UNITED STATES OF AMERICA NUCLEAR REGULATORY COMMISSION

BEFORE THE ATOMIC SAFETY AND LICENSING BOARD

In the Matter of	
TEXAS UTILITIES ELECTRIC) Docket Nos. 50-445 and 50-446
COMPANY, et al.)) (Application for
(Comanche Peak Steam Electric Station, Units 1 and 2)) Operating Licenses)

AFFIDAVIT OF JOHN C. FINNERAN, JR. REGARDING INFORMATION RELATED TO CINCHING DOWN OF U-BOLTS

I, John C. Finneran, Jr., being first duly sworn, hereby depose and state as follows:

I am the Pipe Support Engineer for the Pipe Support
Engineering Group at Comanche Peak Steam Electric Station. In
this position, I oversee the design work of all pipe design
organizations for Comanche Peak. I have previously provided
testimony in this proceeding. A statement of my professional and
educational qualifications was received into evidence as
Applicants Exhibit 142B.

The purpose of this Affidavit is to respond to the Board's request that Applicants provide the "raw data" concerning the torquing of U-bolts referred to in Table 2 to "Affidavit of Robert C. Iotti and John C. Finneran, Jr. Regarding Cinching Down of U-Bolts" attached to Applicants' Motion for Summary

Disposition of CASE's Allegations Regarding Cinching Down of U-Bolts (June 29, 1984). October 24, 1984 Board Memorandum (Raw Data on U-Bolts). Specifically, the Board requested the following four items:

- (1) the raw data,
- (2) the procedure by which the raw data was collected,
- (3) the criteria for selecting the sample, and
- (4) raw data on readings excluded from the sample.

 The Board stated that the data provided (average torque value of the two nuts on each U-bolt) did not allow the Board to "examine the variance of readings on individual bolts [nuts]." October 24

Memorandum at 1.

Attached hereto are the raw data of t'e actual field inspections requested by the Board. I would note that the average torque on the two nuts of each U-bolt was reported since our intent was to determine torque that would establish a preload on the U-bolt and the pipe in the test, where an equal torque would be applied to both legs. The purpose of collecting this data was to provide us an indication of what torque values may be expected in the field in order to reasonably set some parameters for the U-bolt testing program discussed in Applicants' Motion for Summary Disposition on this issue.

The field inspections during which the data were collected were conducted by 3 PSE engineers. While no formal procedures for the inspection were written, the three engineers were given verbal instructions as to what they were to do. The instructions were to measure and record the torque of both nuts on any cinched

down U-bolts that could be found in Unit 2¹ that were unpainted.

(If a U-bolt had been painted, the torque reading would have been affected.) In that torquing practice on safety and non-safety systems was the same, U-bolts on safety as well as non-safety systems were checked. The engineers were told to check torque by tightening the nut and when movement was noted to record the reading on the torque wrench. Calibrated torque wrenches were used. Each leg of the U-bolt was checked where accessible. In addition, the engineers were told to record the size of the pipe (though in a few instances this was overlooked).

The attached raw data contains numerous comments made after the raw data were collected. In that the Board requested the "raw data," we have not attempted to clean it up to make it more understandable. It should be noted that where a support had two U-bolts, the readings for both are noted. Further, where one of the nuts on a U-bolt was not accessible, it was indicated by an N/A or other such reading. Further, in some cases the supports were not included in the sample size for one of several reasons. For the Board, I have listed the reasons below and noted in the margin of the raw data the corresponding reason number for not including the data.

These supports were not included because at the time we summarized the data, we did not know the pipe sizes, i.e., it

In that Unit 1 had already been painted, the only possible source of torque data reflecting true field conditions was Unit 2. The U-bolt configurations employed in Unit 2 are the same as those in Unit 1 and the construction process for torquing U-bolts had remained unchanged for Units 1 and 2. Accordingly, this decision would have had no impact on the adequacy of the data for the purpose needed, as stated above.

was not listed by the engineer and because the summation process was done under time constraints for filing, we did not take the time to go back and check the size at that time. Subsequently, we have checked the sizes and they are all three inch pipe.

- Same as item 1, except the size was 16 inch pipe.
- Same as item 1, except the size was 12 inch pipe.
- 4. Same as item 1, except it was a nonsafety related pipe and we did not go back to check the pipe size.
- 5. The engineer deleted this support because the U-bolt was not cinched, and no reading should have been taken.
- 6. The engineer apparently wrote down the wrong hanger numbers (i.e., no such numbers existed). Accordingly, the numbers could not be verified and thus the support was not included.
- 7. This support was a deadweight 32 inch pipe support in the turbine building. We felt that the deadweight might effect the reading. (It should be noted that no 32 inch pipe supports were included.)
- 8. When this support drawing was initially examined, no U-bolt was listed.
 Accordingly, we thought that the engineer had made a mistake and we did not include it. Subsequently, in again reviewing the support for this filing, we found that the support had been modified and the documentation now reflects a U-bolt.
- 9. This support was the only 1 1/2 inch pipe inspected and it was felt that the concern was not focused on such small bore pipe supports, thus the reading was not entered.
- This support was inadvertently not included.

John C. Finneran, Jr.

STATE OF TEXAS COUNTY OF SOMERVELL

Subscribed and sworn to before me this 9th day of November, 1984.

Notary Public Biel J. Hooges
my Commission Expines MARCH 28, 1988

		TORQUE		
_	HANGER *	BOLT #1	BOLT # 2	
1. 0	5-2-012-412-5425 ?	20	20	
1. 05	2. 012.411 - 542K" 4	52	32	
1. 6	5-2.014.418-5025°"	30	25	
1. 0	2-014-419- SAZKOK	20	30	
4. 4	0-548-288-562	12	11	
5. H	16-549-1-DO	0	-0	
1. 0	0-2-098- 406-546 R	20	17 8	
		17	20 %	
2. 4	7-2-021-404-532R 44 22-013-413-532K	30	46	
B	7-2-018-415-543R 443	48	52 /	
BI	2-2-018-417-543R 442 2-2-018-417-543K	30	36 \$	
3. 78	2-004-402-502KOK	59	59 \$	
	2-2-326-010-55GR 60	25	24/VB	
C5	-5 326-401-556ROK	22	22/0	
	5-2318-700-55312016	15		
SS	2:014; 401-552KCK3'65>	25	25 g	
1 <9	5-2-920-703-553R 3/5	20	IV/A	
	10.548-1289 1'4 05	6	5	
	T-2-021-405 -532 K 4'6	44	45/	
	- 2- 226 - 428 - 536R 43	40	30	
A.	-2-011-403 5221 10t	20	27.	
	2.0 276 - 414 ok but fratis-nut	25	20/21	

- TE - LAKED GLOSS &

un tema de	TORQUE		
HANGER NO.	BOLT #1	BOIT #2	
Ces-2-063-416-52212 84	20	15	
CET-2-012-410-522K 104	35	40/	
25.2.063-417- SZZK 84	41 40 50 75 56 50	30 /	
31.2.037.402. SIZE 8"¢	40	45 .	
24.2.056.401- 5 ZZRK 8.4	50	60 /	
27-7- 283-418-536K 100	75	90/	
2+-2-083-417-536KONO"A	56	58	
2-2-068-407-533 E 180	50	65 /	
2-2-068-402-5335 184	30	40	
PP-2-226-439-526R 07"0	16	27 V9:005	
P-2-226-407-526R6K4"4	40	40 /	
2-2-044-431-522ROK4	30	261	
7-2-017-440-53612 1004	35	27 (R. S.A.	
PCH-2-028-403-5328884	10	20 2 11	

John D. Sampon 1-21-84

EIRE PHOTECTION 125 Z'.o'(5) 12.55 3'-0'(5)13 5 3'-0'(N)135 4'-0'(S) 145	50 45 20.	65 35 15
Z'-0'(5) 12.55 3'-0'(5)13 5 3'-0'(N)135 4'-0'(S) 145	45 20 15	35
3-0'(5)13 5 3-0'(N)135 4'0'(S) 145	20	15
3-0"(N)135 4'0(s) 145	15	
4'0(s) 14s		30
	30	32
1-0(3)113	75	30
105	8	0
1:0"(N)9.55	28	28 .
6"\$ < 5. PIPE 790 HALLWAY	48	55
FIRE PROTECTION 8:0'(5) 9.35	40	45 /
3'075> 9.35	25.	25
1-075) 9.35	2.5	40
(14)	15	30
6.0(5)105	45	25
6-0"(5)115	70	25

. John D. Sampson 1-21-84

<u> </u>	303 0150	
HANGER NO.	TORK	QUE_
DCT-2-013-714-532K 16:2 DCT-2-013-418-533R 16:1 DSI-2-076-404-522K 16:4 DCC-2-031-406-543K 18:4 DCC-2-159-407-553R 12:4	0K 25 0K 25 0K 110	110 85 50 25 V 8 125 87

John D. Sangson 1-28.84

	TO	EQUE
HGR. NO.	801 =1	BOLT # 2
2-193-424-C5Z12 40	43	35
6. a. 2 - 200 - 402 - C 5312 84	27	30 RGare
CE 2- 193 - 423 - C5212 9"1	10	20
HD-551-RB-2 71 74	70	15 1
HD- 551 23.2 70/ 23	10	30 %
8-2-246-419-653R3.6"+	10	10/
Q-2-246-423-C5312'6"0	10	10 /
Mg. 2-151-442-C52KOK4' \$	12	15 RG
P15-2-151-419. C521 04.6	42	32 RC 1
115-2-151-440-CSZIC 4"0	25	361 0
90-2-046-404-C56R 34	9	9 RG
6. CE-2-296-403-653R 64	20	25 577 16
115-2-151-411-CSZR . 4.4	5	101
CC-2-201-420-C53R 3"\$	27	Z5 RG
27-2-053-402-C625 7.3.4.	25	68 Redias
31.2-306-425-C42K OK 9 b	30	21 BG
\$ -2-087-406-CAZR 83	35	45
2p. 2-00 - 416 - C46 R OK 3"0	22	22 RG
Op. 2-001-426- c4612 ? 3'd	30	N/A
\$. 2 - 087 - 409 - CAZR OK 5 \$	60	80
51-2-306-423- C42K OF 9"6	70	50 RGZ
55-2-306 401 · CAZR 4" \$	35	35 RG V

		TORQUE			
HANGER NO.		BOLT # 1	BOLT #2		
52-2-087 - 405- C42R		60	50 /		
SI-2-306-421-C42R	4"4	25	20/86		
VD-2-053-403- C46R		10	15 / RG		
St. 2.306-402-C42ROK		30	25/		
51-2-306-418-C4Z Ra		50	50 Pod		
51-2-088-410-C42Kol	/ 11	32	60/12		
SI-2-010-903-C965 10		20	20 RG		
SI- Z- 095- 409 · CAZR 61	40"p.	40	50		
51-2-171- 401- CAZROL		55	50		
DD-2-109-433-643R OF	, 11	20	22869 RG		
57-2-101 -408-CAIR OK	- 11	84	65 / 18		
\$1-2-163. 903-CAZROK		75	300/ 3		
" " ok		70'	45 1		
WP-2-030 - 922- CAGK OK	- 11	25	35 PG		
8-2-019-411 - CAZKOK	30	20	30		
HO-827- 25K2	2"4	5	4		
	2"4	9	8		
HO-827-24 KZ	2"4	10	10		
	2,4	5	5		
140 - 827 - 27K2	2'4	5	5		
HD- 827- 76KZ	2"0	5	5 22		
140-827-29KZ	2"6	6	5		

HANGER NO.	7		BOIT # 2		
	7.4	BOLT #1	Bac	TAZ	
HD-507-107-	RB2	5	1 4		
148-507-1	14	5	5		
HD-507-121	2'4	5	6	,	
HD - 507 - 108 - 10	23-224	9	6		
110-507-105	2.4	4	5		
HD-507-109. R	B-Z 29	5	5		
· 40 - 507 - 2	344	5	5		
. 40.507-1	3/46	5	5		
HD-964-2	3/0 \$	10	7	1	
140-995-3-102	3/40	4	4	10 1	

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HG16 116.	100	カンデーナス
PRO-2- 115 - 430 C56, 15%	X45	35 /
John O. Sampson 1-28.84		

	TOR	QUE
HANGER NO.		BOXT # 2
7. 8,49-2-017-008-1545 52		
m5-2-033-001-T445 774	27	16 -
8.025-2-095-000 7445 26	No. 45	47/
9+0-2-318-404-T455 124 9+0-2-055-407-T455 10"6	OK-10	10/
6. 492 318. 408. T455 12" F.	15 NO 300H	18
6. CG 2 020 401 1950 20"4	40 Such	25
Ex-2-030-404-T455 12" \$		28
10. 00-2-010-402-7450 30"4	? 20	85
Ex-2-coz.401-T455 14% 50-2-032-403-745D 74%	7 25	35 /
25-2-098-402-7455 144		110 / 1
Pw. 2-001-408-725R 20"6		90
40-2-016-405.735R 30"	125	100
110-2-016-404-T35R 30"	77	92
HD-2.044-402-755 16" HD-2.045-405-7355 16"	125	125
HD-2-009-401 - 7355 (6"	95	55 /
TW-2-099-402- +350 14"	? 45	50 /
VD-2-071-402-7355 40"	55	67
VD-2-070-403- T350 40"	90	75
John D. Sampson 1.28.84	but did to	

John D. Sangson 1.28.84.

SUPPORT #	PIPE d	U-BOLT TYPE	TORQUE	ENLR.	DATE
:5-2-202-402-552R	3"	Pus-30 (1/2*4)	20-25 FT-16	TR	4/14/84
cc-2-190-401-	4 ф	pus-040 (%"4)	2 <u>7</u> 5 FF-16	TR	4/14/84
nes-2-150-450-	4 \$	P45-040 (1/2"\$)	625 FT-16	TR	4/14/84
4F-2-096-410-533K	4"\$	pus 040 (½"Ø)	30-35FT-LB ALL 4 NUTS >25 FT LB	JRM	5-2-94 4-27-94
F-2-103-441-553K	4"ø		JOFT-# 5-10FT-# 10-19FT-# 5-10FT-#	JRM	5-2-84
AF-2-099-419-533K	4"0	PUS-040 (V2* Ø)	15-30 ^{FT-4} 10-15 ^{FT-4} 25-30 ^{FT-4} 5-10 ^{FT-4}	ORM	5-7-84
cs-2-079-410-423	3"ø	pu3-030 (1/2° Ø)	10-15 ^{FT-#}	9RM	5-7-84
T-2-053-444-c624	3"\$	PUS-030 (1/2 0)	5-10 FT-# 5-10 FT-# 5-10 FT-# 10-15 FT-#	grm	5-8-84
I-2-306-425-C42K	4"0	PUS-040 1/2 0	35 FT-#	grm	5-10-84
AF-2-102-423-563S	4"0		23 ^{FT-#}	gam	5-10-84
SI-2-RB-049-709-1	11/20	PUH-015 5%" 0		98M	5-10-84
AF-2-102-422-853K	4"0	PUS-040 Y2" Ø	63FT-# 42FT-#	grm	5-10-84
		-			

9.

SUPPORT =	PIPE &	U-BOLT TYPE	TORQUE	ENGR.	ONTE
13H-2-6 8-402-42K		pun: 100		TK	5-24-84
RH-2-058-401-522R	10"	P45-100 (1/4"P)	55 FF-16 70 FF-16	TR	5-2.4-84
CC-2-028-412534	24"	pus-240 (1"0)	60 FT-16 65 FT-16 60 FT-16 70 FT-18	IR	5-24-84
C7-2-025-408-521K	16"	pus-160 (75" 0)	90 ET-15 90 ET-16 105 FT-16 55-FT-16	IR	5-2.4-84