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October 24, 1984

Mr. Harold R. Denton, Director  
Office of Nuclear Reactor Regulation  
U.S. Nuclear Regulatory Commission  
Washington, DC 20555

Subject: Byron Generating Station Units 1 and 2  
Braidwood Generating Station Units 1 and 2  
Iodine Sampling of Stack Effluent  
NRC Docket Nos. 50-454/455 and 50-456/457

Reference (a): T. R. Tramm letter to H. R. Denton  
dated September 26, 1984

Dear Mr. Denton:

Reference (a) provided additional information regarding the design basis for the shielding associated with iodine sampling of the Byron/Braidwood vent stack effluent under post-accident conditions. During review of this information with members of your Staff, a calculational error was pointed out in the charcoal filter correction. This produced an incorrect Iodine Source Term which caused further inaccuracies in the submittal.

Attachments 1 through 4 to this letter have the correct information underlined. Please substitute them for the Reference (a) attachments.

Please address further questions regarding this matter to this office. One signed original and fifteen copies of this letter and the attachments are provided for NRC review.

Very truly yours,

David H. Smith  
Nuclear Licensing Administrator

Attachments

cc: Byron - Resident Inspector  
J. Streeter - RIII

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ATTACHMENT 1: Calculation of Iodine Source Term

The following iodine source term calculation is based on a loss of all AC power scenario (details of this scenario are available from G. T. Klopp, Project Engineering Department). 100% of the noble gas core inventory and 1.5% of the iodine core inventory is released 33 hours after the event occurs. The duration of the release is 4 hours. At the time of the release, it is assumed that one Auxiliary Building Vent Fan is operable and that the charcoal filters are 10% efficient in filtering iodines.

1. Iodine Core Inventory (Byron FSAR, Table 15.0-8)

I-131	8.8E7	curies	Decayed 33 hours*	5.14E6 curies
I-132	1.34E8	curies		5.30E3 curies
I-133	1.97E8	curies		6.38E7 curies
I-134	2.31E8	curies		8.01E-4 curies
I-135	1.79E8	curies		<u>5.84E6 curies</u>
			TOTAL	<u>7.49E7 curies</u>

\*Release occurs 33 hours after event.

2. Total Fraction of Iodines Released = .015

$$7.49E7 \text{ Ci} \times .015 = 1.12E6 \text{ Ci released}$$

3. Fraction of Iodines Released Per Minute

$$\frac{.015 \times 1 \text{ hr}}{4 \text{ hrs} \times 60 \text{ min}} = 6.25E-5/\text{minute} \times 7.49E7 \text{ Ci} = 4680 \text{ Ci/min}$$

4. Assume One Auxiliary Building Fan On.

$$\frac{4680 \text{ Ci}}{\text{min}} \div \frac{159000 \text{ ft}^3}{\text{min}} = 2.94E-2 \text{ Ci/ft}^3 = 1.04E0 \text{ uCi/cc}$$

5. Assume Charcoal is 10% efficient for Iodines.

$$1.04E0 \text{ uCi/cc} \times .90 = \underline{0.936 \text{ uCi/cc Iodine Source Term}}$$

ATTACHMENT 2: Dose Rate from Iodine Filter Assembly

The following is a calculation of the dose rate from the General Atomic Wide Range Gas Monitor grab sample assembly. A one-minute grab sample is obtained. The monitor flowrate is 0.06 cfm.

1. Contact Dose Rate

$$\underline{9.36E-1} \text{ uCi/cc} \times .06 \text{ ft}^3/\text{min} \times 28320 \text{ cc/ft}^3 \times 1 \text{ min} = \underline{1590} \text{ uCi}$$

on assembly

$$5.6E3 \times \underline{1.59E-3} \text{ Ci} \times .5\text{Mev} = \underline{4.45} \text{ R/hr at 1 cm}$$

2. Dose Rate at One Foot

$$\frac{4.445 (1)^2}{(30.48)^2} = \underline{4.80} \text{ mR/hr at 1 ft.}$$

### ATTACHMENT 3: TIME MOTION STUDY

The following summarizes the dose accumulated in the process of going to the General Atomic Wide Range Gas Monitor, obtaining the grab sample, and transporting the samples back to the laboratory for analysis. The purpose of this summary is to verify Byron can meet criteria of GDC 19 (r-rem whole body and 75-rem extremity). The dose rate specified at the monitor includes dose rates from the sample lines and from the two high range continuously sampling filter assemblies. Dose rates along the path to and from the monitor are based on valves specified in the Postaccident Radiation Zone Maps found in Appendix E of the Byron FSAR (for a major line break accident in containment).

Area	Time spent in Area	Dose Rate in Area	Dose Accumulated in Area
OSC to 451' Aux. Bldg.	3 minutes	1R/hr	50 mR
451' to 426' Aux. Bldg.	1 minute	15 mR/hr	.25mR
426' to 451' Aux. Bldg.	.5 minute	10 R/hr	83.5mR
451' to 477' Aux. Bldg.	1.5 minutes	10R/hr	250mR
At monitor	4 minutes	<u>65mR/hr*</u>	<u>4.5mR</u>
477' to 451' Aux. Bldg.	1.5 minutes	10 R/hr	250mR
451' to Lab	1 minute	15mR/hr	.25mR
		TOTAL	<u>638.5</u>

\*Includes dose rate at 1 foot from grab sample filter assembly, dose rates from sample lines, dose rates from the high range continuous sample casks, and general area dose rate.

Two individuals will be needed to perform this task, thus the total dose is multiplied by 2 to get a TOTAL dose for this task of 1.277 R whole body. The extremity dose to the sample collectors is not expected to exceed 2R.

ATTACHMENT 4: Dose Rates from Sample Lines, Sample Casks

The following calculations document additional dose rates due to sample lines on the Wide Range Gas Monitor and the two continuous sampling filter assembly cask units. Sample line dose rates are based on noble gas activity in the lines. Specific values reported are obtained from "Analysis of Radiation Detectable from Stack Vent Sample Line Under Design Basis Accident Conditions - CECO Contract 37844", prepared by Catalytic, Inc. (November, 1980).

1. Noble Gas Core Inventory (Byron FSAR, Table 15.0-8)

Kr 83 m	1.54E7 Ci	Decayed 33 hours*	7.50E 1 Ci
Kr 85	9.99E5 Ci		9.99E 5 Ci
Kr 85 m	3.95E7 Ci		2.18E 5 Ci
Kr 87	7.59E7 Ci		1.09E 0 Ci
Kr 88	1.08E8 Ci		3.06E 4 Ci
Kr 89	1.40E8 Ci		0 Ci
Xe 131 m	6.68E5 Ci		6.16E 5 Ci
Xe 133	2.03E8 Ci		1.69E 8 Ci
Xe 133 m*	5.16E6 Ci		3.38E 6 Ci
Xe 135	5.55E7 Ci		4.55E 6 Ci
Xe 135M	5.46E7 Ci		0 Xi
Xe 138	1.79E8 Ci		0 Ci
			<u>1.79E 8 Ci</u>

\* Release occurs 33 hours after event.

2. 100% of noble gases released. Fraction released per minute:

$$\frac{1}{4 \text{ hr}} \times \frac{1 \text{ hr}}{60 \text{ min.}} = 4.17\text{E-}3/\text{min} \times 1.79\text{E}8 \text{ Ci} = 7.46\text{E}5 \text{ Ci/min}$$

3. Assume One Auxiliary Building Fan On

$$7.46\text{E}5 \text{ Ci/min} - 159000 \text{ ft}^3/\text{min} = 4.69 \text{ Ci/ft}^3 = 166 \text{ uCi/cc}$$

4. Sample Line Dose Rates

Dose rates are reported for (a) 2 foot section of 1-inch diameter sample line at 6 inches from the line and (b) 2 foot section of 3/8 inch diameter sample line at 6 inches from the line. This results in a conservative dose rate as the sample collector will actually be approximately 2 to 3 feet from the sample lines and actual sample lines are 3/4 inch and 1/8 inch in diameter.

a. Dose rate from 1 inch diameter line at 6 inches.

$$.17 \frac{\text{mrem/hr}}{\text{uCi/cc}} \times 166 \text{ uCi/cc} \times 1.4^* = 39.5 \text{ mrem/hr}$$

\* Dose rate for 2 foot line section is 40% greater than for the .17 mrem/hr/uCi/cc value for a 1 foot line section.

ATTACHMENT 4  
Continued

b. Dose rate from 3/8 inch diameter line at 6 inches

$$.015 \frac{\text{mrem/hr}}{\text{uCi/cc}} \times 166 \text{ uCi/cc} \times 1.4 = 3.5 \text{ mrem/hr}$$

5. Sampling Cask Dose Rates

Dose rates from the two continuous sampling filter assemblies are based on the iodine source term of  $1.04\text{E-}01$  uCi/cc and a sample time of 30 minutes. The lead casks are 2 inches thick.

$$\underline{9.36\text{E-}1} \text{ uCi/cc} \times 28320 \text{ cc/ft}^3 \times .06 \text{ ft}^3/\text{min} \times 30 \text{ min} = \underline{47700} \text{ uCi on filter assembly}$$

$$5.6\text{E}3 \times .5 \text{ MEV} \times \underline{4.77\text{E-}2} \text{ Ci} = \underline{133} \text{ R/hr at 1 cm}$$

$$= \underline{5.2} \text{ R/hr at 5.08 cm unshielded}$$

$$I = I_0 e^{-uX} = 575 e^{- (1.82) \times (5.08\text{cm})}$$

$$= \underline{0.5} \text{ mR/hr at surface of cask}$$

6. Low Range Filter Assemblies

Dose contribution from low range filter assemblies is negligible. Pump actuation setpoints will be established to ensure the low range pump is shut down prior to reaching any significant iodine concentrations in the sampling system.

The setpoint for shutting down the low range pump will initially be established at  $10^{-3}$  uCi/cc noble gas activity (this value may be changed as operating experience is gained).

The ratio of the iodine activity in the stack to the noble gas activity in the stack is .00564 ( $.936 \div 166$ ). Based on this ratio, the iodine activity equivalent to  $10^{-3}$  uCi/cc noble gases is  $5.64\text{E-}6$  uCi/cc.

Assuming a 30 minutes sample time at  $5.64\text{E-}6$  uCi/cc:

$$5.64\text{E-}6 \text{ uCi/cc} \times 28320 \text{ cc/ft}^3 \times 1.6 \text{ ft}^3/\text{min} \times 30 \text{ min} = 7.67 \text{ uCi on filter assembly}$$

$$5.63\text{E}3 \times .5 \text{ mev} \times 7.67\text{E-}6 \text{ Ci} = 21.5 \text{ mR/hr at 1 cm}$$
$$= .02 \text{ mR/hr at 1 foot.}$$