

P. O. BOX 33189

DUKE POWER COMPANY

GENERAL OFFICES

422 SOUTH CHURCH STREET

CHARLOTTE, N. C. 28242

TELEPHONE: AREA 704
373-4011

February 26, 1985

OGTP-872-N-57

C. H. Berlinger
Office of Nuclear Reactor Regulation
U.S. Nuclear Regulatory Commission
Washington, D. C. 20555

Re: TDI Diesel Generator Owners Group
Request for Additional Information
File: MTS-4086

Dear Mr. Berlinger:

Per a verbal request from your staff during our February 21, 1985 meeting at the Riverbend Nuclear Power Plant, enclosed is a copy of the Riverbend 2800KW crankshaft torsional analysis and the support package for the deletion report on Riverbend component 03-650C.

Should you have questions, please call R. J. Deese at (704) 373-3489.

Very truly yours,

Richard W. Donsall

for C. L. Ray, Jr.
Technical Program Director
TDI Diesel Generator Owners Group

CLR/RJD/cr

cc w/attachment: W. W. Laity
J. R. Hamilton

cc w/o attachment: H. R. Denton
J. C. Kammeyer

8503130167 850226
PDR ADOCK 05000458
S PDR

3031
1/1

MEMORANDUM

TO: John Kammeyer
FROM: Lisa Shusto *LMS*
DATE: February 25, 1985
RE: Riverbend Torsional Analysis at 2800 kW Load

Enclosed is a copy of the torsional analysis results performed on Riverbend Nuclear Power Plant at a load of 2800 kW. The stresses for each cylinder are summarized and compared with those at a load of 3500 kW in Table 1. The TN values used for both the 3500 kW and 2800 kW analyses are presented in Table 2. If you have any questions, I may be reached at (415) 856-9400.

LMS/gg

Table 1
 NOMINAL SHEAR STRESSES AT 450 RPM FOR
 DSR-48 13-INCH BY 12-INCH CRANKSHAFT AT RIVERBEND

Location	Amplitude of Nominal Shear Stress (psi)	
	2800 kW	3500 Kw
Between Cylinder No. 1 and Cylinder No. 2	2355	3068
Between Cylinder No. 2 and Cylinder No. 3	2631	3293
Between Cylinder No. 3 and Cylinder No. 4	3873	4842
Between Cylinder No. 4 and Cylinder No. 5	4493	5666
Between Cylinder No. 5 and Cylinder No. 6	5978	7357
Between Cylinder No. 6 and Cylinder No. 7	5272	6191
Between Cylinder No. 7 and Cylinder No. 8	4842	5977
Between Cylinder No. 8 and Flywheel	4799	5903

Table 2

TN VALUES FOR ANALYSES

<u>3500 kW</u>	<u>2800 kW</u>
3.449E+01	2.759E+01
9.193E+01	7.905E+01
1.500E+02	1.280E+02
1.123E+02	9.419E+01
9.775E+01	8.365E+01
7.703E+01	6.595E+01
6.065E+01	5.251E+01
4.804E+01	4.237E+01
3.560E+01	3.187E+01
2.618E+01	2.435E+01
2.083E+01	1.924E+01
1.548E+01	1.465E+01
1.101E+01	1.063E+01
8.478E+00	8.021E+00
6.326E+00	5.801E+00
4.609E+00	4.536E+00
4.012E+00	3.355E+00
2.971E+00	2.688E+00
2.456E+00	2.221E+00
2.046E+00	1.629E+00
1.759E+00	1.524E+00
1.110E+00	9.367E-01
1.130E+00	1.258E+00
9.971E-01	8.272E-01
8.724E-01	6.586E-01

COMPUTER CALCULATION COVER SHEET

PROJECT NO.: PA07596

TASK NO.: DR65

Note: only 2800 KW RUN for Riverbend is attached

VALIDATED COMPUTER CODE:

SHAMS

0005

1

Name

Number

Revision

MAINTAINED AT: Failure Analysis Associates, VAX/780
2225 East Bayshore Road
Palo Alto, California 94303

DESCRIPTION OF CALCULATION

- REDUCED LOAD - RIVERBEND INPUT
Computer Runs at 2800, 3200, and 3300 KW loads for
Shoreham Nuclear Power Plant to determine peak
stresses

Computer Runs at ^{3200, 3300} 2800 and 3500 KW load for
Gulf States Nuclear Power Plant to determine
peak stresses

SUBJECT REPORT

TITLE: Memo to John Kaye REPORT NUMBER: _____

riverbend load that produces stresses
equal to those at Shoreham load of 3500KW

DATE: October 18, 1984

Lisa Shugh

10/11/84

R.N. Lusk

10/12/84

Engineer

Date

Reviewer

Date

SHAFT HARMONIC ANALYSIS BY MODAL SUPERPOSITION

GULF STATES UTILITIES COMPANY -- RIVERBEND NUCLEAR POWER STATION
 CRANKSHAFT TORSIONAL VIBRATION ANALYSIS OF 13/12 INCH CRANKSHAFT,

PAIR START VALVE-AVERAGED OVER 6 FIRINGS
 FIRING CHARACTERISTICS -- NORMAL

JOINT	INERTIA	STIFFNESS
1	0.0000E+00	0.0000E+00
2	0.222E+01	8.4727E+07
3	0.7922E+01	8.4727E+07
4	0.7922E+01	8.4727E+07
5	0.7922E+01	8.4727E+07
6	0.7922E+01	8.4727E+07
7	0.7922E+01	8.4727E+07
8	0.7922E+01	8.4727E+07
9	0.1498E+01	1.6941E+07
10	0.2655E+02	3.0972E+08
11	0.9761E+03	1.4090E+06

MODE NUMBER 1
 NATURAL FREQUENCY 15.89 RAD/SEC 2.48 HZ 148.86 R.P.M.

JOINT	DISPLACEMENT
1	0.01321
2	0.01321
3	0.01321
4	0.01320
5	0.01328
6	0.01319
7	0.01318
8	0.01317
9	0.01316
10	0.01314
11	0.01323

MODE NUMBER 2
 NATURAL FREQUENCY 238.54 RAD/SEC 37.97 HZ 2277.90 R.P.M.

JOINT	DISPLACEMENT
1	0.06682
2	0.06638
3	0.06388
4	0.05932

NATURAL FREQUENCIES AND MODE SHAPES

5 - 0.05286
6 - 0.04469
7 - 0.03509
8 - 0.02415
9 - 0.01284
10 - 0.00837
11 - 0.00357

MODE NUMBER 4
NATURAL FREQUENCY 107.01 HZ 6628.78 R.P.M

JOINT DISPLACEMENT

1 - 0.06343
2 - 0.06007
3 - 0.04499
4 - 0.01317
5 - 0.01001
6 - 0.04634
7 - 0.06181
8 - 0.06348
9 - 0.04492
10 - 0.01437
11 - 0.00210

MODE NUMBER 5
NATURAL FREQUENCY 146.54 HZ 8792.69 R.P.M

JOINT DISPLACEMENT

1 - 0.03906
2 - 0.03518
3 - 0.01519
4 - 0.01108
5 - 0.03356
6 - 0.03892
7 - 0.02566
8 - 0.00007
9 - 0.02556
10 - 0.03944
11 - 0.00374

MODE NUMBER 5
NATURAL FREQUENCY 188.87 HZ 11332.23 R.P.M

JOINT DISPLACEMENT

1 - 0.06399
2 - 0.05344
3 - 0.00248
4 - 0.05045
5 - 0.06328
6 - 0.02560
7 - 0.03238
8 - 0.06457
9 - 0.04533
10 - 0.01747
11 - 0.00081

MODE NUMBER 6
NATURAL FREQUENCY 250.38 HZ 15022.95 R.P.M

JOINT DISPLACEMENT

1	-0.06383
2	-0.04676
3	0.03356
4	0.06690
5	0.00659
6	-0.06294
7	-0.04437
8	0.03632
9	0.06616
10	-0.00770
11	0.00020

MODE NUMBER 7

NATURAL FREQUENCY = 1928.99 RAD/SEC 306.99 HZ 18419.63 R.P.M

JOINT DISPLACEMENT

1	-0.06390
2	-0.03607
3	0.06099
4	0.02970
5	-0.06409
6	-0.02301
7	0.06649
8	0.01606
9	-0.06817
10	0.00439
11	-0.00007

MODE NUMBER 8

NATURAL FREQUENCY = 2229.88 RAD/SEC 354.90 HZ 21293.82 R.P.M

JOINT DISPLACEMENT

1	-0.05894
2	-0.02462
3	0.07004
4	-0.03228
5	-0.04382
6	0.06788
7	-0.01133
8	-0.05868
9	0.05900
10	-0.00262
11	0.00003

MODE NUMBER 9

NATURAL FREQUENCY = 2461.13 RAD/SEC 391.70 HZ 23502.06 R.P.M

JOINT DISPLACEMENT

1	-0.04829
2	-0.01404
3	0.05287
4	-0.06990
5	0.04081
6	0.01171
7	-0.05751
8	0.07029
9	-0.04273
10	0.00150
11	-0.00002

MODE NUMBER 10
NATURAL FREQUENCY = 2608.41 RAD/SEC 415.14 HZ 24908.46 R.P.M

JOINT DISPLACEMENT

1 0.02856
2 0.00581
3 -0.03276
4 0.05473
5 0.06841
6 0.07170
7 -0.06411
8 0.04679
9 -0.02238
10 0.00860
11 0.00001

MODE NUMBER 11
NATURAL FREQUENCY = 3171.40 RAD/SEC 504.74 HZ 30284.69 R.P.M

JOINT DISPLACEMENT

1 0.36297
2 -0.06091
3 0.01795
4 -0.00529
5 0.00156
6 -0.00046
7 0.00014
8 -0.00004
9 0.00001
10 0.00000
11 0.00000

MODAL DAMPING

MODE PERCENT
1 0.02500
2 0.02500
3 0.02500
4 0.02500
5 0.02500
6 0.02500
7 0.02500
8 0.02500
9 0.02500
10 0.02500
11 0.02500

NUMBER OF TIME STEPS = 120
CODE FOR GENERAL LOADING = 0
CODE FOR ENGINE ANALYSIS = 1

NUMBER OF CYLINDERS = 8
NUMBER OF STROKES IN CYCLE = 4
CODE FOR V ENGINE = 0
V ANGLE = 0.00 DEGREES

ENGINE SPEED = 450.00 R.P.M.
 LEFT BANK TIMING = 0.00 DEGREES
 RIGHT BANK TIMING = 0.00 DEGREES

SPRING UNDER

1 4 7 3 8 5 2 6

HARMONIC	PRESSURE		INERTIA	
	COSINE	SINE	COSINE	SINE
1	1.000E+00	0.000E+00	1.000E+00	0.000E+00
2	1.820E+03	1.380E+06	1.380E+06	8.750E-08
3	1.700E+01	1.300E+06	1.300E+06	7.400E+03
4	1.200E+02	1.300E+06	1.300E+06	1.240E-08
5	1.090E+03	1.300E+06	1.300E+06	2.170E+04
6	2.060E+03	1.370E+04	1.300E+06	1.890E-08
7	2.890E+02	1.240E+02	1.200E+06	7.540E+03
8	2.310E+02	1.300E+06	1.300E+06	2.670E-08
9	2.270E+02	1.300E+06	1.300E+06	8.760E+02
10	1.900E+03	1.360E+06	1.300E+06	5.470E-08
11	1.670E+03	3.040E+03	1.300E+06	8.390E+01
12	1.480E+03	2.190E+03	1.300E+06	4.170E-08
13	1.200E+02	1.300E+06	1.300E+06	1.350E+01
14	7.090E+02	1.300E+06	1.300E+06	1.370E-08
15	2.250E+02	1.350E+02	1.300E+06	1.370E+00
16	6.320E+02	3.100E+02	1.300E+06	5.300E-08
17	4.860E+02	3.610E+02	1.300E+06	2.040E-01
18	4.220E+02	2.400E+02	1.300E+06	6.440E-08
19	2.760E+02	1.300E+02	1.300E+06	1.670E+02
20	2.670E+02	1.250E+02	1.300E+06	7.200E-08
21	1.650E+02	1.370E+01	1.300E+06	3.390E-03
22	1.830E+02	1.340E+02	1.300E+06	7.960E-08
23	1.480E+02	1.860E+01	1.300E+06	8.720E-08
24	9.540E+01	1.080E+01	1.300E+06	5.400E-05

CYLINDER LOADING FACTORS

CYLINDER	FACTOR
1	1.000
2	1.000
3	1.000
4	1.000
5	1.000
6	1.000
7	1.000
8	1.000

APPLIED LOAD HARMONICS

COSINE HARMONIC	JOINT OR MODE											
	1	2	3	4	5	6	7	8	9	10	11	
0	0.000E+00	5.480E+03	5.480E+03	5.480E+03	5.480E+03	5.480E+03	5.480E+03	5.480E+03	5.480E+03	5.480E+03	0.000E+00	0.000E+00
1	0.000E+00	-1.020E+04	-1.000E+04	1.428E+04	-1.414E+02	1.414E+02	-1.428E+04	1.000E+04	1.020E+04	0.000E+00	0.000E+00	0.000E+00
2	0.000E+00	5.170E+03	-5.170E+03	2.500E+04	-2.500E+04	-2.570E+04	2.500E+04	-5.170E+03	5.170E+03	0.000E+00	0.000E+00	0.000E+00
3	0.000E+00	4.120E+02	1.700E+04	1.173E+04	1.231E+04	-1.231E+04	-1.173E+04	-1.700E+04	4.120E+02	0.000E+00	0.000E+00	0.000E+00
4	0.000E+00	-1.090E+03	-1.090E+03	1.090E+03	1.090E+03	1.090E+03	1.090E+03	-1.090E+03	-1.090E+03	0.000E+00	0.000E+00	0.000E+00
5	0.000E+00	2.060E+03	-1.730E+04	-6.817E+03	-9.730E+03	9.730E+03	6.817E+03	1.730E+04	-2.060E+03	0.000E+00	0.000E+00	0.000E+00
6	0.000E+00	-2.090E+03	2.090E+03	-1.730E+03	1.730E+03	1.730E+03	-1.730E+03	2.090E+03	-2.090E+03	0.000E+00	0.000E+00	0.000E+00
7	0.000E+00	2.310E+03	7.280E+03	-6.781E+03	-3.514E+03	3.514E+03	6.781E+03	-7.280E+03	-2.310E+03	0.000E+00	0.000E+00	0.000E+00
8	0.000E+00	-2.270E+03	-2.270E+03	-2.270E+03	-2.270E+03	-2.270E+03	-2.270E+03	-2.270E+03	-2.270E+03	0.000E+00	0.000E+00	0.000E+00
9	0.000E+00	1.900E+03	3.960E+03	3.124E+03	4.144E+03	-4.144E+03	-1.457E+02	-3.960E+03	-1.900E+03	0.000E+00	0.000E+00	0.000E+00
10	0.000E+00	-1.670E+03	1.470E+03	3.124E+03	-3.124E+03	-3.124E+03	3.124E+03	1.670E+03	-1.670E+03	0.000E+00	0.000E+00	0.000E+00
11	0.000E+00	1.480E+03	2.190E+03	2.595E+03	5.020E+02	-5.020E+02	-2.595E+03	-2.190E+03	-1.480E+03	0.000E+00	0.000E+00	0.000E+00
12	0.000E+00	-1.170E+03	-1.170E+03	1.170E+03	1.170E+03	1.170E+03	1.170E+03	-1.170E+03	-1.170E+03	0.000E+00	0.000E+00	0.000E+00
13	0.000E+00	9.090E+02	-1.130E+03	-1.563E+02	-1.442E+03	1.442E+03	1.563E+02	1.130E+03	-9.090E+02	0.000E+00	0.000E+00	0.000E+00
14	0.000E+00	-7.250E+02	7.250E+02	-7.538E+02	7.538E+02	7.538E+02	-7.538E+02	7.250E+02	-7.250E+02	0.000E+00	0.000E+00	0.000E+00
15	0.000E+00	6.320E+02	5.200E+02	8.146E+02	7.920E+01	-7.920E+01	8.146E+02	-5.200E+02	-6.320E+02	0.000E+00	0.000E+00	0.000E+00
16	0.000E+00	-4.860E+02	-4.860E+02	-4.860E+02	-4.860E+02	-4.860E+02	-4.860E+02	-4.860E+02	-4.860E+02	0.000E+00	0.000E+00	0.000E+00
17	0.000E+00	4.220E+02	-2.400E+02	-1.287E+02	4.681E+02	-4.681E+02	1.287E+02	2.400E+02	-4.220E+02	0.000E+00	0.000E+00	0.000E+00
18	0.000E+00	-3.760E+02	3.760E+02	1.390E+02	-1.390E+02	-1.390E+02	1.390E+02	-3.760E+02	3.760E+02	0.000E+00	0.000E+00	0.000E+00
19	0.000E+00	2.460E+02	1.250E+02	2.623E+02	-8.556E+01	8.556E+01	-2.623E+02	-1.250E+02	-2.460E+02	0.000E+00	0.000E+00	0.000E+00
20	0.000E+00	-2.670E+02	-2.670E+02	2.670E+02	2.670E+02	2.670E+02	-2.670E+02	2.670E+02	-2.670E+02	0.000E+00	0.000E+00	0.000E+00
21	0.000E+00	1.650E+02	-3.500E+01	-9.192E+01	-1.414E+02	1.414E+02	-9.192E+01	3.500E+01	-1.650E+02	0.000E+00	0.000E+00	0.000E+00
22	0.000E+00	-1.830E+02	1.830E+02	1.340E+02	1.340E+02	1.340E+02	-1.340E+02	1.830E+02	-1.830E+02	0.000E+00	0.000E+00	0.000E+00
23	0.000E+00	1.480E+02	1.860E+01	-1.178E+02	9.150E+01	-9.150E+01	1.178E+02	-1.860E+01	-1.480E+02	0.000E+00	0.000E+00	0.000E+00
24	0.000E+00	-9.560E+01	-9.560E+01	-9.560E+01	-9.560E+01	-9.560E+01	-9.560E+01	-9.560E+01	-9.560E+01	0.000E+00	0.000E+00	0.000E+00

SINE HARMONIC	JOINT OR MODE											
	1	2	3	4	5	6	7	8	9	10	11	
1	0.000E+00	-1.000E+04	1.020E+04	-1.414E+02	-1.428E+04	1.428E+04	1.414E+02	-1.020E+04	1.000E+04	0.000E+00	0.000E+00	0.000E+00
2	0.000E+00	2.500E+04	-2.500E+04	-5.170E+03	5.170E+03	5.170E+03	-5.170E+03	-2.500E+04	2.500E+04	0.000E+00	0.000E+00	0.000E+00
3	0.000E+00	-1.700E+04	-4.120E+02	-1.231E+04	1.173E+04	-1.173E+04	1.231E+04	4.120E+02	1.700E+04	0.000E+00	0.000E+00	0.000E+00
4	0.000E+00	-6.600E+03	-6.600E+03	6.600E+03	6.600E+03	6.600E+03	6.600E+03	-6.600E+03	-6.600E+03	0.000E+00	0.000E+00	0.000E+00
5	0.000E+00	-1.170E+04	-2.060E+03	-9.730E+03	6.817E+03	9.730E+03	-6.817E+03	2.060E+03	1.170E+04	0.000E+00	0.000E+00	0.000E+00
6	0.000E+00	1.730E+03	-1.730E+03	-2.090E+03	2.090E+03	2.090E+03	-2.090E+03	-1.730E+03	1.730E+03	0.000E+00	0.000E+00	0.000E+00
7	0.000E+00	-7.280E+03	2.310E+03	3.514E+03	-6.781E+03	6.781E+03	-3.514E+03	-2.310E+03	7.280E+03	0.000E+00	0.000E+00	0.000E+00
8	0.000E+00	4.714E+03	4.714E+03	4.714E+03	4.714E+03	4.714E+03	4.714E+03	4.714E+03	4.714E+03	0.000E+00	0.000E+00	0.000E+00
9	0.000E+00	-3.960E+03	-1.900E+03	4.144E+03	-1.457E+03	1.457E+03	-4.144E+03	1.900E+03	-3.960E+03	0.000E+00	0.000E+00	0.000E+00
10	0.000E+00	3.124E+03	-3.124E+03	1.670E+03	-1.670E+03	-1.670E+03	1.670E+03	-3.124E+03	3.124E+03	0.000E+00	0.000E+00	0.000E+00
11	0.000E+00	-2.190E+03	1.480E+03	-5.020E+02	2.595E+03	-2.595E+03	5.020E+02	-1.480E+03	2.190E+03	0.000E+00	0.000E+00	0.000E+00
12	0.000E+00	1.532E+03	1.532E+03	-1.532E+03	-1.532E+03	-1.532E+03	-1.532E+03	1.532E+03	1.532E+03	0.000E+00	0.000E+00	0.000E+00
13	0.000E+00	-1.130E+03	-9.090E+02	-1.442E+03	1.563E+02	-1.563E+02	1.442E+03	9.090E+02	1.130E+03	0.000E+00	0.000E+00	0.000E+00
14	0.000E+00	7.538E+02	7.538E+02	-7.250E+02	7.250E+02	7.250E+02	-7.250E+02	-7.538E+02	7.538E+02	0.000E+00	0.000E+00	0.000E+00
15	0.000E+00	-5.200E+02	6.320E+02	-7.920E+01	-8.146E+02	8.146E+02	7.920E+01	-6.320E+02	5.200E+02	0.000E+00	0.000E+00	0.000E+00
16	0.000E+00	3.608E+02	3.608E+02	3.608E+02	3.608E+02	3.608E+02	3.608E+02	3.608E+02	3.608E+02	0.000E+00	0.000E+00	0.000E+00
17	0.000E+00	-2.400E+02	-4.220E+02	4.681E+02	1.287E+02	-1.287E+02	-4.681E+02	4.220E+02	-2.400E+02	0.000E+00	0.000E+00	0.000E+00
18	0.000E+00	1.390E+02	-1.390E+02	3.760E+02	-3.760E+02	-3.760E+02	3.760E+02	-1.390E+02	1.390E+02	0.000E+00	0.000E+00	0.000E+00
19	0.000E+00	-1.250E+02	2.460E+02	8.556E+01	2.623E+02	-2.623E+02	-8.556E+01	-2.460E+02	1.250E+02	0.000E+00	0.000E+00	0.000E+00
20	0.000E+00	6.570E+01	6.570E+01	-6.570E+01	-6.570E+01	-6.570E+01	6.570E+01	-6.570E+01	6.570E+01	0.000E+00	0.000E+00	0.000E+00
21	0.000E+00	-3.500E+01	-1.650E+02	-1.414E+02	-9.192E+01	9.192E+01	1.414E+02	1.650E+02	-3.500E+01	0.000E+00	0.000E+00	0.000E+00
22	0.000E+00	1.340E+02	-1.340E+02	-1.830E+02	1.830E+02	1.830E+02	-1.830E+02	1.340E+02	-1.340E+02	0.000E+00	0.000E+00	0.000E+00
23	0.000E+00	-1.860E+01	1.480E+02	-9.150E+01	-1.178E+02	1.178E+02	9.150E+01	-1.480E+02	1.860E+01	0.000E+00	0.000E+00	0.000E+00
24	0.000E+00	7.080E+01	7.080E+01	7.080E+01	7.080E+01	7.080E+01	-7.080E+01	-7.080E+01	7.080E+01	0.000E+00	0.000E+00	0.000E+00

APPLIED LOAD HARMONICS IN NORMAL COORDINATES

COSINE HARMONIC	JOINT OR MODE										
	1	2	3	4	5	6	7	8	9	10	11
0	5.782E+02	1.969E+03	6.513E+02	1.884E+02	-3.231E+02	3.039E+02	-9.913E+01	1.435E+02	-1.369E+01	-4.721E+01	-2.578E+02
1	-5.952E-01	-5.963E+02	1.044E+03	5.754E+01	6.395E+02	2.759E+03	-1.296E+03	-7.178E+02	-3.595E+02	2.225E+03	3.638E+02
2	-1.469E-01	-1.251E+02	-5.942E+02	-1.105E+03	-1.932E+03	1.711E+03	3.645E+03	-1.573E+03	-5.460E+03	-4.749E+02	-5.637E+02
3	8.806E-01	1.035E+03	-2.931E+03	-4.810E+02	2.493E+03	2.161E+03	-1.869E+02	6.017E+02	6.852E+00	-1.695E+02	2.021E+02
4	3.162E-02	2.672E+01	1.190E+02	2.029E+02	2.972E+02	1.342E+02	3.954E+01	-7.116E+01	-1.605E+02	-3.872E+00	4.245E+01
5	-5.618E-01	-5.968E+02	1.770E+03	3.037E+02	-1.674E+03	-1.635E+03	1.910E+02	-4.487E+02	-5.879E+00	1.542E+03	-3.186E+02
6	2.901E-02	2.428E+01	1.002E+02	1.555E+02	1.886E+02	-3.098E+01	6.180E+01	6.898E+01	6.999E+02	8.588E+01	1.755E+02
7	2.172E-01	2.184E+02	-3.975E+02	-2.230E+01	-2.605E+02	-1.280E+03	7.951E+02	1.279E+03	-3.511E+01	-8.275E+02	1.989E+01
8	-2.395E+02	-8.158E+02	-2.098E+02	-7.803E+01	1.338E+02	-1.259E+02	4.106E+01	-5.946E+01	5.671E+00	1.956E+01	1.066E+02
9	1.522E-02	4.435E+01	-1.315E+01	4.053E-02	1.513E+01	2.466E+02	-3.407E+02	-1.162E+03	2.022E+02	-3.886E+01	-1.865E+02
10	6.836E-03	5.252E+00	4.799E+00	-3.244E+01	-1.680E+02	3.307E+02	8.753E+02	-2.498E+02	-2.516E+02	1.154E+01	1.121E+02
11	2.239E-01	2.328E+02	-5.911E+02	-8.560E+01	3.578E+02	1.505E+02	2.979E+01	4.749E+01	-1.215E-01	1.056E+02	-6.384E+01
12	3.394E-02	2.868E+01	1.277E+02	2.177E+02	3.190E+02	-1.440E+02	4.244E+01	-7.638E+01	-1.723E+02	-4.157E+00	4.556E+01
13	-9.067E-03	-1.155E+01	7.214E+01	1.838E+01	-1.447E+02	-2.172E+02	4.340E+01	-5.715E+01	-1.033E+00	2.989E+02	-7.776E+01
14	1.062E-02	8.904E+00	3.734E+01	5.927E+01	7.631E+01	-2.287E+01	-6.733E+00	3.433E+01	2.704E+02	2.704E+02	6.185E+01
15	3.524E-02	3.529E+01	-6.156E+01	-3.381E+00	-3.733E+01	-1.579E+02	7.037E+01	2.231E+01	2.459E+01	-1.315E+02	-2.457E+01
16	-5.127E+01	-1.747E+02	-5.778E+01	-1.671E+01	2.865E+01	-2.695E+01	8.791E+00	-1.273E+01	1.214E+00	4.187E+00	2.287E+01
17	1.389E-02	1.381E+01	-2.283E+01	-1.173E+00	-1.139E+01	-2.876E+01	-1.173E+01	-1.158E+02	3.006E+01	-4.989E+01	-2.838E+01
18	3.586E-03	2.954E+00	1.051E+01	1.232E+01	2.091E+00	2.994E+01	9.364E+01	-1.806E+01	4.490E+01	9.747E+00	2.876E+01
19	2.306E-02	2.377E+01	-5.622E+01	-7.375E+00	2.428E+00	-4.883E+00	7.375E+00	-4.204E-01	-1.127E-01	4.015E+01	-1.433E+01
20	7.745E-03	6.545E+00	2.914E+01	4.969E+01	7.281E+01	-3.287E+01	9.686E+00	-1.743E+01	-3.933E+01	-9.486E-01	1.040E+01
21	8.429E-03	8.524E+00	-1.681E+01	-1.540E+00	-1.212E+00	-1.814E+01	6.152E+00	-4.432E+00	-1.216E-01	3.817E+01	-1.147E+01
22	2.476E-03	2.071E+00	8.486E+00	1.301E+01	1.528E+01	-1.334E+00	8.615E+00	4.857E+00	5.814E+01	7.298E+00	1.526E+01
23	6.558E-03	6.551E+00	-1.121E+01	-6.011E-01	-6.363E+00	-2.351E+01	6.162E+00	-1.773E+01	8.155E+00	-2.413E+01	-7.859E+00
24	-1.009E+01	-3.436E+01	-1.136E+01	-3.286E+00	5.636E+00	-5.302E+00	1.729E+00	-2.504E+00	2.388E-01	8.236E-01	4.498E+00

SINE HARMONIC	JOINT OR MODE										
	1	2	3	4	5	6	7	8	9	10	11
1	-2.549E-01	-2.523E+02	4.005E+02	1.945E+01	1.657E+02	9.214E+01	7.292E+02	3.748E+03	-8.172E+02	8.911E+02	7.646E+02
2	-2.532E-01	-2.092E+02	-7.669E+02	-9.605E+02	-4.271E+02	-1.670E+03	-5.480E+03	9.250E+02	-3.718E+03	-6.996E+02	-1.938E+03
3	-1.106E+00	-1.129E+03	2.439E+03	2.738E+02	-4.667E+02	1.366E+03	-5.931E+02	3.163E+02	1.098E+01	-3.553E+03	1.119E+03
4	1.915E-01	1.618E+02	7.203E+02	1.228E+03	1.800E+03	-8.124E+02	2.394E+02	-4.309E+02	-9.721E+02	-2.345E+01	2.570E+02
5	-8.666E-01	-8.880E+02	1.991E+03	2.394E+02	-5.828E+02	7.182E+02	-3.902E+02	1.557E+02	6.866E+00	-2.277E+03	7.422E+02
6	-1.124E-02	-9.039E+00	-2.412E+01	-6.240E+00	9.297E+01	-2.522E+02	-6.967E+02	1.812E+02	5.439E+01	-2.647E+01	-1.233E+02
7	-2.696E-01	-2.687E+02	4.508E+02	2.361E+01	2.386E+02	7.352E+02	1.936E+01	1.590E+03	-4.760E+02	9.788E+02	4.523E+02
8	4.973E+02	1.694E+03	5.602E+02	1.621E+02	-2.779E+02	2.614E+02	-8.527E+01	1.235E+02	-1.178E+01	-4.061E+01	-2.218E+02
9	-1.985E-01	-1.986E+02	3.435E+02	1.867E+01	2.026E+02	8.121E+02	-3.051E+02	1.624E+02	-1.856E+02	7.361E+02	1.817E+02
10	-4.004E-02	-3.341E+01	-1.345E+02	-2.005E+02	-2.172E+02	-2.593E+01	-2.602E+02	-4.113E+01	-8.813E+02	-1.168E+02	-2.566E+02
11	-5.173E-02	-4.973E+01	4.464E+01	-8.674E+00	1.656E+02	3.678E+02	-9.195E+01	9.429E+01	2.008E+00	-6.027E+02	1.680E+02
12	-4.443E-02	-3.754E+01	-1.671E+02	-2.850E+02	-4.176E+02	1.885E+02	-5.556E+01	9.998E+01	2.256E+02	5.441E+00	-5.964E+01
13	-1.257E-01	-1.301E+02	3.171E+02	4.348E+01	-1.608E+02	-1.945E+01	-3.048E+01	-9.761E+00	3.882E-01	-1.528E+02	6.063E+01
14	-5.570E-03	-4.522E+00	-1.361E+01	-9.175E+00	2.737E+01	-9.524E+01	-2.695E+02	6.640E+01	-9.712E+00	-1.389E+01	-5.488E+01
15	-1.159E-02	-1.143E+01	1.766E+01	8.236E-01	6.276E+00	-8.478E+00	4.808E+01	2.175E+02	-4.485E+01	3.978E+01	4.183E+01
16	3.807E+01	1.297E+02	4.288E+01	1.240E+01	-2.127E+01	2.001E+01	-6.526E+00	9.450E+00	-9.013E-01	-3.108E+00	-1.698E+01
17	-1.707E-02	-1.713E+01	3.037E+01	1.699E+00	1.935E+01	8.929E+01	-4.917E+01	-5.844E+01	-4.120E+00	6.441E+00	4.753E+00
18	-2.876E-03	-2.434E+00	-1.103E+01	-1.941E+01	-3.100E+01	2.264E+01	4.371E+01	-2.224E+01	-9.350E+01	-9.018E+00	-1.331E+01
19	6.613E-03	7.246E+00	-2.585E+01	-5.126E+00	3.324E+01	4.120E+01	-6.887E+00	1.102E+01	1.771E-01	-4.968E+01	1.210E+01
20	-1.906E-03	-1.611E+00	-7.171E+00	-1.223E+01	-1.792E+01	8.088E+00	-2.384E+00	4.289E+00	9.677E+00	2.334E-01	-2.559E+00
21	-1.200E-02	-1.257E+01	3.388E+01	5.270E+00	-2.513E+01	-1.772E+01	4.437E-01	-5.081E+00	-4.096E-02	8.211E+00	-2.539E-01
22	-7.940E-04	-6.338E-01	-1.516E+00	2.503E-01	8.694E+00	-2.120E+01	-5.783E+01	1.547E+01	8.012E+00	-1.783E+00	-9.417E+00
23	1.645E-03	1.674E+00	-3.272E+00	-2.022E-01	-2.667E+00	-1.668E+01	1.426E+01	3.568E+01	-4.518E+00	-6.667E+00	4.054E+00
24	7.470E+00	2.545E+01	8.414E+00	2.434E+00	-4.174E+00	3.926E+00	-1.281E+00	1.854E+00	-1.769E-01	-6.100E-01	-3.331E+00

DISPLACEMENT HARMONICS

COSINE HARMONIC	JOINT OR MODE										
	1	2	3	4	5	6	7	8	9	10	11
0	3.364E-02	3.364E-02	3.357E-02	3.344E-02	3.325E-02	3.299E-02	3.267E-02	3.228E-02	3.183E-02	3.126E-02	3.111E-02
1	-8.761E-04	-8.761E-04	-7.555E-04	-5.167E-04	-4.463E-04	-3.742E-04	-3.036E-04	-6.434E-05	5.686E-05	5.782E-05	5.802E-05
2	5.617E-06	5.660E-06	-5.498E-05	-5.488E-05	-3.500E-04	-3.496E-04	-5.371E-05	-5.305E-05	8.297E-06	8.950E-06	9.122E-06
3	1.620E-03	1.619E-03	1.617E-03	1.409E-03	1.058E-03	5.583E-04	2.020E-04	-1.623E-05	-3.363E-05	-5.751E-05	-6.292E-05
4	-4.672E-07	-5.318E-07	1.199E-05	3.714E-05	4.959E-05	4.942E-05	3.664E-05	1.118E-05	-1.591E-06	-1.727E-06	-1.785E-06
5	-1.030E-03	-1.029E-03	-1.046E-03	-9.176E-04	-7.032E-04	-3.690E-04	-1.473E-04	-4.716E-06	5.270E-08	3.269E-05	4.034E-05
6	1.347E-05	1.344E-05	3.800E-05	3.737E-05	5.664E-05	5.493E-05	3.227E-05	2.957E-05	1.761E-06	-1.659E-06	-2.457E-06
7	6.046E-04	6.025E-04	5.631E-04	4.287E-04	3.673E-04	3.410E-04	2.680E-04	1.105E-04	3.704E-05	-1.413E-05	-2.623E-05
8	-2.938E-03	-2.925E-03	-2.822E-03	-2.630E-03	-2.353E-03	-1.997E-03	-1.570E-03	-1.080E-03	-5.394E-04	9.973E-05	2.535E-04
9	3.099E-04	3.079E-04	2.741E-04	2.785E-04	2.576E-04	1.802E-04	1.462E-04	1.248E-04	5.315E-05	-2.462E-06	-1.603E-05
10	6.814E-04	6.769E-04	6.717E-04	6.253E-04	5.221E-04	4.389E-04	3.785E-04	2.690E-04	1.311E-04	-3.635E-06	-3.680E-05
11	-1.221E-03	-1.211E-03	-1.174E-03	-1.116E-03	-1.045E-03	-9.399E-04	-7.919E-04	-5.826E-04	-3.250E-04	-7.340E-06	7.226E-05
12	-1.081E-04	-1.070E-04	-8.685E-05	-4.854E-05	-2.179E-05	-7.971E-06	-7.765E-06	-2.112E-05	-1.953E-05	-1.305E-06	3.394E-06
13	4.317E-05	4.275E-05	2.963E-05	2.851E-05	2.797E-05	4.343E-05	4.008E-05	3.341E-05	1.218E-05	3.144E-07	-2.597E-06
14	-2.445E-05	-2.413E-05	-1.372E-05	-1.109E-05	1.063E-06	4.343E-06	-1.455E-06	1.656E-06	-3.981E-06	-4.191E-07	5.344E-07
15	-1.846E-05	-1.819E-05	-2.417E-05	-3.449E-05	-3.275E-05	-2.967E-05	-2.344E-05	-2.513E-05	-1.895E-05	-2.307E-06	2.233E-06
16	1.492E-04	1.466E-04	1.382E-04	1.240E-04	1.054E-04	8.384E-05	6.111E-05	3.913E-05	1.971E-05	2.819E-06	-1.922E-06
17	-1.440E-06	-1.418E-06	-6.292E-06	-7.793E-06	-6.977E-06	-1.098E-05	-8.440E-06	-6.658E-06	-7.009E-06	-1.095E-06	6.355E-07
18	-6.662E-06	-6.513E-06	-1.246E-06	-2.790E-07	-8.825E-07	1.803E-07	2.797E-06	3.516E-06	-5.698E-07	-9.610E-08	4.824E-08
19	1.444E-06	1.413E-06	-1.665E-06	-5.975E-06	-1.267E-05	-1.690E-05	-2.031E-05	-1.840E-05	-1.303E-05	-2.243E-06	1.040E-06
20	-1.614E-05	-1.571E-05	-1.021E-05	-2.584E-07	6.569E-06	9.400E-06	7.876E-06	2.195E-06	-6.041E-07	-1.153E-07	4.360E-08
21	3.430E-06	3.322E-06	7.786E-07	-1.517E-06	-4.718E-06	-5.579E-06	-7.251E-06	-6.715E-06	-5.546E-06	-1.151E-06	3.581E-07
22	-5.444E-06	-5.270E-06	-2.146E-06	-8.797E-07	2.074E-06	3.166E-06	2.232E-06	2.508E-06	2.136E-07	4.366E-08	-1.331E-08
23	3.187E-06	3.081E-06	7.516E-07	-1.891E-06	-2.848E-06	-4.439E-06	-4.207E-06	-4.665E-06	-4.168E-06	-9.174E-07	2.527E-07
24	1.512E-05	1.454E-05	1.251E-05	9.300E-06	5.506E-06	1.832E-06	-1.038E-06	-2.570E-06	-2.481E-06	-5.934E-07	1.457E-07

SINE HARMONIC	JOINT OR MODE										
	1	2	3	4	5	6	7	8	9	10	11
1	-3.815E-04	-3.815E-04	-2.631E-04	-2.648E-04	-2.647E-04	-9.597E-05	-9.572E-05	-9.700E-05	2.207E-05	2.311E-05	2.332E-05
2	5.177E-06	5.158E-06	-2.900E-04	-2.898E-04	-2.284E-04	-2.273E-04	-2.865E-04	-2.845E-04	1.292E-05	1.541E-05	1.597E-05
3	-1.771E-03	-1.770E-03	-1.564E-03	-1.351E-03	-9.889E-04	-7.634E-04	-3.972E-04	-1.747E-04	4.392E-05	6.384E-05	6.844E-05
4	2.194E-05	2.193E-05	9.975E-05	2.550E-04	3.310E-04	3.274E-04	2.442E-04	8.176E-05	-3.155E-06	-1.082E-05	-1.258E-05
5	-1.680E-03	-1.677E-03	-1.523E-03	-1.331E-03	-1.013E-03	-7.659E-04	-4.330E-04	-2.120E-04	-1.419E-05	5.152E-05	6.677E-05
6	-3.165E-06	-3.147E-06	-2.343E-05	-2.311E-05	2.150E-06	2.582E-06	-2.182E-05	-2.129E-05	-2.046E-07	6.165E-07	8.151E-07
7	-6.635E-04	-6.616E-04	-5.647E-04	-4.874E-04	-4.442E-04	-3.142E-04	-2.600E-04	-1.608E-04	-3.168E-05	1.668E-05	2.813E-05
8	4.693E-03	4.674E-03	4.513E-03	4.209E-03	3.769E-03	3.200E-03	2.514E-03	1.724E-03	8.447E-04	-2.027E-04	-4.531E-04
9	-1.119E-03	-1.114E-03	-1.034E-03	-9.066E-04	-8.051E-04	-6.666E-04	-5.283E-04	-3.277E-04	-1.417E-04	1.589E-05	5.407E-05
10	-1.694E-04	-1.686E-04	-2.004E-04	-1.902E-04	-1.950E-04	-1.746E-04	-1.294E-04	-1.007E-04	-3.254E-05	2.966E-06	1.158E-05
11	6.952E-04	6.902E-04	6.876E-04	6.433E-04	5.822E-04	4.701E-04	3.728E-04	2.571E-04	1.505E-04	-9.522E-07	-3.841E-05
12	1.714E-04	1.699E-04	1.433E-04	9.245E-05	5.548E-05	3.395E-05	2.879E-05	4.030E-05	3.203E-05	1.533E-06	-6.189E-06
13	1.830E-04	1.810E-04	1.829E-04	1.859E-04	1.960E-04	1.939E-04	1.832E-04	1.456E-04	8.933E-05	7.248E-06	-1.408E-05
14	1.270E-05	1.256E-05	2.928E-06	2.009E-06	9.595E-06	7.946E-06	-2.847E-06	-4.870E-06	2.247E-06	2.038E-07	-3.249E-07
15	8.770E-06	8.638E-06	1.401E-05	1.093E-05	8.191E-05	1.459E-05	1.044E-05	4.636E-06	6.100E-06	6.178E-07	-8.189E-07
16	-1.212E-04	-1.193E-04	-1.128E-04	-1.019E-04	-8.733E-05	-7.028E-05	-5.201E-05	-3.391E-05	-1.735E-05	-2.175E-06	2.031E-06
17	3.559E-06	3.485E-06	5.887E-06	1.277E-05	1.301E-05	1.053E-05	8.711E-06	1.165E-05	8.567E-06	1.240E-06	-8.360E-06
18	5.623E-06	5.516E-06	3.302E-06	2.361E-06	-3.277E-06	-4.129E-06	-1.147E-07	-5.632E-07	6.271E-07	9.779E-08	-5.373E-08
19	1.912E-06	1.856E-06	3.004E-06	8.670E-07	-2.395E-06	-8.417E-06	-1.030E-05	-9.852E-06	-5.249E-06	-9.903E-07	3.781E-07
20	3.294E-06	3.236E-06	2.157E-06	1.300E-07	-1.176E-06	-1.658E-06	-1.275E-06	-4.909E-08	4.224E-07	7.349E-08	-2.909E-08
21	-3.672E-06	-3.576E-06	-2.647E-06	5.806E-07	5.392E-06	1.059E-05	1.325E-05	1.248E-05	8.082E-06	1.566E-06	-5.578E-07
22	9.497E-07	9.497E-07	-7.015E-07	-6.959E-07	1.591E-06	1.439E-06	-1.137E-06	-1.390E-06	1.110E-07	2.374E-08	-5.605E-09
23	1.510E-06	1.448E-06	1.322E-06	-7.865E-07	-1.659E-06	-8.532E-07	-1.252E-06	-2.502E-06	-1.547E-06	-3.773E-07	8.680E-08
24	-1.035E-05	-9.982E-06	-8.807E-06	-6.947E-06	-4.710E-06	-2.465E-06	-5.872E-07	6.078E-07	9.138E-07	1.952E-07	-4.904E-08

ORDER VIBRATION AMPLITUDE

(DEGREES)

0.5	0.055
1.0	0.000
1.5	0.138
2.0	0.001
2.5	0.113
3.0	0.001
3.5	0.051
4.0	0.047
4.5	0.040
5.0	0.081
6.0	0.012
6.5	0.011
7.0	0.000
7.5	0.001
8.0	0.011
8.5	0.000
9.0	0.000
9.5	0.000
10.0	0.000
10.5	0.000
11.0	0.000
11.5	0.000
12.0	0.001

TIME SECONDS	-----JOINT OR MEMBER-----										
	1	2	3	4	5	6	7	8	9	10	11
0.00000	0.000E+00	-0.113E+03	0.440E+02	0.464E+05	-0.179E+05	-0.230E+05	0.152E+05	-0.932E+02	0.567E+03	0.000E+00	0.000E+00
0.00222	0.000E+00	-0.600E+04	-0.312E+04	0.460E+05	-0.134E+05	-0.203E+05	0.191E+05	-0.404E+04	0.241E+05	0.000E+00	0.000E+00
0.00444	0.000E+00	-0.116E+05	-0.637E+04	0.453E+05	-0.627E+04	-0.174E+05	0.219E+05	-0.762E+04	0.480E+05	0.000E+00	0.000E+00
0.00667	0.000E+00	-0.165E+05	-0.965E+04	0.439E+05	-0.261E+04	-0.146E+05	0.236E+05	-0.109E+05	0.660E+05	0.000E+00	0.000E+00
0.00889	0.000E+00	-0.203E+05	-0.128E+05	0.417E+05	0.342E+04	-0.117E+05	0.242E+05	-0.140E+05	0.751E+05	0.000E+00	0.000E+00
0.01111	0.000E+00	-0.225E+05	-0.157E+05	0.389E+05	0.935E+04	-0.916E+04	0.241E+05	-0.170E+05	0.762E+05	0.000E+00	0.000E+00
0.01333	0.000E+00	-0.230E+05	-0.186E+05	0.358E+05	0.145E+05	-0.798E+04	0.235E+05	-0.196E+05	0.724E+05	0.000E+00	0.000E+00
0.01556	0.000E+00	-0.219E+05	-0.213E+05	0.326E+05	0.183E+05	-0.895E+04	0.223E+05	-0.219E+05	0.665E+05	0.000E+00	0.000E+00
0.01778	0.000E+00	-0.196E+05	-0.237E+05	0.290E+05	0.207E+05	-0.120E+05	0.204E+05	-0.237E+05	0.606E+05	0.000E+00	0.000E+00
0.02000	0.000E+00	-0.160E+05	-0.256E+05	0.250E+05	0.218E+05	-0.142E+05	0.180E+05	-0.252E+05	0.553E+05	0.000E+00	0.000E+00
0.02222	0.000E+00	-0.113E+05	-0.267E+05	0.208E+05	0.216E+05	-0.207E+05	0.154E+05	-0.263E+05	0.512E+05	0.000E+00	0.000E+00
0.02444	0.000E+00	-0.584E+04	-0.273E+05	0.166E+05	0.199E+05	-0.249E+05	0.125E+05	-0.268E+05	0.487E+05	0.000E+00	0.000E+00
0.02667	0.000E+00	-0.158E+05	-0.273E+05	0.124E+05	0.165E+05	-0.274E+05	0.953E+04	-0.263E+05	0.475E+05	0.000E+00	0.000E+00
0.02889	0.000E+00	0.536E+04	-0.268E+05	0.830E+04	0.116E+05	-0.258E+05	0.638E+04	-0.246E+05	0.470E+05	0.000E+00	0.000E+00
0.03111	0.000E+00	0.105E+05	-0.253E+05	0.409E+04	0.589E+04	-0.169E+05	0.320E+04	-0.218E+05	0.467E+05	0.000E+00	0.000E+00
0.03333	0.000E+00	0.152E+05	-0.230E+05	-0.932E+02	-0.113E+03	0.567E+03	0.440E+02	-0.179E+05	0.464E+05	0.000E+00	0.000E+00
0.03556	0.000E+00	0.191E+05	-0.203E+05	-0.404E+04	-0.600E+04	0.241E+05	-0.312E+04	-0.134E+05	0.460E+05	0.000E+00	0.000E+00
0.03778	0.000E+00	0.219E+05	-0.174E+05	-0.762E+04	-0.116E+05	0.480E+05	-0.637E+04	-0.827E+04	0.453E+05	0.000E+00	0.000E+00
0.04000	0.000E+00	0.236E+05	-0.146E+05	-0.109E+05	-0.165E+05	0.660E+05	-0.965E+04	-0.261E+04	0.439E+05	0.000E+00	0.000E+00
0.04222	0.000E+00	0.242E+05	-0.117E+05	-0.140E+05	-0.203E+05	0.751E+05	-0.128E+05	0.342E+04	0.417E+05	0.000E+00	0.000E+00
0.04444	0.000E+00	0.241E+05	-0.916E+04	-0.170E+05	-0.225E+05	0.762E+05	-0.157E+05	0.935E+04	0.389E+05	0.000E+00	0.000E+00
0.04667	0.000E+00	0.235E+05	-0.798E+04	-0.196E+05	-0.230E+05	0.724E+05	-0.186E+05	0.145E+05	0.358E+05	0.000E+00	0.000E+00
0.04889	0.000E+00	0.223E+05	-0.895E+04	-0.219E+05	-0.219E+05	0.665E+05	-0.213E+05	0.183E+05	0.326E+05	0.000E+00	0.000E+00
0.05111	0.000E+00	0.204E+05	-0.120E+05	-0.237E+05	-0.196E+05	0.606E+05	-0.237E+05	0.207E+05	0.290E+05	0.000E+00	0.000E+00
0.05333	0.000E+00	0.180E+05	-0.162E+05	-0.252E+05	-0.160E+05	0.553E+05	-0.256E+05	0.218E+05	0.250E+05	0.000E+00	0.000E+00
0.05556	0.000E+00	0.154E+05	-0.207E+05	-0.263E+05	-0.113E+05	0.512E+05	-0.267E+05	0.216E+05	0.208E+05	0.000E+00	0.000E+00
0.05778	0.000E+00	0.125E+05	-0.249E+05	-0.268E+05	-0.584E+04	0.487E+05	-0.273E+05	0.199E+05	0.166E+05	0.000E+00	0.000E+00
0.06000	0.000E+00	0.953E+04	-0.274E+05	-0.263E+05	-0.158E+03	0.475E+05	-0.273E+05	0.165E+05	0.124E+05	0.000E+00	0.000E+00
0.06222	0.000E+00	0.638E+04	-0.258E+05	-0.246E+05	0.536E+04	0.470E+05	-0.268E+05	0.116E+05	0.830E+04	0.000E+00	0.000E+00
0.06444	0.000E+00	0.320E+04	-0.169E+05	-0.218E+05	0.105E+05	0.467E+05	-0.253E+05	0.589E+04	0.409E+04	0.000E+00	0.000E+00
0.06667	0.000E+00	0.440E+02	0.567E+03	-0.179E+05	0.152E+05	0.464E+05	-0.230E+05	-0.113E+03	-0.932E+02	0.000E+00	0.000E+00
0.06889	0.000E+00	-0.312E+04	0.241E+05	-0.134E+05	0.191E+05	0.460E+05	-0.203E+05	-0.600E+04	-0.404E+04	0.000E+00	0.000E+00
0.07111	0.000E+00	-0.637E+04	0.480E+05	-0.827E+04	0.219E+05	0.453E+05	-0.174E+05	-0.116E+05	-0.762E+04	0.000E+00	0.000E+00
0.07333	0.000E+00	-0.965E+04	0.660E+05	-0.261E+04	0.236E+05	0.439E+05	-0.146E+05	-0.165E+05	-0.109E+05	0.000E+00	0.000E+00
0.07556	0.000E+00	-0.128E+05	0.751E+05	0.342E+04	0.242E+05	0.417E+05	-0.117E+05	-0.203E+05	-0.140E+05	0.000E+00	0.000E+00
0.07778	0.000E+00	-0.157E+05	0.762E+05	0.935E+04	0.241E+05	0.389E+05	-0.916E+04	-0.225E+05	-0.170E+05	0.000E+00	0.000E+00
0.08000	0.000E+00	-0.186E+05	0.724E+05	0.145E+05	0.235E+05	0.358E+05	-0.798E+04	-0.230E+05	-0.196E+05	0.000E+00	0.000E+00
0.08222	0.000E+00	-0.213E+05	0.665E+05	0.183E+05	0.223E+05	0.326E+05	-0.895E+04	-0.219E+05	-0.219E+05	0.000E+00	0.000E+00
0.08444	0.000E+00	-0.237E+05	0.606E+05	0.207E+05	0.204E+05	0.290E+05	-0.120E+05	-0.196E+05	-0.237E+05	0.000E+00	0.000E+00
0.08667	0.000E+00	-0.256E+05	0.553E+05	0.218E+05	0.180E+05	0.250E+05	-0.162E+05	-0.160E+05	-0.252E+05	0.000E+00	0.000E+00
0.08889	0.000E+00	-0.267E+05	0.512E+05	0.216E+05	0.154E+05	0.208E+05	-0.207E+05	-0.113E+05	-0.263E+05	0.000E+00	0.000E+00
0.09111	0.000E+00	-0.273E+05	0.487E+05	0.199E+05	0.125E+05	0.166E+05	-0.249E+05	-0.584E+04	-0.268E+05	0.000E+00	0.000E+00
0.09333	0.000E+00	-0.273E+05	0.475E+05	0.165E+05	0.953E+04	0.124E+05	-0.274E+05	-0.158E+03	-0.263E+05	0.000E+00	0.000E+00
0.09556	0.000E+00	-0.268E+05	0.470E+05	0.116E+05	0.638E+04	0.830E+04	-0.258E+05	0.536E+04	-0.246E+05	0.000E+00	0.000E+00
0.09778	0.000E+00	-0.253E+05	0.467E+05	0.589E+04	0.320E+04	0.409E+04	-0.169E+05	0.105E+05	-0.218E+05	0.000E+00	0.000E+00
0.10000	0.000E+00	-0.230E+05	0.464E+05	-0.113E+03	0.440E+02	-0.932E+02	0.567E+03	0.152E+05	-0.179E+05	0.000E+00	0.000E+00
0.10222	0.000E+00	-0.203E+05	0.460E+05	-0.600E+04	-0.312E+04	-0.404E+04	0.241E+05	0.191E+05	-0.134E+05	0.000E+00	0.000E+00
0.10444	0.000E+00	-0.174E+05	0.453E+05	-0.116E+05	-0.637E+04	-0.762E+04	0.480E+05	0.219E+05	-0.827E+04	0.000E+00	0.000E+00
0.10667	0.000E+00	-0.146E+05	0.439E+05	-0.165E+05	-0.965E+04	-0.109E+05	0.660E+05	0.236E+05	-0.261E+04	0.000E+00	0.000E+00
0.10889	0.000E+00	-0.117E+05	0.417E+05	-0.203E+05	-0.128E+05	-0.140E+05	0.751E+05	0.242E+05	0.342E+04	0.000E+00	0.000E+00
0.11111	0.000E+00	-0.916E+04	0.389E+05	-0.225E+05	-0.157E+05	-0.170E+05	0.762E+05	0.241E+05	0.935E+04	0.000E+00	0.000E+00
0.11333	0.000E+00	-0.798E+04	0.358E+05	-0.230E+05	-0.196E+05	-0.196E+05	0.724E+05	0.235E+05	0.145E+05	0.000E+00	0.000E+00
0.11556	0.000E+00	-0.895E+04	0.326E+05	-0.219E+05	-0.213E+05	-0.219E+05	0.665E+05	0.223E+05	0.183E+05	0.000E+00	0.000E+00
0.11778	0.000E+00	-0.120E+05	0.290E+05	-0.196E+05	-0.237E+05	-0.237E+05	0.606E+05	0.204E+05	0.207E+05	0.000E+00	0.000E+00
0.12000	0.000E+00	-0.162E+05	0.250E+05	-0.160E+05	-0.256E+05	-0.252E+05	0.553E+05	0.180E+05	0.218E+05	0.000E+00	0.000E+00
0.12222	0.000E+00	-0.207E+05	0.208E+05	-0.113E+05	-0.267E+05	-0.263E+05	0.512E+05	0.154E+05	0.216E+05	0.000E+00	0.000E+00
0.12444	0.000E+00	-0.249E+05	0.165E+05	-0.584E+04	-0.273E+05	-0.268E+05	0.487E+05	0.125E+05	0.199E+05	0.000E+00	0.000E+00

0.13333	0.000E+00	-0.169E+05	0.409E+04	0.109E+05	-0.253E+05	-0.218E+05	0.467E+05	0.320E+04	0.589E+04	0.000E+00	0.000E+00
0.13333	0.000E+00	0.567E+03	-0.932E+02	0.152E+05	-0.230E+05	-0.179E+05	0.464E+05	0.440E+02	-0.113E+03	0.000E+00	0.000E+00
0.13556	0.000E+00	0.241E+05	-0.404E+04	0.191E+05	-0.203E+05	-0.134E+05	0.460E+05	-0.312E+04	-0.600E+04	0.000E+00	0.000E+00
0.13778	0.000E+00	0.480E+05	-0.762E+04	0.219E+05	-0.174E+05	-0.827E+04	0.453E+05	-0.637E+04	-0.116E+05	0.000E+00	0.000E+00
0.14000	0.000E+00	0.660E+05	-0.109E+05	0.236E+05	-0.146E+05	-0.261E+04	0.439E+05	-0.965E+04	-0.165E+05	0.000E+00	0.000E+00
0.14222	0.000E+00	0.751E+05	-0.140E+05	0.242E+05	-0.117E+05	0.342E+04	0.417E+05	-0.128E+05	-0.203E+05	0.000E+00	0.000E+00
0.14444	0.000E+00	0.762E+05	-0.170E+05	0.241E+05	-0.916E+04	0.935E+04	0.389E+05	-0.157E+05	-0.225E+05	0.000E+00	0.000E+00
0.14667	0.000E+00	0.724E+05	-0.196E+05	0.235E+05	-0.798E+04	0.145E+05	0.358E+05	-0.186E+05	-0.230E+05	0.000E+00	0.000E+00
0.14889	0.000E+00	0.665E+05	-0.219E+05	0.223E+05	-0.895E+04	0.183E+05	0.326E+05	-0.213E+05	-0.219E+05	0.000E+00	0.000E+00
0.15111	0.000E+00	0.606E+05	-0.237E+05	0.204E+05	-0.120E+05	0.207E+05	0.290E+05	-0.237E+05	-0.196E+05	0.000E+00	0.000E+00
0.15333	0.000E+00	0.553E+05	-0.252E+05	0.180E+05	-0.162E+05	0.218E+05	0.250E+05	-0.256E+05	-0.160E+05	0.000E+00	0.000E+00
0.15556	0.000E+00	0.512E+05	-0.263E+05	0.154E+05	-0.207E+05	0.216E+05	0.208E+05	-0.267E+05	-0.113E+05	0.000E+00	0.000E+00
0.15778	0.000E+00	0.487E+05	-0.268E+05	0.125E+05	-0.249E+05	0.199E+05	0.166E+05	-0.273E+05	-0.584E+04	0.000E+00	0.000E+00
0.16000	0.000E+00	0.475E+05	-0.263E+05	0.953E+04	-0.274E+05	0.165E+05	0.124E+05	-0.273E+05	-0.158E+03	0.000E+00	0.000E+00
0.16222	0.000E+00	0.470E+05	-0.246E+05	0.638E+04	-0.258E+05	0.116E+05	0.830E+04	-0.268E+05	0.536E+04	0.000E+00	0.000E+00
0.16444	0.000E+00	0.467E+05	-0.218E+05	0.320E+04	-0.169E+05	0.589E+04	0.409E+04	-0.253E+05	0.105E+05	0.000E+00	0.000E+00
0.16667	0.000E+00	0.464E+05	-0.179E+05	0.440E+02	0.567E+03	-0.113E+03	-0.932E+02	-0.230E+05	0.152E+05	0.000E+00	0.000E+00
0.16889	0.000E+00	0.460E+05	-0.134E+05	-0.312E+04	0.241E+05	-0.600E+04	-0.404E+04	-0.203E+05	0.191E+05	0.000E+00	0.000E+00
0.17111	0.000E+00	0.453E+05	-0.827E+04	-0.637E+04	0.480E+05	-0.116E+05	-0.762E+04	-0.174E+05	0.219E+05	0.000E+00	0.000E+00
0.17333	0.000E+00	0.439E+05	-0.261E+04	-0.965E+04	0.660E+05	-0.165E+05	-0.109E+05	-0.146E+05	0.236E+05	0.000E+00	0.000E+00
0.17556	0.000E+00	0.417E+05	-0.342E+04	-0.128E+05	0.751E+05	-0.203E+05	-0.140E+05	-0.117E+05	0.242E+05	0.000E+00	0.000E+00
0.17778	0.000E+00	0.389E+05	0.935E+04	-0.157E+05	0.762E+05	-0.225E+05	-0.170E+05	-0.916E+04	0.241E+05	0.000E+00	0.000E+00
0.18000	0.000E+00	0.358E+05	0.145E+05	-0.186E+05	0.724E+05	-0.230E+05	-0.196E+05	-0.798E+04	0.235E+05	0.000E+00	0.000E+00
0.18222	0.000E+00	0.326E+05	0.183E+05	-0.213E+05	0.665E+05	-0.219E+05	-0.219E+05	-0.895E+04	0.223E+05	0.000E+00	0.000E+00
0.18444	0.000E+00	0.290E+05	0.207E+05	-0.237E+05	0.606E+05	-0.196E+05	-0.237E+05	-0.120E+05	0.204E+05	0.000E+00	0.000E+00
0.18667	0.000E+00	0.250E+05	0.218E+05	-0.256E+05	0.553E+05	-0.160E+05	-0.252E+05	-0.162E+05	0.180E+05	0.000E+00	0.000E+00
0.18889	0.000E+00	0.208E+05	0.216E+05	-0.267E+05	0.512E+05	-0.113E+05	-0.263E+05	-0.207E+05	0.154E+05	0.000E+00	0.000E+00
0.19111	0.000E+00	0.166E+05	0.199E+05	-0.273E+05	0.487E+05	-0.584E+04	-0.268E+05	-0.249E+05	0.125E+05	0.000E+00	0.000E+00
0.19333	0.000E+00	0.124E+05	0.165E+05	-0.273E+05	0.475E+05	-0.158E+03	-0.263E+05	-0.274E+05	0.953E+04	0.000E+00	0.000E+00
0.19556	0.000E+00	0.830E+04	0.116E+05	-0.268E+05	0.470E+05	0.536E+04	-0.246E+05	-0.258E+05	0.638E+04	0.000E+00	0.000E+00
0.19778	0.000E+00	0.409E+04	0.589E+04	-0.253E+05	0.467E+05	0.105E+05	-0.218E+05	-0.169E+05	0.320E+04	0.000E+00	0.000E+00
0.20000	0.000E+00	0.932E+02	-0.113E+03	-0.230E+05	0.464E+05	0.152E+05	-0.179E+05	0.567E+03	0.440E+02	0.000E+00	0.000E+00
0.20222	0.000E+00	-0.404E+04	-0.600E+04	-0.203E+05	0.460E+05	0.191E+05	-0.134E+05	0.241E+05	-0.312E+04	0.000E+00	0.000E+00
0.20444	0.000E+00	-0.762E+04	-0.116E+05	-0.174E+05	0.453E+05	0.219E+05	-0.827E+04	0.480E+05	-0.637E+04	0.000E+00	0.000E+00
0.20667	0.000E+00	-0.109E+05	-0.165E+05	-0.146E+05	0.439E+05	0.236E+05	-0.261E+04	0.660E+05	-0.965E+04	0.000E+00	0.000E+00
0.20889	0.000E+00	-0.140E+05	-0.203E+05	-0.117E+05	0.417E+05	0.242E+05	0.342E+04	0.751E+05	-0.128E+05	0.000E+00	0.000E+00
0.21111	0.000E+00	-0.170E+05	-0.225E+05	-0.916E+04	0.389E+05	0.241E+05	0.935E+04	0.762E+05	-0.157E+05	0.000E+00	0.000E+00
0.21333	0.000E+00	-0.196E+05	-0.230E+05	-0.798E+04	0.358E+05	0.235E+05	0.145E+05	0.724E+05	-0.186E+05	0.000E+00	0.000E+00
0.21556	0.000E+00	-0.219E+05	-0.219E+05	-0.895E+04	0.326E+05	0.223E+05	0.183E+05	0.665E+05	-0.213E+05	0.000E+00	0.000E+00
0.21778	0.000E+00	-0.237E+05	-0.196E+05	-0.120E+05	0.290E+05	0.204E+05	0.207E+05	0.606E+05	-0.237E+05	0.000E+00	0.000E+00
0.22000	0.000E+00	-0.252E+05	-0.160E+05	-0.162E+05	0.250E+05	0.180E+05	0.218E+05	0.553E+05	-0.256E+05	0.000E+00	0.000E+00
0.22222	0.000E+00	-0.263E+05	-0.113E+05	-0.207E+05	0.208E+05	0.154E+05	0.216E+05	0.512E+05	-0.267E+05	0.000E+00	0.000E+00
0.22444	0.000E+00	-0.268E+05	-0.584E+04	-0.249E+05	0.166E+05	0.125E+05	0.199E+05	0.487E+05	-0.273E+05	0.000E+00	0.000E+00
0.22667	0.000E+00	-0.263E+05	-0.158E+03	-0.274E+05	0.124E+05	0.953E+04	0.165E+05	0.475E+05	-0.273E+05	0.000E+00	0.000E+00
0.22889	0.000E+00	-0.246E+05	0.536E+04	-0.258E+05	0.830E+04	0.638E+04	0.116E+05	0.470E+05	-0.268E+05	0.000E+00	0.000E+00
0.23111	0.000E+00	-0.218E+05	0.105E+05	-0.169E+05	0.409E+04	0.320E+04	0.589E+04	0.467E+05	-0.253E+05	0.000E+00	0.000E+00
0.23333	0.000E+00	-0.179E+05	0.152E+05	0.567E+03	-0.932E+02	0.440E+02	-0.113E+03	0.464E+05	-0.230E+05	0.000E+00	0.000E+00
0.23556	0.000E+00	-0.134E+05	0.191E+05	0.241E+05	-0.404E+04	-0.312E+04	-0.600E+04	0.460E+05	-0.203E+05	0.000E+00	0.000E+00
0.23778	0.000E+00	-0.827E+04	0.219E+05	0.480E+05	-0.762E+04	-0.637E+04	-0.116E+05	0.453E+05	-0.174E+05	0.000E+00	0.000E+00
0.24000	0.000E+00	-0.261E+04	0.236E+05	0.660E+05	-0.109E+05	-0.965E+04	-0.165E+05	0.439E+05	-0.146E+05	0.000E+00	0.000E+00
0.24222	0.000E+00	0.342E+04	0.242E+05	0.751E+05	-0.140E+05	-0.128E+05	-0.203E+05	0.417E+05	-0.117E+05	0.000E+00	0.000E+00
0.24444	0.000E+00	0.935E+04	0.241E+05	0.762E+05	-0.170E+05	-0.157E+05	-0.225E+05	0.389E+05	-0.916E+04	0.000E+00	0.000E+00
0.24667	0.000E+00	0.145E+05	0.235E+05	0.724E+05	-0.196E+05	-0.186E+05	-0.230E+05	0.358E+05	-0.798E+04	0.000E+00	0.000E+00
0.24889	0.000E+00	0.193E+05	0.223E+05	0.665E+05	-0.219E+05	-0.213E+05	-0.219E+05	0.326E+05	-0.895E+04	0.000E+00	0.000E+00
0.25111	0.000E+00	0.207E+05	0.204E+05	0.606E+05	-0.237E+05	-0.237E+05	-0.196E+05	0.290E+05	-0.120E+05	0.000E+00	0.000E+00
0.25333	0.000E+00	0.216E+05	0.180E+05	0.553E+05	-0.252E+05	-0.256E+05	-0.160E+05	0.250E+05	-0.162E+05	0.000E+00	0.000E+00
0.25556	0.000E+00	0.216E+05	0.154E+05	0.512E+05	-0.263E+05	-0.267E+05	-0.113E+05	0.208E+05	-0.207E+05	0.000E+00	0.000E+00
0.25778	0.000E+00	0.199E+05	0.125E+05	0.487E+05	-0.268E+05	-0.273E+05	-0.584E+04	0.166E+05	-0.249E+05	0.000E+00	0.000E+00
0.26000	0.000E+00	0.165E+05	0.953E+04	0.475E+05	-0.263E+05	-0.273E+05	-0.158E+03	0.124E+05	-0.274E+05	0.000E+00	0.000E+00
0.26222	0.000E+00	0.116E+05	0.638E+04	0.470E+05	-0.246E+05	-0.268E+05	0.536E+04	0.830E+04	-0.258E+05	0.000E+00	0.000E+00
0.26444	0.000E+00	0.589E+04	0.320E+04	0.467E+05	-0.219E+05	-0.253E+05	0.105E+05	0.409E+04	-0.169E+05	0.000E+00	0.000E+00

DISPLACEMENT TIME HISTORY

TIME SECONDS	JOINT OR MEMBER										
	1	2	3	4	5	6	7	8	9	10	11
0.00000	0.308E-01	0.309E-01	0.309E-01	0.311E-01	0.307E-01	0.307E-01	0.309E-01	0.310E-01	0.312E-01	0.314E-01	0.314E-01
0.00222	0.320E-01	0.320E-01	0.321E-01	0.323E-01	0.319E-01	0.317E-01	0.318E-01	0.317E-01	0.317E-01	0.313E-01	0.312E-01
0.00444	0.334E-01	0.333E-01	0.335E-01	0.336E-01	0.333E-01	0.330E-01	0.329E-01	0.325E-01	0.322E-01	0.313E-01	0.310E-01
0.00667	0.344E-01	0.345E-01	0.347E-01	0.349E-01	0.345E-01	0.341E-01	0.338E-01	0.332E-01	0.327E-01	0.312E-01	0.309E-01
0.00889	0.353E-01	0.352E-01	0.354E-01	0.356E-01	0.352E-01	0.347E-01	0.343E-01	0.335E-01	0.329E-01	0.312E-01	0.308E-01
0.01111	0.352E-01	0.352E-01	0.353E-01	0.356E-01	0.353E-01	0.348E-01	0.343E-01	0.335E-01	0.329E-01	0.312E-01	0.308E-01
0.01333	0.343E-01	0.343E-01	0.345E-01	0.348E-01	0.347E-01	0.343E-01	0.339E-01	0.332E-01	0.327E-01	0.312E-01	0.309E-01
0.01556	0.329E-01	0.329E-01	0.331E-01	0.335E-01	0.335E-01	0.333E-01	0.331E-01	0.326E-01	0.324E-01	0.313E-01	0.310E-01
0.01778	0.311E-01	0.311E-01	0.314E-01	0.319E-01	0.321E-01	0.320E-01	0.321E-01	0.319E-01	0.320E-01	0.313E-01	0.312E-01
0.02000	0.298E-01	0.298E-01	0.297E-01	0.297E-01	0.297E-01	0.298E-01	0.311E-01	0.312E-01	0.316E-01	0.314E-01	0.314E-01
0.02222	0.283E-01	0.283E-01	0.285E-01	0.291E-01	0.295E-01	0.298E-01	0.303E-01	0.307E-01	0.314E-01	0.315E-01	0.315E-01
0.02444	0.277E-01	0.277E-01	0.279E-01	0.285E-01	0.289E-01	0.292E-01	0.298E-01	0.303E-01	0.312E-01	0.313E-01	0.316E-01
0.02667	0.279E-01	0.279E-01	0.280E-01	0.285E-01	0.289E-01	0.291E-01	0.297E-01	0.303E-01	0.312E-01	0.316E-01	0.317E-01
0.02889	0.287E-01	0.287E-01	0.286E-01	0.290E-01	0.293E-01	0.295E-01	0.300E-01	0.305E-01	0.313E-01	0.316E-01	0.316E-01
0.03111	0.298E-01	0.298E-01	0.297E-01	0.299E-01	0.300E-01	0.302E-01	0.305E-01	0.308E-01	0.315E-01	0.315E-01	0.315E-01
0.03333	0.310E-01	0.310E-01	0.308E-01	0.309E-01	0.310E-01	0.311E-01	0.312E-01	0.313E-01	0.317E-01	0.314E-01	0.314E-01
0.03556	0.321E-01	0.321E-01	0.319E-01	0.319E-01	0.319E-01	0.321E-01	0.319E-01	0.318E-01	0.319E-01	0.314E-01	0.312E-01
0.03778	0.332E-01	0.332E-01	0.330E-01	0.329E-01	0.329E-01	0.331E-01	0.327E-01	0.324E-01	0.321E-01	0.313E-01	0.311E-01
0.04000	0.343E-01	0.343E-01	0.340E-01	0.339E-01	0.339E-01	0.340E-01	0.339E-01	0.329E-01	0.323E-01	0.312E-01	0.309E-01
0.04222	0.352E-01	0.352E-01	0.349E-01	0.347E-01	0.346E-01	0.347E-01	0.339E-01	0.332E-01	0.325E-01	0.311E-01	0.308E-01
0.04444	0.359E-01	0.359E-01	0.355E-01	0.352E-01	0.351E-01	0.351E-01	0.342E-01	0.335E-01	0.326E-01	0.311E-01	0.308E-01
0.04667	0.360E-01	0.360E-01	0.356E-01	0.353E-01	0.351E-01	0.351E-01	0.342E-01	0.335E-01	0.326E-01	0.312E-01	0.308E-01
0.04889	0.354E-01	0.354E-01	0.351E-01	0.347E-01	0.346E-01	0.347E-01	0.339E-01	0.333E-01	0.325E-01	0.312E-01	0.309E-01
0.05111	0.342E-01	0.342E-01	0.339E-01	0.336E-01	0.336E-01	0.338E-01	0.333E-01	0.329E-01	0.323E-01	0.313E-01	0.310E-01
0.05333	0.325E-01	0.325E-01	0.322E-01	0.321E-01	0.323E-01	0.327E-01	0.324E-01	0.323E-01	0.320E-01	0.314E-01	0.312E-01
0.05556	0.306E-01	0.306E-01	0.304E-01	0.305E-01	0.309E-01	0.314E-01	0.314E-01	0.317E-01	0.317E-01	0.315E-01	0.314E-01
0.05778	0.288E-01	0.288E-01	0.287E-01	0.289E-01	0.296E-01	0.303E-01	0.305E-01	0.310E-01	0.314E-01	0.315E-01	0.316E-01
0.06000	0.275E-01	0.275E-01	0.275E-01	0.279E-01	0.287E-01	0.295E-01	0.299E-01	0.306E-01	0.311E-01	0.316E-01	0.316E-01
0.06222	0.269E-01	0.270E-01	0.270E-01	0.275E-01	0.283E-01	0.292E-01	0.296E-01	0.303E-01	0.309E-01	0.315E-01	0.317E-01
0.06444	0.274E-01	0.274E-01	0.275E-01	0.279E-01	0.287E-01	0.294E-01	0.297E-01	0.303E-01	0.309E-01	0.315E-01	0.316E-01
0.06667	0.288E-01	0.288E-01	0.290E-01	0.292E-01	0.298E-01	0.303E-01	0.303E-01	0.306E-01	0.310E-01	0.314E-01	0.315E-01
0.06889	0.312E-01	0.312E-01	0.314E-01	0.314E-01	0.316E-01	0.317E-01	0.313E-01	0.312E-01	0.312E-01	0.312E-01	0.313E-01
0.07111	0.345E-01	0.345E-01	0.346E-01	0.342E-01	0.340E-01	0.336E-01	0.327E-01	0.320E-01	0.315E-01	0.311E-01	0.310E-01
0.07333	0.381E-01	0.381E-01	0.382E-01	0.375E-01	0.368E-01	0.359E-01	0.344E-01	0.331E-01	0.320E-01	0.310E-01	0.307E-01
0.07556	0.415E-01	0.415E-01	0.415E-01	0.406E-01	0.395E-01	0.381E-01	0.361E-01	0.342E-01	0.326E-01	0.309E-01	0.305E-01
0.07778	0.440E-01	0.440E-01	0.439E-01	0.429E-01	0.415E-01	0.398E-01	0.374E-01	0.351E-01	0.330E-01	0.309E-01	0.304E-01
0.08000	0.450E-01	0.449E-01	0.449E-01	0.438E-01	0.423E-01	0.404E-01	0.380E-01	0.355E-01	0.332E-01	0.309E-01	0.303E-01
0.08222	0.441E-01	0.440E-01	0.441E-01	0.431E-01	0.417E-01	0.399E-01	0.376E-01	0.352E-01	0.331E-01	0.310E-01	0.304E-01
0.08444	0.415E-01	0.415E-01	0.416E-01	0.408E-01	0.397E-01	0.382E-01	0.362E-01	0.344E-01	0.327E-01	0.311E-01	0.307E-01
0.08667	0.377E-01	0.377E-01	0.379E-01	0.375E-01	0.367E-01	0.356E-01	0.343E-01	0.330E-01	0.320E-01	0.312E-01	0.309E-01
0.08889	0.336E-01	0.336E-01	0.340E-01	0.338E-01	0.334E-01	0.328E-01	0.321E-01	0.316E-01	0.313E-01	0.313E-01	0.312E-01
0.09111	0.299E-01	0.300E-01	0.305E-01	0.305E-01	0.305E-01	0.304E-01	0.302E-01	0.303E-01	0.306E-01	0.313E-01	0.315E-01
0.09333	0.276E-01	0.277E-01	0.282E-01	0.284E-01	0.286E-01	0.288E-01	0.289E-01	0.296E-01	0.302E-01	0.314E-01	0.317E-01
0.09556	0.270E-01	0.271E-01	0.276E-01	0.278E-01	0.280E-01	0.283E-01	0.286E-01	0.294E-01	0.302E-01	0.314E-01	0.317E-01
0.09778	0.281E-01	0.281E-01	0.286E-01	0.287E-01	0.288E-01	0.290E-01	0.293E-01	0.299E-01	0.305E-01	0.314E-01	0.316E-01
0.10000	0.304E-01	0.305E-01	0.308E-01	0.307E-01	0.307E-01	0.307E-01	0.308E-01	0.310E-01	0.310E-01	0.313E-01	0.314E-01
0.10222	0.334E-01	0.334E-01	0.336E-01	0.333E-01	0.331E-01	0.329E-01	0.328E-01	0.324E-01	0.318E-01	0.312E-01	0.311E-01
0.10444	0.363E-01	0.363E-01	0.364E-01	0.359E-01	0.355E-01	0.351E-01	0.347E-01	0.338E-01	0.325E-01	0.312E-01	0.308E-01
0.10667	0.385E-01	0.385E-01	0.385E-01	0.379E-01	0.373E-01	0.367E-01	0.362E-01	0.348E-01	0.330E-01	0.311E-01	0.306E-01
0.10889	0.395E-01	0.395E-01	0.394E-01	0.387E-01	0.381E-01	0.374E-01	0.368E-01	0.353E-01	0.333E-01	0.311E-01	0.305E-01
0.11111	0.391E-01	0.390E-01	0.389E-01	0.382E-01	0.376E-01	0.371E-01	0.366E-01	0.351E-01	0.333E-01	0.311E-01	0.306E-01
0.11333	0.372E-01	0.371E-01	0.371E-01	0.365E-01	0.360E-01	0.357E-01	0.355E-01	0.344E-01	0.329E-01	0.311E-01	0.307E-01
0.11556	0.341E-01	0.341E-01	0.342E-01	0.338E-01	0.336E-01	0.336E-01	0.338E-01	0.333E-01	0.324E-01	0.312E-01	0.309E-01
0.11778	0.307E-01	0.307E-01	0.309E-01	0.307E-01	0.309E-01	0.313E-01	0.320E-01	0.320E-01	0.318E-01	0.313E-01	0.312E-01
0.12000	0.276E-01	0.276E-01	0.279E-01	0.280E-01	0.284E-01	0.292E-01	0.303E-01	0.309E-01	0.313E-01	0.314E-01	0.314E-01
0.12222	0.254E-01	0.254E-01	0.258E-01	0.262E-01	0.267E-01	0.278E-01	0.292E-01	0.301E-01	0.309E-01	0.315E-01	0.316E-01
0.12444	0.245E-01	0.246E-01	0.250E-01	0.255E-01	0.261E-01	0.272E-01	0.287E-01	0.298E-01	0.307E-01	0.315E-01	0.317E-01

0.12689	0.267E-01	0.267E-01	0.271E-01	0.275E-01	0.280E-01	0.287E-01	0.299E-01	0.305E-01	0.308E-01	0.315E-01	0.317E-01	0.316E-01
0.13111	0.292E-01	0.292E-01	0.294E-01	0.297E-01	0.298E-01	0.303E-01	0.310E-01	0.312E-01	0.314E-01	0.315E-01	0.315E-01	0.315E-01
0.13333	0.320E-01	0.320E-01	0.320E-01	0.320E-01	0.320E-01	0.314E-01	0.319E-01	0.322E-01	0.319E-01	0.317E-01	0.314E-01	0.313E-01
0.13556	0.348E-01	0.348E-01	0.345E-01	0.342E-01	0.337E-01	0.334E-01	0.333E-01	0.326E-01	0.319E-01	0.312E-01	0.310E-01	0.310E-01
0.13778	0.374E-01	0.374E-01	0.374E-01	0.368E-01	0.363E-01	0.354E-01	0.348E-01	0.342E-01	0.331E-01	0.321E-01	0.311E-01	0.308E-01
0.14000	0.396E-01	0.396E-01	0.388E-01	0.380E-01	0.369E-01	0.360E-01	0.350E-01	0.336E-01	0.322E-01	0.310E-01	0.307E-01	0.307E-01
0.14222	0.413E-01	0.413E-01	0.403E-01	0.394E-01	0.381E-01	0.370E-01	0.358E-01	0.340E-01	0.324E-01	0.309E-01	0.305E-01	0.305E-01
0.14444	0.421E-01	0.421E-01	0.411E-01	0.402E-01	0.389E-01	0.376E-01	0.362E-01	0.343E-01	0.325E-01	0.309E-01	0.305E-01	0.305E-01
0.14667	0.421E-01	0.421E-01	0.411E-01	0.402E-01	0.390E-01	0.378E-01	0.363E-01	0.344E-01	0.326E-01	0.309E-01	0.305E-01	0.305E-01
0.14889	0.411E-01	0.411E-01	0.402E-01	0.395E-01	0.384E-01	0.373E-01	0.359E-01	0.341E-01	0.325E-01	0.310E-01	0.306E-01	0.306E-01
0.15111	0.393E-01	0.393E-01	0.385E-01	0.379E-01	0.370E-01	0.362E-01	0.350E-01	0.335E-01	0.322E-01	0.311E-01	0.308E-01	0.308E-01
0.15333	0.369E-01	0.369E-01	0.362E-01	0.358E-01	0.351E-01	0.346E-01	0.338E-01	0.327E-01	0.319E-01	0.312E-01	0.310E-01	0.310E-01
0.15556	0.343E-01	0.343E-01	0.337E-01	0.334E-01	0.330E-01	0.329E-01	0.325E-01	0.318E-01	0.315E-01	0.313E-01	0.312E-01	0.312E-01
0.15778	0.319E-01	0.319E-01	0.314E-01	0.313E-01	0.311E-01	0.313E-01	0.312E-01	0.310E-01	0.311E-01	0.314E-01	0.314E-01	0.314E-01
0.16000	0.302E-01	0.302E-01	0.297E-01	0.297E-01	0.297E-01	0.300E-01	0.302E-01	0.304E-01	0.309E-01	0.314E-01	0.315E-01	0.315E-01
0.16222	0.294E-01	0.294E-01	0.290E-01	0.289E-01	0.290E-01	0.294E-01	0.297E-01	0.300E-01	0.307E-01	0.314E-01	0.316E-01	0.316E-01
0.16444	0.296E-01	0.296E-01	0.292E-01	0.291E-01	0.291E-01	0.294E-01	0.297E-01	0.301E-01	0.307E-01	0.314E-01	0.315E-01	0.315E-01
0.16667	0.307E-01	0.307E-01	0.303E-01	0.301E-01	0.301E-01	0.302E-01	0.303E-01	0.305E-01	0.309E-01	0.313E-01	0.314E-01	0.314E-01
0.16889	0.326E-01	0.326E-01	0.322E-01	0.319E-01	0.318E-01	0.315E-01	0.313E-01	0.312E-01	0.313E-01	0.312E-01	0.312E-01	0.312E-01
0.17111	0.351E-01	0.351E-01	0.346E-01	0.343E-01	0.340E-01	0.332E-01	0.326E-01	0.321E-01	0.317E-01	0.311E-01	0.310E-01	0.310E-01
0.17333	0.379E-01	0.379E-01	0.373E-01	0.368E-01	0.364E-01	0.351E-01	0.340E-01	0.330E-01	0.322E-01	0.310E-01	0.307E-01	0.307E-01
0.17556	0.404E-01	0.404E-01	0.398E-01	0.390E-01	0.384E-01	0.367E-01	0.352E-01	0.339E-01	0.327E-01	0.310E-01	0.306E-01	0.306E-01
0.17778	0.420E-01	0.420E-01	0.413E-01	0.404E-01	0.396E-01	0.377E-01	0.360E-01	0.345E-01	0.330E-01	0.310E-01	0.305E-01	0.305E-01
0.18000	0.423E-01	0.423E-01	0.416E-01	0.407E-01	0.398E-01	0.379E-01	0.362E-01	0.346E-01	0.330E-01	0.310E-01	0.305E-01	0.305E-01
0.18222	0.411E-01	0.411E-01	0.405E-01	0.396E-01	0.388E-01	0.371E-01	0.355E-01	0.342E-01	0.328E-01	0.310E-01	0.306E-01	0.306E-01
0.18444	0.387E-01	0.387E-01	0.382E-01	0.375E-01	0.369E-01	0.355E-01	0.343E-01	0.333E-01	0.324E-01	0.311E-01	0.308E-01	0.308E-01
0.18667	0.356E-01	0.356E-01	0.352E-01	0.346E-01	0.343E-01	0.334E-01	0.326E-01	0.321E-01	0.318E-01	0.312E-01	0.311E-01	0.311E-01
0.18889	0.323E-01	0.323E-01	0.322E-01	0.318E-01	0.318E-01	0.313E-01	0.309E-01	0.309E-01	0.312E-01	0.313E-01	0.313E-01	0.313E-01
0.19111	0.297E-01	0.297E-01	0.297E-01	0.295E-01	0.298E-01	0.296E-01	0.296E-01	0.300E-01	0.307E-01	0.314E-01	0.315E-01	0.315E-01
0.19333	0.283E-01	0.283E-01	0.283E-01	0.283E-01	0.288E-01	0.288E-01	0.290E-01	0.295E-01	0.305E-01	0.314E-01	0.316E-01	0.316E-01
0.19556	0.282E-01	0.282E-01	0.283E-01	0.284E-01	0.289E-01	0.290E-01	0.291E-01	0.296E-01	0.305E-01	0.314E-01	0.316E-01	0.316E-01
0.19778	0.294E-01	0.294E-01	0.295E-01	0.296E-01	0.300E-01	0.300E-01	0.300E-01	0.303E-01	0.308E-01	0.314E-01	0.315E-01	0.315E-01
0.20000	0.313E-01	0.314E-01	0.314E-01	0.315E-01	0.318E-01	0.317E-01	0.314E-01	0.314E-01	0.313E-01	0.313E-01	0.313E-01	0.313E-01
0.20222	0.335E-01	0.335E-01	0.335E-01	0.336E-01	0.339E-01	0.336E-01	0.330E-01	0.326E-01	0.320E-01	0.313E-01	0.311E-01	0.311E-01
0.20444	0.354E-01	0.354E-01	0.354E-01	0.354E-01	0.356E-01	0.352E-01	0.345E-01	0.338E-01	0.326E-01	0.312E-01	0.309E-01	0.309E-01
0.20667	0.366E-01	0.366E-01	0.366E-01	0.367E-01	0.368E-01	0.363E-01	0.355E-01	0.346E-01	0.329E-01	0.312E-01	0.307E-01	0.307E-01
0.20889	0.368E-01	0.368E-01	0.368E-01	0.370E-01	0.371E-01	0.367E-01	0.359E-01	0.349E-01	0.331E-01	0.311E-01	0.307E-01	0.307E-01
0.21111	0.360E-01	0.360E-01	0.360E-01	0.363E-01	0.365E-01	0.362E-01	0.356E-01	0.347E-01	0.329E-01	0.311E-01	0.307E-01	0.307E-01
0.21333	0.343E-01	0.343E-01	0.344E-01	0.348E-01	0.352E-01	0.351E-01	0.347E-01	0.341E-01	0.326E-01	0.312E-01	0.308E-01	0.308E-01
0.21556	0.321E-01	0.321E-01	0.323E-01	0.328E-01	0.334E-01	0.336E-01	0.335E-01	0.332E-01	0.321E-01	0.312E-01	0.310E-01	0.310E-01
0.21778	0.298E-01	0.298E-01	0.302E-01	0.308E-01	0.316E-01	0.321E-01	0.322E-01	0.323E-01	0.317E-01	0.313E-01	0.312E-01	0.312E-01
0.22000	0.281E-01	0.281E-01	0.285E-01	0.291E-01	0.301E-01	0.308E-01	0.313E-01	0.316E-01	0.314E-01	0.314E-01	0.314E-01	0.314E-01
0.22222	0.271E-01	0.271E-01	0.275E-01	0.282E-01	0.292E-01	0.295E-01	0.307E-01	0.312E-01	0.312E-01	0.315E-01	0.315E-01	0.315E-01
0.22444	0.269E-01	0.270E-01	0.274E-01	0.280E-01	0.287E-01	0.298E-01	0.305E-01	0.311E-01	0.311E-01	0.315E-01	0.316E-01	0.316E-01
0.22667	0.276E-01	0.276E-01	0.280E-01	0.285E-01	0.293E-01	0.301E-01	0.307E-01	0.313E-01	0.312E-01	0.315E-01	0.316E-01	0.316E-01
0.22889	0.289E-01	0.289E-01	0.292E-01	0.295E-01	0.301E-01	0.307E-01	0.312E-01	0.316E-01	0.314E-01	0.315E-01	0.315E-01	0.315E-01
0.23111	0.304E-01	0.304E-01	0.306E-01	0.308E-01	0.311E-01	0.314E-01	0.317E-01	0.319E-01	0.315E-01	0.315E-01	0.314E-01	0.314E-01
0.23333	0.319E-01	0.319E-01	0.321E-01	0.321E-01	0.321E-01	0.322E-01	0.322E-01	0.322E-01	0.317E-01	0.314E-01	0.313E-01	0.313E-01
0.23556	0.333E-01	0.333E-01	0.335E-01	0.334E-01	0.331E-01	0.329E-01	0.326E-01	0.325E-01	0.318E-01	0.313E-01	0.311E-01	0.311E-01
0.23778	0.348E-01	0.348E-01	0.349E-01	0.348E-01	0.341E-01	0.336E-01	0.331E-01	0.327E-01	0.319E-01	0.312E-01	0.310E-01	0.310E-01
0.24000	0.364E-01	0.364E-01	0.364E-01	0.362E-01	0.352E-01	0.343E-01	0.336E-01	0.331E-01	0.320E-01	0.311E-01	0.308E-01	0.308E-01
0.24222	0.380E-01	0.380E-01	0.380E-01	0.376E-01	0.363E-01	0.352E-01	0.342E-01	0.335E-01	0.322E-01	0.310E-01	0.307E-01	0.307E-01
0.24444	0.394E-01	0.394E-01	0.393E-01	0.387E-01	0.373E-01	0.359E-01	0.348E-01	0.338E-01	0.324E-01	0.310E-01	0.306E-01	0.306E-01
0.24667	0.403E-01	0.403E-01	0.400E-01	0.394E-01	0.378E-01	0.364E-01	0.351E-01	0.341E-01	0.326E-01	0.310E-01	0.306E-01	0.306E-01
0.24889	0.404E-01	0.403E-01	0.400E-01	0.393E-01	0.377E-01	0.363E-01	0.350E-01	0.340E-01	0.326E-01	0.311E-01	0.307E-01	0.307E-01
0.25111	0.395E-01	0.395E-01	0.391E-01	0.384E-01	0.369E-01	0.356E-01	0.345E-01	0.337E-01	0.324E-01	0.311E-01	0.308E-01	0.308E-01
0.25333	0.373E-01	0.373E-01	0.374E-01	0.368E-01	0.355E-01	0.345E-01	0.337E-01	0.330E-01	0.321E-01	0.312E-01	0.310E-01	0.310E-01
0.25556	0.356E-01	0.356E-01	0.353E-01	0.349E-01	0.338E-01	0.330E-01	0.326E-01	0.322E-01	0.317E-01	0.313E-01	0.312E-01	0.312E-01
0.25778	0.333E-01	0.333E-01	0.332E-01	0.329E-01	0.320E-01	0.316E-01	0.315E-01	0.314E-01	0.313E-01	0.314E-01	0.314E-01	0.314E-01
0.26000	0.315E-01	0.315E-01	0.314E-01	0.313E-01	0.307E-01	0.305E-01	0.306E-01	0.308E-01	0.309E-01	0.314E-01	0.315E-01	0.315E-01
0.26222	0.304E-01	0.305E-01	0.304E-01	0.304E-01	0.300E-01	0.299E-01	0.302E-01	0.305E-01	0.308E-01	0.314E-01	0.316E-01	0.316E-01
0.26444	0.302E-01	0.303E-01	0.303E-01	0.304E-01	0.300E-01	0.300E-01	0.303E-01	0.306E-01	0.308E-01	0.314E-01	0.315E-01	0.315E-01

MAXIMUM	4.496E-02	4.488E-02	4.379E-02	4.234E-02	4.044E-02	3.798E-02	3.550E-02	3.331E-02	3.157E-02	3.173E-02
TIME	8.000E-02	8.000E-02	8.000E-02	8.000E-02	8.000E-02	8.000E-02	8.000E-02	1.089E-01	2.667E-02	1.267E-01
MINIMUM	2.452E-02	2.503E-02	2.547E-02	2.612E-02	2.722E-02	2.864E-02	2.940E-02	3.018E-02	3.088E-02	3.034E-02
TIME	1.244E-01	1.244E-01	1.244E-01	1.244E-01	1.244E-01	9.556E-02	9.556E-02	9.556E-02	7.778E-02	8.000E-02
RANGE	2.044E-02	1.985E-02	1.832E-02	1.622E-02	1.322E-02	9.335E-03	6.094E-03	3.135E-03	6.949E-04	1.393E-03

MEMBER JOINT OR MEMBER

1	2	3	4	5	6	7	8	9	10	11
0.0000	-0.789E+03	-0.656E+04	0.292E+05	0.627E+04	-0.212E+05	-0.978E+04	-0.128E+05	-0.145E+05	-0.142E+05	0.443E+05
0.0022	-0.345E+03	-0.879E+04	0.295E+05	0.140E+05	-0.806E+04	0.962E+04	0.450E+04	0.277E+05	0.275E+05	0.440E+05
0.0044	0.175E+03	-0.101E+05	0.314E+05	0.243E+05	0.814E+04	0.313E+05	0.247E+05	0.734E+05	0.730E+05	0.437E+05
0.0067	0.691E+03	-0.108E+05	0.330E+05	0.346E+05	0.239E+05	0.509E+05	0.428E+05	0.111E+06	0.110E+06	0.435E+05
0.0089	0.106E+04	-0.116E+05	0.316E+05	0.413E+05	0.352E+05	0.641E+05	0.536E+05	0.131E+06	0.129E+06	0.434E+05
0.0111	0.114E+04	-0.132E+05	0.254E+05	0.415E+05	0.382E+05	0.671E+05	0.536E+05	0.132E+06	0.129E+06	0.434E+05
0.0133	0.902E+03	-0.156E+05	0.141E+05	0.342E+05	0.311E+05	0.585E+05	0.415E+05	0.115E+06	0.113E+06	0.435E+05
0.0156	0.448E+03	-0.182E+05	0.363E+05	0.419E+05	0.150E+05	0.396E+05	0.192E+05	0.866E+05	0.849E+05	0.437E+05
0.0178	0.774E+02	-0.202E+05	0.443E+05	0.565E+04	-0.601E+04	0.146E+05	-0.900E+04	0.516E+05	0.512E+05	0.439E+05
0.0200	-0.554E+03	-0.204E+05	0.498E+05	0.279E+05	-0.271E+05	0.108E+05	-0.371E+05	0.173E+05	0.179E+05	0.442E+05
0.0222	0.904E+03	-0.187E+05	0.360E+05	0.190E+05	-0.437E+05	0.315E+05	-0.601E+05	0.101E+05	-0.863E+04	0.444E+05
0.0244	0.102E+04	-0.143E+05	0.379E+05	0.234E+05	-0.529E+05	0.440E+05	-0.734E+05	-0.261E+05	-0.238E+05	0.446E+05
0.0267	0.870E+03	-0.731E+04	0.334E+05	0.216E+05	-0.533E+05	-0.471E+05	-0.757E+05	-0.293E+05	-0.263E+05	0.446E+05
0.0289	0.512E+03	0.112E+04	0.243E+05	0.160E+05	-0.452E+05	-0.413E+05	-0.676E+05	-0.214E+05	-0.181E+05	0.446E+05
0.0311	0.150E+03	0.923E+04	0.147E+05	0.107E+05	-0.300E+05	-0.285E+05	-0.514E+05	-0.516E+04	-0.256E+04	0.446E+05
0.0333	0.341E+02	0.154E+05	0.813E+04	-0.904E+04	-0.100E+05	-0.110E+05	-0.297E+05	0.164E+05	0.178E+05	0.442E+05
0.0356	0.260E+02	0.193E+05	0.505E+04	-0.113E+05	0.122E+05	0.875E+04	-0.500E+04	0.408E+05	0.408E+05	0.440E+05
0.0378	0.731E+01	0.219E+05	0.300E+04	-0.142E+05	0.343E+05	0.283E+05	0.202E+05	0.656E+05	0.643E+05	0.438E+05
0.0400	0.109E+03	0.245E+05	0.108E+05	0.141E+05	0.537E+05	0.458E+05	0.435E+05	0.879E+05	0.856E+05	0.434E+05
0.0422	0.401E+03	0.275E+05	0.744E+04	-0.100E+05	0.680E+05	0.755E+05	0.622E+05	0.105E+06	0.102E+06	0.434E+05
0.0444	0.735E+03	0.302E+05	0.136E+05	-0.471E+04	0.753E+05	0.623E+05	0.737E+05	0.114E+06	0.110E+06	0.434E+05
0.0467	0.949E+03	0.314E+05	0.158E+05	-0.225E+04	0.744E+05	0.591E+05	0.758E+05	0.113E+06	0.110E+06	0.434E+05
0.0489	0.955E+03	0.276E+05	0.114E+05	0.561E+04	0.651E+05	0.471E+05	0.677E+05	0.102E+06	0.996E+05	0.435E+05
0.0511	0.751E+03	0.265E+05	0.359E+03	-0.154E+05	0.485E+05	0.274E+05	0.500E+05	0.801E+05	0.795E+05	0.437E+05
0.0533	0.371E+03	0.211E+05	0.158E+05	-0.300E+05	0.268E+05	0.240E+04	0.252E+05	0.509E+05	0.515E+05	0.440E+05
0.0556	0.121E+03	0.144E+05	0.345E+05	-0.469E+05	0.352E+04	-0.238E+05	-0.235E+04	0.185E+05	0.201E+05	0.442E+05
0.0578	0.627E+03	0.740E+04	0.527E+05	-0.623E+05	-0.167E+05	-0.462E+05	-0.276E+05	0.116E+05	-0.891E+04	0.445E+05
0.0600	0.104E+04	-0.102E+05	0.664E+05	-0.723E+05	-0.294E+05	-0.602E+05	-0.537E+05	-0.341E+05	-0.305E+05	0.446E+05
0.0622	0.130E+04	-0.432E+04	0.719E+05	-0.733E+05	-0.317E+05	-0.625E+05	-0.533E+05	-0.460E+05	-0.417E+05	0.448E+05
0.0644	0.144E+04	-0.861E+04	0.662E+05	-0.630E+05	-0.221E+05	-0.518E+05	-0.485E+05	-0.456E+05	-0.419E+05	0.448E+05
0.0667	0.144E+04	-0.118E+05	0.482E+05	-0.405E+05	-0.671E+02	-0.276E+05	-0.307E+05	-0.322E+05	-0.294E+05	0.443E+05
0.0689	0.124E+04	-0.133E+05	0.190E+05	-0.663E+04	0.338E+04	0.916E+04	0.221E+03	-0.542E+04	-0.478E+04	0.440E+05
0.0711	0.716E+03	-0.122E+05	0.309E+05	0.355E+05	0.770E+05	0.564E+05	0.426E+05	0.336E+05	0.319E+05	0.437E+05
0.0733	0.153E+03	0.835E+04	0.567E+05	0.805E+05	0.124E+06	0.109E+06	0.921E+05	0.807E+05	0.771E+05	0.439E+05
0.0756	0.119E+04	-0.299E+04	0.908E+05	0.121E+06	0.167E+06	0.159E+06	0.141E+06	0.128E+06	0.123E+06	0.430E+05
0.0778	0.209E+04	0.142E+04	0.114E+06	0.150E+06	0.198E+06	0.196E+06	0.178E+06	0.163E+06	0.159E+06	0.428E+05
0.0800	0.257E+04	0.248E+04	0.123E+06	0.161E+06	0.209E+06	0.210E+06	0.194E+06	0.178E+06	0.174E+06	0.427E+05
0.0822	0.247E+04	0.106E+04	0.116E+05	0.153E+06	0.197E+06	0.198E+06	0.182E+06	0.164E+06	0.161E+06	0.429E+05
0.0844	0.180E+04	-0.898E+04	0.963E+05	0.127E+04	0.165E+05	0.160E+06	0.145E+06	0.123E+06	0.122E+06	0.432E+05
0.0867	0.691E+03	-0.199E+05	0.664E+05	0.885E+05	0.117E+06	0.103E+06	0.891E+05	0.648E+05	0.649E+05	0.436E+05
0.0889	-0.607E+03	0.317E+05	0.335E+05	0.457E+05	0.639E+05	0.410E+05	0.281E+05	0.916E+03	0.237E+04	0.440E+05
0.0911	-0.174E+04	-0.415E+05	0.485E+04	0.799E+04	0.166E+05	-0.146E+05	-0.249E+05	-0.540E+05	-0.513E+05	0.444E+05
0.0933	-0.238E+04	-0.468E+05	-0.152E+05	-0.168E+05	-0.155E+05	-0.520E+05	-0.584E+05	-0.680E+05	-0.845E+05	0.446E+05
0.0956	-0.236E+04	-0.462E+05	-0.182E+05	-0.252E+05	-0.286E+05	-0.642E+05	-0.656E+05	-0.938E+05	-0.905E+05	0.446E+05
0.0978	-0.181E+04	-0.402E+05	-0.574E+04	-0.189E+05	-0.245E+05	-0.499E+05	-0.453E+05	-0.702E+05	-0.678E+05	0.445E+05
0.1000	-0.960E+03	-0.309E+05	0.250E+04	-0.346E+04	-0.918E+04	-0.139E+05	-0.222E+05	-0.222E+05	-0.210E+05	0.442E+05
0.1022	-0.342E+02	-0.206E+05	0.190E+05	0.156E+05	0.111E+05	0.345E+05	0.532E+05	0.395E+05	0.394E+05	0.438E+05
0.1044	0.849E+03	-0.104E+05	0.339E+05	0.338E+05	0.310E+05	0.830E+05	0.108E+06	0.101E+06	0.997E+05	0.435E+05
0.1067	0.160E+04	-0.144E+04	0.535E+05	0.477E+05	0.457E+05	0.119E+06	0.148E+06	0.148E+06	0.146E+06	0.432E+05
0.1089	0.207E+04	0.532E+04	0.612E+05	0.536E+05	0.504E+05	0.135E+06	0.165E+06	0.172E+06	0.168E+06	0.430E+05
0.1111	0.210E+04	0.803E+04	0.611E+05	0.476E+05	0.408E+05	0.155E+06	0.155E+06	0.167E+06	0.164E+06	0.431E+05
0.1133	0.161E+04	0.521E+04	0.517E+05	0.344E+05	0.161E+05	0.942E+05	0.122E+06	0.138E+06	0.135E+06	0.432E+05
0.1156	0.724E+03	-0.300E+04	0.342E+05	-0.164E+05	-0.203E+05	0.487E+05	0.726E+05	0.918E+05	0.901E+05	0.436E+05
0.1178	-0.310E+03	-0.143E+05	0.123E+05	-0.353E+04	-0.608E+05	-0.152E+04	0.180E+05	0.384E+05	0.381E+05	0.439E+05
0.1200	-0.122E+04	-0.261E+05	-0.936E+04	-0.658E+05	-0.969E+05	-0.462E+05	-0.313E+05	-0.110E+05	-0.990E+04	0.443E+05
0.1222	-0.173E+04	-0.354E+05	-0.267E+05	-0.863E+05	-0.121E+06	-0.768E+05	-0.659E+05	-0.466E+05	-0.444E+05	0.446E+05
0.1244	-0.173E+04	-0.407E+05	-0.371E+05	-0.933E+05	-0.129E+06	-0.877E+05	-0.800E+05	-0.624E+05	-0.593E+05	0.447E+05

MAXIMUM 2-566E+03 8-638E+04 9-228E+04 1-347E+05 1-608E+05 2-088E+05 2-104E+05 1-938E+05 1-775E+05 1-741E+05 4-471E+04
TIME 8-000E-02 1-444E-01 8-000E-02 2-489E-01 8-000E-02 8-000E-02 8-000E-02 8-000E-02 8-000E-02 8-000E-02 1-267E-01

MINIMUM -2-376E+03 -4-678E+04 -5-655E+04 -8-432E+04 -9-325E+04 -1-292E+05 -8-774E+04 -7-997E+04 -9-384E+04 -9-050E+04 4-275E+04

TIME 9-333E-02 9-333E-02 2-200E-01 2-222E-01 1-244E-01 1-244E-01 1-244E-01 1-244E-01 9-556E-02 9-556E-02 8-000E-02
RANGE 4-942E+03 1-332E+05 1-488E+05 2-190E+05 2-541E+05 3-381E+05 2-981E+05 2-738E+05 2-714E+05 2-646E+05 1-963E+03

5978

COSINE HARMONIC

JOINT OR MODE

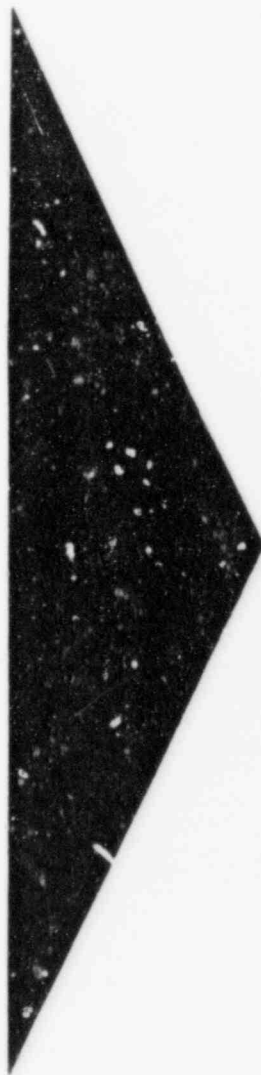
	1	2	3	4	5	6	7	8	9	10	11
0	-7.058E-10	5.480E+03	1.096E+04	1.644E+04	2.192E+04	2.740E+04	3.288E+04	3.836E+04	4.384E+04	4.384E+04	4.384E+04
1	-2.200E+00	-1.022E+04	-2.024E+04	-5.964E+03	-6.107E+03	-5.982E+03	-2.027E+04	-1.027E+04	-7.324E+01	-6.318E+01	8.175E+01
2	-2.456E+00	5.138E+03	-8.340E+00	2.500E+04	-3.328E+01	-2.507E+04	-5.569E+01	-5.198E+03	-5.027E+01	-5.306E+01	1.285E+01
3	6.768E+01	1.600E+02	1.762E+04	2.975E+04	4.233E+04	3.019E+04	1.849E+04	1.474E+03	1.838E+03	1.674E+03	-8.866E+01
4	2.589E+00	-1.061E+03	-2.131E+03	-1.054E+03	1.441E+01	1.083E+03	2.157E+03	1.082E+03	1.045E+01	1.781E+01	-2.514E+00
5	-7.823E+01	1.434E+03	-1.084E+04	-1.816E+04	-2.832E+04	-1.878E+04	-1.208E+04	-4.040E+02	-2.511E+03	-2.371E+03	5.684E+01
6	1.435E+00	-2.081E+03	5.344E+01	-1.632E+03	1.445E+02	1.920E+03	2.293E+02	2.356E+03	2.632E+02	2.472E+02	-3.462E+00
7	1.231E+02	3.334E+03	1.139E+04	5.202E+03	2.223E+03	6.185E+03	1.335E+04	6.225E+03	3.938E+03	3.746E+03	-3.696E+01
8	-7.809E+02	-8.688E+03	-1.626E+04	-2.348E+04	-3.018E+04	-3.622E+04	-4.147E+04	-4.581E+04	-4.918E+04	-4.763E+04	3.572E+02
9	2.461E+02	2.061E+03	-2.741E+02	1.770E+03	6.564E+03	2.880E+03	1.814E+03	6.067E+03	4.278E+03	4.201E+03	-2.258E+01
10	2.587E+02	4.402E+02	3.935E+03	8.743E+03	7.046E+03	5.126E+03	9.271E+03	1.168E+04	1.037E+04	1.027E+04	-8.186E+01
11	-5.719E+02	-3.189E+03	-4.887E+03	-5.984E+03	-8.949E+03	-1.253E+04	-1.773E+04	-2.183E+04	-2.444E+04	-2.464E+04	1.018E+02
12	-6.497E+01	-1.706E+03	-3.246E+03	-2.266E+03	-1.171E+03	-1.753E+01	1.132E+03	-1.352E+02	-1.402E+03	-1.455E+03	4.782E+00
13	2.427E+01	1.112E+03	9.509E+01	4.520E+01	-1.309E+03	2.838E+02	5.649E+02	1.799E+03	9.131E+02	9.018E+02	-3.659E+00
14	-1.895E+01	-8.817E+02	-2.231E+02	-1.030E+03	-2.779E+02	4.913E+02	-2.635E+02	4.776E+02	-2.741E+02	-2.953E+02	7.530E-01
15	-1.564E+01	5.068E+02	6.747E+02	-1.479E+02	-2.610E+02	-5.273E+02	1.432E+02	-5.243E+02	-1.280E+03	-1.406E+03	2.146E+00
16	1.486E+02	7.170E+02	1.198E+03	1.578E+03	1.828E+03	1.925E+03	1.863E+03	1.646E+03	1.299E+03	1.468E+03	-2.707E+00
17	-1.280E+00	4.130E+02	1.272E+02	-6.918E+01	3.393E+02	-2.153E+02	-1.510E+02	2.975E+01	-4.551E+02	-5.359E+02	8.954E-01
18	-8.625E+00	-4.463E+02	-8.194E+01	5.113E+01	-9.005E+01	-2.217E+02	-6.098E+01	3.462E+02	-3.645E+01	-4.470E+01	6.797E-02
19	1.782E+00	2.608E+02	3.651E+02	5.674E+02	3.587E+02	2.886E+02	-1.615E+02	-4.553E+02	-8.299E+02	-1.017E+03	1.466E+00
20	-2.470E+01	-4.660E+02	-8.435E+02	-5.785E+02	-2.399E+02	1.291E+02	4.814E+02	2.371E+02	-3.761E+01	-4.920E+01	6.144E-02
21	6.254E+00	-2.155E+02	-1.945E+02	2.712E+02	7.294E+01	1.417E+02	-4.540E+01	-9.908E+01	-3.382E+02	-6.673E+02	5.046E-01
22	-1.012E+01	-2.647E+02	-1.073E+02	-2.502E+02	-9.259E+01	7.920E+01	-2.341E+01	1.944E+02	1.308E+01	1.764E+01	-1.875E-02
23	6.170E+00	1.973E+02	2.239E+02	8.102E+01	1.349E+02	-1.972E+01	3.883E+01	-4.206E+01	-2.501E+02	-3.624E+02	3.560E-01
24	3.370E+01	1.719E+02	2.720E+02	3.215E+02	3.112E+02	2.432E+02	1.299E+02	-7.561E+00	-1.452E+02	-2.289E+02	2.053E-01

SINE HARMONIC

JOINT OR MODE

	1	2	3	4	5	6	7	8	9	10	11
1	-3.735E+00	-1.003E+04	1.440E+02	-3.207E+03	-1.430E+04	-2.092E+01	1.082E+02	-1.009E+04	-7.964E+01	-6.653E+01	3.286E+01
2	1.061E+00	2.501E+04	-1.928E+01	-5.200E+03	-9.351E+01	5.012E+03	-1.684E+02	-2.520E+04	-1.922E+02	-1.726E+02	2.250E+01
3	-5.053E+01	-1.741E+04	-1.810E+04	-3.065E+04	-1.910E+04	-3.103E+04	-1.885E+04	-1.853E+04	-1.532E+03	-1.426E+03	9.643E+01
4	8.846E-01	-6.594E+03	-1.315E+04	-6.441E+03	3.064E+02	7.052E+03	1.376E+04	7.194E+03	5.897E+02	5.465E+02	-1.773E+01
5	-1.685E+02	-1.309E+04	-1.627E+04	-2.697E+04	-2.089E+04	-2.821E+04	-1.873E+04	-1.676E+04	-5.056E+03	-4.723E+03	9.408E+01
6	-1.046E+00	1.718E+03	-2.709E+01	-2.140E+03	-3.664E+01	2.067E+03	-4.418E+01	-1.787E+03	-6.318E+01	-6.152E+01	1.149E+00
7	-1.133E+02	-8.205E+03	-6.554E+03	-3.662E+03	-1.101E+04	-4.594E+03	-8.403E+03	-1.094E+04	-3.721E+03	-3.549E+03	3.964E+01
8	1.090E+03	1.365E+04	2.574E+04	3.734E+04	4.820E+04	5.814E+04	6.694E+04	7.446E+04	8.059E+04	7.754E+04	-6.384E+02
9	-3.367E+02	-6.716E+03	-1.083E+04	-8.598E+03	-1.174E+04	-1.172E+04	-1.699E+04	-1.576E+04	-1.212E+04	-1.182E+04	7.618E+01
10	-5.163E+01	2.697E+03	-8.590E+02	4.047E+02	-1.732E+03	-3.826E+03	-2.433E+03	-5.777E+03	-2.732E+03	-2.668E+03	1.631E+01
11	2.936E+02	2.178E+02	3.757E+03	5.178E+03	9.491E+03	8.252E+03	9.801E+03	9.029E+03	1.165E+04	1.160E+04	-5.412E+01
12	8.899E+01	2.254E+03	4.309E+03	3.132E+03	1.824E+03	4.367E+02	-9.748E+02	7.003E+02	2.347E+03	2.392E+03	-8.720E+00
13	1.184E+02	-1.623E+02	-2.523E+02	-8.584E+02	1.745E+02	9.086E+02	3.187E+03	4.767E+03	6.315E+03	6.605E+03	-1.983E+01
14	7.980E+00	8.164E+02	7.789E+01	-6.427E+02	1.397E+02	9.145E+02	1.714E+02	-6.030E+02	1.572E+02	1.637E+02	-4.577E-01
15	7.662E+00	-4.548E+02	2.604E+02	2.323E+02	-5.424E+02	3.515E+02	4.921E+02	-1.240E+02	4.218E+02	4.450E+02	-1.154E+00
16	-1.118E+02	-5.494E+02	-9.251E+02	-1.231E+03	-1.444E+03	-1.548E+03	-1.534E+03	-1.403E+03	-1.168E+03	-1.303E+03	2.862E+00
17	4.280E+00	-2.035E+02	-5.832E+02	-2.013E+01	2.096E+02	1.545E+02	-2.491E+02	2.614E+02	5.637E+02	6.431E+02	-1.178E+00
18	6.206E+00	1.876E+02	7.970E+01	4.777E+02	7.219E+01	-3.401E+02	3.800E+01	-1.008E+02	4.073E+01	4.693E+01	-7.570E-02
19	3.272E+00	-9.721E+01	1.810E+02	2.764E+02	5.102E+02	1.595E+02	-3.787E+01	-3.900E+02	-3.276E+02	-4.238E+02	5.328E-01
20	3.366E+00	9.146E+01	1.717E+02	1.107E+02	4.086E+01	-3.248E+01	-1.039E+02	-3.995E+01	2.684E+01	3.177E+01	-4.098E-02
21	-5.554E+00	-7.871E+01	-2.735E+02	-4.077E+02	-4.400E+02	-2.261E+02	6.555E+01	3.726E+02	5.014E+02	6.577E+02	-7.859E-01
22	1.162E+00	1.424E+02	-4.799E-01	-1.938E+02	1.287E+01	2.183E+02	2.142E+01	-1.272E+02	6.717E+00	9.088E+00	-7.897E-03
23	3.565E+00	1.070E+01	1.786E+02	7.393E+01	-6.828E+01	3.379E+01	1.059E+02	-8.091E+01	-8.998E+01	-1.438E+02	1.223E-01
24	-2.124E+01	-9.955E+01	-1.576E+02	-1.896E+02	-1.902E+02	-1.591E+02	-1.013E+02	-2.593E+01	5.529E+01	7.565E+01	-6.910E-02

REPORT APPROVAL FORM



1.6.1

FOR INTERNAL USE ONLY

FAILURE ANALYSIS ASSOCIATES

IN-HOUSE REPORT APPROVAL FORM

Communication Title or Subject:

Calculations for Generator Skof4
and Bearing for River Bend Nuclear
Station Diesel Generator

Communication Number: NLR Communication Date: _____

Project Number: DR-06-03-6506

Task Number (if applicable): _____

Approvals

Craig Vinyler
Task Engineer

Date: 1-21-85

Albert Wells
Corporate Officer

Date: 2-4-85

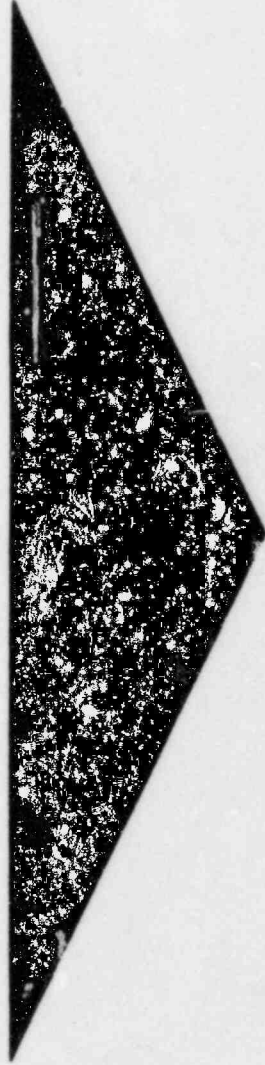
Albert Wells
Communication Reviewer

Date: 2-4-85

W. B. G.
Support Package Reviewer

Date: 25 Jan 85

SUPPORT PACKAGE COVER SHEET AND TABLE OF CONTENTS SP-84-6-47(g)



FAILURE ANALYSIS ASSOCIATES
SUPPORT PACKAGE COVER SHEET

Support Package Number: SP-84-6-47(g)

Communication Number: None

Communication Date: _____

Communication Title or Subject: Calculations for Generator Shaft and Bearing for River Bend Nuclear Station Diesel Generator

Project Number: D2-06-03-652C

Task Number (if applicable): _____

Task Engineer: Craig K. Kula Date: 12-2-84

Reviewer: [Signature] Date: 1/3/85

SUPPORT PACKAGE CONTENTS
(Optional for Non Nuclear Work)

ITEM	SUPPORT OF
1. Hand Calculation Cover Sheet: River Bend Generator Shaft and Bearing Analysis. (13 pages)	Provides outline of necessary calculations.
2. TDI Torsional Analysis for River Bend Diesel Generator by Robert Yang (4 pages)	Provides dimensions, weights, bearing reactions, and moments (used as input of calculation)

FAILURE ANALYSIS ASSOCIATES

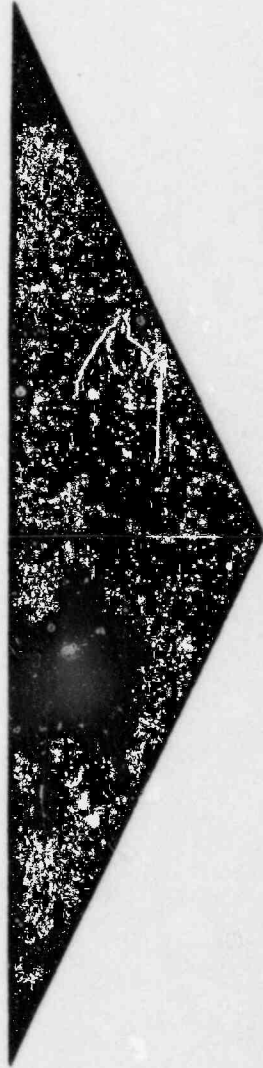
SUPPORT PACKAGE COVER SHEET (CONTINUED)

Support Package Number: SP-84-647(g)

SUPPORT PACKAGE CONTENTS

ITEM	SUPPORT OF
<p>- 3. Torque Excursions Between the Flywheel to Generator and Generator to Grid for River Bend by Lisa Skurto (2 pages)</p>	<p>Provides torque inputs used in calculating stresses</p>
<p>- 4. Telephone Memorandum: Craig Vogler, FAA and Bob Klashen, Rortec (1 page)</p>	<p>Shaft material, weight, magnetic pull</p>
<p>- 5. Telephone Memorandum: Craig Vogler, FAA and Walter Heacham, FAA (1 page)</p>	<p>8" Bearing clearances</p>
<p>6. ASTM A-668 Class D material specification (10 pages)</p>	<p>Provides material properties of generator shaft</p>

COMPONENT DESIGN REVIEW CHECKLIST - RIVER BEND STATION - UNIT 1.



COMPONENT DESIGN REVIEW CHECKLIST
RIVER BEND STATION - UNIT 1

Generator: _____ UTILITY Gulf States Utilities
COMPONENT Shaft & Bearings
GROUP PARTS LIST NO. 03-650C TASK DESCRIPTION NO. DR-06-03-650C-0
SNPS GPL NO. 03-650C CLASSIFICATION TYPE A

TASK DESCRIPTIONS

Design review for this component is not required based on the following:

- The static lateral and dynamic torsional loadings were computed and used to evaluate both the generator shaft factor of safety, for yielding and fatigue, and the bearing operating characteristics. The resulting bearing operating characteristics are within accepted industry allowables and the factors of safety are comparable to the lead engines at Shoreham and Comanche Peak.
- A review of the EDG Component Tracking System indicates that there have been no design related problems associated with this component. There is no site experience for River Bend listed in the Component Tracking System.

There are no maintenance or modification recommendations for this component other than those specified by the vendor.

Quality Revalidation for this component is not required.

PRIMARY FUNCTION

Not required

ATTRIBUTE TO BE VERIFIED

Not required

COMPONENT DESIGN REVIEW CHECKLIST

Page 2 of 2
DR-06-03-650C-0

SPECIFIED STANDARDS

Not required

REFERENCES

Not required

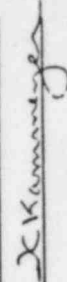
DOCUMENTATION REQUIRED

Not required

GROUP CHAIRPERSON



PROGRAM MANAGER



ITEM 1 HAND CALCULATION COVER SHEET: RIVER BEND GENERATOR SHAFT AND
BEARING ANALYSIS.



HAND CALCULATION COVER SHEET

CALCULATION TITLE River Bend Generator PROJECT NO. 22-0603-6506
Shaft and Bearing Analysis TASK NO. _____

DESCRIPTION OF CALCULATION

The primary purpose of this set of calculations is to determine if the generator shaft and bearing are acceptable for their intended use, in particular, that the factor of safety for static and fatigue failure is adequate and that the bearing oil film thickness is comparable to or surpasses industry recommendation

REFERENCES:

The calculations follow the outline written by Walter Meacham of FAA-Phoenix, in his calculations and support package for Shearon Harris. Other references are included in Support Package SP-84-6-456).

Subject Report: Deletion Justification

for Component 03-6506

Generator Shaft and Bearing

Report Number: 22-06-03-6506 Date: 12-3-84

Craig Vigha
Engineer

12-3-84
Date

W. S. Hall
Reviewer

12/1/84
Date

Wt of Flywheel:

For a solid disk. $W_c = 5\pi r^2 l$

$$W_c = (0.286)(\pi) \left(\frac{42.5}{2} \right)^2 (4.5) = 4074 \text{ lbs} \quad \checkmark \quad (\text{IDE value } 3589)$$

Est. Wt of generator shaft: (Act. weight not available at this time)

$$\left[\frac{\pi}{4} (2.75)^2 (3) + (16.5)(14k) + 44.44(19) \right] + \frac{1}{3} \pi \left(\frac{42.25}{4} \right)^2 (4.30) \left[1 + \left(\frac{4}{3} \right) \right] + \left(\frac{4}{3} \right) \pi (1.75)^2 (9.33k) \right]$$

$$+ (4^2)(\pi)(20) (0.286)$$

$$= \frac{\pi}{4} (0.286) \left[1728 + 3946 + 16043 + \left[\frac{1}{3} \pi (818) (1 + 4.27 + .122) + \pi (3.20) \right] \right] \cdot 286$$

$$= 0.286 [17052 + (1378) + (1005)] = 5560 \text{ lbs est.}$$

Windings - rotor = 25,000 lb

total shaft + rotor \approx approx. 30,560 lbs. \checkmark (5% for Exc. Magnetism
of rotor)

From flange to rot. element = 36.0"

flange to bearing ϕ = 32.0"

$$C = 13 \frac{3}{4} + 3 + 36 = 52.75 \quad \checkmark$$

$$D = 13 \frac{3}{4} + 3 + 82 = 98.75$$

$$W_c \approx 640 \text{ lb}$$

$$A = 7.85$$

$$B = 15.25$$

$$\Sigma R = 0 \therefore R_1 + R_2 = W_c + W_4 + W_6$$

$$R_1 + R_2 = 35297 \approx 35300 \text{ lb}$$

$$\Sigma M = 0 \quad R_2 = \frac{(640)(7.85) + (4074)(15.25) + (52.75)(30,560)}{98.75} = 17008 \text{ lb}$$

$$R_1 = 18312 \text{ lb.} \quad \checkmark$$

Pedestal Bearing Analysis

for 8" bearing:

$$\begin{array}{l} \text{vert: } 8.010 - 8.014 = 8.012 \\ \text{horz: } 8.018 - 8.022 = 8.020 \\ \text{Length: } 16" \end{array}$$

$$0.1 \text{ Visc. } \mu = 3.015 \times 10^{-6} \text{ reyn @ } 155^\circ\text{F}$$

$$\frac{L}{D} = \frac{16}{8} = 2$$

$$R = \frac{1}{2} (8.012) = 4.006$$

$$C = \frac{1}{2} (8.020 - 8.000) = \frac{-0.020}{2} = -0.010$$

$$R+d = \frac{1}{2} (8.020) = 4.010$$

$$d = -0.004$$

$$S = \frac{d}{C} = \frac{-0.004}{-0.010} = .4$$

$$C_m = \frac{1}{2} (8.012 - 8.000) = .006$$

$$s = \frac{3.015 \times 10^{-6} (450/60) (4.006)^2}{17008 / 16 \times 8} = .035$$

$$E_{12} = .805$$

$$h_{min} = (.010)(1 - .805) = .00185 = 1.95 \times 10^{-3} \text{ inches}$$

from table 4-1:

$$\frac{L}{D} > \infty, s = .035 \therefore \frac{P_s}{P} = 1.56$$

$$\text{unit load} = \frac{17008}{16 \times 8} = 133 \text{ psi}$$

$$F_{max} = 133 \times 1.56 = 207 \text{ psi}$$

Min oil film thickness: 1.9×10^{-3} inches ✓
 Peak oil film pressure: 210 psi ✓
 Unit Load: 133 psi ✓

RIVER BEND

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Summary of generator bearing.

Minimum oil film thickness 1.9×10^{-3} inches ✓
Peak oil film pressure 210 psi
Unit load 133 psi

Industry recommendations for oil film thickness:

30 micro-inches per inch of shaft diameter
or $30 \times 10^{-6} \times 8.0'' = 240 \times 10^{-6}$ inches (2.40×10^{-4} in)

It can be concluded that the bearing is acceptable for its intended use.

Ref:

Determine stresses due to torques

$$\tau = \frac{I_x}{J} \quad \text{use stress concentration factor of 2}$$

$$\text{Flywheel: } r = \frac{16,625}{2} = 8.31'' \quad J = \frac{1}{2} \pi (8.31)''^4 = 7490$$

$$T_{\max} = 2.166 \times 10^5 \text{ ft-lb} = 2.60 \times 10^6 \text{ in-lb}$$

$$T_{\min} = -1.088 \times 10^5 \text{ ft-lb} = -1.31 \times 10^6 \text{ in-lb}$$

$$\tau_{\max} = 2 \times \frac{2.6 \times 10^6}{7490} (8.31) = 5769 \text{ psi}$$

$$\tau_{\min} = 2 \times \frac{(-1.31 \times 10^6)}{7490} (8.31) = -2907 \text{ psi}$$

$$\tau_m = \frac{5769 + (-2907)}{2} = 1431 \text{ psi}$$

$$\tau_a = 5769 - 1431 = 4338 \text{ psi}$$

$$\text{Gen-Grid } r = 9.438 \quad J = \frac{1}{2} \pi (9.438)''^4 = 12463$$

$$T_{\max} = 5.588 \times 10^4 \text{ ft-lb} = 6.71 \times 10^5 \text{ in-lb}$$

$$T_{\min} = 5.345 \times 10^4 \text{ ft-lb} = 6.41 \times 10^5 \text{ in-lb}$$

$$\tau_{\max} = 2 \times \frac{6.71 \times 10^5}{12463} (9.438) = 1016 \text{ psi}$$

$$\tau_{\min} = 2 \times \frac{6.41 \times 10^5}{12463} (9.438) = 971 \text{ psi}$$

$$\tau_m = \frac{1016 + 971}{2} = 994$$

$$\tau_a = 1016 - 994 = 22$$

Bending Moment

@ Flywheel

$$M_1 = R_1 \cdot E - U_f(E-B) - W_L(E-A)$$

$$E = B + \frac{1}{2} (\text{flywheel thickness}) = \frac{1}{2} (4.78) + 15.25 = 17.56$$

$$M_1 = (19316)(17.56) - (4074)(2.31) - 690(17.56 - 7.85)$$

$$M_1 = 305,518 \text{ lbf-in}$$

@ Gen-Grid

$$M_2 = R_1 \cdot C - W_C(C-B) - W_L(C-A)$$

$$M_2 = 18316(52.75) - 4074(52.75 - 15.25) - 690(52.75 - 7.85)$$

$$M_2 = 782,413$$

193750

$$\sigma_{\text{max}} = I \frac{Mx}{I} = \text{@ Flywheel: } I \frac{305518(2.31)}{\frac{1}{4} \pi (3.3)^4} = 678 \text{ psi}$$

use 2.5 stress riser:

$$\sigma_{\text{max}} = I 1700$$

$$\sigma_{\text{min}} = 0$$

$$\text{@ Grid-Gen: } I \frac{782413(9.44)}{\frac{1}{4} \pi (9.44)^4} = 1184 \text{ psi}$$

with 2.5 stress riser: $\sigma_{\text{max}} = I 2960 \text{ psi}$

$$\sigma_{\text{min}} = 0$$

Combination Stresses:

$$\text{@ Flywheel: } \sigma_{\text{max}} = (678^2 + 3 \cdot 5769^2)^{1/2} = 10140 \text{ psi}$$

$$\sigma_{\text{min}} = (1700^2 + 3 \cdot (2407)^2)^{1/2} = 5314 \text{ psi}$$

$$\sigma_a = (1700^2 + 3 \cdot (4338)^2)^{1/2} = 7705 \text{ psi}$$

$$\sigma_m = (0 + 3 \cdot (1421)^2)^{1/2} = 2480 \text{ psi}$$

@ Gen-Grid:

$$\hat{\sigma}_{\text{max}} = (2960^2 + 3 \cdot (1016)^2)^{1/2} = 3444 \checkmark$$

$$\sigma_{\text{min}} = (2960^2 + 3 \cdot (971)^2)^{1/2} = 3404 \checkmark$$

$$\hat{\sigma}_a = (2960^2 + 3 \cdot (22)^2)^{1/2} = 2960 \checkmark$$

$$\sigma_m = (0 + 3 \cdot (994)^2)^{1/2} = 1722 \checkmark$$

Static Safety Factors:

Torsion:

$$\text{@ Flywheel: } \eta_T = \frac{S_{xy}}{\tau_{\text{max}}} = \quad S_{xy} = 0.577 S_y$$

$$\eta_T = \frac{21650}{5769} = 3.75 \checkmark$$

for shaft matl of A689
(ALUMINUM)assume 668

$$\text{@ Gen-Grid: } \eta_T = \frac{21650}{1016} = 21.3$$

Combined

$$\text{@ Flywheel: } \eta_\sigma = \frac{S_y}{\hat{\sigma}_{\text{max}}} = \frac{37500}{10140} = 3.7 \checkmark$$

$$\text{@ Gen-Grid: } \eta_\sigma = \frac{37500}{3444} = 10.9$$

RIVER BEND

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Fatigue Safety Factor

$$n_f = \left(\frac{(S_a)^2 + (S_m)^2}{\sigma_a^2 + \sigma_m^2} \right)^{1/2}$$

$$\text{where: } S_m = \frac{S_e}{\frac{\sigma_a}{\sigma_m} + \frac{S_e}{S_u}} \quad \text{and } S_u = \frac{S_e}{\frac{S_e}{S_u}}$$

@ Flywheel:

$$S_m = \frac{26250}{\frac{1705}{2480} + \frac{26250}{75000}} = 7594 \checkmark$$

$$S_a = \frac{-26250}{75000} (7594) + 26250 = 23600 \checkmark$$

$$n_f = \left(\frac{23600^2 + 7594^2}{7705^2 + 2480^2} \right)^{1/2} = 3.06 \checkmark$$

@ Gen-Grid

$$S_m = \frac{26250}{\frac{2960}{1722} + \frac{26250}{75000}} = 12690$$

$$S_a = \frac{-26250}{75000} (12690) + 26250 = 21810 \checkmark$$

$$n_f = \left(\frac{21810^2 + 12690^2}{2960^2 + 1722^2} \right)^{1/2} = 7.4 \checkmark$$

Distortion energy fatigue failure

e Flywheel

$$Ud = \frac{1 \pm \sqrt{3}}{3E} = \frac{1 \pm 0.866}{3(2.0 \times 10^6)} = 1.44 \times 10^{-8}$$

$$Ud_{max} = 1.44 \times 10^{-8} (10140)^2 = 1.49$$

$$Ud_{min} = 1.44 \times 10^{-8} (5314)^2 = 0.41$$

$$Ud_m = 1.44 \times 10^{-8} (2480)^2 = 0.09$$

$$\frac{3E}{1 \pm \sqrt{3}} = \frac{90 \times 10^6}{1.73} = 8320$$

I $8320 \left[(1.49)^{1/2} - 2(0.41)^{1/2} \right] \geq S_y ?$

$$-500 < 37500$$

II $8320 \left[(1.49)^{1/2} - (0.09)^{1/2} \right] \geq S_e ?$

$$7660 < 26250$$

III $8320 \left[(1.49)^{1/2} - (0.09)^{1/2} \left(1 - \frac{26250}{25000} \right) \right] \geq S_e ?$

$$8533 < 26250$$

IV $8320 (1.49)^{1/2} \geq S_y ?$

$$10155 < 10155$$

ADDITIONAL
POSTER

@ Gen- Grid

$$Ud_{max} = \frac{1 + 0.3}{3(30 \times 10^6)} (3444)^2 = 0.17$$

$$Ud_{min} = \frac{1.3}{90 \times 10^6} (3404)^2 = 0.17$$

$$Ud_m = \frac{1.3}{90 \times 10^6} (1722)^2 = 0.043$$

$$I \left[\frac{3(30 \times 10^6)}{1 + 0.3} \right]^{\frac{1}{2}} \left[(.17)^{\frac{1}{2}} - 2(.17)^{\frac{1}{2}} \right] \geq S_y ? \quad -3431 < 37500 \quad \text{ok}$$

$$II \left[\frac{90 \times 10^6}{1.3} \right]^{\frac{1}{2}} \left[(.17)^{\frac{1}{2}} - (.043)^{\frac{1}{2}} \right] \geq S_e ? \quad 1705 < 26250 \quad \text{ok}$$

$$III \left[\frac{90 \times 10^6}{1.3} \right]^{\frac{1}{2}} \left[(.17)^{\frac{1}{2}} - (.043)^{\frac{1}{2}} \left(1 - \frac{2.6250}{75000} \right) \right] \geq S_e ? \quad 2310 < 26250 \quad \text{ok}$$

$$IV \left[\frac{90 \times 10^6}{1.3} \right]^{\frac{1}{2}} (.17)^{\frac{1}{2}} \geq S_y ? \quad 3431 < 37500 \quad \text{ok}$$

Dynamic lateral loads

At center of windings:

$$P = 30560 \text{ lbf}$$

$$a = 52.75''$$

$$b = (D-c) = 46.0''$$

$$r = 52.75''$$

$$l = D = 18.75$$

$$\alpha = \frac{r}{l} = \frac{52.75}{98.75} = .53$$

$$\beta = \frac{b}{l} = \frac{46.0}{98.75} = .47$$

$$\gamma = \frac{x}{l} = \frac{52.75}{98.75} = .53$$

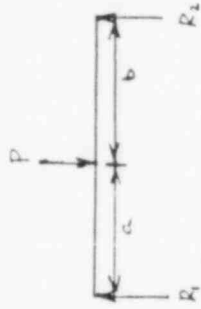
$$I = \frac{1}{4} \pi (9.438)^4 = 6232$$

$$EI\omega = \frac{PI^3}{6} (\beta \cdot \gamma) (\alpha [1+\beta] - \gamma^2)$$

$$= \frac{(30560)(98.75)^3}{6} (.47)(.53) [.53(1+.47) - .53^2]$$

$$= 6.1 \times 10^8$$

$$\omega = \frac{6.1 \times 10^8}{(30 \times 10^6)(6232)} = .0033''$$



@ flywheel

$$P = 4074 \text{ lbf}$$

$$a = B = 15.25$$

$$b = (D - B) = 83.5$$

$$r = C = 52.75$$

$$L = 92.75$$

$$\alpha = \frac{a}{L} = \frac{15.25}{92.75} = .155$$

$$\beta = \frac{b}{L} = \frac{83.5}{92.75} = .85$$

$$\gamma = \frac{r}{L} = \frac{52.75}{92.75} = .53$$

$$I = 6236 \quad (\text{use of units})$$

Total deflection:

$$EI\omega = \frac{PL^3}{6} (\alpha)(1-\beta) [\gamma(2-\gamma) - \alpha^2]$$

$$= \frac{4074(92.75)^3}{6} (.155)(1-.85) [(.53)(2-.53) - .155^2] =$$

$$= 3.60 \times 10^7$$

$$\omega = \frac{3.60 \times 10^7}{(30 \times 10^6)(6236)} = .0002$$

Total deflection at center of windings

$$= 0.0033 + 0.0002 = 0.0035 \text{ "}$$

Dynamic load due to magnetic pull

$$P = 14,000 \text{ lb at } \frac{1}{32} \text{ " displacement} = 448,000 \text{ lb/in.}$$

Force due to static offset

$$F_s = 448,000 (0.0035) = 1568 \text{ lb}$$

Dynamic load due to mass imbalance

$$F_d = m(e + u)\omega^2$$

where m = mass of windings
 e = mass cg offset
 u = static defl.
 ω = rot. speed rad/sec

$$m = \frac{25000}{386.4} = 64.7 \text{ lb/accel}$$

$$e = 0.010 \text{ conservative assumption}$$

$$u = 0.0035$$

$$\omega = 47.12 \text{ rad/sec}$$

$$F_d = 64.7 (0.010 + 0.0035)(47.12)^2 = 1939 \text{ lb}$$

Total Dynamic load - approx:

$$\text{Load} = F_m + F_d = 1568 + 1939 = 3507 \text{ lb}$$

$$\text{Gen weight} = 30560 \text{ lb}$$

$$\% \frac{\text{Dym. load}}{\text{Gen weight}} = \frac{3507}{30560} = 12.7$$

RIVEE BEND

P. 13/13

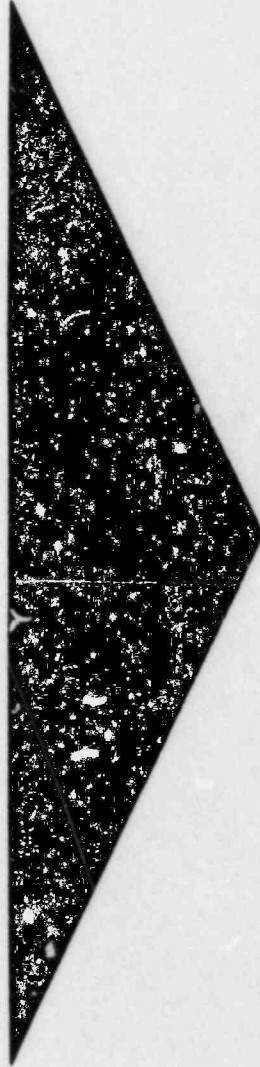
The gener. for shaft material was confirmed to be the same as that used at Shoreham and Comanche Reat (ASTM-A229-class D). ref. phone conversation between Craig Vogler, FAA and Bob Klassen of Portec. Actual shaft weight = 5760

The calculated values for bearing reactions and moments at the flywheel and rotor centerline was checked against those computed by the TDI Torsional Analysis. The comparison is given below

	Calc. Value	TDI Value
Generator bearing R ₂	17008 lbf	16807 lbf
Crankshaft bearing R ₁	18316 lbf	18314 lbf
Moment at Flywheel M ₁	305518 lb-in	273756 lb-in
Moment at Rotor E M ₂	782413 lb-in	730314 lb-in

The conservative factors of safety calculated for the generator shaft for static and fatigue failure indicate the shaft is acceptable for its intended use.

ITEM 2 TDI TORSIONAL ANALYSIS FOR RIVER BEND DIESEL
GENERATOR BY ROLAND YANG.



TORSIONAL AND LATERAL CRITICAL SPEED ANALYSIS

ENGINE NUMBERS 74039/42
 DELAVAL-ENTERPRISE ENGINE MODEL DSR-48
 3500 KW/4889 BHP AT 450 RPM

FOR

STONE & WEBSTER ENGINEERING CORP.
 GULF STATES UTILITIES

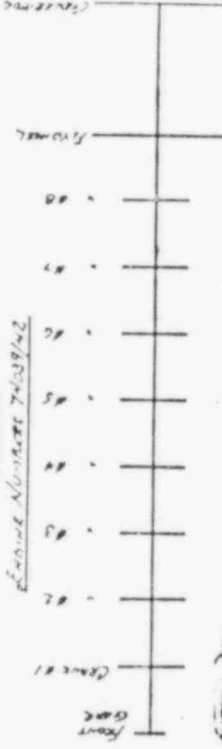


DELAVAL ENGINE & COMPRESSOR DIVISION
 155 - 85TH AVENUE
 OAKLAND, CALIFORNIA 94621

John David Johnson

By: Rolanc Yang
 March 5, 1975

Revision - May 4, 1977

STEELE PORTER UTILITIES COMPANYDE LAVAL ENTERPRISE NR N-B3500 E.S. (4689 SUP) @ 450 RPM225.6 RPM?Generator Data

Generator Crane
 Wallace Pump Drive
 Crane # 1/2
 Shaft

2842
 5310
 11920
 962

I = 6805 48 FT 26"

Crane No. 1

Crane
Shaft

1541.85
 41.81
 1583.66

I = 49222 48 FT 26"

Crane No. 2 (90)

Vertical
 Pin
 2 W. 101.
 Rotor Dr.
 Rotor Dr.

43130
 202170
 679.81
 209.09
 20625

I = 47922 48 FT 26"

Crane No. 8

Crane
Shaft

1641.85
 71.63

I = 30109 48 FT 26"

Generator Frame
 Vertical 229.148
 Generator Shaft Frame

455.08
 13.68
 400

I = 416587 48 FT 26"

Generator Drive

160100 48 FT 26"

I = 4976067 48 FT 26"

I = 187820 48 FT 26"

SIVM 15431801 05/04/77

2.8750000E+01

left reaction = -18314.
right reaction = -16807.

delta	dia	weight	inertia	shear	moment	slope	defl
0.	0.	0.	0.	18314.1	0.	0.000142	0.
3.812	13.000	143.2	1402.0	18170.9	69550.	0.000139	0.000538
1.250	13.000	47.0	1402.0	18124.0	92234.	0.000137	0.000710
5.587	14.000	247.8	1885.7	17876.2	194609.	0.000122	0.001451
4.500	24.000	576.1	16286.0	17300.1	273756.	0.000120	0.001997
0.	0.	3589.0	16286.0	13711.1	273756.	0.000120	0.001997
4.500	24.000	576.1	16286.0	13135.0	334160.	0.000117	0.002531
7.125	16.625	437.7	3749.9	12697.2	426187.	0.000093	0.003244
7.125	16.625	437.7	3749.9	12259.5	515095.	0.000087	0.003845
4.750	19.500	401.5	7097.5	11658.1	572375.	0.000051	0.004114
4.750	19.500	338.1	7097.5	11520.0	619131.	0.000040	0.004301
10.000	19.000	802.4	6397.1	10717.6	730319.	0.000005	0.004511
0.	0.	25000.0	6397.1	-14282.4	730319.	0.000005	0.004511
10.250	16.875	811.7	6230.4	-15094.0	579765.	-0.000031	0.004300
5.440	16.750	425.1	6067.0	-15519.1	496497.	-0.000047	0.004175
5.000	16.750	390.7	6067.0	-15409.8	417925.	-0.000067	0.004004
5.100	16.750	390.7	6067.0	-16300.5	337399.	-0.000070	0.003587
5.310	13.000	349.7	1402.0	-16650.2	184013.	-0.000128	0.002535
11.000	0.000	156.5	201.1	-16806.7	-0.	-0.000296	-0.001800

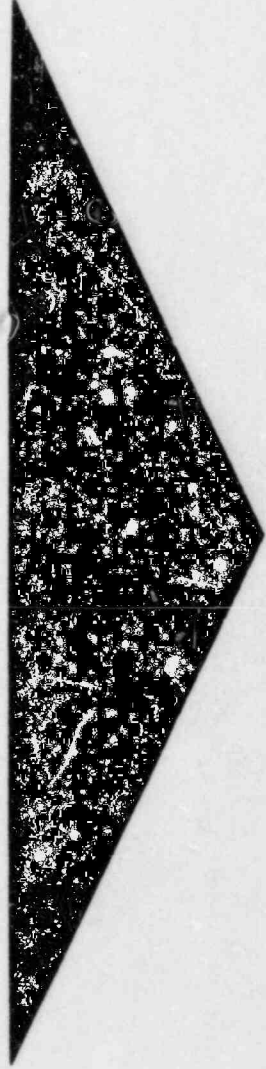
lateral frequency by rayleigh's method = 2880.

PROGRAM STOP AT 1088

USED 11.63 0.115

ITEM 3

TORQUE EXCURSIONS BETWEEN THE FLYWHEEL TO GENERATOR
AND GENERATOR TO GRID FOR RIVER BEND.



MEMORANDUM

TO: Craig Vogler
FROM: Lisa Shustock
DATE: November 7, 1984
RE: TORQUE EXCURSIONS BETWEEN THE FLYWHEEL TO GENERATOR AND GENERATOR TO GRID ON REMAINING CRANKSHAFTS IN DR/OR PROGRAM

The available data on torque excursions between the Flywheel and generator and the generator and grid for the remaining plants in the DR/OR program are listed in Table I.

If you have any questions, feel free to call me.

LMS/gg

TABLE I

Plant	Torque Values Between Flywheel & Generator (ft-lbs)		Torque Values Between Generator & Grid (ft-lbs)		QA
	maximum	minimum	maximum	minimum	
River Bend	2.166 E5	-1.088 E5	5.588 E4	5.345 E4	SP84-6-10(g)
Rancho Seco	1.840 E5	-7.434 E4	5.625 E4	5.290 E4	SP84-6-10(h)
Vogtle	2.558 E5	-3.530 E4	1.096 E5	1.096 E5	*
Perry	2.620 E5	-2.971 E4	1.105 E5	1.088 E5	*
WNP-1	ANALYSIS TO BE PERFORMED AT A LATER DATE				
Bellafonte	ANALYSIS TO BE PERFORMED AT A LATER DATE				

*QA not complete. To be supplied in appropriate DR Support Package

ITEM 4 TELEPHONE MEMORANDUM: CRAIG VOGLER, FaAA AND
BOB KLASHEM, FORTEC.



P. 1/1

J.O. No. _____

IDI OWNER'S GROUP

TELEPHONE MEMORANDUM

CALL DATE 11-27-74 TIME 2:32 AM/PM INCOMING _____ OUTGOING _____

BETWEEN Craig Kaylor OF UTILITY Failure Analysis Associates
AND Bob Klashorn OF Portec

SUBJECT: Material specifications for T-4 Belle-Gard and 650 Pire-Bond

DESCRIPTION:

for S.O. 1751057 - Belle-Gard Material; ASTM A662 class D
weight - shaft: 7422 lbs

rotor windings 3700 lbs
for S.O. 1740842 - Pire-Bond Material ASTM A662 class D
weight - shaft: 5260 lbs

rotor windings: 28000 lb

ACTION: unbalanced magnetic pull (UMP) = 14,000 lbs

FOLLOW UP: _____

ITEM 5 TELEPHONE MEMORANDUM: CRAIG VOGLER, FaAA AND
WALTER MEACHAM, FaAA.



P. 1/1

TO: OWNER'S GROUP

J.O. No. _____

TELEPHONE MEMORANDUM

CALL DATE 11-19-54 TIME 11:10 AM/PM INCOMING _____ OUTGOING _____

BETWEEN Craig Vester OF FAA - Charlotte

AND Walter Measaban OF FAA, Dixon x office

SUBJECT: 8" diameter sterail bearing

DESCRIPTION: The 8" sterail bearing has the following
dimensions:

Vertical: 2.210-8.018

Horizontal: 8.018-6.022

Length: 16.464

ACTION: _____

FOLLOW UP: _____

ITEM 6 ASTM A-668 CLASS D MATERIAL SPECIFICATION.





Designation: A 668 - 72

American National Standard A 668 - 72
Approved Sept. 18, 1972
By American National Standards Institute

Standard Specification for STEEL FORGINGS, CARBON AND ALLOY, FOR GENERAL INDUSTRIAL USE¹

This Standard is issued under the fixed designation A 668; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval.

1. Scope

1.1 This specification covers untreated and heat-treated carbon and alloy steel forgings for general industrial use. Other ASTM specifications for forgings are available for specific applications such as pressure vessels, railroad use, turbine generators, gearing, and others involving special temperature requirements.

1.2 Six classes of carbon steel and seven classes of alloy steel forgings are listed in Table 1, which indicates their required heat treatments, as well as mechanical properties.

1.3 Supplementary requirements of an optional nature are provided. These shall apply only when specified by the purchaser.

1.4 The appendix lists the grades corresponding to the various grades of the superseded ASTM Specifications A 235, A 237, and A 243.

Note—The values stated in U. S. customary units are to be regarded as the standard.

2. Applicable Documents

2.1 ASTM Standards

A 275, Methods for Magnetic Particle Examination of Steel Forgings

A 312, Methods for Macroetch Testing and Inspection of Steel Forgings

A 370, Methods and Definitions for Mechanical Testing of Steel Products²

A 388, Recommended Practices for Ultrasonic Examination of Heavy Steel Forgings

A 509, Definition of a Steel Forging

E 30, Chemical Analysis of Steel, Cast Iron, Open-Hearth Iron, and Wrought Iron

F 44, Definitions of Terms Relating to Heat

Treatment of Metals

3. Descriptions of Terms

3.1 *a ring-shaped or a disk-shaped forging*—forging whose length, as measured on its longitudinal axis, is less than its diameter or main transverse dimension is considered a ring or disk within the meaning of this specification.

3.2 *a ring-shaped forging*—forging whose length, as measured on its longitudinal axis, is more than its diameter shall be considered as a hollow cylinder within the scope of this specification if it has been lengthened by extrusion or forged in a manner similar to that of a ring, namely, expanded in diameter on a mandrel.

4. Basis of Purchase

4.1 When this specification is to be applied to an inquiry, contract, or order, the purchaser shall furnish the following information:

4.1.1 The class of forging desired as listed in Table 1.

4.1.2 The options which may be selected as found in 5.4.2, 6.1.2, 7.3, and 13.1, and

4.1.3 Applicable supplementary requirements.

5. Manufacture

5.1 *Melting Process*—The steel shall be made by the open-hearth, basic-oxygen, or

¹This specification is under the jurisdiction of ASTM Committee A 1 on Steel, Stainless Steel and Related Alloys, and is the direct responsibility of Subcommittee A01.06 on Steel Forgings and Bolts.

²Current edition approved Sept. 29, 1972. Published January 1973.

³Annual Book of ASTM Standards, Part 7.

⁴Annual Book of ASTM Standards, Parts 1, 2, 3, 4, 5, and 10.

⁵Annual Book of ASTM Standards, Part 12.

⁶Annual Book of ASTM Standards, Parts 2 and 10.



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electrolytic process.

6.1.1.1 *Castings*.—Sufficient allowance shall be made from each ingot to secure freedom from piping and undue segregation.

6.1.1.2 *Forging Process*.—The forgings shall receive their hot mechanical work under a hammer, or in a ring rolling mill, each of ample power to work the metal uniformly throughout its section. The finishing shall be brought as close as practicable to finished shape and size by hot mechanical work.

6.1.1.3 *After forging and before reheat for heat treatment*, the forgings shall be allowed to accomplish transformation.

6.1.1.4 *Heat Treatment*.—

6.1.1.4.1 All forgings other than Class A shall be heat treated as shown in Table 3.

6.1.1.4.2 Where options exist within a class, the choice of heat treatment shall be left to the discretion of the manufacturer, unless the purchaser specifies one of the available options.

6. Chemical Requirements

6.1 *Chemical Composition*.—

6.1.1 The steel shall conform to the requirements for chemical composition prescribed in Table 1.

6.1.2 The choice of chemical composition is left to the discretion of the manufacturer, unless otherwise specified by the purchaser.

6.1.3 *Heat Analysis*.—

6.1.3.1 An analysis of each heat shall be made by the manufacturer. When possible, the test sample shall be taken during the pouring of the heat. If the test sample is lost or declared inadequate for chemical determinations, the manufacturer may take alternative samples from locations near the surface of an ingot or bloom, as necessary to establish the analysis.

6.1.3.2 In the case of large ingots poured from two or more heats, the weighted average of the chemical determinations of the several heats shall conform to the requirements specified in Table 1 or by agreement (see 6.1.2).

6.1.3.3 *Product Analysis*.—An analysis may be made by the purchaser from a forging representing each heat, or multiple heat if made in accordance with 6.1.2. Samples for analysis may be taken from the forging, or from a

full size, prolongation at any point from the middle to the outside diameter in the case of disk or solid forgings, or midway between the inner and outer surfaces of hollow forgings or rings or from a test specimen. The chemical composition thus determined shall not vary from the requirements specified in Table 1 or applied upon case 6.1.2 by more than the amount prescribed in Table 2.

7. Mechanical Requirements

7.1 *Tensile Requirements*.—

7.1.1 The material shall conform to the tensile properties prescribed in Table 3.

7.1.2 Tensile specimens shall be machined to the form and dimensions of Fig. 5 of Specification A 370 and shall be tested in accordance with the first part of Specification A 370.

7.1.3 *Size Classification* (see Table 1).

7.1.3.1 *Solid Forgings*.—The nominal or specified rough machined diameter or thickness of solid forgings, disregarding large ends, collars, flanges, and joints, shall determine the size classification. Where there are several sections of equal length but of different diameters, the largest diameter shall apply.

7.1.3.2 *Ring or Hollow Cylinder Forging*.—The size classification shall be determined by its nominal or specified rough machined thickness or width, whichever is the smaller dimension. The thickness shall be measured by the difference between the outside and inside radii. The width shall be measured parallel to the axis of the ring or hollow cylinder.

7.1.4 *Number of Tests*.—Unless the purchaser specifies that forgings shall be furnished in accordance with the requirements of 7.3, the number of tension tests performed shall be as follows:

7.1.4.1 For all classes of heat-treated forgings with rough machined weights less than 5000 lb (2270 kg) each, one test shall be made from each size classification represented in each heat or from each annealing or normalizing charge or from each size classification in each heat in each normalizing or quenching charge represented in each tempering charge. For untreated forging, (Class V weighing less than

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5000 lb each, one test from each heat shall be made.

7.14.2 On all classes, for forgings with rough machined weights of 5000 lb or more, at least one test from each forging shall be made.

7.14.3 On all classes, for forgings with rough machined weights of 7000 lb (3180 kg) or more, two tests will be taken, on ring and disk forgings 180 deg apart, on shafts and long hollow cylinders, one from each end and offset 180 deg.

7.14.4 When forgings are made in multiple as a single forging, that is, forged as one piece and divided after heat treatment, the multiple forging shall be considered as one forging, and the number of tests required shall be as designated in 7.14.1, 7.14.2, and 7.14.3.

7.1.5 Prolongations

7.1.5.1 A sufficient number of the forgings shall have prolongations for extracting specimens for testing. Locations of test specimens for various types of forgings shall be as shown in Fig. 1.

7.1.5.2 The nominal or principal outside rough machine diameter or thickness of the forgings, disregarding large ends, collars, flanges, and journals shall determine the size of the prolongations for test specimens, however, the prolongations on annealed, normalized, or normalized and tempered shafts may be extensions of the small diameter end of the shaft, as shown in Fig. 1.

7.1.5.3 For quenched forgings in Classes E, J, K, L, M, and N, the prolongations shall be sufficiently long so that the center of the gage length (for longitudinal specimens) or axis (for tangential specimens) of the tension test specimen shall be at the following locations:

7.1.5.4 On solid shafts, bars, rotors, or billets (see Fig. 1(a)), at midradius and from the end, $3\frac{1}{2}$ in (89 mm) or $\frac{1}{2}$ the diameter or thickness, whichever is less.

7.1.5.5 On hollow forgings (see Fig. 1(b)), at midwall and from the end, $3\frac{1}{2}$ in, or $\frac{1}{2}$ the wall thickness, whichever is less.

7.1.5.6 On disk forgings (see Fig. 1(c)) (with prolongation on OD), at midthickness and from the OD $3\frac{1}{2}$ in, or $\frac{1}{2}$ the thickness, whichever is less.

7.1.5.7 On disk forgings (see Fig. 1(d)) (with

prolongation on the width or thickness) $3\frac{1}{2}$ in, or $\frac{1}{2}$ the thickness, whichever is less, from any heat-treated surface.

7.1.5.8 On ring forgings (see Fig. 1(d)) (with prolongation on width), at midwall and from the ring face $3\frac{1}{2}$ in, or $\frac{1}{2}$ the wall thickness, whichever is less.

7.1.5.9 On ring forgings (see Fig. 1(d)) (with prolongation on the OD), at midwidth and from the OD $3\frac{1}{2}$ in, or $\frac{1}{2}$ the width, whichever is less.

7.1.5.10 In place of prolongations, the manufacturer may elect to submit an extra forging(s) to represent each test lot, in this event, the representative forging must be made from the same heat of steel, have received the same reduction and type of hot working, be of the same nominal thickness, and have been heat treated in the same furnace charge as the forging(s) it represents.

7.1.6 Tests for acceptance shall be made after final heat treatment of the forgings.

7.1.7 Test specimens shall be parallel to the axis of the forging in the direction in which the metal is most drawn out except that rings, hollow forgings which are expanded, and disks shall be tested in the tangential direction.

7.1.8 Yield point shall be determined on carbon steel Grades A through F, and yield strength on alloy steel Grades G through N. For carbon steel grades not showing a yield point, the yield strength at 0.2 percent offset shall be reported.

7.2 Hardness Tests—Brinell hardness tests shall be taken on each forging (for exception, see 7.1.4.4), regardless of weight or class, after final heat treatment and rough machining.

7.2.1 The average value of the hardness readings on each forging shall fall within the hardness ranges specified in Table 3. The permissible variation in hardness in any forging shall not exceed 30 HB for Classes A through E, 40 HB for Classes F through J, 50 HB for Classes K through N.

7.2.2 At least two hardness tests shall be taken on each flat face of disks and rings approximately at midradius and 180 deg apart, for example, at the 3:00 and 9:00 positions on one face, and 6:00 and 12:00 positions on the opposite face. On solid forgings, at least four

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tests shall be taken on the profiles of the forging, two at each end 180 deg apart.

7.3 If so specified by the purchaser forgings may be supplied on the basis of hardness tests alone. If this option is exercised the class shall be identified with the letter "H" that is "AH", "BH", "CH", etc.

8. Retests

8.1 If the mechanical test results of any test do not conform to the requirements specified because of flaw development in the test specimen during testing, a retest shall be allowed if the defect is not caused by ruptures, cracks, or folds in the steel.

9. Reheat treatment

9.1 When heat treated forgings are specified and the mechanical test results of any test do not conform to the requirements specified, the manufacturer may retreat the part, but not more than three times, and retests shall be made in accordance with 7.2. The retest properties shall conform to the requirements for the class of forgings ordered (Class A).

9.2 When untreated forgings (Class A) are specified, and the mechanical test results of any test do not conform to the requirements specified, the manufacturer may anneal, normalize, or normalize and temper, one or more times, but not more than three times, and retests shall be made in accordance with 7.2. The retest properties shall conform to the requirements for the class of forgings ordered (Class A).

10. Dimensions and Tolerances

10.1 The forgings shall conform to the dimensions and tolerances specified on the purchaser's drawing or order.

11. Finish and Appearance

11.1 The forgings shall conform to the finish specified on the purchaser's drawing or shall otherwise have a good workmanlike appearance.

12. Marking

12.1 Each forging shall be legibly stamped

by the manufacturer with the manufacturer's name or trademark, the manufacturer's serial number, the specification identification number followed by the appropriate class number and where applicable, an AISI Grade designation.

12.2 The type of stamps to be used shall be round, oval, or interrupted and the stamping having a minimum radius of 10 (0.75) mm.

13. Inspection

13.1 The manufacturer shall attend the purchaser's inspector, all reasonable facilities necessary to satisfy him that the material is being furnished in accordance with the specification. Still in position by the purchaser shall not interfere unnecessarily with the manufacturer's operations. All test and inspection, except position analysis, shall be made at the place of manufacture, unless otherwise agreed to.

14. Certification and Reports

14.1 The mill shall furnish test reports to the purchaser with the following information:

14.1.1 Chemical analysis.

14.1.2 Heat treatment.

14.1.3 Results of tests for mechanical properties or hardness, or both, and

14.1.4 The results of any required supplementary tests.

15. Rejection

15.1 Any forging having obvious defects observed prior to or subsequent to acceptance at the manufacturer's plant shall be subject to rejection.

15.2 Samples tested by the purchaser in accordance with 6.3 that represent rejected material shall be preserved for 60 days from the date of the rejection report. In case of dissatisfaction with the results of the tests, the manufacturer may make claim for reworking within that time.

SUPPLEMENTARY REQUIREMENTS

One or more of the following supplementary requirements shall apply only when specified by the purchaser in the inquiry, contract, and order. Details of these supplementary requirements shall be agreed upon by the manufacturer and the purchaser.

S1. Chemical Composition

S1.1 The supplier shall obtain approval of the grade of steel he proposes to apply to the order and reach agreement with the purchaser on the ranges of each element specified in the composition.

S2. Special Forging Techniques

S2.1 Special Forging Techniques are required to produce metal flow during the hot working operation in the direction most favorable for resisting the stresses encountered in service. Verification of forging flow lines shall be by macro-etch testing of sample forgings in accordance with Method A 311.

S3. Rough Turning and Boring

S3.1 The position of any rough turning or boring in the sequence of manufacturing operations.

S4. Carbon Content for Welding

S4.1 For forgings intended for welding, the carbon content (product analysis) shall be limited to 0.35 max percent.

S5. Bend Tests

S5.1 The test specimen shall withstand bending at room temperature through 180 deg F without cracking on the outside of the bend portion of an inside diameter of 1" (25.4 mm).

S6. Magnetic Particle Test

S6.1 Forgings shall be magnetic particle tested in accordance with the latest issue of Methods A 275.

S7. Ultrasonic Test

S7.1 Forgings shall be ultrasonically tested in accordance with the latest issue of Recommended Practice A 598.

S8. Vacuum Treatment

S8.1 Vacuum deoxidized steel shall be supplied.

S9. Tensile Requirements

S9.1 When sizes larger than permitted in Table 1 are required, ductility values may be reduced from the specified values.

S10. Heat Treatment

S10.1 A minimum tempering temperature shall be specified.

S11. Additional Tests

S11.1 Tests in addition to those prescribed in Section 7 may be specified.

S12. Additional Marking

S12.1 Additional identification marking at the locations of the stamping or both may be specified.

TABLE 1. Chemical Requirements

Elements	Composition max percent	
	Class A Material	Class B Material
C	0.25 to 0.35	0.25 to 0.35
Manganese	0.030	0.040
Phosphorus	0.008	0.010
Sulfur	0.008	0.010



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TABLE I. Permissible Variations in Product Analysis.
 Permissible Variations Over the
 Maximum Allowable Minimum
 Limit Based on the Maximum
 Weight of Element (%)

Elements	Coke		Over the Maximum Allowable Minimum Weight (%)
	Maximum Weight (%)	Minimum Weight (%)	
Carbon	99.02	99.00	0.02
Hydrogen	9.00	8.98	0.02
Phosphorus	0.010	0.008	0.002
Sulfur	0.010	0.008	0.002
Nickel	0.010	0.008	0.002
Chromium	0.010	0.008	0.002
Vanadium	0.010	0.008	0.002
Iron	0.010	0.008	0.002

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TABLE 3. Trade Requirements

Class	Net, at home		Trade, Net		Trade, Net per MP	Value From Foreign per MP		Imports from 2 most developed countries	Imports from 2 most developed countries
	Value	Net MP	Value	Net MP		Value	Net MP		
A. All of the world	20,000	20,000	20,000	20,000	1.0	0.0	0.0	0	0
B. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
C. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
D. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
E. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
F. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
G. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
H. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
I. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
J. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
K. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
L. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
M. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
N. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
O. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
P. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
Q. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
R. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
S. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
T. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
U. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
V. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
W. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
X. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
Y. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0
Z. All of the world, except for normalised and temporary	12,000	12,000	12,000	12,000	1.0	0.0	0.0	0	0

TABLE 3 (continued)

Class	No. of counts		Inside Strength		Yield Point		Elongation		Reduction of Area at Max. Hardness
	Over	Under	psi	MPa	psi	MPa	mm/mm	%	
M (B)H (normalised, quenched, and tempered)	7.1778	7.1778	100 000	700	90 000	580	25	50	17.500
	09/27/84	09/27/84	100 000	700	70 000	515	18	50	20.500
F (7)H (normalised, quenched, and tempered)	4.1025	7.1778	970 000	700	100 000	700	16	50	25.271
	7.1778	09/27/84	100 000	700	100 000	675	16	45	23.807
M (M)H (normalised, quenched, and tempered)	4.1025	4.1025	140 000	1000	120 000	625	15	45	29.157
	7.1778	09/27/84	100 000	600	110 000	700	14	40	28.541
N (M)H (normalised, quenched, and tempered)	4.1025	7.1778	160 000	1100	110 000	750	15	40	30.151
	7.1778	09/27/84	100 000	1100	100 000	700	15	30	33.400
			100 000	1100	100 000	600	11	35	31.468

Units: MPa (continued)

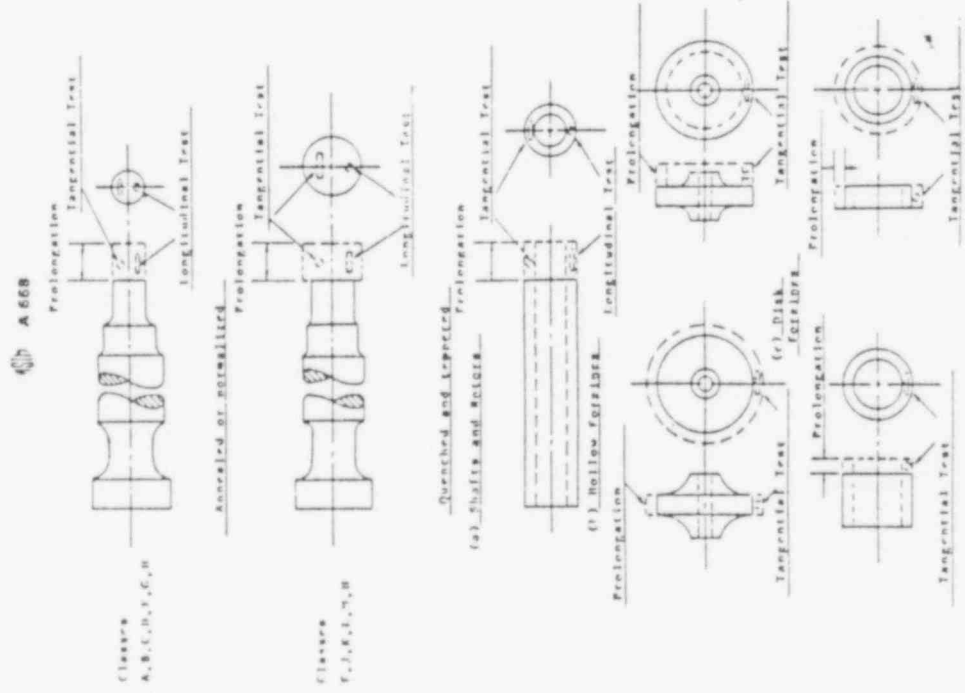


FIG. 1 Location of Test Specimens for Various Types of Forgings

1

[Faint, illegible text, possibly bleed-through from the reverse side of the page. The text is arranged in several lines and appears to be a list or a set of instructions.]

