with the criteria of Unit 1. Adds note to the response of Q130.34 indicating that the response will not be incorporated into the FSAR text as part of the updated FSAR (USAR). Q&R Incorporation:

There is no change in design criteria between Unit 1 and Unit 2. The design criteria for Units 1 and 2 is contained in the Section 3.8 of the FSAR text. The editorial note is added to prepare the Q&R section for deletion when the USAR is prepared.

Change Request Number : SA-92-825.3

Commitment Register Number : Related SER : 3.8 SSER : SER/SSER Impact : No

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- 4) .90 Y * D + L + Ta + Ra + 1.25 Pa + 1.0 (Yj + Yr + Ym) + 1.25 Feqo
- 5) .90 Y = D + L + Ta + Ra + 1.0 Pa + 1.0 (Yj + Yr + Ym) + 1.0 Fegs

In these combinations, thermal loads are neglected when they are secondary and self-limiting in nature and when the material is ductile.

In combinations shown in Items 2.a.3), 4), and 5), and in Items 2.b.3), 4), and 5) the maximum values of Pa, Ta, Ra, Yj, Yr, and Ym, including an appropriate dynamic factor, are used, unless a time history analysis is performed to justify otherwise. For combinations shown in Items 2.b.2), 4), and 5), local stresses caused by concentrated loads Yr, Yj, Ym, and Wt may exceed the allowables when there is no loss of function of any safety-related system. Furthermore, in computing the required section strength, the plastic section modulus of steel shapes is used.

3.8.4.3.4 Variable Loads

For loads which may vary, the values (within the possible range) which produce the most critical combination of loading are used in design.

3.8.4.3.5 Time Dependent Loads

Time dependent loads, such as the effects of creep, shrinkage, and other related effects, are included with dead load effects, as described in Section 9.3.7 of ACI 318-71 building code, where such loads affect design.

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Attachment to TXX-926

SUMMARY TABLE FOR CATEGORY 'I' STRUCTURES

	SUMMART IAS	LE FUR CATEGURY 1 STRUCTUR	(23)			to
TYPE			TYPE	ACTUAL	ALLOW	
OF.		CRITICAL	OF	STRESS	STRESS	×
STRUCTURE	KEY LOCATIONS (4)	LOADING COMBINATION	STRESS	(K\$1)	(KS1)	87 87 87
CONTAINMENT	Bottom of Containment	D+L+1.25 Pa+To+Ta+1.25E+	Tension	49.3	54.0	
BLDG.	Wall @ EL.805'-6"	Ra+Yr+Yj+Ym	Shear	13.6	50.0(2)	
	Top of Containment	D+L+1.25 Pa+To+Ta+1.25E+	Tension	54.0	54.0	
	Wall @ EL.1000'-6"	Ra+Yr+Yj+Ym				
	Inside Face of Equipment	D+L+1.5 Pa+To+Ta+Ra	Tension	54.0	54.0	
	Hatch at = 2250 for					87
	Unit 1, 3150 for Unit 2					87
REACTOR	Steam Generator Compartment	D+L+Ta+Ra+Pa+(Yr+Yj+Ym)+	Axial Tension	54.0	54.0	
BLDG.	#1.West Cavity Wall EL 863	Feqs	and Flexure			
			Transverse	0.087	0.101(3)	
			Shear			
	Steam Generator Upper Lateral	D+L+Ta+Ra+Pa+(Yr+Yj+Ym)+	Axial	20.6	45.0	
	Support Beam (Struct. Stl.)	Feqs	Compression &			
			Flexure			
			Shear	6.72	20.0	87

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SUMMARY TABLE FOR CATEGORY 'I' STRUCTURES

TYPE			TYPE	ACTUAL	ALLOW	×
OF		CRITICAL	OF	STRESS	STRESS	TXX-92601
STRUCTURE	KEY LOCATIONS	LOADING COMBINATION	STRESS	(KS1)	(K\$1)	601
AUXILIARY	5-A Wall East of F-A Above	0.75[1.4D+1.7L+1.9Feqo+	Flexure	54	54	E7
BLDG.	EL 790'-6"	1.7To+1.7Ro]	Shear(1)	25.5	51	87
FUEL BLOG.	C-F Wall Above EL 860'-0"	D+L+To+Ro+Wt	Flexure	37.8	54	
	South of col. Line 1-F		Shear(1)	37.2	51	į 87
	Bottom of A-F Wall Between	0.75[1.4D+1.7L+1.9Feqo+	Flexure	35.1	54	
	4-F and 2-F	1.7 To (W)]				
		D+L+To(W)+Ww	Shear	.047	.103(3)	
SAFEGUARDS	4-S Wall Below EL 610'-6"	0.75[1.4D+1.7L+1.9Feqo+	Flexure	48.6(U1)	54	87
BLDG.	for Unit 1, 13-S Wall	1.7To+1.7Ro]		38.9(U2)		87
	Below EL A10'-6" for Unit 2		Shear(1)	20.6(U1)	51	87
				29.2(U2)		87
	8-S Wall EL 810*-6"	0.75[1.4D+1.7L+1.9Feqo+	Flexure	54 (U1)	54	87
	for Unit 1, 9-S Wall	1.7To + 1.7Ro]		44.3(U2)		87
	Be'ween EL 773*-0" and	1.4D+1.7L+1.9 Feqo	Shear(1)	39.0(U1)	51	87
	790'-6" for Unit 2			41.8(U2)		87

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CPSES/FSAR TABLE 3.8-1 (Sheet 3)

SUMMARY TABLE FOR CATEGORY 'I' STRUCTURES

TYPE			TYPE	ACTUAL	ALLOW	
OF		CRITICAL	OF	STRESS	STRESS	
STRUCTURE	KEY LOCATIONS	LOADING COMBINATION	STRESS	(K\$1)	(K\$1)_	
SERVICE WATER INTAKE STRUCTURE	Bottom of North Exterior Wall EL .755*-0"	1.4D+1.7L+1.9Feqo	Flexure	53.2	54.0	
	Bottom of West Exterior Wall EL 755*-0"			53.7		
REFUELING	Base of the Circumferential	1.4D+1.7L+1.7+Hydro+	Flexure	52.4	54	77
WATER STOR.	Exterior Wall	1.9Feqo	Shear	.122	.126(3)	78
TANKS &						77
CONDENSATE						77
STOR. TANKS						77

87

77

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CPSES/FSAR TABLE 3.8-1 (Sheet 4)

SUMMARY TABLE FOR CATEGORY 'I' STRUCTURES

TYPE			TYPE	ACTUAL	ALLOW	92
OF		CRITICAL	OF	STRESS	STRESS	92601
STRUCTURE	KEY LOCATIONS	LOADING COMBINATION	STRESS	(KS1)_	(KS1).	
REACTOR	Base of the Circumferential	0.75[1.4D+1.7L+1.9Feqo+	Flexure	50.0	54	77
MAKE-UP	Exterior Wall	1.7To+1.7Ro]	Shear	.068	.090(3)	87
WATER						77
STOR. TANK						77
NOTES:						77
(1) Stress s	shown is for shear remforcing st	eel.				77

(2) 1" x 4" Bar Stock

(3) Concrete Shear Stress

(4) Unit 2 stesses are the same as Unit 1 stresses except as noted.

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CPSES/FSAR

Amend the appropriate sections of the FSAR to reflect the change in design criteria for Unit 2 in contrast with the criteria used for Unit 1.

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R130.34 There is no change in design criteria between Units 1 and 2.

Note: The above response will not be incorporated into the FSAR text as part of the Q&R relocation for the Updated Safety Analysis Report (USAR).