

Leadership in Science and Technology

August 19, 1992

Projucg

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Subject: Project 669

In response to your April 24, 1992 letter transmitting the Draft Safety Evaluation Report (DSER) for the Passive Plant Utility Requirements Document, Enclosure 1 provides a data base of the issues identified for Chapters 1, 1A and 12. This data base provides a "road map" for issue resolution. Hand-marked pages to Volume III of the Requirements Document are included for issues where changes are proposed to address NRC concerns.

Enclosure 2 provides a list of the issues in Chapters 1 and 1A which have responses outstanding (all Chapter 12 responses are provided). Our remaining responses for the DSER issues will be provided in the future. Please call John D. Trotter at 415/812-2810 if you have any questions.

Sincerely,

Bockhold

George Bockhold Jr. Senior Manager Advanced LWR Program

cc: J. Wilson/NRC

Enclosures: 2

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# Enclosure 1

Passive Plant DSER Issue Data Base

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### P.1.0-1

Status: Open

Next Action: ALWR

scope of mitigation requirements (2.1, 2.4)

Abstract (DSER, p 1.2-1) "It is not clear to the staff where EPRI places its "significant additional emphasis" on mitigation. There are many examples throughout the Passive Requirements Document about which the staff concludes that the passive plant design criteria place less emphasis on the mitigation of design-basis accidents (DBAs) than do criteria for current plants."	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER
(DSER, p 1.2-16) "However, it does not include requirements for fission-product control or hydrogen control during design-basis loss-of-coolant accidents. EPRI should either include these two issues or justify their exclusion."			

NRC Review

NRR/SPLB J. Kudrick

Last 8/18/92 Updated:

P.1.0-2	Status: Open	Next Action:	ALWR/NRC
egulatory treatment of non-safety-related systems (2.3.1, 4	1.3.1, 7, 10, 12.2.1, 12.2.3, Appendi	х В)	
Abstract DSER, p 1.2-3) "the requirement regarding a ion-safety-related onsite ac power source affects the eliability and availability of those non-safety-related active systems that provide defense-in-depth functions. This issue s enveloped for the passive designs under the issue pertaining to the regulatory treatment of non-safety-systems "	Industry Position See Policy Issue III.A	NPC Position (DSER) See Abstract	Action Description See Policy Issue III.A
DSER, p 1.4-2) "Since these important non-safety-related ystems are not required by EPRI to meet safety-grade riteria, the staff is trying to establish functional performance equirements, acceptance criteria, and other appropriate design uidelines to ensure that such systems have adequate unctional capability and will remain operable when called on. Therefore, the staff's positions on quality group classifications of specific structures, components, and equipment may not be available until the above criteria have been established."			
DSER, p 1.7-2) "The staff concludes that pertinent quality issurance provisions should be applied to these activities ind items. This issue is part of the overall issue regarding he regulatory treatment of non-safety-related systems for bassive plants"			NRC Review
DSER, p 1.12-3) "The specific staff positions on the inservice esting requirements for the essential non-safety-related components will be determined when the staff completes its eview of the issue of regulatory treatment of non-safety-grade systems."		NRR/ NRR/ NRR/ NRR/ NRR/	EMCB EMEB ESGB LHFB LOLB
DSER, p 1.12-11) "EPRI stated that the passive ALWR will ot have safety-related pumps and that the staff's positions ontained in the RAIs should not apply to non-safety-related umps. As discussed in Section 12.2.1 of Chapter 1 of this eport, the specific staff position on the inservice testing equirements for the essential non-safety-related components vill be determined when the staff completes its review of the egulatory treatment of non-safety-related systems."		NRR / NRR /	LPEB PDST PEPB PRAB PRPB RSGB SELB SICB SICB SPLB SRXB
		RES	ast 7/14/92

P.1.0-3

Status: Open

Next Action: NPC

automatic standby liquid control system for passive BWR design (2.3.2, Appendix B)

Abstract (DSER, p 1.2-9) "In its December 6, 1991, letter, EPRI stated that it has determined that automatic actuation of the SLCS was appropriate for evolutionary designs, and that it was modifying the Requirements Document for evolutionary plant designs to reflect that position. Although EPRI has not submitted its position regarding the automatic actuation of the SLCS for passive designs, the staff expects EPRI to provide	Industry Position The URD will be modified to require automatic SLCS. See Issue P.5.V-5	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
SLCS for passive designs, the staff expects EPRI to provide design requirements that are consistent with those for the evolutionary designs regarding this matter."			

NRC Review

NRR/SRXB M. Rubin

Last 8/6/92 Updated: а

Printed on: 8/18/92

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VOLUME III, CHAPTER 1, APPENDIX B:

### LICENSING AND REGULATORY REQUIREMENTS AND GUIDANCE

Section No.	er alle festartis mart som e ander som som		Rev.
2	PLANT OPTIM	PLANT OPTIMIZATION SUBJECTS	
2.1	INTRODUCTI	ON	0
	Plant optimiza tive criteria to available techn are provided in tion, discussio quirements Do optimization si	tion subjects are items for which the ALWR provides alterna- satisfy the underlying basis for the ALWR provides alterna- nology. The technical bases for plant uptimization subjects in plant optimization subject papers including the ALWR posi- on and assessment. The requirements identified in the Re- ocument are consistent with the positions taken in the plant ubject papers contained in this section	0
	LISTING OF O	PTIMIZATION SUBJECTS FOR THE PASSIVE ALWR	2
Section	Lead Chapter	Title	0
2.1.1	Chapter 1	Operating Basis Earthquake and Dynamic Analysis Methods	0
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### VOLUME III, CHAPTER 1, APPENDIX B: LICENSING AND REGULATORY REQUIREMENTS AND GUIDANCE

Section No.		Rev.
1		CALLER AND ADDRESS
\$5.5	ATWS MITIGATION FOR THE ADVANCED BWR	70
2.5.5.	ALWR POSITION	10
	The requirements for the Advanced BWR comply with the regulatory re- quirements for ATWS mitigation with the exception that the Standby Liq- vid Control System is manually initiated instead of automatically initiated. The Requirements Document provides requirements for the Advanced BWR that address the prevention and mitigation of ATWS as required by 10CFR50.62. The Advanced BWR is required to provide an alternate rod insertion system (ARI) that uses sensors and logic diverse and inde- pendent from the reactor protection system. In addition to the ARI, the Advanced BWR is required to provide both an electric and anydraulic in- sertion capability for the control rod drives. A standby liquid control sys- tem initiated by manual action is required to be provided. The Passive BWR operates with natural circulation, thereby eliminating the need for recirculation pumps. Since there are no recirculation pumps, the require- ments for an automatic pump trip are not applicable.	0
2.5.5.2	DISCUSSION	0
	A number of requirements for the Advanced EWR have been developed explicitly for the purpose of increased margins and reduced demands of engineered safety systems. Completed with a highly reliable reactor protection system and a CRD system with enhanced reliability, the sig- nificance of ATWS and its potential effects have been substantially reduced in the Advanced BWR. These requirements include:	0
	<ul> <li>More robust reactor coolant system design (e.g., larger water inven- tory) to accommodate transient conditions, thereby resulting i. fewer transients and challenges requiring actuation of the RPS.</li> </ul>	0
	<ul> <li>The reactor is required to have a negative power coefficient under all conditions.</li> </ul>	0
	<ul> <li>Large relief capacities are required to be provided for all plant condi- tions, including safety grade depressurization.</li> </ul>	0
	<ul> <li>A hydraulic CRD scram system that does not require a scrab dump volume is required for the Advanced BWR.</li> </ul>	0
	<ul> <li>The CRD bedraulic control units and associated rod pairs are divided into four independent scram groups. The combination of rods within each group are arranged so that hot shutdown can be achieved even in the event of failure to scram of an entire rod group.</li> </ul>	0

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### VOLUME III, CHAPTER 1, APPENDIX B: LICENSING AND REGULATORY REQUIREMENTS AND GUIDANCE

#### Section No.

2.5.5.2 -

#### DISCUSSION (CONTIFUED)

The electric insertion function is divided into three independent motor groups and the rods within the groups are arranged in a checker board pattern so that hot shutdown can be achieved even in the event of failure of any one motor group. Rev.

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In the event of a transient requiring scram in the Advanceo BWR, diverse means of achieving reactor shutdown have been provided. These include a hydraulic rod insertion system and an electric motor drive insertion system each of which can be initiated by the RPS or the API. The ARI provides signals to insert rods that are independent and diverse from the electrical RPS signals. The motor drives provide a mechanical diversity for rod insertion hydependent of the hydraulic portion of the CRD system. The ARI is in accordance with the requirement of 10CFR\$0.62(c)(3). The motor driven function provides CRD mechanical diversity to the hydraulic scram in addition to the electrical scram initiation diversity provided by the RPS and the ARI.

An additional diverse means of negative reactivity insertion is provided by the Standby Liquid Control (SLC) system. This system fulfills the requirements of General Design Criteria 26 for an independent reactivity control system of different design principals and has capacity in accordance with 10CFR50.62(c)(4). The need for initiating this system is significantly reduced by the enhanced reliability provided by the CRD system mechanical and electrical requirements for independence and diversity. The importance of automatic SLC initiation is significantly reduced by the enhanced reliability provided by the term hanced by the CRD system design features, thereby assuring the adequacy of manual initiation while still providing protection against the adverse consequences of an independence.

#### 2.5.5.3 ASSESSMENT

The ALWR program emphasis on nuclear safety, design simplification. man-machine interface, and increased margins assures that ATWS event frequency and consequences are very low.

The regulatory requirements of General Design Criteria 26 and 10CFR50.62 are fally addressed by the Advanced BWR requirements for independence and diversity in both the electrical and mechanical capublities of the CRD system and the Standby Liquid Control System.

Due to the increased margins, reduced demands on the reactor protection system, and the enhanced reliability of the CRD system by the provisions of the mechanical and electrical independence and diversity, the automatic initiation of the SLC as required by 10CFR50.62(c)(4) is not necessary for the Advanced BWR.

### VOLUME III, CHAPTER 1, APPENDIX B: LICENSING AND REGULATORY REQUIREMENTS AND GUIDANCE

	Rev.
ALWR Passive Plant Complinice	0
The specific requirements of CFR 50.62 are based on the assumption of specific designs. The reactor protection and auxiliary systems affecting reactor shutdown are substantially different in the passive ALMP design than in current LWR designs. Examples of features substantially different in the passive ALWR and which are referenced by CFR 50.62 are:	0
. The PWR design coes not include an auxiliary feedwater system.	o.
<ul> <li>The BWR derign does not include a recirculation system; it is designed for natural circulation.</li> </ul>	0
<ul> <li>The BWH control rod drive system has been completely redesigned with an electric motor rod drive system for normal reactor control and a hydraulic scram system without scram discharge volumes.</li> </ul>	0
Although an SLCS-will be previded for the SWR, the e-stem is designed to be manually initiated. See Section 2.5.5.	
The passive ALWR Integrated design considered ATWS as a basic design requirement and has provided a design which addresses the intent of CFR 50.62 by providing highly reliable and diverse reactivity control systems and an SLCS.	0
	<ul> <li>ALWR Passive Plant Compline ce</li> <li>The specific requirements of CFR 50.62 are based on the assumption of specific designs. The reactor protection and auxiliary systems affecting reactor shutdown are substantially different in the passive ALMR design. Examples of features substantially different in the passive ALMR design. Examples of features substantially different in the passive ALMR and which are referenced by CFR 50.62 are:</li> <li>The PWR design does not include an auxiliary feedwater system.</li> <li>The BWR derign does not include a recirculation system; it is designed for natural circulation.</li> <li>The BWH control rod drive system has been completely redesigned with an electric motor rod drive system for normal reactor control and a hydraulic scram system without scram discharge volumes.</li> <li>Although an SLCS will be previded for the BWR, the ensure is designed to be manually initiated. See Section 2.5.5.</li> <li>The passive ALWR Integrated design considered ATWS as a basic design requirement and has provided a design which addresses the intent of CFR 50.62 by providing highly reliable and diverse reactivity control systems and an SLCS.</li> </ul>

Requirement	Rationale	Rev.
COMMON REQUIREMENTS OF PSI AND PDHR SYSTEMS (CONTINUED)	COMMON REQUIREMENTS OF PSI AND PDHR SYSTEMS (CONTINUED)	с
<ul> <li>The designer shall identify all valves which are to be lock- ed in position and/or provided with position indication in the control room.</li> </ul>	<ul> <li>Certain critical valves will require locking and/or control room position indication.</li> </ul>	0
<ul> <li>Valve motors shall generally not be automatically stopped due to an electric overload except during valve operation- al testing.</li> </ul>	<ul> <li>To provide for the highest availability when required while still providing equipment protection during more frequent operational testing.</li> </ul>	0
DIVERSE REACTIVITY CONTROL SYSTEM	DIVERSE REACTIVITY CONTROL SYSTEM	0
A diverse reactivity control system that meets the applicable requirements of General Design Criterion (GDC) 26 shall be provided.	This function in the ALWR is provided by the standby liquid control system (SLCS) in the BWR and by the safety injection system (SIS) in the PWR. The normal reactivity control system is specified in Chapter 4.	0
	Requirements for ATWS events as specified in 10CFR50.62 prescribe the SLCS features for BWR plants with the currently used locking-piston drives; the BWR ALWR will utilize an electro-hydraulic drive. (See Chapter 4.) The electric motor drives will be used as the backup scram mechanisms to satis- ty ATWS requirements reduce the probability of on ATWS event and thereby reduce the probability of a required SLCS actuation.	0
	<ul> <li>COMMON REQUIREMENTS OF PSI AND PDHR SYSTEMS (CONTINUED)</li> <li>The designer shall identify all valves which are to be locked in position and/or provided with position indication in the control room.</li> <li>Valve motors shall generally not be automatically stopped due to an electric overload except during valve operation at testing.</li> <li>DIVERSE REACTIVITY CONTROL SYSTEM</li> <li>A diverse reactivity control system that meets the applicable requirements of General Design Criterion (GDC) 26 shall be provided.</li> </ul>	Requirement       Rationale         COMMON REQUIREMENTS OF PSI AND PDHR SYSTEMS (CONTINUED)       COMMON REQUIREMENTS OF PSI ANG PDHR SYSTEMS (CONTINUED)         • The designer shall identify all valves which are to be lock- ed in position and/or provided with position indication in the control room.       • Certain critical valves will require locking and/or control room position indication.         • Valve motors shall generally not be automatically stopped due to an electric overload except during valve operation- al testing.       • To provide for the highest availability when required while still providing equipment protection during more frequirements of General Design Criterion (GDC) 26 shall be provided.       • To provide for the highest availability when required while still providing equipment protection during more frequirements of General Design Criterion (GDC) 26 shall be provided.         • Makes reactivity control system that meets the applicable provided.       • To provide for the highest availability when required while still providing equipment protection during more frequirements of General Design Criterion (GDC) 26 shall be provided.       • To provide for the highest availability when required system (SLS) in the BWR and by the satisfy liquid control system (SLCS) in the BWR and by the satisfy liquid control system (SLCS) in the BWR and by the satisfy liquid control system (SLCS) features for BWR plants with the currently used locking piston drives; the BWR plants with the currently used locking piston drives; the BWR plants with the currently used locking piston drives; the BWR plants with the currently used locking piston drives; the BWR probability of on ATWS event and there by reduce the probability of a requireed SLCS actuation.

#### Paragraph No. Requirement Rationale Rev 4.4.2 Performance Requirements Performance Regulrements 0 4.4.2.1 The depressurization system shall be capable of depressuriz-The PSIS requires the reactor vessel to be depressurized to 13 ing the reactor vessel to the extent that drywell and reactor drywell pressure for PSIS injection. pressure reach equillbrium. The rate of depressurization shall not be excessively rapid so 4.4.2.2 The effects of a rapid depressurization rate (i.e., vessel 0 as to exceed the design limit on reactor vessel blowdowns mechanical stress and water carryover in the steam disand/cr cause excessive carryover of moisture and still assure charge) must be balanced against the additional complexity PSIS Injection before core uncovery can occur. of the depressurization system and the safety requirements of maintaining core coverage. System and Equipment Requirements 4.4.3 System and Equipment Requirements 0 4.4.3.1 The depressurization system shall work in conjunction with the The PSIS requires the reactor vessel to be decressurized to 0 drywell pressure for PSIS Injection. PSIS and shall have the same system initiating signals. 4.4.3.2 The DPS shall have appropriate redundancy of components Redundancy and ability to perform system requirements for 0 core cooling are required by criterion 35 of 10CFR50 Appenand features. The performance regulrement of no core damage, as specified in Section 2.3.6, shall be met, assuming dix A. an initiating event and the limiting single failure. 4.4.3.3 The depressurization valves shall work in conjunction with the Additional reactor vessel relief capacity may be needed G SRVs and ATWS Initiation signals to provide additional reactor during an ATWS event. vessel relief capacity if needed during an ATWS event. 4.4.3.4 Depressurization system actuation circuit continuity testing The ability to test actuation circuitry during power operation 0 capability during power operation shall be provided. enhances overall plant availability. 4.4.3.5 Depressurization system actuating devices shall be testable. If Surveillance testing is required to assure system function and 0 removal of the actuation device is required for testing, it shall avallability. 4.4.34 sy removal and replacement An automatic, DPS inhibit shall be provided to prevent dilution of the boron INSERT injection flow during an ATWS event. The inhibit shall be initiated by signals

**VOLUME III. CHAPTER 5: ENGINEERED SAFETY SYSTEMS** 

unique to an ATWS event and shall be compatible with the automatic SLCS injection specifi ed in section 4.5.

#### Rational:

While a DPS inhibit is not preferred it should be provided when low pressure injection flow from the PSIS would excessively dilute the SLCS boron flow and

Ph, 2 5.4-16

Paragraph No.	Requirement	Rationale	Rev.
4.4.3	System and Equipment Requirements (Continued)	System and Equipment Requirements (Continued)	0
4.4.3.¢ 7	The SRV and DPS valves shall be of designs that are sufficient- ly in tependent to avoid significant vulnerability to common cause failure.	Given the requirements of Section 4.4.3.2 for redundancy within the depressurization system, assuring independence in the manner in which the valves within each group functions will ensure negligible risk of failure to depressurize.	0

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<ul> <li>4.5 BWR STANDBY LIQUID CONTROL (SLC) SYSTEM</li> <li>4.5.1 Definition</li> <li>4.5.1 Scope</li> <li>This section, together with the applicable portions of Sections 2 and 3 of this chapter, provides the requirements for the BWR SLC system of the ALWR plant.</li> <li>The SLC system consists of a high pressure accumulator tank containing a liquid control chemical, piping, valves, and controls and instrumentation as shown in Figure 5.4.3.</li> <li>4.5.1.2 Functions the capability for</li> <li>The SLC system provides a means of inserting negative reactivity into the reactor core which is separate and diverse from the control rod system.</li> </ul>
<ul> <li>4.5.1 Definition</li> <li>4.5.1.1 Scope</li> <li>This section, together with the applicable portions of Sections 2 and 3 of this chapter, provides the requirements for the BWR SLC system of the ALWR plant.</li> <li>The SLC system consists of a high pressure accumulator tank containing a liquid control chemical, piping, valves, and controls and instrumentation as shown in Figure 5.4.3.</li> <li>4.5.1.2 Functions the capability for 0</li> <li>The SLC system provides a means of inserting negative reactivity into the reactor core which is separate and diverse from the control rod system.</li> </ul>
<ul> <li>4.5.1.1 Scope</li> <li>This section, together with the applicable portions of Sections 2 and 3 of this chapter, provides the requirements for the BWR SLC system of the ALWR plant.</li> <li>The SLC system consists of a high pressure accumulator tank containing a liquid control chemical, piping, valves, and controls and instrumentation as shown in Figure 5.4.3.</li> <li>4.5.1.2 Functions the cape billity for 0. The SLC system provides a means of inserting negative reactivity into the reactor core which is separate and diverse from the control rod system.</li> </ul>
This section, together with the applicable portions of Sections 2 and 3 of this chapter, provides the requirements for the BWR SLC system of the ALWR plant.       0         The SLC system consists of a high pressure accumulator tank containing a liquid control chemical, piping, valves, and controls and instrumentation as shown in Figure 5.4.3.       0         4.5.1.2       Functions the cape billity for       0         The SLC system provides a means of inserting negative reactivity into the reactor core which is separate and diverse from the control rod system.       0
<ul> <li>The SLC system consists of a high pressure accumulator tank containing a liquid control chemical, piping, valves, and controls and instrumentation as shown in Figure 5.4.3.</li> <li>4.5.1.2 Functions the capability for 0</li> <li>The SLC system provides a means of inserting negative reactivity into the reactor core which is separate and diverse from the control rod system.</li> </ul>
4.5.1.2 Functions the capability for 0 The SLC system provides a means of inserting negative reactivity into the preactor core which is separate and diverse from the control rod system.
The SLC system provides a means of inserting negative reactivity into the reactor core which is separate and diverse from the control rod system.
It provides reactor shutdown from full power operation to cold subcritical, with no assistance from control rod movement, by mixing a neutron absor ber with the primary reactor coolant. The system is used in the event that actual a sufficient number of control rods cannot be inserted to maintain sub- criticality. The SLCS is not required to shut down the reactor of to be a
. 4.5.1.3 :nterfaces 0
<ul> <li>The principal piping interface with the SLC is the reactor vessel (Chap- ter 4) into which the liquid control is injected; entry may be via one of the reactor coolant injection lines.</li> </ul>
<ul> <li>Plant electrical dc power systems (Chapter 11) are used to actuate 0 valves.</li> </ul>
<ul> <li>Monitoring of the system status and actuation signals are provided via 0 the instrumentation and control systems in Chapter 10.</li> </ul>
<ul> <li>The filter demineralizers of the reactor water cleanup system (Chapter 0</li> <li>3) shall be isolated coincident with an SLC injection initiation to avoid removal or dilution of pentaborate in the reactor.</li> </ul>
<ul> <li>The demineralized water supply system (Chapter 2) provides water 0 for the initial mixing of boron chemicals.</li> </ul>
<ul> <li>The plant high pressure nitrogen supply system (Chapter 7) provides 0 clean gas for mixing of the boron solution.</li> </ul>

Paragraph No.	Requirement	Rationale	Rev.
4.5.2	Performance Requirements	Performance Requirements	0
4.5.2.1	SLCS design shall meet the requirements for safety-related systems covered in Sections 2 and 3 of this chapter.	These requirements are ALWR design basis requirements.	0
4.5.2.2	The system shall have the capability for controlling the reac- tivity difference between the steady-state power operating con- dition at any time in core life and the cold shutdown condition.	The requirements are to assure the proper functioning of the system.	0
4.5.2.3	The minimum injection flow capability shall be sufficient to bring the reactor from full rated condition to cold shutdown with margin and hold it there while allowing for xenon decay. The injection flow rate and pressure, selection of injection loca- tion, and distribution system, if required, shall also ensure ade- quate mixing and distribution within the reactor for all design basis conditions.	The flow rate, boron content, and injection system design to meet the system functional requirements under conditions of the licensing design basis event will be established by the Plant Designer because it depends on plant size unique parameters.	0
4.5.2.4	Assuming failure of normal scram and the back-up electric motor drives while at normal operation, the system with injec- tion initiated by the counter shall be capable of maintaining (1) the reactor vessel below the emergency limit, (2) contain- ment below its design pressure, and (3) a coolable fuel geometry.	The SLCS provides a further back-up to the electric drives in the event of multiple failures (e.g., failure of normal scram, ARI and electric drives) and for severe accident protection. Automatic feedwater runtback as described in Chepter 2 Section 4.2.3.7 is provided as an additional ATWS mitigation feature.	0
4.5.2.5	The minimum liquid control storage capacity shall be sufficient to provide adequate margin when considering reactor coolant temperature, voids, Doppler effect, equilibrium and shutdown margin. An additional margin of 25 percent to be confirmed by the analyses specified in Section 4.5.2.6 shall be provided above calculated value to allow for mixing and distribution within the reactor system. Also, when determining the actual amount of sodium pentaborate needed, consideration shall be riber to dilution by the shutdown cooling system.	The basis given for the additional capacity margin is used in current designs and considers maldistribution of boron in the reactor system, the time required to homogeneity, and natural convection of the mixture as a function of its con- centration and temperature.	0

Page 5.4-20

Paragraph No.	Requirement	Rationale	Rev.
4.5.3.3	Arrangement	Arrangement	0
	The cocumulator tank and nitrogen supply, including nitrogen control valves, relier valves, and remotely actuated injection valves shall be located outside containment in an accessible area.	To facilitate testing and maintenance and for access during emergency situations.	0
4.5.3.4	Testing	Testing	0
4.5.3.4.1	The system shall include provisions for functional testing of components without contaminating the reactor system with boron solution during each refueling or planned outage.	The requirements are included to support the refueling out- age schedule and plant capacity factors specified in Chapter 1.	0
4.5.3.4 2	Provisions shall be made for sampling and chemical analysis of the liquid control solution during plant operation and shut- down.	Verification of solution concentration is required to ensure adequate shutdown margin. Sampling requirements in more detail are in Chapter 3.	0
4.5.3.5	Instrumentation and Control	Instrumentation and Control	0
4.5.3.5.1	The SLCS shall be capable of Initiation by manual operator ac- tion through a key teched switch in the main control room specifically designed to preclude inadvertent actuation	The need for automatic operation required by 100FR50.62 is baing met by the independent insertion capability of the electric motor drives of the electro-hydraulic control rod drives. (See Chapter 4.) The key lock is provided to prevent inadvertent operations.	) 0
4.5.3.5-2	The system shall be capable of operation in the event of loss of ac power, with a coincident most limiting single component failure. Electric power for operating components, including controls and instrumentation, shall be obtained from ap- propriately independent buses that are connectable to emer- gency dc power sources.	These requirements are necessary to meet the regulatory re- quirements for reliability. Heaters, if required to maintain the chemical solution above saturated temperature, would not be considered operating components and therefore would not need to be supplied from emergency power.	0
4.5.3.5	I The SLCS shall be automatically actuated on signals) which are unique to an ATH/S event. The automatic actuation logic shall be highly reliable and designed to avoid inadvertent operation. Manual initiation capability by direct operation action in the MCR shall be provided.	Automatic operation is required by 10 CFR 50.42. The design of the logic should balance the need for reliable actuation with the competin need to avoid spurious boron injection.	75

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Paragraph No.	Reguirement	Rationale	Rev
8.6.3	Integration and Coordination	Integration and Coordination	0
	The M-MIS for the Depressurization System shall be integrated and coordinated with the M-MIS for other plant systems as re- quired by 8.2.4. In particular, this includes:	It is expected that requirements on separation and segmenta- tion will result in very few direct connections between the Depressurization System M-MIS and other plant M-MIS. The performance requirements of Chapter 5 lead to the integra- tion and coordination defined in this requirement.	0
	<ul> <li>The conditions in the Reactor Coolant System;</li> </ul>		0
	<ul> <li>The M-MIS for the Passlv<sup>-</sup> Safety Injection System;</li> </ul>		0
	<ul> <li>For BWRs, the M-MIS for the overpressure protection of the Reactor Coolant System, i.e., the safety relief valves;</li> </ul>		Û
	<ul> <li>For PWRs, the M-MIS for the backup reactor trip portion of the Reactor Protection System, If provided.</li> </ul>		0
8.7	BWR STANDBY LIQUID CONTROL (SLC) SYSTEM	BWR STANDBY LIQUID CONTROL (SLC) SYSTEM	0
8.7.1	Functions	Functions	0
	The M-MIS for the SLC System shall provide the monitoring and control necessary to inject a solution containing a neutron absorber into the reactor coolant so that there is sufficient negative reactivity to bring the reactor to a cold subcritical condition without the control rods.	This allocation of functions is consistent with Section 4.5 of Chapter 5. monual initiation	0
8.7.2	Control and Monitoring Strategies Cofability	Control and Monitoring Strategies	0
	The SLC system shall be initiated, toby by direct operator ac- tion in the MCR. This operator action shall involve protective features which effectively preclude inadvertent actual on and assure that the Shift Supervisor concurs in the system actua- tion.	This is consistent with Section 4.5 of Chapter 5. The inadver- tent injection into the system would require substantial cleanup effort.	0

## VOLUME III, CHAPTER 10: MAN-MACHINE INTERFACE SYSTEMS

# VOLUME III, CHAPTER 10: MAN-MACHINE INTERFACE SYSTEMS

Peragraph No.	Requirement	Rationale	Rev.
8.7.3	Integration and Coordination Mutamatic initiation of	Antegration and Coordination	0
	The M-MIS for the SLC system will be integrated with the M- MIS design of other plant systems only as necessary to as- sure that adequate information is available from the neutron monitoring and rod control systems for the operator to deckde to use the SLC system. In addition, per Section 7.12.2.3, the RWCU system will isolate automatically upon actuation of the SLC system to ensure it does not remove the neutron absor- ber from the reactor coolant.	It is expected that there will be no direct connection between the SLC system M-MIS and other plant M-MIS except for the RWCU system M-MIS. End. that wighting the Curtomatic for Curtomatic Sicc	2
8.8	CONTAINMENT ISOLATION M-MIS	CONTAINMENT ISOLATION M-MIS	0
8.8.1	Functions	Functions	0
	The Containment Isolation M-MIS provides the control and monitoring necessary to isolate the containment to minimize the release of radioactivity to the environment.	This allocation of functions is consistent with Section 6.2 of Chapter 5.	0
8.8.2	Control and Monitoring Strategies	Control and Monitoring Strategies	0
8.8.2.1	Confirmation of Isolation Action	Confirmation of Isolation Action	0
	The containment isolation shall be initiated and accomplished without operator action. The operators shall be provided with a comprehensive operator aid (display) and appropriate con- trols which will allow them expeditiously and efficiently to:	Although the is, lation is automatic, the operators provide valuable backup. There are, however, many components involved in an isolation. Unless special steps are taken to aid the characteristic they will not provide an effective backup.	0
	<ul> <li>Contirm that the required isolation has been completed and to take manual action. If necessary, to complete the Isolation;</li> </ul>		0
	<ul> <li>The initiation of the isolation was based on information;</li> </ul>		0
	<ul> <li>Take manual control to return isolated systems to service when conditions permit.</li> </ul>		0
	Page 10.8-26		

P.1.0-4

III.B

Status: Open

Next Action: NRC

check valve categorization (2.3.2)

Abstract (DSER, p 1.2-10) "Treatment of check valves as active components would cause these valves to be evaluated more stringently than they were in previous licensing reviews."	Industry Position The ALWR program endorses ANSI-ANS 58.9-1981, "Single Failure Criteria for Light Water Reactor Safety Related Fluid Systms" which considers check-valves to be active components when they are required to change state to perform their safety function. The standard gives examples when the proper function of a component can be demonstrated despite any clauble condition. It requires documentation of the exemptions in the single failure analysis. Thus, the consideration of check valves in either active or passive failure will be made on a case by case basis by the plant designer.	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change (Ch 5)
	(Chapter 5, section 4.2.3.1.1 will be made consistent with Chapter 1, section 2.2 to clarify this point.)	N	NRC Review

Last 8/6/92 Updated:

aragraph No.	Requirement	Rationale	Aev.
4.2.2	Performance Requirements	Periormance Requirements	0
	The PSIS shall meet performance requirements as specified in Sections 2 and 3.	Section 2 provides top level <i>prevention</i> requirements; Section 3 provides PSIS requirements common to the BWR and PWR designs.	0
4.2.3	System and Equipment Requirements	System and Equipment Requirements	0
4.2.3.1	Arrangement	Arrangement	0
4.2.3.1.1	The PSIS shall be divided into an appropriate number of redun- dant components and features. As a minimum, the following shall be provided:	Separation of the PSIS into redundant components and fea- tures is required to meet regulatory requirements which re- quire accomplishment of the licensing design basis function assuming an initiating event and the limiting failure.	0
	<ul> <li>Multiple piping shall be provided for the core coolant makeup from the PSIS pool(s) and the suppression pool to the reactor vessel. They shall have sufficient redundan- cy and mechanical separation as specified in Section 2.</li> </ul>		0
	<ul> <li>Redundancy of components(i.e., valves, controls and in- strumentation) shall be provided as necessary to meet Section 2 requirements.</li> </ul>	<ul> <li>Redundant components provide single failure protection. Passive safety systems may include active features such as <del>check volves</del> instrumentation, and single-action val- ves which initiate systems operation (see Section 1.2.1.1).</li> </ul>	0
	<ul> <li>A single PSIS pool may be utilized. The total pool volume may be provided by a number of segments which are connected in such a way that they perform as a single unit.</li> </ul>		0

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### P.1.0-5

II.F

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Status: Open

### Next Action: NRC/ALWR

tornado wind speeds (4.5.2.5)

Abstract (DSER, p 1.4-21) "In the draft Commission paper on passive plant policy issues dated February 27, 1992, the staff stated	Industry Position The industry expects Commission endorsement of the wind-speed	NRC Position (DSER) See Abstract	Action Description NRC (Commission) review Policy on wind-speed.
that it will accept the tornado design basis of 300 mph recently proposed by EPRI. Table 1.4-1 shows the design-basis tornado parameters that are considered acceptable to the staff. However, until the staff resolves this issue with the Commission, it considers this to be an open issue"	Furthermore, we concur with site-specific evaluations of explosion and specific air-traffic patterns. However, criteria for general aircraft impact should be developed on a generic basis.		NRC/ALWA develop generic criteria for general airc: aft impact

NRC Review

NRR/PRPB J. Lee

Last 7/17/92 Updated:

P.1.0-6

II.D

Status: Open

Next Action: ALWR

leak before break (4.5.5)

Abstract (DSER, p 1.4-26) "The NRC staff concludes that EPRI must commit to and reference NUREG-1061 in the requirement section of Sections 4.5.5.2.2 and 4.5.5.2.4."	Industry Position See Policy II.D	NRC Position (DSER) See Abstract	Action Description See Policy II.D

NRC Review

NRR/EMEB D. Terao NRR/EMCB

Last 7/14/92 Updated:

P.1.0-7

Status: Open

Next Action: NPC

seismic evaluation and design of small-bore piping (4.7.3)

Abstract (DSER, p 1.4-42) "Pending completion of this review (of NCIG-14, EPRI NP-6628), the staff's position is that the methodology in EPRI NP-6628 is not acceptable."	Industry Position NRC should complete review	NRC Position (DSER) See Abstract	Action Description NRC to complete review

NRC Review

NRR/EMEE J. Brammer NRR/ESGB

Last 7/2/92 Updated:

P.1.0-8

Status: Open

Next Action: NPC

use of IEEE Standard 323 (4.8.2)

Abstract (DSER, p 1.4-49) "IEEE Standard 323, 1983 version, has not been found acceptable by the staff. Where differences exist between IEEE Standard 323 and 10 CFR 50.49, the designer must follow the NRC regulation, or identify and justify the differences for the staff to review. Therefore, the above statement in Section 4.8.2.1 of the Requirements Document is not acceptable. The phrase "as outlined in IEEE Standard 323" should be deleted from the sentence."	ER) See Abstract NRC to revisive response	ew this
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NRC Review

NRR/SPLB G. Hubbard

Last 8/6/92 Updated:

P.1.0-9

Status: Open

Next Action: NPC

method of environmental qualification of mechanical and electrical equipment (4.8.2)

quaincation should be in accordance with 10 CFH 50.49 (i).	Abstract (DSER, p 1.4-50) "Section 4.8.2 4 of Chapter 1 of the Requirements Document states that qualification vill be accomplished by physical test or by experience, demonstrating the equipment's similarity to previously qualified equipment or to equipment which has been exposed to other more severe environments. The staff finds that the above statement can easily be misinterpreted, and therefore, it needs to be clarified by stating that the method of qualification should be in accordance with 10 CFR 50.49 (f)."	Industry Position We agree. A URD change will be made to Section 4.8.2.4.	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
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NRC Review

NRR/SPLE G. Hubbard

Last 8/6/92 Updated:

aragraph No.	Requirement	Rationale	Rev.
4.8.2	Environmental Qualification of Mechanical and Electrical Equipment	Environmental Qualification of Mechanical and Electrical Equipment	0
4.8.2.1	The Plant Designer shall insure that mechanical and electrical equination of the equired for use in the operating environment under which it will be required to perform its design function. Mechanical equipment qualification shall meet the require- ments of applicable industry standards for the class of equip- ment involved. Class 1E electrical equipment shall be environ- mentally qualified in accordance with 10CFR50.49, as outlined in IEEE Standard 323.	This program is required to demonstrate that the equipment will perform its design function on demand to meet system performance requirements when subjected to the design en- vironmental conditions. Establishment of mechanical environ- mental qualification requirements is in a developmental stage. Industry standards current at the time of equipment qualifica- tion should be used.	0
4. 2.2	The Plant Designer shall make maximum use of provisions in other parts of Section 4.0 to remove excessive conservatisms from environmental analysis and to provide environmental en- velopes which closely match the calculated design conditions. Analyses performed to define the environmental envelope shall be completed after analysis variables have been finalized.	The most significant gains to be made in the area of environ- mental qualification are in the definition of more realistic en- vironmental envelopes for equipment qualification. Un- reasonably harsh environmental envelopes have greatly in- creased the costs of environmental qualification without a cor- responding increase in safety.	0
4.8.2.3	Pertinent environmental qualification parameters include, but are not necessarily limited to temperature, pressure, humidity, radiation, chemical spray and aging.	Elimination of unnecessarily conservative design scenarios will lessen such problems.	0
4.8.2.4	Qualification shall be accomplished by physical test or by ex- perience, demonstrating the equipment's similarity to pre- viously qualified equipment or to equipment which has been exposed to other more severe environments.	The use of proven equipment is the optimum approach to equipment qualification. Equipment which has undergone complete qualification tests and has demonstrated reliable service should be the primary choice.	0
	For Class IE electrical equipment, such		
	qualification shall follow the methodology stated in 10 °FA 50.43 (f) outlined		
	below: Page 1.4-48		

## VOLUME III, CHAPTER 1: OVERALL REQUIREMENTS

( see next fags)

- Testing an identical item of equipment under identical conditions or under similar conditions with a supporting analysis to show that the equipment to be qualified is acceptable.
- (2) Testing a similar item of equipment with a supporting analysis to show that the equipment to be qualified is acceptable.
- (3) Experience with identical or similar equipment under similar conditions with a supporting analysis to show that the equipment to be qualified is acceptable.
- (4) Amalysis in combination with partial type test data that supports the analytical assumptions and conclusions.

P.1.0-10

Status: Open

Next Action: NRC

limits on nitrites, nitrates, and total halogens as chlorine (5.2.8)

Abstract (DSER, p 1.5-7) "the staff concludes that EPRI should revise the Passive Requirements Document to include limits on nitrites, nitrates, and total halogens as chlorine. In addition, a total limit on total chlorine + total sulfur + total nitrite + total	Industry Position We are unaware on any technical basis for limits on nitritec and nitrates, NRC should explain technical requirement.	NRC Position (DSER) See Abstract	Action Description NRC to review response and continue dialog.
nitrate expressed as mole-equivalents of chlorine should also be included."			

NRC Review

NRR/EMCB G. orgiev

Last 7/2/92 Updated:

P. .0-11

Status: Open

Next Action: NPC

PWR water chemistry (5.5.2)

Abdaraci (DSER, p.1.5-26) "for PWR water chemistry, Section 5.5.2.4 of the Passive Requirements Document should reference EPRI NP-7077, Reminion 2, instead of EPRI NP-5960, Revision 1."	Industr: Position We agree. The URD will be revised to reference Revision 2, EPRI NP-7077, "PWR Primary Water Chemistry Guidlines" in Section 5.5.2.4.	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
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NRC Review

NRR/EMCB G. Georgiev

Last 8/6/92 Updated:

## VOLUME III, CHAPTER 1: OVERALL REQUIREMENTS

nued)         Water Chemistry Design Basis (Continued)           control values given in circulating piping (e.g.,         The current guidelines (1987 Revision) is directed toward op- timizing protection to the recirculation piping; in the ALWR.	0
control values given in The current guidelines (1987 Revision) is directed toward op- circulating piping (e.g., timizing protection to the recirculation piping; in the ALWR,	0
vessel lower plenum. which has no such piping, the maximum protection should be directed to the reactor vessel pressure boundary.	
n considering carbon nt service with less WC. The evaluation n buildup, and pitting The side effects of HWC must be considered in selection of materials. For example, in one plant, higher radiation levels (due to crud and cobalt) have been observed in some carb- on steel piping.	0
PWR Water Chemistry Design Basis	0
<ul> <li>PWR shall be in ac-</li> <li>The guidance for auxiliary systems in Table 1.5-4 are provided to assure compliance with the EPRI guidelines. Based on experience and the system and component design features xecified in the ALWR Requirements Document, the guidelines: Revision 2, revisions;</li> <li>provided in Table</li> </ul>	G
por or blar HV atic s th Suic visi	<ul> <li>recirculating piping (e.g., ponents, and other non- or vessel lower plenum.</li> <li>then considering carbon bank service with less HWC. The evaluation ation buildup, and pitting</li> <li>s</li> <li>the PWR shall be in ac- w</li> <li>w</li> <li>buidelines: Revision 2, ent revisions;</li> <li>res provided in Table</li> <li>the sprovided in Table</li> </ul>

\* : Revision 2, EPRI NP-7077

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#### Page 1.5-33

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Status: Open

Next Action: NRC

reliability assurance program framework (6.2)

Abstract (DSER, p 1.6-4) "The staff concludes that a RAP should contain and define the basic framework (scope, purpose, and objective) and the program elements, and should describe how the elements would be coplied to the plant structures, systems, and equipment."	Industry Position We believe the staff's concern was addressed by Revision 3 of Chapter 1, Section 6.	NRC Position (DSER) See Abstract	Action Description NRC to review Ch. 1, Section 6, Revision 3
(DSER, p 1.6-7) ", he staft concludes that a RAP should contain and define the basic framework (scope, purpose, and objective) and the program elements, and should describe how the elements would be applied to the plant structures, systems, and equipment."			

NRC Review

NRR/LPEB R. Correia

Last 7/2/92 Updated:

### P.1.0-13

Status: Open

Next Action: NPC

quantitative reliability and availability goals (6.2)

Abstract (DSER, p 1.6-5) "The staff concludes that a RAP should contain overall reliability and availability design goals based on safety requirements that have associated with them core-damage frequencies or probabilities. The staff agrees that plant availability, outage duration, and outage frequency are appropriate quantitative design requirements. However, quantitative reliability and availability requirements that will be responsive to those safety requirements that have associated with them core-damage frequencies or probabilities should also be included as design requirements for non-safety-related	Industry Position We believe the staff's concern was addressed by Revision 3 of Chapter 1, Section 6.	NRC Position (DSER) See Abstract	Action Description NRC to review Ch 1, Section 6
systems."			

NRC Review

NRR/LPEB R. Correia

Last 7/2/92 Updated:

P.1.0-14

Status: Open

Next Action: NRC

integration of reliability engineering techniques (6.2, 6.3, 6.4)

Abstract (DSER, p 1.6-6) "The staff concludes that a RAP should contain reliability engineering techniques performed during the design phase to ensure the overall design reliability and availability goals that are based on plant safety are met. The staff acknowledges that the techniques described in Section 6.2.3 of the Requirements Document are reliability program elements that will be applicable in the design phase of a plant and are acceptable. However, how these techniques	Industry Position We believe the staff's concern was addressed by Revision 3 of Chapter 1, Section 6.	NRC Position (DSER) See Abstract	Action Description NRC to re iew Ch 1, Section 6, Rev 3
will relate to the overall reliability program and how they will be integrated and considered in the RAP is not specified." (DSER, p 1.6-7) "The staff concludes that a RAP should contain reliability engineering techniques performed during the design phase to ensure the overall design reliability and availability goals will be met. As discussed above, the staff acknowledges that the techniques described in Section 6.2.3 of Chapter 1 of the Requirements Document are reliability program elements that are applicable in the design phase of a plant and are acceptable. However, as stated above, how these techniques will be instructed and considered in the			
<ul> <li>(DSER, p 1.6-8) "During its review of the Requirements Document, the staff found many of the elements of a RAP contained in other sections and chapters, such as Sections 2.3.3.7 and 2.3.3.8 of Chapter 1, Sections 2.2.12 and 3.4.5 of Chapter 5, and Section 6.1.6.3 of Chapter 10. However, as discussed above, EPRI did not state how these elements will be integrated and considered in the total reliability program."</li> </ul>		2	NRC Review NRR/LPEB R. Correia
			Last 7/2/92 Jpdated:

P.1.0-15

Status: Open

Next Action: NEC

relationship of system requirements to overall plant safety reliability and availability goals (6.2)

Abstract (DSER, p 1.6-6) "The staff concludes that the designer should establish a set of system reliability and availability goals to ensure that the overall reliability and availability goals that are based on plant safety will be met. The staff finds the requirements specified in Section 6.2.4 acceptable however, the connection of the system requirements to overall plant safety reliability and availability goals is not specified."	Industry Position We believe the staff's concern was addressed by Revision 3 of Chapter 1, Section 6.	NRC Position (DSER) See Abstract	Action Description NRC to review Ch 1, Section 6, Rev 3
sarely renability and evaluability goals is not specified.			물건 가지 가장

NAC Review

NRR/LPEB R. Correia

Last 7/2/92 Updated:

	ALWR/NRC OPEN ISSUES		
P.1.0-16	Status: Open	Next Action	* NRC
ifference between reliability assurance program for s	afety- and non-safety-related systems (6.3	3)	
Abstract	Industry Position	NRC Position	Action Description

NRC Review

NRR/LPEB R. Correia

Last 7/2/92 Updated:

P.1.0-17

Status: Open

Next Action: NRC

human factors considerations for operation and maintenance provisions (8.2)

Abstract (DSER, P.1.8-2) "In Section 8.2.8.4 of the DSER for Chapter 1, the staff recommended that IEEE P1023/D5, "Guide for the Application of Human Factors Engineering to Systems, Equipment, and Facilities of Nuclear Power Generating Stations," and EPRI 2360, "Human Factors Methods for Assessing and Enhancing Power Plant Maintainability," be inferenced in this section. The staff concludes that this recommendation is applicable to passive plant designs. These documents are not referenced in the Requirements Document "	Industry Position The URD will be changed (Section 8.2.1.2) to reference IEEE 1023 - 1988. Chapter 10, Section 3.7.7 contains a reference to EPRI NP-4350, "Human Engineering Design Guidelines for Maintainability", which in turn references the older report EPRI 2360, "Human Factors Methods for Assessing and Enhancing Power Plant Maintainability".	NAC Position (DSER) See Abstract	Action Desc NRC review pen change
Document."	Plant Maintainability".		- 1

NRC Review

NRR/LHFB D. Smith

Last 8/19/92 Updated:
## VOLUME III, CHAPTER 1: OVERALL REQUIREMENTS

Paragraph No.	Requirement	Rationale	Rev
8.2	PROVISIONS TO ENHANCE OPERABILITY AND MAINTAINABILITY	PROVISIONS TO ENHANCE OPERABILITY AND MAINTAINABILITY	0
8.2.1	Solution to Known Operations and Maintenance Problems	Solution to Known Operations and Maintenance Problems	0
8.2.1.1	The Plant Designer and Constructor shall document known operations and maintenance problems specific to the ALWR design and their solutions in a report available for Utility review prior to plant commitment. This report shall be based on review of the data sources listed in Table 1.8-1 and shall cover, as a minimum, the problem areas listed in Tables 1.8-2	Utility inputs on the ALWR Program have repeatedly stressed the need to systematically identify and resolve problems that exist in present plants. The Plant Designer is also en- couraged to look to foreign data sources (in addition to Table 1.8-1).	0
	and 1.8-3. The report shall cover all issues of plant perfor- mance and not be restricted to nuclear or non-nuclear equip- ment and shall be performed at a detailed enough level so that root causes can be determined and appropriate solutions prepared.	Based on a review of experience, a number of operation and maintenance problems that exist in the present nuclear plants can already be identified, and are listed in Tables 1.8-2 and 1.6-3.	
8.2.1.2	Human actors design principles shall be consistently applied throughout the design process for each operation or main- tenance work space in the ALWR plant to reduce operation and maintenance errors during all plant modes.	Human errors that affect plant performance may be system-, design-, or human-induced. Human factors applications focus on eliminating from the ALWR the causes of human er- rors that exist in the present plants. (Information on human errors can be found in many of the references of Table 1.8-1.)	0
8.2.2	Procedures and Training	Procedures and Training	0
8.2.2.1	Consistent with the standard plant design described in Section 11.5, procedures and training for operation and maintenance shall be standardized. A standard set of operating and main- tenance procedures and training shall be developed for each ALWR design. In addition, standardization between ALWR designs should be addressed to the extent practical.	A standardized set of procedures and training should permix achieving high quality and performance in operation and maintenance activities. It is recognized that there will be dif- ferences due to design-unique factors; however, stand- ardization to some degree between ALWR designs should be achievable through the utility/operations review described in Section 11.11.	0
THE IEEE .	1023-1388, quick for the Afflication of Human	- 1555 d la 103-1288 - 100 humi	deg
itos Enginea. iclea Paver	ng to Systems, Equipment, and Facilities of Page 1.8-2 Jonnating Stations will be unliged	I the it is a count hopen for	cen

P.1.0-18

Status: Open

Next Action: NRC

computer security reference (11.12)

Abstract (DSER, p 1.11-6) "Section 5.9 of Attachment 1 to Section 11 of Chapter 1 states: "The plant designer will certify the IMS security system in accordance with Guidelines for Computer Security and Accreditation (GUIDE 83)." GUIDE 83 does not appear to be a correct citation."	Industry Position The URD will be changed to eliminate the reference to "Guide 83"	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
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NRC Review

NRR/RSGB R. Dube

Last 8/6/92 Updated:

Printed on: 8/18/92

## ATTACHMENT 1 TO SECTION 11

Volume

Paragraph No.	Requirement	Rev.
5.8	QUALITY ASSURANCE	0
	The IMS shall be capable of automatically maintaining complete records of the design as it evolves. A method utilized to achieve this provision is described in Section 5.7.	0
	Rationale:	0
	Since design verification is achieved by peer design reviews which are recorded in the IMS, and the IMS is constructed to provide a single verified official traceable information source, the quality of the design can be demonstrated by appropriate IMS queries at any work station at any time.	0
5.9	COMPUTER AND NETWORK SECURITY	0
	An IMS security level, together with the methods utilized to achieve the desired risk level, shall be proposed by the Plant Designer for review and approval by the Plant Owner. The Plant Designer shall certify the IMS security system in accordance with Guidelines for Computer Security and Accreditation (GUIDE 83). The Plant Designer shall be responsible to maintain the securit for the IMS at the approved and certified level.	0
	Rationale: Delete (NBS FIPS PUB 102.) Add	0
	This requirement is intended to cover all aspects of security including un- authorized disclosures of information and data loss or contamination. There are a number of commercially applied methods to minimize com- puter system vulnerability to data loss or contamination. Since no system is absolutely safe, risk management involves analysis of risks, cost of recovery, cost of risk reduction, and acceptance of residual risk. Factors to be considered in a risk analysis are; the necessity of the system to function at a given level of performance, maintaining data accuracy and preserving continuity of operation. Plant Owner management must decide what performance level is required relative to what level of residual risk is acceptable. The Plant Designer is responsible to demonstrate that the proposed methods achieve the acceptable security level. Reference 2 provides more information on the subject of computer and network security.	2

Page 1.11-58

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P.1.C-1

Status: Confirm

Next Action: NRC

tornado wind speeds (4.5.2)

Abstract (DSER, p 1.4-21) "During a January 30, 1992, meeting with the staff, EPRI indicated that it would delete the reference to the tornado recurrence interval from the Requirements	Industry Position Agree. Changes will be made in Revision 4 of Volume III	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
Document. EPHI should revise rable 1.2-6 accoronigly.			[전화 13 46 <sup>11</sup> 24]

NRC Review

NRR/PRPB J. Lee

Last 8/6/92 Updated:

Printed on: 8/18/92

## Table 1.2-6

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# ENVELOPE OF ALWR PLANT SITE DESIGN PARAMETERS<sup>(1)</sup>

	Rev.
EXTREME WIND:	0
Basic wind speed:110 mph <sup>(2)</sup>	0
Importance factors: 1.0 <sup>(3)</sup> /1.11 <sup>(4)</sup>	0
TORNADO	0
<ul> <li>Maximum tornado wind speed:260 mph</li> </ul>	. 0
. Translational velocity 57 mph Maximum Rotational Speed: 240,	npho
· Radius: 1524 Maximum Translational Speed: 50 mpt	0
. Maximum etm dP 140 psid Radius of Maximum Rotational S	head isogr
· Bats of prossure change: 27 pst/sec. Maximum Remue Dirof : 2	e.e. si
Missile Spectra: SpectrumA of SRP 3.5.1.4)	0
. Missile Velocity: 35% of Maximum Horizontal Windspeed Rate of The	some Drop 1.2)
Missile Altitude: 00 ft above grade for large soft and large rigid mis- siles; all elevations for the small rigid missile.	<u>B</u>
SOIL PROPERTIES(8)	0
<ul> <li>Minimum Bearing Capacity demand: ≥ 15 ksf</li> </ul>	0
<ul> <li>Minimum Shear Wave Velocity: ≥ 1000 fps</li> </ul>	0
Liquefaction Potential: None	0
(at Site-Specific SSE Level)	0
SEISMOLOGY	0
<ul> <li>SSE PGA<sup>(9)</sup>: 0.30g<sup>(10)(11)</sup></li> </ul>	0
. SSE Design Response Spectra: per Reg. Guide 1.60	1
SSE Time History: Envelope SSE Response Spectra	0

## Table 1.2-6

## ENVELOPE OF ALWE PLANT SITE DESIGN PARAMETERS(1)

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	ATMOSPI	HERIC DISPER	SION (Chi/G	( <sup>13)</sup>			3		
							110		
Down Dista	nce	0-2 hr	0-8 hr	8-24 hr	1-4 day	4-30 day	3		
0.5 m	ile	1.0 E-3					3		
2.0 m	ile	-	1.35 E-4	1.0 E-4	5.4 E-5	2.2 E-5	3		
NOTE	S:						0		
(1)	Further de sequent cl and ill:	finition on appli hapters coverin	ication of sits g various are	design para as of design.	meters may be for For example, Vo	und in sub- lumes il	0		
		Chapter 6 Chapter 8 Chapter 9	Building Des Plant Cooling Site Support	ign and Arrar Water Syste Systems.	ngement ems				
(2)	50-year re	50-year recurrence interval.							
(3)	Importance factor to be used for non-safety-related structures as defined in ANSI A58.1-1982.								
(4)	Importance factor to be used for safety-related structures as defined in ANSI A58.1-1982.								
(5)	Probable maximum flood level (PMF), as defined in ANSI/ANS 2.8-1983, Deter- mining Design Basis Flooding at Power Reactor Sites. Minimum value to be basis of standard plant design with provisions as defined in Chapter 6 for ac- commodation of flood levels up to maximum value.								
(8)	Maximum of .32 as fo	value for 1 hour bund in Nationa	1 sq. mile P I Weather Se	MP with ratio rvice Publical	of 5 minutes to 1 tion HMR No. 52.	hour PMP	0		
1	P.000,000- ANSI/ANS plosions ar tion paper	year tornado re 2.3-1983. Pres e assumed to t on tornado des	currence inte sure effects a be non-contro ign for additi	eval with asso ssociated with olling for the onal information	ociated parameter in potential off-site design. See ALW ion.	s based on ex- R optiontza-	0		
(6)	Values of b assure wide be evaluate wide applic	earing capacity e application of of parametrical cation.	and shear w a standard r y against ran	vave velocity nat-type foun iges of possit	are included in the dation design. De ble soil properties	s table to asign must to verify	¢		

## Table 1.2-6

## ENVELOPE OF ALWR PLANT SITE DESIGN PARAMETERS<sup>(1)</sup>

Rev.

NOTES (CONTINUED):

×.

0	yes .	PGA	= Peak	Ground	Acceleration.
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()<sup>(6)</sup> Free-field at plant grade elevation.

10 (M) Envelopes all present U.S. nuclear sites except those on California coastline.

11 (14) The indicated ambient temperatures are to be used in accordance with requirements specified in the appropriate sections of Chapters 8 and 9.

12 (14) The ChillQ values are to be used for the 10CFR100 dose evaluation and were determined using meteorological data representative of an 80-90th percentile U.S. site. The ChillQ values were calculated following guidance in Regulatory Guide 1.145 considering ground level release, building wake (building area of 33,800 ft<sup>2</sup>), and lateral plume meander under stable atmospheric conditions.

P.1.C-2

Status: Confirm

Next Action: NRC

internal flooding design criteria (4.5.5)

(DSER, p 1.4-27) "The staff will confirm that EPRI will add information about internal flooding to Table 1.2-4 of Chapter 1 of the Requirements Document as committed to in a letter uated May 22, 1991." (DSER) See Abstract N Rev. 3 of Volume III	NRC to review Rev.3
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NRC Review

NRR/SPLB C. Li

Last 7/2/92 Updated:

Printed on: 8/18/92

P.1.C-3

Status: Confirm

Next Action: NPC

compliance with Regulatory Guides 1.26 and 1.29 (9)

Abstract (DSER, p 1.9-2) "the commitment to Regulatory Guides 1.26 and 1.29 is shown in Table B.1-2 as an optimization subject regarding the BWR main steamline isolation valves (MSIVs) and leakage control system, with Chapter 3 of the Requirements Document being listed as the lead chapter. The staff concludes that Table B.1-2 should clearly state that both of these regulatory guides will be complied with, with the exception of the MSIVs and leakage control system."	Industry Position The clarification of what the optimization issue aplies to is found in the text of Section 2.3.1 of Appendix B. That Section is referenced in Table B.1-2.	NRC Position (DSER) See Abstract	Action Description NRC to review this response.
			and the second

NRC Review

NRR/LPEB S. Magruder

Last 7/17/92 Updated:

Printed on: 8/18/92

Next Action: none

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P.1.V-1

See. 20

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6- E

Status: Closed(Cert)

implementation of design characteristics intended to enhance accident resistance (2.2)

Abstract (DSER, p 1.2-2) "Section 2.2 of Chapter 1 of the Passive Requirements Document specifies the ALWR design "haracteristics that are intended to enhance accident resistance, such as emphasizing simplification, providing ample design margin, using the best available materials and water chemistry, using the best proven diagnostic monitoring techniques, and maintaining a negative overall power reactivity coefficient under all conditions. Improved design margin is attained by the use of a 15-percent fuel design margin; lower core power densities; a larger reactor vessel, pressurizer, and steam generator secondary side; a longer transient rasponse time; and sufficient margins to limiting conditions for operation and reactor trip setpoints.	agree	Indurtry Position	(DSER) See Abstract	Action Description
The staff concludes that these design characteristic requirements are acceptable in principle. However, the staff will evaluate the acceptability of the implementation of each specific design characteristic during its review of an individual application for final design approval and design certification. "			N	NRC Review IRR/SRXB M. Rubin

Last 7/14/92 Updated:

Printed on: 3/18/92

P.1.V-2

Status: Open

Next Action: none

bounding analysis by standard site design parameters (2.3.1)

Abstract (DSER, p.1.2-4) "Among the general requirements, Section 2.3.1.8 of Chapter 1 addresses plant siting. Table 1.2.6 lists the envelope of standard site design parameters, for which the requirements are discussed in greater detail in Section 4.5.2 of Chapter 1. These siting parameters are intended to cover most, but not all, potential sites for future ALWRs in the United States. As such, the Passive Requirements Document requires that the plant designer review the conditions at the plant owner's site against the standard design siting parameters is order to assess the possible need for modification of any design parameter. Further, it requires that the final design parameters to be used for the particular site be approved in writing by the plant owner.	Industry Position Agree	NRC Position (DSER) See Abstract	Action Description
The results of staff's review of the envelope of standard site design parameters are given in Section 4.5.2 of this DSER chapter. In the DSER for Chapter 1 of the Requirements Document for evolutionary plant designs, the staff identified an open issue concerning worst-case site parameters. As for the final site design parameters to be used for any particular site, approval by the plant owner only is not sufficient. Approval by the NRC staff is also required. In addition, if one or more than one site-specific design parameter exceeds the standard site design parameters at some potential nuclear plant site, the plant owner should conduct a plant-specific evaluation against these parameters and submit a detailed review to the staff for approval. "		NI NI	NAC Review RR/PRPB J. Leg RR/ESGB

P.1.V-3

Status: Open

Next Action: NRC

selection of initiating events and their frequency categorization (2.3.2)

17		DIRA R	A STATE OF THE OWNER
(DSER, p 1.2-6) "The events and accidents in Table 1.2-1 of Chapter 1 are generally consistent with the initiating events described in Chapter 15 of the SRP with the following exceptions. Item 3.1, "reactor coolant pump trips (PWR)," should include both partial and complete reactor coolant pump trips (both are moderate-frequency events). Category 2, "decrease in heat removal by secondary system," should include steam pressure regulator failure and turbine trip without bypass as moderate frequency events. Item 6.1, "inadvertent opening of a pressurizer safety valve in a PWR or a safety or relief valve in a BWR," should continue to be categorized as a moderate-frequency event rather than an infrequent event. There are also certain acceptable exceptions because of the design features unique to the ALWR passive plants. For example, the recirculation pump trip and pump shaft seizure events for BWRs are not included in the list because there are no recirculation pumps in the passive BWRs. Control rod assembly malfunctions as passive BWRs may also be excluded if proper justification features, interlocks, and routine surveillance. However, because the Passive Requirements Document does not present an actual design, the staff concludes that there is insufficient justification to delete consideration of the rod drop event as an accident. The plant designer must justify the exclusion of BWR control rod assembly malfunctions from consideration in safety analyses during the design-specific review."	Table is not an inclusive listing of events to be considered in the safety analysic.	(DSER) See Absrract	NRC review this resulting

Last 3/18/92 Updated:

## P.1.V-4

Status: Closed(Cert)

Not Action: none

acceptance criteria for transient and accident analysis (2.3.2)

Abstract (DSER, p 1.2-8) "Section 2.3.2.7 of Chapter 1 states that the plant designer will perform a consequence analysis for moderate-frequency and infrequent events with coincident single failures and specifies the acceptance criteria for these events, including limiting faults as summarized in Table 1.2-2c. In Revision 2 of the Passive Requirements Document, EPBI added a footnote to Table 1.2-2c to specify fuel cladding failure criteria for input to the radiological consequence analyses. That is, for the PWR, the fuel cladding failure criteria will be less than the 95 05 departure from nucleate boiling ratio (DNBR) limit, and for the BWR, it will be less than the minimum critical power ratio (MCPR), except for (1) a LOCA event or (2) a fuel handling and cas drop event. For a LOCA, EPBI specifies that the vendo, should use the source term as defined in Section 2.5.2 of Appendix B to Chapter 1, and for a fuel handling and cask drop ovent, the vendor should use the number of assemblies involved. These failure criteria are consistent with the SRP, except for the source term for LOCA consequence analysis. Table 1.2-2c also specifies limits based on 10 CFR Part 20 and Appendix I to 10 CFR Part 50 for moderate-frequency and infrequent events, and specifies that, for PWRs, the radiological consequences of infrequent events may exceed	Agree	(DSER) See Austract	NRC Review
the guidelines of 10 CFR Part 20 but cannot be such that they to interrupt or restrict public use of those areas beyond the exclusion areas. The staff concludes that the EPRI-proposed criteria are not specific enough to determine if they are consistent with the staff's review criteria. The plant designer should specify the exact acceptance criteria and identify deviations from those in the SRP, if any, and the bases for the deviations. The staff will address this matter during its review of an individual application for final design approval and design certification."		MRR.	SKAB M. KUDIN

P.1.V-5

Status: Closed(Cert)

Next Actica: None

passive plant anticipated transient without scram response analysis (2.3.2)

Abstrac' (DSER, p 1.2-9) "Section 2.'3.2.2 of Chapter 1 of the Passive Requirements Document specifies that analysis and acceptance criteria for events involving failures of multiple active components associated with anticipated transients without scham (ATWS) and station blackhut will be in accordance with 10 CFR 50.62 and 10 CFR 50.63. respectively. However, 10 CFR 50.62 does not specify analysis and acceptance criteria, except for the prescriptive equipment design requirements that were based on analyses of the current generation of LWRs. The staff will require each plant dasigner to perform an analysis for the ATWS events to demonstrate that passive plant ATWS response is consistent with that considered by the staff in its formulation of the 10 CFR 50.62 design requirements for current plants. The staff	Industry Position Agree	NRC Position (DSER) See Abstract	Action Description
CFR 50.62 design requirements for current plants. The staff will address this matter during its review of an individual application for final design approval and design certification."			

NRC Review

NRR/SRXB M. Rubin

P.1.V-6

III.A

Status: Open

Next Action: ALWR/NRC

operator actions 72 hours after accident (2.3.2)

#### Abstract

(DSER, p 1.2-11) "Not only is the 72-hour the design basis for the safety systems, i justification for not requiring support syste for safety-related functions. These design consistent with the policies for passive Al Volume I of the Requirements Document. Passive Requirements Document does no justifications or bases to substantiate thes objectives. Since the safety systems are 72-hour duration after the initiation of accid on other non-safety-grade active systems core-damage prevention and mitigation fur the staff is concerned about the reliability these non-safety-prade active support sys 2.4.2.8 of Chapter 5 of the Passive Requi specifies that non-safety-related equipment plant recovery after the assumed 72-bour a be designed for the expected environment period. However, the Passive Requirement not identify which equipment will be need recovery after 72 hours and (2) continued a Although Chapter 3 of the Passive Require specifies that the active support systems defense-in-depth functions, such as reacto and decay heat removal functions, they are meet the requirements for safety-grade sy the Passive Requirements Document spec simple, unambiguous operator actions and accomplished offsite assistance will be ne hours to prevent fuel damage. However, t definition of what constitutes 'simple, una action and easily accomplished offsite ass

timeframe used as is also used as a ms to be designed bases are WRs stated in However, the provide sufficient e policies and designed for ents and may rely to perform ctions thereafter, and availability of tems. Section ements Document t necessary for ocident duration will during the 72-hour	Industry Position • One of the concerns of the staff's is "the reliability and availability of non-safety systems". See the Policy Issue for further discussion. • The other concern is about the plant recovery after 72 hours. The staff should consider the modifications made in the RAI response dated 8/16/91 to sections 2.2.11 and 2.2.15 of Chapter 5.	NRC Position (DSER) See Abstract	Action Description See III.A and also NRC to consider 8/16/91 response
its Document does of for (1) plant occident mitigation. ements Document			NRC Review
will provide		URR/	LOLB
r coolant makaup		NRR/	LPEB
stems in addition		NRR/	PDST
ities that only		NRR/	PEPB
l easily		NRR/	PRAB
cessary after 72		NRL/	PRPB
nere is no clear		NRR/	RSGB
istance ' "		NRE/	SELB
		NRR/	SICB
		NRR/	SPLB
		NRR/	SRXB
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Last 8/18/92 Updated:

P.1.V-7

111.A

Status: Open

Next Action: ALWR/NRC

use of 72-hour design basis (2.3.2)

		ITRA B LT	
(DSER, p 1.2-12) "Regulatory Guide 1.27, "Ultimate Heat Sink for Nuclear Power Plants," requires that a safety-related ultimate heat sink consisting of at laast two sources of water be provided with the capability to provide sufficient cooling for "at least 30 days" to permit simultaneous safe-shutdown and cooldown of all nuclear units that it serves and to maintain them in a safe-shutdown condition. Since PDHR systems provide a safety-grade means to transfer decay heat to the ultimate heat sinks, the requirement of a 72-hour capability for these systems is inconsistent with the 30-day capability of the safety-related ultimate heat sink specified in the regulatory guide.	See issue P.1.V-6	(DSER) See Abstract	see P.1.V-6
The staff will evaluate use of a 72-hour safety system design basis (i.e., requiring safety systems to be designed with 72-hour capability without reliance on operator action and other support system assistance) during its review of an individual specific application for final design approval and design certification. Each applicant must justify the use of the 72-hour timeframe design basis, the type of equipment and its quality and its availability for plant recovery after 72 hours,			NRC Review
and demonstrate that available non-safety-grade systems will provide for long-term cooling."			(*
provide for long term sooning.		DV PC PC	/LOLB
		NRE	(DDCT
		1000	(PPDD
		NDD	(DDAD
		ND D	(DDDD
		DIR P	(PCCD
		NTD D	(/RSGD
		17.9.10	/ SELD
		NTE E	CDID
		NPE	CRYB
		220	LI GRAD
		N.D.C	
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Pr	age 28	Print	ed on: 8/18/92

P.1.V-8

Status: Closed(Cert)

Next Action: None

technical basis for severe-accident management program and emergency operating procedures guidelines (2.3.4)

Abstract (DSER, p 1.2.16) "The staff concludes that EPRI's statements that the EOPs (or guidelines) will be provided by the plant designer as an integral part of the total plant design, will be based on detailed analyses of the functions and tasks of the operators, and will be verified and validated by active simulation is acceptable. If there are situations in which there is the potential for a human error of commission, the operators will be provided with procedural guidance and, if that is not sufficient, physical interlocks and inhibits will be incorporated in the design. Also, the procedures will not preclude operator action after the initiation of a passive system if that action can mitigate the consequences of an event; however, any such actions will have to be consistent with the need to permit safety system actuation to proceed to completion. Furthermore, such procedural guidance will have to be fully verified and validated.	Agree	NRC Position (DSER) See Abstract	Action Description
In addition, the normal plant design configuration limiting the ability to initiate overrides, along with the inclusion of unambiguous symptoms for manual control of safety systems, will limit the contribution of errors of commission to plant risk.			NRC Review
The staff concludes that these design objectives are acceptable. However, it will evaluate the technical bases for the severe accident management and EOP guidelines, and the design of acceptable means (i.e., hardware or software inhibits) to prevent operator override of safety system functions without unduly restricting the operators' ability to respond to system failures or unanticipated event progression during its review of an individual application for final design approval and design certification.		NRR/1	PRAB R. Palla

P.1.V-9

Status: Closed(Cert)

Next Action: none

acceptability of analytical codes and methodologies for safety analysis (2.5)

Abstract (DSER, p 1.2-17) "Acceptable analytical codes used for ALWR analyses must have the capability to handle system performance and phenomena unique to passive ALWR designs, such as operation of gravity-fed safety injection systems, natural circulation heat exchangers at both high and low pressures and in the presence of noncondensible gases, critical flow in the automatic depressurization valves over the range of expected operating conditions, boron transport under gravity-driven system conditions, and natural circulation stability of the simplified BWR design. The codes must also be capable of handling interactions among passive safety systems as well as active systems. The analytical methods and codes must be validated with appropriate test cata, including separate effects and integral effect tests with consideration of scaling effects. In its letter dated July 1, 1991, regarding the need for large-scah, full-height, and full-pressure integral testing of the passive safety systems, EPRI indicated that the ALWR Utility Steering Committee has established an analysis and testing review team, which is reviewing the detailed analysis and test plans for the passive	Industry Position Agree	(DSER) See Abstract	Action Description
plant designs and providing appropriate guidance. The staff			NRC Review
methodologies used for safety analyses as well as validation data, including test plans and facilities, during its review of an individual application for final design approval and design certification."		NRF	/SRXB M. Rubin

#### P.1.V-10

the systems and equipment to be designed to withstand a complete loss of bulk ac power for at least 2 hours without exceeding equipment design limits. The staff considers these design objectives as important defense-in-depth goals. Each of these requirements is acceptable provided the designer performs design-specific analyses to demonstrate that the

specified design limits are met. The staff will evaluate these analyses during its review of an individual application for final

design approval and design certification. \*

Statua: Closed(Cert)

Next Action: NRC/ALWR

defense-in-depth analysis (2.5, 3.5)

Abstract (DSER, p 1.3-3) "Section 3.5.3 of Chapter 1 requires that the plant responses to reactor trips, which are not complicated by failures beyond those that caused the trip, do not result (1) in the initiation of the emergency core cooling system, the primary safety or relief valve, or the backup feedwater system and (2) in the uncovering of uncovering the pressurizer heaters. Section 3.5.4 requires the plant to be capable of a turbine trip from 40 percent or loss (BWR) and 100 percent or less (PWR) of the rated power without reactor trip and the lifting of the main steam safety valves. Section 3.5.5 requires	Industry Position The URD asks that design limits for the plant's infrequent and moderate frequency vents are not exceeded without reliance on safety systems. This is not a licensing concerr and should not be a SER issue.	NRC Position (DSER) See Abstract	Action Description NRC to consider removal of this issue or continue discussion as needed.
that the inadvertent closure of the mainstream isolation valves (MSIVs) while at full power not result in the actuation of the safety/relief valves for BWRs. Section 3.5.6 requires that the loss of a running main feedwater or condensate pump while at full power not result in a reactor trip. Section 3.5.7 requires			

NRC Review

NRR/SRXB M. Rubin

P.1.V-11

Status: Closed(Cert)

Next Action: ALWR/NRC

60-year plant life (3.3, 4.8.2, 8.2, 11.3)

Abstract (DSER, p 1.3-1) "As stated in SECY-89-013, "Design Requirements Related to the Evolutionan; Advanced Light Water Reactors," the staff will review the ALWR designs for a 60-year life notwithstanding the fact that a 40-year license term limitation is specified in the Atomic Energy Act and NRC's regulations. Although the Commission paper was directed to the evolutionary designs, the staff concludes that it is equally applicable to the passive designs. It is the applicants' responsibility to identify the components and systems that are affected. The staff will address plant life during its review of an individual applications for final design approval and design certification. These applications will have to provide information and programs to support design life and the staff's reviews of such issues as fatigue, corrosion, and thermal aging."	Industry Position Section 11.3 was revised (Rev. 3) to better express the industry position. A design life plan shall be provided, which will include a design life classification system, condition monitoring and plant environmental monitoring. There is no contradiction with what the NRC staff is saying so there appears to be no issue.	NRC Position (DSER) See Abstract	Action Description ALWR/NRC discussion to clarity issue.
(DSER, p 1.4-50) "It should be noted that ALWRs are designed for 60 years of operation, while the current plants are designed for 40 years. The staff concludes that the plant designer should ensure that plant equipment important to safety must be qualified for its intended service, and be able to perform its safety functions throughout its design life. The staff will address this issue during its review of an individual application for final design approval and design certification."		NR® / PI	NRC Review

P.1.V-12

Status: Open

Next Action: NRC

operation of PWR with a secured reactor coolant pump (3.5)

Abstract [DSER, p 1.3-2] "Section 3.5.2 of Chapter 1 requires the PWR plant to be capable of operating at reduced power with a secured coolant pump to enhance the availability of the plant and to reduce reactor trips. Appendix B to Chapter 1 indicates EPRI's commitment to comply with Generic Letter (GL) 86-09, "Technical Resolution of Generic Issue No. B-59- (N-1) Loop Operation in BWRs and PWRs." GL 86-09 states that (N-1) loop operation is acceptable provided acceptable evaluation results are shown for certain plant-specific design characteristics, such as the impact of the down loop on instrumentation and control systems, human factors, operational systems, safety systems, status of valves, core-flew distribution, and potential for cold water reactivity insertion. Since these characteristics are highly dependent on the specific design of the plant, acceptability of operation with one secured reactor coolant pump is subject to plant-specific evaluation to address the concerns delineated in GL 86-09. The staff will evaluate that analysis during its review of an individual application for final design approval and design certification."	Industry Position The requirement about "being capable of operating at reduced power with a secured coolant pump" has been deleted (Rev 3). This issue should be closed.	NRC Position (DSER) See Abstract	Action Description NRC to review Rev. 3
			NRC Review

NRR/SRXB G. Hsii

P.1.V-13

Status: Closed(Cert)

Next Action: none

fuel burnup requirements (3.6)

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Abstract (DSER, p 1.3-3) "Section 3.6 of Chapter 1 requires ALWR core designs that have a capability of up to a 24-month fuei cycle and fuel mechanical designs that have a peak bundle burnup of at least 45,000 and 55,000 megawatt days per metric tons of uranium (MWD/MTU) for BWRs and PWRs, respectively. These minimum fuel burnup requirements are inconsistent with the EPRI-proposed requirements of 50,000 and 60,000 MWD/MTU specified in Sections 4.2.2.2 and 7.2.2.2 of Chapter 4 for BWRs and PWRs, respectively. In addition, although these specific values are inconsistent with each other, they are greater than NRC-approved fuel burnup levels. To support this high fuel burnup operation, each ALWR design applications will need to include sufficient high fuel burnup data to demonstrate fuel integrity in the areas of fissior gas release, cladding corrosion due to oxidation and hydriding, and reduction in cladding material strength."	Agree	Hidustry Position	(DSER) See Abstract	Action Description

NRC Review

NRR/SRXB G. Hsil

P.1.V-14

Staius: Closed(Cert)

Next Action: none

extended operating life of control blades and control rod assemblies (3.6)

Abstract (DSER, p 1.3-3) "Section 4.2.6.2 of Chapter 4 requires the BWR control blades used for maximum core insertion to be designed with a minimum exposure capability of 4.0E+21 neutrons/m2 (nvt) with a target of 8.0E+21 nvt, and the blades not used for maximum core insertion to be designed for an operating life of 13 or 20 reactor full-power years (RFPYs), which may be selected by the plant owner. Section 7.2.3 of Chapter 4 requires the PWR control rod assemblies to be designed for a minimum operating lifetime of 15 RFPYs with an objective of 20 RFPYs. These requirements are beyond the operating experience data of the current LWRs. To support the desired extended operating life of the control blades and control rod assemblies, each ALWR design application will need to include sufficient performance data to demonstrate that	Industry Position Agree	NRC Position (DSER) See Abstract	Action Description
include sufficient performance data to demonstrate that irradiation effects, including material hardening, absorber depletion, and swelling, will not impair structural integrity."			

NRC Review

NRR/SRXB G. Hsii

P.1.V-15

III.A

Status: Open

Next Action: ALWR/NRC

safety classification (4.3.1)

Abstract (DSER, p 1.4-2) "General Design Criterion (GDC) 1, "Quality Standards and Records," of 10 CFR Part 50, Appendix A, requires that nuclear power plant structures, systems, and components important to safety be designed, fabricated, erected, and tested to quality standards commensurate with the importance of the safety function to be performed. Regulatory Guide (RG) 1.26, "Quality Group Classification and Standards for Water, Steam, and Radioactive Waste Containing Components of Nuclear Power Plants," is the principal document used by the staff in its review of this subject. However, the ALWR Requirements Document proposes the use of ANSI/ANS 51.1, "Nuclear Safety Criteria for the Design of Stationary PWRs," and ANSI/ANS 52.1, "Nuclear Safety Criteria for the Design of Stationary BWRs" as an alternative way of complying with RG 1.26. The staff has not completely endorsed these two industry standards for the unique designs of the passive ALWRs, neither of these standards will be applicable to these plants. As discussed in Section 4.31 of Appendix B to Chapter 1 of the Passive Requirements Document, SRP Section 3.2.2, "System Quality Components Document, SRP Section 3.2.2, "System Quality	Industry Position See Policy Issue III.A	NRC Position (DSER) See Abstract	Action Description See Policy Issue III.A
applicable. Many of the passive systems that EPRI has classified as non-safety-related are similar to systems in current LWR designs are classified as safety-related. However, these passive plant non-safety-related systems are relied on to provide defense-in-depth capabilities to serve as the first line of defense in the event of transients and plant upsets to reduce challenges to the passive safety systems. Since these important non-safety-related systems are not required by EPRI to meet safety-grade criteria, the staff is trying to establish functional performance requirements, acceptance criteria, and other appropriate design guidelines to ensure that such systems have adequate functional capability and will remain operable when called on. Therefore, the staff's positions on quality group classifications of specific structures, components, and equipment may not be available until the above criteria have been established. In addition, in order for the staff to develop positions on quality group classifications, applicable piping and instrumentation diagrams should be available. However, this level of detail is not appropriate for the Requirements Document."		NRR/E Las Updated	MEB

## P.1.V-16

Status: Open

Next Action: NRC

seismic qualification by experience (4.3.2, 4.8.1)

Abstract (DSER, p 1.4-49) "Current NRC guidance (Regulatory Guide 1.100, Revision 2) recognizes the use of experience data as a means of seismic qualification of equipment. However, the earthquake experience data base methodology described in IEEE-344-1987 -which, as stated in Regulatory Guide 1.100, Revision 2, is to be evaluated by the staff on a case-by-case basis - is different from the detailed criteria and approach provided in the SQUG Generic Implementation Procedure (GIP). The staff does not accept the GIP as a qualification procedure. Rather, it is a verification procedure and is intended to be used only by the older operating plants under the A-46 resolution. Since the staff does not accept the GIP as a qualification procedure, it is not applicable to newer operating reactors or future AL WR plants. The development of the GIP verification procedures and criteria was not necessarily based on the required elements of IEEE 344-1987 or staff requirements for newer operating reactors. Thus, a significant portion of the data base in the A-46 methodology is not applicable to future ALWRs.	Industry Position The URD has been updated (Rev 2). In section 4.8.1.8, there is no longer a reference to SQUG but to Reg. Guide 1.100, Rev 2 and to the fact that the experience data method may require NRC evaluation for acceptance on a case by case basis. It is planned that an industry guideline document for using experience data will be developed under EPRI management. It will be submitted for NRC review and approval. This will then become the basis for approval in lieu of case by case approval.	NRC Position (DSER) See Abstract	Action Description NRC review Rev 2 and continue the dialog as necessary	
Therefore, consistent with RG 1.100, Revision 2, the staff will evaluate the use of experience data on a case-by-case basis for plant-specific applications (see Section 3 of Chapter 2 of this report for a specific application of experience data). "		NRR/	NRC Review ESGB	

Last 8/6/92 Updated:

P.1.V-17

Status: Open

Next Action: NPC

non-seismic building structures (4.3.2.3, 4.7.2.10)

Abstract (DSER, p 1.4-6) "Revision 0 of Section 4.3.2.3 of Chapter 1 of the Passive Requirements Document requires that non-seismic (NS) building structure the designed to the Zone 2A specification in the Uniform Building Code (UBC) with an importance factor of 1.25 assigned to the structures. In its letter dated April 24, 1991, the staff questioned the use of Zone 2A, which according to the UBC seismic zone map, is lower than the specifications for many regions in the United States. In its July 2, 1991, response, EPRI noted that the UBC Zone 2A specification is intended solely to provide a high degree of investment protection for NS items. However, since many regions in the United States are designated as UBC seismic Zone 2B or higher, the use of the Zone 2A specification in these zones is not acceptable for the design of any NS items. The staff will require the use of Zone 2B of the UBC in an application for final design approval and design certification."	Industry Position The requirements of Zone 2A are compatible with areas in which plants are expected to be sited. Zone 2B is too conservative. Furthermore, design of non-safety structures need not be NRC controlled.	NRC Position (DSER) See Abstract	Action Description NRC to reconsider position
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NRC Review

NRR/ESGB

Last 8/6/92 Updated:

## P.1.V-18

Status: Closed(Cert)

Next Action: none

structural design and construction codes (4.4, 4.4.1)

Abstract	Industry Position	I NRC Position	1 Action Description
(DSER, p 1.4-7) "Section 4.4 of Chapter 1 of the Passive Requirements Document provides EPRI-proposed requirements relative to the applicability of major design and construction codes, industry standards, and regulatory positions to the ALWR passive plant design. Tables 1.4-2 and 1.4-3 in Chapter 1 list industry technical standards and major structural design and construction codes, respectively, that are applicable to the ALWR. Several of these standards have not been endorsed by the staff and should not be used as the basis for plant design and construction. In its letter dated August 1, 1991, EPRI agreed to revise Section 4.4 to state that the use of applicable structural design and construction codes and industry standards that conflict with NRC positions will be resolved by the plant designer with the NRC and the resolution will be fully documented. The intent of this requirement was to ensure that the staff's reviews of applications for final design approval cnd design certification for passive plants will be conducted using acceptance criteria that include those codes and standards most recently approved by the NRC. In Revision 2 to Section 4.4 of Chapter 1, this requirement was revised in accordance with the staff's request. The staff concludes that this commitment is acceptable. The staff will evaluate this matter during its review of an individual EDA/DC or COI applications "	Agree	(DSER) See Abstract	NRC Review

P.1.V-19

I.M

Status: Open

Next Action: ALWR

elimination of operating-basis earthquake from design (4.4.3, 4.7.3, Appendix B)

Abstract (DSER, p. 1.4-10) "in SECY-90-016 and the draft policy paper on passive plants dated February 27, 1992, the staff stated that it agrees that the OBE should not control the design of safety-related systems. As a result, the staff is currently involved in the rulemaking plocess for Appendix A to 10 CFR Part 100 to decouple the OBE from the SEE in siting considerations. The staff is also evaluating the possibility of redefining the OBE in order to satisfy the OBE's function without explicitly analyzing responses. This change would diminish the role of the OBE in design by establishing a level that, if exceeded, would require that the plant be shut down for inspection activities. The staff agrees in principle with EPRI regarding the deletion of the OBE from plant design. However, certain issues related to the treatment of earthquake cycles for piping and equipment fatigue evaluations, seismic anchor motion effects, postulated pipe break location criteria, and concrete structure design need to be adequately resolved as a direct consequence of eliminating the OBE from design. The elimination of the OBE from design would require all current OBE design-related checks to be performed for the SSE. The staff is developing various alternatives with the industry to revise the codes and standards when design-related checks are based on the OBE. Resolution of these issues may result in staff recommendations for changes in applicable ASME Code, Section III rules. Therefore, the staff concludes that the elimination of the OBE from design is acceptable. However, the details of how current OBE-related design checks will be performed using the SSE will be resolved between industry and the staff through the appropriate code-related activities or supplemental regulatory guidance. The supplemental regulatory guidance could be in the form of revised SRP sections or the ITAAC (inspections, tests, analyses, and acceptance criteria). The elimination of the OBE from design approved. In the interi	Industry Position See Policy Issue I.M	(DSER) See Abstract	Action Description See Policy Issue I.M NRC Review ESGB
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		opuare	

P.1.V-20

Status: Open

Next Action: NRC

definition of support group (4.4.3)

Abstract (")SER, p 1.4-11) "Section 4.4.3.3.4 of Chapter 1 states that the plant designer may use approved independent support motion response spectrum analyses techniques as a basis for seismic design and identifies this use as an exception to SRP Section 3.9.2. "Dynamic Testing and Analysis of Systems, Components, and Equipment." The staff's position regarding a definition of "approved techniques" is that this method is only acceptable when use in accordance with the information and recommendations in Sections 2.3 and 2.4 of NUREG-1061, "Report of the U.S. NRC Piping Review Committee," Volume 4. As a part of this position, a support group is defined by supports that have the same time history input. This usually means all supports located on the same floor (or portions of a floor) of a structure. The staff concludes that Sections 4.4.3.3.4 and 4.7.3.4 of Chapter 1 should be revised to provide this commitment. In the interim, the staff will review individual applications for final design approval and design certification in accordance with be above position."	Industry Position Agree. A URD change will be made.	NRC Position (DSER) See Abstract	Action Description NRC review per & ink change
design certification in accordance with the above position.			

NRC Review

NRR/EMEB J. Brammer

Last 8/6/92 Updated:

Printed on: 8/18/92

## **VOLUME III, CHAPTER 1: OVERALL REQUIREMENTS**

raragraph No.	Requirement	Rationale	Rev.
4.4.3	Regulatory Positions (Continued)	Regulatory Positions (Continued)	0
4.4.3.3.1	The evaluation of the dynamic effects of pipe ruptures postu- lated in SRP 3.6.2 will not be performed for those systems or analyzable portions of systems successfully evaluated accord- ing to leak-before-break criteria. See Section 4.5.5.2 for specific criteria.	The ALWR approach is consistent with NRC's "Broad Scope" change to GDC 4.	2
4.4.3.3.2	The Plant Designer shall not combine seismic and pipe rup- ture events for systems in which LBB is demonstrated. This is in exception to SRP 3.9.3.	LBB demonstrates that pipe rupture will not occur due to sels- mic loads.	0
4.4.3.3.3	The Flant Designer shall use approved realistic damping criteria in the analyses of buildings, structures and equipment.	More realistic SSE damping values for piping systems will lead to significant improvements in equipment support design and spacing. Regulatory Guide 1.84 permits the use of damping values in accordance with ASME Code Case N- 411.	1
4.4.3.3.4	The Plant Designer may use approved independent support motion response spectrum analyses techniques as a basis for seismic design. This is in exception to SRP 3.9.2.	Envelope response spectrum analyses have been proven to be excessively conservative in many cases. (See $4.7.3.4$ )	×
4.4.3.3.5	The Plant Designer may use spectral shifting analyses as an al- ternative to spectrum broadening. This is in exception to SRP 3.9.2 and Regulatory Guide 1.122.	Broadened response spectra artificially increase the total energy input for analytical models. NRC has conditionally ac- cepted ASME Code Case N-397 specified for use on a case- by-case basis in Regulatory Guide 1.84. Code Case N-397 has been annulled and provisions inserted into ASME Section III, Subsection NCA, Appendix N.	2
4.4.3.3.6	In the analysis of vibratory loads with significant high frequen- cy input, the Plant Designer may combine high frequency modal results by algebraic combination. Non-linear analysis may be used to account for gaps between pipes and supports for such loadings. This is in exception to Regulatory Guides 1.92 and SRP 3.9.2.	This is consistent with the recommendation of NRC Piping Review Committee in NUREG-1061; however, the NRC staff position is that acceptance of algebraic combination would be on a case-by-case basis. It is anticipated that on-going re- search will refine the definition of the transition between low and high frequency ranges.	2

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Page 1.4-6

agraph No.	Requirement	Rationale	Re
4.7.3	Systems and Equipment (Continued)	Systems and Equipment (Continued)	0
4.7.3.3	The spectral peak shifting procedures of ASME Section III, Subsection NCA, Appendix N may be utilized for design of sys- tems with closely spaced structural modes and artificially broadened spectrum input. Modal and spatial components of response shall be combined in accordance with ASME III, Ap- pendix N, except that algebraic combination shall be used for the responses of modes above the ZPA cutoff frequency for loadings having significant high frequency content.	Spectral peak broadening can create overly conservative sels- mic energy input to the system when two or more structural modes fall within the broadened peak. While the spectral peak broadening analyses hay be appropriate for standard engineering designs, more sophisticated analyses are jus- tified for "as-built" analyses. Enveloped peak responses, rather than combined responses, more accurately reflect the response of the system since only one mode at a time will be excited at the peak of the artificially broadened range. Excep- tions to Regulatory Guides 1.92 and 1.122 will be required to implement these techniques; refer to Sections 4.4.3.3.5 and 4.4.3.3.6.	
4.7.3.4	Independent support motion response spectrum analyses, in- cluding appropriate seismic anchor motion (SAM), may be used in lieu of a single envelope of input at all supports in order to minimize excess conservatism when piping systems cross several building floor levels. When this methodology is used, the recommendations in NUREG-1061, Volume 2, Sec- tion 2.4, shall be followed.	Alternative procedures for evaluating multiple supported sys- tems are identified in NUREG/CR-3811. Grouping of spectrum input by attachment points mitigates the excess conservatisms present when an isolated higher elevation input dominates the analysis of the entire system. (Reference NUREG-1061, Vol. 4, Section 2.), a sufficient group as define flab that have the same time history unfut.	i ho
4.7.3.5	Stiffness and frequency requirements on piping support struc- tures shall be specified to justify the use of uncoupled dynamic analysis of piping. If physical limitations are such that these requirements make a design impractical, analytical models of the piping support structures may be included in the piping analysis.	ASCE Standard for Seismic Analysis of Safety-Related Nuclear Structures provides guidance concerning when in- tegrated analyses are appropriate. It should be noted that PVRC does not recommend use of support stiffnesses in piping models as a standard technique for all analyses.	
4.7.3.6	Equipment nozzle stiffnesses shall be appropriately con- sidered.	Equipment nozzle flexibilities should be explicitly modeled in piping analyses to reduce the calculated loads and to improve the moments at the nozzle. Care must be taken to avoid iterative analyses due to changes in erection and layout.	(

P.1.V-21

Status: Closed(Cert)

Next Action: none

use of Appendix N of ASME Code, Section III (4.4.3, 4.7.3)

Abstract (DSER, p 1.4-40) "ection 4.7.3.1 of Chapter 1 states that dynamic analysis techniques for safety class components will be in accordance with Appendix N of ASME Code, Section III. Appendix N is a nonmandatory appendix that is still evolving and does not currently agree with some staff positions. Therefore, it has not been endorsed by the staff, and the staff has no immediate plans to review this document. In its letter dated May 17, 1991, the staff requested EPRI to delete the reference to Appendix N and to reference applicable regulatory guides, Standard Review Plan sections, or staff-approved ASME Code Cases in the requirement portion of Section 4.7.3.1. In its letter dated August 1, 1991, EPRI stated that only the rationale portion of Section 4.7.3.1 would be changed and that this change would only address the use of Code Case N-397. The issue of Code Case N-397 is discussed in Section 4.4.3 of this report. Code Case N-397 is only one of several issues that are either currently in Appendix N or are being proposed for future addenda to this document and that have not been endorsed by the staff.	Industry Position Agree. Appendix N defines precisely the seismic analysis methodology. We understand that the NRC will analyze Appendix N within the FDA review, if referenced in a vendor's submittal.	NRC Position (DSER) See Abstract	Action Description
coefficient method, use of the independent support motion response spectrum method of analysis, and the			NRC Review
nonexceedance probability level in Subsection N-1725 of Appendix N. EPRI's response is not acceptable. Therefore, the staff will evaluate this issue during its review of an individual application for final design approval and design certification in accordance with applicable Slandard Review Plan sections in lieu of Appendix N to ASME Code, Section III."			NRR/EMEB J. Brammer

P.1.V-22

Status: Closed(Cert)

Next Action: none

analysis of vibratory loads with significant high-frequency input (4.4.3)

Abstract (DSER, p 1.4-12) "In Sections 4.4.3.3.6 and 4.7.3.3 of Chapter 1 and Section 2.1.1 of Appendix B to Chapter 1. EPRI states in various ways that in the analysis of vibratory loads (other than seismic) with significant high-frequency input (i.e., 33 to 100 Hz), the plant designer may combine high-frequency modal results by algebraic combination. This is a deviation from RG 1.92, "Combining Modal Desponses and Special Components in Seismic Response Analysis," that the staff currently evaluates on a case-by-case basis. In Revision 2 of the Passive Requirements Document, EPRI added a qualification to the rationale portion of Sections 4.4.3.3.6 and 4.7.3.3 of Chapter 1, and to Section 2.1.1 of Appendix B to Chapter 1. that indicates that in analyses of vibratory loads with high-frequency input, if high-frequency modal results are combined by algebraic combination, the staff will review the methodology on a case-by-case basis. However, the staff does not agree that the plant designer will necessarily treat the rationale as a requirement. Therefore, this same qualification should be added to the requirement pertion of Sections 4.4.3.3.6 and 4.7.3.3 of Chapter 1. Therefore, this same qualification should be added to the requirement	Industry Position • Agree it will be done on a case by case basis. • Modification of the URD is not needed because it's already written in Appendix B	NAC Position (DSER) See Abstract	Action Description
portion of Sections 4.4.3.3.6 and 4.7.3.3 in addition to Section 2.1.1 of Appendix B to Chapter 1. In the interim, the staff will review individual applications for final design approval and design certification in accordance with the above position."		NR	NRC Review R/EMEB J. Brammer

P.1.V-23

Status: Closed(Cert)

Next Action:

use of nonlinear analysis to account for gaps between pipes and piping supports (4.4.3)

required. The staff does not agree that merely identifying this procedure as an exception to the SRP is sufficient for a requirement. The staff position applies to the requirement portion of Sections 4.4.3.3.6 and 4.7.3.12 and to Section 2.1.1.2 of Appendix B to Chapter 1. Therefore, the staff will review individual applications for final design approval and design certification in accordance with the above position."	Abstract (DSER, p 1.4.12) "IIn its letter dated May 17, 1991, the staff requester: EPRI to revise the raquirement portion of Sections 4.4.3.3.6 and 4.7.3.12 of Chapter 1 and Section 2.1.1.2 of Appendix B to Chapter 1 to require that if nonlinear analyses are used to account for gaps between pipes and piping supports subjected to vibratory loads with high-frequency input, such analyses must be submitted to the staff for review and approval before they are used. In its response to this RAI, EPRI stated that since this procedure was identified as an exception to SRP Section 3.9.2 in the requirement portion of the above sections, no further changes were required. The staff does not agree that merely identifying this procedure as an exception to the SRP is sufficient for a requirement. The staff position applies to the requirement portion of Sections 4.4.3.3.6 and 4.7.3.12 and to Section 2.1.1.2 of Appendix B to Chapter 1. Therefore, the staff will review individual applications for final design approval and design certification in accordance with the above position."	Industry Position Agree it will be done on a case by case basis	NRC Position (DSER) See Abstract	Action Description
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NRC Review

NRR/EMEB J. Brammer

Last 8/6/92 Updated:

P.1.V-24

Status: Closed(Cert)

Next Action: none

probabilistic approach for changing existing loads and/or loading combinations (4.5.1)

Abstract	Industry Position	NRC Position	Action Description
(DSER, p 1.4.13) "Section 4.5.1 of Chapter 1 of the Passive Requirements Document provides general requirements for loads and conditions including natural phenomena, site proximity man-made hazards, plant operating loads, and in-plant hazards. Section 4.5.1.2 of Chapter 1 states that, on a case-by-case basis, the plant designer may, with the approval of the NRC, develo;) quantitative mechanistic design loads and combinations directly from design-basis events, using probabilistic methodology. The staff concludes that this is acceptable. However, it is not currently accepting a probabilistic approach as a basis for changing existing loads and/or loading combinations, and the loading combinations recommended in SRP Sections 3.7, 3.8, and 3.9 remain valid.	Agree	(DSER) See Abstract	
The staff will address this issue during its review of an individual application for final design approval and design certification."			

NRC Review

NRR/EMEB J. Brammer

P.1.V-25

Status: Open

Next Action: NRC

recurrence interval for wind loadings (4.5.2.1)

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(DSER, p 1.4-14) "The use of importance factor 1.11 for adjusting the recurrence interval from 50 to 100 years is suitable for the design of safety related structures because the application of an importance factor of 1,11 to calculate the wind speed for a 100-year recurrence interval is equivalent to the guidance in SRP Section 3.3.1, "Wind Loadings." For non safety related struc tures, the use of a 1.0 importance factor implies ' it a 50 year recurrence interval is suit able Howev he staff's interpretation of ANSI A58.1 1982 is that an extreme wind associated with a 50 year recurrence interval is suitable to calculate the wind speed only for Category I and IV structures. Since non-safety-related structures in an ALWR plant are more important than Category IV structures, the staff concludes that both safetyand non-safety-related structures should be designed for an extreme w. J associated with a 100 year recurrence interval. The importance factor of 1.0 is not acceptable for non-safety-related structures that are important to safety (e.g., turbine building). EPRI has not provided adequate justification for its position. Therefore, the staff will address this item during its review of an individual application for final design approval and design certification."

Industry Position NRC Position Action Description Consistent with the relative (DSER) See Abstract NRC to review this importance of the safety related and response non-safety related structures. different importance factors are proposed for the two classes of structures. It is noted that the 110 mph extreme wind speed specified in Chapter 1, Table 1.2-6, is extremely conservative for most of the potential sites. The specification of 110 mph as the design wind speed with the appropriate importance factors provides a conservagtive design basis for both the safety related aa well as the non-safety related structures.

NRC Review

NRR/PRPB J. Lee
P.1.V-26

Status: Open

Next Action: ALWR

maximum ground water level (4.5.2.2)

Abstract (DSER, p 1.4-15) "Maximum ground water level The Passive Requirements Dccument requires the maximum ground water level to be 2 foot below grade. This requirement is not acceptable; the maximum ground water level should be at grade. EPRI has not provided adequate justification for its position. Therefore, the staff will address this item during its review of an individual application for final design approval and design certification."	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER
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**NRC Review** 

NRR/ESGB

Last 6/18/92 Updated:

P.1.V-27

Status: Open

Next Action: ALWR

precipitation for roof design (4.5.2.2)

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Abstract (DSER, p 1.4-15) "Precipitation (for roof design) - The Passive Requirements Document specified a maximum rainfall rate of 10 in./hr and a maximum snow load of 50 pounds per square foot (psf). In the DSER dated September 1987 on Chapter 1 of the Requirements Document for evolutionary plants, the staff raised a concern that the rainfall rate of 10 in./hr was much too low, citing that the probable maximum precipitation (PMP) in a five-minute interval over one square mile is 6.3 inches at the Great Lakes area and 6.2 inches along the Gulf Coast. The revised Table 1.2-6 specifies a higher 1-square mile, 1-hour PMP of 19.4 inches, together with a 1-square-mile, 5-minute PMP of 6.2 inches. The 5-minute PMP value appears reasonable; however, that might exclude a number of Great Lakes area sites. EPRI should use the SRP guidelines and relevant RGs for developing an adequate structural and flood-prevention design basis for the PMP. EPRI has not provided adequate justification for its position. Therefore, the staff will address this item during its review of application for final design approval and design	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Helpend to DSER	
an individual application for final design approval and design certification."			NRC Review	

NRR/PRPB J. Lee

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Last 8/18/92 Updated:

	Next Action: ALWR		(DSEP) See Abstract (ALWR) Respond to DSER	NRC Review	NRR/PRPB J. Lee		1 ast 8/18/92 Updated:	Printed on: R/18/92
R/NEC OPEN ISSUES	Status: Open		Industry Position					48
ALWI	P.1.V-28	snow loading (4.5.2.2)	Abstract (DSER, p 1.4-16) "In the DSER dated September 1987 on Chaoter 1 of the Fiequirements Document for evolutionary plants, the staff stated that the 50-pst snow load might limit sites to below 38" north latitude in some regions, citing, for example, the 69-pst snow load and 72-psf snow plus ice load that were used in the design of the Beaver Valley plant. However, in Table 1.2-6 of Chapter 1 of the Passive Requirements Document, the 50 psf snow load was retained. The staff concludes that this snow load is unacceptable. EPRI has not provided adequate justification for its position. Therefore, the staff will address this item during its review of an individual application for final design approval and design certification."					Page

# P.1.V-29

Status: Closed(COL)

Next Action: none

detailed quantification of soil parameters (4.5.2.3)

Abstract (DSER, p 1.4-16) "In its letter dated April 24, 1991, the s aff indicated that Table 1.2.6 should give a range of soil properties to provide consistent guidance to the vendors of the standard plants and potential utilities. In its response dated July 2, 1991, Er-RI stated that the level of effort needed to quantify more specific scil parameters was beyond the scope of the Passive Requirements Document, and that the ALWR objectives will be scilled as long as the standard plant design is suitable for a large range of foundation siting conditions that fall within the envelope of parameters of Table 1.2.6. The staff will address this issue during its review of an application for a combined operating license (COL) "	Industry Position Agree. The criteria will be checked later during siting.	NRC Position (DSER) See Abstract	Action Description
an application for a combined operating license (COL)."			

NRC Review

NRR/ESGB

Last 8/6/92 Updated:

P.1.V-30

Status: Closed(COL)

Next Action: none

minimum margin against liquefaction (4.5.2.3)

Abstract (DSER, p 1.4.17) "in its letter dated April 24, 1991, the staff requested that EPRI d-velop evaluation guidelines regarding the minimum margin against liquefaction. In its letter dated July 2, 1952 (sic 1991? JDT), EPRI stated that the specific guidelines had not been developed for the Requirements Document, and a site-specific evaluation must be performed when a plant is to be founded on a soil site. Consistent with the scope and level of technical details included in the Requirements Document, the staff concludes that the guidelines for minimum margin against liquefaction potential may be addressed by the applicant for a COL as a site-specific issue if the plant is to be founded on a soil site, or if any structures are to be founded on soil having a liquefaction potential at sites with multiple soil conditions. Such guidelines should include a detailed evaluation of the liquefaction potential (as described in SRP Section 2.5.4, "Stability of Subsurface Materials and Foundations"), and consequences of liquefaction, of all subsurface soils, including the settlement of foundations. These evaluations will be based on soil properties obtained by state-of-the-art	Industry Position Agree. The criteria will be checked later during siting.	NRC Position (DSER) See Abstract	Action Description
laboratory and field tests and involve application of both deterministic and probabilistic procedures."			NRC Review
		NRR/ES	GB

Last 8/6/02 Updated:

# P.1.V-31

Status: Closed( \_)

Next Action: none

external hazards evaluation (4.5.2.3)

Abstract (DSER, p 1.4-17) "In its letter date 1 April 24, 191, the staff requested EPRI to define the analyses or evaluation methods that will be used to evaluate hazards such as active faults, man-induced hazards, and soil stability. In its response dated July 2, 1991, EPRI noted that these issues were not applicable in the design of standard plants and should be considered in site-specific assessments, and that it anticipated that NRC-approved state-of-the-art analyses and evaluation methods will be used at that time. The staff will address this issue during its review of an application for a	Industry Position Agree. The criteria will be checked later during siting.	NRC Position (DSER) See Abstract	Action Description
COL.			

NRC Review

NRR/ESGB

Last 8/6/92 Updated:

# P.1.V-32

I.M

Status: Open

Next Action: ALWR

number of full-stress cycles (4.5.2.4, 4.8.1)

Abstract (DSER, p 1.4-18) "In Section 4.5.2.4 of Chapter 1, the OBE was deleted for consideration in the design process. As discussed in Section 4.4.3 and Appendix B of Chapter 1 of this report, the staff is evaluating the effect of this change on current staff positions. This evaluation will address the requirement in Sections 4.5.2.4.4.1 and 4.8.1.1 of Chapter 1, which reduces the number of full-stress cycles for 1/2 SSE from 59 to 20. The results of this evaluation will be included in the supplemental regulatory guidance discussed in Section 4.4.3 of this DSER chapter. The staff will review an individual application for final design approval and design certification in accordance with the supplemental guidance."	Industry Position The concern is generic and should be resolved in the context of the Requirements See Issue "I.M"	NRC Position (DSER) See Abstract	Action Description See Issue "I.M"	
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NRC Review

NRR/ESGB P. Sobel

Last 8/6/92 Updated:

# P.1.V-33

Status: Closed(Site)

Next Action: none

site-specific safe-shutdown earthquake (SSE) (4.5.2.4)

Abstract (DSER, p 1.4-19) "Although the design-basis SSE of an RG 1.60 spectrum with a zero period acceleration of 0.30g is sufficient for most potential sites in the United States, it may not envelop the ground motion for sites near seismically active areas in the Easturn and Central United States or sites in the Western United States, in addition to those along the California coast. The staff has observed that recordings of earthquakes in the Eastern United States possess more high-frequency (greater than 5 Hz) ground motion than those earthquakes whose records were used to develop the RG 1.60 response spectrum. This could limit the sites at which designs using 0.3g zero period RG 1.60 response spectrum	Industry Position Agree	NRC Position (DSER) See Abstra *	Action Description
response spectrum. This could limit the sites at which designs using 0.3g zero period RG 1.60 response spectrum could be located. The staff will review the site specific SSE with respect to the design basis at the time of siting."			

NRC Review

NRR/ESGB P. Sobel

Last 8/6/92 Updated:

P.1.V-34

Status: Closed(Cert)

Next Action: none

power spectrum density function of the time history (4.5.2.4)

Abstract (DSER, p 1.4-19) "In Table 1.2-6, the criterion for the SSE ground motion we history (time history) is that the response spectra obtained from the time history envelop the design response spectra. Compared to SRP Section 3.7.1, the staff's position is that this criterion should also include the requirement that the power spectrum density (PSD) function of the time history envelop an approved target PSD function if a single time history is used. In addition, SRP Section 3.7.1 specifies a different acceptance criterion if multiple time histories are used. The staff requires that the time history compte fully with the SPD. The staff will address this during	Industry Position Agree	NRC Position (DSER) See Abstract	Action Description
histories are used. The staff requires that the time history comply fully with the SRP. The staff will address this during its review of an individual application for final design approval and design certification."			

NRC Review

NRR/SRXB

Last 7/14/92 Updated:

P.1.V-35

Status: Closed(Cert)

Next Action: NRC

design temperature (4.5.2.7)

Abstract (DSER, p.1.4-22) "Design temperatures are not included or discussed in Section 4.5.2 of Chapter 1. In Table 1.2.6 of Chapter 1 of the Requirements Document, the ambient temperature is expressed in terms of the maximum and minimum temperatures for both 1 percent exceedance probability and 0 percent exceedance probability. The staff is not certain how the ambient temperature values would be used when they are derived from a probabilistic method and are associated with certain probabilities of exceedance.	Industry Position The method proposed by EPRI/ALWR is currently used and is based on the statistics done on the two hours (0 percent exceedence) or about three days (1 percent exceedence). The method proposed by the staff is the same (for 1 hour, 1 day) and no more deterministic.	NRC Position (DSER) See Abstract	Action Description NRC to consider removaing as an issue.
Table 1.2.6 of the Requirements Document also provides a criterion requiring the site be such as to permit atmospheric heat rejection of cooling water system heat loads or to provide cooling water at the flow rates and temperatures to be specified by the plant designer to achieve certain probability-based cooling performance limits. To review the safety related water supply, the staff typically uses daterministic values based on worst 1 hour, 24 hour, and 30 day values of record. Therefore, the staff will use the deterministic approach to review an individual application for final design approval and design certification."	This does not appear to be an issue.		NRC Review

NRR/PRPB J. Lee

Last 8/6/92 Updated:

P.1.V-36

Status: Open

Next Action: ALWR

protective against surface vehicle bombs (4.5.3)

NRC Review NRR/RSGB R. Dube

Last 8/18/92 Updated:

P.1.V-37

Status: Open

Next Action: NRC

design against internal-missile generation (4.5.5)

Abstract (DSER, p 1.4-26) "In Table B.1-2 of Appendix B to Chapter 1 of the Requirements Document, EPRI commits to comply with the staff review guidance in SRP Section 3.5.1.1, "Internally Generated Missiles (Outside Containment);" SRP Section 3.5.1.2, "internally Generated Missiles (Inside Containment);" and SRP Section 3.5.1.4, "Missiles Generated by Natural Phenomena." The staff concludes that this commitment is acceptable. However, Section 4.5.5.4.1 of Chapter 1 states that ANSI/ANS 58.1, "Plant Design Against Missiles," will be used for guidance in meeting the requirements for internal-missile generation. The staff has not endorsed ANSI/ANS 58.1. Therefore, the staff concludes that where differences exist between the above SRP sections and ANSI/ANS 58.1, the guidance of the SRP sections should be used. If a plant designer identifies and provides justification for the differences, the staff will review the justification on a case-by-case basis and address the issue during its review of an individual application for final design approval and design	Industry Position We would like the NRC to specify which parts of ANSI/ANS 58.1 are in dispute.	NRC Position (DSER) See Abstract	Action Description NRC to indicate disputed parts of standards.
case-by-case basis and address the issue during its review of an individual application for final design approval and design certification."			

NRC Review

NRR/EMCB

Last 7/14/92 Updated:

	one		Action Description	GB GB	7/14/92	n: 8/18/92
	ert) Next Action: n		(DSER) See Abstract	NRR/ES	Updisted:	Printed o
C OPEN ISSUES	Status: Closed(C		Industry Position			
ALWR/NRC	P.1.V-38	design of concrete containment (4.6.1.1)	Abstract (DSER, p 1.4-27) "Section 4.6.1.1 uf Chapter 1 requires that the design of concrete containments natisfy the load combinations shown in ASME Code, Section III, Division 2, Section CC, and the design of steel containments follows SiRP Saction 3.8.2, "Steel Containment." The staff concludes that the specified load combinations for the staff concludes that the specified load combination of the staff of the staff of design conform with SRP System 3.8.2, and are acceptable. Descurse SRP Section 3.8.2, "Concrete Containment," and RG 1.136, "Materials, Cons"+v.4.1, n, and Testing of Concrete Containment," provide viditional guidance of the Passive Requirements Document, the staff requested EPRI to confirm its position regarding compliance. In its letter dated July 2, 1991, EPRI indicated that while it is impractical to list all applicable RGs and SRP sections in individual paragraphs of the Passive Requirements Document, the requirement of compliance for the ALWRs is shown in Table B.1.1.01 Appendix B to Charter' 1.01 ansure that the plant designer will use proper additional	regulatory guidance for the load combinations, the staff's position is that concr) containment design will follow the guidelines of SRP Section 3.8.1 and RG 1.136. The staff will evaluate this issue during its review of an individual application for final design approval and design certification.		Page 59

P.1.V-39

Status: Closed(Cert)

Next Action: none

load combinations for Category I buildings and structures (4.6.1.2)

Abstract (DSER, p 1.4-28) "Section 4.6.1.2 of Chapter 1 requires the design of other seismic Category I reinforced concrete and steel structures to satisfy the load combinations specified in American National Standards Institute/American Concrete Society (ANSI/ACI) 349 and ANSI/American Institute of Steel Construction (AISC) N690, respectively. In its letter dated April 24, 1991, the staff noted that RG 1.142, "Safety-Related Concrete Structures for Nuclear Power Plants," and SRP Sections 3.8.3, "Concrete and Steel Internal Structures of Steel or Concrete Containments," and 3.8.4, "Other Seismic Category I Structures," provide additional guidance on the use of ANSI/ACI 349 for concrete Category I buildings and that the NPC has not approved the use of ANSI/AISC N690 for steel Category I structures. In its	Industry Position Agree	NRC Position (DSER) See Abstract	Action Description
impractical to list all applicable RGs and SRP sections in individual paragraphs of the Passive Requirements Document, the requirement of compliance for the ALWRs is shown in Table B.1.1 of Appendix B to Chapter 1 of the Passive Requirements Document. To ensure that the plant designer will use proper additional regulatory guidance for load combinations, the staff position is to require adherence to SRP Sections 3.8.3 and 3.8.4 and RG 1.142. The staff will evaluate compliance during its review of an individual application for final design approval and design certification."		NRR/E	NRC Review SGB

Last 7/14/02 Updated:

P.1.V-40

Status: Open

Next Action: NFC

design of Category I steel structures (4.6.1.2)

Abstract (DSER, p 1.4-28) "EPRI proposes to use ANSI/AISC N690 for the design of Category I steel structures. The acceptability of using this code is uncertain because this code has not been reviewed and approved by the staff. Therefore, the staff will evaluate this issue during its review of an individual application for final design approval and design certification." Industry Position ANSI/AISC N690 defines precisely the design of Category 1 steel structures. NRC should review it as identify specific areas of disagreement.	NRC Position (DSER) See Abstract	Action Description NRC to identify specifics.
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NRC Review

NRR/ESGB

Last 7/14/92 Updated:

P.1.V-41

Status: Open

and Action: ALWR

combination of pipe rupture loads with seismic loads for seismic Category I structures (4.6.1.3, 4.6.1.4)

Abstract (DSER, p 1.4-32) "In summary, the staff concludes that eliminating the combination of pipe rupture loads (global effects) with seismic loads for the containment and other seismic Category I structures is not acceptable. Furthermore, the proposal to decc. all LOCA and SSE loads for equipment and systems is not acceptable at this time because of the inconsistency that would be created in the SRP and the insufficient technical bases to extend the decoupling to structures. The staff will evoluate this issue during the roman	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER
structures. The staff will evaluate this issue during its review of an individual application for final design approval and design certification."			

NRC Review

NRR/EMEB J. Brammer

Last 8/19/92 Updated:

ALWR		Action Descriptie A (ALWR) Respond to DSER	NRC Revise	MEP J. Brammer	st 8/19/92	on: 8/19/92
Next Action: /		(DSER) See Abstract		NRR/E	La	Printed
Status: Open		Industry Position				8
P.1.V-42	combination of loss-of-coolant-accident and SSE loads (4.6.1.7)	Abstract (DSER, p 1.4-34) "This position allows, in principle, the elimination of load corrbinations (except an SSE plus LOCA) with a probability of occurrence less than 1.0E-6 per reactor-year. However, such an elimination will be approved by the staff only when a specific design applicant justifies fits contention with specific examples of how and where the design is governed and a comparison of structural margins will evaluate this lissue during its review of an individual application for final design approval and design certification."				Page

P.1.V-43

Status: Open

Industry Position

Next Action: ALWR

Action Description

NRC Position

load combinations for safety-related portions of the plant (4.6.2)

#### Abstract

(DSER, p 1.4-34) "Sections 4.6.2.3 and 4.6.2.5 and Table 1.4-5 and 1.4-7 of Chapter 1 have eliminated the loading combination of SSE and LOCA on the basis of recommendations given in NUREG-1061, Volume 4, NUREG-1061 recommends the elimination of this loading combination only for piping systems in the majority of P The staff has not endorsed this recommendation. The cu staff position, as stated in Appendix A to SRP Section : is that SSE and LOCA loads should be combined and included in the Service Level D loads. This position is applicable to both BWRs and PWRs. In its letter dated 17, 1991, the staff requested that the rationale portion of Sections 4.6.2.3 and 4.6.2.5 and load combinations in Ta 1.4-5 and 1.4-7 be revised to agree with the above staff position. In addition, a note should be added to Tables. and 1.4-7 to state that the method of combination of dyn responses to loads is in accordance with NUREG-0484. "Methodology for Combining Dynamic Responses," Revi 1, dated May 1980. In its letter dated August 1, 1991. I stated that the SSE and LOCA loads are not combined because each event is of very low probability, and they unrelated. The staff agrees that EPRI's position could b applicable only to piping systems in the majority of PWI plants. However, the staff's position is based on the requirements of GDC 2 of Appendix A to 10 CFR Part 50 which states that all structures, systems and component designed to withstand the effects of appropriate combinations of normal and accident conditions with natu phenomena. Historically, the staff has interpreted GDC requiring that the effects of the SSE and LOCA be combi for the design of all safety-related portions of the plant. change in this interpretation requires either an exemption or a revision of GDC 2. Therefore, the staff position remains as stated above and as reflected in SRP Section 3.9.3. result, the staff will review an individual application for fin design approval and design certification in accordance will this position."

Last 8/19/92 Updated:

P.1.V-44

Status: Open

Next Action: NPC

dynamic analysis techniques (4.7.2.3)

Abstract (DSEA, p 1.4.37) "Section 4.7.2.3 of Chapter 1 requires that dynamic analysis techniques comply with ASCE 4.86, as well as other applicable codes and standards, and be qualified and proven. In its letter dated April 24, 1991, the staff commented that the NRC has not accepted all analysis techniques in ASCE 4.86. In its response of July 2, 1991, EPRI stated that ASCE 4.86 is intended to supplement the overall criteria and methodology specified in RGs and SRP sections, and that Table B.1.1 of Appendix B to Chapter 1 of the Passive Requirements Document confirms EPRI's commitment to comply with the regulatory positions, except	Industry Position • ASCE 4-86 is intended to supplement the overall criteria and methodology specified in Reg Guides and the SRP • NRC should review it and define specific areas of disagreement	NRC Position (DSER) See Abstract	Action Description NRC review ASCE 4-86 and continue dialog as needed
this section of Chapter 1 are not acceptable because ASCE 4-86 has not been reviewed and approved by the staff. Therefore, the staff concludes that the SRP and RG guidelines should be used for the plant analysis and design of future ALWRs. Plant designers proposing to use ASCE 4-86 should submit a request for the staff review and approval on a case-by-case basis. The staff will evaluate this issue during its review of an individual application for final design approval and design approval			NRC Review

NRR/ESGB

Last 8/6/92 Updated:

P.1.V-45

Status: Closed(Cert)

Next Action:

methodology for generating of design spectra or time histories (4.7.2.5)

Abstraci (DSER, p 1.4-37) "Section 4.7.2.5 of Chapter 1 requires that the generation of design response spectra or time histories be based on methods that minimize unnecessary conservatism. Since the Passive Requirements Document did not indicate the need for NRC approval of methods such as the spectrum-to-spectrum generation procedure, the staff requested a complete discussion of the limitations and verifications for such procedures. In its response of July 2, 1991, EPRI did not address the NRC concern sufficiently. The staff position is that all analysis methods used for licensing basis and safety margin basis must be approved by the NRC staff. The staff will evaluate this issue during its review of an individual application for final design approval	Industry Position Agree	NRC Position (DSER) See Abstract	Action Description
and design certification."			

NRC Review

NRR/ESGB

Last 7/14/92 Updated:

t Action: None		Action Description	NRC Review	NRR/ESGB	Updated: 7/14/92	Printed on: 8/18/92
Cert) Nex		(DSER) See Abstract				
Status: Closed(		rea rea				29
P.1.V-46	structural damping values (4.7.2.6)	Abstract (DSEP, p 1.4-38) "Section 4.7.2.6 of Chapter 1 requires that structural damping values be based on confirmed test results. rather than conservative assumptions, whenever such data are available. In its letter dated April 24, 1991, the staff requested the basis for using less conserva tive damping values. In its response of July 2, 1991, EPRI cited cable trays and hangers as an example for which extensive tests have been done by some utilities to generate more realistic damping values than those provided in RG 1.61. The staff position of using structural damping for the design of structures is described in RG 1.61. However, the staff will not exclude the use of structural damping based on test results. Therefore, the staff will evaluate the structural damping values during its review of an individual application for fin al design approval and design certification.				Page

ALWR		Action Description (ALWR) Respond to DSER	ES GB	ast 8/16/92 ed: <b>i on: 8/18/92</b>
Next Action.		(DSER) Sea Abstract	RER	Up 3ah
Status: Open		Industry Position		18
P.1.V-47	masonry walls in Category I buildings (4.7.2.7)	Abstract (DSER, p. 1.4-38) "Section 4.7.2.7 of Chapter 1 requires that masonry walls used as temporary or permanent partitions in Category i building, with consideration given to the effect they could have on safety-related items, and that they be designed according to applicable requirements of the Uniform Building Code (UBC). The use of the UBC for the design of masonry walls in Category I structures and the use of masonry welds in Category I structures and the use of masonry welds for the design of masonry welds for this deviation, ther-fore, the SRP guidelines. The staff concludes that EPRI has not provided sufficient justification for this deviation, ther-fore, the SRP guidelines. The staff or this deviation for the design of masonry welds in Category I structures and the use of masonry welds in the Category I structures as load-carrying members or non-load-carrying members. The staff will evaluate this issue during its review of an individual application for finel design approval and design certification.		Bage

P.1.V-48

Status: Open

Next Action: NRC

use of expansion anchor bolts - compliance with Office of Inspection and Enforcement Bulletin 79-02 (4.7.2.8, 4.7.3)

Abstract (DSER, p 1.4-38) "Section 4.7.2.8 of Chapter 1 specifies the use of the direct bearing or undercut type of anchor bolts to ensure the ductile behavior of the bolt when high capacity is needed and the use of wedge and sleeve anchors for small loads. In its letter dated April 24, 1991, the staff questioned the use of expansion bolts for all safety significant applications and encouraged qualification testing under field conditions. Where the expansion anchors are used, the NRC requires the use of the conservative safety factors of Inspection and Enforcement Bulletin (IEB) 79 02 to account for uncertainty in field installation. In its response of July 2, 1991, EPRI acknowledged that it is intended to use expansion bolts only when necessary and that the expansion bolts will be of the undercut type (e.g., Maxibolts) in lieu of friction type, EPRI also noted that the conservative safety factors or IEB 79 02 are intended for friction type expansion anchors and may not apply to Maxibolts. The response is not acceptable because the issue of uncertainty in field installation was not addressed and there is no assurance that the ICP 70.00 and the tester of the response to the tester.	Industry Position We agree that the 79-02 inspection methods and safety factors are applicable to wedge or sleeve type anchors, which are permitted only for small loads. For applications requiring substantial pullout capacity Maxibolts would be used only if embedded anchorage was not preengineered. The Maxibolt installation procedure includes a tensioning of each bolt installed which serves as a proof test of the pullout capacity. For this reason, additional testing of Maxiboits is not required.	NRC Position (DSER) See Abstract	Action Description NRC to review this response
Therefore, plant designers should submit to the NRC staff the safety factors they propose to use for the capacity of the Maxibolts. The staff will evaluate this issue during its review of an individual application for final design approval and		NRR	NRC Review /EMZB J. Brammer

Last 8/6/92 Updated:

P.1.V-49

Status: Open

Next Action: ALWR

stability of shell-type structures under compression (4.7.2.9)

(DSER, p 1.4-39 the potential for for shell type stru requires that, aft uncertainties in n description, a mi load combination Requirements D based on ASME supplemented by 284 provides low Section NE, the designer regardi asymmetric cont specific condition response of July professional cont careful review of apply Code Case do not apply. E scope of the Pas limitations of the to the staff. The be used for the Code Case N-28 during its review approval and der

bstract ) "Section 4.7.2.9 of Chapter 1 requires that global and local shell buckling be considered ictures under compression. In addition, it er appropriate consideration of the various naterials, erection tolerances, and load nimum factor of safety be maintained for all is. In Revision 2 to the Passive ocument, the minimum factor of safety was Code. Section III, Subsection NE, and y Code Case N 284. Because Code Case N rer safety factors against shell buckling than staff requested that EPRI alert the plant ing the application of Code Case N 284 to ainments with large openings or provide its under which N 284 can be used. In its 2, 1991, EPRI stated that experienced tainment vessel designers, working under the utility owners and regulators, will not e N 284 where provisions of the code case PRI also stated that it was beyond the ssive Requirements Document to explain the specific code case. This is not acceptable et aff concludes that NE security results.	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER	
e staff concludes that NE requirements should evaluation of shell-type structures. As for 84, the staff will evaluate its applicability of an individual application for final design sign certification."		NRR/	ESGB	

Last 8/18/92 Updated:

P.1.V-50

Status: Open

Next Action: NRC

use of ASME Code Cases N-411 and N-420 in same analysis (4.7.3)

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Abstract (DSER, p 1.4-41) "Sections 4.7.3.2 and 4.7.3.11 of Chapter 1 of the Requirements Document allow the plant designer to use ASME Code, Section III Code Cases N-411 and N-420 unconditionally. In its letter dated May 17, 1991, the staff requested that the following sentence be added to this requirement: "ASME Code Cases N-411 and N-420 may only be used in separate analyses and as further conditioned in RG 1.84." In its letter dated August 1, 1991, EPRI stated that since its intent to comply with RG 1.84 is indicated in Appendix B of Chapter 1 of the Passive Requirements Document, this additional sentence is unnecessary. The staff's understanding of the Passive Requirements Document is that a requirement in any section could override such a commitment in Appendix B. Therefore, this response is unacceptable and the staff's position remains as stated in its letter of May 17, 1991. The staff will evaluate this issue during its review of an individual application for final design approval and design certification in acr "dance with the above position."	Industry Position There is no intention that committments in Appendix B could be overridden by other parts of the URD. Any and all contradictions that are brought to our attention will be eliminated and if the NRC reviewer is aware of any such contradictions, he should tell us. Otherwise, the review can assume Appendix B committments are bona fide committments.	NRC Position (DSER) See Abstract	Action Description NRC review this response.

NRC Review

NRR/EMEB J. Brammer

Last 8/6/92 Updated:

#### P.1.V-51

Status: Open

Next Action: NRC

use of ASME Code Case N-411 (4.7.3)

#### Abstract

(DSER, p 1.4-41) "In its letter dated May 17, 1991, th requested that Section 4.7.3.8 be revised to clarify the a single damping value for both the OBE and the SS letter dated August 1, 1991, EPRI stated that the AL program has deleted the OBE in the design process a damping values in RG 1.61 for the SSE will be applied structules and systems except for piping, for which A Code Case N-411 is applicable. The elimination of the is discussed in Section 4.4.3 of this report. The resol this issue may affect Section 4.7.3.8 of Chapter 1. of Code Case N-411, as stated in EPRI's response : August 1, 1991, is not completely acceptable. The staff requested that the requirement portion of Section 4.7.3.8 be revised to include a requirement that Code Case N-411 can be used only as conditioned by RG 1.84. In its response, EPRI stated that since Table B.1-2 of Appendix B to Chapter 1 indicates a commitment to comply with RG 1.84, this revision was unnecessary. The staff's understanding of the Passive Requirements Document is that a requirement in any section could override such a commitment. Therefore, this portion of the response is unacceptable and the staff position remains as stated in its letter of May 17, 1991 The staff will evoluate this issue during its review of an individual application for final design approval and design certification, assuming that the requirement in Section 4.7.3.8 does not override the commitment to RG 1.84 in Appendix B to Chapter 1."

ne staff e use of E. In its WR and that	Industry Position There is no intention that commitments in Appendix B could be overridden by other parts of the URD. Any and all contradictions that are brought to our attention will be	NRC Position (DSER) See Abstract	Action Description NRC to review this response	
SME SME ution of he use	eliminated and it the NHC reviewer is aware of any such contradictions, he should tell us. Otherwise, the review can assume Appendix B commitments are bona fide commitments.			

NRC Review

NRR/EMEB J. Brammer

Last 8/6/92 Updated:

# P.1.V-52

Status: Ope

Industry Position

Next Action: ALWR

NRC Position

(DSER) See Abstract

construction of core support structures (4.7.3)

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(DSER, p 1.4-43) "Section 4.7.3.23 of Chapter 1 states that core support structures will be designed to the criteria specified in ASME Code. Section III. Subsection NG. In its. letter dated May 17, 1991, the staff requested that this requirement be revised to read: "Core support structures will be constructed to the criteria specified in ASME Code, Section III. Subsection NG, where "construction" is as defined in ASME Code, Section III, NB/NC/ND-1100(a)," In its letter dated August 1, 1991, EPRI agreed with the staff's request, except that the requirement still contains the words "designed to" rather than "constructed to," which is not completely acceptable. During its reviews of individual applications for final design approval and design certification, the staff will require that core support structures be constructed to the rules of ASME Code, Section III, Subsection NG, where "construction" is either as defined above or as defined in ASME Code, Section III, Subsection NG-1110."

NRC Review

Action Description

(ALWR) Respond to DSER

NRR/EMEB J. Brammer

Last 8/18/92 Updated:

P.1.V-53

Status: Open

Next Action: ALWR

design fatigue curves (4.7.3)

#### Abs

(DSER, p 1.4-44) Requirements Doc the ALWR will be 6 guestions relative t ASME fatigue desig established almost best-fit curves of fa either 2 on stress o conservative at eac intended to cover s and scatter of data currently available, may not be sufficie fatique test data as In its letter dated M commitment in Sec effects in the desig systems, compone August 1, 1991, El research results vie ASME fatigue desi will provide the pro staff does not agre response and conc completely accepta revised for many y until these curves a applying for license design fatigue curv the Requirements would be sufficient will evaluate this is application for final

ment states that the plant design life for D years. This proposed design life raises	the second se	The second second second second second
the margins available in the current n curves. These margins were 30 years ago and were obtained from tigue test data by applying a factor of 20 on cycles, whichever was more h point. These factors were originally		
ich effects as environment, size effect, However, on the basis of limited data he staff concludes that these margins t to account for variations in the original a result of various environmental effects. ay 17, 1991, the staff requested a ion 4.7.3 of Chapter 1 to consider such is of applicable ASME Code, Class 1		
is, and equipment. In its letter dated RI stated that if additional data or I findings requiring changes to the current in curves, the Code consensus process		NRC Review
er venicle to attect such tindings. The with all of the discussions in this udes that the above commitmen' is not ile. The ASME Code curves may not be ars. Therefore, the staff's position is that e revised, all ALWRs and all plants renewal should propose appropriate is that will be reviewed by the staff. For ocument, a commitment to this position Pending such a commitment, the staff ue during its review of an individual design approval and design certification."	NRR (	'EMEB J. Brammer

Last 8/18/92 Updated:

# P.1.V-54

Status: Closed(Ceri)

Next Action: none

use of zinc to reduce radiation fields (5.2.7)

Abstract (DSER, p.1.5-5) "To reduce general radiation fields resulting from the presence of cobalt-60 in the oxide layer of the RCS piping, zinc additions may be made to the coelant in BWRs in limited, controlled amounts. Zinc injection reduces the radiation fields by replacing the cobalt with zinc in the piping oxide layer. One of the side effects of zinc injection is the creation of zinc-65, which increases piping dose rates and requires special consideration during radioactive disposal. EPRI	Industry Position Agree	NRC Position (DSER) See Abstract	Action Description
EPRI is investigating a way to solve this problem by using a zinc isotope depleted in zinc-64. The staff will review this issue again at the vendor application stage to determine what advances have been made in this area."			1

NRC Review

NRR/PRPB C. Hinson

Last 7/17/92 Updated:

# P.1.V-55

Status: Open

Next Action: ALWR

grinding controls for PWRs (5.3.1.1)

(DSER, p 1.5-9; he staff considers these requirements acceptable. The implementation of these requirements will ensure that wrought austenitic stainless steel will perform in service as designed. However, the staff requires that the grinding controls also be applied to PWR applications. The staff will evaluate this issue during its review of an application for a COL."	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER
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NRC Review

NRR/EMCB G. Georgiev

Last 8/18/92 Updated:

P.1.V-56

Status: Open

Next Action: ALWR

use of Alloy 600 (5.3.1.3)

Abstract	Industry Position	NRC Position	Action Description
(DSER, p 1.5-11) "The staff considers these requirements acceptable. The implementation of these requirements will ensure that Ni-Cr-Fe alloys will perform in service as designed. However, the staff will require that the applicant for any standard design application identify the use of Alloy 600 and provide described information concerning its use. Those applications will be reviewed and approved by the staff on a case-by-case basis. In addition, the use of other Ni-Cr-Fe alloys such as Alloy 690 or 800 should be considered in applications for which primary water stress corrosion cracking (PWSCC) is a concern. These applications also will be reviewed on a case basis."	moustry Position	(DSER) See Abstract	(ALWR) Respond to DSER

NRC Review

NRR/EMCB G. Georgiev

Last 8/18/92 Updated:

P.1.V-57

Status: Open

Next Action: NRC

affect(sic) of fabrication processes on intergranular stress corrosion cracking (5.3.1.8)

IGSCC in service. The staff considers it important that adequate field and shop fabrication processes be used to minimize the sensitization of materials to IGSCC and will review specific controls as a part of the COL process."		
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NRC Review

NRR/EMCB G. Georgiev

Last 8/6/92 Updated:

P.1.V-58

Status: Open

Next Action: NRC

selection of seal, gaskets, and protective coatings (5.3.5)

Abstract (DSER n 1.5-20) "Section 5.3.5 of Chapter 1 of the Passive Require into Document requires that the plant designer conduct a rogram for evaluating the effects of intended products on other ALWR components under normal and postaccident conditions. For each product evaluated, the designer will provide recommendations and limits for its use in the steam supply systems and other applications in the ALWR. Information from component vendors will be relied upon only when substantiated by operational experience.	Incustry Position The URD will be revised to require the designer to specify the ANSI standard (if any) covering , the particular product and the applicable process.	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
The staff considers these requirement, acceptable. The implementation of these requirements will ensure that seal, gackets, and protective coatings are selecte. "Assed on operational experience. However, the staff will require that the applicant specify the specific ANSI standard covering this subject. The staff will evaluate these components during its review of an individual application for final design approval and design certification."			

NRC Review

NRR/EMCB G. Georgiev

Last 8/5/92 Updated:

**COLUME III, CHAPTER 1: OVERALL REQUIREMENTS** 

l'arton ... n No.

Requirement

Coatings, Lutracits and Hydraulic Fluids, Cleaning, Pack-Seals, Gaskets, Packings, Sealants, Paints and Protective aging and Store ve Materials 23.5

The Plant Designer shall conduct a program for evaluating the other applications in the ALWR. Information from component operational experience. The program should encompass the product evaluated, the Designer shell provide recommanda tions and limits for its use in the steam supply systems and vendors should be relied upon only when substantiated by effects of intended products on other ALWR components under normal and post-accident conditions. For each material categories of Table 1.5-1.

Rationale

Coatings, Lubricants and Hydraulic Fluids, Cleaning, Pack Seals, Gaskets, Packings, Sealants, Paints and Protective aging and Storage Materials

contributed to down-time in operating reactors. Specific con-Experience has shown therour a evaluation to be essential in materials available in the marketplace, many of which have life), compatibility with materials in contact, leaching or outsiderations include: deterioration with time (including shelf selecting the proper product from the great variety of gassing of impurities, and resistance to environment

The Designer Shall partial ecommender to the variety of possible non-metallic materials and Rount's including recommender to used during design, there are many applications throughout and Rount's including rejuinces and testing which should be considered. This is tur-To specific ANSI Standards if any, supply Systems and other for each hadness evaluated for use in the Nuclear Staue applied ous in ALWR

tenance and testing which should be considered. This is furwill help simplify the selection process and preclude use of similar requirements on component vendors and crectors, product category. The plant designer's study of available product experience and qualifications, as well as placing undesirable products.

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P.1.V-59

Status: Open

Industry Position

Next Action: ALWR

NRC Position

(DSER) See Abstract

aging of cable insulations and other electrical materials (5.3.6)

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(DSER, p 1.5-20) "Section 5.3.6 of Chapter 1 of the Passive Requirements Document requires that materials used in the plant's electrical systems, particularly those used in safety-related applications, be reviewed for functional reliability during normal, abnormal, plant operation, and accident conditions. The fire-retardant characteristics of the materials used in the electrical systems will be addressed in order to minimize the probability of fire and the subsequent consequences should a fire occur.

The staff concludes that this requirement acceptable. However, it is not clear that this requirement is sufficient to address such issues as aging of cable insulations and other electrical materials over the design life and full range of environmental conditions. The staff will evaluate this issue during its review of an individual application for final design approval and design certification.

NRC Review

ion Description

(ALW-r) Respond to DSER

NRR/SPLB G. Hubbard

Last 8/18/92 Updated:

P.1.V-60

Status: Open

Next Action: ALWR

use of hydrogen water chemistry for the advanced BWR design (5.5.2)

Abstract (DSER, p 1.5-25) "Section 5.5.2.1 of Chapter 1 requires that the water chemistry design basis for BWR plant systems be in accordance with EPRI NP-4947-SR, "BWR Hydrogen Water Chemistry (HWC) Guidelines," 1987 Revision, and its subsequent revisions, and as supplemented by the guidelines provided in Table 1.5-1 of this report.	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSE
The HWC specific control values given in EPRI's guidelines relative to recirculating piping (a.g., 230 mV) will apply to nozzles, components, and other non-replaceable components in the reactor vessel lower plenum.			
EPRI addresses the use of HWC for the advanced BWR design. The use of HWC at plants such as Hatch, Brunswick, and Duane Arnold has resulted in unexpectedly high operational and post-shutdown radiation levels in RCS piping. EPRI has acknowledged the potential drawbarks of using HWC and has stated that investigations are under way to identify a solution to some of the problems resulting from the use of HWC. A special evaluation will be made when considering carbon and low alloy material for reactor coolant service with less than 10 ppm oxygen as the result of HWC. The evaluation will include erosion/corrosion, radiation buildup, and pitting at shutdown. The staff will evaluate the issue of HWC use during its review of an individual application for final design approval and design certification to determine what advances have been made in this area."		NF	NRC Review R/EMCB G. Georgiev

Last 8/18/92 Updated:
P.1.V-61

Status: Open

Next Action: NRC

plant-specific reliability assurance program (6.5)

Abstract (DSER, p 1.6-8) "The staff concludes that, with the exceptions noted above, the reliability and availability requirements established in the Passive Requirements Document are consistent with accepted industry practices and principles and do not conflict with current regulatory requirements and guidelines. They are, therefore, acceptable. However, by themselves, the reliability and availability requirements do not provide sufficient information for the staff to determine if the ALWR design referencing the EPRI requirements will adequately incorporate RAP considerations in a manner that will ensure plant safety and reliability. Therefore, applicants defencing the Passive Requirements Document will be required to provide sufficient information to demonstrate that their RAP will result in a plant that is designed and will perform in a manner that will ensure plant	Industry Position The RAP has been modified (Re. 3. of Ch 1, Section 6). We consider that the considerations in it ensure plant safety.	NRC Position (DSER) See Abstract	Action Description NRC review Rev 3.
safety and reliability."			

NRC Review

NRR/LPEB R. Correia

Last 8/6/92 Updated:

# P.1.V-62

Status: Closed(COL)

Next Action: none

inspection of construction activities (7, 11.13)

Abstract (DSER, p 1.7-1) "The NRC has the statutory responsibility, regardless of construction schedula to verify that the plant is	Industry Position Agree	(DSER) See Abstract	Action Description
constructed in accordance with the design documents tendered with the application for an operating license. The owners/builder must ensure that construction activities permit verification of the acceptability of the plant configuration in accordance with the requisite NRC Inspection Manual chapters. The staff will evaluate this during its review of a specific application for a COL."			

NRC Review

NRR/PDST

Last 8/6/92 Updated:

# P.1.V-63

Status: Closed(COL)

Next Action: none

installed operating-phase security system (7)

Abstract (DSER, p 1.7-2) "In Section 7.9.6 of Chapter 1 of the Passive Requirements Document, EPRI requires the utility to establish security boundaries as part of the startup testing program. In a letter dated May 13, 1991, EPRI agreed that the detailed construction and startup schedule will have to address NRC review and approval of the installed security system for the operating phase before first fuel loading, but that this milestone is beyond the scope of the ALWR Requirements Document. This will be addressed by the staff during its review of a specific application for a COL.	Industry Position Agree	NRC Position (DSER) See Abstract	Action Description
The staff expects that at least sixty days prior to loading fuel, a licensee for a COL will have confirmed that security systems and programs described in its physical security plan, safeguards contingency plan, and guard qualification and training plan have achieved operational status and are available for NRC inspection. Operational status means that the security systems and programs are functioning in entirety as they would when the reactor is operating and will reman so. The COL licensee's determination that operational status has been achieved must be based on tests conducted under realistic operating conditions of sufficient duration that demonstrated that the equipment is properly operating and capable of long-term, reliable operation, that procedures have been developed, approved, and implemented, and that personnel responsible for security operations and maintenance have been appropriately trained and have demonstrated their capability of performing their assigned duties and responsibilities."		NRR	NRC Review RSGB R. Dube

Last 8/6/92 Updateri:

gree

Industry Position

P.1.V-64

Status: Closed(COL)

Next Action: none

NRC Position

(DSER) See Abstract

reliability of modular construction (7)

#### Abstract

DSER, p 1.7-3) "Specific licensing criteria addrescing modular construction have not been developed for nuclear power plant construction. Structures, systems, and components that are assembled using modular construction techniques must possess, as a minimum, the same degree of structural strength and reliability of such items provided in currently licensed plants that were constructed using current onsite construction techniques. Items to be considered include segmented rebar cage connections and in-containment steel/concrete sandwich-type shear walls for which there are no modular construction design criteria and for which test information is limited. Other areas of concern include the integrity of joints (including strength and ductility), seismic damping values and stiffness Cegradation in structural modules, quality assurance and quality control requirements for transportation and installation of modules, and the scope of the verification testing after the modules are installed. This will be addressed by the staff during its review of a specific application for a COL, should the applicant propose use of these techniques."

NRC Review

Action Description

NRR/ESGB

Last 8/6/92 Updated:

P.1.V-65

Status: C'osed(COL)

Hext Action: none

inspection and verification of security locks robotically (8.3)

Abstract (DSER, p.1.8-3) "The plant designer will perform an analysis to determine the effectiveness of using robotic applications in the ALWR. Inspection/eurveillance functions of include reading of instruments and gauges, performing of include reading of instruments and gauges, performing of include surveys and measuring radii tion levels, and the surveys surveys. EPRI strikes hat the maint nance functions of include steam generator inspection and maintenant of rod drive removal, radwaste drum handling, spring consolidation, equipment decontamination, and that se surveillance and maintenance tasks. The Residements Document specifies that the ALWR will include design features such as wider doors and aisles, ramps and modular construction of equipment and syrems (for ease of equipment removal and replacement) of facilitate the use of robotic devices. Table 1.8-4 includes "verify security locks" as one of several functions to be evaluated by the plant designer as a candidate for robotic inspection and surveillance. However, in its letter of May 17, 1991, EPRI stated that details of the security functions to be performed and the consideration of replacing a security officer are outside the	Industry Position	(DSER) See Abstract	Action Description
cope of the Requirements Document. This will be addressed by the staff during its review of a specific application for a			LAC Review
COL.*		NRE/	RSGB R. Dube

Last 8/6/92 Updated:

# ALWR/NRC OF SN ISSUES

P.1.V-66

Stores Open

Next Action: ALWR

NRC Position

(DSER) See Abstract

compliance of design certification applications with Commission's advecting audance (10)

Abstract

Industry Position

(DSER, p 1.10-1) "Section 10.2 of Chapter 1 states that the ALWR will be designed to comply with the NRC regulatory requirements and guidance in effect on January 1, 1990, consistent with the commitments in Section 1 of Appendix B to Chapter 1 of the Passive Requirements Document. EPRI states that these requirements and guidance include applicable Commission regulations specified in Title 10 of the Code of Federal Regulations, general design criteria, NRC policy statements, regulatory guides, the Standard Review Pian, and other documentation that resolves unresolved and generic safety issues. Although the staff understands EPRI's need to "freeze" the requirements it addresses TO those in effect on January 1, 1990, the staff expects that the design certification applications will be in compliance with the Commission's regulations and guidance that are applicable and in effect at the time the certification is issued. The staff will evaluate this compliance during its review of an individual application for final design approval and design certification."

**NRC Review** 

Action Description

(ALWR) Respond to DSER

NRR/PDST

Last 8/18/92 Updated:



Status: Open

Next Action: ALWR

issue resolution for final design approval and design certification reviews (10)

Abstract (DSER, p 1 10-1) "In addition, issue resolutions that are different from those arrived at during the staff's review of the Passive Requirements Document may be developed as the staff completes its reviews of the detailed design information provided in the final design approval and design certification applications, and as these designs are inigated in the design certification hearings. Therefore, the staff expects that the ALWR plant designers will comply with issue resolutions adopted by the NRC staff during its reviews of the final design approval and design certification applications in accordance with the requirements of 10 CFR Part 52. The staff will evaluate this compliance during its review of an is dividual application for final design approval and design certification."	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER

NRC Review

NRR/PDST

Last 8/18/92 Updated:

P.1.V-68

II.L

Status: Closed(Cert)

Next Action: none

inspections, tests, analyses, and acceptance criteria (10)

(DSER, p 1.10 guidelines for evaluating pilo design. As der Analyses, and Certifications a Tier 1 ITAAC Tier 1 design expects that th level in nature functional perf criteria values stated accepta properly imple guidance on s Requirements submittal prov for staff review plant designer will evaluate t individual appl certification an license."

Abstract	I Industry Position	I NRC Position	I Action Description	h
1-4) "The staff is developing additional the scope and content of ITAAC, and is of ITAAC submittals based on the GE ABWR scribed in SECY-91-178, "Inspections, Tests, I Acceptance Criteria (ITAAC) for Design and Combined Licenses," dated June 12, 1991, will be at a level of detail corresponding to the information on the certified design rule. The staff he Tier 1 verification requirements will be high and will addres the design at a system ormance level or detail. Numerical acceptance will only be specified when failure to meet the ance criteria would clearly indicate a failure to ment the design. While including appropriate scope and content for ITAAC submittals in the Document would ensure that each design wide a complete and adequate ITAAC package w, ITAAC is clearly the responsibility of the during the design certification phase. The staff he proposed ITAAC during its review of an lication for final design approval and design	See issue II.L	(DSER) See Abstract	NRC Review	
nd shapplication for a combined operating		ND D	(05.00	
		NRR,	12001	

Last 8/6/92 Updated:

P.1.V-69 Status: Closed(Cert) Next Action: none	vi simplification objective (11.4)	Distract     Industry Position     Industry Position       "Section 11.4 of Chapter 1 of the Passive ocument states that ALWR design should be ocument states that ALWR design should be of mechanical components (valves, hangers, snubbers) and a minimum of nd controls will be used. EPRI specifies be designed to simplify cperations during attion, including operator actions to diagnose and an accident conditions.     Industry Position     Action Description	with the overall objective to strupity trations. The staff will ensure that if this objective is in accordance with the gulations and guidance during its review of an tion for final design approval and design	NRC Review	MR./PDST	L'st 7/14/92 Updated:	Page 90 Printed cn: 8/18/92
P.1.V-69	mplementation of simplification	Abstract (DSER, p 1.11-2) "Section 11.4 of Requirements Document states th simpler than that of current operal minimum number of mechanical of pumps, heat exchangers, snubbe instrumentation and controls will that the plant will be designed to all modes of operation, including of and manage abnormal and accide	The staff agrees with the overall operations. The statistic systems and operations. The statimplementation of this objective is Commission's regulations and guidindividual application for final desicentification."				

Next Action: none		act Action Description act	
Cert)		(DSER) See Abstr	
Status: Closed(		Industry Position	
Г	]	agree	
P.1.V-70	implementation of standardization objective (11.5)	Abstract (DSER, p 1.11-2) "Section 11.5 of Chapter 1 of the Passive Requirements Document states that the ALWR design will be developed as a standard plant design, including, as a minimum, a standard design basis, standard site envelope, standard equipment, and standard technical documentation.	The staff supports the concept of standardization, as can be seen in the promulgation of 10 CFR Part 52, the issues of the Commission's Standardization Policy, and the staff's efforts in the review of the EPRI Requirements Document. The staff will ensure that implementation of this concept is in accordance with the Commission's regulations and guidance during its review of an tridividual application for final design approval and design certification."

NRC Review

NRR/PDST

Last 7/14/92 Updated: Printed on: 8/18/92

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P.1.V-71

Status: Open

Next Action: NRC

inservice testing requirements for the essential non-safety-related components (12.2.1, 12.2.3)

Abstract (DSER, p 1.12-3) "The staff concludes that all passive safety-related equipment, including non-Code safety-related pumps and valves, must be tested in accordance with ASME Code, Section XI. The staff may not require the essential non-safety-related components to meet all of the safety-grade criteria. However, the staff concludes that there are uncertainties concerning the lack of a proven operational performance history. These uncertainties make the essential non-safety-related systems and components more important in providing the detense-in-depth to prevent and mitigate accidents and core damage. The staff is still evaluating this issue for the passive plant designs. The specific staff positions on the inservice testing requirements for the essential non-safety-related components will be determined when the staff completes its review of the issue of regulatory treatment of non-safety-grade systems. Therefore, the staff will evaluate this issue during its review of individual application for final design approval and design certification."	Industry Position Chapter 1, section 12 of the URD has been substantially revised. For essential valves and pumps, testing is required in accordance with ASME Code Section XI. This should be sufficient to close this issue.	NRC Position (DSER) See Abstract	Action Description NRC review this response
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NRC Review

NRR/EMEB

Last 8/6/92 Updated:

P.1.V-72

Status: Closed(cert)

Next Action: none

quarterly testing of pumps and valves (12.2.2)

Abstract (DSER, p 1.12-4) "In its letter dated May 17, 1991, the staff requested that the passive ALWR systems be designed to accommodate the applicable ASME Code, Section XI requirements for quarterly testing of pumps and valves, rather than allow designs that only accommodate testing during cold shutdowns or refueling outages. In its letter dated August 1, 1991, EPRI responded to this request by stating that the frequency of testing should be determined by such factor: as component design, application, PRA insights, and design alternatives. EPRI further stated that the ALWR program does not propose to change the manner in which the code has been applied to recently licensed plants. For the reasons discussed in Section 12.2.1 of this report, the staff concludes that its position as stated in RAI 210.39(b) of the May 17, 1991, letter will improve the component reliability for passive ALWRs. Therefore, the staff concludes that EPRI's response is not acceptable. The staff will evaluate this during its review of individual applications for final design approval and design certification in accordance with the above position."	Industry Position All essential (safety and non-safety but important to investment protection) valves of Passive ALWR systems will accomodate the requirements of ASME Code Section XI. This includes the possibility to defer the testing in particular cases as permitted by the Code. For special systems (eg: IRWST injection for the PWR) special and additional requirements are shown in the relevant Chapters of Volume III.	NRC Position See DSER	Action Description none

NRC Review

NRR/EMEB

Last 7/17/92 Updated:

P.1.V-73

Status: Open

Next Action: ALWR

check valve testing methods (12.2.2)

Abstract (DSER, p 1.12-5) "The staff disagrees with EPRI's position that a commitment to check valve testing methods requires a detailed design analysis. The staff concludes that a commitment to check valve testing methods should be part of the Passive Requirements Document. In addition, a requirement should be added to the list of guidelines from EPRI Report NP-5479, "Application Guidelines for Check Valves in Nuclear Power Plants," in the requirement portion of	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER
and the application of valves, the plant designer should also consider parts clearance, disc stability, and wear relative to actual operational flow conditions. Pending such changes the staff will evaluate this during its review of individual applications for final design approval and design certification in accordance with the above positions."			

NRC Review

NRR/EMEB

Last 8/16/92 Updated:

P.1.V-74

Status: Closed(Cert)

Next Action: none

full-flow testing of check valves (12.2.2)

Abstract (DSER, p 1.12-6) "In its letter dated May 17, 1991, the staff requested EPRI to revise Section 12.2.7.2 in Chapter 1 of the Passive Requirements Document to reflect the staff's position on full-flow testing of check valves as described in the letter. In its August 1, 1991, response, EPRI referred to its position as provided in its responses to RAI 210.39(b) and (f). For reasons similar to those discussed above, EPRI's response is not acceptable. The staff maintains that testing method and testability are important to reliability assurance and that a commitment to the staff's position on full-flow testing of check valves should be part of the Passive Requirements Document. Pending such a commitment, the staff will review individual applications for final design approval and design certification in accordance with the above position."	Industry Position The URD endorses the Staff position requiring system design that will permit full-flow testing of installed safety-related check valves to demonstrate operability of the valves under operating conditions.	NRC Position (DSER) See Abstract	Action Description
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NRC Review

NRR/EMEB

Last 8/19/92 Updated:

P.1.V-75

Status: Open

Next Action: ALWR

provisions to test hydraulically and pneumatically operated valves under design-basis differential pressure and flow (12.2.2)

		TRAK II	
Abstract (DSER, p 1.12-6) "In its letter dated May 17, 1991, the staff requested EPRI to require the plant designer to commit to test hydraulically and pneumatically operated valves in accordance with the forthcoming ASME/ANSI OM Part 18, "Performance Testing of Hydraulic Operated Valve Assemblies in LWR Plants," and Part 19, "Performance Testing of Pneumatically Operated Valve Assemblies in LWR Plants." In its letter dated August 1, 1991, EPRI responded to this request by stating that it is committed to available and applicable codes and standards. At the time that equipment is designed, the plant designer will identify applicable revisions of each document. This response is not entirely acceptable. The staff position is that designs should incorporate provisions to test hydraulically and pneumatically operated valves under design-basis differential pressure and flow. The design-basis capability of these types of valves will be expected to be verified before installation, before startup and periodically through a program similar to that recommended for motor-operated valves in Generic Letter 89-10, dated June 28, 1989. Pending such a commitment, the staff will evaluate this during its review of individual applications for anal design	Industry Position	NHC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER
positions."		NRR/	EMEB

Last 8/18/92 Updated:

on: ALWR	Action Description (ALWR) Respond to DSER	NRC Review R / EMEB	Last 8/18/92 Jated:	ted on: 8/18/92
Next Activ	(DSER) See Abstract	NRJ	n	Drin
Status: Open	ves (MOVs) (12.2.2) Industry Position			47
P.1.V-76	qualification testing of active and non-active motor-operated value (DSER, p. 1.12-7) "In its May 17, 1991 letter, the staff requested additional information on qualification testing of active and nonactive MOVs. In its August 1, 1991, response. EPRIs stated that nonactive MOVs should be designed for potential mispositioning, but qualification testing is not required. This statement does not completely agree with the current staff guidelines on valve mispositioning. The system either should be designed to prevent mispositioning or should required to be subjected to qualification testing to demostrate corputing to recort through actions taken at any time locality (manual or electrical), at a motor control center or in the control room and includes deliberate changes of valve position fund the above position.			Pace

# P.1.V-77

Status: Open

Next Action: ALWR

technical concerns regarding MOVs (12.2.2)

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Abstract (DSER, p. 1.12-8) "Recent industry experience and the results of NRC inspections of MOV programs have indicated several areas requiring attention in the EPRI document. Speci-fically, in addition to the technical information to be provided with each valve described in Section 12.2.2.5 of Chapter 1 of the Passive Requirements Document, operator loads as a function of fluid temperature (subcooling) and seismic/dynamic effects, as well as precise internal dimensions of the valve, should be provided. In addition to consideration of stem leakage in establishing the proper globe valve orientation described in Section 12.2.2.6.2 of Chapter 1 of the Passive Requirements Document, any reliance on a globe valve to isolate flow or the use of the valve for throttling flow should also be considered in establishing proper orientation. In addition to ensuring that the valve bonnet and disc will be designed to prevent pressurization due to heatup of fluid trapped in the bonnet should be designed to prevent its internal pressurization greater than both the upstream and downstream piping, or the motor operator should be designed to overcome such	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER
pressurization. EPRI should revise Section 12.3.2.3.3 of			NRC Review
Chapter 1 to require that provisions be made for the			
because of the importance of information regarding the conversion of torque to thrust (i.e., stem factor). As a clarification of Section 6.2.2.1.4 of Chapter 5 regarding the capability of isolation valves to close against conditions that may exist during events requiring containment isolation, the isolation valves should be designed and test-qualified to be able to isolate flow resulting from a pipe break at the worst-case differential pressure (e.g., a condition resulting from a failure to scram the reactor in a timely manner), because the potential for a break in a line from the reactor vessel would likely be greatest when the reactor pressure was abnormally high. Pending modification of these sections, the staff will evaluate this during its review of individual applications for final design approval and design certification in accordance with the above positions."		NRR/	EMEB

P.1.V-78

Status: Onen

Industry Position

Next Action: ALWR

Action Description

NAC Position

leak rate testing for individual containment isolation valve (12.2.2)

#### Abstract

(DSER, p 1.12-8) responded to the requirement desc Passive Requirer plant designer to subjected to Typ 10 CFR Part 50 required for CIVs Section 12.2.7.1 Document, which testing of essenti OM Part 10. Fur specific inservice the Passive Requ design certificatio EPRI's position the testing requirement Requirements Do the staff has also result in individua not acceptable. of individual appl certification in ac

) "In its letter dated August 1, 1991, EPRI e staff's request by explaining that the minimized in Section 6.2.2.2 of Chapter 5 of the ments Document is intended to require the minimize the number of valves that will be e C testing in accordance with Appendix J to rather than to set down the type of testing . EPRI's response also referred to of Chapter 1 of the Passive Requirements requires the plant designer to provide for ial valves in accordance with ASME/ANSI thermore, EPRI stated that the designation of testing requirements is beyond the scope of uirements Document and properly belongs in on documentation. The staff disagree: with hat the designation of specific inservice ents is beyond the scope of the Passive ocument. For the reasons discussed above, o determined that EPRI's response will not	(DSER) See Abstract	(ALWR) Respond to DSER
al CIV leakage rate testing and is, therefore, The staff will evaluate this during its review ications for final design approval and design cordance with the above staff position."	NRR/I	NRC Review

Last 8/18/92 Updated:

P.1.V-79

Status: Open

Next Action: NPC

frequency and extent of disassembly and inspection of safety-related pumps (12.2.3)

that will establish the frequency and the extent of disassembly and inspection of safety-related pumps, including the basis for the frequency and the extent of each disassembly. In its letter dated August 1, 1991, EPRI responded to this request by referring to its position that was provided in the responses to RAIs 210.39(c) and (d). The staff's evaluation of these responses is discussed above. For similar reasons to those discussed above, the staff will evaluate this issue during its review of individual applications for final design approval and design certification."		
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NRC Review

NRR/EMEB

Last 8/19/92 Updated:

P.1A.O-1

Status: Open

Next Action: NRC

reporting of core-damage-frequency results as mean values (1.7)

Abstract (DSER, p 1A.1-9) "The staff requires that the EPRI guidance be revised to require reporting of mean value core-damage-frequency results, wherever possible."	Industry Position The URD will be changed to require "mean value core damage frequency wherever possible"	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change

NRC Review

NRR/PRAB

Last 8/6/92 Updated:

agrativi riv.	Assumption/Groundrule	Rationale	Re
1.2.3	Core Demage Frequency Requirement _ a mean value	Core Damage Frequency Requirement	(
	The plant design shall be such that a real slic assessment of the core-damage frequency will produce an estimate no higher than 1x10 <sup>-6</sup> events/reactor year (including both Internal and external events).	This requirement minimizes the financial risk to the utility from loss of the large capital investment in the generating sta- tion. The public astimate as defined in Section 1.3 has been obseen for this comparison-	
1.3	POINT ESTIMATE QUANTIFICATION	POINT ESTIMATE QUANTIFICATION	
\$ In.	For each primary event input into the PR4 model, a point estimate will be derived to represent that event in calculating the frequency of event sequences. The mean value shall be the point estimate used for this purpose. These mean values shall be obtained for core damage sequences and radionuclide release categories of interest.	PRA results, in the form of realistic beat estimates for the fre- quarcy of core damage and the frequency of serious radionicilide release, will be used to compare against the ALWR Requirements Document values given to Chapter 1. Section 1.4.1. The use of sean input values for quartifica- tion and comparison to the ALWR Top-Level Requirements has been specified for several reasons. First, the use of mean values is reasonable, since in the absence of formal propagation of uncertainty, their use in the quantification process provides the most meaning to point estimate. As a practical nester, for the passive plant this point estimate should be very close to the true mean value, since it is unlike- ly that combinations of identibel independent events whose uncertainty distributions would be correlated will be important to the results. Putthermore, the mean value is typically in- fluenced by the extreme values in the uncertainty distribution. Por example, for an event whose probability of failure is repre- sented by a lognormal distribution with an error factor of 3 (a typical distribution for a basic event in a PRA model), the mean value is at about the bith percentile of the distribution. Thus, the use of point estimates calculated from mean input values for comparison against the ADWR criteria provides added assurance that the design le robust, even accounting for random variability in equipment of human performance, or leck of precise the two addes of failure area.	

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Status: Open

Next Action: NAC

point-estimate quantification (1.8)

Abstract (DSER, p 1A.1-9) "As noted in Sections 1.9 and 6 of this DSER appendix, a point-estimate quantification by itself is not adequate and must be supplemented by an uncertainty analysis with uncertainties propagated from basic event uncertainties, including uncertainties on phenomenological issues."	Industry Position We feel that the most appropriate approach to deal with the problems of uncertainty is to perform an extensive set of censitivity studies. However, the URD will be modified to require a propagation of uncertainties for dominant sequences in the Level 1 PRA.	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change

NRC Review

NRR/PRAB

Last 8/6/92 Updated:

ME III, CHAPTER 1, APPENDIX A: PRA KEY ASSUMPTIONS AND GROUNDRULES         Assumption/Groundria         Assumption/Groundria         Assumption/Groundria         Assumption/Groundria         Core Damage Frequency Requirement         The plant design nhall be such that a realific assessment of the point design nhall be such that a realific assessment of the requirement maintrizes the financial rule of the number of the realization assessment of the requirement maintrizes the financial rule of the realization assessment of the realization of control content control control control control control control c	a	0	•	0	0	
ME III, CHAPTER 1, APPENDIX A: PRA KEY Assumption/Groundrule Assumption/Groundrule Core Damage Frequency Req uterment The plant design shall be such that a realistic assessment of the core damage frequency will produce an estimate no higher than 1x10's events/reactor year (induding both Internal and external events) POINT ESTIMATE QUANTIFICATION For each primary event input (no the PPA model, a point ee- timatewill be derived to repredent that event in calculating the frequencies shall be proper that event in calculating the point estimate used for this purpole. These mean values shall be propregated intrough the PFA model, a point ee- timatewill be doneed to repredent that event in calculating the frequencies shall be contained for core barmage soquences and indonuclide releable collatined in the relating	Retionale	Core Damage Frequency Requirement	This requirement maintizes the financial rich of the utsity from loss of the large capital investment in the generating sta- tion. The polal astimate as defined in Section 1.3 has been ckeen for this compartson-	POINT ESTIMATE QUANTIFICATION	PRA results, in kite form of realistic bdet estimate for the fre- quency of core damage and the frequency of serious radionabilitie release, sell be used to compare against the ALWR Requirements Dequiment values given lo Chapter 1. Section 1.4.1. The use of been input values for qualingtifica- tion and comparison to the 6MWR Top-Lewel Requirements thon and comparison to the 6MWR Top-Lewel Requirements thon and comparison to the 6MWR Top-Lewel Requirements thon and comparison to the 6MWR Top-Lewel Requirements	propagation of uncentainty, their use in the subsence of normal propagation of uncentainty, their use in the quantification proceeds provides the most measuringly is point estimate. As a practical heters, to the passive plant this point estimate. As a practical heters, to the passive plant this point estimate. As a practical heters, to the passive plant this point estimate. If that combinations of toeshore the mean welfue, since it is unlike in the results. Pupthetione would be correlated will be important to the results. Pupthetione would be correlated will be important to the results. Pupthetione would be correlated will be important to the results. Pupthetione whoes a probability of tatihat alon for example, for an event mean values in the uncentainty distribution there a lognormus distribution with an error factor of 3 (a hypical distribution for a basic event in a PRM model), the mean value is at about the distribution mean in use of the distribution Thue, the use of point estimating calculated from mean in use whoes for ophyperison against the AbwR orferts provides added assurbings that the design ja provide the mean in use added assurbings that the design ja provide the addited for random variability in equipment on human performance.
	Assumption/Groumdrule	Core Damage Frequency Requirement p man value	The plant design shall be such that a realistic assessment of the core damage frequency will produce an estimate no higher than 1x10 <sup>-6</sup> events/reactor year (inducting both internal and external events)	POINT ESTIMATE QUANTIFICATION	For teach primary event input anto the PRA model, a point ee- timate will be deelwed to represent that event in calculating the frequency of event sequences. We mean value shall be the point estimate used for this purpose. These mean values ahall be propagated through the PRA models, and point estimate frequencies shall be obtained for core damage sequences and radionucides release categories of interest.	

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#### Insert 1 (A/G)

1.3 QUANTIFICATION

Point estimates of the risk measures of interest shall be obtained. To the extent practicable, these point estimates shall be mean values. Where formal propagation of uncertainty is not performed, the point estimates shall be obtained by propagating mean values for primary events.

# QUANTIFICATION

To the extent possible, these point estimates should be mean values, or values that are consistent with mean values. Where point estimates are used to characterize risk results, the mean value is the representation that is most commonly used. In cases for which the meaningful propagation of probability distributions to calculate an actual mean value is not possible or not practical, use of mean values for the input parameters provides the most consistent and meaningful results.

# VOLUME III, CHAPTER 1, APPENDIX A: PRA KEY ASSUMPTIONS AND GROUNDRULES

aregraph No.	Assumption/Groundrule	Rationale	Rev.
1.5	POINT ESTIMATE QUANTIFICATION (CONTINUED)	POINT ESTIMATE QUANTIFICATION (CONTINUED)	0
	In the event that the PRA analysts choose to propagate the on- certainty distributions for primary events through the se- quence quantification, the recuting mean frequencies shall be used for comparison to the quantitative risk criteria presented in Chapter 1, Section 1.4.1.	Some PRA analysts may choose to perform a more rigorous propagation of the sources of uncertainty that can be easily represented in a quantitative manner. In such cases, the cal- culated mean values should be compared to the risk criteria, rather than some other parameter of the distribution (such as the median or 95th-percentile value). The qualitative evalua- tion should still be performed for this case, however, for the reasons outlined in Paragraph 1.4.	0)
1.4	UNCERTAINTY TREATMENT	UNCERTAINTY TREATMENT	6
	A careful assessment of the potential impact on risk due to un- certainties shall be medie, as outlined below.	A thorough understanding of important sources of uncertain- ty is essential to a proper perspective on the risk results and ineights. Although point-estimate values will be used for com- parison to the quantitative objectives, it is important that their context be clearly established. Insights gained from an as- sessment of uncertainties may appropriately result in addition- al, or different, risk-based decisions regarding particular design features.	3
mant (	A qualitative uncertainty analysis, shall be performed as part of the PRA. This analysis shall, as a minimum, involve the iden- tification and description of the potentially important sources of uncertainty, and an assessment of the significance of these uncertainties with respect to the results and conclusions of the PRA.	Many of the most important sources of uncertainty do not readily fund the neeters to meaningful quantitative treatment. It is important that the analysts give careful, systematic con- sideration to the sources of uncertainty that could be impor- tant and to the impact each of these sources might have on the results.	3
TT	Le quantitation uncertainty assessments) shalf be supplemented with a	Section 12.7 of NUREG/CR-2300 (Ref. 2) describes methods for such analysis, and Section 12.3.2 of NSAC-60 (Ref. 4) provides #// application of a qualitative uncertainty analysis.	

Page A.1-6

P04

## Insert 2 (A/G)

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Quantitative assessments of uncertainty shall be performed, to the extent that they are practical and meaningful. The nature of the quantitative uncertainty assessments for each element of the PRA is defined in Section 6.

# Insert 2 (rationale)

Quantitative assessments of uncertainties can supplement point estimates of risk by providing important perspectives on the results. The nature of these quantitative assessments should be commensurate with the ability to characterize uncertainties and the meaningfulness of the results obtained, as described in Section 6.

# VOLUME III, CHAPTER 1, APPENDIX A: PRA KEY ASSUMPTIONS AND GROUNDRULES

Paragraph No.	Assumption/Groundrule	Rationale	Re
1.4	UNCERTAINTY TREATMENT (CONTINUED)	UNCERTAINTY TREATMENT (CONTINUED)	
2 1.4.2	The <b>destination</b> uncertainty analysis shall be supplemented by a series of quantitative sensitivity studies that investigate the potential impact of particularly important uncertainties. Fur- ther specification of potential sensitivity studies is provided throughout the remaining guidelines presented in this docu- ment, and is summarized in Section 6.	Quantitative sensitivity studies provide a further important perspective with respect to the potential effects of variability in assumptions, parameter values, etc. on the risk measures of interest. Investigating important issues that lend themsel- ves to quantitative treatment is a necessary element in risk- based decision-making concerning the designs.	
1.5	DOCUMENTATION	DOCUMENTATION	
	The PRA shall be thoroughly documented, as outlined below.		
1.5.1	The models, data and assumptions for each portion of the PRA shall be formally documented to a sufficient level of detail such that an independent group and recreate the results with a minimum level of interaction with the original analysts. This documentation shall include at least the following: <ul> <li>The reviews made of industry experience and of the plant design to arrive at a comprehensive set of initiating events.</li> </ul>	Documentation of the PRA at this level is important for several reasons, including establishing credibility with the NRC and other reviewers; ensuring that the PRA is suitable for use as a "living model" of the plant, as called for in Sec- tion 11.6.3 of Chapter 1; providing the information needed to support the development of the Reliability Assurance Pro- gram; and supporting the plant reliability and availability analyses.	
	<ul> <li>The system interactions and success criteria that form the bases for the core damage event trees.</li> <li>The system fault-tree (or equivalent) models, including assumptions regarding design details not yet available, types of failure modes included and excluded, the treatment of dependent failures, reviews made for human interactions, and coordination with the reliability data base</li> </ul>	More extensive guidance on documentation for PRA can be found in NUREG/CR-2300 (Ref. 2), NUREG/CR-2815 (Pef. 3), and in Documentation Design for PRA, EPRI Report NP-3470 (Ref. 43).	
	<ul> <li>The details of the human reliability analysis, as described later in Section 2.9.</li> </ul>		

#### Paragraph No. Assumption/Groundrule Rationala Rev UNCERTAINTY AND BENSITIVITY ANALYSES 6 UNCERTAINTY AND SENSITIVITY ANALYSES 0 uncertainty and Senathrity studies shall be performed for those issues or A comprehensive set of sensitivity studies is needed to pro-0 parameters that are judged to have relatively large espociated vide adequate perspective with respect to uncertainty in the uncertainty or that are particularly important to the PRA PRA results and the significance of potential contributors to results). These separativity studies shall include limportant risk. As discussed in Paragraph 1.4, such studies are conaspects from each of the areas buillned below. The sensitivity Unserk sidered to provide more meaningful input to the plant desigstudies may be qualitative or quantitative, depending on the ner and to decision-makers regarding the areas that are nost nature of the Issue being addressed. important with respect to risk. This section describes many R of the areas in which densitivity should be considered a unertainly most cases, this that represents a complication of the stude suggested in individual sections of this document... ANALYSIS OF SYSTEMS AND SEQUENCES ANALYSIS OF SYSTEMS AND SEQUENCES 0 Areas that may be of particular importance with respect to the These are the primary areas that may be rooft uncertain or 0 estimated frequency of core damage include the following: are likely to be important to phentrequency of core pamaged This paragraph as rev. in [4] They also include some areas that are of interest for other reasons, as outlined below. 8.1.1 Frequencies of rare initiating events that are important con-Initiating events with very long recurrence intervals inherently 0 tributors to risk, and any initiating events whose frequencies have the potential for large uncertainty. For some initiating are assessed to be low relative to similar events for other events, feetures unique to the passive plant may warrant nuclear power plants, or that are unique to the passive plant iower best-estimate frequencies; these should be explored so designs. that the rationale for and effects of the lower frequencies are adequately understood and communicated.

# VOLUME III, CHAPTER 1, APPENDIX A: PRA KEY ASSUMPTIONS AND GROUNDRULES

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Uncertainties in the results of the PRA shall be investigated through appropriate quantitative and qualitative assessments. Propagation of uncertainties shall be performed where it is feasible and provides useful results." Quantitative and qualitative sensitivity studies shall be performed where propagation is not practical, or where the uncertain issues do not readily lend themselves to quantitative treatment.

#### INSERT X

For the frequency of core damage, probability distributions shall be developed for each of the primary events in the plant models These distributions shall be propagated to provide a quantitative characterization of both the mean core-damage frequency and uncertainty associated with that frequency.

This propagation shall be supplemented with welldefined sensitivity studies to investigate sources of uncertainty that do not readily lend themselves to quantification.

Areas that may be of particular importance ....

Propagation of probability distributions for primary events in the level 1 portion of a PRA is a standard task in most PRAs, and is relatively straightforward to accomplish. In addition to potentially providing further insight into the features of the plant design important to risk, the propagation of uncertainties permits the mean coredamage frequency to be calculated. This allows accounting for correlations among the failure data that could cause the propagation only of mean values to result in a result different from the mean core-damage frequency. Sensitivity studies are are a more effective means to investigate "modeling" uncertainties, and to consider alternative views of some reliability data.

(it is only asked for level I PAA).

P.1A.O-3

Status: Open

Next Action: ALWR

quantitative treatment of uncertainties (1.9)

Abstract (DSER, p 1A.1-1) "The Passive Requirements Document should provide guidance and a framework for systematically conducting and interpreting sensitivity analyses and for identifying those issues that require further consideration in the context of a quantitative uncertainty analysis. Essential elements of this framework that should be specified in the Passive Requirements Document include: (1) initial screening of issues for applicability to the passive design, (2) sensitivity analyses to further delineate issues of potential risk significance, and (3) systematic analysis of issue uncertainty as part of a broader assessment of uncertainty in the overall risk measures. It should be noted that the treatment of uncertainties for Level 2 issues need not be as extensive as that of NUREG-1150, but must be such that the staff has reasonable assurance that the PRA reflects the significance of kny actions, events, and phenomena for the plant design and the effectiveness of the accident-mitigation systems "	Industry Position See P.1A.O-2	NRC Position (DSER) See Abstract	Action Description NRC review the response to P.1A.O-2
systems."			

NRC Review

NRR/PRAB

Last 7/15/92 Updated:

# P.1A.O-4

Status: Open

Next Action: NPC

guidance on presenting results of PRA (1.10)

Abstract (DSER, p 1A,1-12) "In addition to the expanded guidance in Section 1.5, the Passive Requirements Document should require reporting of the following:	Industry Position The staff asks to specifically present some results. The URD will be modified to take that into account.	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
<ul> <li>the frequency of challenging passive decay heat removal (passive residual heat removal or isolation condenser), and the leading contributions to this frequency (the combinations of failures most likely to cause this event)</li> <li>the frequency of challenging the passive inventory makeup systems, and the leading contributions to this frequency of systems to the frequency of challenging the depressurization function, and the leading contributions to this frequency (for some designs, this will be the same as challenging passive inventory makeup systems; for others, it will not)</li> <li>the conditional probability that the depressurization function will fail to reduce the reactor coolant system pressure to the point at which gravity injection can function as designed, and the leading contributions to this event</li> <li>the conditional probability that the staging of the depressurization will fail in such a way as to affect the fuel adversely (e.g., excessive blowdown caused by opening too many valves or the wrong valves first), and the resulting occupational exposure to the workforce</li> <li>the frequency with which depressurization will actuate spuriously, and the leading contributions to this event</li> <li>the method of truncation used in the quantification process</li> </ul>	For the last additional remark about the conditional probability of failures of the different sources of gravity injection, it has no reason to be written in the parr aph "form of results" and should be put in another place. Moreover some sensitivity studies have already been asked for that purpose in section 6.1.2 and 6.1.3.	NRR/	NRC Review PRAB
In addition, the Passive Requirements Document should provide PRA guidance on providing a thorough assessment of the conditional probability that the sources of gravity injection (core makeup tanks, incontainment refueling water storage tank, GDCS, etc.) will, for some reason, be unable to perform their functions as required (e.g., lack of inventory, improper chemistry, human error, leaks)."			
		L. L.	ast 8/18/92

# VOLUME III, CHAPTER 1, APPENDIX A: PRA KEY ASSUMPTIONS AND GROUNDRULES

aragraph No.	Assumption/Groundrule	Rationale	Rev
1.5	DOCUMENTATION (CONTINUED)	DOCU IENTATION (CONTINUED)	3
	<ul> <li>The data base used for initiating event frequencies, com- ponent failure rates, common-cause failure rates, and maintenance unavailabilities, including an assessment of the applicability of available data for particularly important types of events or components.</li> </ul>		3
	<ul> <li>The sequence quantification process, including how any truncation was applied and how sequence-specific aspects such as recovery events were handled.</li> </ul>		3
	<ul> <li>The development of the containment event tree and the rationale for events included and excluded.</li> </ul>		3
	<ul> <li>The bases for the selection of best-estimate values for the events in the containment event tree and a discussion of the potential ranges of these values.</li> </ul>		3
	• The bases for the source-term characterizations.		3
1.5.2	The results of the PRA shall be compiled and presented in such a manner that they clearly convey the quantitative risk measures, the aspects of plant design and operation that are important contributors to those risk measures as well as those responsible for limiting risk, and the effects of important sour- ces of uncertainty.	Clear explanations of the key results is crucial both to proper- ly characterizing the comparisons of the assessed risk measures to the overall safety criteria for the plant design, as well as to understanding the significance of the results in a qualitative manner. The discussions of results should be aug- mented by clear tabular and graphical representations. Specific forms of presentation are discussed further in Chap- ter 13 of the PRA Procedures Guide (Ref. 2).	3
1.5.3	The formal documentation for the PRA shall include a sum- mary of the manner in which the PRA effort was integrated into the design process. Specifically, it shall discuss any sig- nificant design changes or decisions made based at least in part on use of the PRA models and data.	Documentation of the use of the PRA in the design process is required by Section 11.6.3 of Chapter 1. It is important to demonstrate that the design process appropriately benefited from the insights available from the PRA.	3
	Page A.1-8	I doest here	



# Add to the Rationale of Volume III, Chapter 1A, Section 1.5.2

In order to understand the significance of the results with respect to passive plant concepts, the documentation should address and describe the quantification of specific events such as: 1) the frequency of challenging passive decay heat removal and important contributions to this frequency, 2) the frequency of challenging the depressurization function and the passive inventory makeup systems, 3) the frequency of spurious depressurization, and 4) the conditional probability that depressurization will fail or that the staging of depressurization will fail (e.g., excessive blowdown caused by opening too many valves or the wrong valves).

P.1A.0-5

Status: Open

Next Action: NRC

guidance on modeling detail required to represent passive system behavior (2.1)

Abstract (DSER, p 1A.2-2) "EPRI should provide guidance that states that the language in the Passive Requirements Document regarding modeling is the minimum level of sophistication required, and that more careful and detailed modeling of some systems (e.g., consideration of a continuous or more finely discretized spectrum of selected physical process variables) may be necessary to adequately represent system behavior."	Industry Position The industry asumes that the functional operation of passive systems have to be demonstrated on a deterministic basis (testing programs for example.) The probabilistic tool can not be used to make assumptions regarding the design performance characteristics of passive systems. Probabilistic analysis is based on the probabilities of failure of the different components which lead to physical consequences based on testing or deterministic studies. The PRA will use the testing information and studies generated for designing the externe to possible	NRC Position (DSER) See Abstract	Action Description NRC review this response
	the spectrum of the second products.		NRC Review

NRR/PRAB

Last 7/15/92 Updated:

P.1A.O-6

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Status: Open

Next Action: NPC

guidance on modeling interactions between passive and active systems (2.1)

Abstract (DSER, p 1A.2-2) "EPRI should provide guidance on modeling potential systems interactions between passive and active systems, since the philosophy of passive plants appears to be to use non-safety-grade active systems as the first line of defense in the event of a transient."	Industry Position Industry agrees that the potential systems interactions have to be taken into account. It will be integrated into the requirements.	NRC Position (DSEH) See Abstract	Action Description NRC review pen & ink change

NRC Review

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NRR/PRAB

Last 8/6/92 Updated:

# VOLUME III, CHAPTER 1, APPENDIX A: PRA KEY ASSUMPTIONS AND GROUNDRULES

Paragraph No.	Assumption/Groundrule	Rationale	Rev
2.6	MODELING OF DEPENDENCIES	MODELING OF DEPENDENCIES	0
	The potential for dependent failures shall be considered in a comprehensive manner and shall be treated quantitatively using the best available methods. The types of dependencies that shall be treated explicitly are outlined in the following paragraphs.	Dependencies have the potential to defeat redundancy in the design, and they deserve careful attention in PRA. This is par- ticularly true for the ALWR since the greater degree of redun- dancy called for in the design requirements would tend to make dcpendencies relatively more important. It is particular- ly important to understand the potential effects of such de- pendencies on an integrated level for the plant.	0
2.6.1	Sequence Functional Dependencies	Sequence Functional Dependencies	0
The interaction 2.6.2	Sequence functional dependencies shall be incorporated into the sequence event trees or equivalent sequence logic. These functional dependencies indicate the effects of the status of one system or safety function on the success or failure of another, or of the same system in different configurations and/or performing different safety functions. Functional de- pendencies between systems or functions responsible for core cooling and containment systems shall be modeled explicitly.	This is required for proper modeling of the sequences. Both success and failure of a system can affect the performance of another system and the same system in a different con- figuration or role. Million In once case france and active systems have attracting secure once no onfoto system used as first like of defense attractof a to Inter-system Dependencies	0
Inter-system dependencies, including both hard-wired depen encles (e.g., through electric power, cooling water, interlocks permissives, etc.) and functional dependencies (e.g., ambien cooling, adequate net-positive suction word, etc.) shall be in cluded explicitly in the system fault the second other models.	Shared support systems or other inter-system dependencies may result in bypassing intended redundancy or diversity in the systems designed to prevent core damage.	0	
P.1A.0-7

Status: Open

Next Action: NRC

guidance for developing the success criteria for passive systems (2.3)

Abstract (DSER,p 1A.2.2) "The staff believes that the fundamental differences between active and passive design concepts will necessitate a different approach to defining the success criteria, and that the Passive Requirements Document should provide additional guidance on this aspect of the PRA."	industry Position It is not the role of probabilistic studies to define the success criteria, but rather the role of deterministic studies (thermal-hydraulic studies for example.) Specific analysis will have to be done to determine the success criteria of the plant taking into account active systems, passive systems and their possible interactions. It will be a large number of studies, but the approach is not different from the current process.	NRC Position (DSER) See Abstract	Action Description NRC review this response
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NRC Review

NRR/SRXB

Last 7/15/92 Updated:

P.1A.O-8

Status: Open

Next Action: ALWR

determination of an appropriate mission time (2.10)

Abstract (DSER, p 1A.2-9) "the staff concludes that the Passive Requirements Document should be revised to require that (1) the scope of the PRAs performed for passive plant designs be expanded to include treatment of the plant evolutions and system functions (active and passive) necessary to bring the	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER
condition of 400°F, and to maintain either of these conditions for the long term, and (2) mission times be determined and justified by the plant designer consistent with this expanded scope."			

NRC Review

NRR/SRXB

Last 8/18/92 Updated:

P.1A.0-9

Status: Open

Next Action: ALWR

requirements to address those important passive design-specific areas of uncertainty (6.1)

Abstract (DSER, p 1A.6-2) "The staff requires EPRI to provide guidance on how a full uncertainty analysis will be performed for the Level 1 portion of the PRA, with uncertainties propagated from basic events, including initiating event frequencies, data, common cause/mode failure, success	Industry Position See P.1A.O-2	NRC Position (DSER) See Abstract	Action Description See P.1A.O-2
criteria, and human error."			

NRC Review

NRR/PRAB

Last 7/15/92 Updated:

P.1A.O-10

Status: Open

Next Action: NRC

failure rate for the main stepup transformers (8.2)

Abstract (CAN NOT FIND THE REFERENCED SECTION "8.2" HENCE CAN NOT DETERMINE THE ISSUE -JDT 4/29/92)	Industry Position NGC should clarify this "issue"	NRC Position (DSER) See Abstract	Action Description NRC clarity this issue
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NRC Review

NRR/SELB J. Lazevnick

Last 7/15/92 Updated:

SUES	osed(Cert) Next Action: none		e URD is (DSER) See Abstract Action Description	NRR / PRAB NRR / SRXB	Updated 8/6/92	Printed on: 8/18/92
/R/NRC OPEN ISS	Status: Clo		Agree but no change to the needed.			ge 11
ALW	P.1A.V-1	long-term decay heat remove <sup>1</sup> in the PRA (1.£)	Abstract Abstract (DSER, p 1A.1-7) "In response to staff questions in this area. EPRI indicated that the Passive Requirements Dr.pument will be revised to include (1) an addition to Section 2.3.3.7 of Chapter 1 to require that "all operating conditions (including shutdown ones) shall be taken into account" in the PRA analysis and (2) additional requirements in Appendix A to Chapter 1 to encumpass shutdown conditions within the PRA. The Appendix A modifications will require a Level 1 analysis and a simplified evaluation of release frequencies and magn/tudes for shutdown conditions. EPRI also proposed an additional section in the Pascive Requirements bocument providing guidance for the conduct of a simplified PRA for conditions other than full power. The staff has not yet completed its review of the simplified method and is evaluating the need for consideration of external events during shutdown.	The modifications proposed by EPRI are noteworthy and go a long way toward addressing staff concerns regarding the trunctional assessment of plant response and the systematic treatment of ascessment of plant response and the systematic treatment of asceidents initiated in modes other than full-power operation. However, the Passive Requirements Document does not provide sufficient guidance regarding treatment of long-term DHR in the PRA. Based on the above considerations and the evaluations de scribed in Chapter 5, the staff concludes that the scope of the PRA for passive plant designs must include treatment of all plant evolutions and system tunctions (active and passive) necessary to bring the reactor to cold shutdown and to maintain this condition for the long term. The PRA must model (1) all equipment that the NRC requires to be available in passive plants to prevent operator is likely to attempt to use to prevent or mitigate any include consideration of accident-management measures or strategies for establishing and maintain this condition for containment heat removal. Mission times for associated plant equipment must be justified and consistent with this objective as discussed in Section 2.10 of this appendix. The staff will evaluate thres aspects of the PRA during its review	design certification.	Pag

P.1A.V-2

Status: Open

Next Action: ALWR

justification of mission times and success criteria (2.10)

#### Abstract

(DSER, p 1A.2-9) "Although the risk significance of long-term core cooling may not be as great for passive plant designs in absolute terms, the results of the French studies suggest that greater attention should be paid in the PRA to events outside the 24-hour time window that has been traditionally assumed in the PRA. This may be particularly important for passive plant designs in that they use a combination of passive and non-safety active systems to perform long-term residual heat removal, and that the reliability of these systems may be less than for current plant designs. In view of the potential risk contribution from plant operations later than 24 hours, the staff considers the guidance on mission time in the Passive Requirements Document to be inadequate.

On the basis of the considerations discussed above, as well as in Section 1 of this DSER Appendix, the staff concludes that the Passive Requirements Document should be revised to require that (1) the scope of the PRAs performed for passive plant designs be expanded to include treatment of the plant evolutions and system functions (active and passive) necessary to bring the reactor to (a) cold shutdown and (b) a static shutdown condition of 400°F, and to maintain either of these conditions for the long term, and (2) mission times be determined and justified by the plant designer consistent with this expanded scope. This will necessitate consideration of mission times considerably longer than 24 hours, as well as explicit treatment of actions by on-site operating staff and offsite support organizations that may need to be accomplished within this timetrame. Determination of an appropriate mission time should be based on consideration of (1) passive and active system performance and reliability late in an event, (2) availability and reliability of available backup systems or components, and (3) actions required to be taken by operating staff and offsite response organizations, and the provisions that would be in place to ensure such actions could be taken in a timely manner. Mission times may be different for going to cold shutdown and static shutdown. The different types of equipment and operator actions needed to go to these modes. must be reflected explicitly in the system and function success criteria (see Section 2.3). Mission times and success criteria will have to be justified by the plant designer and will be reviewed by the staff as part of the final design approval process for each passive design PRA."

Industry Position **NRC** Position Action Description (DSER) See Abstract (ALWR) Respond to DSER **NRC Review** NRR / PRAB Last 8/19/82 Updated:

P.1A.V-3

Status: Open

Next Action: ALWR

reliability data (2.11)

Abstract (DSER, p 1A.2-11) "Reliability data for non-safety-related (but normally safety-related in tradi-tional PWRs and BWRs; components must be justified on the basis of the quality of the equipment purchased, test intervals, capability to perform its intended function in an adverse environment, experimental data, and applicable technical specifications. This is part of the overall concern regarding the regulatory treatment of non-safety-related systems for the passive plant designs. This is an open issue that must be satisfactorily resolved	Industry Position	NRC Position (DSER) See Abstract	Action Description (ALWR) Respond to DSER
This is an open issue that must be satisfactorily resolved before the staff can complete its review of Appendix A to Chapter 1."			

NRC Review

NRR/PRAB

Last 8/19/92 Updated:

P.1A.V-4

Status: Closed(Cert)

Next Action: none

review of core-damage-sequence binning (4.1)

Abstract (DSER, p 1A.4-1) "In Section 4.1 of Appendix A to Chapter 1, EPRI states that core-damage sequences are expected to be binned (grouped). If core-damage bins are used, they must be defined so that all sequences within a particular bin lead to similar effects with respect to containment sequence and source term phenomena. EPRI requires that the definition of bins provide a means to ensure that the defineation of core-damage sequences is discriminated sufficiently to afford the proper level of coordination with the containment analysis. This is intended to provide (1) a means of managing the number of accident sequences and (2) an additional means of gaining information needed for the in-plant analysis. The binning of sequences is an acceptable procedure to limit the number of containment analyses performed. As EPRI states, it is necessary that all sequences within a bin lead to similar effects with respect to containment and source term phenomena. The staff will	Industry Position Agree	(DSER) See Abstract	Action Description
containment and source term phenomena. The staff will review core-damage-sequence binning when the design-specific PRA is submitted."			

NRC Review

NRR/PRAB

Last 7/17/92 Updated:

Next Action: none

P.1A.V-5

Status: Closed(Cert)

review of actual groupings of the accident sequences into plant damage states (4.2)

Action Description

NRC Review

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NRR/PRAB

Last 7/17/92 Updated

P.1A.V-6

Status: Open

Next Action: ALWR

review of the evaluation of containment leakage paths (4.3)

*steam generator tube rupture (FWR only) *residual heat removal isolation failurs high-pressure coolant injection (BWR only) *core spray (BWR only) *core spray (BWR only) *cedwater and main steam (BWR only) *headwater and main steam (BWR only) In the NUREG-1150 studies for Surry and Sequeyah, bypass sequences dominate early fatality risk. The staff agrees that containment bypass sequences are important and, therefore, agrees with the EPRI requirement to assess such sequences. The staff notes, however, that the requirement to assess all connections to the reactor coolant system may be unrealistic; otherwise, even instrument lines would need to be considered. The staff suggests that EPRI modify this section to incorporate some screening criteria below which connected piping would not need to be addressed in detail."	Abstract (JSER, p 1A.4-3) "Section 4.4 of Appendix A to Chapter 1 requires that containment bypass sequences be assessed and include all connections to the reactor coolant system. EPRI states that containment bypass sequences can result in significant releases from the containment and have the potential to be important risk contributors. Examples of bypass sequences that have been identified as important in past PRAs include	Industry Position	NRC Position (DSER) See Abstract	(ALWR) Respond to DSER
In the NUREG-1150 studies for Surry and Sequevah, bypass sequences dominate early fatality risk. The staff agrees that containment bypass sequences are important and, therefore, agrees with the EPRI requirement to assess such sequences. The staff notes, however, that the requirement to assess all connections to the reactor coolant system may be unrealistic; otherwise, even instrument lines would need to be considered. The staff suggests that EPRI modify this section to incorporate some screening criteria below which connected piping would not need to be addressed in detail."	*steam generator tube rupture (PWR only) *residual heat removal isolation failurs *high-pressure coolant injection (BWR only) *core spray (BWR only) *feedwater and main steam (BWR only)			
	In the NUREG-1150 studies for Surry and Sequeyah, bypass sequences dominate early fatality risk. The staff agrees that containment bypass sequences are important and, therefore, agrees with the EPRI requirement to assess such sequences. The staff notes, however, that the requirement to assess all connections to the reactor coolant system may be unrealistic; otherwise, even instrument lines would need to be considered. The staff suggests that EPRI modify this section to incorporate some screening criteria below which connected piping would not need to be addressed in detail."		NRR. NRR.	NRC Review SPLB PRAB

Last 8/19/92 Updated: 1

P.1A.V-7

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Status: Closed(Cert)

Next Action: none

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computer codes for in-plant sequence assessment (4.4)

	and the second	Industry Position	NAC Position	Action Description
Abstract (DSER, p 1A.4-3) "ection states that the MAAP con- assess the thermal-hydr involved in accident pro- of MAAP as an integrate the staff concludes that reliance on MAAP and 1 dealing with deficiencies the staff is concerned the MAAP code (or other co- adequately treat certain phenomena, and that the the MAAP code will not in the field. A particular adequacy of the code for has not been demonstra- staff.	t n 4.5.2 of Appendix A to Chapter 1 ode will be the primary tool used to aulic and other physical processes gression. While recognizing the value ed code for severe-accident analysis, this requirement places an undue ails to establish a requirement for of the this code. More specifically, hat for best-estimate calculations, the des for that matter) will not physically important severe-accident be generally accepted by the experts concern for passive plants is that the r predicting natural circulation flows ated by EPRI and assessed by the	Agree	(DSER) See Abstract	
In its response to a staf EPRI proposed a modif Document to further c which use of codes other success criteria for core phenomena that are no subject to large uncertai addresses the staff's cor MAAP code for determin to review applications for certification against the approved by the NRC a acceptability of the plan case-by-case basis."	f request for additional information, ication to the Passive Requirements by, by example, the situations in ar than MAAP might be more imples were "to develop realistic cooling, or to investigate specific t addressed by MAAP or that may be nties." This modification adequately nearn regarding the adequacy of the sing success criteria. The staff intends or final design approval and design codes most recently endorsed and it that time, and will evaluate the t designer's analyses on a			NRC Review
				Last 7/17/92 Updated:
	Pr	ige 17		Printed on: 8/18/92



Abstract (DSER, p 1A.5-2) "As part of design certification for each passive ALWR, the staff will require ALWR vendors to provide an assessment of additional risk measures (such as person-rem, and early and latent fatalities) to support the vendor's assessment of Severe Accident Litigation Design Alternatives (SAMDAs) for the ALWR design. Meteorological data alone is insufficient to calculate these additional risk measures, and will need to be supplemented with bounding population data, such as that provided in Regulatory Guide 4.7."	Industry Position • Annex B has been totally modified to be consistent with 10CFR100 • The paragraph of the DSER seems to ask to put data on bounding population in the URD. We need this request clarified.	NAC Position (DSER) See Abstract	Action Description NRC review the modified Annex B(Rev 3) NRC clarify second concern
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NRC Review

NRR/PRPB J. Lee

Last 8/19/92 Updated:

P.1A.V-9

Status: Closed(Cert)

Next Action: none

differences in computer codes used for calculating offsite consequences (5.2)

Abetract	1	Industry Position	I NDC Position	Action D	ecciption
(DSER, p 1A.5-2) "ection 5.2.2 of Appendix A to Chapter 1 states that either MACCS or CRAC2, or another suitable code, will be used for calculating offsite consequences. Although the CRAC2 code provides an acceptable characterization of the consequences of severe accidents, the MACCS code represents an improvement over CRAC2 and is preferred by the staff for calculating cancer risk. The present version of MACCS (Version 1.5) uses the results of the BEIR III study in the calculation of health effects. However, the BEIR III study has been superseded by the BEIR V study. The BEIR V results indicate a higher cancer risk from low levels of ionizing radiation than did the earlier BEIR III report. The results of the BEIR V study should be taken into account in the calculation of health effects. The staff is preparing an	Agree	mousary Position	(DSER) See Abstract	Action D	escription
addendum to NUREG/CR 4214, Revision 1, Part II, to address the modification of models resulting from recent reports on the health effects of ionizing radiation. The risk coefficients for fatal cancers would be approximately doubled or tripled by the model modifications (memorandum dated April 11, 1990, from J. M. Taylor, NRC, to Chairman K. M. Carr, "Evaluation of Recent Reports on Health Effects of Low-Level Ionizing Badiation"). Until these modifications are				NRC Review	
incorporated into MACCS, the staff concludes that the use of CRAC2 is acceptable, but that the effect of model differences must be taken into account in interpreting risk results. The staff will address this issue during its review of an individual application for final design approval and design certification.				NRR/PRPB J. Lee	

Last 7/17/92 Updated:



Status: Open

Next Action: NRC

source terms for represent vive accident sequences are bounded by the physically-based source term (6.3)

Abstract (DSER, p 1A.6-5) "In a February 7, 1991 response to an NRC question concerning plant certification issues contained in SECY-91-151, EPRI stated that the plant designers must confirm as part of the PRA that the source terms for representative accident sequences for their actual standard plant designs are bounded by the physically-based source term in the Requirements Document. However, no mention of the need for PRA analysts to perform this source term assessment is made in Appendix A to Chapter 1.	Industry Position Agree. However, for Volume III, the changes to address this issue are being made to Chapter 5, Section 2.4.1.2 instead of to Chapter 1A, Section 4.9.	NRC Position (DSER) See Abstract	Action Description NRC review proposed URD revision (Rev 4)
In response to staff concerns regarding the lack of guidance on this matter in Appendix A, EPRI indicated that "as part of the on-going source term development, additional guidance will be provided to ensure that this check on the physically-based source term relative to those derived in the PRA is made."			
By letter dated March 19, 1992, EPRI subsequently provided a new section 4.9 to Chapter 1, Appendix A which re aires that designers confirm that the PRA source terms for representative accident sequences for their design are bounded by the physically-based source term used in licensing calculations. The staff considers this acceptable, and will evaluate this analysis as part of the design certification review for each ALWR PRA."		NRI	NRC Review R/PRPB J. Lee

Last 8/19/92 Updated:

# VOLUME III, CHAPTER 5: ENGINEERED SAFETY SYSTEMS

Paragraph No.	Requirement	Rationale	Rev
2.4	MITIGATION	MITIGATION	0
2.4.1	Source Term Definition	Source Term Definition	0
2.4.1.1	A physically-based source term shall be used as the passive plant accident mitigation feature design basis as defined for each standard plant design in Appendix B.	A physically-based source term is being required as the design basis for the Passive ALWR in order to factor in the source term experience gained in nearly thirty years since TID 14844 was issued. The physically-based source term also provides coupling of the source term and containment thermal-hydraulics, thereby assuring a more consistent, rational basis for containment design features and mitigation systems as well as a <b>near receive consistent</b> associated physically based source term will be specific to that design.	0
		Appendix B defines the physically-based source term for a passive PWR and a passive BWR meeting the ALWR requirements. The report, "Estimate of Physically-Based Source Term for Passive Advanced Light Water Reactors," provides the basis for the various aspects of the Appendix B source terms.	0
2.4.1.2	The Flant Designer shall confirm that, for the core damage event used as the basis for estimating the physically based source term, the source term for the standardized plant design is bounded by the source term in Appendix B.	This is necessary to assure that the actual standardized plani design systems and features are consistent with the specified source term.	0
	Sec attachment		

Page 5.2-14

Requirement: The Plant Designer shall empare the first product release to the environment for functional sequences lypes (see Chapter 5- Section E. 5. 2.3) greater than approximately 10" for year, with the firm product release to the environment from the updated design far source tan. Cases after which the PRA release exceeds the design source this release stand be reported and reflained.

Reflace 2. 4. 1. 2. by the following

-Ratimale:

The PRA provides a significant amount of information on the integrated plant service accident feiformance, and a comparison to assure that there are no protochilistically important sequences with fixin product release greater than the daign horis provide additional confidence in the updated source term.



Abstract (DSER, p 12.2-9) "the staff concludes that EPRI's source terms for the design of the radioactive waste processing systems given in Passive Requirements Document Table 12.1.1 are inconsistent with SRP Sections 11.2 and 11.3. The staff considers that the 0.25-percent failed fuel percentage for	Industry Position The industry disagrees, however, it has been determined that the system designs are not likely to be affected, and thus the URD will be modified to accomodate the NRC's	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
a PWR, specified in the Passive Requirements Document, and the 100,000 $\mu$ Ci/sec noble gas release rate (30 minutes' decay) for the offgas system for a BWR specified in the Passive Requirements Document are inadequate bases for designing radioactive waste processing systems and evaluating offsite radioactive nuclide concentration in effluents in accordance with the limits specified in 10 CFR Part 20."	position. We will modify the URD to require use of SRP 11.2 and 11.3 unmodified for regulatory conformance evaluation.		

NRC Review

NRR/SPLB Chandra

Last 8/6/92 Updated:

1005422

# VOLUME III, CHAPTER 12: RADIOACTIVE WASTE PROCESSING SYSTEMS

Paragraph No.	Requirement	Rev.
1.5	POLICY STATEMENTS	0
	ALWR program policy statements regarding radioactive waste processing systems (RWPS) follow. They are intended to assist the reader in gaining an understanding of the requirements given in subsequent sections and the approach that was taken in their formulation.	0
1.5.1	Good Neighber Policy	0
	The Good Neighbor policy as stated in Volume I is that the plant be a good neighbor to its surrounding environment and population, and re- quirements to limit radioactive releases from normal operation shall be defined. The radioactive release limitations will apply to solid waste ship- ment quantities and radioactive liquid and radioactive gaseous release quantities to the environment.	0
	Volume I top tier design requirements which apply to radwaste are the fol- lowing Plant Characteristics:	0
licensing -	. The design basis for radioactive waste processing shall use a select	2
agen expected	fuel rate consistent with regulatory requirements. For purposes of nor- mal operation performance evaluation, the Designer shall utilize either	, X , NUREG
,~~1	ANGLANS 18.1 or .025% failed fuel for PWRs, and a noble gas release rate of 15,000 uCl/sec at 30 minutes for BWRs shall be utilized. (Also see Table 12:11.)	Review Pians 11.1 and 11.2.
	<ul> <li>The ALWR shall be designed and constructed so that the amount of radioactive gaseous, liquid and solid waste released from the plant shall be equal to or better than comparable values for the 10% best plants of the same type (i.e., BWR or PWR) currently operating in the U.S.</li> </ul>	0
	In order to specify the design requirements to limit radioactive releases of liquids and gases, operating plant data were obtained from the then most recently available (1984 and 1985) annual reports of the radioactive materials released from nuclear power plants in the U.S. (NUREC/CR-2907). The 10% best PWR and BWR plants were determined for both gaseous and liquid releases. This data base does not represent the plants operating in the U.S. at the time of these requirements, however, the data chosen present an adequate goal.	0
	This data source gives neither fuel leakage information nor the relative amounts of radioactivity released from gaseous radwaste and from ventila- tion air sources. It is thus not possible to define the specific basis for the performance of these plants. Nevertheless, on a comparative basis, the 10% best plants were established and are to be used as a reference condi- tion for use in evaluating ALWR designs.	0

#### Table 12.1-1



#### FUEL SOURCE TERM FOR RADWASTE SYSTEM DESIGN

- ANSI/ANS 18.1 is periodically updated to reflect cumulative experience and may be revised prior to the finalization of any design. The version of ANSI/ANS 18.1 used for design should be checked for consistency with NUREG-0016 and NUREG-0017 and, if there are any substantive differences, made consistent with NRC evaluations.
- \*\* The Designer may use either the source terms in ANSI/ANS 18.1 or the value indicated in this table.

Delete the table

## VOLUME III, CHAPTER 12: RADIOACTIVE WASTE PROCESSING SYSTEMS

2

Paragraph No.	Require	ment		Rev
1.5.1	Good Neighbor Policy (Continue	id)		0
to state	It should be realized that the amore vironment via the liquid and gased gree of fission product input from into ventilation air via valve and of The radioactivity removal mechan tive waste processing systems set radioactivity. To properly design beyond the regulatory requirement of fuel leakage and input of radioactivity the values of fuel leakage of Teble t5:2:)	unts of redioactivity bus pathways are a fuel defects and of her radioactive equi isms of the liquid ar ve to limit and com the systems to mee its it is necessary to activity into ventilation 12.1-1 are to be us	released to the en- measure of the de- radioactivity input ipment seal leakage. Ind gaseous radioac- trol release of it specific goals o specify the extent on air. To this end add (Sec. Section Free marmal, Section	o test operatio
	It is expected that design to releases based upon these values will com- pare favorably with those of the 10% best operating plants. Reasons for this are: The ALWR requirements provide a number of features to eliminate or reduce input of racioactive substances into the liquid and gaseous radwaste systems or into the environment. These include valve designs to minimize leakage into ventilation air and into liquids, a go if of zero fuel leakage and minimal fuel manufacturing defects, materials im- provements to limit Cobalt 60 production, and the Requirements of this chapter for the radwaste systems, etc. (See Appendix B.)			0
	For the solid wet and dry radioac study by Sargent and Lundy usin foundation.	tive wastes volumet g EPRI reports NP3	s were derived from a 370 and NP5526 as a	0
	The norms of platformance based upon the best operating plants are:			0
	GASEOUS	EFFLUENTS		0
	Policy Basis	BWR	PWR	0
	Total radioactivity, excluding tritium, will be equal to or lower than the 1984-85 10% best plants of the same type in the U.S.	2000 Ci./yr.	200 Ci./yt.	0
	LIQUID EFFLUENTS			0
	Burt but by 1 by	a second second second		

# VOLUME III, CHAPTER 12: RADIOACTIVE WASTE PROCESSING SYSTEMS

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Peregraph No.	Requirement	Rev.
1.6.1	Good Neighbor Policy (Continued)	0
	SOLID WASTES	0
	Low level dry and wet waste 3500 Cu.Ft./yr. 1750 Cu.Ft./yr. will be equal to or lower than the 10% best plants of the same type in the U.S.	0
	Dry waste volumes are based on the as-compacted form for the compac- tible fraction of dry wastes and on the as-shipped form for non-compac- tible dry wastes. Wet waste volumes are based on the dewatered volume not the as-shipped volume.	0
	The ability to achieve the solid waste goals not only requires an ap- propriate design, but is dependent on (1) how the plant is operated and (2) national and local regulations established by agencies regulating form and concentration of wastes to be shipped and disposed. Requirements for shipping and disposal have been established by such agencies inde- pendently of how a plant is designed and operated.	0
	The Volume I good neighbor policy also includes requirements to limit non-radioactive, hazardous, and toxic chemical releases. As stated in 1.2 above, implementation of this aspect of the good neighbor policy is not in the scope of Chapter 12.	C
1.5.2	Fuel Source Term Parameters for RWPS Design and Evaluation	0
	The fuel defect source terms for RWPS design and evaluation have been selected to provide the bases for (1) evaluation of annual average off-site dose in accordance with 10CFR50, Appendix I, (2) evaluation of 24-hour off-site radionuclide concentrations in effluents in accordance with the limits of 10CFR20, and (3) evaluation of the RWPS performance for comparison with good neighbor policy goals.	2
	Table 12.1-1 shows the values to be used for the above purposes. For the PWR, the values are given in percent falled fuel. For the BWR, the release rates are measured in the GRWPS in terms of UCI/sec at 30-minute decay.	2
1.5.3	Base Line Design and Options	0
	A top tier design requirement (Volume I, page v) is that the ALWR "must be acceptable for most available sites in the U.S." From the viewpoint of the LRWPS, this means that the LRWPS is not designed for "zero liquid release."	0
	Page 12.1-9	

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# VOLUME III, CHAPTER 12: RADIOACTIVE WASTE PROCESSING SYSTEMS

Paragraph No.	Requirement	Rationale	Rev
2.2	KEY PERFORMANCE REQUIREMENTS	KEY PERFORMANCE REQUIREMENTS	0
2.2.1	Goals of Radioactive Releases and Waste Reduction	Goals of Radioactive Releases and Waste Reduction	0
2.2.1.1	The radioactive waste processing systems shall (in concert with other features specified in the Requirements Document) enable the ALWR to meet the goals of reducing radioactive releases and of reducing solid low level waste volume from the ALWR plant.	This is an ALWR program general requirement and is re- quired to meet the "good neighbor" policy of Section 1.5.1.	0
2.2.1.2	The Plant Designer shall demonstrate for the given design that the expected inputs to the radwaste processing systems and process methods result in outputs that meet Chapter 12 and overall ALWR objectives and policies.	This will show that the ALWR objectives and requirements relative to reducing radwaste inputs and outputs are met and that effective processing methods are employed. The Plant Designer should consider the information provided in ANS/ANSI Standards 55.1, 55.4, 55.6, and 40.35 as a design base, as modified by the changes due to the ALWR.	0
2.2.2	Source and Input Terms	Source and Input Terms	0
2.2.2.1 Licensing kragreph 1,5.1 en	Pesign basic fission product radioactivity concentrations in reactor coolant and associated release rates shall be based upon the fuel leakages given in Table 12.1.1. The several values given in Table 12.1.1 shall be used for the purposes stated in the policy statement of 1.5.2. The Plant Designer shall make the evaluation necessary to show that the licensing requirements and evaluations against "good neighbor" policy goals are met. Activation product source terms in reactor coolant shall be consistent with those given in NUREG-0016 for the BWR and in NUREG-0017 for the PWB and/in ANSI/ANS 18.1 for both.	The fission product and activation product bases for design are provided, along with requirements for evaluation of the design	2

Page 12.2-2

P.12.0-2

Status: Open

Next Action: NPC

basis for 2-minute delay requirement for BWR turbine gland seal system exhaust (3.3.1)

Abstract (DSER, p 12.3-5) "since EPRI requires only the use of essentially non-radioactive steam for the BWR turbine gland seal system, it is not clear why EPRI has identified a 2-minute delay line as a requirement for the offgases from the BWR turbine gland seal system exhaust under certain circumstances."	Industry Position Two minute delay for gland exhaust effluent was revised in Revision 2 in Figure 12.3-1 and Section 3.2.4.1.2. Two minute delay is no longer required, rather designer analysis.	NRC Position (DSER) See Abstract	Action Description NRC review this response

NRC Review

Last 7/16/92 Updated:

P.12.0-3

Status: Open

Next Action: NRC

production sources for "essentially nonradioactive steam" (3.3.1)

Abstract (DSER, p 12.3-5) "EPRI has not explained why essentially nonradioactive steam is preferred over totally clean steam for the BWR turbine gland seals and how such steam is to be produced."	Industry Position Totally clean steam will unnecessarily generate additional liquid radwaste because of the need to evaporate demineralized water at all times. Steam that has had sufficient time to decay N-16 is sufficient for this application. The normal source of such steam can be from anywhere in the turbine/ feedwater heating cycle where it can be demonstrated that N-16 is not a problem.	NRC Position (DSER) See Abstract	Action Description NRC review this response
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NRC Review

NRR/SPLB Chandra

Last 7/16/92 Updated:



Status: Open

Naxt Action: NIPC

discrepancy between Figure 12.3-1 and requirement in Cha r 13 (3.5.1)

Abstract (DSER, p 12.3-5) "Figure 12.3-1 does not reflect the requirement in Chapter 13"	Industry Position Agree. Chapter 13, Section 3.2.4.4 was changed in Rev. 3 to only require monitoring.	NRC Position (DSER) See Abstract	Action Description VRC review Rev. 3 of Chapter 13, Section 3.2.4.4.

NRC Review

NRR/SPLB Chandra

Last 8/18/92 Updated:

P.12.0-5

Status: Open

Next Action: NRC

use of post-filter downstream of charcoal adsorber in ventilation exhaust systems (3.3.3)

Abstract (DSER, p 12.3-7) "the staff concludes that it will be inappropriate to assume the regulatory guide efficiencies for the i. noval of elemental and organic iodine from the effluent streat if there is no HEPA filter downstream of the charcoal adsorber for collecting carbon fines."	Industry Position The ALWR position is that designers should meet regulatory dose criteria without charcoal. If this can be done, charcoal need not be installed and the question of downstream filters is moot.	NRC Position (DSER) See Abstract	Action Description NRC review need for charcoal and, if needed, newer industry standards.
	On the other hanc, charcoal is required, the ALWR program believes the most recent (1989) standards (N509/N510) should be used. Those design standards call for "bag filters downstream of charcoal, not HEPAs. This change is made possible by the advances in charcoal technology and quality.		
	The NRC should continue the dialog with the ALWR and not remain with old and outdated requirements.		NDC Davian
			NHC Neview
		NPP	SPLB Chandra

Last 7/16/92 Updated:

Next Action: NRC

P.12.0-6

Status: Open

guidance regarding direct piping from radio active plant systems to sumps or waste collection tanks (BWR) (4.2)

Abstract (DSER, p 12.4-4) "EPR' I work provided adequate guidance or requirements regarding usest piping from radicactive plant systems to sumps or radicactive waste collection tanks to eliminate potential sources of airborne radicactivity for BWRs."	Industry Position Agree - As stated, it is misleading in that it implies applicability to PWRs only, which was not the intent. We will modify requirement 4.2.2.2 to make it clear that direct piping of drains applies to BWRs as well as	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
	PWRs.		

NRC Review

NRR/SPLB Chandra

Last 8/6/92 Updated:

# VOLUME III, CHAPTER 12: RADIOACTIVE WASTE PROCESSING SYSTEMS

Paragraph No.	Requirement	Rationale	Rev.
4.2.2.2	Segregation Within Subsystems	Segregation Within Subsystems	0
4.2.2.2.1	In the PWR, reactor coolant which normally contains hydrogen and may contain fission gases shall be collected in covered drain tanks or routed directly via CVCS to the borated waste processing subsystem.	Hydrogen containing wastes must be kept from entry of oxygen by exclusion or by nitrogen blanketing. A covered tank is one wherein air is excluded by use of diaphragms or inert gas blanketing in a non-vented tank.	0
4.2.2.2.2	Liquid radioactive wastes from non-hydrogen bearing (PWR) radioactive or potentially radioactive plant systems shall be directly piped to sumps or tanks in the various buildings, or to radwaste collection tanks.	Wastes are directly piped; open funnels or routing via trenches is not permitted. The wastes are thereby contained and are not a source of alrhome radioactivity.	0
Bick radioactive	<ul> <li>At least one floor drain sump in LRWPS service in each building shall be a building low point.</li> </ul>	<ul> <li>Floor drain sumps collect building drainage. Equipment drain sumps (or tanks) need only be below equipment drain elevations.</li> </ul>	0
ant systems /	<ul> <li>Wastes routed to sumps shall flow by gravity.</li> </ul>	<ul> <li>In most cases, there is no driving force for flow other than gravity.</li> </ul>	0
o bian	<ul> <li>The leakage from pump shaft seals and water from pump casing drains shall be collected and routed to the ap- propriate LRWPS subsystem, as defined in Section 4.2.2.1.</li> </ul>	<ul> <li>Pump drainage needs to be routed to the LRWPS sub- system provided for the type of water which is present.</li> </ul>	0
	<ul> <li>Pump baseplate drains shall be routed to the floor drain subsystem because these may be contaminated with oil.</li> <li>However, every effort shall be made to minimize oil leakage and to keep it out of LRWPS. See Section 4.2.2.3.3</li> </ul>	<ul> <li>Baseplate drains can be different from pump seal water. The use of mechanical seals also minimizes the leakage from seals.</li> </ul>	0

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P.12.0-7

Status: Open

Next Action: NFC

requirements for LRWPS filter housing and components (4.2)

Abstract (DSER, p 12.4-4) "EPRI has not provided adequate guidance or requirements for filter housing and components. This is an outstanding issue that must be resolved before the staff can complete its review of Chapter 12."	Industry Position This is addressed directly in Chapter 1, Section 12.9 generally and Sections 12.9.1.1 and 12.9.2 specifically; and indirectly in Chapter 12, Section 2.2.2.2 by reference to ANS/ANSI 55.6.	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
	To clarify this, we will modify Chapter 12 to refer to Chapter 1, Section 12.9		

NRC Review NRR/SPLB Chandra

Last 8/6/92 Updated:

# VOLUME III, CHAPTER 12: RADIOACTIVE WASTE PROCESSING SYSTEMS

	Requirement	Rationale	Rev.
Paragraph No.	Connect Desig Tente (DWD)	Covered Drain Tanks (PWR)	0
4.5.8	The reactor coolant drain tank and the auxiliary building Grain tank and/or its equivalent in the LRWPS shall have adequate provisions to prevent release of radioactive gases and for exvgen exclusion to prevent hydrogen explosions. Typical in-	Fluid contained in these tanks will not have been degassified so personnel radiation exposure due to releases is an impor- tant concern for meeting ALARA requirements. Hydrogen must be controlled to preclude the possibility of explosion.	0
	dustry methods include the use of a diaphragm cover and/or	WOEMENTS-LRWPS	
X FI	an inert cover gas. LTERS QHO (4.5.9.1 ION EXCHANGER REG Ion Exchangers) FILTER	*** Ion Exchangers	0
1.0.0		Resin Type	0
(4.5.9.1	The resins used shall be strong acid styrene-divinylbenzene cation and strong base quarternary amine resins except where special ion selective resins are used.	These resin types show the best removal characteristics for the variety of ions requiring removal.	0
1.	2 Desis Form	Resin Form	0
4.5.9.7	The resin form, H+ for cation resin and OH- for anion resin, shall be selected, except in Boron service.	H+ and OH- resins provide the best removal capacity.	0
1	3 Constal Regine	Special Resins	0
9.5.9.8	When treated wastes are to be discharged to the environment rather than recycled for reuse, the addition of a bed of sodium- aluminum silicate type ion exchanger, e.g., large-port Mor- denite, shall be considered and qualified for use upstream of the mixed hed.	This zeolite material has shown a large capacity for radio- cesium and thus shows potential for more economical processing and reduced solid radioactive waste; however, its use should first be qualified by testing. (See EPRI NP-5099.)	0
Chaj roga for o	ater 1 Section 12.9 provides equipment inorments for filters and ion archange all water treating systems including LRW	ens PS.	
	Page 12.4-56		

P.12.0-8

Status: Open

Next Action: NRC

requirements for LRWPS filters (4.2)

	Abstract (DSER, p 12.4-4) "EPRI has not provided adequate guidance or requirements for various types of filters in the LRWPS including the capability to disassemble, reassemble, and replace internal components,"	Industry Position This is addressed directly in Chapter 1, Section 12.9 generally and Sections 12.9.1.2 and 12.9.2.7 specifically; and indirectly in Chapter 12, Section 2.2.2.2 by reference to ANS/ANSI 55.6. To clarify this we will modify Chapter 12 to refer to Chapter 1, Section 12.9	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
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NRC Review

NRR/SPLB Chandra

Last 8/6/92 Updated:

# VOLUME III, CHAPTER 12: RADIOACTIVE WASTE PROCESSING SYSTEMS

Paragraph No.	Requirement	Rationale	Rev.
4.5.8	Covered Drain Tanks (PWR)	Covered Drain Tanks (PWR)	0
	The reactor coolant drain tank and the auxiliary building drain tank and/or its equivalent in the LRWPS shall have adequate provisions to prevent release of radioactive gases and for oxygen exclusion to prevent hydrogen explosions. Typical in-	Fluid contained in these canks will not have been degassified so personnel radiation exposure due to releases is an impor- tant concern for meeting ALARA requirements. Hydrogen must be controlled to preclude the possibility of explosion.	0
V -	an inert cover gas.	QUIREMENTS-LRWPS	
4.5.9	Ion Exchangers	Ton Exchangers X	0
4.5.9.1	I Resin Type	Resin Type	0
	The resins used shall be strong acid styrene-divinylbenzene cation and strong base quarternary amine resins except where special ion selective resins are used.	These resin types show the best removal characteristics for the variety of lons requiring removal.	0
4.5.9.2	Aesin Form	Resin Form	0
	e resin form, H+ for cation resin and OH- for anion resin, shall be selected, except in P-pron service.	H+ and OH- resins provide the best removal capacity.	0
4.5.9.9	3 Special Resins	Special Resins	0
	When treated wastes are to be discharged to the environment rather than recycled for reuse, the addition of a bed of sodium- aluminum silicate type ion exchanger, e.g., large-port Mor- denke, shall be considered and qualified for use upstream of the mixed bed.	This zeolite material has shown a large capacity for radio- cesium and thus shows potential for more economical processing and reduced solid radioactive waste; however, its use should first be qualified by testing. (See EPRI NP-5099.)	0
Chap rogu for a	ater 1 Section 12.9 provides equipment inements for filters and ion exchange all water treating systems including LRW Page 12.4-56	ers.	

P.12.0-9

Status: Open

Next Action: NRC

requirements for LRWPS ion exchangers. (4.2)

Abstract (DSER, p 12.4-4) "EPRI has not specified design considerations and operational requirements for ion exchangers (e.g., addition and removal; retention; strainers; underdrains; and disassembly, assembly, and replacement of internal components)."	Industry Position This is addressed directly in Chapter 1, Section 12.9 and 12.9.3 generally and Sections 12.9.1.1, 12.9.1.2, 12.9.3.13 through 12.9.3.14 specifically; and indirectly in Chapter 12, Section 2.2.2.2 by reference to ANS/ANSI 55.6. To clarify this, we will modify Chapter 12 to refer to Chapter 1, Section 12.9	NRC Position (DSER) See Abstract	Action Description NRC review pen & ink change
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NRC Review

NRR/SPLB Chandra

Last 8/6/92 Updated:

# VOLUME III, CHAPTER 12: RADIOACTIVE WASTE PROCESSING SYSTEMS

Darmaraah No	Requirement	Rationale	Rev.
A 5 0	Covered Drain Tanks (PWR)	Covered Drain Tanks (PWR)	0
4.3.0	The reactor coolant drain tank and the auxiliary building drain tank and/or its equivalent in the LRWPS shall have adequate provisions to prevent release of radioactive gases and for oxygen exclusion to prevent hydrogen explosions. Typical In-	Fluid contained in these tanks will not have been degassified so personnel radiation exposure due to releases is an impor- tant concern for meeting ALARA requirements. Hydrogen must be controlled to preclude the possibility of explosion.	0
	dustry methods include the use of a diaphragm cover and/or	WREMENTS-LRWPS	
× FIL	an inert cover gas. (4.5.9.1 ION EXCHANGER REG TZRS 940 Ion Exchangers FILTERS	"Ion Exchangers X	0
1	I Bacin Tune	Resin Type	0
(4.5.9.1,	The resins used shall be strong acid styrene-divinylbenzene cation and strong base quarternary amine resins except where special ion selective resins are used.	These resin types show the best removal characteristics for the variety of ions requiring removal.	0
4503	Reein Form	Resin Form	0
4.3.3.4	The resin form, H+ for cation resin and OH- for anion resin, shall be selected, except in Boron service.	H+ and OH- resins provide the best removal capacity.	0
aroa	Special Resins	Special Resins	0
4.3.3.8	When treated wastes are to be discharged to the environment rather than recycled for reuse, the addition of a bed of sodium- aluminum silicate type ion exchanger, e.g., large-port Mor- denite, shall be considered and qualified for use upstream of the mbxed bed.	This zeolite material has shown a large capacity for radio- cesium and thus shows potential for more economical processing and reduced solid radioactive waste; however, its use should first be qualified by testing. (See EPRI NP-5099.)	0
Char	ter 1 Section 12.9 provides againpment		
1	inoments for filters and ion exchange	~ )	
( for a	Il water treating dysteins including LRWI	ps.	
	Page 12.4-56		

none	Action Description	NRC Review SPLB Chandra	at 7/16/92 di: 8/18/92 on: 8/18/92
ert) Next Action:	(DSER) See Abstract	NRR / S	Update
Status: Closed(C	nt paths (2.2.8) Industry Position		
P.12.V-1	requirements for radioactive waste processing systems and effluen <b>Abstract</b> (DSER, p 12.2-13) "The staff concludes that the Passive Requirements Document does not adequately and explicitly address all associated regulatory requirements for control, monitoring, and sampling of radioactive wasts processing systems and effluent paths. Therefore, the staff will review the plant-specific design for the control, monitoring, and effluent paths against the criteria in SRP Section 11.5 during the review of an individual application for final design approval and design certification."		Page 10

## P.12.V-2

Status: Closed(Cert)

Next Action: none

GRWPS hydrogen control design (3.3.4)

Abstract	Industry Position	NRC Position	Action Description
(DSER, p12.3-8) "Although EPRI committed, in Chapter 1 of the Passive Requirements Document, to comply with SRP Section 11.3, Chapter 12 of the Passive Requirements Document does not address all the criteria in the SRP. The staff expects that applicants referencing the Passive Requirements Document will comply with the SRP, as committed to in Chapter 1"	Agree	(DSER) See Abstract	

NRC Review NRR/SPLB Chandra

Last 7/16/92 Updated:
## ALWR/NRC OPEN ISSUES

P.12.V-3

Status: Open

Next Action: NAC

design of dry waste shipping containers (5.5)

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Abstract (DSER, p 12.5-7) "the staff will review the design of shipping containers both for wet and dry solid wastes on a plant-specific basis against the acceptance criterion in SRP Section 11.4, "Solid Waste Management Systems' and applicable sections of 10 CFR Part 61."	Industry Position The NRC's observation is correct and is intended to be that way in the URD. That is, they do not specify shipping container design. However, it is not clear why shipping containers should be considered part of the plant design and license.	NRC Position (DSER) See Abstract	Action Description NRC review this response.
	The NRC should consider deleting shipping container design from the SRP 11.4 insofar as it relates to plant design.		

NRC Review

NRR/SPLB Chandra

Last 7/16/92 Updated:

Printed on: 8/18/92

## Enclosure 2

## List of DSER Issues in Chapters 1 and 1A with Responses Outstanding

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