



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D. C. 20555

SOUTH CAROLINA ELECTRIC & GAS COMPANY

SOUTH CAROLINA PUBLIC SERVICE AUTHORITY

DOCKET NO. 50-395

VIRGIL C. SUMMER NUCLEAR STATION, UNIT NO. 1

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 28
License No. NPF-12

1. The Nuclear Regulatory Commission (the Commission) has found that:
 - A. The application for amendment to the Virgil C. Summer Nuclear Station, Unit No. 1 (the facility) Facility Operating License No. NPF-12 filed by the South Carolina Electric & Gas Company acting for itself and South Carolina Public Service Authority (the licensees), dated July 22, 1983, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act) and the Commission's regulations set forth in 10 CFR Chapter I;
 - B. The facility will operate in conformity with the application, as amended, the provisions of the Act, and the regulations of the Commission;
 - C. There is reasonable assurance: (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations set forth in 10 CFR Chapter I;
 - D. The issuance of this license amendment will not be inimical to the common defense and security or to the health and safety of the public;
 - E. The issuance of this license amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.
2. Accordingly, the license is hereby amended by page changes to the Technical Specifications as indicated in the attachments to this license amendment and paragraph 2.C(2) of Facility Operating License No. NPF-12 is hereby amended to read as follows:

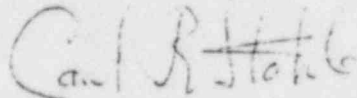
(2) Technical Specifications

The Technical Specifications contained in Appendix A, as revised through Amendment No. 28, are hereby incorporated into this license. South Carolina Electric & Gas Company shall operate the facility in accordance with the Technical Specifications and the Environmental Protection Plan.

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3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION



Elinor G. Adensam, Chief
Licensing Branch No. 4
Division of Licensing

Enclosure:
Technical Specification Changes

Date of Issuance: October 12, 1984

ATTACHMENT TO LICENSE AMENDMENT NO. 28

FACILITY OPERATING LICENSE NO. NPF-12

DOCKET NO. 50-395

Replace the following pages of the Appendix "A" Technical Specifications with the enclosed pages. The revised pages are identified by Amendment number and contain vertical lines indicating the areas of change. To maintain document completeness, the corresponding overleaf pages are also provided.

Amended
Page

2 - 8
2 - 9
2 - 10

Overleaf
Page

2 - 7

Delete page 2 - 11

TABLE 2.2-1 (continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

<u>Functional Unit</u>	<u>Total Allowance (TA)</u>	<u>Z</u>	<u>S</u>	<u>Trip Setpoint</u>	<u>Allowable Value</u>
18. Safety Injection Input from ESF	NA	NA	NA	NA	NA
19. Reactor Trip System Interlocks					
A. Intermediate Range Neutron Flux, P-6	NA	NA	NA	$\geq 1 \times 10^{-10}$ amps	$\geq 6 \times 10^{-11}$ amps
B. Low Power Reactor Trips Block, P-7					
a. P-10 input	7.5	4.56	0	$\leq 10\%$ of RTP	$\leq 12.2\%$ of RTP
b. P-13 input	7.5	4.56	0	$\leq 10\%$ turbine impulse pressure equivalent	$\leq 12.2\%$ of turbine impulse pressure equivalent
C. Power Range Neutron Flux P-8	7.5	4.56	0	$\leq 38\%$ of RTP	$\leq 40.2\%$ of RTP
D. Low Setpoint Power Range Neutron Flux, P-10	7.5	4.56	0	$\geq 10\%$ of RTP	$\geq 7.8\%$ of RTP
E. Turbine Impulse Chamber Pressure, P-13	7.5	4.56	0	$\leq 10\%$ turbine impulse pressure equivalent	$\leq 12.2\%$ turbine pressure equivalent
20. Reactor Trip Breakers	NA	NA	NA	NA	NA
21. Automatic Actuation Logic	NA	NA	NA	NA	NA

RTP = RATED THERMAL POWER

TABLE 2.2-1 (Continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

NOTATION

NOTE 1: OVERTEMPERATURE ΔT

$$\Delta T \leq \Delta T_0 \left\{ K_1 - K_2 \frac{(1 + \tau_1 S)}{(1 + \tau_2 S)} [T - T'] + K_3(P - P') - f_1(\Delta I) \right\}$$

- Where:
- ΔT = Measured ΔT by RTD Manifold Instrumentation
 - ΔT_0 = Indicated ΔT at RATED THERMAL POWER
 - K_1 = 1.090
 - K_2 = 0.01450
 - $\frac{1 + \tau_1 S}{1 + \tau_2 S}$ = The function generated by the lead-lag controller for T_{avg} dynamic compensation
 - $\tau_1, \text{ \& } \tau_2$ = Time constants utilized in the lead-lag controller for T_{avg} , $\tau_1 = 33$ secs., $\tau_2 = 4$ secs.
 - T = Average temperature °F
 - T' \leq 587.4°F Reference T_{avg} at RATED THERMAL POWER
 - K_3 = .0006728
 - P = Pressurizer pressure, psig
 - P' = 2235 psig, Nominal RCS operating pressure
 - S = Laplace transform operator, sec^{-1} .

TABLE 2.2-1 (Continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

NOTATION (Continued)

NOTE 1: (Continued)

and $f_1(\Delta I)$ is a function of the indicated difference between top and bottom detectors of the power-range nuclear ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that:

- (i) for $q_t - q_b$ between -34 percent and +8 percent $f_1(\Delta I) = 0$ where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t + q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER.
- (ii) for each percent that the magnitude of $q_t - q_b$ exceeds -34 percent, the ΔT trip setpoint shall be automatically reduced by 1.67 percent of its value at RATED THERMAL POWER.
- (iii) for each percent that the magnitude of $q_t - q_b$ exceeds +8 percent, the ΔT trip setpoint shall be automatically reduced by 1.11 percent of its value at RATED THERMAL POWER.

NOTE 2: The channel's maximum trip setpoint shall not exceed its computed trip point by more than 3.6 percent ΔT span.

NOTE 3: OVERPOWER ΔT

$$\Delta T \leq \Delta T_0 \left\{ K_4 - K_5 \left(\frac{\tau_3 S}{1 + \tau_3 S} \right) T - K_6 [T - T''] \right\}$$

Where: ΔT = as defined in Note 1

ΔT_0 = as defined in Note 1

K_4 = 1.091

K_5 = 0.02/°F for increasing average temperature and 0 for decreasing average temperature

$\frac{\tau_3 S}{1 + \tau_3 S}$ = The function generated by the rate-lag controller for T_{avg} dynamic compensation

TABLE 2.2-1 (Continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTSNOTATION (Continued)

NOTE 3: (Continued)

τ_3	=	Time constant utilized in the rate-lag controller for T_{avg} , $\tau_3 = 10$ secs.
K_6	=	0.001190/ $^{\circ}$ F for $T > T''$ and $K_6 = 0$ for $T \leq T''$
T	=	as defined in Note 1
T''	<	587.4 $^{\circ}$ F Reference T_{avg} at RATED THERMAL POWER
S	=	as defined in Note 1

NOTE 4: The channel's maximum trip setpoint shall not exceed its computed trip point by more than 2.7 percent ΔT span.