

AN ASSESSMENT OF BOLTING INTEGRITY
AT PALO VERDE NUCLEAR GENERATING STATION
UNITS 1, 2 AND 3

Prepared for
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1.0 INTRODUCTION AND SUMMARY

1.1 Background

Threaded fasteners are utilized in widespread and varied applications in nuclear power plants. Fasteners are used in vessel internals applications, as pressure boundary closures and as structural fasteners in power plants. They are used in a variety of environments ranging from the high temperature, high pressure primary water nuclear environment to the ambient temperature industrial environment associated with auxiliary equipment remote from the nuclear reactor containment. The performance of fasteners used in nuclear power plants has been excellent, in general. However, the persistent nature of modest numbers of failures in recent years has prompted the industry to examine more closely the potential failure mechanisms associated with threaded fasteners and to provide recommendations regarding actions which may be undertaken to minimize failures. Because of concerns raised in this area, an assessment of bolting integrity at Palo Verde Nuclear Generating Station Units 1, 2 and 3 was performed, as documented in this report.

The problem of fastener failures in nuclear power plants is not a single issue but represents several distinct areas of concern. Issues which must be addressed include: (1) failures of fasteners used in vessel internals such as plenum, thermal shield and core barrel fasteners, (2) failures of primary pressure boundary fasteners due to boric acid wastage or stress corrosion cracking, (3) failures of structural fasteners resulting from stress corrosion cracking, and (4) failures of fasteners due to poor installation practices associated with improper lubrication or improper torquing.

The issue of fastener failures has received widespread attention by the industry, by vendors of fasteners and equipment, by the Electric Power Research Institute (EPRI) and by the Nuclear Regulatory Commission (NRC). Significant attention has been given to the fastener problem in nuclear plants since 1980, when, following the corrosion problems observed at the Fort Calhoun nuclear plant with pressure boundary closures, the NRC issued an Information Notice No. 80-27 on June 11, 1980, to all PWR owners regarding

the potential for boric acid corrosion wastage of pressure boundary bolts. The Institute for Nuclear Power Operations (INPO), following their independent studies of fastener failures issued a Significant Operating Experience Report (SOER-81-12) on June 24, 1981, re-emphasizing the need for careful inspection of all pressure boundary bolts because of the boric acid concerns. In 1982, following the observation of stress corrosion cracking in steam generator manway studs, the NRC issued another Information Notice (No. 82-06) on March 12, 1982, and later on June 2, 1982, the NRC issued an Inspection and Enforcement Bulletin (No. 82-02), regarding the boric acid wastage and stress corrosion cracking concerns associated with pressure boundary closures. Copies of Notice 82-06 and Bulletin 82-02 are attached as Appendix A to this report. Subsequent to the issue of the I&E Bulletin, the NRC identified the fastener failure issue as a generic safety issue affecting all light water reactor types and requiring significant action (Unresolved Safety Issue, B-29). These items illustrate that considerable attention is being directed toward pressure boundary closures, through regulatory channels.

The industry, vendors and EPRI have also been actively addressing the issue of fastener degradation in nuclear power plants. In addition to the SOER issued by INPO in 1981, EPRI has embarked upon research programs which address and scope the problems associated with fasteners for vessel internals as well as the primary pressure boundary cracking concerns. Westinghouse, Combustion Engineering and Babcock and Wilcox Owners Groups have supplemented the EPRI efforts by additional programs directed at resolving the material-environment degradation issues associated with fastener failures at nuclear power plants. The NRC funded a literature search performed by Lawrence Livermore National Laboratory which has identified thresholds for stress corrosion cracking of structural bolts in aqueous environments and in industrial environments.

As a result of the major research efforts underway to identify and eliminate sources of fastener degradation in nuclear power plant application, much is understood about the problem and mitigating actions are readily at hand to reduce or eliminate many of the concerns. For example, the stress corrosion failures of core internals fasteners has spawned research programs which

have resulted in development of better alloys or improved heat treatments which will reduce or eliminate materials susceptibility in this environment. In addition, recommendations have been made regarding materials or heat treatment changes, lubrication and sealant changes, and design modifications to reduce problems associated with boric acid wastage and stress corrosion cracking of pressure boundary and structural fasteners. Research programs are ongoing at EPRI and in utility owners groups to further define limits of applicability of fasteners and margins associated with the use of fasteners in critical component application.

The issue of overtorquing and of undertorquing has similarly received much attention in the nuclear power industry. As a result of structural fastener failures at Prairie Island, at Midland and at Palo Verde nuclear stations, failure analysis studies were undertaken to examine the causes of the failures, determine the extent of the problem and provide remedial actions to mitigate the phenomenon. Major sampling studies were performed at Midland and at Palo Verde on structural bolts. The Midland study consisted of hardness measurements of approximately 6000 structural bolts to determine the population of fasteners which had not met the requirements of the procurement material specification. The survey revealed that while only a small number of fasteners were overly hard (approximately 1%), many were overly soft. This observation illustrated why some fasteners fail immediately during torquing. The overly soft fasteners are overloaded, the overly hard fasteners fail by stress corrosion cracking (or hydrogen embrittlement). A significant study was also performed at Palo Verde examining pretorquing in critical structural fasteners used inside containment. The results of that study are examined in depth in this report and in part form the basis of the report findings.

As stated above, the problem of fastener failures is not a single issue but a combination of issues involving stress corrosion cracking; general corrosion and wastage, and installation concerns. The issues of stress corrosion cracking and general corrosion and wastage have been examined in depth in other studies and continue to be examined in owners groups and in EPRI sponsored programs. The installation concerns have been addressed in other programs and are the focus of this Palo Verde report.

The objective of this study was to examine the reliability of all structural fasteners at the Palo Verde Nuclear Generating Station for the three units under construction. However, due to access limitations and since the vessel internals fasteners are already quality checked within the ASME Section III, class NG component requirements, these fasteners were not included in this study. Likewise, the ASME Section III Class 1 pressure boundary fasteners are pressure leak checked and fall under the subsequent inspection requirements of the NRC Inspection and Enforcement Bulletin 82-02. Therefore, these fasteners were considered to be already checked (or will be checked) as to their structural reliability.

Consequently, the study performed for Palo Verde regarding bolting integrity focused on the structural fasteners used at the power plant. Because of the extensive programs already performed at Palo Verde examining the structural reliability of critical fasteners, this study was able to be performed as an independent review and verification study relying on the vast quantity of previously generated fastener reliability data to provide the data base necessary to this program. It was our observation that the Palo Verde Nuclear Power Station bolting integrity verification efforts performed by the utility and by its prime contractor (Bechtel) represents the most extensive study of its type performed to date for any nuclear power plant. Because of the extensive nature of those previous examinations of bolting integrity, all necessary information was at hand to perform this independent investigation.

By limiting this study to critical structural fasteners at Palo Verde, the specific objective of this study could be defined as a study of overtorquing or undertorquing associated with the installation of structural fasteners at the plant. Associated with these two major issues are the issues of double nutting (using the second nut to prevent loosening of the first nut), the use of acid cleaning with phosphoric or muriatic acid to remove corrosion products from the fasteners, and the use of lubricants in the installation of the fasteners.

Overtorquing of fasteners is generally not an operational concern (Ref. 1, 2 and 3). In fact, the American Institute of Steel Construction (AISC) has no requirement on the maximum preload of fasteners. The requirement is that the

minimum preload be 70% of the minimum specified ultimate tensile strength of the material used. The reason no maximum preload is specified is because a properly installed fastener never experiences a load as high as that experienced during installation. The reasons are as follows. First, the fastener load decreases approximately two to twenty percent (as shown in the calculations later in this report) upon release of the torque wrench or tensioner. Second, thread relaxation (or load redistribution) results in reduction of preload. Compression of the lubricant or dirt also reduces preload. Finally, stress relaxation (or creep) further reduces the preload on a fastener. Consequently, an overtorqued bolt will either fail mechanically by overload during installation or it will operate at a load significantly less than the preload during service. One exception occurs in the case of overly hard bolts. These fasteners can fail by delayed cracking due to stress corrosion or hydrogen embrittlement. In general, for fasteners such as SA-193 grade B7 a hardness of approximately Rc 38 is required before a fastener becomes significantly susceptible to stress corrosion cracking or hydrogen embrittlement, in room temperature moist air. Further, this environmentally assisted cracking usually occurs quickly within hours or days of the initial installation. Any additional potential for stress corrosion due to residue from acid cleaning of bolts would also fall in this category of early failure, if at all. Any retorquing or recheck will obviously uncover such failures.

As observed in the Midland bolting study (and confirmed in the Palo Verde studies to be discussed in this report), the problem of structural fastener strength is typically one of overly soft fasteners, not overly hard fasteners. Consequently, the stress corrosion cracking problem is practically non-existent. The great likelihood is that the fasteners will fail upon installation because of improper heat treatment (overly soft fasteners) or excessive torquing, and not from stress corrosion or hydrogen embrittlement. Therefore, the overtorquing issue of structural fasteners is self-controlling. If the fastener survives installation, and if it does not fail as result of stress corrosion cracking or hydrogen embrittlement, it will not fail as a result of overtorquing.

The problem of fastener undertorquing is a much more subtle phenomenon, difficult to detect and consequently of much greater threat to structural reliability of a component. Undertorquing can result from improperly calibrated equipment, dirty or rusted bolts, improper cleaning, improper lubrication or no lubrication used, improper threads, and human error, among other reasons. The principal result of such undertorquing is the potential reduction in the fatigue resistance and load-bearing capability of the fastener, as will be explained and investigated in this report.

Since the problem is difficult to detect and to eliminate, the major focus of this study was to investigate the likelihood of undertorquing in critical safety significant structural fasteners at Palo Verde and assess the impact of such undertorquing on design margins.

1.2 Summary

The objective of this study was to assess bolting integrity at Palo Verde, Units 1, 2 and 3. Emphasis was focused on structural steel bolting, since reactor coolant pressure boundary bolting, reactor internals bolting, and component support bolting must meet ASME Code Quality Assurance requirements and is also the object of ongoing NRC studies (Appendix A).

Critical structural steel bolting was evaluated with regard to overtorquing, undertorquing, and lubrication and nutting procedures. The results of bolt hardness measurements and torquing surveys previously made at Palo Verde formed an integral part of this evaluation. The study included an examination of Palo Verde, Unit 2 installed bolting and the torque wrench calibration room. Palo Verde Deficiency Evaluation Reports (DER's), specifications and procedures, Certified Material Test Reports (CMTRs) and NRC Construction Assessment Team (CAT) findings relating to bolting were also reviewed.

It was concluded that variation in bolt torque from specified values (American Institute of Steel Construction, AISC) was found in critical friction structural steel bolting during torque checks by Bechtel. This was especially true for Unit 2, where bolting was primarily installed by

calibrated torque wrenches, as compared to the "turn-of-the-nut" approach used at Unit 1 and air impact wrenches used at Unit 3. These deficiencies were corrected during the inspection. A review of other torque check studies on installed fasteners revealed that torque variations are not unusual, due to the major effects of bolt condition, lubrication, connection surface conditions, installation equipment and human error. Because of the difficulty of consistently relating bolt torque to preload, the ASME Code does not explicitly specify bolting preload and the AISC withdrew direct torque control in 1980 (Ref. 1).

The potential impact of these variations in preload, had they not been detected and corrected, was determined by assuming a range of torque/preload relationships (based on experience at Palo Verde) and computing preloads in the bolts. Calculated preloads were used to evaluate overtorquing and under torquing ramifications. Because the bolting hardness at Palo Verde is essentially below the threshold of Rockwell C41 (Ref. 1) for stress corrosion cracking (SCC), shown in Reference 12, overtorquing is not expected to be a problem in this respect. Any potential for SCC due to acid cleaning of bolts would also be mitigated by meeting this hardness threshold. The degree of overtorquing at Palo Verde led to the computed prediction of a certain number of bolt overload failures during torquing, which was indeed the experience. However, these failures are readily discovered and corrected during torquing. It was also computed that the bolt stresses during torquing are generally higher than in service, because of the shear stresses imparted by the torquing operation. In a properly designed joint the bolt stress at installation is the highest stress the bolt will experience and if the bolt does not fail then, and SCC is not a concern, then overtorque will not lead to failure during service (Ref. 1, 2 and 3). It is generally concluded (Ref. 1 and 2) that high preload is beneficial and reduces the excursion in bolt load due to cyclic external loads, as illustrated in this report. Thus, it is concluded that overtorquing is not a problem at Palo Verde.

The effect of undertorquing was evaluated with regard to multiple loose bolts in a connection, and such situations were compared to typical joint design loads and fatigue stress ranges supplied by Bechtel (Ref. 4). Unit 2 had a potential problem in this area had bolt torques not been checked and

corrected, due to a number of connections with multiple loose bolts (shown later in this report); thus prompting a more thorough evaluation of joint design margins. It was found that the typical structural steel joints and equipment anchor bolts were conservatively oversized by Bechtel, especially with regard to fatigue vibrations. For the designs studied, the design margins are generally about 1.5 for joint reaction loads (allowable AISC/actual), indicating that approximately 1/3 of the bolts in such a joint could be completely loose. Note that allowable AISC loads also contain additional margins and also that such loose bolts in critical friction connections were corrected. With regard to fatigue, the typical high cycle stress ranges evaluated for Palo Verde were low enough that no bolt preload was required to mitigate fatigue loadings. Thus, it is concluded that there is only a very low probability that loose bolts could cause a problem at Palo Verde. This conclusion is consistent with failure experience at other plants (Appendix A).

The principal double-nutting application at Palo Verde is for ASME component supports, such as pipe U-bolts. These fasteners were installed in accordance with the ASME Code paragraph NF-4725 which requires locking devices to prevent loosening during service. The Bechtel installation specification (Ref. 5 and 6) is in accordance with NF-4725. Since the function of the double-nutting is simply for locking, and not for carrying load by the second nut, the size of the outer nut is not critical. In fact, NF-4725 permits other means of locking, such as drilled and wired nuts and upset threads, which do not involve a second nut. Thus, the double-nutting procedures at Palo Verde are acceptable.

In summary, because of the extensive studies, inspections, corrective actions and inherent joint design margins at Palo Verde, Units 1, 2 and 3, the bolted joint integrity is considered above-average and acceptable for service. The key points are that deficiencies in critical connections were corrected, and that typical Palo Verde bolted connections are conservatively oversized.

2.0 PLANT EXAMINATION

In order to become more familiar with specific bolting installation procedures and the plant layout at Palo Verde, a day was spent walking through Unit 2 (considered representative of all three units), observing bolting installations and visiting the Bechtel calibration room.

2.1 Unit 2 Containment

A tour was made of all levels inside containment at Unit 2 to observe bolting. The following observations were made:

- Critical friction fasteners were marked where checked for torque,
- No "finger-loose" bolts were found,
- Double-nutted connections were observed, where both nuts were the same size or the outer one was approximately half the thickness of the first nut,
- "Torque-Seal" markings were used in approximately 50 observed fasteners to indicate nuts checked and not disturbed,
- Air-impact wrench torquing of a connection,
- Torque wrench torquing of a small electrical connection,
- Clean appearance of connection and bolting visible surfaces in all of several thousand observed bolts.

Based on these observations, it appeared that the inspection of critical friction fasteners was thorough, and that bolting workmanship was high quality in its current condition. A very high level of attention, supervision and care was being given to the bolt torquing operations which were observed.

2.2 Calibration Room

The Bechtel calibration room was visited, and the calibration of several torque wrenches was observed. No problems were found with the procedure, and it was being closely followed. Although final calibrations were performed in strict accordance with the procedure, in the case of large wrenches quite a few attempts had to be made to achieve a smooth torquing to the final desired value. This is because of the very high loads on the wrench required to reach the preload torque on large, high-strength, bolts. This could potentially lead to the undertorquing of large bolts when applying torque wrenches for actual installations, where loading can be more awkward. Evaluation of torque-checking data later in this report verifies that large, high-strength bolts installed with torque wrenches were predominantly undertorqued. The AISC (Ref. 7) recognizes variability in the use of torque wrenches and withdrew the recognition of torque control methods on August 14, 1980, except for arbitration of inspection disputes.

3.0 PALO VERDE DOCUMENT REVIEW

Numerous documents relating to bolting at Palo Verde were reviewed for pertinence to the issue of bolting integrity. The most relevant results of this review are considered below.

3.1 NRC CAT Findings

Reference 8 presents the results and responses from an NRC Construction Assessment Team inspection conducted in September of 1983. This inspection raised concerns regarding undertorqued, high-strength structural steel connections. More specifically, a number of loose and undertorqued bolts were found in the Auxiliary and Containment Buildings. This resulted in Bechtel's reinspection of 100% off all accessible critical steel connections in Units 1, 2, and 3, as will be discussed in following sections of this report (Ref. 9).

3.2 Deficiency Evaluation Reports

A large number of Deficiency Evaluation Reports (DERs) were reviewed in order to accumulate bolting data, assess past experience, and determine the current status of bolted connections at Palo Verde. Special attention was given to the following DERs.

- DER 81-14 - A354BD bolt cracking and hardness measurements, resulting in derating installations and hardness testing.
- DER 83-30 - A354BD anchor bolt failure during installation, resulting in reinstallation.
- DER 83-18 - One nut, rather than double-nut for locking on U-bolts, resulting in adding second nut.
- DER 83-15 - A354BD anchor bolt failure during installation, resulting in revised torquing.

- DER 82-61 - Type 410 martensitic stainless steel reactor coolant pump cap screw failures by hydrogen induced SCC, resulting in revised heat treatment.
- DER 83-53 - Missing bolts in Unit 3 containment building embed plates, resulting in 100% inspection of all such accessible bolts.
- DER 84-34 - Loose bolts in safety injection tank keyways, resulting in rework and repair.
- DER 84-32 - Undertorqued bolts in safety injection tank upper seismic supports, resulting in 100% reinspection of all such accessible bolts.

The above list indicates recognition of potential problems in the bolting area, and demonstrates effective identification and resolution of nonconformances, as confirmed by the analyses of this study.

3.3 Specifications and Procedures

The following bolting specifications and procedures were reviewed in detail regarding Palo Verde bolting integrity.

- Bechtel Specification No. 13-PM-204, "Specification for Field Fabrication and Installation of Nuclear Piping Systems for the Arizona Public Service Company Palo Verde Nuclear Generating Station Units 1, 2 and 3", Rev. 13, Feb. 23, 1984.
- AISC Specification for "Structural Joints Using ASTM A325 or A490 Bolts", Aug. 14, 1980.
- Bechtel Procedure No. 201.1, Rev. 20 "Nuclear Pipe Hangers and Supports Installation", April 1984.
- Bechtel Specification No. 13-CM-320, Rev. 9, "Installation Specification of Structural and Miscellaneous Steel, etc.", April 1984.

- Bechtel Procedure No. 7.0, Rev. 20, "Calibration and Control of Construction Measuring and Test Equipment", April 1984.
- Bechtel Procedure No. 14.0, Rev. 19, "Approved Materials for Construction, Nuclear Compatibility", April 1984.
- PVNGS FSAR Section 3.7.3.2, "Determination of Number of Earthquake Cycles", Amendment 4, May 1981.

The above documents contain no apparent deviations from acceptable and reasonable practices.

3.4 CMTRs

Certified Material Test Reports (CMTRs) for close to 50,000 bolts, with nearly 200 bolts tested to represent this sample, were reviewed for tensile yield strength and hardness properties. Purchase dates ranged from 1976 through 1984. Bolting materials included SA-193 Gr. B7, A540-B23, A325, SA-320 Gr. L, SA-564 Gr. 630 and A490. It was found that various combinations of minimum tempering or aging treatments (usually 1100°F), hardness maximums of Rc38, and/or tensile yield strengths of less than 150 Ksi would tend to preclude concerns about SCC for these materials. Grade A354BD bolts are a special case (discussed in DER 81-14 in a preceding section) with specific hardness and loading controls as follow.

3.5 Hardness Studies

Extensive hardness surveys of Palo Verde A354BD studs and bolts are documented in Reference 10, under DER 81-14. The appendices to Reference 10 include failure analyses by Bechtel and reviews and evaluations by Teledyne and by Battelle Pacific Northwest Laboratories. When four of these studs cracked during May and June, 1981, the failure mechanism was identified as SCC which resulted from excessive stud hardness (Ref. 10). Because of the

small test sampling required by the ASTM A354BD specification, a number of nonconforming materials passed undetected. Such materials which failed by SCC had hardness around Rc49, far in excess of the ASTM specification requirement range of Rc33 to 38. Based on recommendations by Bechtel, Teledyne and Battelle, guidelines for reduced short term and long term stress allowables were implemented for fasteners with hardness outside the specification limits. Bolts with hardness exceeding Rc43 were removed by saw-cutting. Those with Rc41 and 42 were simply secured with a hand-tight nut while Bechtel Engineering performed a review of all design calculations utilizing these fasteners. The reduction of long term stresses to below threshold levels for SCC (as a function of hardness) is a reasonable approach, as will be discussed later in this report.

3.6 Torquing Studies

Based on the NRC CAT findings (Ref. 8), Bechtel CIP No. 551.0 (Ref. 9) required 100% reinspection of all accessible critical friction connections. Such critical friction connections were determined by Bechtel (Ref. 8) to be limited to the Containment Buildings for Units 1, 2, and 3.

The results of such extensive measurements offer a unique opportunity to evaluate installation procedures and the effectiveness of various methods (turn-of-nut, torque wrench, and air impact wrench) of applying preload. All of such measured results from Bechtel data are tabulated in Appendix B for Unit 1, from micro-computer output produced in this study. Approximately half of the torque-check results for Unit 2 and for Unit 3 are tabulated similarly in Appendices C and D. Fewer results were tabulated for Units 2 and 3, but they are considered to be representative of the total data base. Most of the results are reported in terms of fraction of nut turn deviations from required torque values, although some measured break-away torque values are also reported.

The key point in these studies is that deficiencies were defined and corrected, within the limitations of the method. However, a thorough independent analysis of the potential impact of these deficiencies, if they had gone undetected, is also considered in the next sections of this report.

Such an evaluation is useful in explaining past experiences of bolt breakage during installation, in extending these results to joints and nuts which were not reinspected, and in assessing the sensitivity of preload to parameters such as torque or friction coefficients.

4.0 OVERTORQUING REVIEW AND EVALUATION

Overtorquing of bolts at Palo Verde is evaluated in terms of the potential failure mechanisms of SCC, overload and fatigue. The measured Palo Verde data base is assessed with respect to these mechanisms and conclusions are reached.

4.1 Potential Failure Mechanisms

Potential failure mechanisms for the Palo Verde structural steel bolting are overload, SCC and fatigue. SCC has been the most frequently observed failure mode among PWR structural steel bolting (Ref. 11). SCC generally results from overly hard and out-of-specification material, high sustained tensile stresses, and an aggressive environment developed from high humidity. High preload and the use of lubricants containing molybdenum disulfide also is suspected to contribute to SCC susceptibility (Ref. 11). It has been shown (Ref. 12) that material below a hardness level of about Rc38 to Rc41 is below the threshold for SCC.

Overload failures during service are very rare, and it is generally concluded (Ref. 1, 2 and 3) that if an overtorqued bolt does not fail during preloading, then it will not fail in service under proper design allowable loadings. This is because the stresses are highest in the bolt during preload, as will also be illustrated in this report.

Fatigue failures in nuclear bolting have likewise been few (Ref. 11) and are much more likely to occur in undertorqued rather than overtorqued bolts. High preloads are recognized (Ref. 1, 2 and 3) as a very effective way of limiting alternating stress ranges and mitigating fatigue, as will also be demonstrated in this report.

4.2 Hardness Threshold for SCC

Figure 4-1 shows the threshold for SCC in low alloy bolting steels, as a function of yield strength (Ref. 12). It can be seen that for yield strengths

below approximately 150 Ksi, the SCC threshold is above $50 \text{ ksi}(\text{in})^{1/2}$. This corresponds to a combination of bolt load and defect size which one would not expect to find in service, and consequently SCC is not expected. As seen in Figure 4-2 (Ref. 12), this yield strength level corresponds to a hardness of Rc37 for steels such as 4140 and 4340. Thus, SCC is eliminated as a concern at Palo Verde for materials with hardness less than Rc37 to 38. Reference 12 indicates that hardness as high as Rc41 can be tolerated, since the SCC threshold is still quite high and high stresses would be required to cause a concern. As was previously mentioned, review of CMTRs revealed bolting materials below these thresholds. In the case of DER 81-14, where out-of-spec. A354BD studs showed higher hardnesses, the sustained stresses in these bolts were appropriately decreased to accommodate the slightly lower SCC threshold. Furthermore, as was experienced with DER 81-14, such SCC failures would have most likely already occurred and been detected during subsequent reinspections. Thus, further SCC of structural bolting at Palo Verde is not likely.

4.3 Overload Analysis

The torquing data base in Appendices B, C and D was analyzed quite extensively in order to evaluate effects on bolting preload and fastener integrity. Before discussing these analyses more extensively, however, it is first prudent to briefly review some basic concepts in the loading of bolted connections, as given in References 2 and 3.

Figure 4-3 illustrates the loads in a bolted connection where the terms are defined as:

- P = total external load on bolted assembly
- F_i = preload on bolt
- P_b = portion of P taken by bolt
- P_m = portion of P taken by members
- F_b = resultant bolt load
- F_m = resultant load on members.

The increase in deformation of the bolt, $\Delta\delta_b$, due to P_b is given by the stiffness or spring constant of the bolt and the following equation:

$$\Delta \delta_b = \frac{P_b}{K_b} \quad (4-1)$$

Similarly, the decrease in compression of the connected members due to the external load P is given by:

$$\Delta \delta_m = \frac{P_m}{K_m} \quad (4-2)$$

Since $\Delta \delta_b$ must equal $\Delta \delta_m$ when the members have not separated, then

$$\frac{P_b}{K_b} = \frac{P_m}{K_m} \quad (4-3)$$

Also, since $P = P_b + P_m$, then

$$F_b = P_b + F_i = \frac{K_b P}{K_b + K_m} + F_i \quad (4-4)$$

and

$$F_m = \frac{K_m P}{K_b + K_m} - F_i \quad (4-5)$$

The above relationships for compression in the fastened members and tension in the bolt, due to preload and external loads, are illustrated in Figure 4-3(b).

The stiffness of the members can be approximated by

$$K_m = \frac{2\pi d^2 E}{L} \quad (4-6)$$

and in the bolt as

$$K_b = \frac{\pi d^2 E}{4L} \quad (4-7)$$

where

- d = bolt diameter
- E = elastic modulus
- l = length of the grip

For the bolt and member of approximately the same material (steel), it can be seen that

$$K_m = 8K_b \quad (4-8)$$

Now an illustration can be given to show the effectiveness of the preload in reducing the proportion of the external load which is taken by the bolt. Assume a preload bolt stress of 75% of the bolt minimum ultimate tensile strength (UTS), or 75% of 150 Ksi equals 112.5 Ksi, and a working stress of 1/3 UTS, or 50 Ksi. From equation (4-4), when all terms are divided by the bolt stress area, it can be seen that the resultant stress taken by the bolt is only 112.5 plus 50/9, or 118.1 Ksi. This is an extreme example since the working stress is near the maximum permitted by Table 2 of Reference 7.

Thus, in most cases at Palo Verde increases in resultant bolt load due to external loads would be a small fraction of the preload and would have an insignificant effect. An effective analogy is shown in Figure 4-3(c) where a fish-scale is loaded with 150 lb. (preload), blocked at that deformation, and the load removed. For an infinitely stiff block, any subsequently applied loads of less than 150 lb. will have no effect on the movement of the scale.

Furthermore, a certain amount of relaxation of preload stresses in the bolt due to removal of torquing shear stresses in the bolt is demonstrated by the Mohr's circle in Figure 4-4(a), where

- σ_x = bolt tensile stress
- τ_{xy} = bolt shear stress, due to torquing
- σ_1 = maximum normal tensile stress, or principal stress
- S_p = proof or yield stress
- S_u = ultimate tensile stress

Fracture of the bolt is controlled by σ_1 , which is given in Reference 13 (for a uniaxial stress state) as

$$\sigma_1 = \frac{\sigma_x}{2} + \left[\left(\frac{\sigma_x}{2} \right)^2 + \tau_{xy}^2 \right]^{1/2} \quad (4-9)$$

where

$$\tau_{xy} = \frac{16T}{\pi d^3} \quad (4-10)$$

with the torque, T, being a function of the preload, the torque coefficient K, and the bolt diameter

$$T = KF_i d \quad (4-11)$$

Figure 4-4(a) illustrates that significant relaxation in the bolt occurs due to removal of torsional (torquing) stresses of preload. Further relaxation occurs due to settling in of dirt and lubricants on threads and due to low temperature stress relaxation (creep).

The preceding concepts demonstrate that if a bolt does not fail during tightening, it should never fail by overload. This will be quantified by analysis of the Palo Verde data base, and will conversely show that a certain number of bolting failures during preload are to be expected. The main point is that overload failures during service are very unlikely for bolted joints.

4.4 Fatigue Analysis

The basis for evaluating fatigue resistance in bolting is illustrated in Figure 4-4(b) for a steel with UTS=100 Ksi (Ref. 2). Basically, the fatigue endurance limit, \dot{S}_e , is given (Ref. 2) as:

$$S_e = K_a K_b K_e S_{uts} \quad (4-12)$$

where

K_a = surface effect (0.73 for finish machined)

K_b = size effect (0.85 for less than 2" dia.)

K_e = thread root effect (0.454)

S_{uts} = ultimate tensile strength

Equation (4-12) reduces to

$$S_e = .141 S_{uts} \quad (4-13)$$

Now an equation for the allowable alternating stress (Goodman Line) in Figure 4-4(b) can be derived as

$$\text{allow. } \sigma_a = 0.141 \left[S_{uts} - \left(\frac{\sigma_{\max.} + \sigma_{\min.}}{2} \right) \right], \quad (4-14)$$

and used to evaluate the effects of preload on fatigue life.

Alternating and mean stresses are defined as

$$\sigma_a = \frac{\sigma_{\max} - \sigma_{\min}}{2} \quad (4-15)$$

$$\sigma_m = \frac{\sigma_{\max} + \sigma_{\min}}{2} \quad (4-16)$$

For alternating stresses falling above the Goodman Line in Figure 4-4(b), fatigue failure is predicted in less than 10^6 cycles. For σ_a below the line, fatigue failure is not probable.

The earlier example of preload analysis and overload considerations (Section 4.3), can be extended to include fatigue considerations. From that example, the effect of preload can be seen to significantly reduce the resultant stress on the bolt caused by external loads. For the preload of 112.5 Ksi and a working stress of 50 Ksi the resultant stress on the bolt is 118.1 Ksi. Now

a fatigue stress range of 3 Ksi ($\sigma_a = 1.5$ Ksi) will be superimposed on this loading. In this case, $\sigma_{max} = (50 + 1.5)/9 + 112.5 = 118.2$ Ksi and $\sigma_{min} = (50 - 1.5)/9 + 112.5 = 117.9$ Ksi. Thus, it can be seen that for high preload, the effects of realistic fatigue cycling, even superimposed on a very high working stress, are negligible. Thus, fatigue is not a concern in the case of high preload, or even overtightening. This is a recognized fact in practice (Ref. 1, 2 and 3).

4.5 Palo Verde Data Base

Although the preceding generic conclusions indicate that overtightening is not a concern regarding bolt failures in service, a close look was also taken at the specific Palo Verde data base. In so doing, a range of torque coefficients, K, were employed to compute preload. Values of K representing different conditions of bolt lubrication are given in Appendix E and range from 0.11 for lubricated bolts to 0.43 for rusty bolts. A value of K=0.16 represents a bolt used without lubrication, and K=0.20 is the text-book value of torque coefficient (Ref. 3).

The statistical distributions of preload torques and deviations from specified turn-of-the-nut values are given in Tables 4-1 through 4-3 for Units 1, 2 and 3. These statistics represent the data base in Appendices B through C, discussed earlier. It can be seen that a very large number of bolts were sampled. For a typical specified turn-of-the-nut value of 0.5 turn (Ref. 7), it can also be seen that there were a number of deviations from the specified value (nut rotation =0 for cases where specification was met in Tables 4-1 through 4-3). Reference 7 does permit a 30 degree (0.083 turn) leeway in meeting the 0.5 turn requirement; thus such values in excess of 30 degrees were analyzed separately. The samples included both A325 and A490 bolts, and bolt sizes of 7/8", 1" and 1-3/8" diameter.

Distributions of the above results are shown in Figures 4-5 through 4-7 for nut rotation deviations at Units 1, 2 and 3. These figures indicate quite good adherence to the specification at Units 1 and 3, and more frequent deviations at Unit 2. This could be due to the different methods of installation predominantly used at each unit (turn-of-nut at Unit 1, torque

wrench at Unit 2, and air impact wrench at Unit 3). Again, it is only the deviations in nut rotation of greater than 0.1 that are of concern, and all deviations were corrected.

From the standpoint of overtorquing, the torque measurements on Unit 2 are of more interest than turn-of-nut deviations (undertorque). Based on the Unit 2 torque measurements, preloads and bolt stresses were computed. Preloads were also derived from nut rotation measurements from the following equation

$$F_i = \frac{(F_i \text{ spec.})}{0.5} (0.5 - \text{Nut Rotat.}) \quad (4-17)$$

The results of these preload calculations are given in Appendices F through J for Units 1, 2 and 3. Frequency distributions for Unit 2 preload stress as a ratio of minimum specified UTS are given in Figures 4-8 through 4-11 for the four torque coefficients previously discussed. A stress ratio of 0.70 is the aim of Reference 7, for preload. It can be seen in these figures that significant deviations exist from the stress ratio of 0.70. A very large effect of assumed K is also seen in Figures 4-8 through 4-11. A K of 0.11 could cause some bolt failures during preload, whereas K=0.43 (rusty bolt) would result in significant undertorquing.

Similar results from other studies (Ref. 1) are shown in Figures 4-12 and 4-13. Figure 4-12 illustrates that significant scatter in preload can occur for a given torque, even under controlled laboratory conditions. Figure 4-13 shows extremely high scatter in preload for reinspected as-installed bolts. In comparison, the results at Palo Verde Unit 2 appear reasonable.

Again, as recognized by Reference 7, torque/preload relationships are quite variable even under the best conditions.

In further considering overload failures, Figure 4-14 shows the ratio of maximum principal stress (including torque shear stresses) to minimum UTS during preload, as a function of K for nut-turn to the specified 0.5 turn. It can be seen that a number of bolts would be expected to fail during preload

(ratio greater than unity), especially for low values of K. This prediction is mitigated by the fact that many bolts have strengths considerably in excess of the minimum specified value. Tempering this prediction is the fact that bolts which do not fail on preload will relax significantly following the removal of torque. Figure 4-15 shows this effect, where the relaxation ranges from approximately 2 to 20% just from the absence of torquing shear stresses, based on the calculations in the Appendices of this report. Adding this effect to other relaxation mechanisms gives confidence that properly designed bolts will not fail by overload in service.

4.6 Overtorquing Conclusions

Overtorquing has been shown to lead to possible bolt failures during preload. However, because of meeting material hardness limits and because 100% of accessible critical friction joints have been checked, it is not a concern during service for Palo Verde structural steel for the most likely mechanisms considered: SCC, overload, and fatigue.

TABLE 4-1

PALO VERDE 1 TORQUE CHECK STATISTICS FOR CRITICAL FRICTION FASTENERS
 (UNITS ARE FRACTION OF TURN AND NO. OF NUTS CHECKED)

ALL NUT ROTAT:	NO.	1609.000
	AVG.	0.015
	MAX.	1.083
	STD.	0.058
NON-ZERO NUT ROTAT:	NO.	268.000
	AVG.	0.092
	MIN.	0.016
	MAX.	1.083
	STD.	0.114
> 30 DEG. NUT ROTAT:	NO.	59.000
	AVG.	0.255
	MIN.	0.104
	MAX.	1.083
	STD.	0.155

BOLT GRADE	NO.
A325	958.000
A490	651.000

BOLT SIZE	NO.
0.875	1070.000
1.000	41.000
1.375	498.000

4-10

TABLE 4-2

PALO VERDE 2 TORQUE CHECK STATISTICS FOR CRITICAL FRICTION FASTENERS
 (UNITS ARE FRACTION OF TURN FOR NUT ROTATION AND FT-LB. FOR TORQUE, AND NO. OF NUTS CHECKED)

ALL NUT ROTAT:	NO.	636.000	ALL NUT TORQUE: (1.375 IN)	NO.	106.000
	AVG.	0.078		AVG.	697.406
	MAX.	1.333		MAX.	2550.000
	STD.	0.186		MIN.	150.000
NON-ZERO NUT ROTAT:	NO.	220.000		STD.	434.604
	AVG.	0.227			
	MAX.	1.333			
	STD.	0.258			
4-11 >30 DEG. NUT ROTAT:	NO.	103.000			
	AVG.	0.421			
	MIN.	0.125			
	STD.	0.267			
BOLT GRADE A325	NO.	427.000			
BOLT GRADE A490		315.000			
BOLT SIZE 0.875		581.000			
BOLT SIZE 1.000		23.000			
BOLT SIZE 1.375		138.000			

TABLE 4-3

PALO VERDE 3 TORQUE CHECK STATISTICS FOR CRITICAL FRICTION FASTENERS
 (UNITS ARE FRACTION OF TURN FOR NUT ROTATION AND FT-LB. FOR TORQUE, AND NO. OF NUTS CHECKED)

ALL NUT ROTAT:	NO.	504.000	ALL NUT TORQUE:	NO.	120.000
	AVG.	0.009		AVG.	2385.000
	MAX.	0.500		MAX.	2385.000
	STD.	0.043		STD.	0.000
NON-ZERO NUT ROTAT:	NO.	47.000	>30 DEG. NUT ROTAT:	NO.	11.000
	AVG.	0.096		AVG.	0.261
	MAX.	0.500		MIN.	0.167
	STD.	0.107		STD.	0.107

BOLT GRADE	NO.	SIZE (IN)	NO.
A325	410.000	0.875	487.000
BOLT GRADE	NO.	SIZE (IN)	NO.
A490	214.000	1.000	17.000
		SIZE (IN)	NO.
		1.375	120.000

4-12

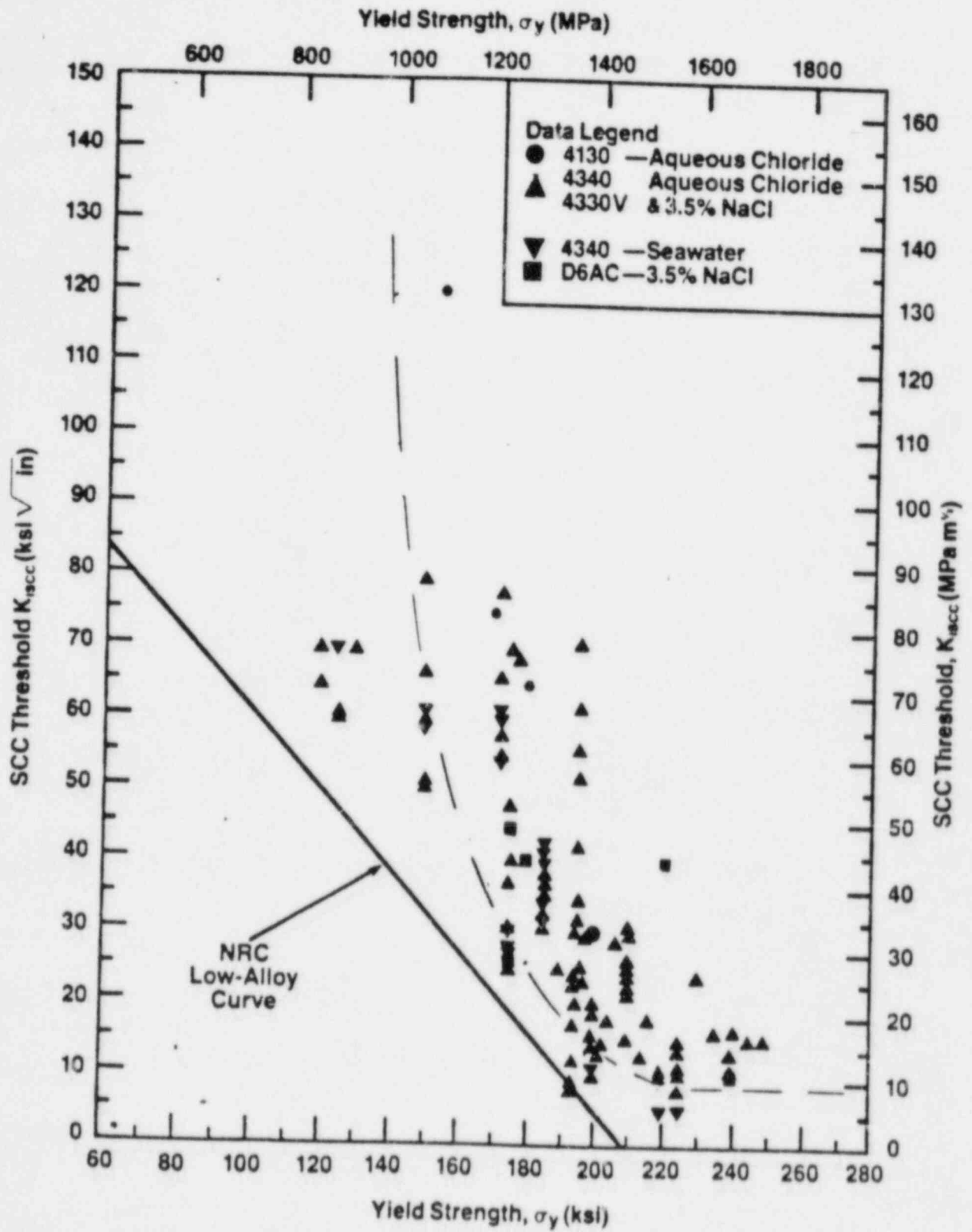


Figure 4-1. SCC Threshold Data for Bolting Steels in Aqueous Chloride Solutions (Ref. 12)

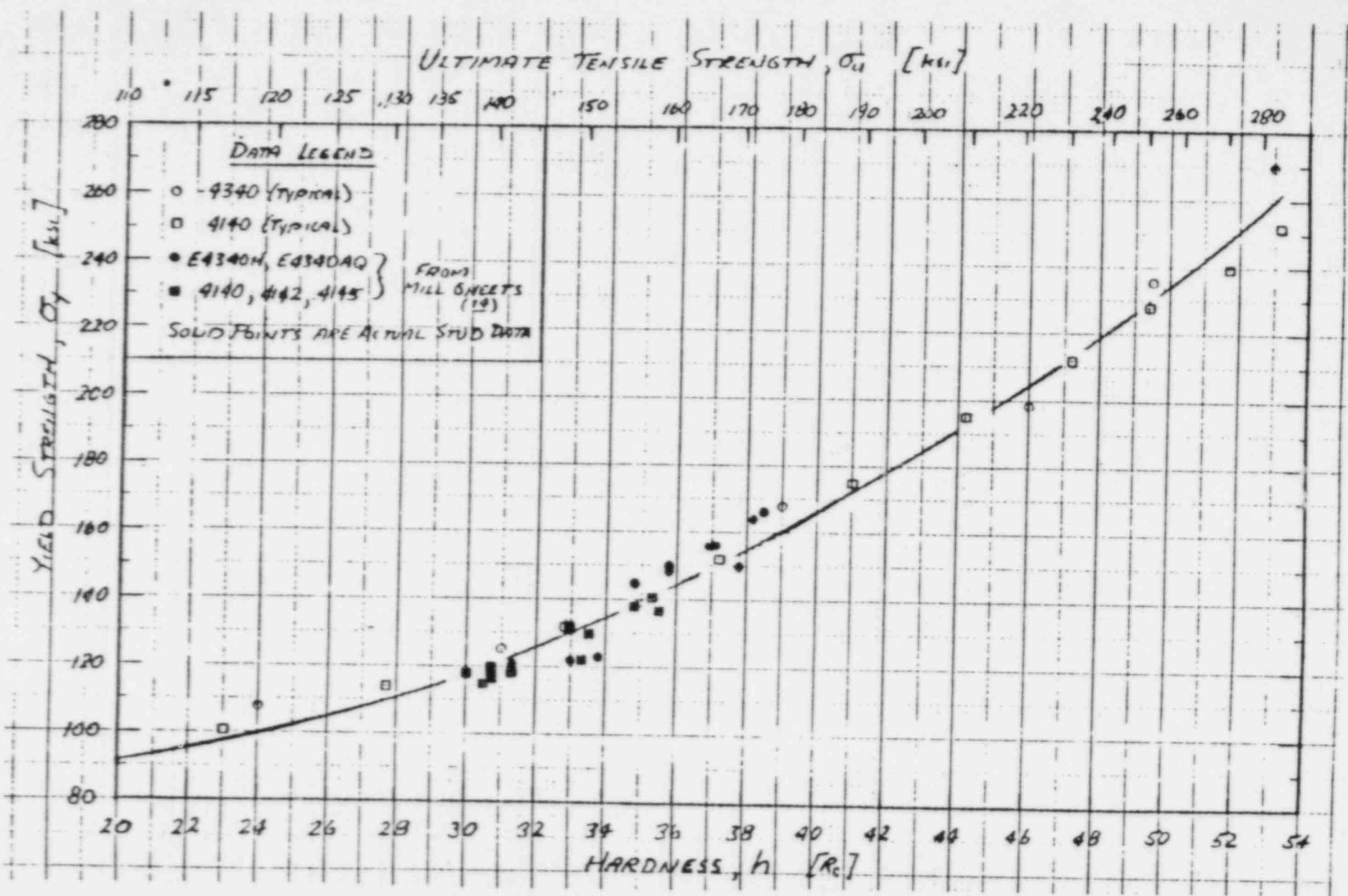
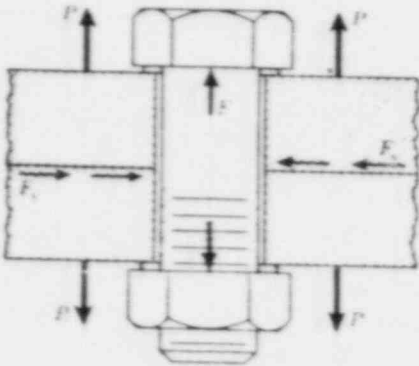
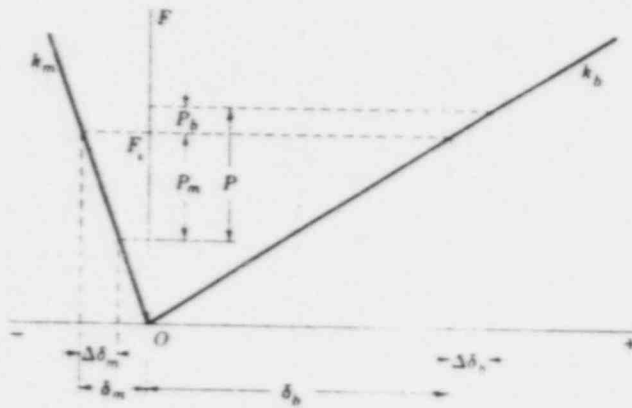


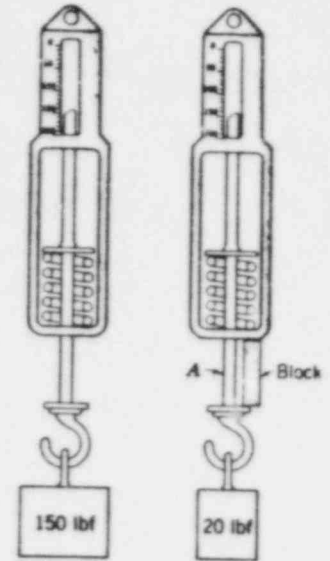
Figure 4-2. Yield Strength as a Function of Hardness for 4340 and 41XX Bolting Steels (Ref. 12)



a) Loads in a bolted connection

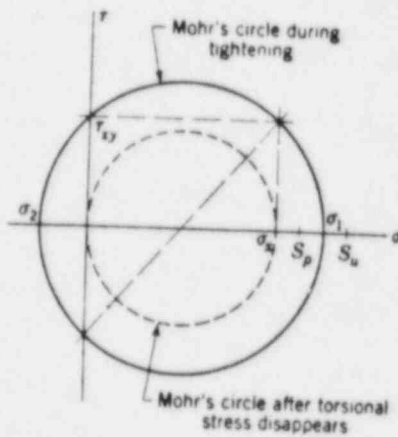


b) Load-deflection diagram for bolt (b) and member (m)

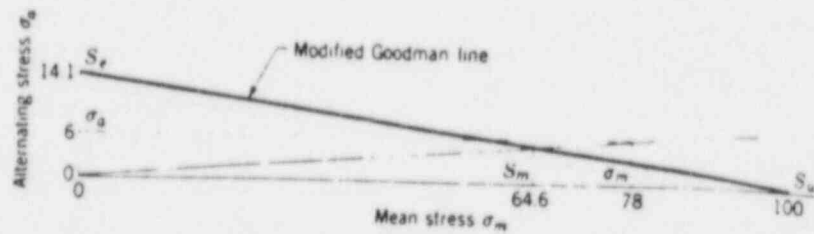


c) Fish-scale analogy of preload effect in a bolted joint

Figure 4-3. Basic Concepts in the Loading of Bolted Connections (Ref. 2)



a) Mohr's circle for a bolt, showing the torquing effect (shear stress τ_{xy})



b) Modified Goodman diagram showing the mean stress effect on allowable alternating stress in fatigue

Figure 4-4. Illustration of Loading Effects in Bolted Connections (Ref. 2)

PV 1 NUT ROTATION

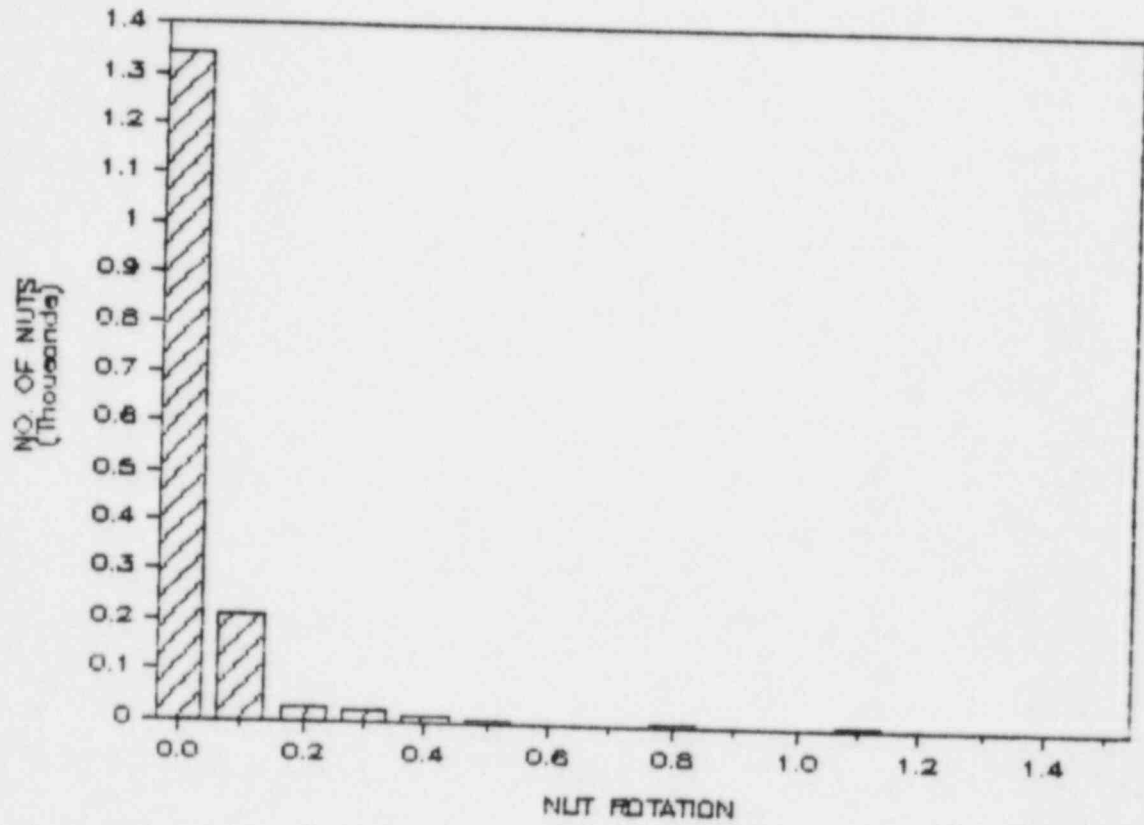


Figure 4-5. Distribution of Measured Nut Rotation Deviations from Requirements for Palo Verde 1

PV 2 NUT ROTATION

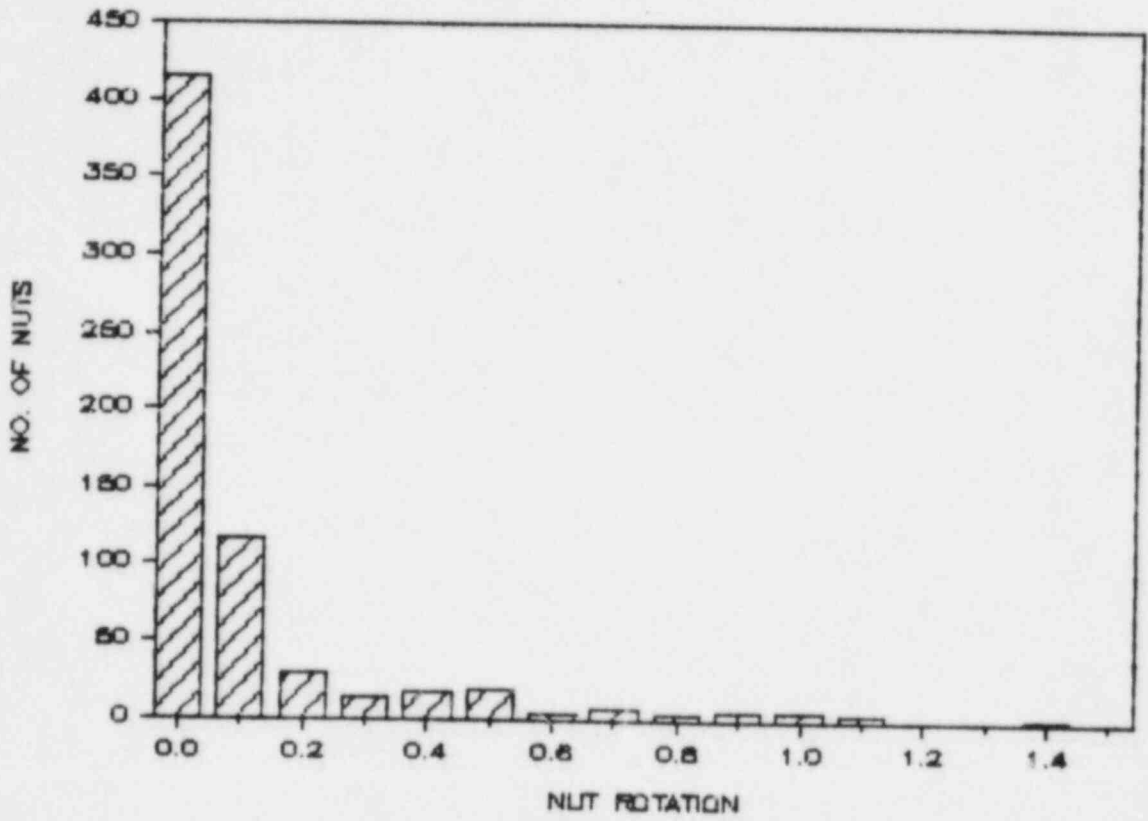


Figure 4-6. Distribution of Measured Nut Rotation Deviations from Requirements for Palo Verde 2

PV 3 NUT ROTATION

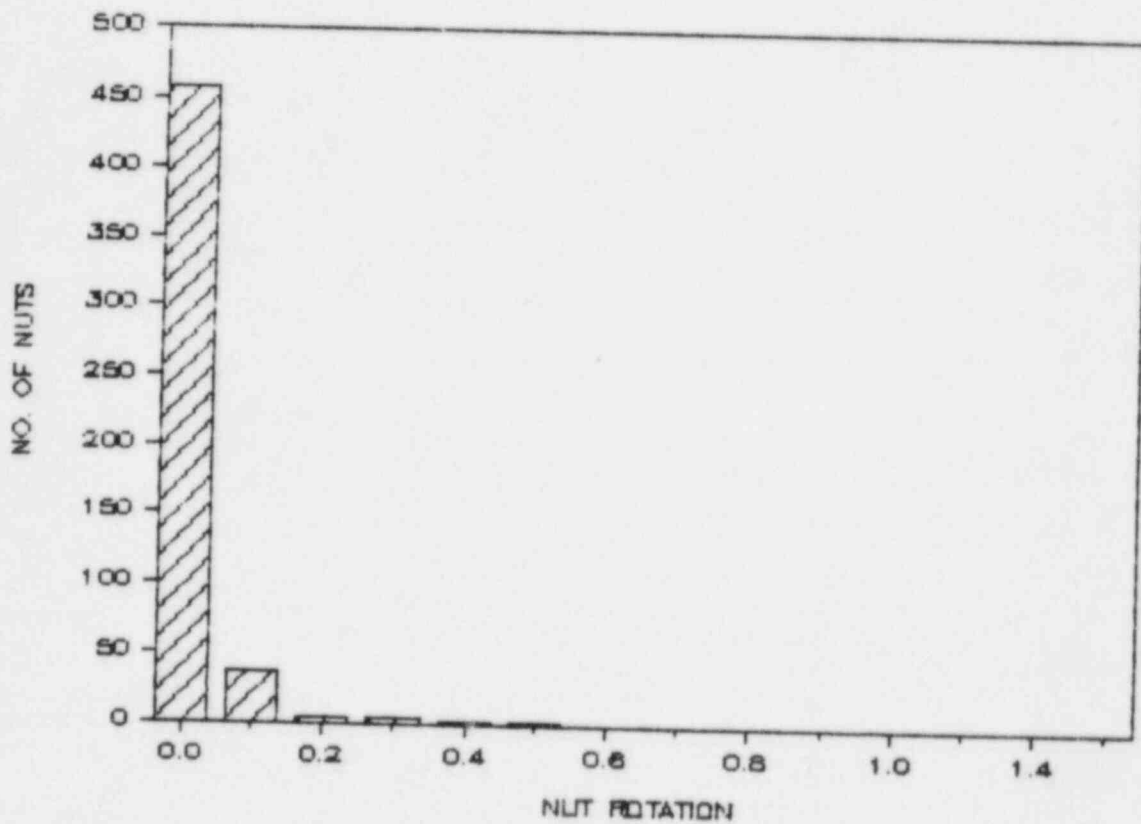


Figure 4-7. Distribution of Measured Nut Rotation Deviations from Requirements for Palo Verde 3

PV 2 PRELOAD BY TORQUE WRENCH

ASSUMED $K=0.11$

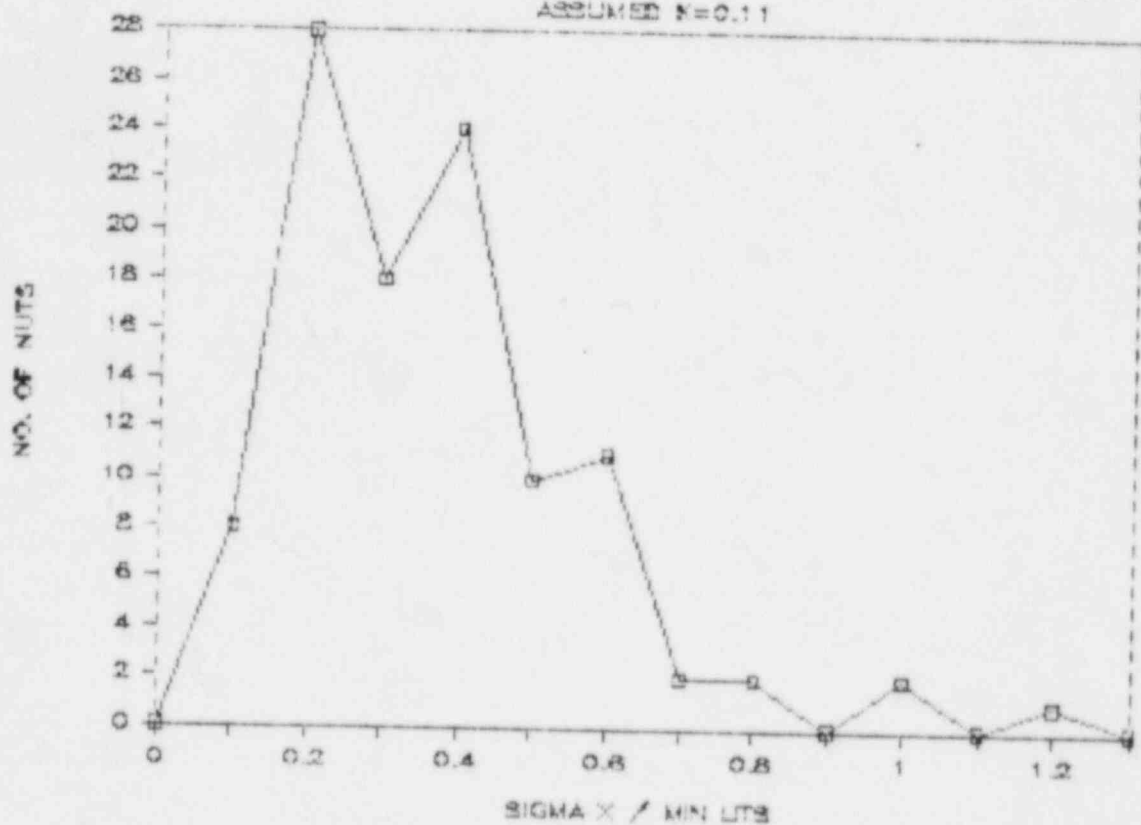


Figure 4-8. Distribution of Calculated Preload Stress/Min. UTS for $K = 0.11$ at Palo Verde 2

PV 2 PRELOAD BY TORQUE WRENCH

ASSUMED $K=0.16$

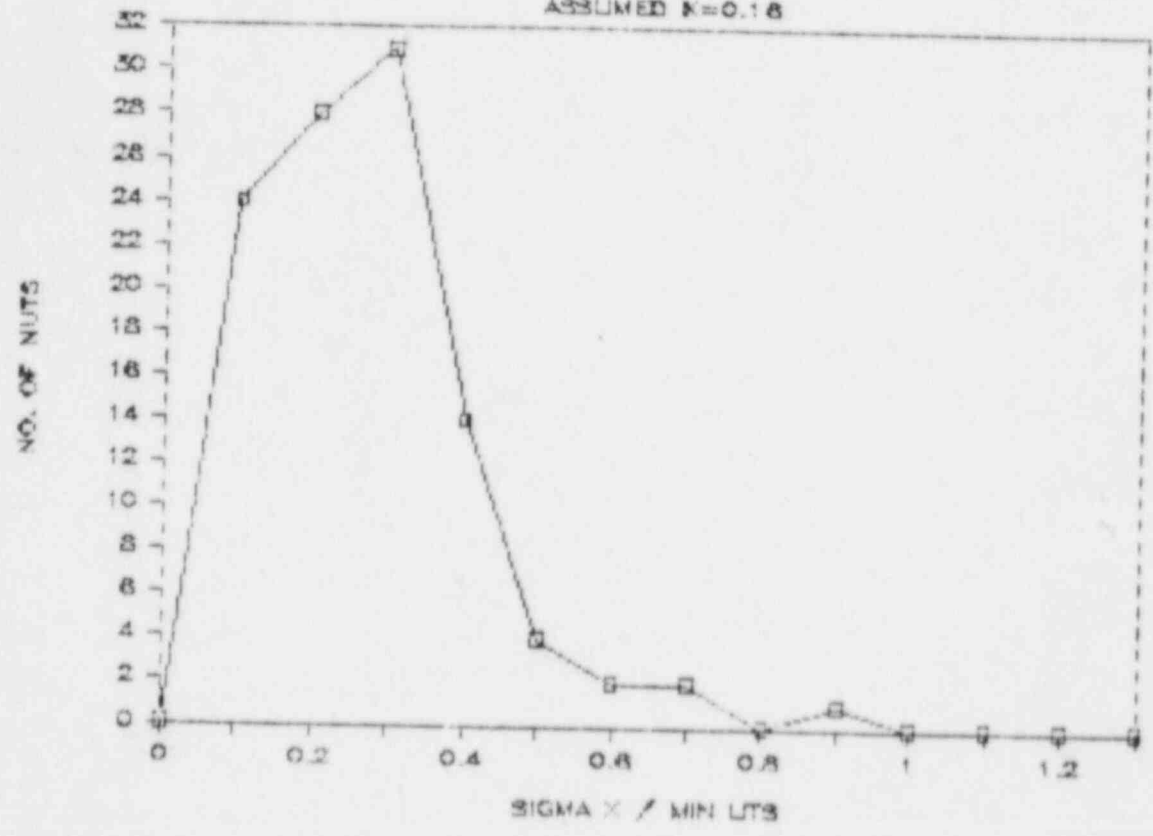


Figure 4-9. Distribution of Calculated Preload Stress/Min. UTS for $K = 0.16$ at Palo Verde 2

PV 2 PRELOAD BY TORQUE WRENCH

ASSUMED $K=0.20$

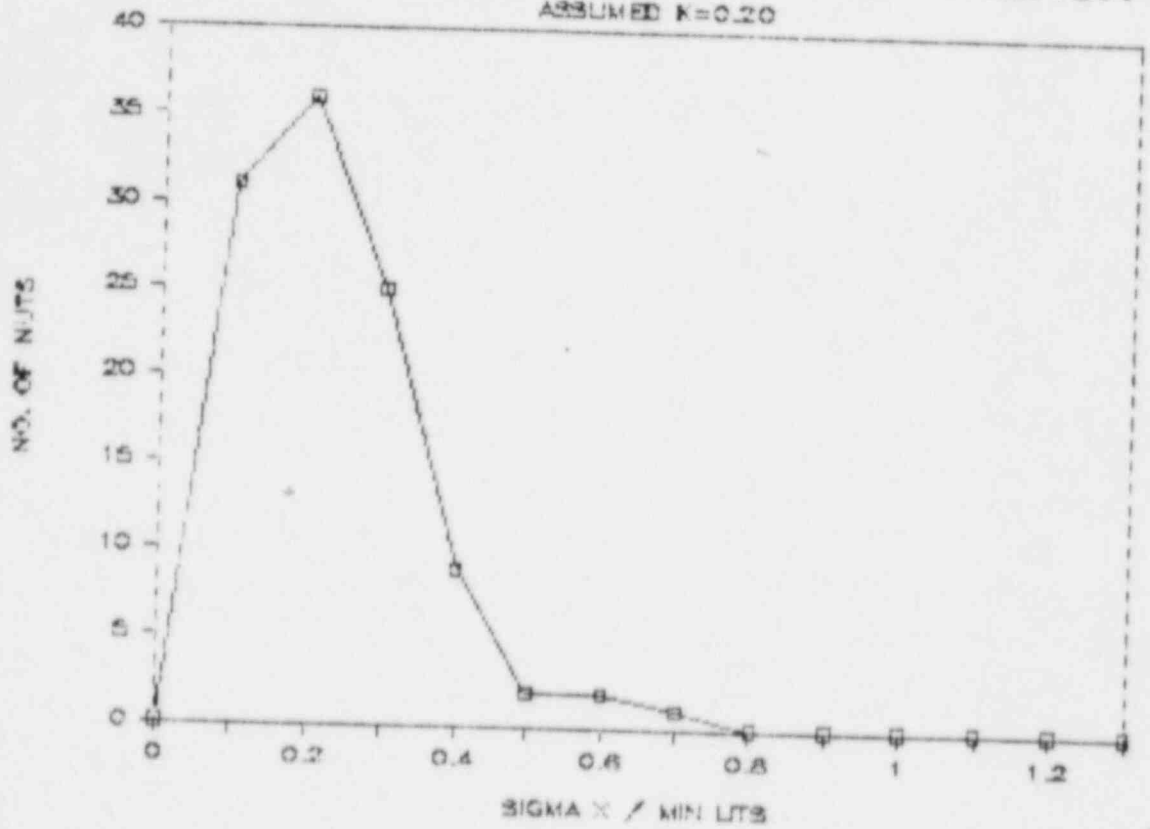


Figure 4-10. Distribution of Calculated Preload Stress/Min. UTS for $K = 0.20$ at Palo Verde 2

PV 2 PRELOAD BY TORQUE WRENCH

ASSUMED $K=0.43$

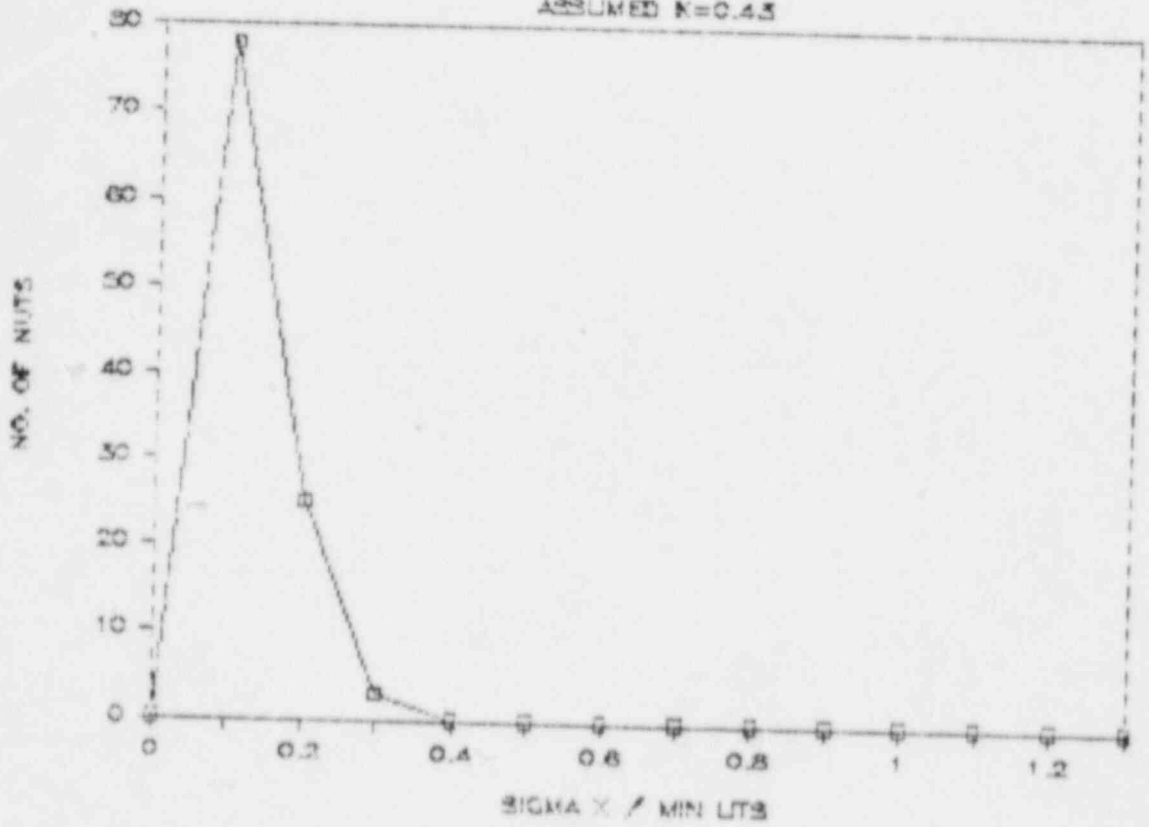


Figure 4-11. Distribution of Calculated Preload Stress/Min. UTS for $K = 0.43$ at Palo Verde 2

LAB. TEST
 SKIDMORE-WILHELM TENSILE TESTER
 1 1/4" A490 BOLTS
 GRIP 3.5"

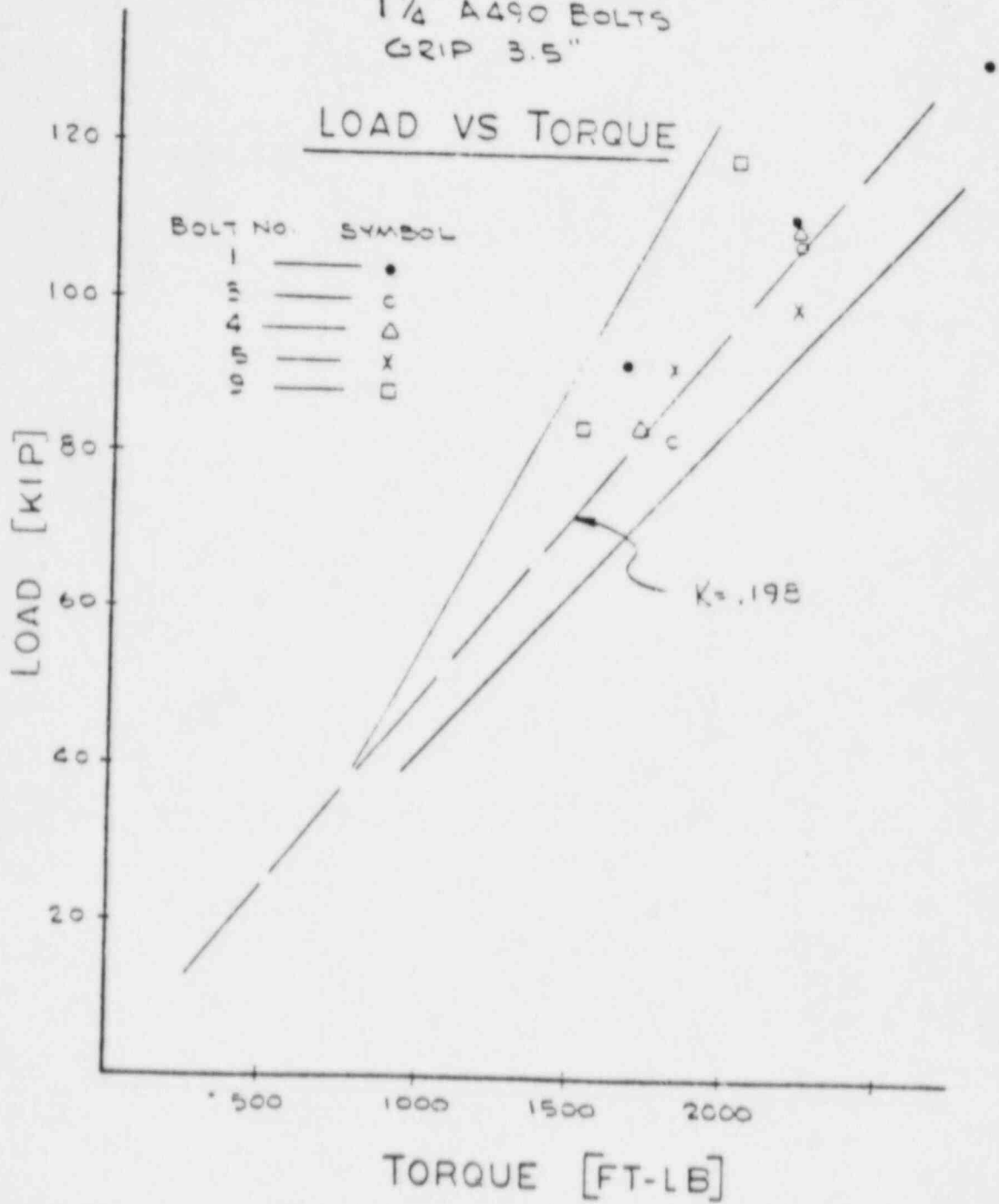


Figure 4-12. Example of Load Vs. Torque Variation Under Controlled Laboratory Conditions from Another Study (Ref. 1)

LOAD VS RESTART TORQUE

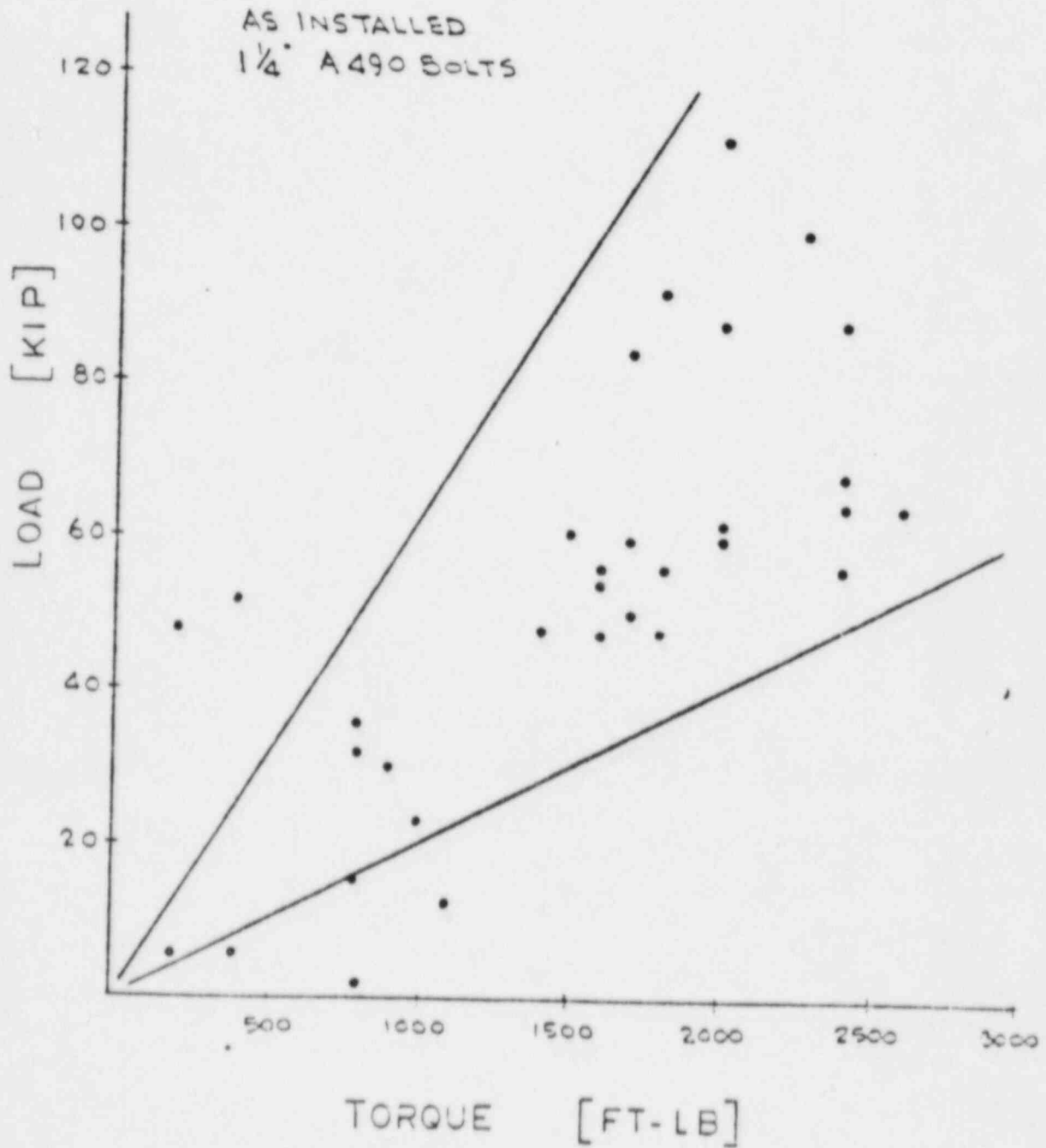


Figure 4-13. Example of Load Vs. Restart Torque Measured on Field-Installed Bolts from Another Study (Ref. 1)

TORQUE COEFFICIENT EFFECT

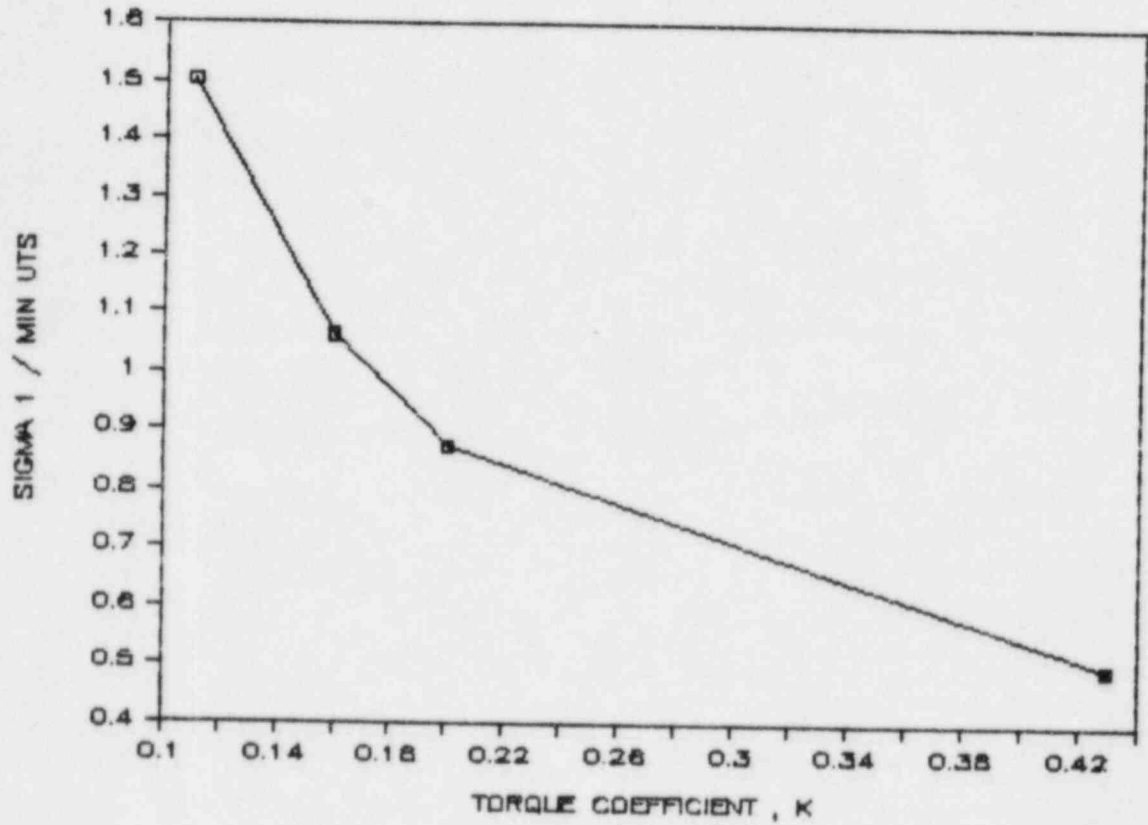


Figure 4-14. Effect of the Torque Coefficient on Principal Stress/Min. UTS During Preload to 1/2 Turn, Showing Potential for Overload Failure During Preload

PV BOLT RELAXATION (MIN.) (ALL PRELOAD LEVELS)

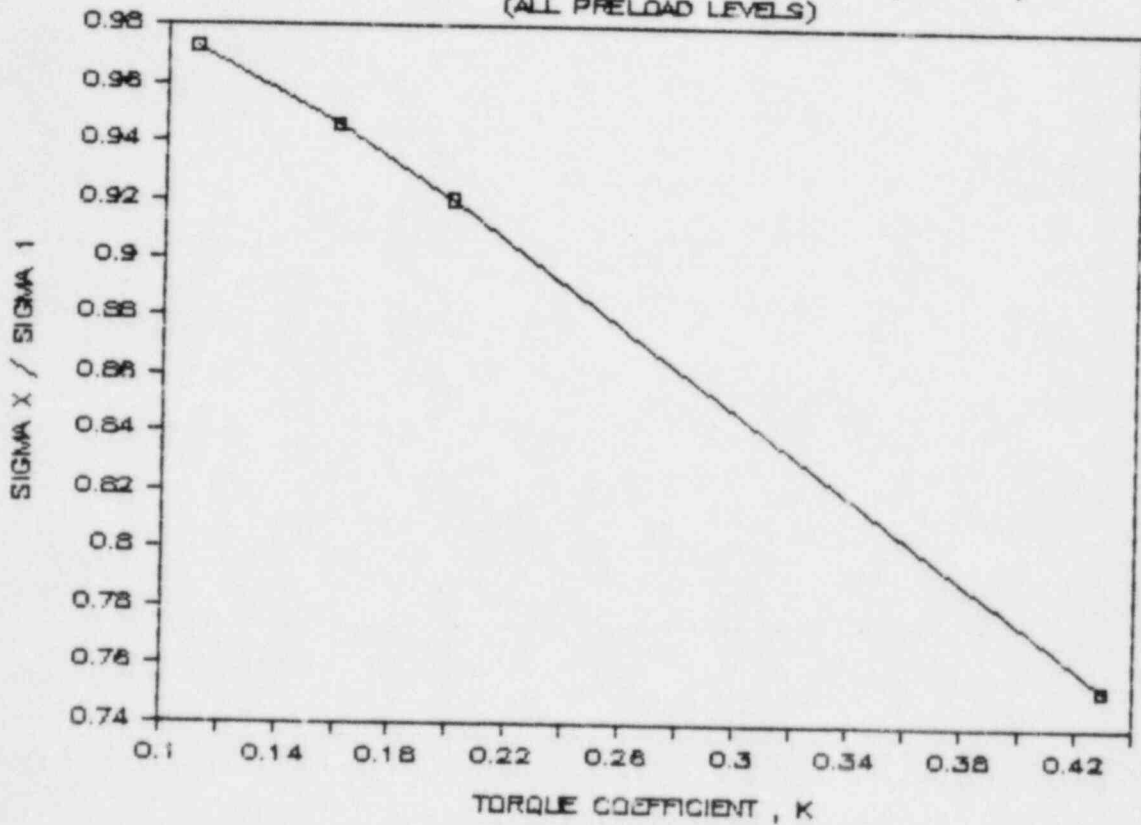


Figure 4-15. Palo Verde Bolt Stress Relaxation as a Result of Removing Torquing Shear Stress

5.0 UNDERTORQUING REVIEW AND EVALUATION

As with overtorquing, undertorquing will be considered with regard to potential failure mechanisms in service, and the Palo Verde data base will be specifically examined in this respect.

5.1 Potential Failure Mechanisms

Potential failure mechanisms, for properly designed bolts, due to undertorquing are: slippage in slotted holes, leakage in reactor coolant pressure boundary connections, and fatigue. As seen in Reference 14, leakage in bolted flange connections can be detected and remedied by tightening the bolts. Thus, this potential failure mechanism is handled in the above manner and will not be further considered here. Slippage of loose bolts in slotted holes can be a concern for structural steel. However, if a problem could occur, it would most likely have already shown some indications of slippage. Furthermore, as seen in Appendix K most connections have considerable design margins above and beyond the usual AISC margins. For example, with a stress design margin of 1.5 (typical in Appendix K) approximately 1/3 of the bolts in a connection could be completely loose and still meet the AISC design. Because of the above, and because all accessible critical friction joints have been reinspected and corrected, the mechanism of joint slippage will not be considered further.

The mechanism of most concern in undertorqued bolts (References 1, 2 and 3) is fatigue, which will be considered in more detail below.

5.2 Fatigue Evaluation for Palo Verde

The methodology of Section 4.0 of this report has been applied to predict fatigue margins at Palo Verde. Because Unit 2 showed a tendency toward multiple loose or undertorqued bolts in a connection, calculations of fatigue resistance were made with the assumption of no preload at all. In order to realistically make this evaluation, information was obtained from Bechtel (Reference 4) on typical fatigue loadings at Palo Verde, as shown in

Appendix K. Based on Appendix K, the maximum cyclic stress range per bolt was assumed to be 3 Ksi for cases of vibration and high cycle fatigue in rotating equipment. This stress, along with the assumption of zero preload, was used to compute fatigue margins for the common bolting grades at Palo Verde, as shown in Table 5-1 and Figure 5-1. These results show factors against high cycle fatigue failure ranging from 2 to 5, depending on the bolt grade, even for no preload. The approximate maximum allowable stress was also conservatively assumed (Table 5-1) in order to include maximum mean stress effects. The consideration of alternating stresses due to earthquakes is a relatively low cycle event (960 cycles per plant life for 2 earthquakes) based on the FSAR (Reference 15). Earthquake cycling is considered to be included in the fatigue endurance stress concepts (greater than 10^6 cycles of life) employed above.

Further margin against fatigue is provided by the fact that connections in general carry some preload, even when some percentage of connections are loose or undertorqued. The correlation between nut rotation deviation and preload stress for various bolt conditions is shown in Figure 5-2. Figure 5-2 indicates that nut rotations of half the specified turn (0.5) for all bolts in a connection would still result in a joint preload stress of from about 0.15 to 0.70 of minimum UTS.

5.3 Undertorquing Conclusions

Based on vibratory stress ranges at Palo Verde supplied by Bechtel, ample margins against fatigue exist, even for severe undertorquing situations. Because of the design margins, and because 100% of accessible critical friction joints have been checked (and would see only low cycle fatigue, Ref. 15), undertorquing is not expected to cause failure at Palo Verde.

TABLE 5-1

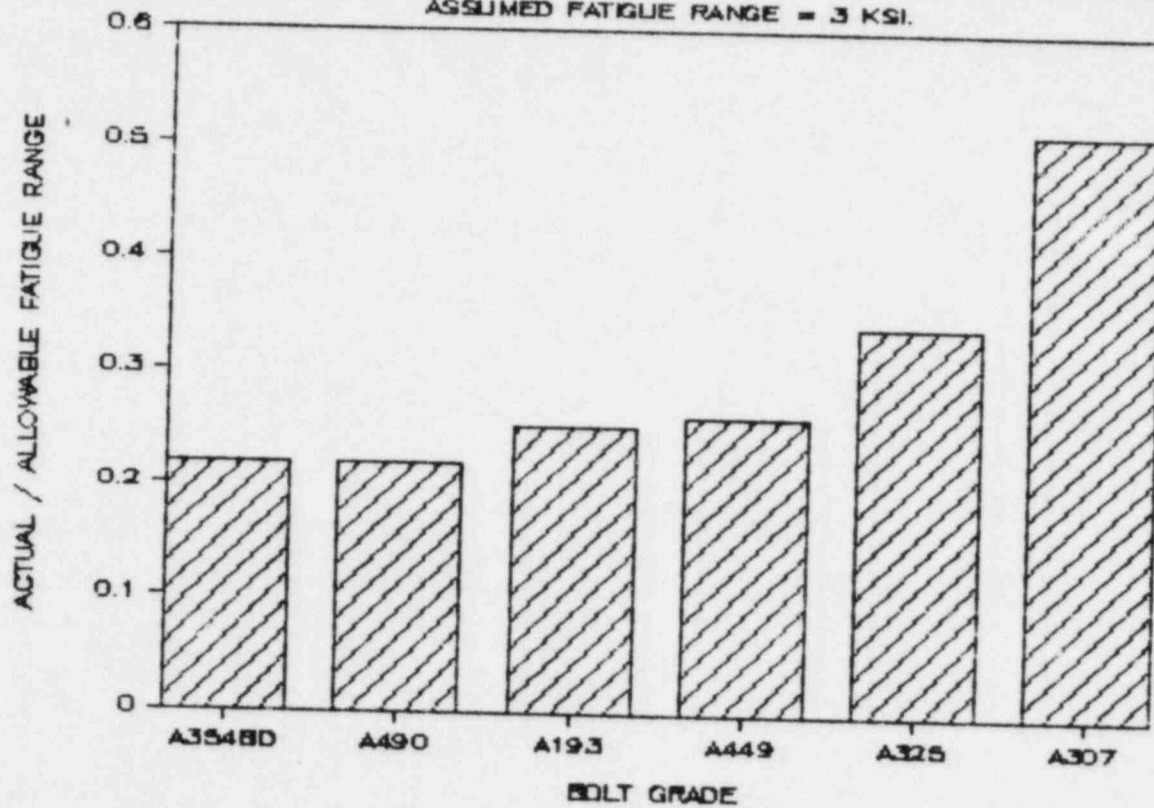
PREDICTED FATIGUE RESISTANCE FOR PALO VERDE BOLTING

PALO VERDE FATIGUE RESISTANCE OF UNDER-TORQUED BOLTS (ZERO PRELOAD ASSUMED)

BOLT GRADE	BOLT SIZE (IN)	NUT ROTAT TH/IN	N	A	TURN SPEC	TURN ACT	F _i ACT	SIGMA X	UTS MIN	ASSUMED			ALLOWABLE	
										FATIGUE RANGE/BOLT	ALLOWABLE STRESS	FATIGUE RANGE/BOLT	ACTUAL/ALLOWABLE RANGE	
A325	0.875	0.500	9.000	0.462	0.500	0.000	0.000	0.000	105000.000	3000.000	44000.000	8812.500	0.340	
A490	0.875	0.500	9.000	0.462	0.500	0.000	0.000	0.000	150000.000	3000.000	54000.000	13747.500	0.218	
A307	0.875	0.500	9.000	0.462	0.500	0.000	0.000	0.000	50000.000	3000.000	20000.000	5851.500	0.513	
A193	0.875	0.500	9.000	0.462	0.500	0.000	0.000	0.000	125000.000	3000.000	42000.000	11914.500	0.252	
A354BD	0.875	0.500	9.000	0.462	0.500	0.000	0.000	0.000	150000.000	3000.000	54000.000	13747.500	0.218	
A449	0.875	0.500	9.000	0.462	0.500	0.000	0.000	0.000	120000.000	3000.000	40000.000	11491.500	0.261	

FATIGUE MARGIN PER BOLT , ZERO PRELOAD

ASSUMED FATIGUE RANGE = 3 KSI.



5-4

Figure 5-1. Calculated Fatigue Margins at Palo Verde for High Cycle Fatigue Vibrations with an Assumed Actual Stress Range of 3 Ksi and Zero Preload While at Maximum Working Stresses ($\approx 1/3$ UTS)

PV NUT ROTATION VS. PRELOAD

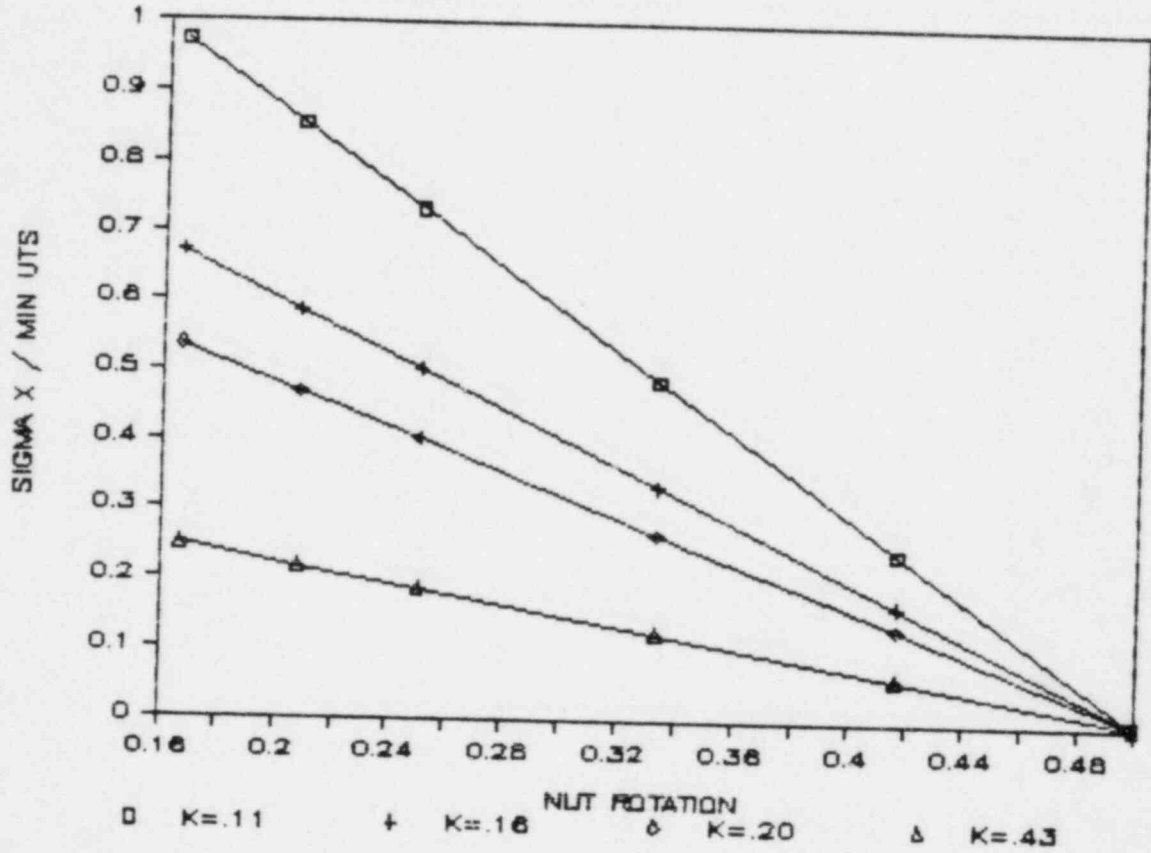


Figure 5-2. Effect of Nut Rotation Deviation from a Requirement of 1/2 Turn on Preload Stress/Min. UTS for Various Torque Coefficients

6.0 DOUBLE-NUTTING REVIEW AND EVALUATION

Double-nutting is the practice of putting two nuts on a single bolt. There are several reasons for this practice: (1) load-sharing between the two nuts, and (2) the second nut acts as a locking device to prevent loosening the first nut. In cases of load-sharing, the second nut is generally designed to be larger than the first nut, since it can see a significant proportion of the load. This is especially true for "soft" nuts, where yielding of the threads will permit more load transfer (Reference 2), and a large second nut is required for adequate preload and load-bearing capacity.

However, in the case of Palo Verde, the double-nutting was employed on U-bolts and pipe hangers simply as a locking device to comply with ASME Code NF-4725 (References 5 and 6). The first, or primary, nut in these cases was designed to take the full load of the connection. Thus, the practice at Palo Verde of making both nuts the same size or the second nut half-size is acceptable. In fact, NF-4725 permits locking devices such as nut drilling and wiring and thread upsetting, where no second nut at all is employed. Therefore, the size of the second nut at Palo Verde is not a concern when used as a locking device as described above.

7.0 CONCLUSIONS

The following conclusions were reached as a result of assessing bolting integrity at Palo Verde Units 1, 2 and 3.

1. Because of extensive studies, reinspections, corrective actions and inherent joint design margins at Palo Verde Units 1, 2 and 3, the bolted joint integrity is considered above-average and acceptable for service. The key points are that typical Palo Verde bolted connections are overdesigned, and deficiencies in critical connections have been corrected.
2. Variations in bolt torque from specified AISC values were found in critical friction joint structural bolting during torque checks, especially at Unit 2. Bolt condition and torquing methods contributed to these variations. Similar variations have been found in other studies (Ref. 1) and are not unexpected. All accessible critical joints at Palo Verde were reinspected and are now properly torqued.
3. SCC, overloading and fatigue were considered as possible failure mechanisms due to overtorquing. SCC is not an expected failure mechanism because of Palo Verde bolting generally having hardnesses below the threshold for SCC. (Sustained load derating was implemented in certain cases of high hardness). This conclusion regarding SCC also applies to bolts which were acid cleaned. Fatigue was shown to not be a concern for overtorqued bolts, through use of a generic calculation. It was shown that although a number of overload failures was predicted during preload torquing, that stress relaxation after preload is significant and precludes such failures during the service of properly designed bolts. Therefore, overtorquing is not a problem unless the bolt fails immediately.
4. The effect of undertorquing was evaluated with respect to possible multiple loose bolts in a connection. It was found that fatigue is the most likely failure mechanism of concern for undertorqued bolts.

Detailed typical joint designs for Palo Verde were found to include relatively large margins against fatigue. It was shown that such designs could tolerate the evaluated cases of high cycle fatigue at Palo Verde, even with no preload on the bolts.

5. The double-nutting practice at Palo Verde is acceptable for its intended purpose of locking the primary nut in place, in accordance with ASME Code NF-4725.

8.0 REFERENCES

1. Looram, M. E., "Preload Control for Structural Bolting", presented at Bolting Degradation or Failure in Nuclear Plants Seminar, sponsored by EPRI, Knoxville, TN, Nov. 2-4, 1983.
2. Shigley, J. E., Mechanical Engineering Design, Chapter 7, "The Design of Screws, Fasteners, and Joints", McGraw-Hill, NY, Second Ed., c. 1972.
3. Juvinall, R. C., Engineering Considerations of Stress, Strain, and Strength, McGraw-Hill, NY, p. 310.
4. Bechtel Letter B/SIA-E-49741, MOC350421, W. G. Bingham to J. F. Copeland, Nov. 8, 1984.
5. Bechtel Specification No. 13-PM-204, "Specification for Field Fabrication and Installation of Nuclear Piping Systems for the Arizona Public Service Company Palo Verde Nuclear Generating Station Units 1, 2 and 3", Rev. 13, February 23, 1984.
6. Corner & Lada Co. Inc. Load Capacity Data Sheet for Component Standard Supports, Double Bolt Pipe Clamp, P209A0-27-2, Rev. 1, April 1, 1977.
7. Specification for "Structural Joints Using ASTM A325 or A490 Bolts", AISC, Aug. 14, 1980.
8. NRC Construction Assessment Team (CAT) Report Findings and Responses, Attachment D, II.B.1 and II.B.2, Inspection conducted Sept. 1983.
9. Bechtel Construction Inspection Planning for Job No. 10407, CIP No. 551.0, "Critical Friction-Type High Strength Bolted Connections", issued March 2, 1984.
10. Shiosaka, D. R., "Engineering Evaluation of Nonconforming ASTM A354 Grade BD Studs and Bolts", DER No. 81-14 (and appendices), Sept. 1982.
11. Billy, A. F., "Background and History of the Bolting Degradation or Failure in Nuclear Plants Issue", presented at Bolting Degradation or Failure in Nuclear Plants Seminar, sponsored by EPRI, Knoxville, TN, Nov. 2-4, 1983.
12. Cipolla, R. G., "Fracture Mechanics Based Methodology for Assessing the Integrity of High Strength Bolting Materials", presented at Bolting Degradation or Failure in Nuclear Plants Seminar, sponsored by EPRI, Knoxville, TN, Nov. 2-4, 1983.
13. Dieter, G. E., Jr., Mechanical Metallurgy, McGraw-Hill, NY, c. 1961, p. 23.
14. ASME Boiler and Pressure Vessel Code, Section III, Article XII-1000, "Design Considerations for Bolted Flange Connections", Winter 1983 Addenda.

15. PVNGS FSAR, Section 3.7,3.2, "Determination of Number of Earthquake Cycles", Amendment 4, May 1981.

APPENDIX A
NRC IE INFORMATION NOTICE NO. 82-06
and
NRC IE BULLETIN NO. 82-02

SSINS No.: 6835
Accession No.
8202040130
IN 82-06

UNITED STATES
NUCLEAR REGULATORY COMMISSION
OFFICE OF INSPECTION AND ENFORCEMENT
WASHINGTON, D. C. 20555

March 12, 1982

IE INFORMATION NOTICE NO. 82-06: FAILURE OF STEAM GENERATOR PRIMARY SIDE MANWAY
CLOSURE STUDS

Description of Circumstances:

The Nuclear Regulatory Commission (NRC) was notified by Maine Yankee Atomic Power Company and by Combustion Engineering (CE) that during routine disassembly of a steam generator primary side manway at Maine Yankee, 6 of the 20 manway closure studs failed and another 5 were found by ultrasonic testing to be cracked. These are 1½ x 10 inch studs of SA 540 grade B 24 alloy steel. The studs had been exposed to boric acid from a small primary coolant leak and to Furmanite sealing compound (primary grade) applied in an attempt to seal this leak. The studs exhibited evidence of surface corrosion attack possibly as a result of an interaction associated with stud preload, lubricant, Furmanite and primary coolant leakage environment. A metallurgical analysis to determine the failure mechanism is currently underway at CE. The entire set of studs on the affected steam generator (SG #2) have been replaced and an ultrasonic examination of all primary manway studs on steam generator units 2 and 3 is being performed. Further corrective actions are pending stud failure analysis and its applicability to other primary boundary closures.

In the last few years there have been a significant number of incidents of failed or severely degraded bolts and studs. Examples of the latter; primary coolant pump stud-bolts (Calvert Cliffs and Ft Calhoun) and steam generator primary manway closures studs (Oconee and ANO-1). The failures described were attributed to stress corrosion cracking and corrosion wastage of high strength studs that are difficult to detect.

The NRC has contacted the CE Regulatory Response Group and requested a review of the problem.

This IE information notice is provided as an early notification of a potentially significant matter that is still under review by the NRC staff. If NRC evaluation so indicates, further licensee action may be requested. In the interim, we expect that licensees will review this information for applicability to their facilities.

No written response to this information notice is requested. If you need additional information, please contact the Regional Administrator of the appropriate NRC Regional Office.

Attachment:
Recently issued IE Information Notices

UNITED STATES
NUCLEAR REGULATORY COMMISSION
OFFICE OF INSPECTION AND ENFORCEMENT
WASHINGTON, D. C. 20555

June 2, 1982

IE BULLETIN NO. 82-02: DEGRADATION OF THREADED FASTENERS IN THE REACTOR
COOLANT PRESSURE BOUNDARY OF PWR PLANTS

Addressees:

All pressurized water nuclear power reactor facilities holding an operating license (OL), for action. All other nuclear power reactor facilities holding an operating license or construction permit (CP), for information.

Purpose:

The purpose of this bulletin is to: (1) notify licensees and construction permit holders about incidents of severe degradation of threaded fasteners (bolts and studs) in closures in the reactor coolant pressure boundary (RCPB), and (2) to require appropriate actions. A response to this bulletin is required from pressurized water reactors (PWRs) holding an operating license as discussed below.

Description of Circumstances:

In May 1980, Omaha Public Power District (OPPD) submitted a special maintenance report to the NRC about the significant corrosion wastage experienced with closure studs in the reactor coolant pumps at its Fort Calhoun facility. The corrosion wastage was attributed to boric acid attack as a result of leakage at flexitallic gasketed joints between the pump casing and pump cover. These closure studs are 3.5 inches in diameter, and are manufactured of SA 193-B7 (AISI 4140) low-alloy, high-strength steel. Accordingly, the NRC issued Information Notice No. 80-27 on June 11, 1980 to all PWR licensees about the potential for undetected boric acid corrosion wastage and emphasized the need for supplemental visual inspection of pressure-retaining bolting in pump and valve components. Subsequently, similar occurrences of corrosion wastage from boric acid water leakage have been identified at other PWR plants, as discussed below.

On March 10, 1982, the NRC was notified by Maine Yankee Atomic Power Company and Combustion Engineering (C-E) that during routine disassembly of a steam generator primary manway at Maine Yankee, 6 of the 20 manway closure studs failed and another 5 were found, by ultrasonic examination using specialized techniques, to be cracked. Leakage had been noted from this manway during the current operating cycle and several efforts were made to eliminate the leakage. These efforts involved increasing the joint operating compression through torquing the studs to hydrotest levels and repeatedly injecting Furmanite sealant. Normal plant operation continued until a planned maintenance outage.

Preliminary results of a metallurgical analysis C-E performed on the affected studs have indicated that the failure mode was stress-corrosion cracking (SCC). By Information Notice No. 82-06 (issued March 12, 1982), the Office of Inspection and Enforcement notified all licensees and construction permit holders about this degradation to emphasize the increased potential for studs to fail by the joint action of stud preload, material conditions and a corrosive environment generated by the presence of primary coolant leakage. As a follow-up to the information notice, the utility established that the root cause of leakage was due to an interference contact between the gasket retainer lip and vessel cladding which prevented proper compression of the flexitall gasket during reinstallation of the manway cover. This problem was corrected and all 20 studs were replaced. Magnetic particle and ultrasonic examinations of the studs in manways of the other two steam generators identified no other failures.

In the last several years a significant number of incidents have been reported of bolts and studs that have failed or become severely degraded because of boric acid corrosion wastage or SCC mechanisms. Preliminary results of an NRC staff review of threaded fastener experience in operating nuclear power plants have identified that specific generic actions need to be taken before the study is complete. The staff review identified 44 incidents of threaded fastener degradation since 1964. From Table 1 it can be seen that since 1977, 15 incidents related to primary coolant pressure boundary application have been recorded. These incidents involved 9 PWR plants. Of concern is that degradation and failure of such threaded fasteners constitute a potential loss of RCPB integrity and, in the extreme case, a loss-of-coolant accident could occur, should extensive fastener failures in a pressure-retaining closure not be detected.

In some instances, it has been reported that sealant compounds have been injected into bolted closures in the RCPB as a means of convenient maintenance to control leakage. A review of the limited chemical analysis available on Furmanite indicates it has a variable composition with respect to concentration of chlorine, fluorine, and sulfur which are leachable and well recognized promoters of SCC. Consequently, prolonged exposure of this sealant to leakage and high temperature conditions causing a gradual release of its potentially corrosive ions must be taken into account.

Also, certain lubricants may be formulated with molybdenum disulfide (MoS_2) which contains a significant level of sulfide constituent. Experience suggests that MoS_2 has a pronounced tendency to decompose in the presence of high temperature and moisture conditions to release sulfide which is a known promoter of SCC.

Therefore, care should be exercised in the selection and application of lubricants and injection sealants to minimize the risk of SCC from potentially corrosive ions due to the gradual breakdown and/or synergistic interaction of such materials with prolonged exposure to leakage conditions. This would be of

particular concern for fastener materials made of high-strength low-alloy steels and, austenitic and martensitic stainless steels (i.e., 304, 316, 416, 17-4 PH, etc.) which are known to be susceptible to halogen/sulfide SCC degradation.

The above concerns are further compounded by the fact that under the present ASME Code Section XI inservice inspection rules ultrasonic examination is not required on threaded fasteners in sizes 2 inches and less in diameter (e.g., Table IWB-2500-1). However, except for the reactor coolant pump stud wastage, most failures have occurred in fastener sizes 2 inches and smaller. Furthermore, experience has clearly shown that Code-specified ultrasonic testing (UT) methods are not singularly adequate to detect corrosion wastage conditions. Moreover, the present Code UT procedures are not sufficiently sensitive to detect initiation of stress corrosion cracking (SCC) but requires the use of specialized UT techniques and calibration standards based on notch reflectors simulating critical flaw parameters to enhance reliability of detection. At the present time, visual examination (e.g., IWA 2210, VT-1) appears to be the only method to detect borated water corrosion wastage or erosion-corrosion damage and may require insulation removal and/or disassembly of the component, in some cases, in order to have direct visual access to the threaded fasteners. Therefore, degradation could go undetected when there is no clear evidence of leakage in the surrounding area. Similarly, the reliability of visual examination alone is questionable in detection of SCC initiation of threaded fasteners either in-situ or removed. Accordingly, it is necessary that a combination of nondestructive examination techniques (UT, VT-1, MT, PT) be employed to the maximum extent practical to enhance detection of the degradation mechanisms discussed above.

Actions To Be Taken by PWR Facilities Holding Operating Licenses:

The scope of action items listed below is limited to the RCPB. Included are the threaded fasteners (studs or bolts) in (1) steam generator and pressurizer manway closures, (2) valve bonnets, and pump flange connections installed on lines having a nominal diameter of 6 inches or greater and (3) control rod drive (CRD) flange and pressurizer heater connections that do not have seal welds to provide leak-tight integrity. That is, CRDs having an omega seal weld design are excluded from this bulletin action. The reactor vessel head closure studs are also excluded for those PWR licensees committed to the provisions of Regulatory Guide 1.65, "Materials and Inspection for Reactor Vessel Closure Studs."

Action Item 1 is to be completed prior to the performance of the subsequent action items. Action Item 2 is to be performed within the next cycle, but no later than the completion of the next refueling outage that is initiated after 60 days from the date of this bulletin. The report requested by Action Item 3 is to be submitted within 60 days from the date of this bulletin.

1. Where procedures do not exist, develop and implement maintenance procedures for threaded fastener practices. These procedures should

include, but not limited to the following: (1) maintenance crew training of proper bolting/stud practices, tools application, specifications and requirements, (2) detensioning and retensioning practices (torque iteration), specified tolerances, and other controls for disassembly and reassembly of component closure/seal connections, (3) gasket installation and controls, and (4) retensioning methods and other measures to eliminate reactor coolant leakage during operations.

Quality assurance measures should also be established for proper selection, procurement, and application of fastener lubricants and injection sealant compounds to minimize fastener susceptibility to SCC environments.

2. Threaded fasteners of closure connections, identified in the scope of this bulletin, when opened for component inspection or maintenance shall be removed*, cleaned, and inspected per IWA-2210 and IWA-2220 of ASME Code Section XI (1974 edition or later) before being reused.
3. NRC Information Notice Nos. 80-27 and 82-06, and similar INPO (Institute of Nuclear Power Operations) correspondence (with recommendations) have been issued in regard to corrosion problems associated with bolts/studs in RCPB closures (INPO/NSAC SER 81-12). To assist the Nuclear Regulatory Commission in its ongoing review and assessment of the scope of the problem you are asked to provide the following information for closures and connections within the scope of this bulletin:
 - a. Identify those bolted closures of the RCPB that have experienced leakage, particularly those locations where leakage occurred during the most recent plant operating cycle. Describe the inspections made and corrective measures taken to eliminate the problem. If the leakage was attributed to gasket failure or its design, so indicate.
 - b. Identify those closures and connections, if any, where fastener lubricants and injection sealant materials have been or are being used and report on plant experience with their application particularly any instances of SCC of fasteners. Include types and composition of materials used.
4. A written report signed under oath or affirmation under provisions of Section 182a, Atomic Energy Act of 1954 as amended, shall be submitted to the Regional Administrator of the appropriate NRC Regional Office within 60 days following the completion of the outage during which Action Item 2 was performed. The report is to include:
 - a. A statement that Action Item 1 has been completed.

* Fasteners "seized" or designed with interference fit, may be inspected in place.

- b. Identification of the specific connections examined as required by Action Item 2.
 - c. The results of the examinations performed on the threaded fasteners as required by Action Item 2. If no degradation was observed for a particular connection, a statement to that effect, identification of the connection and, whether the fasteners were examined in place or removed is all that is required. If degradation was observed, the report should provide detailed information.
5. A written report signed under oath or affirmation under provisions of Section 182a, Atomic Energy Act of 1954 as amended, shall be submitted to the Regional Administrator of the appropriate NRC Regional Office within 60 days of the date of this bulletin. The report is to provide the information requested by Action Item 3.

Potential occupational exposure of personnel as a result of the above requirements should be considered in the program formulation process in an effort to maintain incurred exposures as low as reasonably achievable. Personnel exposure-savings techniques such as use of steam generator primary manway cover-handling fixtures offer substantial time and man-rem savings.

This request for information was approved by the Office of Management and Budget under clearance number 3150-0086. Comments on burden and duplication should be directed to the Office of Management and Budget, Reports Management, Room 3208, New Executive Office Building, Washington, D.C. 20503.

While no specific request or requirement is intended, the following information would be helpful to the NRC in evaluating the cost of this bulletin:

1. Staff time to perform requested inspection.
2. Radiation exposure attributed to requested inspections.
3. Staff time spent to prepare written responses.

If you have any questions regarding this matter, please contact the Regional Administrator of the appropriate NRC Regional Office, or this office.

Richard C. DeYoung, Director
Office of Inspection and Enforcement

Technical Contact: W. J. Collins
301-492-4780

Attachments:

1. Table 1
2. List of Recently Issued IE Bulletins

TABLE 1. SUMMARY OF DEGRADED THREADED FASTENERS IN REACTOR COOLANT PRESSURE BOUNDARY

Degraded Reactor Coolant Pressure Boundary Threaded Fasteners	No. of Reported Incidents	Plants (Year Incident Reported) & Reactor Vendor	Mode of Failure *
Pressurizer manway closure studs	2	Calvert Cliffs 2 (1981) C-E St. Lucie 1 (1978) C-E	BC BC
Steam generator manway closure studs	7	Maine Yankee (1982) C-E Oconee 3 (1980) B&W Arkansas 1 (1978) B&W Arkansas 1 (1980) B&W Calvert Cliffs 1 (1980) C-E St. Lucie 1 (1977) C-E San Onofre 1 (1977) W	SC SC BC SC BC BC SC
Reactor coolant pump closure studs	5	Ft. Calhoun (1980) C-E Calvert Cliffs 1 (1980) C-E Calvert Cliffs 2 (1981) C-E Oconee 3 (1981) B&W Oconee 2 (1981) B&W	BC BC BC BC BC
Emergency injection check valve studs	1	Calvert Cliffs 2 (1981) C-E	BC

* C = stress corrosion; BC = borated water corrosion.

APPENDIX B

PALO VERDE UNIT 1 HIGH STRENGTH BOLT TORQUE CHECK
FOR CRITICAL FRICTION FASTENERS

PALO VERDE UNIT 1 HIGH STRENGTH BOLT TORQUE

INSP. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONN. NO.	BOLT NO.	NUT	ROTAT
3-7-84	A325	0.875	535	34	01		0.750
3-2-84	A325	0.875	529	04	01		0.333
3-7-84	A325	0.875	535	25	05		0.333
3-7-84	A325	0.875	535	25	04		0.333
3-9-84	A490	1.000	532	24	06		0.271
3-9-84	A490	1.000	532	24	07		0.250
3-5-84	A325	0.875	532	06	03		0.250
3-7-84	A325	0.875	533	10	07		0.250
3-5-84	A325	0.875	536	14	01		0.250
3-9-84	A490	1.000	532	24	09		0.250
3-6-84	A325	0.875	532	17	07		0.250
3-2-84	A325	0.875	529	04	02		0.250
3-5-84	A325	0.875	536	14	02		0.250
3-8-84	A325	0.875	533	31	07		0.167
3-2-84	A325	0.875	529	06	02		0.167
3-6-84	A325	0.875	532	19	05		0.167
3-9-84	A490	1.000	532	24	08		0.167
3-6-84	A325	0.875	532	26	04		0.167
3-7-84	A325	0.875	533	14	01		0.167
3-5-84	A325	0.875	530	01	03		0.167
3-5-84	A325	0.875	532	06	02		0.167
3-6-84	A325	0.875	532	26	02		0.167
3-9-84	A490	0.875	535	33	01		0.125
3-6-84	A325	0.875	532	14	01		0.111
3-7-84	A325	0.875	535	37	05		0.083
3-8-84	A325	0.875	533	34	02		0.083
3-6-84	A325	0.875	533	02	09		0.083
3-7-84	A325	0.875	533	10	06		0.083
3-5-84	A325	0.875	532	05	08		0.083
3-6-84	A325	0.875	532	19	06		0.083
3-9-84	A490	1.000	532	06	07		0.083
3-9-84	A490	1.000	532	24	10		0.083
3-7-84	A325	0.875	535	08	06		0.083
3-5-84	A325	0.875	532	06	04		0.083
3-9-84	A490	0.875	535	31	04		0.083
3-6-84	A325	0.875	532	26	01		0.083
3-6-84	A325	0.875	532	17	05		0.083
3-7-84	A325	0.875	535	34	03		0.083
3-6-84	A325	0.875	532	16	02		0.083
3-7-84	A325	0.875	535	34	02		0.083
3-6-84	A325	0.875	532	16	03		0.083
3-8-84	A325	0.875	533	34	07		0.083
3-6-84	A325	0.875	532	16	05		0.083
3-8-84	A325	0.875	533	04	01		0.083
3-6-84	A325	0.875	533	02	08		0.083
3-5-84	A325	0.875	531	01	07		0.083
3-5-84	A325	0.875	532	06	01		0.083
3-6-84	A325	0.875	532	26	03		0.083
3-6-84	A325	0.875	532	17	01		0.083
3-8-84	A325	0.875	533	02	03		0.083
3-8-84	A325	0.875	533	27	01		0.083
3-6-84	A325	0.875	532	26	05		0.083
3-8-84	A325	0.875	533	04	03		0.083

3-8-84	A325	0.875	536	16	02	0.083
3-5-84	A325	0.875	532	06	06	0.083
3-8-84	A325	0.875	533	34	08	0.083
3-6-84	A325	0.875	532	16	04	0.083
3-6-84	A325	0.875	532	16	01	0.083
3-5-84	A325	0.875	532	01	01	0.083
3-6-84	A325	0.875	533	02	07	0.083
3-7-84	A325	0.875	533	10	01	0.056
3-7-84	A325	0.875	533	10	08	0.056
3-6-84	A325	0.875	533	01	01	0.042
3-9-84	A490	0.875	535	15	05	0.042
3-8-84	A325	0.875	533	28	06	0.042
3-8-84	A325	0.875	533	01	01	0.042
3-6-84	A325	0.875	532	17	04	0.042
3-6-84	A325	0.875	532	27	02	0.042
3-6-84	A325	0.875	532	17	02	0.042
3-7-84	A325	0.875	535	35	01	0.042
3-8-84	A325	0.875	533	24	01	0.042
3-6-84	A325	0.875	532	26	07	0.042
3-7-84	A325	0.875	535	37	01	0.042
3-7-84	A325	0.875	535	37	04	0.042
3-5-84	A325	0.875	530	01	05	0.042
3-7-84	A325	0.875	533	07	07	0.042
3-8-84	A325	0.875	533	24	07	0.042
3-6-84	A325	0.875	532	19	08	0.042
3-6-84	A325	0.875	534	07	01	0.042
3-8-84	A325	0.875	536	16	01	0.042
3-9-84	A490	0.875	535	33	09	0.042
3-5-84	A325	0.875	532	01	02	0.042
3-8-84	A325	0.875	536	12	01	0.042
3-8-84	A325	0.875	533	27	02	0.042
3-5-84	A325	0.875	532	06	05	0.042
3-7-84	A325	0.875	535	07	08	0.042
3-8-84	A325	0.875	536	12	03	0.042
3-5-84	A325	0.875	532	01	05	0.042
3-8-84	A325	0.875	536	11	01	0.042
3-6-84	A325	0.875	532	20	01	0.042
3-8-84	A325	0.875	536	11	03	0.042
3-5-84	A325	0.875	531	01	01	0.042
3-8-84	A325	0.875	533	33	02	0.042
3-8-84	A325	0.875	533	27	06	0.042
3-8-84	A325	0.875	533	33	01	0.042
3-7-84	A325	0.875	535	37	06	0.042
3-5-84	A325	0.875	532	05	06	0.042
3-8-84	A325	0.875	533	33	03	0.042
3-7-84	A325	0.875	533	10	02	0.042
3-7-84	A325	0.875	535	28	06	0.042
3-5-84	A325	0.875	532	02	01	0.031
3-5-84	A325	0.875	530	01	04	0.028
3-5-84	A325	0.875	530	01	02	0.028
3-5-84	A325	0.875	530	01	03	0.028
3-5-84	A325	0.875	530	01	04	0.028
3-7-84	A325	0.875	535	07	02	0.021
3-7-84	A325	0.875	535	37	03	0.021
3-5-84	A325	0.875	532	05	05	
3-9-84	A490	0.875	535	24	07	

3-6-84	A325	0.875	534	22	06	0.021
3-9-84	A490	0.875	535	24	06	0.021
3-9-84	A490	0.875	535	24	04	0.021
3-7-84	A325	0.875	535	37	02	0.021
3-8-84	A325	0.875	533	34	06	0.021
3-7-84	A325	0.875	535	35	03	0.021
3-8-84	A325	0.875	533	34	01	0.021
3-7-84	A325	0.875	535	25	06	0.021
3-8-84	A325	0.875	533	33	08	0.021
3-7-84	A325	0.875	535	12	05	0.021
3-8-84	A325	0.875	533	31	05	0.021
3-7-84	A325	0.875	535	07	14	0.021
3-8-84	A325	0.875	536	13	03	0.021
3-7-84	A325	0.875	535	07	13	0.021
3-6-84	A325	0.875	534	22	04	0.021
3-7-84	A325	0.875	535	07	12	0.021
3-8-84	A325	0.875	533	24	05	0.021
3-7-84	A325	0.875	535	07	11	0.021
3-8-84	A325	0.875	533	27	04	0.021
3-7-84	A325	0.875	535	07	10	0.021
3-7-84	A325	0.875	533	07	06	0.021
3-7-84	A325	0.875	535	07	09	0.021
3-9-84	A490	0.875	535	24	05	0.021
3-7-84	A325	0.875	535	07	07	0.021
3-8-84	A325	0.875	533	34	03	0.021
3-7-84	A325	0.875	535	07	04	0.021
3-8-84	A325	0.875	533	31	06	0.021
3-7-84	A325	0.875	535	07	01	0.021
3-8-84	A325	0.875	536	11	02	0.021
3-6-84	A325	0.875	533	02	06	0.021
3-8-84	A325	0.875	533	27	05	0.021
3-6-84	A325	0.875	532	26	10	0.021
3-7-84	A325	0.875	535	37	07	0.021
3-6-84	A325	0.875	532	26	06	0.021
3-5-84	A325	0.875	531	01	02	0.021
3-6-84	A325	0.875	532	15	02	0.021
3-8-84	A325	0.875	536	12	02	0.021
3-6-84	A325	0.875	532	13	04	0.021
3-9-84	A490	0.875	535	15	06	0.021
3-7-84	A325	0.875	533	08	07	0.021
3-5-84	A325	0.875	536	14	03	0.021
3-6-84	A325	0.875	532	13	02	0.021
3-5-84	A325	0.875	532	02	09	0.016
3-5-84	A325	0.875	532	01	08	0.016
3-7-84	A325	0.875	535	14	07	0.000
3-7-84	A325	0.875	535	26	03	0.000
3-7-84	A325	0.875	535	26	04	0.000
3-5-84	A325	0.875	532	07	06	0.000
3-7-84	A325	0.875	535	26	05	0.000
3-5-84	A325	0.875	532	07	08	0.000
3-7-84	A325	0.875	535	26	06	0.000
3-5-84	A325	0.875	532	08	01	0.000
3-7-84	A325	0.875	535	26	07	0.000
3-5-84	A325	0.875	532	08	03	0.000
3-7-84	A325	0.875	535	28	01	0.000
3-5-84	A325	0.875	532	08	05	0.000



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3-7-84	A325	0.875	535	28	02	0.000
3-5-84	A325	0.875	532	05	01	0.000
3-7-84	A325	0.875	535	28	03	0.000
3-5-84	A325	0.875	532	05	03	0.000
3-7-84	A325	0.875	535	28	04	0.000
3-5-84	A325	0.875	532	07	04	0.000
3-7-84	A325	0.875	535	28	05	0.000
3-5-84	A325	0.875	532	05	07	0.000
3-5-84	A325	0.875	530	01	06	0.000
3-5-84	A325	0.875	532	05	09	0.000
3-7-84	A325	0.875	535	28	07	0.000
3-5-84	A325	0.875	530	01	02	0.000
3-5-84	A325	0.875	530	01	05	0.000
3-5-84	A325	0.875	530	01	06	0.000
3-7-84	A325	0.875	535	35	02	0.000
3-5-84	A325	0.875	530	01	04	0.000
3-5-84	A325	0.875	532	03	02	0.000
3-5-84	A325	0.875	532	09	02	0.000
3-7-84	A325	0.875	535	35	04	0.000
3-5-84	A325	0.875	532	09	04	0.000
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3-5-84	A325	0.875	532	09	06	0.000
3-7-84	A325	0.875	535	35	06	0.000
3-6-84	A325	0.875	534	20	02	0.000
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3-6-84	A325	0.875	534	21	01	0.000
3-5-84	A325	0.875	532	02	08	0.000
3-6-84	A325	0.875	534	21	03	0.000
3-5-84	A325	0.875	530	01	03	0.000
3-6-84	A325	0.875	534	21	05	0.000
3-5-84	A325	0.875	530	01	02	0.000
3-6-84	A325	0.875	534	21	07	0.000
3-5-84	A325	0.875	530	01	01	0.000
3-6-84	A325	0.875	534	21	01	0.000
3-5-84	A325	0.875	532	02	07	0.000
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3-7-84	A325	0.875	535	37	08	0.000
3-6-84	A325	0.875	534	21	05	0.000
3-5-84	A325	0.875	530	01	08	0.000
3-6-84	A325	0.875	534	21	07	0.000
3-5-84	A325	0.875	530	01	07	0.000
3-6-84	A325	0.875	534	21	09	0.000
3-5-84	A325	0.875	530	01	06	0.000
3-6-84	A325	0.875	534	21	11	0.000
3-7-84	A325	0.875	535	34	04	0.000
3-6-84	A325	0.875	534	21	13	0.000
3-7-84	A325	0.875	535	34	05	0.000
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3-7-84	A325	0.875	535	34	06	0.000
3-6-84	A325	0.875	534	22	03	0.000
3-7-84	A325	0.875	535	34	07	0.000
3-6-84	A325	0.875	534	22	05	0.000

3-7-84	A325	0.875	533	07	01	0.000
3-6-84	A325	0.875	534	22	07	0.000
3-7-84	A325	0.875	533	07	02	0.000
3-6-84	A325	0.875	534	22	09	0.000
3-7-84	A325	0.875	533	07	03	0.000
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3-7-84	A325	0.875	533	07	04	0.000
3-6-84	A325	0.875	534	22	13	0.000
3-7-84	A325	0.875	533	07	05	0.000
3-6-84	A325	0.875	534	24	01	0.000
3-5-84	A325	0.875	532	02	06	0.000
3-6-84	A325	0.875	534	24	03	0.000
3-5-84	A325	0.875	530	01	05	0.000
3-6-84	A325	0.875	534	24	05	0.000
3-7-84	A325	0.875	533	07	08	0.000
3-6-84	A325	0.875	534	24	07	0.000
3-7-84	A325	0.875	533	07	09	0.000
3-6-84	A325	0.875	534	17	02	0.000
3-7-84	A325	0.875	533	07	10	0.000
3-6-84	A325	0.875	534	17	04	0.000
3-7-84	A325	0.875	533	08	01	0.000
3-6-84	A325	0.875	534	17	06	0.000
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3-6-84	A325	0.875	534	14	03	0.000
3-7-84	A325	0.875	533	08	04	0.000
3-6-84	A325	0.875	534	14	05	0.000
3-7-84	A325	0.875	533	08	05	0.000
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3-7-84	A325	0.875	533	08	06	0.000
3-6-84	A325	0.875	534	16	01	0.000
3-5-84	A325	0.875	532	02	05	0.000
3-6-84	A325	0.875	534	16	03	0.000
3-7-84	A325	0.875	533	08	08	0.000
3-6-84	A325	0.875	534	16	05	0.000
3-7-84	A325	0.875	533	12	01	0.000
3-6-84	A325	0.875	534	16	07	0.000
3-7-84	A325	0.875	533	12	02	0.000
3-6-84	A325	0.875	534	13	01	0.000
3-7-84	A325	0.875	533	12	03	0.000
3-6-84	A325	0.875	534	13	03	0.000
3-7-84	A325	0.875	533	12	04	0.000
3-6-84	A325	0.875	534	13	05	0.000
3-7-84	A325	0.875	533	12	05	0.000
3-6-84	A325	0.875	534	13	07	0.000
3-7-84	A325	0.875	533	12	06	0.000
3-6-84	A325	0.875	534	10	02	0.000
3-7-84	A325	0.875	533	12	07	0.000
3-6-84	A325	0.875	534	10	04	0.000
3-7-84	A325	0.875	533	12	08	0.000
3-6-84	A325	0.875	534	10	06	0.000
3-5-84	A325	0.875	530	01	04	0.000
3-6-84	A325	0.875	534	10	08	0.000
3-5-84	A325	0.875	530	01	03	0.000
3-6-84	A325	0.875	534	12	01	0.000



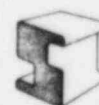
**STRUCTURAL
INTEGRITY
ASSOCIATES, INC.**

3-7-84	A325	0.875	533	10	03	0.000
3-6-84	A325	0.875	534	12	03	0.000
3-7-84	A325	0.875	533	10	04	0.000
3-6-84	A325	0.875	534	12	05	0.000
3-7-84	A325	0.875	533	10	05	0.000
3-6-84	A325	0.875	534	12	07	0.000
3-5-84	A325	0.875	530	01	02	0.000
3-6-84	A325	0.875	534	06	01	0.000
3-5-84	A325	0.875	530	01	01	0.000
3-6-84	A325	0.875	534	06	03	0.000
3-5-84	A325	0.875	530	01	05	0.000
3-6-84	A325	0.875	534	06	05	0.000
3-7-84	A325	0.875	533	13	01	0.000
3-6-84	A325	0.875	534	06	07	0.000
3-7-84	A325	0.875	533	13	02	0.000
3-6-84	A325	0.875	534	06	09	0.000
3-7-84	A325	0.875	533	13	03	0.000
3-6-84	A325	0.875	534	04	02	0.000
3-7-84	A325	0.875	533	13	04	0.000
3-6-84	A325	0.875	534	04	04	0.000
3-7-84	A325	0.875	533	13	05	0.000
3-6-84	A325	0.875	534	03	02	0.000
3-7-84	A325	0.875	533	13	06	0.000
3-6-84	A325	0.875	534	03	04	0.000
3-5-84	A325	0.875	530	01	01	0.000
3-6-84	A325	0.875	534	07	02	0.000
3-7-84	A325	0.875	533	14	02	0.000
3-6-84	A325	0.875	534	07	04	0.000
3-7-84	A325	0.875	533	14	03	0.000
3-6-84	A325	0.875	534	07	06	0.000
3-7-84	A325	0.875	533	14	04	0.000
3-6-84	A325	0.875	532	10	01	0.000
3-7-84	A325	0.875	533	14	05	0.000
3-6-84	A325	0.875	532	10	03	0.000
3-7-84	A325	0.875	533	14	07	0.000
3-6-84	A325	0.875	532	10	05	0.000
3-7-84	A325	0.875	533	14	08	0.000
3-6-84	A325	0.875	532	10	07	0.000
3-7-84	A325	0.875	533	15	01	0.000
3-6-84	A325	0.875	532	10	09	0.000
3-7-84	A325	0.875	533	15	02	0.000
3-6-84	A325	0.875	532	12	02	0.000
3-7-84	A325	0.875	533	15	03	0.000
3-6-84	A325	0.875	532	12	04	0.000
3-7-84	A325	0.875	533	15	04	0.000
3-6-84	A325	0.875	532	12	06	0.000
3-7-84	A325	0.875	533	15	05	0.000
3-5-84	A325	0.875	532	07	01	0.000
3-7-84	A325	0.875	533	15	06	0.000
3-5-84	A325	0.875	532	04	09	0.000
3-7-84	A325	0.875	533	16	01	0.000
3-6-84	A325	0.875	532	13	06	0.000
3-7-84	A325	0.875	533	16	02	0.000
3-6-84	A325	0.875	532	13	08	0.000
3-7-84	A325	0.875	533	16	03	0.000
3-6-84	A325	0.875	532	14	02	0.000



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3-7-84	A325	0.875	533	16	04	0.000
3-6-84	A325	0.875	532	14	04	0.000
3-7-84	A325	0.875	533	16	05	0.000
3-6-84	A325	0.875	532	14	06	0.000
3-7-84	A325	0.875	533	16	06	0.000
3-5-84	A325	0.875	530	01	07	0.000
3-7-84	A325	0.875	533	18	01	0.000
3-5-84	A325	0.875	530	01	06	0.000
3-7-84	A325	0.875	533	18	02	0.000
3-6-84	A325	0.875	532	17	06	0.000
3-7-84	A325	0.875	533	18	03	0.000
3-6-84	A325	0.875	532	17	08	0.000
3-7-84	A325	0.875	533	18	04	0.000
3-5-84	A325	0.875	530	01	02	0.000
3-7-84	A325	0.875	533	18	05	0.000
3-5-84	A325	0.875	530	01	05	0.000
3-7-84	A325	0.875	533	18	06	0.000
3-6-84	A325	0.875	532	15	01	0.000
3-7-84	A325	0.875	533	18	07	0.000
3-6-84	A325	0.875	532	15	03	0.000
3-7-84	A325	0.875	533	18	08	0.000
3-6-84	A325	0.875	532	15	05	0.000
3-7-84	A325	0.875	533	19	01	0.000
3-6-84	A325	0.875	532	15	07	0.000
3-7-84	A325	0.875	533	19	02	0.000
3-6-84	A325	0.875	532	18	01	0.000
3-7-84	A325	0.875	533	19	03	0.000
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3-8-84	A325	0.875	533	29	01	0.000
3-6-84	A325	0.875	532	18	05	0.000
3-8-84	A325	0.875	533	29	02	0.000
3-6-84	A325	0.875	532	19	01	0.000
3-8-84	A325	0.875	533	29	03	0.000
3-6-84	A325	0.875	532	19	03	0.000
3-8-84	A325	0.875	533	29	04	0.000
3-5-84	A325	0.875	530	01	03	0.000
3-8-84	A325	0.875	533	29	05	0.000
3-6-84	A325	0.875	532	19	07	0.000
3-8-84	A325	0.875	533	29	06	0.000
3-5-84	A325	0.875	530	01	09	0.000
3-8-84	A325	0.875	533	30	01	0.000
3-6-84	A325	0.875	532	20	03	0.000
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3-6-84	A325	0.875	532	20	05	0.000
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3-6-84	A325	0.875	532	23	01	0.000
3-8-84	A325	0.875	533	30	04	0.000
3-6-84	A325	0.875	532	23	03	0.000
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3-6-84	A325	0.875	532	23	07	0.000
3-8-84	A325	0.875	533	31	01	0.000
3-6-84	A325	0.875	532	23	09	0.000
3-8-84	A325	0.875	533	31	02	0.000
3-5-84	A325	0.875	530	01	08	0.000



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3-8-84	A325	0.875	533	31	03	0.000
3-5-84	A325	0.875	530	01	06	0.000
3-8-84	A325	0.875	533	31	04	0.000
3-5-84	A325	0.875	530	01	02	0.000
3-8-84	A325	0.875	533	26	05	0.000
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3-8-84	A325	0.875	533	26	06	0.000
3-6-84	A325	0.875	532	26	09	0.000
3-8-84	A325	0.875	533	26	07	0.000
3-6-84	A325	0.875	532	27	01	0.000
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3-6-84	A325	0.875	532	27	03	0.000
3-5-84	A325	0.875	530	01	08	0.000
3-6-84	A325	0.875	532	27	05	0.000
3-5-84	A325	0.875	530	01	07	0.000
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3-8-84	A325	0.875	533	27	03	0.000
3-6-84	A325	0.875	533	01	04	0.000
3-5-84	A325	0.875	532	02	04	0.000
3-6-84	A325	0.875	533	02	01	0.000
3-5-84	A325	0.875	532	02	03	0.000
3-6-84	A325	0.875	533	02	03	0.000
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3-6-84	A325	0.875	533	02	05	0.000
3-8-84	A325	0.875	533	02	01	0.000
3-5-84	A325	0.875	533	28	05	0.000
3-8-84	A325	0.875	530	01	02	0.000
3-5-84	A325	0.875	533	28	03	0.000
3-8-84	A325	0.875	533	01	03	0.000
3-6-84	A325	0.875	533	28	03	0.000
3-8-84	A325	0.875	533	03	01	0.000
3-6-84	A325	0.875	533	28	04	0.000
3-8-84	A325	0.875	533	03	03	0.000
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3-5-84	A325	0.875	533	03	07	0.000
3-6-84	A325	0.875	530	01	04	0.000
3-8-84	A325	0.875	533	03	09	0.000
3-7-84	A325	0.875	533	24	02	0.000
3-8-84	A325	0.875	535	03	01	0.000
3-7-84	A325	0.875	533	24	03	0.000
3-8-84	A325	0.875	535	03	03	0.000
3-7-84	A325	0.875	533	24	04	0.000
3-5-84	A325	0.875	535	03	05	0.000
3-7-84	A325	0.875	532	02	02	0.000
3-8-84	A325	0.875	535	03	07	0.000
3-7-84	A325	0.875	533	24	06	0.000
3-8-84	A325	0.875	535	06	02	0.000
3-5-84	A325	0.875	530	01	03	0.000
3-7-84	A325	0.875	535	06	04	0.000
3-8-84	A325	0.875	533	24	08	0.000
3-7-84	A325	0.875	535	06	06	0.000
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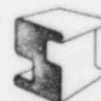


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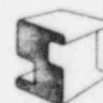
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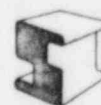
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3-9-84	A325	0.875	535	22	03	0.000
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3-9-84	A325	0.875	535	22	04	0.000
3-6-84	A325	0.875	532	19	04	0.000
3-9-84	A325	0.875	535	22	05	0.000
3-6-84	A325	0.875	532	20	04	0.000
3-9-84	A325	0.875	535	22	06	0.000
3-6-84	A325	0.875	532	23	05	0.000
3-9-84	A325	0.875	535	22	07	0.000
3-5-84	A325	0.875	530	01	03	0.000
3-9-84	A490	0.875	535	29	01	0.000
3-5-84	A325	0.875	530	01	07	0.000
3-9-84	A490	0.875	535	29	02	0.000
3-6-84	A325	0.875	533	01	05	0.000
3-9-84	A490	0.875	535	29	03	0.000
3-5-84	A325	0.875	530	01	04	0.000
3-9-84	A490	0.875	535	29	04	0.000
3-6-84	A325	0.875	533	03	06	0.000

3-9-84	A490	0.875	535	29	05	0.000
3-7-84	A325	0.875	535	03	04	0.000
3-9-84	A490	0.875	535	29	06	0.000
3-7-84	A325	0.875	535	06	05	0.000
3-9-84	A490	0.875	535	29	07	0.000
3-7-84	A325	0.875	535	06	13	0.000
3-9-84	A490	0.875	535	30	01	0.000
3-5-84	A325	0.875	530	01	02	0.000
3-9-84	A490	0.875	535	30	02	0.000
3-7-84	A325	0.875	535	08	02	0.000
3-9-84	A490	0.875	535	30	03	0.000
3-7-84	A325	0.875	535	12	03	0.000
3-9-84	A490	0.875	535	30	04	0.000
3-7-84	A325	0.875	535	13	04	0.000
3-9-84	A490	0.875	535	30	05	0.000
3-7-84	A325	0.875	535	13	12	0.000
3-9-84	A490	0.875	535	30	06	0.000
3-7-84	A325	0.875	535	17	06	0.000
3-9-84	A490	0.875	535	30	07	0.000
3-5-84	A325	0.875	531	01	04	0.000
3-9-84	A490	0.875	535	40	01	0.000
3-7-84	A325	0.875	535	25	01	0.000
3-9-84	A490	0.875	535	40	02	0.000
3-7-84	A325	0.875	535	20	02	0.000
3-9-84	A490	0.875	535	40	03	0.000
3-5-84	A325	0.875	532	07	05	0.000
3-9-84	A490	0.875	535	40	04	0.000
3-5-84	A325	0.875	530	01	05	0.000
3-9-84	A490	0.875	535	40	05	0.000
3-6-84	A325	0.875	534	20	01	0.000
3-9-84	A490	0.875	535	31	01	0.000
3-6-84	A325	0.875	534	21	02	0.000
3-9-84	A490	0.875	535	31	02	0.000
3-5-84	A325	0.875	532	07	03	0.000
3-9-84	A490	0.875	535	31	03	0.000
3-6-84	A325	0.875	534	24	06	0.000
3-2-84	A325	0.875	530	05	03	0.000
3-6-84	A325	0.875	534	14	08	0.000
3-9-84	A490	0.875	535	31	05	0.000
3-6-84	A325	0.875	534	10	01	0.000
3-9-84	A490	0.875	535	31	06	0.000
3-6-84	A325	0.875	534	12	08	0.000
3-9-84	A490	0.875	535	31	07	0.000
3-6-84	A325	0.875	534	03	03	0.000
3-9-84	A490	0.875	535	32	01	0.000
3-6-84	A325	0.875	532	10	08	0.000
3-9-84	A490	0.875	535	32	02	0.000
3-5-84	A325	0.875	530	01	01	0.000
3-9-84	A490	0.875	535	32	03	0.000
3-5-84	A325	0.875	530	01	01	0.000
3-9-84	A490	0.875	535	32	04	0.000
3-6-84	A325	0.875	532	18	06	0.000
3-9-84	A490	0.875	535	32	05	0.000
3-6-84	A325	0.875	532	23	02	0.000
3-9-84	A490	0.875	535	32	06	0.000
3-6-84	A325	0.875	532	26	08	0.000



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3-9-84	A490	0.875	535	32	07	0.000
3-6-84	A325	0.875	533	02	04	0.000
3-2-84	A325	0.875	530	05	02	0.000
3-6-84	A325	0.875	533	03	10	0.000
3-9-84	A490	0.875	535	33	02	0.000
3-7-84	A325	0.875	535	06	09	0.000
3-9-84	A490	0.875	535	33	03	0.000
3-5-84	A325	0.875	532	03	07	0.000
3-9-84	A490	0.875	535	33	04	0.000
3-7-84	A325	0.875	535	12	07	0.000
3-9-84	A490	0.875	535	33	05	0.000
3-7-84	A325	0.875	535	17	02	0.000
3-9-84	A490	0.875	535	33	06	0.000
3-7-84	A325	0.875	535	14	11	0.000
3-9-84	A490	0.875	535	33	07	0.000
3-7-84	A325	0.875	535	20	06	0.000
3-9-84	A490	0.875	535	33	08	0.000
3-5-84	A325	0.875	530	01	05	0.000
3-2-84	A325	0.875	530	05	01	0.000
3-6-84	A325	0.875	534	21	10	0.000
3-9-84	A490	0.875	535	33	10	0.000
3-6-84	A325	0.875	534	17	07	0.000
3-9-84	A490	0.875	535	33	11	0.000
3-6-84	A325	0.875	534	10	09	0.000
3-9-84	A490	0.875	535	33	12	0.000
3-6-84	A325	0.875	534	07	07	0.000
3-9-84	A490	0.875	535	33	13	0.000
3-6-84	A325	0.875	532	17	03	0.000
3-9-84	A490	0.875	535	33	14	0.000
3-5-84	A325	0.875	530	01	01	0.000
3-9-84	A490	0.875	535	38	01	0.000
3-5-84	A325	0.875	530	01	06	0.000
3-9-84	A490	0.875	535	38	02	0.000
3-7-84	A325	0.875	535	06	01	0.000
3-9-84	A490	0.875	535	38	03	0.000
3-5-84	A325	0.875	530	01	01	0.000
3-9-84	A490	0.875	535	38	04	0.000
3-7-84	A325	0.875	535	14	03	0.000
3-9-84	A490	0.875	535	38	05	0.000
3-5-84	A325	0.875	532	08	04	0.000
3-9-84	A490	0.875	535	38	06	0.000
3-6-84	A325	0.875	534	22	12	0.000
3-9-84	A490	0.875	535	38	07	0.000
3-6-84	A325	0.875	534	06	08	0.000
3-2-84	A325	0.875	529	05	02	0.000
3-6-84	A325	0.875	532	15	06	0.000
3-2-84	A325	0.875	529	05	01	0.000
3-6-84	A325	0.875	533	03	02	0.000
3-2-84	A325	0.875	529	03	02	0.000
3-7-84	A325	0.875	535	13	08	0.000
3-2-84	A325	0.875	529	03	01	0.000
3-6-84	A325	0.875	534	21	02	0.000
3-2-84	A325	0.875	529	02	02	0.000
3-6-84	A325	0.875	532	13	01	0.000
3-9-84	A490	1.000	532	06	04	0.000
3-7-84	A325	0.875	535	07	03	0.000



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3-9-84	A490	1.000	532	06	05	0.000
3-6-84	A325	0.875	534	16	08	0.000
3-5-84	A325	0.875	530	01	07	0.000
3-6-84	A325	0.875	532	23	10	0.000
3-9-84	A490	1.000	532	06	06	0.000
3-2-84	A325	0.875	529	02	01	0.000

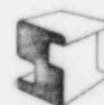
PALO VERDE UNIT 1 HIGH STRENGTH BOLT TORQUE

INSP. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONN. NO.	BOLT NO.	NUT	ROTAT
3-14-84	A325	0.875	536	02	01		1.083
3-19-84	A325	0.875	535	11	06		0.500
3-19-84	A325	0.875	535	38	05		0.500
3-19-84	A325	0.875	535	11	05		0.500
3-12-84	A325	1.000	530	09	02		0.333
3-19-84	A325	0.875	535	38	02		0.333
3-12-84	A325	0.875	530	17	07		0.333
3-19-84	A325	0.875	535	05	04		0.333
3-19-84	A325	0.875	535	38	03		0.292
3-12-84	A325	0.875	532	11	03		0.278
3-13-84	A325	0.875	531	05	03		0.271
3-19-84	A325	0.875	535	38	04		0.250
3-12-84	A325	0.875	532	16	06		0.250
3-12-84	A325	0.875	530	17	06		0.250
3-19-84	A325	0.875	535	38	07		0.250
3-12-84	A325	1.000	530	09	03		0.250
3-19-84	A325	0.875	535	38	06		0.250
3-12-84	A325	1.000	530	07	04		0.250
3-19-84	A325	0.875	535	11	01		0.208
3-19-84	A325	0.875	535	11	04		0.208
3-12-84	A325	0.875	530	17	04		0.167
3-12-84	A325	1.000	530	09	04		0.167
3-19-84	A325	0.875	535	11	02		0.167
3-19-84	A325	0.875	535	11	07		0.167
3-12-84	A325	1.000	530	09	05		0.167
3-12-84	A325	0.875	530	13	06		0.167
3-12-84	A325	1.000	530	07	09		0.167
3-19-84	A325	0.875	535	11	09		0.167
3-12-84	A325	0.875	532	11	03		0.167
3-12-84	A325	0.875	530	17	01		0.167
3-12-84	A325	0.875	532	17	05		0.167
3-14-84	A325	0.875	536	11	06		0.167
3-9-84	A490	1.000	533	05	01		0.147
3-12-84	A325	1.000	530	07	05		0.125
3-22-84	A490	1.375	540	06*E	03		0.125
3-12-84	A325	1.000	530	09	07		0.104
3-19-84	A325	0.875	535	04	06		0.083
3-12-84	A325	1.000	530	09	07		0.083
3-12-84	A325	1.000	530	09	07		0.083
3-12-84	A325	1.000	530	07	08		0.083
3-12-84	A325	1.000	530	07	07		0.083
3-12-84	A490	0.875	534	09	08		0.083
3-19-84	A325	0.875	535	04	04		0.083
3-19-84	A325	0.875	535	04	01		0.083
3-12-84	A325	0.875	532	11	04		0.083
3-19-84	A325	0.875	535	04	05		0.083
3-12-84	A325	0.875	532	11	06		0.083
3-12-84	A325	0.875	532	11	02		0.083
3-12-84	A325	0.875	532	21	03		0.083
3-14-84	A325	0.875	536	17	03		0.083
3-19-84	A325	0.875	535	05	03		0.083
3-12-84	A325	0.875	533	09	03		0.083
3-12-84	A325	1.000	530	09	09		0.083
3-30-84	A490	1.375	541	04E	06		0.083



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3-13-84	A325	0.875	531	03	01	0.083
3-12-84	A325	0.875	533	09	08	0.083
3-12-84	A325	0.875	532	21	04	0.083
3-13-84	A325	0.875	531	04	07	0.083
3-12-84	A325	1.000	530	07	02	0.083
3-19-84	A325	0.875	535	38	01	0.083
3-12-84	A325	0.875	532	21	02	0.083
3-28-84	A490	1.375	540	20W	01	0.083
3-22-84	A490	1.375	540	06*E	04	0.056
3-12-84	A325	0.875	532	21	06	0.042
3-30-84	A490	1.375	541	04E	02	0.042
3-12-84	A325	0.875	532	21	05	0.042
3-12-84	A325	0.875	533	09	07	0.042
3-13-84	A325	0.875	531	05	04	0.042
3-12-84	A325	1.000	530	09	01	0.042
3-12-84	A325	1.000	530	07	05	0.042
3-12-84	A325	0.875	530	17	01	0.042
3-9-84	A490	1.000	533	05	07	0.042
3-19-84	A325	0.875	535	04	03	0.042
3-9-84	A490	1.000	533	05	06	0.042
3-14-84	A325	0.875	536	17	01	0.042
3-19-84	A325	0.875	535	04	05	0.042
3-12-84	A325	0.875	533	09	05	0.042
3-22-84	A490	1.375	540	06*E	06	0.042
3-12-84	A325	0.875	532	21	07	0.042
3-19-84	A325	0.875	535	04	02	0.042
3-12-84	A325	0.875	532	11	04	0.042
3-12-84	A325	0.875	532	21	01	0.042
3-12-84	A490	0.875	534	08	04	0.042
4-5-84	A490	1.375	541	05E	02	0.021
3-20-84	A490	1.375	540	22	02A	0.021
3-28-84	A490	1.375	540	15W	01	0.021
3-12-84	A490	0.875	534	25	03	0.021
3-28-84	A490	1.375	540	20E	08	0.021
4-5-84	A490	1.375	540	41E	02	0.021
3-9-84	A490	1.000	533	05	10	0.021
3-30-84	A490	1.375	540	42W	07	0.021
3-9-84	A490	1.000	533	05	09	0.021
3-12-84	A325	0.875	533	09	01	0.021
3-28-84	A490	1.375	540	20E	01	0.021
3-12-84	A325	0.875	533	09	03	0.021
3-12-84	A325	1.000	530	07	06	0.021
3-30-84	A490	1.375	540	35W	03	0.021
3-12-84	A325	0.875	530	17	03	0.021
3-30-84	A490	1.375	540	35W	02	0.021
4-5-84	A490	1.375	541	05E	03	0.021
3-30-84	A490	1.375	541	04W	02	0.021
3-28-84	A490	1.375	540	14W	07	0.021
4-5-84	A490	1.375	540	41E	03	0.021
3-12-84	A325	1.000	530	07	01	0.021
3-30-84	A490	1.375	540	42W	05	0.021
4-5-84	A490	1.375	541	05E	04	0.021
3-12-84	A325	0.875	533	09	04	0.021
3-28-84	A490	1.375	540	14W	05	0.021
3-13-84	A325	0.875	531	03	05	0.021
3-13-84	A325	0.875	531	03	02	0.021

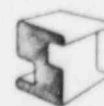


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3-12-84	A325	0.875	532	21	08	
4-5-84	A490	1.375	541	05E	05	0.021
3-12-84	A325	0.875	533	09	06	0.021
3-30-84	A490	1.375	540	42W	02	0.021
4-5-84	A490	1.375	540	41E	06	0.021
3-12-84	A490	0.875	534	08	01	0.021
3-28-84	A490	1.375	540	18E	03	0.021
3-28-84	A490	1.375	540	10E	05	0.000
3-13-84	A325	0.875	531	03	06	0.000
3-28-84	A490	1.375	540	10E	06	0.000
3-13-84	A325	0.875	531	04	01	0.000
3-28-84	A490	1.375	540	16W	01	0.000
3-13-84	A325	0.875	531	04	03	0.000
3-28-84	A490	1.375	540	16W	02	0.000
3-13-84	A325	0.875	531	04	05	0.000
3-28-84	A490	1.375	540	16W	03	0.000
3-13-84	A325	0.875	531	03	04	0.000
3-28-84	A490	1.375	540	16W	04	0.000
3-13-84	A325	0.875	531	06	01	0.000
3-28-84	A490	1.375	540	16W	05	0.000
3-13-84	A325	0.875	531	06	03	0.000
3-28-84	A490	1.375	540	16W	06	0.000
3-13-84	A325	0.875	531	05	02	0.000
3-28-84	A490	1.375	540	17E	01	0.000
3-12-84	A325	0.875	530	17	02	0.000
3-28-84	A490	1.375	540	17E	02	0.000
3-13-84	A325	0.875	531	05	06	0.000
3-28-84	A490	1.375	540	17E	03	0.000
3-13-84	A325	0.875	531	05	08	0.000
3-28-84	A490	1.375	540	17E	04	0.000
3-13-84	A325	0.875	531	06	05	0.000
3-28-84	A490	1.375	540	17E	05	0.000
3-14-84	A325	0.875	536	01	02	0.000
3-28-84	A490	1.375	540	17E	06	0.000
3-12-84	A325	0.875	530	19	03	0.000
3-28-84	A490	1.375	540	18W	01	0.000
3-14-84	A325	0.875	536	02	03	0.000
3-28-84	A490	1.375	540	18W	02	0.000
3-14-84	A325	0.875	536	17	02	0.000
3-28-84	A490	1.375	540	18W	03	0.000
3-12-84	A325	0.875	533	09	10	0.000
3-28-84	A490	1.375	540	18W	04	0.000
3-14-84	A325	0.875	534	19	02	0.000
3-28-84	A490	1.375	540	18W	05	0.000
3-14-84	A325	0.875	534	19	04	0.000
3-28-84	A490	1.375	540	18W	06	0.000
3-14-84	A325	0.875	534	19	06	0.000
3-28-84	A490	1.375	540	19	01	0.000
3-14-84	A325	0.875	534	19	01	0.000
3-28-84	A490	1.375	540	19	02	0.000
3-14-84	A325	0.875	534	01	03	0.000
3-28-84	A490	1.375	540	19	03	0.000
3-14-84	A325	0.875	534	01	05	0.000
3-28-84	A490	1.375	540	19	04	0.000
3-14-84	A325	0.875	534	01	07	0.000
3-28-84	A490	1.375	540	19	05	0.000



3-14-84	A490	1.000	532	25	05	
3-28-84	A490	1.375	540	19	06	0.000
3-14-84	A490	1.000	532	25	07	0.000
3-12-84	A490	0.875	534	23	03	0.000
3-12-84	A325	0.875	533	09	02	0.000
3-28-84	A490	1.375	540	20W	02	0.000
3-12-84	A325	0.875	532	21	09	0.000
3-28-84	A490	1.375	540	20W	03	0.000
3-12-84	A325	0.875	533	17	03	0.000
3-28-84	A490	1.375	540	20W	04	0.000
3-12-84	A325	0.875	533	17	01	0.000
3-28-84	A490	1.375	540	20W	05	0.000
3-19-84	A325	0.875	535	05	02	0.000
3-28-84	A490	1.375	540	20W	06	0.000
3-12-84	A325	0.875	533	11	06	0.000
3-28-84	A490	1.375	540	20W	07	0.000
3-19-84	A325	0.875	535	05	06	0.000
3-28-84	A490	1.375	540	20W	08	0.000
3-19-84	A325	0.875	535	05	08	0.000
3-12-84	A490	0.875	534	23	02	0.000
3-12-84	A325	0.875	533	11	04	0.000
3-28-84	A490	1.375	540	20E	02	0.000
3-12-84	A325	0.875	533	11	02	0.000
3-28-84	A490	1.375	540	20E	03	0.000
3-12-84	A490	0.875	534	09	07	0.000
3-28-84	A490	1.375	540	20E	04	0.000
3-19-84	A325	0.875	535	10	01	0.000
3-28-84	A490	1.375	540	20E	05	0.000
3-19-84	A325	0.875	535	10	03	0.000
3-28-84	A490	1.375	540	20E	06	0.000
3-19-84	A325	0.875	535	10	05	0.000
3-28-84	A490	1.375	540	20E	07	0.000
3-19-84	A325	0.875	535	10	07	0.000
3-12-84	A490	0.875	534	23	01	0.000
3-19-84	A325	0.875	535	18	02	0.000
3-12-84	A490	0.875	534	26	07	0.000
3-19-84	A325	0.875	535	18	03	0.000
3-28-84	A490	1.375	540	15W	02	0.000
3-19-84	A325	0.875	535	18	05	0.000
3-28-84	A490	1.375	540	15W	03	0.000
3-19-84	A325	0.875	535	18	07	0.000
3-28-84	A490	1.375	540	15W	04	0.000
3-12-84	A490	0.875	534	09	03	0.000
3-28-84	A490	1.375	540	15W	05	0.000
3-12-84	A490	0.875	534	09	01	0.000
3-28-84	A490	1.375	540	15W	06	0.000
3-12-84	A490	0.875	534	08	06	0.000
3-28-84	A490	1.375	540	15E	01	0.000
3-20-84	A490	1.375	540	22	01A	0.000
3-28-84	A490	1.375	540	15E	02	0.000
3-20-84	A490	1.375	540	22	03A	0.000
3-28-84	A490	1.375	540	15E	03	0.000
3-20-84	A490	1.375	540	22	05A	0.000
3-28-84	A490	1.375	540	15E	04	0.000
3-20-84	A490	1.375	540	22	01B	0.000
3-28-84	A490	1.375	540	15E	05	0.000



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3-20-84	A490	1.375	540	22	03B	0.000
3-28-84	A490	1.375	540	15E	06	0.000
3-20-84	A490	1.375	540	22	05B	0.000
3-28-84	A490	1.375	540	01W	01	0.000
3-21-84	A490	1.375	540	23W	01	0.000
3-28-84	A490	1.375	540	01W	02	0.000
3-21-84	A490	1.375	540	23W	03	0.000
3-28-84	A490	1.375	540	01W	03	0.000
3-21-84	A490	1.375	540	23W	05	0.000
3-28-84	A490	1.375	540	01W	04	0.000
3-21-84	A490	1.375	540	24E	01	0.000
3-28-84	A490	1.375	540	01W	05	0.000
3-21-84	A490	1.375	540	24E	03	0.000
3-28-84	A490	1.375	540	01W	06	0.000
3-21-84	A490	1.375	540	24E	05	0.000
3-28-84	A490	1.375	541	01E	01	0.000
3-21-84	A490	1.375	540	25W	01	0.000
3-28-84	A490	1.375	541	01E	02	0.000
3-21-84	A490	1.375	540	25W	03	0.000
3-28-84	A490	1.375	541	01E	03	0.000
3-21-84	A490	1.375	540	25W	05	0.000
3-28-84	A490	1.375	541	01E	04	0.000
3-21-84	A490	1.375	540	26E	01	0.000
3-28-84	A490	1.375	541	01E	05	0.000
3-21-84	A490	1.375	540	26E	03	0.000
3-28-84	A490	1.375	541	01E	06	0.000
3-21-84	A490	1.375	540	26E	05	0.000
3-28-84	A490	1.375	541	02W	01	0.000
3-21-84	A490	1.375	540	27W	01	0.000
3-28-84	A490	1.375	541	02W	02	0.000
3-21-84	A490	1.375	540	27W	03	0.000
3-28-84	A490	1.375	541	02W	03	0.000
3-21-84	A490	1.375	540	27W	05	0.000
3-28-84	A490	1.375	541	02W	04	0.000
3-21-84	A490	1.375	540	27W	07	0.000
3-28-84	A490	1.375	541	02W	05	0.000
3-21-84	A490	1.375	540	27E	01	0.000
3-28-84	A490	1.375	541	02W	06	0.000
3-21-84	A490	1.375	540	27E	03	0.000
3-28-84	A490	1.375	541	02W	07	0.000
3-21-84	A490	1.375	540	27E	05	0.000
3-28-84	A490	1.375	541	02W	08	0.000
3-21-84	A490	1.375	540	27E	07	0.000
3-28-84	A490	1.375	541	02W	09	0.000
3-21-84	A490	1.375	540	28W	01	0.000
3-29-84	A490	1.375	541	02E	01	0.000
3-21-84	A490	1.375	540	28W	03	0.000
3-29-84	A490	1.375	541	02E	02	0.000
3-21-84	A490	1.375	540	28W	05	0.000
3-29-84	A490	1.375	541	02E	03	0.000
3-21-84	A490	1.375	540	28W	07	0.000
3-29-84	A490	1.375	541	02E	04	0.000
3-21-84	A490	1.375	540	28E	01	0.000
3-29-84	A490	1.375	541	02E	05	0.000
3-21-84	A490	1.375	540	28E	03	0.000
3-29-84	A490	1.375	541	02E	06	0.000



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3-21-84	A490	1.375	540	28E	05	0.000
3-29-84	A490	1.375	541	02E	07	0.000
3-21-84	A490	1.375	540	28E	07	0.000
3-29-84	A490	1.375	541	02E	08	0.000
3-21-84	A490	1.375	540	01W	01	0.000
3-29-84	A490	1.375	541	02E	09	0.000
3-21-84	A490	1.375	540	01W	03	0.000
3-29-84	A490	1.375	541	03W	01	0.000
3-21-84	A490	1.375	540	01W	05	0.000
3-29-84	A490	1.375	541	03W	02	0.000
3-21-84	A490	1.375	540	01E	01	0.000
3-29-84	A490	1.375	541	03W	03	0.000
3-21-84	A490	1.375	540	01E	03	0.000
3-29-84	A490	1.375	541	03W	04	0.000
3-21-84	A490	1.375	540	01E	05	0.000
3-29-84	A490	1.375	541	03W	05	0.000
3-21-84	A490	1.375	540	07W	01	0.000
3-29-84	A490	1.375	541	03W	06	0.000
3-21-84	A490	1.375	540	07W	03	0.000
3-29-84	A490	1.375	541	03W	07	0.000
3-21-84	A490	1.375	540	07W	05	0.000
3-29-84	A490	1.375	541	03W	08	0.000
3-21-84	A490	1.375	540	07W	07	0.000
3-29-84	A490	1.375	541	03E	01	0.000
3-21-84	A490	1.375	540	07E	01	0.000
3-29-84	A490	1.375	541	03E	02	0.000
3-21-84	A490	1.375	540	07E	03	0.000
3-29-84	A490	1.375	541	03E	03	0.000
3-21-84	A490	1.375	540	07E	05	0.000
3-29-84	A490	1.375	541	03E	04	0.000
3-21-84	A490	1.375	540	07E	07	0.000
3-29-84	A490	1.375	541	03E	05	0.000
3-21-84	A490	1.375	540	06*W	01	0.000
3-29-84	A490	1.375	541	03E	06	0.000
3-21-84	A490	1.375	540	06*W	03	0.000
3-29-84	A490	1.375	541	03E	07	0.000
3-21-84	A490	1.375	540	06*W	05	0.000
3-29-84	A490	1.375	541	03E	08	0.000
3-21-84	A490	1.375	540	06*W	07	0.000
3-29-84	A490	1.375	541	21W	01	0.000
3-21-84	A490	1.375	540	06*E	02	0.000
3-29-84	A490	1.375	541	21W	02	0.000
3-21-84	A490	1.375	540	06*E	03	0.000
3-29-84	A490	1.375	541	21W	03	0.000
3-21-84	A490	1.375	540	06*E	05	0.000
3-29-84	A490	1.375	541	21W	04	0.000
3-21-84	A490	0.875	534	23	06	0.000
3-29-84	A490	1.375	540	21W	05	0.000
3-21-84	A490	1.375	540	02W	01	0.000
3-29-84	A490	1.375	541	21W	06	0.000
3-21-84	A490	1.375	540	02W	03	0.000
3-29-84	A490	1.375	541	21W	07	0.000
3-21-84	A490	1.375	540	02W	05	0.000
3-29-84	A490	1.375	541	21W	08	0.000
3-21-84	A490	1.375	540	03E	01	0.000
3-29-84	A490	1.375	541	21E	01	0.000



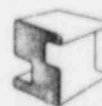
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ASSOCIATES, INC.**

3-22-84	A490	1.375	540	03E	03	0.000
3-29-84	A490	1.375	540	21E	02	0.000
3-22-84	A490	1.375	540	03E	05	0.000
3-29-84	A490	1.375	540	21E	03	0.000
3-22-84	A490	1.375	540	04W	01	0.000
3-29-84	A490	1.375	540	21E	04	0.000
3-22-84	A490	1.375	540	04W	03	0.000
3-29-84	A490	1.375	540	21E	05	0.000
3-22-84	A490	1.375	540	04W	05	0.000
3-29-84	A490	1.375	540	21E	06	0.000
3-22-84	A490	1.375	540	05E	01	0.000
3-29-84	A490	1.375	540	21E	07	0.000
3-22-84	A490	1.375	540	05E	03	0.000
3-29-84	A490	1.375	540	21E	08	0.000
3-22-84	A490	1.375	540	05E	05	0.000
3-29-84	A490	1.375	540	29W	01	0.000
3-28-84	A490	1.375	540	08W	01	0.000
3-29-84	A490	1.375	540	29W	02	0.000
3-28-84	A490	1.375	540	08W	04	0.000
3-29-84	A490	1.375	540	29W	03	0.000
3-28-84	A490	1.375	540	08W	06	0.000
3-29-84	A490	1.375	540	29W	04	0.000
3-28-84	A490	1.375	540	18E	02	0.000
3-29-84	A490	1.375	540	29W	05	0.000
3-28-84	A490	1.375	540	18E	04	0.000
3-29-84	A490	1.375	540	29W	06	0.000
3-28-84	A490	1.375	540	18E	06	0.000
3-29-84	A490	1.375	540	29E	01	0.000
3-28-84	A490	1.375	540	14W	02	0.000
3-29-84	A490	1.375	540	29E	02	0.000
3-28-84	A490	1.375	540	14W	04	0.000
3-29-84	A490	1.375	540	29E	03	0.000
3-28-84	A490	1.375	540	14W	06	0.000
3-29-84	A490	1.375	540	29E	04	0.000
3-28-84	A490	1.375	540	14W	08	0.000
3-29-84	A490	1.375	540	29E	05	0.000
3-28-84	A490	1.375	540	14E	02	0.000
3-29-84	A490	1.375	540	29E	06	0.000
3-28-84	A490	1.375	540	14E	04	0.000
3-30-84	A490	1.375	541	04W	01	0.000
3-28-84	A490	1.375	540	14E	06	0.000
3-12-84	A490	0.875	534	26	06	0.000
3-28-84	A490	1.375	540	14E	08	0.000
3-30-84	A490	1.375	541	04W	03	0.000
3-28-84	A490	1.375	540	13W	02	0.000
3-30-84	A490	1.375	541	04W	04	0.000
3-28-84	A490	1.375	540	13W	04	0.000
3-30-84	A490	1.375	541	04W	05	0.000
3-28-84	A490	1.375	540	13W	06	0.000
3-30-84	A490	1.375	541	04W	06	0.000
3-28-84	A490	1.375	540	13W	08	0.000
3-30-84	A490	1.375	541	04E	01	0.000
3-28-84	A490	1.375	540	13E	02	0.000
3-12-84	A490	0.875	534	26	05	0.000
3-28-84	A490	1.375	540	13E	04	0.000
3-30-84	A490	1.375	541	04E	03	0.000



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3-28-84	A490	1.375	540	13E	06	0.000
3-30-84	A490	1.375	541	04E	04	0.000
3-28-84	A490	1.375	540	13E	08	0.000
3-30-84	A490	1.375	541	04E	05	0.000
3-28-84	A490	1.375	540	11W	02	0.000
3-12-84	A490	0.875	534	26	04	0.000
3-28-84	A490	1.375	540	11W	04	0.000
3-30-84	A490	1.375	540	36W	01	0.000
3-28-84	A490	1.375	540	11W	06	0.000
3-30-84	A490	1.375	540	36W	02	0.000
3-28-84	A490	1.375	540	12E	02	0.000
3-30-84	A490	1.375	540	36W	03	0.000
3-28-84	A490	1.375	540	12E	04	0.000
3-30-84	A490	1.375	540	36W	04	0.000
3-28-84	A490	1.375	540	09W	06	0.000
3-30-84	A490	1.375	540	36W	05	0.000
3-28-84	A490	1.375	540	09W	02	0.000
3-30-84	A490	1.375	540	36W	06	0.000
3-28-84	A490	1.375	540	09W	04	0.000
3-30-84	A490	1.375	540	36E	01	0.000
3-28-84	A490	1.375	540	09W	06	0.000
3-30-84	A490	1.375	540	36E	02	0.000
3-28-84	A490	1.375	540	10E	02	0.000
3-30-84	A490	1.375	540	36E	03	0.000
3-28-84	A490	1.375	540	10E	04	0.000
3-30-84	A490	1.375	540	36E	04	0.000
3-13-84	A325	0.875	531	04	02	0.000
3-30-84	A490	1.375	540	36E	05	0.000
3-13-84	A325	0.875	531	04	06	0.000
3-30-84	A490	1.375	540	36E	06	0.000
3-13-84	A325	0.875	531	06	02	0.000
3-30-84	A490	1.375	541	36W	01	0.000
3-13-84	A325	0.875	531	03	03	0.000
3-30-84	A490	1.375	541	36W	02	0.000
3-13-84	A325	0.875	531	05	07	0.000
3-30-84	A490	1.375	541	36W	03	0.000
3-14-84	A325	0.875	536	01	01	0.000
3-30-84	A490	1.375	541	36W	04	0.000
3-14-84	A325	0.875	536	02	02	0.000
3-30-84	A490	1.375	541	36W	05	0.000
3-12-84	A325	0.875	533	17	05	0.000
3-30-84	A490	1.375	541	36W	06	0.000
3-14-84	A325	0.875	534	19	03	0.000
3-30-84	A490	1.375	541	36W	07	0.000
3-14-84	A325	0.875	534	19	07	0.000
3-30-84	A490	1.375	541	36W	08	0.000
3-14-84	A325	0.875	534	01	04	0.000
3-30-84	A490	1.375	541	36E	02	0.000
3-14-84	A490	1.000	532	25	04	0.000
3-30-84	A490	1.375	541	36E	03	0.000
3-14-84	A490	1.000	532	25	09	0.000
3-30-84	A490	1.375	541	36E	04	0.000
3-12-84	A325	0.875	533	17	04	0.000
3-30-84	A490	1.375	541	36E	05	0.000
3-19-84	A325	0.875	535	05	01	0.000
3-30-84	A490	1.375	541	36E	06	0.000



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3-19-84	A325	0.875	535	05	05	0.000
3-30-84	A490	1.375	541	36E	07	0.000
3-12-84	A325	0.875	533	11	05	0.000
3-30-84	A490	1.375	541	36E	08	0.000
3-12-84	A325	0.875	533	11	01	0.000
3-30-84	A490	1.375	540	35W	01	0.000
3-19-84	A325	0.875	535	10	02	0.000
3-12-84	A490	0.875	534	26	03	0.000
3-19-84	A325	0.875	535	10	06	0.000
3-12-84	A490	0.875	534	26	02	0.000
3-19-84	A325	0.875	535	18	02	0.000
3-30-84	A490	1.375	540	35W	04	0.000
3-19-84	A325	0.875	535	18	06	0.000
3-30-84	A490	1.375	540	35W	05	0.000
3-12-84	A490	0.875	534	09	02	0.000
3-30-84	A490	1.375	540	35W	06	0.000
3-12-84	A490	0.875	534	08	05	0.000
3-30-84	A490	1.375	540	35W	07	0.000
3-20-84	A490	1.375	540	22	04A	0.000
3-30-84	A490	1.375	540	35W	08	0.000
3-20-84	A490	1.375	540	22	02B	0.000
3-30-84	A490	1.375	540	35E	01	0.000
3-20-84	A490	1.375	540	22	06B	0.000
3-30-84	A490	1.375	540	35E	02	0.000
3-21-84	A490	1.375	540	23W	04	0.000
3-30-84	A490	1.375	540	35E	03	0.000
3-21-84	A490	1.375	540	24E	02	0.000
3-30-84	A490	1.375	540	35E	04	0.000
3-21-84	A490	1.375	540	24E	06	0.000
3-30-84	A490	1.375	540	35E	05	0.000
3-21-84	A490	1.375	540	25W	04	0.000
3-30-84	A490	1.375	540	35E	06	0.000
3-21-84	A490	1.375	540	26E	02	0.000
3-30-84	A490	1.375	540	35E	07	0.000
3-21-84	A490	1.375	540	26E	06	0.000
3-30-84	A490	1.375	540	35E	08	0.000
3-21-84	A490	1.375	540	27W	04	0.000
3-30-84	A490	1.375	540	42W	01	0.000
3-21-84	A490	1.375	540	27W	08	0.000
3-12-84	A490	0.875	534	26	01	0.000
3-21-84	A490	1.375	540	27E	04	0.000
3-30-84	A490	1.375	540	42W	03	0.000
3-21-84	A490	1.375	540	27E	08	0.000
3-30-84	A490	1.375	540	42W	04	0.000
3-21-84	A490	1.375	540	28W	04	0.000
3-12-84	A490	0.875	534	25	07	0.000
3-21-84	A490	1.375	540	28W	08	0.000
3-30-84	A490	1.375	540	42W	06	0.000
3-21-84	A490	1.375	540	28E	04	0.000
3-12-84	A490	0.875	534	25	06	0.000
3-21-84	A490	1.375	540	28E	08	0.000
3-30-84	A490	1.375	540	42W	08	0.000
3-21-84	A490	1.375	540	01W	04	0.000
3-30-84	A490	1.375	540	42E	01	0.000
3-21-84	A490	1.375	540	01E	02	0.000
3-30-84	A490	1.375	540	42E	02	0.000



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3-21-84	A490	1.375	540	01E	06	0.000
3-30-84	A490	1.375	540	42E	03	0.000
3-21-84	A490	1.375	540	07W	04	0.000
3-30-84	A490	1.375	540	42E	04	0.000
3-21-84	A490	1.375	540	07W	08	0.000
3-30-84	A490	1.375	540	42E	05	0.000
3-21-84	A490	1.375	540	07E	04	0.000
3-30-84	A490	1.375	540	42E	06	0.000
3-21-84	A490	1.375	540	07E	08	0.000
3-30-84	A490	1.375	540	42E	07	0.000
3-22-84	A490	1.375	540	06*W	04	0.000
3-30-84	A490	1.375	540	42E	08	0.000
3-22-84	A490	1.375	540	06*W	08	0.000
3-30-84	A490	1.375	540	30W	01	0.000
3-12-84	A490	0.875	534	08	02	0.000
3-30-84	A490	1.375	540	30W	02	0.000
3-22-84	A490	1.375	540	06*E	08	0.000
3-30-84	A490	1.375	540	30W	03	0.000
3-22-84	A490	1.375	540	02W	04	0.000
3-30-84	A490	1.375	540	30W	04	0.000
3-22-84	A490	1.375	540	03E	02	0.000
3-30-84	A490	1.375	540	30W	05	0.000
3-22-84	A490	1.375	540	03E	06	0.000
3-30-84	A490	1.375	540	30W	06	0.000
3-22-84	A490	1.375	540	04W	04	0.000
3-30-84	A490	1.375	540	31E	01	0.000
3-22-84	A490	1.375	540	05E	02	0.000
3-30-84	A490	1.375	540	31E	02	0.000
3-22-84	A490	1.375	540	05E	06	0.000
3-30-84	A490	1.375	540	31E	03	0.000
3-28-84	A490	1.375	540	08W	05	0.000
3-30-84	A490	1.375	540	31E	04	0.000
3-9-84	A490	1.000	533	06	08	0.000
3-30-84	A490	1.375	540	31E	05	0.000
3-28-84	A490	1.375	540	14W	01	0.000
3-30-84	A490	1.375	540	31E	06	0.000
3-12-84	A490	0.875	534	23	05	0.000
3-30-84	A490	1.375	540	32W	01	0.000
3-28-84	A490	1.375	540	14E	01	0.000
3-30-84	A490	1.375	540	32W	02	0.000
3-28-84	A490	1.375	540	14E	05	0.000
3-30-84	A490	1.375	540	32W	03	0.000
3-28-84	A490	1.375	540	13W	01	0.000
3-30-84	A490	1.375	540	32W	04	0.000
3-28-84	A490	1.375	540	13W	05	0.000
3-30-84	A490	1.375	540	32W	05	0.000
3-28-84	A490	1.375	540	13E	01	0.000
3-30-84	A490	1.375	540	32W	06	0.000
3-28-84	A490	1.375	540	13E	05	0.000
3-30-84	A490	1.375	540	33E	01	0.000
3-28-84	A490	1.375	540	11W	01	0.000
3-30-84	A490	1.375	540	33E	02	0.000
3-28-84	A490	1.375	540	11W	05	0.000
3-30-84	A490	1.375	540	33E	03	0.000
3-28-84	A490	1.375	540	12E	03	0.000
3-30-84	A490	1.375	540	33E	04	0.000



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3-28-84	A490	1.375	540	09W	01	0.000
3-30-84	A490	1.375	540	33E	05	0.000
3-28-84	A490	1.375	540	09W	05	0.000
3-30-84	A490	1.375	540	33E	06	0.000
3-28-84	A490	1.375	540	10E	03	0.000
3-30-84	A490	1.375	540	34W	01	0.000
3-13-84	A325	0.875	531	04	04	0.000
3-30-84	A490	1.375	540	34W	02	0.000
3-13-84	A325	0.875	531	05	01	0.000
3-30-84	A490	1.375	540	34W	03	0.000
3-13-84	A325	0.875	531	06	04	0.000
3-30-84	A490	1.375	540	34W	04	0.000
3-12-84	A325	0.875	533	17	06	0.000
3-30-84	A490	1.375	540	34W	05	0.000
3-14-84	A325	0.875	534	19	05	0.000
3-30-84	A490	1.375	540	34W	06	0.000
3-14-84	A325	0.875	534	01	06	0.000
3-30-84	A490	1.375	540	34W	07	0.000
3-12-84	A325	0.875	532	21	10	0.000
3-30-84	A490	1.375	540	34W	08	0.000
3-12-84	A325	0.875	533	15	06	0.000
3-30-84	A490	1.375	540	34E	01	0.000
3-12-84	A325	0.875	533	11	03	0.000
3-30-84	A490	1.375	540	34E	02	0.000
3-19-84	A325	0.875	535	10	04	0.000
3-30-84	A490	1.375	540	34E	03	0.000
3-19-84	A325	0.875	535	18	04	0.000
3-30-84	A490	1.375	540	34E	04	0.000
3-12-84	A490	0.875	534	08	07	0.000
3-30-84	A490	1.375	540	34E	05	0.000
3-20-84	A490	1.375	540	22	06A	0.000
3-30-84	A490	1.375	540	34E	06	0.000
3-21-84	A490	1.375	540	23W	02	0.000
3-30-84	A490	1.375	540	34E	07	0.000
3-21-84	A490	1.375	540	24E	04	0.000
3-30-84	A490	1.375	540	34E	08	0.000
3-21-84	A490	1.375	540	25W	06	0.000
3-30-84	A490	1.375	540	37W	01	0.000
3-21-84	A490	1.375	540	27W	02	0.000
3-30-84	A490	1.375	540	37W	02	0.000
3-21-84	A490	1.375	540	27E	02	0.000
3-30-84	A490	1.375	540	37W	03	0.000
3-21-84	A490	1.375	540	28W	02	0.000
3-30-84	A490	1.375	540	37W	04	0.000
3-21-84	A490	1.375	540	28E	02	0.000
3-30-84	A490	1.375	540	37W	05	0.000
3-21-84	A490	1.375	540	01W	02	0.000
3-30-84	A490	1.375	540	37W	06	0.000
3-21-84	A490	1.375	540	01E	04	0.000
3-30-84	A490	1.375	540	38E	01	0.000
3-21-84	A490	1.375	540	07W	06	0.000
3-30-84	A490	1.375	540	38E	02	0.000
3-21-84	A490	1.375	540	07E	06	0.000
3-30-84	A490	1.375	540	38E	03	0.000
3-22-84	A490	1.375	540	06*W	06	0.000
3-30-84	A490	1.375	540	38E	04	0.000

3-12-84	A490	0.875	534	23	07	0.000
3-30-84	A490	1.375	540	38E	05	0.000
3-22-84	A490	1.375	540	02W	06	0.000
3-30-84	A490	1.375	540	38E	06	0.000
3-22-84	A490	1.375	540	04W	02	0.000
3-30-84	A490	1.375	540	39W	01	0.000
3-22-84	A490	1.375	540	05E	04	0.000
3-30-84	A490	1.375	540	39W	02	0.000
3-28-84	A490	1.375	540	18E	01	0.000
3-30-84	A490	1.375	540	39W	03	0.000
3-28-84	A490	1.375	540	14W	03	0.000
3-30-84	A490	1.375	540	39W	04	0.000
3-28-84	A490	1.375	540	14E	03	0.000
3-30-84	A490	1.375	540	39W	05	0.000
3-28-84	A490	1.375	540	13W	03	0.000
3-30-84	A490	1.375	540	39W	06	0.000
3-28-84	A490	1.375	540	13E	03	0.000
3-30-84	A490	1.375	540	40E	01	0.000
3-28-84	A490	1.375	540	11W	03	0.000
3-30-84	A490	1.375	540	40E	02	0.000
3-28-84	A490	1.375	540	12E	05	0.000
3-30-84	A490	1.375	540	40E	03	0.000
3-28-84	A490	1.375	540	10E	01	0.000
3-30-84	A490	1.375	540	40E	04	0.000
3-13-84	A325	0.875	531	04	08	0.000
3-30-84	A490	1.375	540	40E	05	0.000
3-14-84	A325	0.875	536	01	03	0.000
3-30-84	A490	1.375	540	40E	06	0.000
3-14-84	A325	0.875	534	01	02	0.000
4-5-84	A490	1.375	540	41W	01	0.000
3-12-84	A325	0.875	533	17	02	0.000
4-5-84	A490	1.375	540	41W	02	0.000
3-12-84	A490	0.875	534	09	06	0.000
4-5-84	A490	1.375	540	41W	03	0.000
3-12-84	A490	0.875	534	09	05	0.000
4-5-84	A490	1.375	540	41W	04	0.000
3-20-84	A490	1.375	540	22	04B	0.000
4-5-84	A490	1.375	540	41W	05	0.000
3-21-84	A490	1.375	540	25W	02	0.000
4-5-84	A490	1.375	540	41W	06	0.000
3-21-84	A490	1.375	540	27W	06	0.000
4-5-84	A490	1.375	540	41W	07	0.000
3-21-84	A490	1.375	540	28W	06	0.000
4-5-84	A490	1.375	540	41W	08	0.000
3-21-84	A490	1.375	540	01W	06	0.000
4-5-84	A490	1.375	540	41E	01	0.000
3-21-84	A490	1.375	540	07E	02	0.000
3-12-84	A490	0.875	534	25	05	0.000
3-22-84	A490	1.375	540	06*E	02	0.000
3-12-84	A490	0.875	534	25	04	0.000
3-22-84	A490	1.375	540	03E	04	0.000
4-5-84	A490	1.375	540	41E	04	0.000
3-28-84	A490	1.375	540	08W	03	0.000
4-5-84	A490	1.375	540	41E	05	0.000
3-12-84	A490	0.875	534	23	04	0.000
3-12-84	A490	0.875	534	25	02	0.000



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3-28-84	A490	1.375	540	13W	07	0.000
4-5-84	A490	1.375	540	41E	07	0.000
3-28-84	A490	1.375	540	12E	01	0.000
4-5-84	A490	1.375	540	41E	08	0.000
3-13-84	A325	0.875	531	03	07	0.000
4-5-84	A490	1.375	541	05W	01	0.000
3-14-84	A325	0.875	534	19	01	0.000
4-5-84	A490	1.375	541	05W	02	0.000
3-19-84	A325	0.875	535	05	07	0.000
4-5-84	A490	1.375	541	05W	03	0.000
3-12-84	A490	0.875	534	08	03	0.000
4-5-84	A490	1.375	541	05W	04	0.000
3-21-84	A490	1.375	540	26E	04	0.000
4-5-84	A490	1.375	541	05W	05	0.000
3-21-84	A490	1.375	540	28E	06	0.000
4-5-84	A490	1.375	541	05W	06	0.000
3-22-84	A490	1.375	540	06*W	02	0.000
4-5-84	A490	1.375	541	05W	07	0.000
3-22-84	A490	1.375	540	04W	06	0.000
4-5-84	A490	1.375	541	05W	08	0.000
3-28-84	A490	1.375	540	14E	07	0.000
4-5-84	A490	1.375	541	05W	09	0.000
3-28-84	A490	1.375	540	09W	03	0.000
4-5-84	A490	1.375	541	05E	01	0.000
3-14-84	A490	1.000	532	25	06	0.000
3-12-84	A490	0.875	534	25	01	0.000
3-21-84	A490	1.375	540	23W	06	0.000
3-9-84	A490	1.000	533	05	08	0.000
3-21-84	A490	1.375	540	07W	02	0.000
3-9-84	A490	1.000	533	06	10	0.000
3-28-84	A490	1.375	540	18E	05	0.000
3-9-84	A490	1.000	533	06	09	0.000
3-13-84	A325	0.875	531	05	05	0.000
4-5-84	A490	1.375	541	05E	06	0.000
3-21-84	A490	1.375	540	27E	06	0.000
4-5-84	A490	1.375	541	05E	07	0.000
3-28-84	A490	1.375	540	13E	07	0.000
3-22-84	A490	1.375	540	02W	02	0.000
3-19-84	A325	0.875	535	10	08	0.000
4-5-84	A490	1.375	541	05E	08	0.000
4-5-84	A490	1.375	541	05E	09	0.000

APPENDIX C

PALO VERDE UNIT 2 HIGH STRENGTH BOLT TORQUE CHECK
FOR CRITICAL FRICTION FASTENERS

PALO VERDE UNIT 2 HIGH STRENGTH BOLT TORQUE

INSP. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONN. NO.	BOLT NO.	NUT ROTAT	TORQUE
4-16-84	A490	1.375	534	39	01		300,000
4-16-84	A490	1.375	534	39	02		300,000
4-16-84	A490	1.375	534	39	03		150,000
4-16-84	A490	1.375	534	39	04		150,000
4-16-84	A490	1.375	534	40	01		350,000
4-16-84	A490	1.375	534	40	02		350,000
4-16-84	A490	1.375	534	40	03		300,000
4-16-84	A490	1.375	534	40	04		300,000
4-16-84	A490	1.375	534	41	01		200,000
4-16-84	A490	1.375	534	41	02		350,000
4-16-84	A490	1.375	534	41	03		200,000
4-16-84	A490	1.375	534	41	04		250,000
4-16-84	A490	1.375	534	41	05		250,000
4-16-84	A490	1.375	534	41	06		250,000
4-16-84	A490	1.375	534	42	01		250,000
4-16-84	A490	1.375	534	42	02		350,000
4-16-84	A490	1.375	534	42	03		325,000
4-16-84	A490	1.375	534	42	04		375,000
4-16-84	A490	1.375	534	42	05		350,000
4-16-84	A490	1.375	534	42	06		250,000
4-16-84	A490	1.375	535	47	01		1250,000
4-16-84	A490	1.375	535	47	02		1250,000
4-16-84	A490	1.375	535	47	03		1300,000
4-16-84	A490	1.375	535	47	04		1300,000
4-16-84	A490	1.375	535	47	05		1450,000
4-16-84	A490	1.375	535	47	06		1200,000
4-16-84	A490	1.375	535	48	01		900,000
4-16-84	A490	1.375	535	48	02		1000,000
4-16-84	A490	1.375	535	48	03		1700,000
4-16-84	A490	1.375	535	48	04		700,000
4-16-84	A490	1.375	535	48	05		850,000
4-16-84	A490	1.375	535	48	06		1250,000
4-16-84	A490	1.375	535	45	01		2000,000
4-16-84	A490	1.375	535	45	02		1200,000
4-16-84	A490	1.375	535	45	03		600,000
4-16-84	A490	1.375	535	45	04		600,000
4-16-84	A490	1.375	535	45	05		600,000
4-16-84	A490	1.375	535	45	06		750,000
4-16-84	A490	1.375	535	46	03		550,000
4-16-84	A490	1.375	535	46	04		500,000
4-16-84	A490	1.375	535	46	05		450,000
4-16-84	A490	1.375	535	46	06		650,000
4-13-84	A490	1.375	535	43	01		1150,000
4-13-84	A490	1.375	535	43	02		900,000
4-13-84	A490	1.375	535	43	03		700,000
4-13-84	A490	1.375	535	43	04		600,000
4-13-84	A490	1.375	535	43	05		800,000
4-13-84	A490	1.375	535	43	06		600,000
4-13-84	A490	1.375	535	44	01		750,000
4-13-84	A490	1.375	535	44	02		750,000
4-13-84	A490	1.375	535	44	03		750,000
4-13-84	A490	1.375	535	44	04		750,000
4-13-84	A490	1.375	535	44	05		750,000

4-13-84	A490	1.375	535	44	06	700,000
4-13-84	A490	1.375	535	42	01	500,000
4-13-84	A490	1.375	535	42	02	1000,000
4-13-84	A490	1.375	535	42	03	200,000
4-13-84	A490	1.375	535	42	04	500,000
4-13-84	A490	1.375	535	53	01	500,000
4-13-84	A490	1.375	535	53	02	400,000
4-13-84	A490	1.375	535	53	03	400,000
4-13-84	A490	1.375	535	53	04	175,000
4-13-84	A490	1.375	535	53	05	400,000
4-13-84	A490	1.375	535	53	06	200,000
4-13-84	A490	1.375	535	54	01	500,000
4-13-84	A490	1.375	535	54	02	550,000
4-13-84	A490	1.375	535	54	03	250,000
4-13-84	A490	1.375	535	54	04	275,000
4-13-84	A490	1.375	535	54	05	275,000
4-13-84	A490	1.375	535	54	06	400,000
4-13-84	A490	1.375	535	55	01	700,000
4-13-84	A490	1.375	535	55	02	800,000
4-13-84	A490	1.375	535	55	03	300,000
4-13-84	A490	1.375	535	55	04	650,000
4-13-84	A490	1.375	535	55	05	600,000
4-13-84	A490	1.375	535	55	06	300,000
4-13-84	A490	1.375	535	56	01	600,000
4-13-84	A490	1.375	535	56	02	300,000
4-13-84	A490	1.375	535	56	03	300,000
4-13-84	A490	1.375	535	56	04	750,000
4-13-84	A490	1.375	535	56	05	600,000
4-13-84	A490	1.375	535	56	06	450,000
4-12-84	A490	1.375	534	31	01	1100,000
4-12-84	A490	1.375	534	31	02	750,000
4-12-84	A490	1.375	534	31	03	500,000
4-12-84	A490	1.375	534	31	04	500,000
4-12-84	A490	1.375	534	31	05	800,000
4-12-84	A490	1.375	534	31	06	1100,000
4-12-84	A490	1.375	534	32	01	1000,000
4-12-84	A490	1.375	534	32	02	2000,000
4-12-84	A490	1.375	534	32	03	1600,000
4-12-84	A490	1.375	534	32	04	550,000
4-12-84	A490	1.375	534	32	05	1100,000
4-12-84	A490	1.375	534	32	06	1000,000
4-12-84	A490	1.375	534	33	01	800,000
4-12-84	A490	1.375	534	33	02	700,000
4-12-84	A490	1.375	534	33	03	700,000
4-12-84	A490	1.375	534	33	04	900,000
4-12-84	A490	1.375	534	33	05	700,000
4-12-84	A490	1.375	534	33	06	900,000
4-12-84	A490	1.375	534	34	01	800,000
4-12-84	A490	1.375	534	34	02	800,000
4-12-84	A490	1.375	534	34	03	700,000
4-12-84	A490	1.375	534	34	04	200,000
4-12-84	A490	1.375	534	34	05	275,000
4-12-84	A490	1.375	534	34	06	275,000
3-22-84	A525	0.875	535	19	07	
3-20-84	A490	0.875	535	21	07	
3-19-84	A525	0.875	532	18	06	



**STRUCTURAL
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1. 853

3-20-84	A490	0.875	535	21	04	1.000
3-22-84	A325	0.875	535	19	06	1.000
3-19-84	A325	0.875	532	18	03	0.917
3-22-84	A325	0.875	535	19	05	0.917
3-19-84	A325	0.875	532	18	01	0.917
3-19-84	A325	0.875	532	18	04	0.833
3-20-84	A490	0.875	535	21	06	0.833
3-20-84	A490	0.875	535	21	05	0.833
3-22-84	A325	0.875	535	19	02	0.833
3-22-84	A325	0.875	535	19	03	0.833
3-19-84	A325	0.875	532	18	02	0.750
3-13-84	A325	0.875	531	01	05	0.750
3-19-84	A325	0.875	532	18	05	0.750
3-23-84	A325	0.875	535	04	06	0.667
3-13-84	A490	0.875	535	15	05	0.667
3-13-84	A325	0.875	534	02	04	0.667
3-23-84	A325	0.875	535	04	07	0.667
3-22-84	A325	0.875	535	19	01	0.667
3-14-84	A325	0.875	535	11	01	0.667
3-16-84	A325	0.875	533	16	02	0.667
3-13-84	A325	0.875	534	02	06	0.583
3-14-84	A325	0.875	535	25	07	0.583
3-15-84	A325	0.875	535	07	04	0.583
3-13-84	A325	0.875	534	02	03	0.500
3-14-84	A325	0.875	535	25	04	0.500
3-14-84	A325	0.875	535	11	02	0.500
3-14-84	A325	0.875	535	25	02	0.500
3-13-84	A325	0.875	535	05	08	0.500
3-14-84	A325	0.875	535	25	03	0.500
3-14-84	A325	0.875	535	25	06	0.500
3-15-84	A325	0.875	535	07	03	0.500
3-22-84	A325	0.875	535	19	04	0.500
3-14-84	A325	0.875	535	17	03	0.500
3-13-84	A325	0.875	534	02	07	0.500
3-14-84	A325	0.875	535	25	05	0.458
3-13-84	A325	0.875	535	05	03	0.458
3-14-84	A325	0.875	535	17	04	0.458
3-23-84	A325	0.875	535	04	05	0.417
3-13-84	A325	0.875	535	05	01	0.417
3-23-84	A325	0.875	535	04	04	0.417
3-20-84	A490	0.875	535	21	03	0.417
3-15-84	A490	1.000	532	25	07	0.375
3-13-84	A325	0.875	535	05	04	0.375
3-14-84	A325	0.875	535	11	03	0.333
3-13-84	A325	0.875	534	02	05	0.333
3-13-84	A325	0.875	535	05	07	0.333
3-14-84	A325	0.875	535	11	05	0.333
3-19-84	A325	0.875	533	27	02	0.333
3-19-84	A325	0.875	533	27	01	0.333
3-16-84	A325	0.875	533	34	04	0.333
3-13-84	A490	0.875	535	02	07	0.333
3-13-84	A325	0.875	535	05	02	0.333
3-13-84	A325	0.875	534	02	02	0.333
3-13-84	A325	0.875	535	05	06	0.333
3-13-84	A325	0.875	534	02	01	0.333
3-14-84	A325	0.875	535	25	01	0.333



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3-14-84	A325	0.875	535	11	04	0.333
3-16-84	A325	0.875	533	34	05	0.333
3-13-84	A325	0.875	535	05	05	0.292
3-14-84	A325	0.875	535	11	06	0.250
3-13-84	A325	0.875	531	06	03	0.250
4-6-84	A490	0.875	540	37	05	0.250
3-13-84	A325	0.875	531	06	04	0.250
3-23-84	A325	0.875	535	04	03	0.250
3-13-84	A325	0.875	531	06	05	0.250
3-13-84	A325	0.875	531	06	01	0.250
3-15-84	A490	1.000	532	25	06	0.250
3-16-84	A325	0.875	533	16	03	0.250
3-15-84	A325	0.875	536	05	03	0.250
3-14-84	A325	0.875	535	17	01	0.208
3-13-84	A490	0.875	535	15	06	0.208
3-15-84	A325	0.875	536	05	02	0.188
3-22-84	A325	0.875	535	27	07	0.167
3-13-84	A325	0.875	531	06	02	0.167
3-14-84	A325	0.875	530	11	04	0.167
3-16-84	A325	0.875	532	12	05	0.167
3-20-84	A490	0.875	535	38	02	0.167
3-16-84	A325	0.875	532	12	06	0.167
3-15-84	A325	0.875	536	05	01	0.167
3-16-84	A325	0.875	533	34	06	0.167
3-23-84	A325	0.875	535	04	02	0.167
3-16-84	A325	0.875	533	16	04	0.167
3-20-84	A490	0.875	535	30	13	0.167
3-23-84	A325	0.875	535	04	01	0.167
4-6-84	A490	1.375	540	10	06	0.167
3-15-84	A490	1.000	532	25	10	0.167
3-22-84	A325	0.875	535	27	02	0.167
3-13-84	A490	0.875	535	24	01	0.167
3-14-84	A325	0.875	532	01	01	0.167
3-15-84	A325	0.875	535	07	14	0.167
3-14-84	A325	0.875	532	01	07	0.167
3-14-84	A325	0.875	530	11	06	0.167
3-14-84	A325	0.875	532	02	07	0.167
3-14-84	A325	0.875	535	17	07	0.167
3-14-84	A325	0.875	535	11	07	0.167
3-22-84	A325	0.875	535	27	06	0.167
3-22-84	A325	0.875	535	27	03	0.167
4-6-84	A490	1.375	540	25	02	0.125
4-6-84	A490	1.375	540	24	04	0.125
3-13-84	A490	0.875	535	15	04	0.125
3-14-84	A325	0.875	532	01	05	0.083
4-6-84	A490	1.375	540	25	04	0.083
3-13-84	A325	0.875	531	01	01	0.083
3-14-84	A325	0.875	530	11	02	0.083
3-16-84	A325	0.875	532	12	04	0.083
3-14-84	A325	0.875	530	11	01	0.083
3-16-84	A325	0.875	532	12	03	0.083
3-14-84	A325	0.875	530	16	01	0.083
4-6-84	A490	1.375	540	10	01	0.083
3-14-84	A325	0.875	530	11	05	0.083
3-20-84	A490	0.875	535	23	05	0.083
3-14-84	A325	0.875	532	02	06	0.083



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3-13-84	A490	0.875	535	24	02	0.083
3-14-84	A325	0.875	530	12	08	0.083
3-13-84	A490	0.875	535	24	06	0.083
4-6-84	A490	1.375	540	16	05	0.083
3-15-84	A490	1.000	532	25	04	0.083
3-13-84	A325	0.875	531	01	04	0.083
3-13-84	A490	0.875	535	15	03	0.083
3-14-84	A325	0.875	530	12	09	0.083
3-15-84	A490	1.000	532	25	09	0.083
3-13-84	A490	0.875	535	02	05	0.083
4-6-84	A490	1.375	540	10	02	0.083
3-16-84	A325	0.875	533	34	01	0.083
4-6-84	A490	0.875	540	37	02	0.083
4-5-84	A490	1.375	540	03E	05	0.083
3-14-84	A325	0.875	535	17	02	0.083
3-13-84	A325	0.875	531	01	03	0.083
3-20-84	A490	0.875	534	08	06	0.083
3-14-84	A325	0.875	530	11	03	0.083
4-6-84	A490	1.375	540	12	06	0.083
3-14-84	A325	0.875	530	16	02	0.083
4-6-84	A490	1.375	540	18	06	0.083
3-14-84	A325	0.875	530	12	07	0.083
3-22-84	A325	0.875	535	27	05	0.083
3-14-84	A325	0.875	532	01	06	0.083
4-6-84	A490	1.375	540	18	03	0.083
3-14-84	A325	0.875	532	01	02	0.083
3-15-84	A325	0.875	535	07	06	0.083
3-16-84	A325	0.875	533	19	01	0.083
3-20-84	A490	0.875	535	21	02	0.083
4-6-84	A490	1.375	540	39	03	0.083
3-20-84	A490	0.875	535	30	05	0.083
4-6-84	A490	1.375	540	24	06	0.083
3-20-84	A325	0.875	532	26	03	0.083
3-14-84	A325	0.875	532	01	08	0.083
3-22-84	A325	0.875	535	27	08	0.083
3-13-84	A490	0.875	535	02	02	0.083
3-20-84	A490	0.875	535	30	07	0.083
3-16-84	A325	0.875	533	16	01	0.083
3-20-84	A490	0.875	535	38	06	0.083
3-14-84	A325	0.875	532	01	04	0.083
3-20-84	A325	0.875	532	26	01	0.083
4-6-84	A490	1.375	540	39	06	0.083
3-20-84	A490	0.875	535	30	03	0.083
4-5-84	A490	1.375	540	15W	03	0.042
4-6-84	A490	1.375	540	10	03	0.042
4-6-84	A490	1.375	540	38	04	0.042
4-5-84	A490	1.375	540	05E	01	0.042
3-20-84	A490	0.875	535	38	07	0.042
4-5-84	A490	1.375	540	04W	04	0.042
3-20-84	A490	0.875	535	21	01	0.042
3-22-84	A325	0.875	535	27	04	0.042
3-20-84	A490	0.875	535	38	03	0.042
4-6-84	A490	1.375	540	18	05	0.042
3-20-84	A490	0.875	535	38	01	0.042
3-13-84	A490	0.875	535	24	05	0.042
3-19-84	A325	0.875	533	27	04	0.042



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3-19-84	A325	0.875	533	23	06	0.042
4-9-84	A490	0.875	540	36E	03	0.042
3-13-84	A490	0.875	535	24	03	0.042
3-13-84	A490	0.875	535	15	02	0.042
4-6-84	A490	1.375	540	18	01	0.042
3-13-84	A490	0.875	535	02	03	0.042
4-6-84	A490	1.375	540	16	06	0.042
3-13-84	A325	0.875	534	04	04	0.042
4-6-84	A490	1.375	540	16	04	0.042
3-20-84	A490	0.875	535	38	04	0.042
3-14-84	A325	0.875	535	17	05	0.042
3-13-84	A490	0.875	535	02	04	0.042
3-16-84	A325	0.875	533	34	08	0.042
3-13-84	A490	0.875	535	15	01	0.042
4-6-84	A490	1.375	540	12	05	0.042
4-9-84	A490	0.875	540	36W	02	0.042
4-6-84	A490	1.375	540	39	05	0.042
4-6-84	A490	0.875	540	38	02	0.042
3-15-84	A325	0.875	535	07	12	0.042
3-14-84	A325	0.875	532	02	08	0.042
4-6-84	A490	1.375	540	40	04	0.042
3-20-84	A490	0.875	535	23	04	0.036
3-14-84	A325	0.875	532	01	03	0.031
3-23-84	A325	0.875	530	02	04	0.021
4-5-84	A490	1.375	540	05E	05	0.021
4-6-84	A490	1.375	540	23	05	0.021
3-13-84	A490	0.875	535	24	07	0.021
4-6-84	A490	1.375	540	23	02	0.021
3-16-84	A325	0.875	533	21	04	0.021
4-6-84	A490	1.375	540	25	01	0.021
3-16-84	A325	0.875	533	21	02	0.021
3-16-84	A325	0.875	533	34	02	0.021
3-16-84	A325	0.875	533	16	06	0.021
3-16-84	A325	0.875	533	34	07	0.021
3-15-84	A325	0.875	536	06	03	0.021
4-6-84	A490	1.375	540	18	02	0.021
3-15-84	A325	0.875	536	13	01	0.021
4-6-84	A490	1.375	540	18	04	0.021
3-16-84	A325	0.875	533	16	05	0.021
4-6-84	A490	1.375	540	24	05	0.021
3-13-84	A490	0.875	535	15	07	0.021
3-20-84	A490	0.875	535	30	01	0.021
3-23-84	A325	0.875	530	02	01	0.021
3-13-84	A490	0.875	535	24	04	0.021
3-20-84	A490	0.875	535	38	05	0.021
4-6-84	A490	1.375	540	26	06	0.021
3-13-84	A490	0.875	535	02	01	0.021
3-14-84	A325	0.875	535	17	06	0.021
3-20-84	A490	0.875	535	30	06	0.021
3-19-84	A325	0.875	533	27	03	0.000
3-14-84	A325	0.875	530	12	02	0.000
3-14-84	A325	0.875	530	12	03	0.000
3-20-84	A325	0.875	533	03	06	0.000
3-14-84	A325	0.875	530	12	04	0.000
3-20-84	A325	0.875	533	03	08	0.000
3-14-84	A325	0.875	530	12	05	0.000

3-20-84	A325	0.875	533	03	10	0.000
3-14-84	A325	0.875	530	12	06	0.000
3-20-84	A325	0.875	532	26	02	0.000
4-5-84	A490	1.375	540	04W	03	0.000
3-20-84	A325	0.875	532	26	04	0.000
4-5-84	A490	1.375	540	04W	02	0.000
3-20-84	A325	0.875	532	26	06	0.000
4-5-84	A490	1.375	540	04W	01	0.000
3-20-84	A325	0.875	532	26	08	0.000
4-5-84	A490	1.375	540	03E	06	0.000
3-20-84	A325	0.875	532	26	10	0.000
4-5-84	A490	1.375	540	03E	04	0.000
3-20-84	A325	0.875	532	27	02	0.000
4-5-84	A490	1.375	540	03E	03	0.000
3-20-84	A325	0.875	532	27	04	0.000
4-5-84	A490	1.375	540	03E	02	0.000
3-20-84	A325	0.875	533	03	02	0.000
4-5-84	A490	1.375	540	03E	01	0.000
3-13-84	A490	0.875	535	02	06	0.000
4-5-84	A490	1.375	540	02W	06	0.000
3-13-84	A325	0.875	535	03	04	0.000
4-5-84	A490	1.375	540	02W	05	0.000
3-22-84	A325	0.875	535	27	01	0.000
4-5-84	A490	1.375	540	02W	04	0.000
3-20-84	A490	0.875	535	23	02	0.000
4-5-84	A490	1.375	540	02W	03	0.000
3-23-84	A325	0.875	538	04	03	0.000
4-5-84	A490	1.375	540	02W	02	0.000
3-20-84	A490	0.875	535	23	06	0.000
4-5-84	A490	1.375	540	02W	01	0.000
3-23-84	A325	0.875	538	04	01	0.000
4-6-84	A490	1.375	540	16	03	0.000
3-23-84	A325	0.875	531	04	07	0.000
4-6-84	A490	1.375	540	16	02	0.000
3-23-84	A325	0.875	531	04	05	0.000
4-6-84	A490	1.375	540	16	01	0.000
3-23-84	A325	0.875	531	04	03	0.000
3-14-84	A325	0.875	535	20	01	0.000
3-20-84	A490	0.875	535	30	02	0.000
3-14-84	A325	0.875	535	20	02	0.000
3-20-84	A490	0.875	535	30	04	0.000
3-14-84	A325	0.875	535	20	03	0.000
3-23-84	A325	0.875	530	02	03	0.000
3-14-84	A325	0.875	535	20	04	0.000
3-20-84	A490	0.875	535	30	01	0.000
3-14-84	A325	0.875	535	20	05	0.000
3-20-84	A490	0.875	535	30	03	0.000
3-14-84	A325	0.875	535	20	06	0.000
3-20-84	A490	0.875	535	30	05	0.000
3-14-84	A325	0.875	535	20	07	0.000
3-23-84	A325	0.875	530	02	02	0.000
4-6-84	A490	1.375	540	12	04	0.000
3-20-84	A490	0.875	535	30	14	0.000
4-6-84	A490	1.375	540	12	03	0.000
3-20-84	A490	0.875	534	23	02	0.000
4-6-84	A490	1.375	540	12	02	0.000

3-20-84	A490	0.875	534	23	04	0.000
4-6-84	A490	1.375	540	12	01	0.000
3-20-84	A490	0.875	534	23	06	0.000
4-6-84	A490	1.375	540	10	05	0.000
3-20-84	A490	0.875	534	20	03	0.000
4-6-84	A490	1.375	540	10	04	0.000
3-20-84	A490	0.875	534	08	02	0.000
4-6-84	A490	1.375	540	26	05	0.000
3-20-84	A490	0.875	534	08	04	0.000
3-14-84	A325	0.875	535	37	01	0.000
4-4-84	A325	0.875	532	21	09	0.000
3-14-84	A325	0.875	535	37	02	0.000
3-19-84	A325	0.875	532	17	01	0.000
3-14-84	A325	0.875	535	37	03	0.000
3-19-84	A325	0.875	532	17	03	0.000
3-14-84	A325	0.875	535	37	04	0.000
3-19-84	A325	0.875	532	17	05	0.000
3-14-84	A325	0.875	535	37	05	0.000
3-19-84	A325	0.875	532	17	07	0.000
3-14-84	A325	0.875	535	37	06	0.000
4-4-84	A325	0.875	532	21	08	0.000
3-14-84	A325	0.875	535	37	07	0.000
4-4-84	A325	0.875	532	21	06	0.000
3-14-84	A325	0.875	535	37	08	0.000
4-4-84	A325	0.875	532	21	04	0.000
3-14-84	A325	0.875	535	35	01	0.000
3-19-84	A325	0.875	533	20	01	0.000
3-14-84	A325	0.875	535	35	02	0.000
3-19-84	A325	0.875	533	20	03	0.000
3-14-84	A325	0.875	535	35	03	0.000
3-19-84	A325	0.875	533	20	05	0.000
3-14-84	A325	0.875	535	35	04	0.000
3-19-84	A325	0.875	533	20	07	0.000
3-14-84	A325	0.875	535	35	05	0.000
4-4-84	A325	0.875	532	21	02	0.000
3-14-84	A325	0.875	535	35	06	0.000
4-9-84	A490	0.875	540	36W	01	0.000
3-14-84	A325	0.875	535	35	07	0.000
3-19-84	A325	0.875	533	27	05	0.000
3-13-84	A325	0.875	530	05	01	0.000
3-19-84	A325	0.875	533	23	01	0.000
3-13-84	A325	0.875	530	05	02	0.000
3-19-84	A325	0.875	533	23	03	0.000
3-13-84	A325	0.875	530	05	03	0.000
3-19-84	A325	0.875	533	23	05	0.000
3-13-84	A325	0.875	530	05	04	0.000
3-16-84	A325	0.875	532	12	01	0.000
3-13-84	A325	0.875	530	05	05	0.000
4-4-84	A490	1.000	532	24	08	0.000
3-13-84	A325	0.875	530	05	06	0.000
4-4-84	A490	1.000	532	24	06	0.000
3-13-84	A325	0.875	530	05	07	0.000
3-16-84	A325	0.875	532	13	01	0.000
3-13-84	A325	0.875	530	05	08	0.000
3-16-84	A325	0.875	532	13	03	0.000
4-6-84	A490	1.375	540	26	04	0.000

3-16-84	A325	0.875	532	13	05	0.000
4-6-84	A490	1.375	540	26	03	0.000
3-16-84	A325	0.875	532	13	07	0.000
4-6-84	A490	1.375	540	26	02	0.000
3-16-84	A325	0.875	532	07	01	0.000
4-6-84	A490	1.375	540	26	01	0.000
3-16-84	A325	0.875	532	07	03	0.000
4-6-84	A490	1.375	540	25	06	0.000
3-16-84	A325	0.875	532	07	05	0.000
4-6-84	A490	1.375	540	25	05	0.000
3-16-84	A325	0.875	532	07	07	0.000
3-13-84	A325	0.875	531	01	02	0.000
3-16-84	A325	0.875	532	07	09	0.000
4-6-84	A490	1.375	540	25	03	0.000
3-16-84	A325	0.875	532	08	02	0.000
4-6-84	A490	1.375	540	24	03	0.000
3-16-84	A325	0.875	532	08	04	0.000
4-6-84	A490	1.375	540	24	02	0.000
3-16-84	A325	0.875	532	08	06	0.000
3-13-84	A325	0.875	531	02	01	0.000
3-16-84	A325	0.875	533	08	02	0.000
3-13-84	A325	0.875	531	02	02	0.000
3-16-84	A325	0.875	533	08	04	0.000
3-13-84	A325	0.875	531	02	03	0.000
3-16-84	A325	0.875	533	08	06	0.000
3-13-84	A325	0.875	531	02	04	0.000
3-16-84	A325	0.875	533	08	08	0.000
3-13-84	A325	0.875	531	02	05	0.000
3-16-84	A325	0.875	533	15	02	0.000
3-13-84	A325	0.875	531	02	06	0.000
3-16-84	A325	0.875	533	15	04	0.000
3-13-84	A325	0.875	531	02	07	0.000
3-16-84	A325	0.875	533	15	06	0.000
3-13-84	A325	0.875	534	03	01	0.000
4-4-84	A490	1.000	532	24	03	0.000
3-13-84	A325	0.875	534	03	02	0.000
4-4-84	A490	1.000	532	24	01	0.000
3-13-84	A325	0.875	534	03	03	0.000
4-5-84	A325	1.000	533	05	09	0.000
3-13-84	A325	0.875	534	03	04	0.000
3-16-84	A325	0.875	533	19	02	0.000
3-13-84	A325	0.875	534	04	01	0.000
3-16-84	A325	0.875	533	19	04	0.000
3-13-84	A325	0.875	534	04	02	0.000
3-16-84	A325	0.875	533	19	06	0.000
3-13-84	A325	0.875	534	04	03	0.000
4-5-84	A325	1.000	533	05	07	0.000
4-6-84	A490	1.375	540	24	01	0.000
4-5-84	A325	1.000	533	05	06	0.000
4-6-84	A490	1.375	540	23	06	0.000
3-16-84	A325	0.875	533	21	06	0.000
4-6-84	A490	1.375	540	23	04	0.000
4-5-84	A325	1.000	533	05	04	0.000
4-6-84	A490	1.375	540	23	03	0.000
4-5-84	A490	1.375	540	15E	05	0.000
4-6-84	A490	1.375	540	23	01	0.000

4-5-84	A490	1.375	540	15E	03	0.000
4-6-84	A490	1.375	540	40	06	0.000
4-5-84	A490	1.375	540	15E	01	0.000
4-6-84	A490	1.375	540	40	05	0.000
3-14-84	A325	0.875	532	02	02	0.000
4-6-84	A490	1.375	540	40	03	0.000
3-14-84	A325	0.875	532	02	04	0.000
3-13-84	A325	0.875	534	11	01	0.000
4-5-84	A490	1.375	540	15W	06	0.000
3-13-84	A325	0.875	534	11	02	0.000
4-5-84	A490	1.375	540	15W	04	0.000
3-13-84	A325	0.875	534	11	03	0.000
4-5-84	A490	1.375	540	15W	02	0.000
3-13-84	A325	0.875	534	11	04	0.000
3-14-84	A325	0.875	530	16	03	0.000
3-13-84	A325	0.875	534	11	05	0.000
3-14-84	A325	0.875	530	16	05	0.000
3-13-84	A325	0.875	534	11	06	0.000
3-14-84	A325	0.875	530	16	07	0.000
3-13-84	A325	0.875	534	11	07	0.000
3-14-84	A325	0.875	530	18	01	0.000
3-13-84	A325	0.875	534	13	01	0.000
3-14-84	A325	0.875	530	18	03	0.000
3-13-84	A325	0.875	534	13	02	0.000
3-14-84	A325	0.875	530	18	05	0.000
3-13-84	A325	0.875	534	13	03	0.000
3-14-84	A325	0.875	530	18	07	0.000
3-13-84	A325	0.875	534	13	04	0.000
4-5-84	A490	1.375	540	05E	04	0.000
3-13-84	A325	0.875	534	13	05	0.000
4-5-84	A490	1.375	540	05E	02	0.000
3-13-84	A325	0.875	534	13	06	0.000
4-5-84	A490	1.375	540	04W	05	0.000
3-13-84	A325	0.875	534	13	07	0.000
3-20-84	A325	0.875	533	03	05	0.000
3-13-84	A325	0.875	534	14	01	0.000
3-20-84	A325	0.875	533	03	09	0.000
3-13-84	A325	0.875	534	14	02	0.000
3-20-84	A325	0.875	533	03	03	0.000
3-13-84	A325	0.875	534	14	03	0.000
3-20-84	A325	0.875	532	26	07	0.000
3-13-84	A325	0.875	534	14	04	0.000
3-20-84	A325	0.875	532	27	01	0.000
3-13-84	A325	0.875	534	14	05	0.000
3-20-84	A325	0.875	532	27	05	0.000
3-13-84	A325	0.875	534	14	06	0.000
3-13-84	A325	0.875	535	03	05	0.000
3-13-84	A325	0.875	534	14	07	0.000
3-20-84	A490	0.875	535	23	01	0.000
3-13-84	A325	0.875	534	14	08	0.000
3-23-84	A325	0.875	538	04	02	0.000
3-13-84	A325	0.875	534	15	01	0.000
3-23-84	A325	0.875	531	04	08	0.000
3-13-84	A325	0.875	534	15	02	0.000
3-23-84	A325	0.875	531	04	04	0.000
3-13-84	A325	0.875	534	15	03	0.000

3-23-84	A325	0.875	531	04	01	0.000
3-13-84	A325	0.875	534	15	04	0.000
3-20-84	A490	0.875	535	30	07	0.000
3-13-84	A325	0.875	534	15	05	0.000
3-20-84	A490	0.875	535	30	04	0.000
3-13-84	A325	0.875	534	15	06	0.000
4-4-84	A325	0.875	532	21	10	0.000
3-13-84	A325	0.875	534	15	07	0.000
3-20-84	A490	0.875	534	23	03	0.000
3-13-84	A325	0.875	534	22	01	0.000
3-20-84	A490	0.875	534	23	07	0.000
3-13-84	A325	0.875	534	22	02	0.000
3-20-84	A490	0.875	534	08	03	0.000
3-13-84	A325	0.875	534	22	03	0.000
3-20-84	A490	0.875	534	08	07	0.000
3-13-84	A325	0.875	534	22	04	0.000
3-19-84	A325	0.875	532	17	04	0.000
3-13-84	A325	0.875	534	22	05	0.000
3-19-84	A325	0.875	532	17	08	0.000
3-13-84	A325	0.875	534	22	06	0.000
4-4-84	A325	0.875	532	21	05	0.000
3-13-84	A325	0.875	534	22	07	0.000
3-19-84	A325	0.875	533	20	02	0.000
3-16-84	A325	0.875	533	22	01	0.000
3-19-84	A325	0.875	533	20	06	0.000
3-16-84	A325	0.875	533	22	02	0.000
4-4-84	A325	0.875	532	21	01	0.000
3-16-84	A325	0.875	533	22	03	0.000
3-19-84	A325	0.875	533	27	06	0.000
3-16-84	A325	0.875	533	22	04	0.000
3-19-84	A325	0.875	533	23	04	0.000
3-16-84	A325	0.875	533	22	05	0.000
3-16-84	A325	0.875	532	12	02	0.000
3-16-84	A325	0.875	533	22	06	0.000
4-4-84	A490	1.000	532	24	05	0.000
3-16-84	A325	0.875	533	22	07	0.000
3-16-84	A325	0.875	532	13	04	0.000
3-16-84	A325	0.875	533	29	08	0.000
3-16-84	A325	0.875	532	13	08	0.000
3-16-84	A325	0.875	533	29	09	0.000
3-16-84	A325	0.875	532	07	04	0.000
3-16-84	A325	0.875	533	29	10	0.000
3-16-84	A325	0.875	532	07	08	0.000
3-16-84	A325	0.875	533	29	11	0.000
3-16-84	A325	0.875	532	08	03	0.000
3-16-84	A325	0.875	533	29	12	0.000
3-16-84	A325	0.875	533	08	01	0.000
3-16-84	A325	0.875	533	26	01	0.000
3-16-84	A325	0.875	533	08	05	0.000
3-16-84	A325	0.875	533	26	02	0.000
3-16-84	A325	0.875	533	15	01	0.000
3-16-84	A325	0.875	533	26	03	0.000
3-16-84	A325	0.875	533	15	05	0.000
3-16-84	A325	0.875	533	26	04	0.000
4-4-84	A490	1.000	532	24	02	0.000
3-16-84	A325	0.875	533	26	05	0.000



**STRUCTURAL
INTEGRITY
ASSOCIATES, INC.**

4-5-84	A325	1.000	533	05	08	0.000
3-16-84	A325	0.875	533	26	06	0.000
3-16-84	A325	0.875	533	19	05	0.000
3-16-84	A325	0.875	533	26	07	0.000
3-16-84	A325	0.875	533	21	03	0.000
3-16-84	A325	0.875	533	26	08	0.000
4-5-84	A325	1.000	533	05	05	0.000
3-16-84	A325	0.875	533	24	01	0.000
4-5-84	A490	1.375	540	15E	04	0.000
3-16-84	A325	0.875	533	24	02	0.000
3-14-84	A325	0.875	532	02	01	0.000
3-16-84	A325	0.875	533	24	03	0.000
3-14-84	A325	0.875	532	02	05	0.000
3-16-84	A325	0.875	533	24	04	0.000
3-14-84	A325	0.875	532	02	09	0.000
3-16-84	A325	0.875	533	24	05	0.000
3-14-84	A325	0.875	530	16	04	0.000
3-16-84	A325	0.875	533	24	06	0.000
3-14-84	A325	0.875	530	16	08	0.000
3-16-84	A325	0.875	533	24	07	0.000
3-14-84	A325	0.875	530	18	04	0.000
3-16-84	A325	0.875	533	24	08	0.000
4-5-84	A490	1.375	540	05E	06	0.000
4-6-84	A490	1.375	540	40	02	0.000
4-5-84	A490	1.375	540	04W	06	0.000
4-6-84	A490	1.375	540	40	01	0.000
3-20-84	A325	0.875	533	03	07	0.000
3-16-84	A325	0.875	533	34	03	0.000
3-20-84	A325	0.875	532	26	05	0.000
4-6-84	A490	1.375	540	39	04	0.000
3-20-84	A325	0.875	532	27	03	0.000
4-6-84	A490	1.375	540	39	02	0.000
3-13-84	A325	0.875	535	03	03	0.000
4-6-84	A490	1.375	540	39	01	0.000
3-20-84	A490	0.875	535	23	07	0.000
4-6-84	A490	1.375	540	38	06	0.000
3-23-84	A325	0.875	531	04	02	0.000
4-6-84	A490	1.375	540	38	05	0.000
3-20-84	A490	0.875	535	30	02	0.000
3-16-84	A325	0.875	533	33	01	0.000
3-20-84	A490	0.875	534	23	01	0.000
3-16-84	A325	0.875	533	33	02	0.000
3-20-84	A490	0.875	534	08	01	0.000
3-16-84	A325	0.875	533	33	03	0.000
3-19-84	A325	0.875	532	17	02	0.000
3-16-84	A325	0.875	533	33	04	0.000
4-4-84	A325	0.875	532	21	07	0.000
3-16-84	A325	0.875	533	33	05	0.000
3-19-84	A325	0.875	533	20	04	0.000
3-16-84	A325	0.875	533	33	06	0.000
4-4-84	A490	1.000	532	24	10	0.000
3-16-84	A325	0.875	533	33	07	0.000
4-4-84	A490	1.000	532	24	09	0.000
3-16-84	A325	0.875	533	33	08	0.000
3-16-84	A325	0.875	532	13	02	0.000
4-6-84	A490	0.875	540	38	03	0.000

3-16-84	A325	0.875	532	07	02	0.000
3-15-84	A490	1.000	532	25	05	0.000
3-16-84	A325	0.875	532	08	01	0.000
4-6-84	A490	0.875	540	38	01	0.000
3-16-84	A325	0.875	533	08	03	0.000
4-6-84	A490	0.875	540	37	06	0.000
3-16-84	A325	0.875	533	15	03	0.000
4-6-84	A490	0.875	540	37	04	0.000
4-5-84	A325	1.000	533	05	10	0.000
4-6-84	A490	0.875	540	37	03	0.000
3-16-84	A325	0.875	533	21	01	0.000
3-15-84	A325	0.875	536	15	01	0.000
4-5-84	A490	1.375	540	15E	06	0.000
3-15-84	A325	0.875	536	15	02	0.000
3-14-84	A325	0.875	532	02	03	0.000
3-15-84	A325	0.875	536	15	03	0.000
4-5-84	A490	1.375	540	15W	01	0.000
3-15-84	A325	0.875	536	16	01	0.000
3-14-84	A325	0.875	530	18	02	0.000
3-15-84	A325	0.875	536	16	02	0.000
4-5-84	A490	1.375	540	05E	03	0.000
3-15-84	A325	0.875	536	16	03	0.000
3-20-84	A325	0.875	533	03	04	0.000
3-15-84	A325	0.875	536	14	01	0.000
3-20-84	A325	0.875	533	03	01	0.000
3-15-84	A325	0.875	536	14	02	0.000
3-23-84	A325	0.875	531	04	06	0.000
3-15-84	A325	0.875	536	14	03	0.000
3-20-84	A490	0.875	535	30	06	0.000
3-15-84	A325	0.875	536	06	01	0.000
3-20-84	A490	0.875	534	08	05	0.000
3-15-84	A325	0.875	536	06	02	0.000
4-4-84	A325	0.875	532	21	03	0.000
4-6-84	A490	0.875	540	37	01	0.000
3-19-84	A325	0.875	533	23	02	0.000
4-9-84	A490	0.875	540	36E	06	0.000
3-16-84	A325	0.875	532	13	06	0.000
3-15-84	A325	0.875	536	13	02	0.000
3-16-84	A325	0.875	532	08	05	0.000
3-15-84	A325	0.875	536	13	03	0.000
4-4-84	A490	1.000	532	24	04	0.000
3-15-84	A325	0.875	536	08	01	0.000
3-16-84	A325	0.875	533	21	05	0.000
3-15-84	A325	0.875	536	08	02	0.000
4-5-84	A490	1.375	540	15W	05	0.000
3-15-84	A325	0.875	536	08	03	0.000
3-14-84	A325	0.875	530	18	06	0.000
4-9-84	A490	0.875	540	36E	05	0.000
3-20-84	A325	0.875	532	26	09	0.000
4-9-84	A490	0.875	540	36E	04	0.000
3-23-84	A325	0.875	530	02	05	0.000
4-9-84	A490	0.875	540	36E	02	0.000
3-19-84	A325	0.875	532	17	06	0.000
4-9-84	A490	0.875	540	36E	01	0.000
4-4-84	A490	1.000	532	24	07	0.000
4-9-84	A490	0.875	540	36W	06	0.000

3-16-84	A325	0.875	533	08	07	0.000
4-9-84	A490	0.875	540	36W	05	0.000
4-5-84	A490	1.375	540	15E	02	0.000
3-15-84	A325	0.875	535	07	08	0.000
3-14-84	A325	0.875	530	12	01	0.000
3-15-84	A325	0.875	535	07	09	0.000
3-20-84	A490	0.875	534	23	05	0.000
3-15-84	A325	0.875	535	07	10	0.000
3-16-84	A325	0.875	532	07	06	0.000
3-15-84	A325	0.875	535	07	11	0.000
3-14-84	A325	0.875	530	16	06	0.000
4-9-84	A490	0.875	540	36W	04	0.000
3-19-84	A325	0.875	533	20	08	0.000
3-20-84	A490	0.875	535	23	03	0.000
3-16-84	A325	0.875	533	19	03	0.000
3-15-84	A325	0.875	535	07	13	0.000
4-9-84	A490	0.875	540	36W	03	0.000

APPENDIX D

PALO VERDE UNIT 3 HIGH STRENGTH BOLT TORQUE CHECK
FOR CRITICAL FRICTION FASTENERS

PALO VERDE UNIT 3 HIGH STRENGTH BOLT TORQUE

INSP. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONN. NO.	BOLT NO.	NUT ROTAT	TORQUE
4-24-84	A490	1.375	535	53	01		2385.000
4-24-84	A490	1.375	535	53	02		2385.000
4-24-84	A490	1.375	535	53	03		2385.000
4-24-84	A490	1.375	535	53	04		2385.000
4-24-84	A490	1.375	535	53	05		2385.000
4-24-84	A490	1.375	535	53	06		2385.000
4-24-84	A490	1.375	535	54	01		2385.000
4-24-84	A490	1.375	535	54	02		2385.000
4-24-84	A490	1.375	535	54	03		2385.000
4-24-84	A490	1.375	535	54	04		2385.000
4-24-84	A490	1.375	535	54	05		2385.000
4-24-84	A490	1.375	535	54	06		2385.000
4-24-84	A490	1.375	535	55	01		2385.000
4-24-84	A490	1.375	535	55	02		2385.000
4-24-84	A490	1.375	535	55	03		2385.000
4-24-84	A490	1.375	535	55	04		2385.000
4-24-84	A490	1.375	535	55	05		2385.000
4-24-84	A490	1.375	535	55	06		2385.000
4-24-84	A490	1.375	535	56	01		2385.000
4-24-84	A490	1.375	535	56	02		2385.000
4-24-84	A490	1.375	535	56	03		2385.000
4-24-84	A490	1.375	535	56	04		2385.000
4-24-84	A490	1.375	535	56	05		2385.000
4-24-84	A490	1.375	535	56	06		2385.000
4-20-84	A490	1.375	535	49	01		2385.000
4-20-84	A490	1.375	535	49	02		2385.000
4-20-84	A490	1.375	535	49	03		2385.000
4-20-84	A490	1.375	535	49	04		2385.000
4-20-84	A490	1.375	535	49	05		2385.000
4-20-84	A490	1.375	535	49	06		2385.000
4-20-84	A490	1.375	535	50	01		2385.000
4-20-84	A490	1.375	535	50	02		2385.000
4-20-84	A490	1.375	535	50	03		2385.000
4-20-84	A490	1.375	535	50	04		2385.000
4-20-84	A490	1.375	535	50	05		2385.000
4-20-84	A490	1.375	535	50	06		2385.000
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4-20-84	A490	1.375	535	51	02		2385.000
4-20-84	A490	1.375	535	51	03		2385.000
4-20-84	A490	1.375	535	51	04		2385.000
4-20-84	A490	1.375	535	51	05		2385.000
4-20-84	A490	1.375	535	51	06		2385.000
4-20-84	A490	1.375	535	52	01		2385.000
4-20-84	A490	1.375	535	52	02		2385.000
4-20-84	A490	1.375	535	52	03		2385.000
4-20-84	A490	1.375	535	52	04		2385.000
4-20-84	A490	1.375	535	52	05		2385.000
4-20-84	A490	1.375	535	52	06		2385.000
4-19-84	A490	1.375	535	43	01		2385.000
4-19-84	A490	1.375	535	43	02		2385.000
4-19-84	A490	1.375	535	43	03		2385.000
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4-19-84	A490	1.375	535	43	05		2385.000

4-19-84	A490	1.375	535	43	06	
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4-19-84	A490	1.375	535	44	02	2385.000
4-19-84	A490	1.375	535	44	03	2385.000
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4-19-84	A490	1.375	535	44	05	2385.000
4-19-84	A490	1.375	535	44	06	2385.000
4-19-84	A490	1.375	535	45	01	2385.000
4-19-84	A490	1.375	535	45	02	2385.000
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4-19-84	A490	1.375	535	45	04	2385.000
4-19-84	A490	1.375	535	45	05	2385.000
4-19-84	A490	1.375	535	45	06	2385.000
4-19-84	A490	1.375	535	46	01	2385.000
4-19-84	A490	1.375	535	46	02	2385.000
4-19-84	A490	1.375	535	46	03	2385.000
4-19-84	A490	1.375	535	46	04	2385.000
4-19-84	A490	1.375	535	46	05	2385.000
4-19-84	A490	1.375	535	46	06	2385.000
4-19-84	A490	1.375	534	35	01	2385.000
4-19-84	A490	1.375	534	35	02	2385.000
4-19-84	A490	1.375	534	35	03	2385.000
4-19-84	A490	1.375	534	35	04	2385.000
4-19-84	A490	1.375	534	35	05	2385.000
4-19-84	A490	1.375	534	35	06	2385.000
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4-19-84	A490	1.375	534	38	06	2385.000
4-18-84	A490	1.375	534	27	01	2385.000
4-18-84	A490	1.375	534	27	02	2385.000
4-18-84	A490	1.375	534	27	03	2385.000
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4-18-84	A490	1.375	534	28	04	2385.000
4-18-84	A490	1.375	534	28	05	2385.000
4-18-84	A490	1.375	534	28	06	2385.000
4-18-84	A490	1.375	534	33	01	2385.000

4-18-84	A490	1.375	534	33	02	
4-18-84	A490	1.375	534	33	03	2385.000
4-18-84	A490	1.375	534	33	04	2385.000
4-18-84	A490	1.375	534	33	05	2385.000
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4-18-84	A490	1.375	534	34	02	2385.000
4-18-84	A490	1.375	534	34	03	2385.000
4-18-84	A490	1.375	534	34	04	2385.000
4-18-84	A490	1.375	534	34	05	2385.000
4-18-84	A490	1.375	534	34	06	2385.000
3-23-84	A325	0.875	532	09	01	0.500
3-22-84	A325	0.875	530	17	06	0.417
3-23-84	A325	0.875	531	02	04	0.333
3-26-84	A325	0.875	532	21	03	0.250
3-22-84	A325	0.875	530	03	02	0.250
3-26-84	A325	0.875	532	21	02	0.250
3-27-84	A325	0.875	535	06	08	0.208
3-26-84	A325	0.875	532	27	01	0.167
3-22-84	A325	0.875	530	16	05	0.167
3-22-84	A325	0.875	530	03	08	0.167
3-22-84	A325	0.875	530	03	04	0.167
3-23-84	A325	0.875	530	03	06	0.083
3-23-84	A325	0.875	531	02	03	0.083
3-22-84	A325	0.875	530	02	02	0.083
3-23-84	A325	0.875	531	03	03	0.083
3-28-84	A325	0.875	535	02	01	0.083
3-27-84	A325	0.875	535	13	02	0.083
3-22-84	A325	0.875	530	28	01	0.083
3-22-84	A325	0.875	530	03	01	0.083
4-3-84	A325	0.875	529	01	03	0.083
3-26-84	A325	0.875	533	03	01	0.083
3-22-84	A325	0.875	530	09	06	0.083
3-22-84	A325	0.875	530	03	07	0.042
3-29-84	A490	0.875	535	16	04	0.042
3-28-84	A490	0.875	534	23	06	0.042
3-28-84	A490	0.875	534	08	02	0.042
3-27-84	A325	0.875	535	08	01	0.042
3-22-84	A325	0.875	530	06	09	0.042
3-27-84	A325	0.875	534	16	03	0.042
3-29-84	A490	0.875	535	10	09	0.042
3-22-84	A325	0.875	530	23	01	0.042
3-27-84	A325	0.875	535	17	07	0.042
3-28-84	A490	0.875	534	06	12	0.021
3-28-84	A490	0.875	534	09	03	0.021
3-27-84	A325	0.875	535	09	02	0.021
3-28-84	A490	0.875	534	06	10	0.021
3-28-84	A490	0.875	534	09	01	0.021
3-22-84	A325	0.875	530	09	07	0.021
3-28-84	A490	0.875	534	16	02	0.021
3-29-84	A490	0.875	535	09	05	0.021
3-28-84	A490	0.875	534	02	01	0.021
3-22-84	A325	0.875	530	08	03	0.021
3-28-84	A490	0.875	534	16	07	0.021
3-26-84	A325	0.875	534	09	06	0.021
3-26-84	A325	0.875	534	07	07	0.021

3-28-84	A490	0.875	534	09		
3-29-84	A490	0.875	535	23	04	0.021
3-27-84	A325	0.875	534	21	05	0.021
3-27-84	A325	0.875	534	10	10	0.000
3-29-84	A490	0.875	535	33	05	0.000
3-27-84	A325	0.875	534	10	10	0.000
3-29-84	A490	0.875	535	33	06	0.000
3-27-84	A325	0.875	534	10	12	0.000
3-29-84	A490	0.875	535	33	07	0.000
3-27-84	A325	0.875	534	10	14	0.000
3-29-84	A490	0.875	535	29	08	0.000
3-30-84	A490	1.000	532	25	02	0.000
3-29-84	A490	0.875	535	29	05	0.000
3-27-84	A325	0.875	534	12	04	0.000
3-29-84	A490	0.875	535	29	01	0.000
3-27-84	A325	0.875	534	12	06	0.000
3-29-84	A490	0.875	535	30	02	0.000
3-27-84	A325	0.875	534	12	01	0.000
3-29-84	A490	0.875	535	30	03	0.000
3-27-84	A325	0.875	534	12	03	0.000
3-29-84	A490	0.875	535	30	04	0.000
3-27-84	A325	0.875	534	12	05	0.000
3-29-84	A490	0.875	535	30	05	0.000
3-27-84	A325	0.875	534	12	08	0.000
3-29-84	A490	0.875	535	23	06	0.000
3-27-84	A325	0.875	534	12	02	0.000
3-29-84	A490	0.875	535	23	07	0.000
3-27-84	A325	0.875	534	12	04	0.000
3-29-84	A490	0.875	535	12	08	0.000
3-26-84	A325	0.875	533	14	07	0.000
3-29-84	A490	0.875	535	24	01	0.000
3-26-84	A325	0.875	533	14	01	0.000
3-29-84	A490	0.875	535	24	02	0.000
3-26-84	A325	0.875	533	14	03	0.000
3-29-84	A490	0.875	535	24	03	0.000
3-26-84	A325	0.875	533	14	05	0.000
3-29-84	A490	0.875	535	24	04	0.000
3-26-84	A325	0.875	533	14	07	0.000
3-29-84	A490	0.875	535	02	05	0.000
3-26-84	A325	0.875	533	14	02	0.000
3-29-84	A490	0.875	535	02	06	0.000
3-26-84	A325	0.875	533	14	04	0.000
3-29-84	A490	0.875	535	02	07	0.000
3-26-84	A325	0.875	533	14	06	0.000
3-29-84	A490	0.875	535	02	08	0.000
3-26-84	A325	0.875	533	09	01	0.000
3-29-84	A490	0.875	535	16	01	0.000
3-26-84	A325	0.875	533	09	03	0.000
3-29-84	A490	0.875	535	16	02	0.000
3-26-84	A325	0.875	533	09	05	0.000
3-29-84	A490	0.875	536	16	03	0.000
3-26-84	A325	0.875	533	16	07	0.000
3-28-84	A325	0.875	536	14	04	0.000
3-26-84	A325	0.875	533	16	02	0.000
3-28-84	A325	0.875	533	16	05	0.000
3-26-84	A325	0.875	536	15	01	0.000
				16	06	0.000

3-28-84	A325	0.875	536	15	03	0.000
3-26-84	A325	0.875	533	18	01	0.000
3-28-84	A325	0.875	536	16	02	0.000
3-26-84	A325	0.875	533	18	02	0.000
3-28-84	A325	0.875	536	17	01	0.000
3-26-84	A325	0.875	533	18	03	0.000
3-28-84	A325	0.875	536	17	03	0.000
3-26-84	A325	0.875	533	18	04	0.000
3-29-84	A490	0.875	535	33	05	0.000
3-26-84	A325	0.875	533	18	05	0.000
3-28-84	A325	0.875	535	13	04	0.000
3-26-84	A325	0.875	533	18	06	0.000
3-28-84	A325	0.875	535	13	06	0.000
3-26-84	A325	0.875	533	18	07	0.000
3-28-84	A325	0.875	535	17	01	0.000
3-26-84	A325	0.875	533	08	01	0.000
3-28-84	A325	0.875	535	17	03	0.000
3-26-84	A325	0.875	533	08	02	0.000
3-28-84	A325	0.875	535	17	05	0.000
3-26-84	A325	0.875	533	08	03	0.000
3-28-84	A325	0.875	535	17	07	0.000
3-26-84	A325	0.875	533	08	04	0.000
3-29-84	A490	0.875	535	33	03	0.000
3-26-84	A325	0.875	533	08	05	0.000
3-29-84	A490	0.875	535	33	01	0.000
3-26-84	A325	0.875	533	08	06	0.000
3-29-84	A490	0.875	535	31	06	0.000
3-26-84	A325	0.875	533	08	07	0.000
3-29-84	A490	0.875	535	31	07	0.000
3-26-84	A325	0.875	533	08	04	0.000
3-29-84	A490	0.875	535	31	08	0.000
3-26-84	A325	0.875	533	09	02	0.000
3-28-84	A490	0.875	534	08	01	0.000
3-26-84	A325	0.875	533	09	05	0.000
3-28-84	A490	0.875	534	08	02	0.000
3-26-84	A325	0.875	533	09	07	0.000
3-27-84	A325	0.875	536	01	03	0.000
3-26-84	A325	0.875	533	09	02	0.000
3-27-84	A325	0.875	536	02	04	0.000
3-26-84	A325	0.875	533	09	01	0.000
3-27-84	A325	0.875	536	02	05	0.000
3-30-84	A490	1.000	532	25	03	0.000
3-27-84	A325	0.875	536	03	04	0.000
3-26-84	A325	0.875	533	09	02	0.000
3-27-84	A325	0.875	536	04	07	0.000
3-26-84	A325	0.875	533	09	01	0.000
3-27-84	A325	0.875	536	04	08	0.000
3-26-84	A325	0.875	533	09	03	0.000
3-27-84	A325	0.875	536	05	09	0.000
3-26-84	A325	0.875	533	09	02	0.000
3-27-84	A325	0.875	536	06	10	0.000
3-30-84	A490	1.000	532	24	01	0.000
3-27-84	A325	0.875	536	06	10	0.000
3-26-84	A325	0.875	532	27	03	0.000
3-27-84	A325	0.875	533	26	02	0.000
3-26-84	A325	0.875	532	27	02	0.000
3-26-84	A325	0.875	532	27	03	0.000

3-27-84	A325	0.875	533	26	04	0.000
3-26-84	A325	0.875	532	27	04	0.000
3-27-84	A325	0.875	533	26	06	0.000
3-26-84	A325	0.875	532	27	05	0.000
3-26-84	A325	0.875	533	26	08	0.000
3-27-84	A325	0.875	532	19	01	0.000
3-26-84	A325	0.875	533	27	02	0.000
3-27-84	A325	0.875	532	19	02	0.000
3-26-84	A325	0.875	533	27	04	0.000
3-27-84	A325	0.875	532	19	03	0.000
3-26-84	A325	0.875	533	27	06	0.000
3-27-84	A325	0.875	532	19	04	0.000
3-26-84	A325	0.875	533	28	02	0.000
3-27-84	A325	0.875	532	19	05	0.000
3-26-84	A325	0.875	533	28	04	0.000
3-27-84	A325	0.875	532	19	06	0.000
3-26-84	A325	0.875	533	28	06	0.000
3-27-84	A325	0.875	532	19	07	0.000
3-26-84	A325	0.875	533	29	02	0.000
3-27-84	A325	0.875	532	19	08	0.000
3-26-84	A325	0.875	533	29	04	0.000
3-27-84	A325	0.875	532	21	01	0.000
3-30-84	A490	1.000	533	29	06	0.000
3-27-84	A325	0.875	532	24	09	0.000
3-30-84	A490	1.000	535	34	02	0.000
3-27-84	A325	0.875	532	24	08	0.000
3-26-84	A325	0.875	535	34	04	0.000
3-27-84	A325	0.875	532	21	04	0.000
3-26-84	A325	0.875	535	34	06	0.000
3-27-84	A325	0.875	532	21	05	0.000
3-26-84	A325	0.875	535	34	08	0.000
3-27-84	A325	0.875	532	21	06	0.000
3-26-84	A325	0.875	535	26	02	0.000
3-27-84	A325	0.875	532	21	07	0.000
3-26-84	A325	0.875	535	26	04	0.000
3-27-84	A325	0.875	532	21	08	0.000
3-26-84	A325	0.875	535	26	06	0.000
3-27-84	A325	0.875	532	21	09	0.000
3-26-84	A490	0.875	535	31	01	0.000
3-27-84	A325	0.875	532	21	10	0.000
3-26-84	A325	0.875	535	28	03	0.000
3-27-84	A325	0.875	534	07	01	0.000
3-26-84	A325	0.875	535	28	05	0.000
3-27-84	A325	0.875	534	07	02	0.000
3-26-84	A325	0.875	535	28	07	0.000
3-27-84	A325	0.875	534	07	03	0.000
3-26-84	A325	0.875	535	14	02	0.000
3-27-84	A325	0.875	534	07	04	0.000
3-26-84	A325	0.875	535	14	04	0.000
3-27-84	A325	0.875	534	07	05	0.000
3-26-84	A325	0.875	535	14	06	0.000
3-27-84	A325	0.875	534	07	06	0.000
3-30-84	A490	1.000	535	25	01	0.000
3-27-84	A325	0.875	532	24	07	0.000
3-26-84	A325	0.875	535	25	03	0.000
3-26-84	A325	0.875	534	04	01	0.000

3-27-84	A325	0.875	535	25	05	0.000
3-26-84	A325	0.875	534	04	02	0.000
3-27-84	A325	0.875	535	25	07	0.000
3-26-84	A325	0.875	534	04	03	0.000
3-27-84	A325	0.875	535	06	02	0.000
3-26-84	A325	0.875	534	04	04	0.000
3-27-84	A325	0.875	535	06	04	0.000
3-23-84	A325	0.875	532	17	01	0.000
3-27-84	A325	0.875	535	06	06	0.000
3-23-84	A325	0.875	532	17	02	0.000
3-30-84	A490	1.000	532	25	10	0.000
3-23-84	A325	0.875	532	17	03	0.000
3-30-84	A490	1.000	532	25	08	0.000
3-23-84	A325	0.875	532	17	04	0.000
3-30-84	A490	1.000	532	25	07	0.000
3-23-84	A325	0.875	532	17	05	0.000
3-27-84	A325	0.875	535	06	14	0.000
3-23-84	A325	0.875	532	17	06	0.000
3-27-84	A325	0.875	535	24	02	0.000
3-23-84	A325	0.875	532	17	07	0.000
3-27-84	A325	0.875	535	24	04	0.000
3-23-84	A325	0.875	532	17	08	0.000
3-27-84	A325	0.875	534	24	06	0.000
3-23-84	A325	0.875	532	18	01	0.000
3-27-84	A325	0.875	534	03	01	0.000
3-23-84	A325	0.875	532	18	02	0.000
3-27-84	A325	0.875	534	03	03	0.000
3-23-84	A325	0.875	532	18	03	0.000
3-27-84	A325	0.875	534	03	05	0.000
3-23-84	A325	0.875	532	18	04	0.000
3-27-84	A325	0.875	534	03	07	0.000
3-23-84	A325	0.875	532	18	05	0.000
3-27-84	A325	0.875	534	21	02	0.000
3-23-84	A325	0.875	532	18	06	0.000
3-27-84	A325	0.875	534	21	04	0.000
3-23-84	A325	0.875	532	18	07	0.000
3-27-84	A325	0.875	534	21	06	0.000
3-23-84	A325	0.875	532	18	08	0.000
3-27-84	A325	0.875	534	21	08	0.000
3-23-84	A325	0.875	532	07	01	0.000
3-30-84	A490	1.000	532	25	06	0.000
3-23-84	A325	0.875	532	07	02	0.000
3-27-84	A325	0.875	534	21	02	0.000
3-23-84	A325	0.875	532	07	12	0.000
3-27-84	A325	0.875	534	21	03	0.000
3-23-84	A325	0.875	532	07	14	0.000
3-27-84	A325	0.875	534	14	04	0.000
3-23-84	A325	0.875	532	07	02	0.000
3-27-84	A325	0.875	534	14	05	0.000
3-23-84	A325	0.875	532	07	04	0.000
3-27-84	A325	0.875	534	14	06	0.000
3-23-84	A325	0.875	532	07	06	0.000
3-27-84	A325	0.875	534	14	07	0.000
3-23-84	A325	0.875	532	07	08	0.000
3-27-84	A325	0.875	534	20	08	0.000
3-23-84	A325	0.875	532	07	02	0.000
3-27-84	A325	0.875	534	07	09	0.000

3-27-84	A325	0.875	534	20	04	0.000
3-23-84	A325	0.875	532	08	01	0.000
3-27-84	A325	0.875	534	20	06	0.000
3-23-84	A325	0.875	532	08	02	0.000
3-27-84	A325	0.875	534	10	01	0.000
3-23-84	A325	0.875	532	08	03	0.000
3-27-84	A325	0.875	534	10	03	0.000
3-23-84	A325	0.875	532	08	04	0.000
3-29-84	A490	0.875	535	33	11	0.000
3-23-84	A325	0.875	532	08	05	0.000
3-29-84	A490	0.875	535	29	01	0.000
3-23-84	A325	0.875	532	08	06	0.000
3-29-84	A490	0.875	535	29	05	0.000
3-30-84	A490	1.000	532	24	06	0.000
3-29-84	A490	0.875	535	30	02	0.000
3-23-84	A325	0.875	532	09	02	0.000
3-29-84	A490	0.875	535	30	06	0.000
3-23-84	A325	0.875	532	09	03	0.000
3-29-84	A490	0.875	535	23	03	0.000
3-23-84	A325	0.875	532	09	04	0.000
3-29-84	A490	0.875	535	23	07	0.000
3-23-84	A325	0.875	532	09	05	0.000
3-29-84	A490	0.875	535	24	04	0.000
3-23-84	A325	0.875	532	09	06	0.000
3-29-84	A490	0.875	535	33	06	0.000
3-23-84	A325	0.875	532	01	01	0.000
3-29-84	A490	0.875	535	02	05	0.000
3-23-84	A325	0.875	532	01	02	0.000
3-29-84	A490	0.875	535	09	02	0.000
3-23-84	A325	0.875	532	01	03	0.000
3-29-84	A490	0.875	535	09	06	0.000
3-23-84	A325	0.875	532	01	04	0.000
3-28-84	A325	0.875	536	14	03	0.000
3-23-84	A325	0.875	532	01	05	0.000
3-28-84	A325	0.875	536	16	01	0.000
3-23-84	A325	0.875	532	01	06	0.000
3-28-84	A325	0.875	536	17	02	0.000
3-23-84	A325	0.875	532	01	07	0.000
3-28-84	A325	0.875	535	13	03	0.000
3-23-84	A325	0.875	532	01	08	0.000
3-28-84	A325	0.875	535	13	07	0.000
3-23-84	A325	0.875	532	02	01	0.000
3-28-84	A325	0.875	535	17	04	0.000
3-23-84	A325	0.875	532	02	02	0.000
3-29-84	A490	0.875	535	33	04	0.000
3-23-84	A325	0.875	532	02	03	0.000
3-29-84	A490	0.875	535	31	07	0.000
3-23-84	A325	0.875	532	02	04	0.000
3-29-84	A490	0.875	535	31	03	0.000
3-23-84	A325	0.875	532	02	05	0.000
3-28-84	A490	0.875	534	08	06	0.000
3-23-84	A325	0.875	532	02	06	0.000
3-27-84	A325	0.875	536	01	03	0.000
3-23-84	A325	0.875	532	02	07	0.000
3-27-84	A325	0.875	536	03	01	0.000
3-23-84	A325	0.875	532	02	08	0.000

3-27-84	A325	0.875	536	04	02	0.000
3-23-84	A325	0.875	532	02	09	0.000
3-27-84	A325	0.875	536	05	03	0.000
3-23-84	A325	0.875	532	03	01	0.000
3-27-84	A325	0.875	533	26	01	0.000
3-23-84	A325	0.875	532	03	02	0.000
3-27-84	A325	0.875	533	26	05	0.000
3-23-84	A325	0.875	532	03	03	0.000
3-27-84	A325	0.875	533	27	01	0.000
3-23-84	A325	0.875	532	03	04	0.000
3-27-84	A325	0.875	533	27	05	0.000
3-23-84	A325	0.875	532	03	05	0.000
3-27-84	A325	0.875	533	28	03	0.000
3-23-84	A325	0.875	532	03	06	0.000
3-27-84	A325	0.875	533	29	01	0.000
3-23-84	A325	0.875	532	03	07	0.000
3-27-84	A325	0.875	533	29	05	0.000
3-23-84	A325	0.875	532	03	08	0.000
3-27-84	A325	0.875	535	34	03	0.000
3-23-84	A325	0.875	532	03	09	0.000
3-27-84	A325	0.875	535	34	07	0.000
3-23-84	A325	0.875	531	01	01	0.000
3-27-84	A325	0.875	535	26	03	0.000
3-23-84	A325	0.875	531	01	02	0.000
3-27-84	A325	0.875	535	26	07	0.000
3-23-84	A325	0.875	531	01	03	0.000
3-27-84	A325	0.875	535	28	04	0.000
3-23-84	A325	0.875	531	01	04	0.000
3-27-84	A325	0.875	535	14	01	0.000
3-23-84	A325	0.875	531	01	05	0.000
3-27-84	A325	0.875	535	14	05	0.000
3-30-84	A490	1.000	532	24	05	0.000
3-27-84	A325	0.875	535	25	02	0.000
3-30-84	A490	1.000	532	24	04	0.000
3-27-84	A325	0.875	535	25	06	0.000
3-30-84	A490	1.000	532	24	03	0.000
3-27-84	A325	0.875	535	06	03	0.000
3-30-84	A490	1.000	532	24	02	0.000
3-27-84	A325	0.875	535	06	07	0.000
3-23-84	A325	0.875	531	02	05	0.000
3-27-84	A325	0.875	535	06	11	0.000
3-23-84	A325	0.875	531	02	06	0.000
3-27-84	A325	0.875	535	24	01	0.000
3-23-84	A325	0.875	531	02	07	0.000
3-27-84	A325	0.875	534	24	05	0.000
3-22-84	A325	0.875	530	15	01	0.000
3-27-84	A325	0.875	534	03	02	0.000
3-22-84	A325	0.875	530	15	02	0.000
3-27-84	A325	0.875	534	03	06	0.000
3-22-84	A325	0.875	530	15	03	0.000
3-27-84	A325	0.875	534	21	03	0.000
3-22-84	A325	0.875	530	15	04	0.000
3-27-84	A325	0.875	534	21	07	0.000
3-22-84	A325	0.875	530	15	05	0.000
3-27-84	A325	0.875	534	21	11	0.000
3-22-84	A325	0.875	530	15	06	0.000

3-27-84	A325	0.875	534	14	01	0.000
3-22-84	A325	0.875	530	15	07	0.000
3-27-84	A325	0.875	534	14	05	0.000
3-22-84	A325	0.875	530	15	08	0.000
3-27-84	A325	0.875	534	20	01	0.000
3-22-84	A325	0.875	530	16	01	0.000
3-27-84	A325	0.875	534	20	05	0.000
3-30-84	A490	1.000	532	24	01	0.000
3-27-84	A325	0.875	534	10	02	0.000
4-3-84	A325	0.875	538	03	03	0.000
3-29-84	A490	0.875	535	33	13	0.000
4-3-84	A325	0.875	538	03	02	0.000
3-29-84	A490	0.875	535	29	07	0.000
4-3-84	A325	0.875	538	03	01	0.000
3-29-84	A490	0.875	535	33	09	0.000
3-22-84	A325	0.875	530	16	06	0.000
3-29-84	A490	0.875	535	24	02	0.000
4-3-84	A325	0.875	538	02	03	0.000
3-29-84	A490	0.875	535	02	03	0.000
3-22-84	A325	0.875	530	16	08	0.000
3-29-84	A490	0.875	535	09	04	0.000
3-22-84	A325	0.875	530	10	01	0.000
3-28-84	A325	0.875	536	15	02	0.000
3-22-84	A325	0.875	530	10	02	0.000
3-28-84	A325	0.875	535	13	01	0.000
3-22-84	A325	0.875	530	10	03	0.000
3-28-84	A325	0.875	535	17	02	0.000
3-22-84	A325	0.875	530	10	04	0.000
3-29-84	A490	0.875	535	33	02	0.000
3-22-84	A325	0.875	530	10	05	0.000
3-28-84	A490	0.875	534	08	04	0.000
3-22-84	A325	0.875	530	10	06	0.000
3-27-84	A325	0.875	536	02	02	0.000
3-22-84	A325	0.875	530	10	07	0.000
3-27-84	A325	0.875	536	05	01	0.000
3-22-84	A325	0.875	530	10	08	0.000
3-27-84	A325	0.875	533	26	03	0.000
3-22-84	A325	0.875	530	10	09	0.000
3-27-84	A325	0.875	533	27	03	0.000
3-22-84	A325	0.875	530	11	11	0.000
3-27-84	A325	0.875	533	28	05	0.000
3-22-84	A325	0.875	530	11	11	0.000
3-27-84	A325	0.875	535	34	01	0.000
3-22-84	A325	0.875	530	11	11	0.000
3-27-84	A325	0.875	535	26	01	0.000
3-22-84	A325	0.875	530	11	11	0.000
3-27-84	A325	0.875	535	28	02	0.000
3-22-84	A325	0.875	530	11	11	0.000
3-27-84	A325	0.875	535	14	03	0.000
3-22-84	A325	0.875	530	11	11	0.000
3-27-84	A325	0.875	535	25	04	0.000
3-22-84	A325	0.875	530	01	01	0.000
3-27-84	A325	0.875	535	06	05	0.000
3-22-84	A325	0.875	530	01	02	0.000
3-27-84	A325	0.875	535	06	13	0.000
4-3-84	A325	0.875	538	02	02	0.000

3-27-84	A325	0.875	534	24	07	0.000
3-22-84	A325	0.875	530	01	04	0.000
3-27-84	A325	0.875	534	21	01	0.000
3-22-84	A325	0.875	530	01	05	0.000
3-27-84	A325	0.875	534	21	09	0.000
3-22-84	A325	0.875	530	01	06	0.000
3-27-84	A325	0.875	534	14	03	0.000
3-22-84	A325	0.875	530	01	07	0.000
3-27-84	A325	0.875	534	20	03	0.000
3-22-84	A325	0.875	530	01	08	0.000
3-27-84	A325	0.875	534	10	04	0.000
4-3-84	A325	0.875	538	02	01	0.000
3-29-84	A490	0.875	535	30	04	0.000
4-3-84	A325	0.875	538	04	03	0.000
3-29-84	A490	0.875	535	24	06	0.000
4-3-84	A325	0.875	538	04	02	0.000
3-28-84	A325	0.875	536	14	01	0.000
4-3-84	A325	0.875	538	04	01	0.000
3-28-84	A325	0.875	535	13	05	0.000
3-22-84	A325	0.875	530	03	05	0.000
3-29-84	A490	0.875	535	31	05	0.000
4-3-84	A325	0.875	538	01	03	0.000
3-27-84	A325	0.875	536	03	03	0.000
4-3-84	A325	0.875	538	01	02	0.000
3-27-84	A325	0.875	533	26	07	0.000
4-3-84	A325	0.875	538	01	01	0.000
3-27-84	A325	0.875	533	29	03	0.000
3-22-84	A325	0.875	530	04	01	0.000
3-27-84	A325	0.875	535	26	05	0.000
3-22-84	A325	0.875	530	04	02	0.000
3-27-84	A325	0.875	535	14	07	0.000
3-22-84	A325	0.875	530	04	03	0.000
3-30-84	A490	1.000	532	25	09	0.000
3-22-84	A325	0.875	530	04	04	0.000
3-27-84	A325	0.875	534	03	04	0.000
3-22-84	A325	0.875	530	04	05	0.000
3-27-84	A325	0.875	534	21	13	0.000
3-22-84	A325	0.875	530	17	01	0.000
3-27-84	A325	0.875	534	20	07	0.000
3-22-84	A325	0.875	530	17	02	0.000
3-29-84	A490	0.875	535	33	08	0.000
3-22-84	A325	0.875	530	17	03	0.000
3-28-84	A325	0.875	536	16	03	0.000
3-22-84	A325	0.875	530	17	04	0.000
3-27-84	A325	0.875	536	01	01	0.000
3-22-84	A325	0.875	530	17	05	0.000
3-27-84	A325	0.875	533	28	01	0.000
4-3-84	A325	0.875	529	06	02	0.000
3-27-84	A325	0.875	535	28	06	0.000
4-3-84	A325	0.875	529	06	01	0.000
3-27-84	A325	0.875	535	24	03	0.000
3-22-84	A325	0.875	530	14	01	0.000
3-27-84	A325	0.875	534	14	07	0.000
3-22-84	A325	0.875	530	14	02	0.000
3-29-84	A490	0.875	535	02	07	0.000
3-22-84	A325	0.875	530	14	03	0.000



**STRUCTURAL
INTEGRITY
ASSOCIATES, INC.**

3-27-84	A325	0.875	536	06	02	0.000
3-22-84	A325	0.875	530	14	04	0.000
3-27-84	A325	0.875	535	06	01	0.000
3-22-84	A325	0.875	530	14	05	0.000
3-29-84	A490	0.875	535	29	03	0.000
3-22-84	A325	0.875	530	14	06	0.000
3-27-84	A325	0.875	535	34	05	0.000
3-28-84	A325	0.875	535	17	06	0.000
3-27-84	A325	0.875	534	21	05	0.000
3-22-84	A325	0.875	530	14	07	0.000
3-22-84	A325	0.875	530	14	08	0.000

APPENDIX E

TORQUE COEFFICIENTS MEASURED BY BECHTEL
FOR BOLTS IN VARIOUS CONDITIONS

CALCULATION SHEET

SIGNATURE W. Quinn DATE 3-9-53 CALC. NO. _____
 PROJECT PVINGS CHECKED _____ DATE _____
 SUBJECT UNIT 3 - A325 BOLT TENSIONING JOB NO. 10407
 SHEET 1 OF _____ SHEET _____

29 - 7/8" ϕ A325 BOLTS SOME WITHOUT LUBRICATION
 SOME RUSTED AND THE REST LUBRICATED
 WITH DIFFERENT TYPES OF LUBRICANT, WERE
 TENSIONED USING AN AIR DRIVEN IMPACT
 WRENCH UNTIL THE WRENCH STOPPED TEN-
 SIONING.

THE TENSION VALUES ON THE BOLT TEN-
 SIONING CALIBRATOR WERE RECORDED, THE
 TORQUE WAS MEASURED WITH A HAND
 TORQUE WRENCH AND EVERY BOLT WAS
 PUNCH MARKED.

DETERMINATION OF THE COEFFICIENT OF
 FRICTION "C" IN EVERY CASE, BASED ON
 THE TORQUE FORMULA.

$$T = \frac{(C)(D)(TENSILE\ FORCE)}{12} \quad (\text{RESULTS IN FT-LB})$$

$$C = \frac{12 \cdot (T)}{D \cdot (TENSILE\ FORCE)}$$

T = TORQUE
 C = COEFFICIENT OF FRICTION
 D = BOLT NOMINAL DIAMETER



CALCULATION SHEET

LA 003

SIGNATURE G. Calder DATE 3-9-63

CALC. NO. _____

PROJECT P I N G S

CHECKED _____ DATE _____

SUBJECT UNIT 3 - A325 BOLT TENSIONING

JOB NO 10407

SHEET 2 OF _____ SHEETS

BOLT No	TENSION (KIPS)	TORQUE Ft-Lbs	LUBRICANT	COEFFICIENT OF FRICTION "C"	BRINNELL HARDNESS		REMARKS
					BOLT	WASHER	
02	38	390	USED BOLTS AS USED DAILY NO LUBRICANT USED	0.141			
03	48	530		0.151			
04	47	—		0.161			
05	51	600		0.146			
06	49	520					
1	42	500	CUTTING OIL	0.163			
2	28	360		0.176			
3	42.5	550		0.177			
4	51.5	580	SAE 30 OIL	0.154			
5	37.5	345		0.126			
6	50	540	LIQUID WRENCH	0.148			
7	45	560		0.171			
8	50.5	710	"NEVER SEEZE" PURE NICKEL	0.193			YIELDED AND WENT DN (AS WHEN CHECKING TORQUE)
9	51	560		0.151			
10	55	600	"N 5000" GRAPHITE	0.150			
11	42	480		0.157			
12	44.5	520		0.160			
13	50	610	WD40	0.167			
14	40	475		0.163			
15	36	400	MARFAK GREASE	0.152			
16	44	450		0.140			
17	32.5	445	NONE	0.188			YIELDED & LOWERED TO 2 WHEN TORQUE CHECKING
18	41	420		0.140			
19	45	560	NONE	0.171			
20	46	550		0.164			
21	49.5	600	NONE	0.166			
22	40.5	970		0.328			
23	29	900	NONE	0.426			
24	30	580		0.265			



STRUCTURAL INTEGRITY ASSOCIATES, INC.

SIGNATURE Van J. Hester DATE 5-17-83

CALC NO. _____

PROJECT PVNGS

CHECKED _____ DATE _____

SUBJECT TEST DATA FOR NCR CC-4087 E DER 83-30

JOB NO. 10407

SHEET _____ OF _____ SHEETS

SAMPLE NO.	MATERIAL TYPE	DIAMETER (INCHES)	THREADS PER INCH	F _u (LBS)	.7 F _u (LBS)	ACTUAL TENSION	TORQUE (FT-LBS)	FRICTION COEF. (C)
1	A325	3/4	10	40,100	28,070	28,100	215	0.122
2	A325	3/4	10	40,100	28,070	28,100	220	0.125
3	A325	3/4	10	40,100	28,070	28,100	225	0.128
4	A325	3/4	10	40,100	28,070	28,100	240	0.137
5	A325	1	8	72,700	50,890	51,000	500	0.118
6	A325	1	8	72,700	50,890	51,000	580	0.136
7	A325	1	8	72,700	50,890	51,000	580	0.136
8	A325	1	8	72,700	50,890	51,000	580	0.136
9	A325	1/4	7	101,700	71,190	71,100	540	0.127
10	A325	1/4	7	101,700	71,190	71,500	888	0.120
11	A325	1/4	7	101,700	71,190	71,500	962	0.129
12	A325	1/4	7	101,700	71,190	71,500	1129	0.151
13	A325	1/4	7	101,700	71,190	71,100	1092	0.147
14	A490	3/8	9	69,300	48,510	44,100	470 520	0.145
15	A490	3/8	9	69,300	48,510	44,100	440	0.123
16	A490	3/8	9	69,300	48,510	44,500	420	0.116
17	A490	3/8	9	69,300	48,510	49,100	540	0.151
18	A490	1	8	90,900	63,630	64,100	930	0.155
19	A490	1	8	90,900	63,630	64,000	700	0.131
20	A490	1	8	90,900	63,630	64,100	740	0.139
21	A490	1	8	90,900	63,630	64,500	750	0.140
22	A490	1/4	7	145,350	101,745	103,000	1591	0.148
23	A490	1/4	7	145,350	101,745	103,000	1480	0.138
24	A490	1/4	7	145,350	101,745	103,900	1480	0.137
25	A490	1/4	7	145,350	101,745	102,000	1351	0.127
26	A354 BD	1	8	90,900	63,630	64,000	865	0.162
27	A354 BD	1	8	90,900	63,630	64,000	900	0.150
28	A354 BD	1	8	90,900	63,630	63,600	805	0.152
29	A354 BD	1	8	90,900	63,630	64,200	720	0.135
30	A354 BD	1	8	90,900	63,630	64,500	895	0.167
31	A354 BD	1	8	90,900	63,630	64,500	800	0.149

CONT'D



NCR CC4087 -
 PAGE 6 of 6
 5/17/83

SIGNATURE Van J. Hester DATE 5-17-83

CALC. NO. _____

PROJECT PVNGS

CHECKED _____ DATE _____

SUBJECT TEST DATA FOR NCR CC 4087 E DER 83-30

JOB NO. _____

SHEET _____ OF _____ SHEETS

SAME No.	MATERIAL TYPE	DIAMETER (INCHES)	THREADS PER INCH	Fu (LBS)	.7 Fu (LBS)	ACTUAL TENSION	TORQUE (FF-LBS)	FRICTION COEF. (C)
31	A354 BD	1/4	8	150,000 145,350	105,000 101,745	105,100	1554	0.142
32	A354 BD	1/4	8	150,000 145,350	105,000 101,745	105,100	1625	0.149
33	A354 BD	1/4	8	150,000 145,350	105,000 101,745	106,000	1591	0.144
34	A354 BD	1/4	8	150,000 145,350	105,000 101,745	106,000	1647	0.149
35	A354 BD	1/4	7	145,350	101,745	102,000	1554	0.146
36	A354 BD	1/4	7	145,350	101,745	102,100	1480	0.139
37	A193 B7	3/4	10	41,750	29,225	29,100	220	0.121
38	A193 B7	3/4	10	41,750	29,225	29,100	220	0.121
39	A193 B7	3/4	10	41,750	29,225	29,500	240	0.130
40	A193 B7	3/4	10	41,750	29,225	29,100	235	0.129
41	A193 B7	1	8	75,750	53,025	52,400	640	0.145
42	A193 B7	1	8	75,750	53,025	53,000	720	0.163
43	A193 B7	1	8	75,750	53,025	53,500	530	0.119
44	A193 B7	1	8	75,750	53,025	53,900	500	0.111
45	A193 B7	1/4	7	121,125	84,790	85,000	1147	0.130
46	A193 B7	1/4	7	121,125	84,790	85,500	1332	0.150
47	A193 B7	1/4	7	121,125	84,790	86,500	1364	0.152
48	A193 B7	1/4	7	121,125	84,790	86,000	1147	0.128

*
$$C = \frac{\text{TORQUE} \times 12}{(\text{BOLT DIA.}) \times (\text{TENSION})}$$

Fu = MINIMUM SPECIFIED TENSILE STRENGTH

TEST PERFORMED BY: VAN J. HESTER

WITNESSED BY: (QC) GARY GRIFFITH 8-17-83

WITNESSED BY: (FE) GUS CALDAS

TORQUE WRENCH USED: JMA 0936 (DUE DATE 9/8/83)

DIRECT TEN INDICATOR USED: JMA 0064 (DUE DATE 5/14/83)

* INSTRUMENT NOT USED ON 5/15/83 AND 5/24/83 FOR ABOVE TESTS. CALIBRATION IS WITHIN TOLERANCE. SEE PAGE 8



NCR CC 4087
PAGE 7c 8

APPENDIX F

PALO VERDE UNIT 1 PRELOAD CALCULATIONS
FOR NUTS MEASURED AS GREATER THAN 30° ROTATION FROM REQUIREMENT

3-19-84	A325	0.875	535	38	05	0.500	9.000	0.462	0.110	0.500	0.000	39000.000	6825.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000
3-14-84	A325	0.875	536	02	01	1.063	9.000	0.462	0.110	0.500	0.000	39000.000	6825.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000
3-14-84	A325	0.875	536	11	01	0.147	9.000	0.462	0.110	0.500	0.000	39000.000	6825.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000
3-5-84	A325	0.875	536	14	02	0.250	9.000	0.462	0.110	0.500	0.353	39000.000	6825.000	50053.476	108403.192	105000.000	1.032	18312.379	111413.163	1.061	0.973
3-5-84	A325	0.875	536	14	01	0.250	9.000	0.462	0.110	0.500	0.250	39000.000	6825.000	35454.545	76785.594	105000.000	0.731	12911.453	78917.672	0.752	0.973
3-22-84	A490	1.375	540	06/E	07	0.104	6.000	1.155	0.110	0.500	0.296	121000.000	33275.000	174166.667	150808.936	150000.000	1.005	25644.321	155102.062	1.034	0.972



**STRUCTURAL
INTEGRITY
ASSOCIATES, INC.**

FIELD VERGE 1 MIT ROTATION 30 DEGREES, PRELOAD CALCULATION (K=0.160)

Table with columns: INSD, DATE, BOX, GRADE, SIZE, DIM, NO, COM, NO, BOLT, NO, MIT, ROTAT, THY, IN, A, ASSUMED, TURN, SPEC, TORQUE, F1, SPEC, ACT, S10M, UTS, MIN, S10M, UTS, MIN, S10M, UTS, MIN, S10M, UTS, MIN, S10M, UTS, MIN, S10M, UTS, MIN. The table contains 38 rows of data, each representing a different bolt and nut assembly.



STRUCTURAL
INTEGRITY
ASSOCIATES, INC.

3-19-84	6325	0.875	535	38	05	0.500	9.000	0.462	0.160	0.500	0.000	39000.000	6825.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3-14-84	6325	0.875	536	02	01	1.083	9.000	0.462	0.160	0.500	0.000	39000.000	6825.000	0.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000	0.000
3-4-84	6325	0.875	536	11	01	0.147	9.000	0.462	0.160	0.500	0.000	39000.000	6825.000	34411.765	74527.194	105000.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3-5-84	6325	0.875	536	14	02	0.250	9.000	0.462	0.160	0.500	0.250	39000.000	6825.000	24375.000	52790.096	105000.000	0.503	12971.453	18312.625	78763.814	0.750	0.946	0.946
3-5-84	6325	0.875	536	14	01	0.250	9.000	0.462	0.160	0.500	0.250	39000.000	6825.000	24375.000	52790.096	105000.000	0.503	12971.453	18312.625	78763.814	0.531	0.946	
3-22-84	6490	1.375	540	064E	07	0.104	6.000	1.155	0.160	0.500	0.396	121000.000	33275.000	119735.583	103681.144	500000.000	0.691	25864.35	15746.325	0.732	0.946	0.946	0.946

PAID VERDE 1 NUT ROTATION 30 DEGREES, PRELOAD CALCULATION (R=0.20)

Table with columns: INGS, DATE, BOLT, GRADE, SIZE, (IN), DMS, NO., CONG. NO., BOLT NO., NUT ROTAT, TH/IN, N, A, R, ASSUMED, TURN, TURN, SPEC, F1, SPEC, TURBOLE, F1, SPEC, ACT, S1(SHM), UTS, UTS MIN, TRL, S1(SHM), S1(SHM) 1/ S1(SHM) 1/ UTS MIN, S1(SHM) 1/ S1(SHM) 1/.



3-19-84	RL25	0.875	535	38	05	0.500	9.000	0.462	0.200	0.500	0.000	39000.000	6825.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000
3-14-84	RL25	0.875	536	02	01	1.063	9.000	0.462	0.200	0.500	0.000	39000.000	6825.000	0.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000
3-14-84	RL25	0.875	538	11	01	0.147	9.000	0.462	0.200	0.500	0.000	39000.000	6825.000	0.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000
3-5-84	RL25	0.875	536	14	02	0.256	9.000	0.462	0.200	0.500	0.256	39000.000	6825.000	27529.412	59621.755	105000.000	0.568	18322.635	64757.178	0.617	0.920
3-5-84	RL25	0.875	538	14	01	0.250	9.000	0.462	0.200	0.500	0.250	39000.000	6825.000	19500.000	42242.077	105000.000	0.462	12971.452	45895.001	0.437	0.920
3-22-84	RL30	1.375	540	06+E	07	0.124	6.000	1.155	0.200	0.500	0.396	121000.000	33275.000	95791.667	82594.915	150000.000	0.553	25844.321	50317.352	0.437	0.920

3-19-84	R225	0.875	535	38	05	0.500	2.000	0.462	0.430	0.500	0.000	39000.000	6825.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000	0.000
3-14-84	R225	0.875	536	02	01	1.083	9.000	0.462	0.430	0.500	0.000	39000.000	6825.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000	0.000
3-14-84	R225	0.875	536	11	01	0.147	9.000	0.462	0.430	0.500	0.000	39000.000	6825.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000	0.000
3-5-84	R225	0.875	536	14	02	0.250	9.000	0.462	0.430	0.500	0.250	39000.000	6825.000	12804.378	27731.049	105000.000	0.264	36837.790	0.351	0.753	0.248	0.753
3-5-84	R225	0.875	536	14	01	0.250	9.000	0.462	0.430	0.500	0.250	39000.000	6825.000	9049.767	19642.826	105000.000	0.187	2609.593	0.248	0.753	0.248	0.753
3-22-84	0490	1.375	540	06+E	07	0.104	6.000	1.125	0.430	0.500	0.396	121000.000	33275.000	44254.664	38579.030	150000.000	0.257	51504.722	0.248	0.753	0.248	0.749



APPENDIX G

PALO VERDE UNIT 2 PRELOAD CALCULATIONS
FOR NUTS MEASURED AS GREATER THAN 30° ROTATION FROM REQUIREMENT

APPENDIX H
PALO VERDE UNIT 2 PRELOAD CALCULATIONS
BASED ON RESTART TORQUE

APPENDIX I

PALO VERDE UNIT 3 PRELOAD CALCULATIONS
FOR NUTS MEASURED AS GREATER THAN 30° ROTATION FROM REQUIREMENT

FIELD VERGE 3 NUT ROTATION 30 DEGREES, PRELOAD CALCULATION (K=0.110)

INSP. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONC. NO.	BOLT NO.	NET WT (LBS)	TH/IN	SE/IN	K	RESUMED TURN	TURN	F1	TORQUE	F1	ACT	UTS	MIN	UTS	MIN	UTS	MIN	TRU	STRENGTH	UTS	MIN	UTS	MIN
3-22-84	A325	0.875	530	03	02	0.250	9.000	0.462	0.110	0.500	0.250	39000.000	6825.000	35454.545	76785.594	105000.000	0.731	12971.453	78917.672	0.752	0.973	0.731	12971.453	78917.672	0.752	0.973	
3-22-84	A325	0.875	530	03	04	0.167	9.000	0.462	0.110	0.500	0.333	39000.000	6825.000	47272.727	102380.792	105000.000	0.975	17295.270	105223.562	1.002	0.973	0.975	17295.270	105223.562	1.002	0.973	
3-22-84	A325	0.875	530	03	08	0.167	9.000	0.462	0.110	0.500	0.333	39000.000	6825.000	47272.727	102380.792	105000.000	0.975	17295.270	105223.562	1.002	0.973	0.975	17295.270	105223.562	1.002	0.973	
3-22-84	A325	0.875	530	15	05	0.167	9.000	0.462	0.110	0.500	0.333	39000.000	6825.000	47272.727	102380.792	105000.000	0.975	17295.270	105223.562	1.002	0.973	0.975	17295.270	105223.562	1.002	0.973	
3-22-84	A325	0.875	530	17	06	0.417	9.000	0.462	0.110	0.500	0.083	39000.000	6825.000	11818.182	25395.198	105000.000	0.244	4323.818	26325.851	0.251	0.973	0.244	4323.818	26325.851	0.251	0.973	
3-23-84	A325	0.875	531	02	04	0.333	9.000	0.462	0.110	0.500	0.167	39000.000	6825.000	23636.364	51190.376	105000.000	0.488	8647.625	52811.761	0.500	0.973	0.488	8647.625	52811.761	0.500	0.973	
3-25-84	A325	0.875	532	09	01	0.250	9.000	0.462	0.110	0.500	0.250	39000.000	6825.000	35454.545	76785.594	105000.000	0.731	12971.453	78917.672	0.752	0.973	0.731	12971.453	78917.672	0.752	0.973	
3-26-84	A325	0.875	532	21	02	0.250	9.000	0.462	0.110	0.500	0.250	39000.000	6825.000	35454.545	76785.594	105000.000	0.731	12971.453	78917.672	0.752	0.973	0.731	12971.453	78917.672	0.752	0.973	
3-26-84	A325	0.875	532	21	02	0.167	9.000	0.462	0.110	0.500	0.333	39000.000	6825.000	47272.727	102380.792	105000.000	0.975	17295.270	105223.562	1.002	0.973	0.975	17295.270	105223.562	1.002	0.973	
3-27-84	A325	0.875	532	27	01	0.208	9.000	0.462	0.110	0.500	0.250	39000.000	6825.000	41363.636	89583.133	105000.000	0.853	15133.361	92076.617	0.877	0.973	0.853	15133.361	92076.617	0.877	0.973	



FIELD VERGE 3 NUT ROTATION 30 DEGREES, PRELOAD CALCULATION (K=0.160)

INSP. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONG. NO.	BOL. T. NO.	NET ROTAT	TH/IN	SE. IN	A	RESUMED TURN	TURN	F1	TORQUE	F1	UTS	SIGMA	SIGMA I	SIGMA I/	TRU	SIGMA	SIGMA I/	SIGMA I/
									N	H	SPEC	ACT	SPEC	ACT	MIN	I	MIN	MIN	IV	I	MIN	I/
3-22-84	A325	0.875	530	03	02	0.250	3.000	0.462	0.160	0.500	0.250	390000.000	6825.000	24375.000	52790.096	1050000.000	0.503	12971.453	55805.202	0.531	0.946	
3-22-84	A325	0.875	530	03	04	0.167	3.000	0.462	0.160	0.500	0.333	390000.000	6825.000	32500.000	70386.795	1050000.000	0.670	17295.270	74436.936	0.709	0.946	
3-22-84	A325	0.875	530	03	08	0.167	3.000	0.462	0.160	0.500	0.333	390000.000	6825.000	32500.000	70386.795	1050000.000	0.670	17295.270	74436.936	0.709	0.946	
3-22-84	A325	0.875	530	16	06	0.417	3.000	0.462	0.160	0.500	0.083	390000.000	6825.000	8125.000	17596.699	1050000.000	0.168	4321.818	18621.734	0.177	0.946	
3-23-84	A325	0.875	531	02	04	0.333	3.000	0.462	0.160	0.500	0.167	390000.000	6825.000	16250.000	35131.397	1050000.000	0.335	8647.635	37253.468	0.359	0.946	
3-26-84	A325	0.875	532	09	01	0.250	3.000	0.462	0.160	0.500	0.250	390000.000	6825.000	24375.000	52790.096	1050000.000	0.503	12971.453	55805.202	0.531	0.946	
3-26-84	A325	0.875	532	21	03	0.250	3.000	0.462	0.160	0.500	0.250	390000.000	6825.000	24375.000	52790.096	1050000.000	0.503	12971.453	55805.202	0.531	0.946	
3-26-84	A325	0.875	532	27	01	0.167	3.000	0.462	0.160	0.500	0.333	390000.000	6825.000	32500.000	70386.795	1050000.000	0.670	17295.270	74436.936	0.709	0.946	
3-27-84	A325	0.875	535	06	08	0.208	3.000	0.462	0.160	0.500	0.292	390000.000	6825.000	28437.300	61588.445	1050000.000	0.587	15133.361	65106.069	0.620	0.946	



PRELIM VELOC 3 NUT ROTATION 30 DEGREES, PRELIM CALCULATION (N=0,200)

INCF. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONTR. NO.	BLK. NO.	NUT	ROTAT.	TR/IN	N	RESUMED	TURN	TURN	ACT	F ₁	TORQUE	F ₁	SPEC	ACT	F ₁	ACT	UTS	MIN	UTS	SIGMA	UTS	MIN	UTS	SIGMA	UTS	MIN	UTS	SIGMA	UTS	MIN	UTS	SIGMA				
3-22-84	A325	0.875	530	03	02		0.250	9.000	0.462	0.200	0.500	0.250	39000.000	0.000	6825.000	19500.000	6825.000	19500.000	42232.077	105000.000	42232.077	105000.000	0.402	12971.453	45298.001	0.437	0.920													
3-22-84	A325	0.875	530	03	04		0.157	9.000	0.462	0.200	0.500	0.333	39000.000	0.000	6825.000	26000.000	6825.000	26000.000	56309.438	105000.000	56309.438	105000.000	0.538	17295.270	61197.334	0.583	0.920													
3-22-84	A325	0.875	530	03	08		0.157	9.000	0.462	0.200	0.500	0.333	39066.000	0.000	6825.000	26000.000	6825.000	26000.000	56309.438	105000.000	56309.438	105000.000	0.538	17295.270	61197.334	0.583	0.920													
3-22-84	A325	0.875	530	16	05		0.167	9.000	0.462	0.200	0.500	0.333	39000.000	0.000	6825.000	26000.000	6825.000	26000.000	56309.438	105000.000	56309.438	105000.000	0.538	17295.270	61197.334	0.583	0.920													
3-22-84	A325	0.875	530	17	06		0.417	9.000	0.462	0.200	0.500	0.983	39000.000	0.000	6825.000	5500.000	6825.000	5500.000	14077.359	105000.000	14077.359	105000.000	0.134	4323.818	15299.334	0.146	0.920													
3-23-84	A325	0.875	531	02	04		0.333	9.000	0.462	0.200	0.500	0.167	39000.000	0.000	6825.000	13000.000	6825.000	13000.000	28154.718	105000.000	28154.718	105000.000	0.268	8647.525	30598.667	0.291	0.920													
3-26-84	A325	0.875	532	09	01		0.500	9.000	0.462	0.200	0.500	0.000	39000.000	0.000	6825.000	0.000	6825.000	0.000	0.000	105000.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3-26-84	A325	0.875	532	21	02		0.250	9.000	0.462	0.200	0.500	0.250	39000.000	0.000	6825.000	19500.000	6825.000	19500.000	42232.077	105000.000	42232.077	105000.000	0.402	12971.453	45298.001	0.437	0.920													
3-26-84	A325	0.875	532	21	03		0.250	9.000	0.462	0.200	0.500	0.250	39000.000	0.000	6825.000	19500.000	6825.000	19500.000	42232.077	105000.000	42232.077	105000.000	0.402	12971.453	45298.001	0.437	0.920													
3-26-84	A325	0.875	532	27	01		0.167	9.000	0.462	0.200	0.500	0.333	39000.000	0.000	6825.000	26000.000	6825.000	26000.000	56309.438	105000.000	56309.438	105000.000	0.538	17295.270	61197.334	0.583	0.920													
3-27-84	A325	0.875	532	06	08		0.208	9.000	0.462	0.200	0.500	0.292	39000.000	0.000	6825.000	22750.000	6825.000	22750.000	49270.756	105000.000	49270.756	105000.000	0.469	15133.361	53547.668	0.510	0.920													

PAID VERGE 3 NUT ROTATION) 30 DEGREES , PRELOD CALCULATION (K=0.430)

INSP. DATE	BOLT	GRADE	SIZE (IN)	DATE	NO.	CONV. NO.	BOLT NO.	NUT	ROTAT	TH/IN	SO. IN	K	ASSUMED TURN	TURN	F ₁	TORQUE	F ₁	ACT	FI	STEM	UTS	MIN	UTS	MIN	STEM	XY	STEM	UTS	MIN	STEM	XY	STEM	UTS	MIN	STEM	XY						
3-22-84	A325	0.875	530	03	02			02	0.250	9.000	0.462	0.430	0.500	0.250	39000.000	6825.000	9069.767	19642.826	19642.826	105000.000	0.187	12971.453	26091.593	0.248	0.753																	
3-22-84	A325	0.875	530	03	04			04	0.167	9.000	0.462	0.430	0.500	0.333	39000.000	6825.000	12093.023	26190.435	26190.435	105000.000	0.249	17295.270	34788.790	0.331	0.753																	
3-22-84	A325	0.875	530	03	08			08	0.167	9.000	0.462	0.430	0.500	0.333	39000.000	6825.000	12093.023	26190.435	26190.435	105000.000	0.249	17295.270	34788.790	0.331	0.753																	
3-22-84	A325	0.875	530	16	05			05	0.167	9.000	0.462	0.430	0.500	0.333	39000.000	6825.000	12093.023	26190.435	26190.435	105000.000	0.249	17295.270	34788.790	0.331	0.753																	
3-22-84	A325	0.875	530	17	06			06	0.417	9.000	0.462	0.430	0.500	0.083	39000.000	6825.000	3023.256	6547.699	6547.699	105000.000	0.062	4323.818	8697.198	0.063	0.753																	
3-23-84	A325	0.875	531	02	04			04	0.333	9.000	0.462	0.430	0.500	0.167	39000.000	6825.000	6046.512	13095.218	13095.218	105000.000	0.000	0.000	0.000	0.166	0.753																	
3-23-84	A325	0.875	532	09	01			01	0.500	9.000	0.462	0.430	0.500	0.000	39000.000	6825.000	0.000	0.000	0.000	105000.000	0.000	0.000	0.000	0.000	0.000																	
3-26-84	A325	0.875	532	21	02			02	0.250	9.000	0.462	0.430	0.500	0.250	39000.000	6825.000	9069.767	19642.826	19642.826	105000.000	0.187	12971.453	26091.593	0.248	0.753																	
3-26-84	A325	0.875	532	21	03			03	0.250	9.000	0.462	0.430	0.500	0.250	39000.000	6825.000	9069.767	19642.826	19642.826	105000.000	0.187	12971.453	26091.593	0.248	0.753																	
3-26-84	A325	0.875	532	27	01			01	0.167	9.000	0.462	0.430	0.500	0.333	39000.000	6825.000	12093.023	26190.435	26190.435	105000.000	0.249	17295.270	34788.790	0.331	0.753																	
3-27-84	A325	0.875	535	06	06			06	0.298	9.000	0.462	0.430	0.500	0.292	39000.000	6825.000	10581.295	22916.631	22916.631	105000.000	0.218	15133.361	30440.192	0.290	0.753																	



APPENDIX J
PALO VERDE UNIT 3 PRELOAD CALCULATIONS
BASED ON RESTART TORQUE

4-18-84	4490	1.375	534	33	02	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	33	03	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	33	04	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	33	05	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	33	06	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	34	01	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	34	02	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	34	03	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	34	04	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	34	05	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972
4-18-84	4490	1.375	534	34	06	2385.00	28620.00	6.000	1.155	0.110	121000.000	33275.000	189223.140	163846.166	150000.000	1.092	28035.070	168516.361	1.123	0.972



PAID VERDE UNIT 3 HIGH STRENGTH BOLT TORQUE (K=0.160)

INSP. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONN. NO.	BOLT NO.	TORQUE	N	A	ASSUMED	F1	TORQUE	F1	SIGMA	UTS	SIGMA X /	TAL	SIGMA Y /	SIGMA X /	UTS MIN	UTS X	UTS MIN	UTS Y	UTS MIN	UTS X	UTS MIN	UTS Y	UTS MIN	UTS X	UTS MIN	UTS Y				
4-24-84	A490	1.375	535	01	2385-0X	28620.000	6.000	1.155	0.160	121000.000	33275.000	130090.909	112644.239	150000.000	0.751	28035.070	119235.980	0.795	0.945															

PAID VERDE UNIT 3 HIGH STRENGTH BOLT TORQUE (K=0.200)

INSP. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONN. NO.	BOLT NO.	TORQUE	N	A	ASSUMED	F1	TORQUE	F1	SIGMA	UTS	SIGMA X /	TAL	SIGMA Y /	SIGMA X /	UTS MIN	UTS X	UTS MIN	UTS Y	UTS MIN	UTS X	UTS MIN	UTS Y	UTS MIN	UTS X	UTS MIN	UTS Y				
4-24-84	A490	1.375	535	01	2385.000	28620.000	6.000	1.155	0.200	121000.000	33275.000	104072.727	90115.391	150000.000	0.601	28035.070	96125.210	0.654	0.918															

PAID VERDE UNIT 3 HIGH STRENGTH BOLT TORQUE (K=0.430)

INSP. DATE	BOLT GRADE	SIZE (IN)	DWG. NO.	CONN. NO.	BOLT NO.	TORQUE	N	A	ASSUMED	F1	TORQUE	F1	SIGMA	UTS	SIGMA X /	TAL	SIGMA Y /	SIGMA X /	UTS MIN	UTS X	UTS MIN	UTS Y	UTS MIN	UTS X	UTS MIN	UTS Y	UTS MIN	UTS X	UTS MIN	UTS Y			
4-24-84	A490	1.375	535	01	2385.000	28620.000	6.000	1.125	0.430	121000.000	33275.000	48405.930	41914.135	150000.000	0.279	28035.070	55959.408	0.373	0.749														



APPENDIX K

RANGE OF VIBRATION STRESSES IN ANCHOR BOLTS
FOR ROTATING EQUIPMENT AND ACTUAL VS. ALLOWABLE LOADS
IN EQUIPMENT ANCHORAGE AND STRUCTURAL STEEL JOINTS (PER BECHTEL REF. 4)

TABLE A. RANGE OF STRESSES IN THE ANCHOR BOLTS DUE TO VIBRATIONS IN THE ROTATING TYPE EQUIPMENT

No.	Name of Equipment	Location	Dwg. No.	Type, Number and Size of Anch. Bolts	Torque Required	Actual Vibratory Stress	Allowable Stress per ATSC Appendix B ₆ for 2×10^6 Cycles or More	Remarks
1	High Pressure Safety Injection Pump SIB-P02	Aux El. 40'	15-C-ZAS-110	14-3/4" ϕ A-307	0 (Snug Tight)	2.3 ksi	Variation of at least 8 ksi (Table B3)	
2	Essential Chilled Water Pump ECB-P01	Control El. 74'	13-C-ZJS-100	8-1/2" ϕ A-307	0 (Snug Tight)	0.75 ksi	Variation of at least 8 ksi (Table B3)	
3	Containment Spray Pump SIA-P03	Aux El. 40'	13-C-ZAS-242	3-2" ϕ A-193	240-250 ft-lbs	1.0 ksi	#	See note
	13-C-ZAS-110		12-1-1/4" ϕ A-307	0 (Snug Tight)	1.9 ksi	Variation of at least 8 ksi (Table B3)	Support at basemat	
4	Diesel Generator Room Essential Exhaust Fan (HDA-J01)	DGB El. 131'-0"	DET 11 on 13-C-ZGS-116	4-1/2" ϕ A-307	0 (Snug Tight)	1.0 ksi	Variation of at least 8 ksi (Table B3)	
5	Essential Air Handling Unit HAA-Z06	Aux El. 120'	13-P-ZAL-206 13-C-ZAS-585	4-7/8" ϕ A-307	0 (Snug Tight)	0.23 ksi	Variation of at least 8 ksi (Table B3)	

NOTE: The prestress corresponding to a torque of 240 ft-lbs is 2.8 ksi which is larger than the stresses in the bolts due to vibration.

TABLE B. ACTUAL VS. ALLOWABLE LOADS IN EQUIPMENT ANCHORAGE

Name of Equipment	Location	Dwg. No.	No. Size and Type of Anchor Bolts	Actual Load in the Anchor Bolts	Allowable Load in the Anchor Bolts	Remarks
1. Containment CEDM Air Cooling Unit	Top of Reactor Vessel Missile Shield Slab	13-C-ZCS-382	10-1" ϕ A449 Anchor Bolts Supplied	NOMINAL	42.4 ^k /Bolt	Vendor requires 10-1 ϕ A-307 anchor bolts. Therefore no calculations have been made.
2. Containment Normal Air Cooling Unit Fans	EL. 140'	13-C-ZCS-534	6-5/8" ϕ A307	3.5 ^k Tension	4.52 ^k	Fan is SUSPENDED FROM PLATFORM.
3.a Containment Reactor Cavity	EL. 95'-11	13-C-ZCS-544	4-1" ϕ A325	Shear 1.13 ^k /Bolt Tension 0.7 ^k /Bolt	Shear 11.78 ^k /Bolt Tension 31.4 ^k /Bolt	
3.b Fan Support Beam C8 x 18.75	EL. 95'-11	13-C-ZCS-544	2-7/8" ϕ A325	Shear 2.1 ^k	Shear 18.4 ^k	



TABLE C. ACTUAL VS. ALLOWABLE LOADS IN STRUCTURAL STEEL JOINTS

Building	Location	Dwg. No.	Beam Connection Type	Actual Reaction	Allowable Reaction per Table I of AISC	Margin (F.S.)
1. Auxiliary	El. 120 Ft.	13-C-ZAS-533	4 7/8" ϕ A325-N	46.6 ^k	72.2 ^k	1.55
2. Control	El. 120 Ft.	13-C-ZJS-510	6 7/8" ϕ A325-N	93 ^k	108.2 ^k	1.16
3. Auxiliary	El. 120 Ft.	13-C-ZAS-584	2 7/8" ϕ A325-N	9.5 ^k	18.04 ^k	1.90
4. Containment	El. 100'-0"	13-C-ZCS-530	9-1" ϕ A325	165.5 ^k	212 ^k	1.28 ¹
5. Containment	El. 140'-0"	13-C-ZCS-535	7 7/8" ϕ A490F	107.6 ^k	168.4	1.57 ²
6. Containment	El. 140'-0"	13-C-ZCS-535	7 7/8" ϕ A490F	96.1 ^k	168.4	1.75 ²
7. Containment	El. 140'-0"	13-C-ZCS-573 Det. 1	6 1-3/8" ϕ A490F	Shear 13.6 ^k /Bolt Ten. 13.4 ^k /Bolt	Shear 26.4 ^k /Bolt Ten. 80.2 ^k /Bolt	1.94 ³
8.a Containment	El. 155'-0"	13-C-ZCS-540	12 1-3/8" ϕ A490F	Shear 75.88 ^k /Bolt	Shear 79.52 ^k /Bolt	1.05 ⁴
8.b Containment	El. 155'-0"	13-C-ZCS-540	6 1-3/8" ϕ A490	1096 ^k	1796 ^k	1.64
8.c Containment	El. 155'-0"	13-C-ZCS-540	16 1-3/8" ϕ A490	667 ^k	3828 ^k	5.74
9. Containment	El. 140'-0"	13-C-ZCS-534	10 7/8" ϕ A490	216.0 ^k w/o pipe reaction	241.0 ^k	1.12
				261 w/pipe reaction	362 ^k	1.39
10. Containment	El. 140'-0"	13-C-ZCS-535	7 7/8" ϕ A490	86.2 ^k w/o pipe reaction	126 ^k	1.46

TABLE C. ACTUAL VS. ALLOWABLE LOADS IN
STRUCTURAL STEEL JOINTS

Building	Location	Dwg. No.	Beam Connection Type	Actual Reaction	Allowable Reaction per Table I of AISC	Margin (F.S.)
10. CONTD.				114.4 ^k w/pipe reaction	189 ^k *	1.65
<ol style="list-style-type: none"> 1. Critical connection 2. Critical connection providing lateral support for safety injection tank 3. Critical connection attaching keyway to structural steel beam 4. Critical connection pipe whip restraint for main steam line 						

* ALLOWABLES ARE INCREASED
PER DESIGN CRITERIA IN CASE
WHERE PIPE REACTIONS ARE
INCLUDED

NOTE: The critical connections were identified on the following basis;

1. The connections for steel members which provided support for critical components such as the safety injection tanks.
2. Structural steel supporting large piping such as main steam line pipe whip restraints
3. The primary 'Column Circle' connections for members which do not support concrete slabs and 'radial' members which link the main columns to the reinforced concrete interior structures.
4. Members which provide primary seismic support for platforms