

January 22, 1985

Attachment to Letter from D. C. Hintz to W. S. Little

Supplement to  
Kewaunee's 1984 ILRT Report  
Originally Submitted  
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Introduction

This report presents the 'as-found' containment leakage rate calculation for the Kewaunee Nuclear Plant Containment at the end of Cycle IX. Type C leakage, greater than the capacity of the local leak rate tester, was identified through a containment penetration with redundant isolation valves in series. The 'as-found' integrated leakage rate is determined by combining the directly measured containment leakage with a conservative measure of (pre-post) repair differential leakage. The combination of the directly measured 1984 integrated leakage rate and the (pre-post) repair differential leakage could not be quantified. This is considered a failure of the 1984 Type A test.

As stated in 10 CFR 50, Appendix J, V.B.3, upon failure of a Type A test the following points shall be covered in a summary report:

- An analysis and interpretation of the test data
- The least squares fit analysis of the test data
- The instrumentation error analysis
- The structural conditions of the containment or components, if any, which contributed to the failure in meeting the acceptance criteria
- Results and analyses of the supplemental verification test employed to demonstrate the validity of the leakage rate test measurements shall also be included.

Section I of this report contains the 'as-found' leakage rate calculation and sections II through VI discuss the five (5) points required by 10 CFR 50, Appendix J, V.B.3.

I. 'As Found' Containment Leak Rate

Type B and C leakage tests were performed during the 1984 Refueling Outage prior to the Type A test. This order of testing is consistent with KNPP Technical Specifications and exemptions granted to WPSC from Appendix J provided a conservative measure of (pre-post) repair differential leakage is added to the Type A results.

When Type C leakage repairs are made prior to and during the same outage as a Type A test, (pre-post) repair differential leakage added to the Type A test will include improvements in the penetration's overall ability to isolate containment; e.g.,

(1) Penetration with 2 testable isolation valves in series:

Before repair: Valve 1 leaks 8 SCFH

Valve 2 leaks 6 SCFH

After repair: Valve 1 leaks 2 SCFH

Valve 2 leaks 1 SCFH

'Repaired leakage': 5 SCFH

(2) Penetration with 2 testable isolation valves in series:

Before repair: Valve 1 leaks 8 SCFH

Valve 2 leaks 6 SCFH

After repair: Valve 1 leaks 2 SCFH

Valve 2 leaks 5 SCFH

'Repaired leakage': 4 SCFH

Penetration geometries other than those with 2 testable isolation valves in series will be evaluated on a case-by-case basis using appropriate conservatism. Type B leakage repaired prior to and during the same outage as a Type A test will also be evaluated on a case-by-case basis using appropriate conservatism.

1984

As-Found Integrated Leakage Rate Determination

Kewaunee Nuclear Power Plant

Table 1 Leakage Repaired in 1984 Prior to the Type A Test

<u>Penetration Repaired</u>	<u>Initial Leakage</u>	<u>Final Leakage</u>	<u>Repaired Leakage</u>
12	0.088SCFH	0.053SCFH	0.035SCFH/1.54 x 10 <sup>-5</sup> wt%/day
11 <sup>1</sup>	>20SCFH	0.068SCFH	>20SCFH/>8.77 x 10 <sup>-3</sup> wt%/day

$$\begin{array}{l} \text{As Found} \\ \text{Integrated} \\ \text{Leakage Rate} \end{array} = \begin{array}{l} \text{Leakage Rate} \\ \text{Determined} \\ \text{With Type A Test} \end{array} + \begin{array}{l} \text{Type B\&C Leakage Repaired} \\ \text{Prior to Type A Test} \end{array}$$

$$\text{As Found Integrated Leakage Rate} = 0.0162 \text{ wt\%/day} + 1.54 \times 10^{-5} \text{ wt\%/day} + >8.77 \times 10^{-3} \text{ wt\%/day}$$

$$= >0.0250 \text{ wt\%/day}$$

Note that the 'as-found' leakage rate is indeterminate. This resulted from the leakage through redundant isolation valves at penetration #11 exceeding the capability of the measuring device.

<sup>1</sup>See LER 305-84-006

Since the 'as-found' 1984 Type A test results are not quantified it cannot be positively said that the test passed, nor can it be positively concluded that the test was a failure. Conservatively, the 'as-found' 1984 Type A test is considered a failure.

## II. Analysis and Interpretation of the Test Data

The 1984 ILRT test data were analyzed using the Mass Point Method (ANSI 56.8-1981). A summary of the data reduction method can be found in Appendix B of Kewaunee's 1984 ILRT Report (reference 1). The raw data and intermediate calculation results are in Appendix D of the same report.

The calculated leakage rate, 0.0162 wt%/day (at 95% UCL), demonstrates the leak tightness of Kewaunee's Containment for Cycle X.

## III. Least Squares Fit Analysis of the Test Data

A least squares analysis was performed with the following as the independent and dependent variables, respectively:

$$\left( \begin{array}{l} \text{Change in time} \\ \text{measured from } t=0 \end{array} , \begin{array}{l} \text{Weight fraction of containment} \\ \text{atmosphere remaining up to and} \\ \text{including data set } i \end{array} \right)$$

The slope of the curve is the containment leakage rate in weight fraction per hour and the y intercept is the weight fraction in containment at time zero.

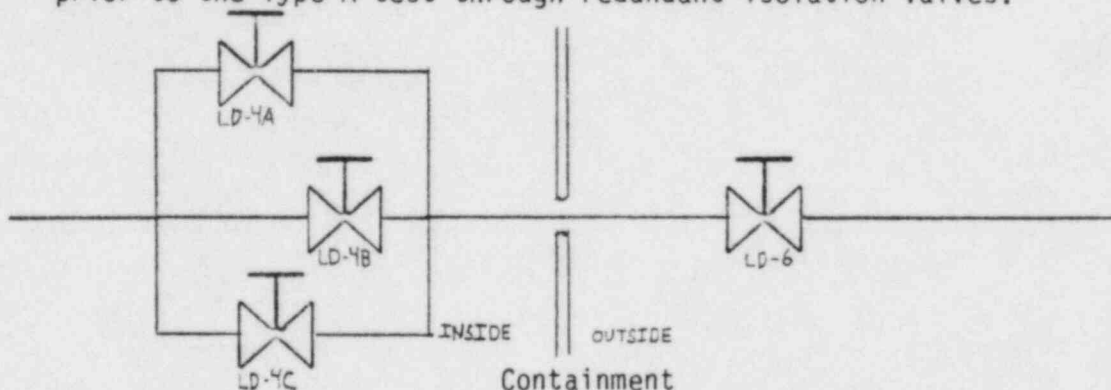
This calculation was performed via computer; the data and results are found in the 1984 Kewaunee ILRT report, Appendix D.

#### IV. Instrumentation Error Analysis

A figure of merit analysis for the instruments used in the 1984 ILRT is presented in Appendix B of the 1984 Kewaunee ILRT report (reference 1). The analysis is consistent with ANSI 56.8-1981, Appendix G. The instruments were determined to be suitable for their intended use.

#### V. Conditions Which Contributed to Failure of the Type A Test

Kewaunee's 1984 'as-found' Type A test was considered a failure since Type C leakage greater than the capacity of the local leak rate tester was identified prior to the Type A test through redundant isolation valves.<sup>1</sup>



The leakage was repaired by replacing the seat ring gaskets in valves LD-4A and LD-4B and adjusting the stroke on LD-6. Note that LD-4A is in parallel with LD-4B which together are in series with LD-6. These repairs resulted in reducing the Type C leakage through penetration #11 from >20SCFH to 0.068 SCFH.

#### VI. Results and Analyses of Supplemental Verification Test Employed to Demonstrate the Validity of the Leakage Rate Test Measurement

The condition which caused the Type A test failure was corrected prior to performance of the Type A tests, i.e., B and C tests were performed prior to the A

<sup>1</sup>See LER 305-84-006

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test. Therefore, the relevant supplemental test is the same supplemental verification test that illustrated acceptable results of Kewaunee's 1984 Type A test. The supplemental test was successful and is described in section I.1 of Kewaunee's 1984 Type A test report (reference 1).