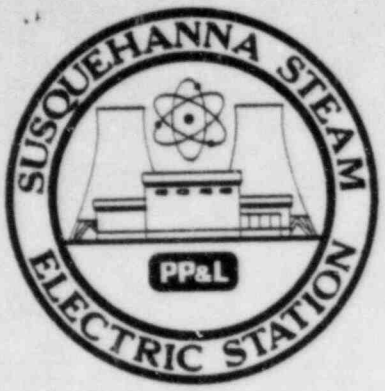

AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-387
UNIT One
DATE October 5, 1984
COMPLETED BY L.A. Kuczynski
TELEPHONE (717)542-3759

MONTH September, 1984

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1	1033	17	1025
2	1009	18	1010
3	1023	19	1038
4	1032	20	1031
5	1039	21	1022
6	1042	22	614
7	1043	23	734
8	1035	24	963
9	902	25	1011
10	1033	26	1030
11	1028	27	1043
12	941	28	1044
13	1029	29	714
14	1028	30	760
15	712	31	-
16	782		

INSTRUCTIONS

On this format, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

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IE24
1/1

OPERATING DATA REPORT

DOCKET NO. 50-387
DATE October 5, 1984
COMPLETED BY L.A. Kuczynski
TELEPHONE (717)542-3759

OPERATING STATUS

Unit 1

1. Unit Name: Susquehanna Steam Electric Station
2. Reporting Period: September, 1984
3. Licensed Thermal Power (MWt): 3,293
4. Nameplate Rating (Gross MWe): 1,152
5. Design Electrical Rating (Net MWe): 1,065
6. Maximum Dependable Capacity (Gross MWe): 1,068
7. Maximum Dependable Capacity (Net MWe): 1,032
8. If Changes Occur in Capacity Ratings (Items Number 3 Through 7) Since Last Report, Give Reasons:
   None

Notes

9. Power Level To Which Restricted, If Any (Net MWe): None
10. Reasons For Restrictions, If Any: None

	This Month	Yr.-to-Date	Cumulative
11. Hours In Reporting Period	720	6,575	1:,544
12. Number Of Hours Reactor Was Critical	720	4,613.5	8,458.8
13. Reactor Reserve Shutdown Hours	0	249.1	405.8
14. Hours Generator On-Line	720	4,488.9	8,257.2
15. Unit Reserve Shutdown Hours	0	0	0
16. Gross Thermal Energy Generated (MWH)	2,206,860	13,674,000	24,935,661
17. Gross Electrical Energy Generated (MWH)	716,120	4,453,730	8,120,280
18. Net Electrical Energy Generated (MWH)	689,988	4,288,825	7,825,198
19. Unit Service Factor	100	68.3	71.5
20. Unit Availability Factor	100	68.3	71.5
21. Unit Capacity Factor (Using MDC Net)	92.9	63.2	65.7
22. Unit Capacity Factor (Using DER Net)	90	61.2	63.6
23. Unit Forced Outage Rate	0	15.4	13.8

24. Shutdowns Scheduled Over Next 6 Months (Type, Date, and Duration of Each):
    Refueling Outage; February 9, 1985; 15 weeks.

25. If Shut Down At End Of Report Period, Estimated Date of Startup: N/A

26. Units In Test Status (Prior to Commercial Operation):

	Forecast	Achieved
INITIAL CRITICALITY		
INITIAL ELECTRICITY		
COMMERCIAL OPERATION		

UNIT SHUTDOWNS AND POWER REDUCTIONS

REPORT MONTH September, 1984

DOCKET NO. 50-387
UNIT NAME One
DATE October 5, 1984
COMPLETED BY L.A. Kuczynski
TELEPHONE (717)542-3759

No.	Date	Type[1]	Duration (Hours)	Reason[2]	Method of Shutting Down Reactor[3]	Licensee Event Report #	System Code[4]	Component Code[5]	Cause & Corrective Action to Prevent Recurrence
11	840915	S	0	H	5	NA	RC	FUELXX	Scheduled power reduction to optimize fuel use until refueling outage.
12	840922	S	0	H	5	NA	RC	FUELXX	Scheduled power reduction to optimize fuel use until refueling outage. Replacement of reactor recirculation pump motor-generator set brushes was also accomplished.
13	840929	S	0	H	5	NA	RC	FUELXX	Scheduled power reduction to optimize fuel use until refueling outage.

1
F: Forced
S: Scheduled

2
Reason:
A-Equipment Failure (Explain)
B-Maintenance or Test
C-Refueling
D-Regulatory Restriction
E-Operator Training & License Examination
F-Administrative
G-Operational Error (Explain)
H-Other (Explain)

3
Method:
1-Manual
2-Manual Scram.
3-Automatic Scram.
4-Continuation from previous month
5-Reduction
9-Other

4
Exhibit G - Instructions for Preparation of Data Entry Sheets for Licensee Event Report (LER) File (NUREG-0161)

5
Exhibit I - Same Source

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UNIT 1
SUSQUEHANNA STEAM ELECTRIC STATION

Docket Number 50-387 Date October 5, 1984
Completed by L.A. Kuczynski Telephone (717)542-3759

Challenges to Main Steam Safety Relief Valves

None

Changes to the Offsite Dose Calculation Manual

See Attachment.

Major Changes to Radioactive Waste Treatment Systems

None.

ATTACHMENT TO UNIT ONE

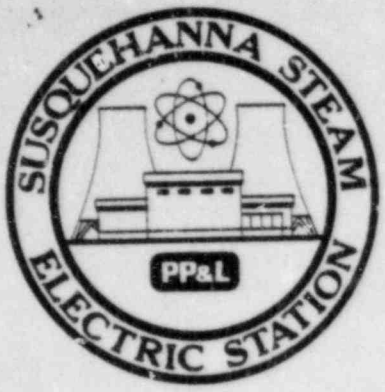
September, 1984, Monthly Operating Report

Charges to the Offsite Dose Calculation Manual

These revised pages were made effective July 9, 1984, upon signature by the Manager-Nuclear Support.

Changes have been denoted by revision bars in the right margin.

The changes were made to incorporate a new setpoint calculation methodology for vent monitors, based on actual (or expected) effluent isotope mixes.



AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-388
UNIT Two
DATE October 5, 1984
COMPLETED BY L.A. Kuczynski
TELEPHONE (717)542-3759

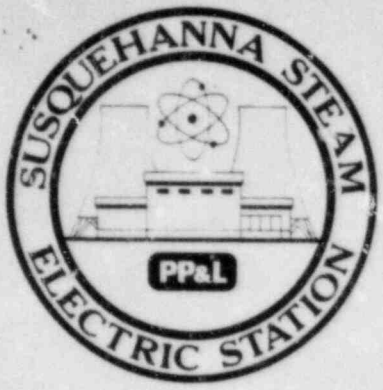
MONTH September, 1984

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1	0	17	714
2	0	18	729
3	0	19	689
4	189	20	564
5	371	21	0
6	399	22	129
7	414	23	502
8	50	24	583
9	321	25	705
10	630	26	771
11	733	27	987
12	720	28	1002
13	571	29	1014
14	580	30	39
15	721	31	-
16	710		

INSTRUCTIONS

On this format, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

(9/77)



OPERATING DATA REPORT

DOCKET NO. 50-388
DATE October 5, 1984
COMPLETED BY L.A. Kuczynski
TELEPHONE (717)542-3759

OPERATING STATUS

Unit 2

1. Unit Name: Susquehanna Steam Electric Station
2. Reporting Period: September, 1984
3. Licensed Thermal Power (MWt): 3,293
4. Nameplate Rating (Gross MWe): 1,152
5. Design Electrical Rating (Net MWe): 1,065
6. Maximum Dependable Capacity (Gross MWe): *
7. Maximum Dependable Capacity (Net MWe): *
8. If Changes Occur in Capacity Ratings (Items Number 3 Through 7) Since Last Report, Give Reasons:
   None

Notes

* To be determined.

9. Power Level To Which Restricted, If Any (Net MWe): None
10. Reasons For Restrictions, If Any: None

	This Month	Yr.-to-Date	Cumulative
11. Hours In Reporting Period	720	2,147	2,147
12. Number Of Hours Reactor Was Critical	612.8	1,653.4	1,653.4
13. Reactor Reserve Shutdown Hours	152.6	495	495
14. Hours Generator On-Line	567.4	1,333.7	1,333.7
15. Unit Reserve Shutdown Hours	0	142.4	142.4
16. Gross Thermal Energy Generated (MWH)	1,182,556	2,127,542	2,127,542
17. Gross Electrical Energy Generated (MWH)	374,820	629,070	629,070
18. Net Electrical Energy Generated (MWH)	356,012	587,463	587,463
19. Unit Service Factor	NA	NA	NA
20. Unit Availability Factor	NA	NA	NA
21. Unit Capacity Factor (Using MDC Net)	NA	NA	NA
22. Unit Capacity Factor (Using DER Net)	NA	NA	NA
23. Unit Forced Outage Rate	NA	NA	NA

24. Shutdowns Scheduled Over Next 6 Months (Type, Date, and Duration of Each):
    Pre-Commercial, October 27, 1984, 10 weeks.

25. If Shut Down At End Of Report Period, Estimated Date of Startup: October 2, 1984
26. Units In Test Status (Prior to Commercial Operation):

	Forecast	Achieved
INITIAL CRITICALITY	05/09/84	05/08/84
INITIAL ELECTRICITY	06/28/84	07/03/84
COMMERCIAL OPERATION	12/31/84	

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SUSQUEHANNA STEAM ELECTRIC STATION
PP&L

UNIT SHUTDOWNS AND POWER REDUCTIONS

REPORT MONTH September, 1984

DOCKET NO. 50-388
UNIT NAME Two
DATE October 5, 1984
COMPLETED BY L.A. Kuczynski
TELEPHONE (717)542-3759

No.	Date	Type[1]	Duration (Hours)	Reason[2]	Method of Shutting Down Reactor[3]	Licensee Event Report #	System Code[4]	Component Code[5]	Cause & Corrective Action to Prevent Recurrence
*9	840828	F	72.2	A	4	84-017	HA	VALVEX	Reactor scram following turbine trip on moisture separator drain tank high level. Cause for high level was malfunctioning drain valve on piping from high pressure turbine exhaust to moisture separator.
10	840908	F	20.4	A	3	84-018	HA	INSTRU	Reactor scrammed as a result of a turbine control valve fast closure signal (See attached page)
11	840913	F	0	B	5	N/A	CB	INSTRU	Power reduction for reactor recirculation system troubleshooting.
12	840920	S	37.3	B	3	N/A	ZZ	ZZZZZZ	Reactor scram occurred as part of scheduled startup testing.
13	840930	F	22.7	H	3	84-021	**	**	Reactor scram due to turbine trip on high moisture separator drain tank (See attached page)

*Renumbered per NRC direction.
**Undetermined at this time.

1
F: Forced
S: Scheduled

2
Reason:
A-Equipment Failure (Explain)
B-Maintenance or Test
C-Refueling
D-Regulatory Restriction
E-Operator Training & License Examination
F-Administrative
G-Operational Error (Explain)
H-Other (Explain)

3
Method:
1-Manual
2-Manual Scram.
3-Automatic Scram.
4-Continuation from previous month
5-Reduction
9-Other

4
Exhibit G - Instructions for Preparation of Data Entry Sheets for Licensee Event Report (LER) File (NUREG-0161)

5
Exhibit I - Same Source

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UNIT 2 SHUTDOWNS AND POWER REDUCTIONS (continued):

No. 10

generated from a false power-load unbalance signal during performance of a surveillance. The unit responded per design throughout the transient. The pressure transmitter which provided the false input was recalibrated and a procedure change was made to alert operations personnel of impending turbine trip if the circumstances develop again. The procedure also provides action to be taken to prevent the turbine trip.

No. 13

level. Evaluation of cause(s) and action(s) to prevent recurrence still being determined.

UNIT 2
SUSQUEHANNA STEAM ELECTRIC STATION

Docket Number 50-388 Date October 5, 1984
Completed by L.A. Kuczynski Telephone (717)542-3759

Challenges to Main Steam Safety Relief Valves

None.

PENNSYLVANIA POWER & LIGHT COMPANY
SUSQUEHANNA STEAM ELECTRIC STATION
OFFSITE DOSE CALCULATION MANUAL

Prepared By J.E. Widmer Date 6/27/84

Reviewed By K.E. Shank Date 6/28/84

PORC Review Required Yes ( ) No (✓) Date

Approved By [signature] Date 7/9/84
Manager-Nuclear Support

CONTROLLED

TABLE OF CONTENTS

JUL 09 1984

CONTROLLED

LIST OF TABLES

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1. All exposure pathways of significance at the critical receptor locations;

2. Dose contributions to critical receptors from multiple release points; and

3. Dose contributions from major radioisotopes expected to be present in gaseous effluents.

The general methodology for establishing plant ventilation gaseous effluent monitor setpoints is based upon vent release rates derived from site-specific meteorological dispersion conditions, vent flow rates, and measured or expected radioisotopic mixtures in the gaseous effluents. The vent release rates can then be converted to vent concentrations for input as setpoints for the applicable detectors. Since the vent monitors are programmed to calculate concentrations of iodine-131 and particulate being released based on the rate of accumulation of activity on the filters, setpoints can be established for the iodine and particulate channels.

The following method is used for calculating vent monitor high radiation alarm setpoints:

1. An isotopic mixture is selected for the detector in question, if applicable. Noble gas and particulate detector setpoints are based on actual isotopic mixtures obtained from vent sample analysis or the FSAR/FES expected release mixtures if actual samples do not contain sufficient detectable activity to accurately estimate the mixtures. The assumed isotopic mixtures are periodically reviewed to verify that they remain representative of plant effluents.

2. The selected noble gas or particulate mixture is used in the GASPAR program run to calculate the associated doses. The total source term (total curies used for the calculation) does not matter as long as the proper nuclides are present in the relative proportions indicated in sample analysis data or FSAR/FES tables.

   For the iodine-131 setpoint, any release total for I-131 can be entered. The highest calculated annual average relative concentrations (χ/Qs) at the site boundary are used for these GASPAR calculations.

3. The following ratio concept is used to calculate a release rate limit for the assumed mixture (or I-131):

$$\frac{\text{Calculated Dose (mrem)}}{\text{Total GASPAR Source Term (Ci)}} = \frac{\text{Dose Rate Limit (mrem/yr)}}{\text{Limiting Release Rate (Ci/yr)}}$$

   The limiting release rate of the assumed mixture (or I-131) can therefore be calculated:

$$\text{Limiting Release (Ci/yr)} = \frac{\text{(Total GASPAR Source Term, Ci) (Dose Rate Limit, mrem/yr)}}{\text{(Calculated Dose, mrem)}}$$

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For the noble gas setpoint, the calculated whole body and skin dose rates via the plume pathway are subject to the 10CFR20-derived limits of 500 and 3000 mrem/yr, respectively. The whole body dose rate limit is usually most restrictive. For particulates and for iodine-131, the maximum calculated organ dose via the inhalation pathway is subject to the limit of 1500 mrem/yr.

4. The limiting release rates are converted to limiting vent concentrations using high limit vent flow rates.

Limiting Vent Concentration, uCi/cc =

$$\frac{\text{(Limiting Release Rate, Ci/yr) (10E6uCi/Ci)}}{\text{(5.26E5 min/yr) (Vent High Limit Flow Rate, cc/min)}}$$

Sample calculations of liquid and gaseous effluent monitor setpoints are presented in Appendix A.

Vent flow rates and sample flow rates are monitored and recorded for each of the five SSES release points. The measured flow rates are used to calculate vent concentrations and release rates. Flow channel setpoints are set at 10% and 90% of the calibrated sensor ranges to provide indication of possibly abnormal flow rates.

SPECIFICATION 3.11.2.6 - THE CONCENTRATION OF HYDROGEN OR OXYGEN IN THE MAIN CONDENSER OFFGAS TREATMENT SYSTEM SHALL BE LIMITED TO LESS THAN OR EQUAL TO 4% BY VOLUME.

Hydrogen recombiners are used at SSES to maintain the relative concentration of components of potertially explosive gas mixtures outside the explosive envelope. The main condenser offgas treatment system explosive gas monitoring system (offgas hydrogen analyzers) have setpoints of 1% hydrogen to alarm and 2% hydrogen to isolate.

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TABLE 2

DOSE FACTORS FOR NOBLE GASES AND DAUGHTERS[a]

Radionuclide	Whole Body Dose Factor K_i (mrem/yr per µCi/m^3)	Skin Dose Factor L_i (mrem/yr per µCi/m^3)	Gamma Air Dose Factor M_i (mrad/yr per µCi/m^3)	Beta Air Dose Factor N_i (mrad/yr per µCi/m^3)
Kr-83m	7.56E-02[b]	---	1.93E+01	2.88E+02
Kr-85m	1.17E+03	1.46E+03	1.23E+03	1.97E+03
Kr-85	1.61E+01	1.34E+03	1.72E+01	1.95E+03
Kr-87	5.92E+03	9.73E+03	6.17E+03	2.03E+04
Kr-88	1.47E+04	2.37E+03	1.52E+04	2.93E+03
Kr-89	1.66E+04	1.01E+04	1.73E+04	1.06E+04
Kr-90	1.56E+04	7.29E+03	1.63E+04	7.83E+03
Xe-131m	9.15E+01	4.76E+02	1.56E+02	1.11E+03
Xe-133m	2.51E+02	9.94E+02	3.27E+02	1.48E+03
Xe-133	2.94E+02	3.06E+02	3.53E+02	1.05E+03
Xe-135m	3.12E+03	7.11E+02	3.36E+03	7.39E+02
Xe-135	1.81E+03	1.86E+03	1.92E+03	2.46E+03
Xe-137	1.42E+03	1.22E+04	1.51E+03	1.27E+04
Xe-138	8.83E+03	4.13E+03	9.21E+03	4.75E+03
Ar-41	8.84E+03	2.69E+03	9.30E+03	3.28E+03

[a] The listed dose factors are for radionuclides that may be detected in gaseous effluents and derived from Table B-1 in Reg. Guide 1.109.

[b] 7.56E-02 = 7.56 x 10^{-2}.

$$\frac{5000 + f}{f} = \frac{10 \cdot (1E-5)}{1E-7}$$

$f = 5$ gpm

For an identified mixture with an actual MPC of 7.22E-7 µCi/ml and the same activity, blowdown flow and X and Y values as above, the LRW discharge monitor setpoint value and LRW discharge flow setpoint become:

Setpoint concentration (c) = 3E-5 µCi/ml

Setpoint value = 2.3E3 cpm + Background

LRW discharge flow setpoint (f) = 36 gpm

A.1.2 Gaseous Effluent Monitors

A.1.2.1 Noble Gas Monitor

To determine the release rate limit for noble gases, an isotopic mixture representative of plant effluents is selected. For example, the following mixture from Table 4.4 of the SSES Final Environmental Statement (FES) can be used:

Argon-41	25	Ci/yr per reactor
Krypton-83m	4	
Krypton-85m	1,700	
Krypton-85	270	
Krypton-87	32	
Krypton-88	660	
Xenon-131m	71	
Xenon-133m	14	
Xenon-133	12,500	
Xenon-135m	220	
Xenon-135	590	
Xenon-138	290	
Total	16,376	Ci/yr per reactor

The above annual release quantities are entered into GASPAR with the following annual average dispersion estimates (Reference: 1982 SSES Meteorology Report):

Relative Concentration	4.1E-5 sec/m^3
Decayed Relative Concentration	4.1E-5 sec/m^3
Decayed Depleted Relative Concentration	3.8E-5 sec/m^3
Deposition Rate	4.2E-8 m^{-2}

This set of annual average meteorological parameters is the most conservative over the period 1973-1982.

The total body dose via the plume pathway which results is 18.3 mrem. Equation 5 of the ODCM is then used to calculate the limiting release rate from each of the five plant release points:

Limiting Release Rate =

$$\frac{(32{,}752\ \text{Ci})\ \ (500\ \text{mrem/yr})}{(36.6\ \text{mrem})\ \ (5\ \text{vents})} = 8.95\text{E}4\ \text{Ci/yr per vent}$$

This limiting release rate is then converted to limiting (setpoint) concentrations using Equation 6 of the ODCM and high limit vent flow rates.

Sample High Limit Vent Flow Rates:

Unit 1 Reactor Building Vent	4.75E9 cc/min
Unit 2 Reactor Building Vent	4.75E9 cc/min
Standby Gas Treatment System Vent	5.04E8 cc/min
Unit 1 Turbine Building Vent	8.63E9 cc/min
Unit 2 Turbine Building Vent	6.50E9 cc/min

Limiting Vent Concentration =

$$\frac{(8.95E4\ Ci/yr/vent)\ \ (1E6\ uCi/Ci)}{(5.26E5\ min/yr)\ \ (4.75E9\ cc/min)} = 3.58E\text{-}5\ uCi/cc$$

for Reactor Buildings 1&2

Substituting the other vent flow rates into Equation 6 as above, the following noble gas high radiation setpoint concentrations are calculated for the remaining vents:

Standby Gas Treatment System	3.37E-4 uCi/cc
Unit 1 Turbine Building	1.97E-5 uCi/cc
Unit 2 Turbine Building	2.62E-5 uCi/cc

A.1.2.2 Iodine-131 Monitor

When the FES expected annual release quantity for I-131 (2.40E-1 curies) is entered into GASPAR with the dispersion estimates of A.1.2.1, the maximum calculated organ dose via the inhalation pathway is 4.88 mrem to the child thyroid. Using Equation 5 of the ODCM, the limiting I-131 release rate is calculated as follows:

Limiting Release Rate =

$$\frac{(.24\ Ci)\ \ (1500\ mrem/yr)}{(4.88\ mrem)\ \ (5\ vents)} = 1.48E1\ Ci/yr/vent$$

Using Equation 6 of the ODCM, the limiting (setpoint) I-131 concentrations can be calculated for each of the five plant vents.

JUL 09 1984

Limiting Vent Concentration =

$$\frac{(14.8\ \text{Ci/yr/vent})\ (1E6\ \text{uCi/Ci})}{(5.26E5\ \text{min/yr})\ (4.75E9\ \text{cc/min})} = 5.92E\text{-}9\ \text{uCi/cc}$$

for Reactor Buildings 1&2

Substituting the other vent flow rates into Equation 6 of the ODCM above, the high radiation setpoints for the remaining plant vents are calculated to be the following:

Standby Gas Treatment System	5.58E-8 uCi/cc
Unit 1 Turbine Building	3.26E-9 uCi/cc
Unit 2 Turbine Building	4.33E-9 uCi/cc

A.1.2.3 Particulate Monitor

Following are the SSES Final Environmental Statement (FES) expected annual release quantities for particulate radionuclides:

Cr-51	1.2E-4 Ci/yr per reactor
Mn-54	3.6E-4
Fe-59	1.6E-4
Co-58	5.8E-5
Co-60	1.1E-3
Zn-65	5.5E-5
Sr-89	1.8E-5
Sr-90	3.1E-6
Zr-95	8.7E-6
Sb-124	5.1E-6
Cs-134	1.3E-4

Cs-136	1.3E-3
Cs-137	2.1E-4
Ba-140	4.2E-5
Ce-141	2.9E-5
Total	3.6E-3 Ci/yr per reactor

When the above annual release quantities are entered into GASPAR with the annual average dispersion estimates of A.1.2.1, the maximum calculated organ dose via the inhalation pathway is 1.33E-2 mrem to the teen lung. Using Equation 5 of the ODCM, the limiting release rate of particulates can be calculated:

Limiting Release Rate =

$$\frac{(7.2E\text{-}3\ Ci)\ (1500\ mrem/yr)}{(2.66E\text{-}2\ mrem)\ (5\ vents)} = 8.12E1\ Ci/yr/vent$$

Using Equation 6 of the ODCM, the limiting (setpoint) particulate concentrations can be calculated for each of the five plant vents.

Limiting Vent Concentration =

$$\frac{(81.2\ Ci/yr/vent)\ \ (1E6\ uCi/Ci)}{(5.26E5\ min/yr)\ \ (4.75E9\ cc/min)} = 3.25E\text{-}8\ uCi/cc$$ for Reactor Buildings 1&2

When the vent flow rates for the remaining five plant vents are substituted into Equation 6 as above, the following high radiation setpoint concentrations result.

Standby Gas Treatment System	3.06E-7 uCi/cc
Unit 1 Turbine Building	1.79E-8 uCi/cc
Unit 2 Turbine Building	2.38E-8 uCi/cc

JUL 09 1984

PP&L Pennsylvania Power & Light Company
Two North Ninth Street • Allentown, PA 18101 • 215 / 770-5151

Bruce D. Kenyon
Vice President-Nuclear Operations
215/770-7502

OCT 09 1984

Director, Data Automation &
Management Information Division
Attention: Mr. M. R. Beebe
Management Information Branch
Office of Resource Management
U.S. Nuclear Regulatory Commission
Washington, D.C. 20555

SUSQUEHANNA STEAM ELECTRIC STATION
MONTHLY OPERATING REPORTS
ER 100450 FILE 841
PLA-2330

Docket Nos. 50-387/NPF-14
50-388/NPF-22

Dear Mr. Beebe:

The September 1984 monthly operating reports for Susquehanna SES Units 1 and 2 are attached.

Very truly yours,

B. D. Kenyon
Vice President-Nuclear Operations

Attachment

cc: Dr. Thomas E. Murley
Regional Administrator-Region I
U.S. Nuclear Regulatory Commission
631 Park Avenue
King of Prussia, PA 19406

Director
Office of Inspection and Enforcement
U.S. Nuclear Regulatory Commission
Washington, D.C. 20555
Attn: Document Control Desk (12 copies)

Mr. R. H. Jacobs - NRC
Mr. R. L. Perch - NRC

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Department of Environmental
Resources
Bureau of Radiation Protection
P.O. Box 2063
Harrisburg, PA 17120

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