

September 2, 1992

Ken R. Jaquay
Rockwell International
Mail Stop T487
6633 Canoga Avenue
Canoga Park, CA 91303

Dear Ken:

Subject: ABWR postulated Pipe Break Dynamic Nonlinear Time History Analysis

Enclosed are the responses to the ABWR piping audit comments pertaining to the subject analysis. If you have any questions please call me (408-925-4824) or Henry Hwang (408-925-1984).

Sincerely,

J.N.F.

Jack N. Fox
Advanced Reactor Programs

cc: Chet Poslusny/Shou Hou

290092

9210050228 920902
PDR TOPPAK ENCL/EMERGENT
A PDR

See attached
distribution 2222
per C. Poslusny

SUBJECT: ABWR POSTULATED PIPE BREAK DYNAMIC NONLINEAR
TIME HISTORY ANALYSIS

CC: SJ Lin J Wallach
M Herzog EO Swain
J N Fox

RESPONSES TO AUDIT COMMENTS (Prepared by Henry Hwang) 4 Hwang 9/1/91

Analysis Model Description:

The pipe break non-linear time history analysis can be performed by ANSYS program. Attach A shows the input example of the main steam pipe. The selection of the input are described as follows:

Analysis : KAN=4
Plastic pipe : use STIF 20
Plastic elbow: use STIF 60
Pipe whip restraint : use STIFF 39

A small PC program has been written to convert force time history output to ANSYS time history input format. The verification of the program can be performed by individual visual checking.

PA = 373,570 lb

Audit Comment 1 :

The time step used in the Main Steam Break Structure (MSBS) analysis is 0.001 second. In order to prove the convergency of the solution, GE agreed to use 0.0005 second time steps in a repeat of the analysis.

Response :

In order to show that the analysis time step 0.001 second is adequate, an analysis with time step of 0.0005 second has been performed. The results of the analysis are plotted in the following figures. Comparisons of the results between 0.001 sec and 0.0005 sec time step showed that the differences are less than 3%. Therefore, time step of 0.001 sec can be used in future analysis.

Figure 1-1 : ANSYS analysis model- element plot.

Figure 1-2 : ANSYS analysis model- nodal plot.

Figure 2 : Impact force at the pipe whip restraint. DT=0.001 sec
(pa=373,600 lb, max impact=670,000 lb)

Figure 3 : Bending moment time histories. DT=0.001 sec.
at elm. 2I ,at elbow near break

Figure 4 : Displacement time histories. DT=0.001 sec
at the break location

Figure 5 : Moment time history at headfitting, (Elm 42J)
DT=0.001 sec.

Figure 6 : Force time histories at headfitting. (Elm 42J)
DT=0.001 sec

Figure 7 : Bending moment time histories. DT=0.001 sec
at elm 22J ,before main steam guide

Figure 8 : Bending moment time histories. DT=0.001 sec
at elm 42I ,near headfitting

Figure 9 : Bending moment time histories. DT=0.001 sec.
at Elm 38I, 1st elm after MSIV.

Figure 2A: Impact force at the pipe whip restraint. DT=0.0005 sec
(pa=373,600 lb, max impact=670,000 lb)

Figure 3A: Bending moment time histories. DT=0.0005 sec.
at elm. 2I ,at elbow near break

Figure 4A: Displacement time histories. DT=0.0005 sec
at the break location

Figure 5A: Moment time history at headfitting, (Elm 42J)
DT=0.0005 sec.

Figure 6A: Force time histories at headfitting. (Elm 42J)
DT=0.0005 sec

Figure 7A: Bending moment time histories. DT=0.0005 sec
at elm 22J ,before main steam guide

Figure 8A: Bending moment time histories. DT=0.0005 sec
at elm 42I ,near headfitting

Comment 2 :

The displacements from the terminal end Main Steam Break Structure (MSBS) analysis (using ANSYS) results shows large displacements and rotation at the break. The thrust direction changes during the event which could affect the stress in the "Holy Pipe" area. Therefore, GE will use static elastic analyses for the original and displaced position to confirm the validity of the small displacement assumption in the non-linear time history analysis results.

Response :

Because of nonlinearity in the material and the pipe whip restraint, using static analysis to compare the results of large displacements is not as accurate as the time history analysis. Therefore, the following time history analysis is performed instead of static time history analysis.

The original coordinates at the break (Node 4) and the next node (Node 5) to the elbow are as follows:

	X	Y	Z
4	69.75	611.97	214.66
5	73.94	611.97	227.56

Delta	-4.19	0.0	-12.90

Figure 4A show the displacement differences at Node 4 and Node 5. It can be seen the maximum displacement differences are :

	Ux	Uy	Uz
U4 - U5	1.0	5.3	1.0

The new coordinate for Node 4 become:

$$\begin{aligned} X_4 &= 69.75 + 1.0 = 70.75" \\ Y_4 &= 611.97 + 5.3 = 617.27 \\ Z_4 &= 214.66 + 1.0 = 215.66" \end{aligned}$$

The force direction has been changed also, the values of Delta becomes:

	X	Y	Z	
Delta	-4.19+1	0+5.3	-12.9+1	
=	-3.19	5.3	-11.9	SRSS = 13.4
D Cosine	0.238	-0.395	0.890	

Reaction force

The total blowdown force is resolved to the new direct cosine for the analysis of large displacement effect:

$$\begin{aligned} F_x &= 88,800 \text{ lb} \\ F_y &= -147,400 \text{ lb} \\ F_z &= 332,114 \text{ lb} \end{aligned}$$

The results of the analysis are shown in the figures below.

Figure 2B: Impact force at the pipe whip restraint. DT=0.001 sec
(pa=373,600 lb, max impact=670,000 lb)
(Included rotated blowdown angle)

Figure 4B: Displacement time histories. DT=0.001 sec
at the break location
(Included rotated blowdown angle)

Figure 5B: Moment time histories at 42J (headfitting)
(Included rotated blowdown angle)

Figure 6B: Force time histories at 42J (headfitting)
(Included rotated blowdown angle)

Figure 7B: Bending moment time histories. DT=0.001 sec
at elm 22J ,before main steam guide
(Included rotated blowdown angle)

Figure 9B: Force time histories at 22J, before main steam guide.
(Included rotated blowdown angle)

It is noted that not all the plots as shown in the design configuration are plotted because some of the plots are not needed for comparison and it take too long to plot.

Comparisons of the bending moments and bending stresses at the head fitting are as follows:

Pipe = 28" OD x 1.423" t

$$\begin{aligned} I &= (28^4 - 25.154^4) \times 3.1416/64 \\ &= 10520 \text{ in}^4 \\ Z &= 751 \text{ in}^3 \end{aligned}$$

Assume break occurs at normal operation, T=552 deg. F.
Sm = 18,570 psi for SA-350-LF2 (Carbon steel)

$$\begin{aligned} \text{Allowable limit} &= 2.25 Sm \\ &= 41780 \text{ psi} \end{aligned}$$

The maximum bending moment between the MSIV's will be developed about 0.075 second after the break. The decompressing wave travels at 1600 ft/sec. It has traveled a distance of $1600 \times 0.075 = 120$ ft when the maximum moment occurs. Therefore, the pressure between the MSIV at the time when the maximum bending moment is developed will be much less than normal operating pressure of 1050 psi.

$$\begin{aligned} Sp &= PD/4t \\ &< 1050 \times 28/(4 \times 1.423) \\ &= 5165 \text{ psi} \end{aligned}$$

Weight stress, Swt = < 500 psi

$$Sp + Swt < 5665 \text{ psi}$$

Results 1 = Using normal procedure with time step 0.001 sec.

Results 2 = Study case with time step 0.0005 sec.

Results 3 = Study case with time step 0.001 sec.
Include force angle rotated.

Moment and stresses at the headfitting

	Ma (E6)	Mb (E6)	Mc (E6)	Mr (E6)	B2 M/Z psi
Result 1	15.3	15.0	13.3	25.2	33600
Result 2	15.0	15.0	13.3	25.1	33500
Result 3	20.5	4.5	9.0	22.8	30400

This can be seen that the values calculated from the result 1 is slightly conservative. From Figure 9, moment time history plots at element 38I, the first element after MSIV, the maximum bending are as follows:

	Ma (E6)	Mb (E6)	Mc (E6)	Mr (E6)	B2 M/Z psi
38I	15.0	13.0	11.5	22.94	30,600

This shows that the maximum stress between isolation valve is at the headfitting. The combined stress is as follows:

$$\begin{aligned} Sp + Sw + S \text{ break} &= 5165 + 500 + 33600 \\ &= 39,265 \text{ psi} \end{aligned}$$

Allowable stress = 41,780 psi

All the stresses are within the allowable limit of 2.25 Sm.

CONCLUSIONS :

1) The stresses between the MSIV's does not increase due to the force direction change as result of the displacements at the break location. This shows that the nonlinear analysis based on design location is acceptable.

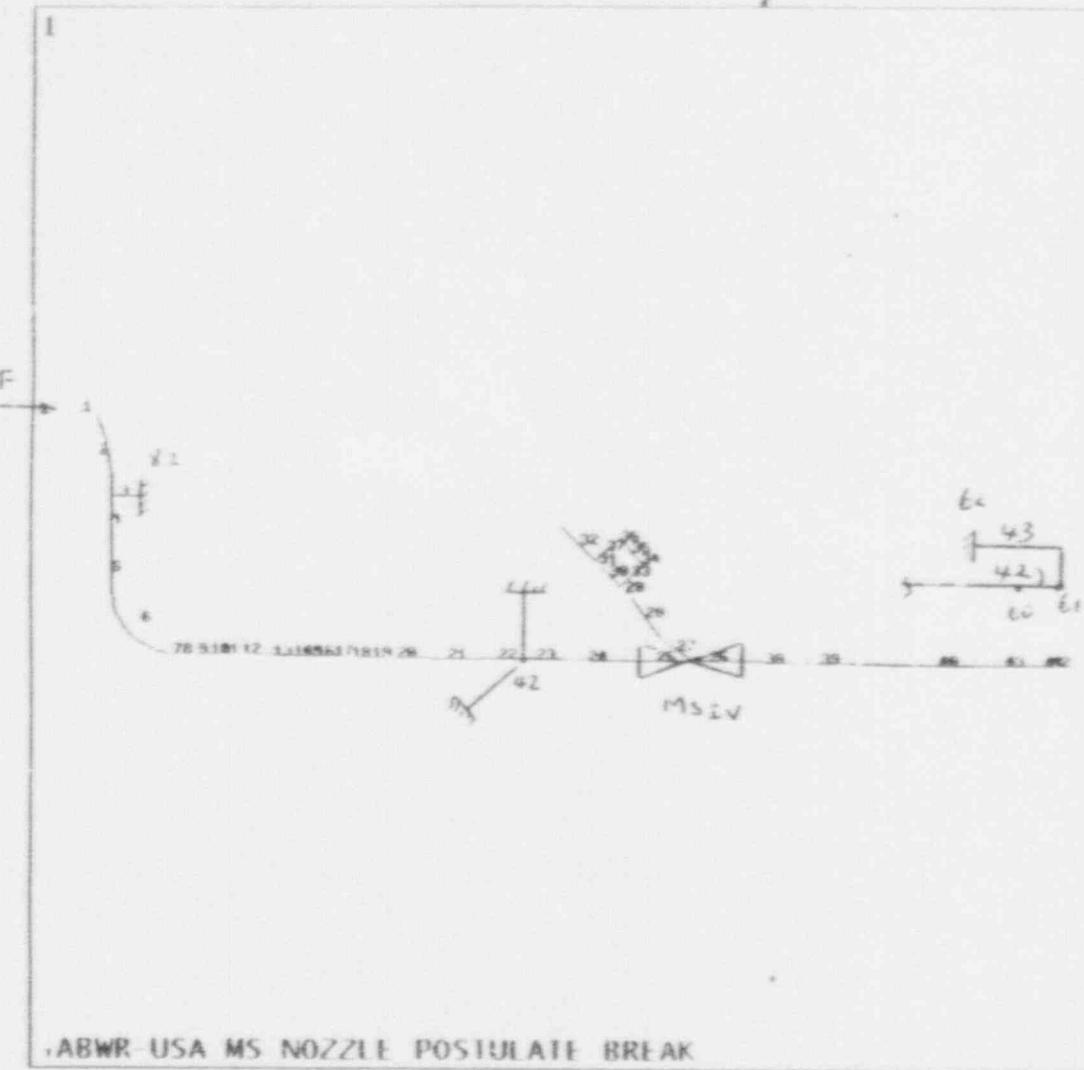
2) Calculated pipe whip restraint load by ANSYS is 670,000 lb. The PDA calculated peak restraint load of 666,000 lb .

PDA program is acceptable to be used for sizing the pipe whip restraints.

3) The rotated angle load resulted in downward thrust load will reduce the vertical displacement predicted by the analysis from the design position.

This shows that the analysis from design position is acceptable.

4) The input listing for the as design case are shown in Attachment 1.



ANSYS 4.4A
AUG 31 1992
16:46:09
POST1 ELEMENTS
ELEM NUM

ZV =1
DIST=351.175
XF =389
YF =528.71
ZF =182.01

PRODUCE ELEMENT PLOT
POST1 -INP-

Figure 1-1 : ANSYS analysis model- element plot.

ANSYS 4.4A
AUG 31 1992
16:47:41
POST1 NODES

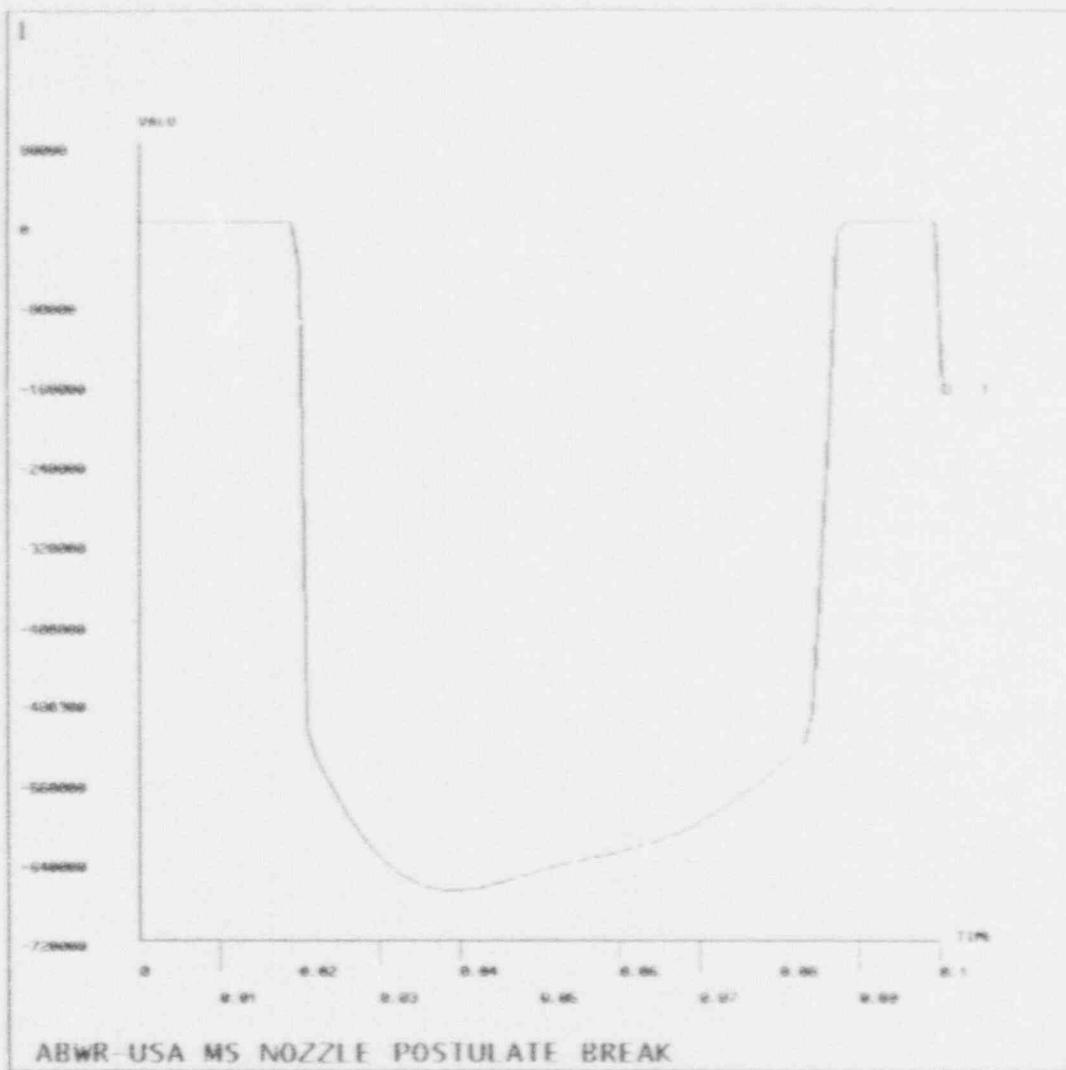
ZV =1
DIST=351.175
XF =389
YF =528.71
ZF =182.01



,ABWR-USA MS NOZZLE POSTULATE BREAK

PRODUCE NODE PLOT
POST1 -INP=

Figure 1-2 : ANSYS analysis model- nodal plot.



CURVE	VARIABLE	NAME	
1	2	3	1

POST26 INP=

ANSYS 4.4A
AUG 7 1992
13:54:18
POST26

ZV =1
DIST=0.6666
XF =0.5
YF =0.5
ZF =0.5

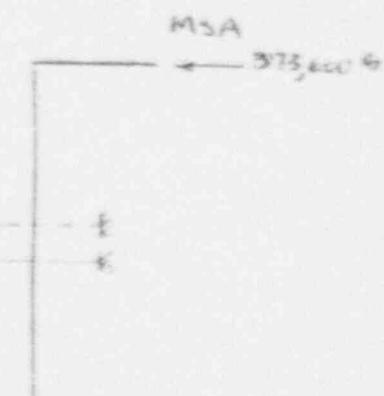
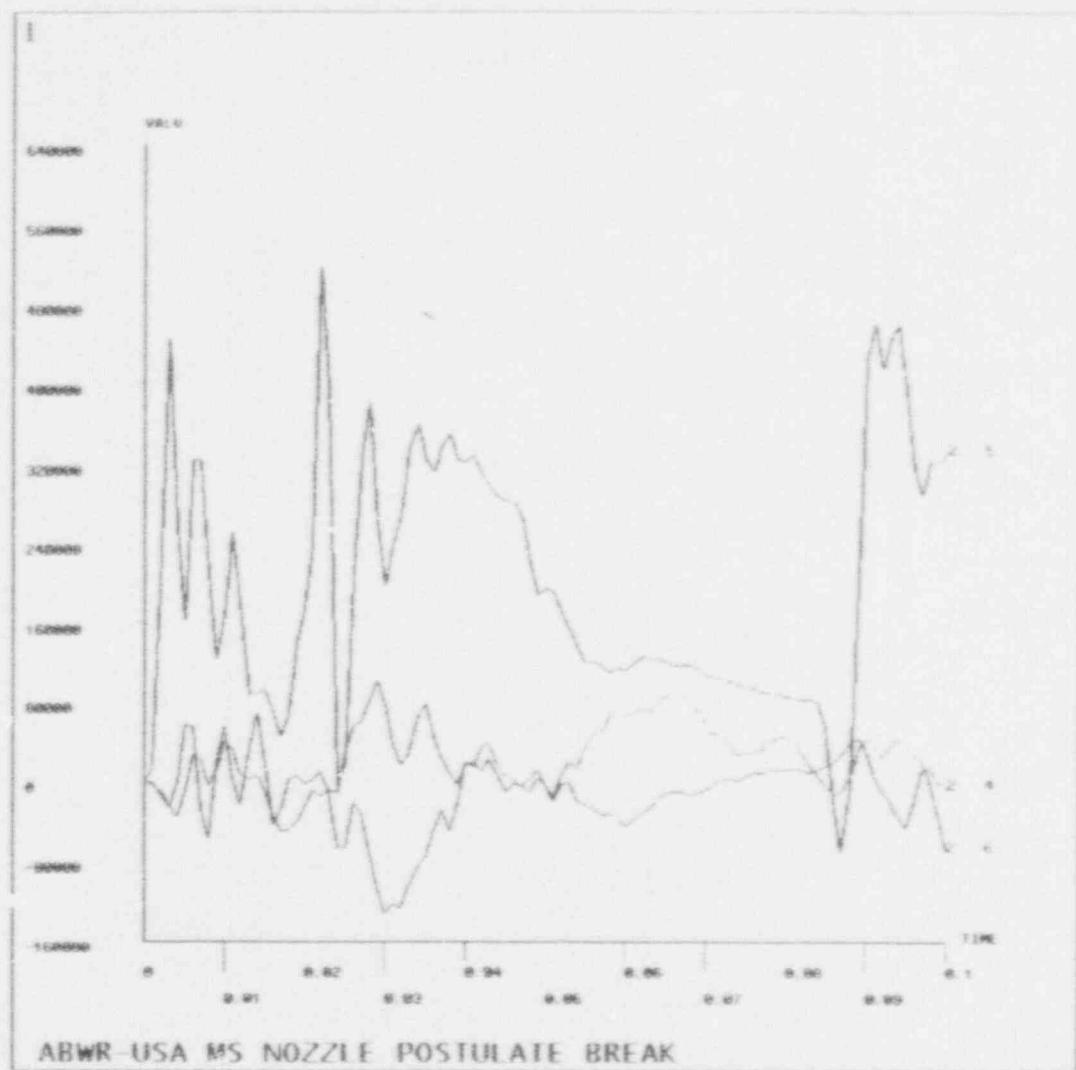
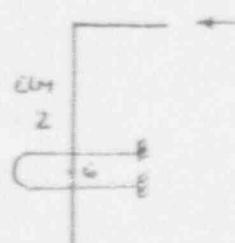


Figure 2 : Impact force at the pipe's whip restraint. DT=0.001 sec
(pa=373,600 lb, max impact=670,000 lb)



ANSYS 4.4A
AUG 7 1992
14:00:09
POST26

ZV = 1
DIST = 0.6666
XF = -0.5
YF = -0.5
ZF = -0.5

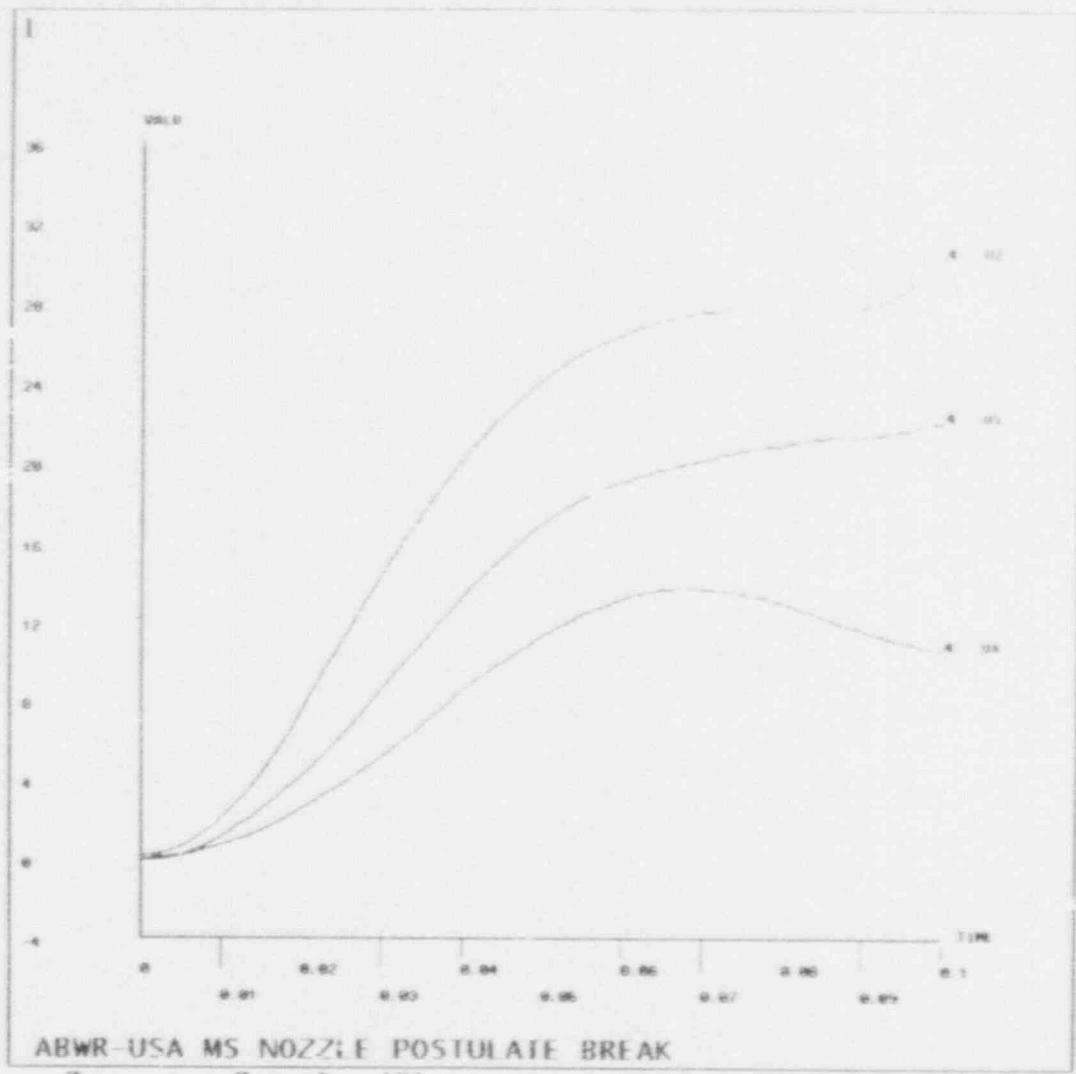


ABWR-USA MS NOZZLE POSTULATE BREAK

2	3	2	5
3	4	2	6

POST26-INP=

Figure 3 : Bending moment time histories. DT=0.001 sec.
at elm. 2I , at elbow near break



ANSYS 4.4A
AUG 7 1992
14:03:25
POST26

ZV =1
DIST=0.6666
XF =0.5
YF =0.5
ZF =0.5

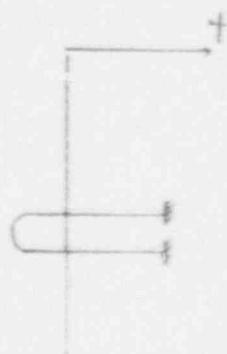
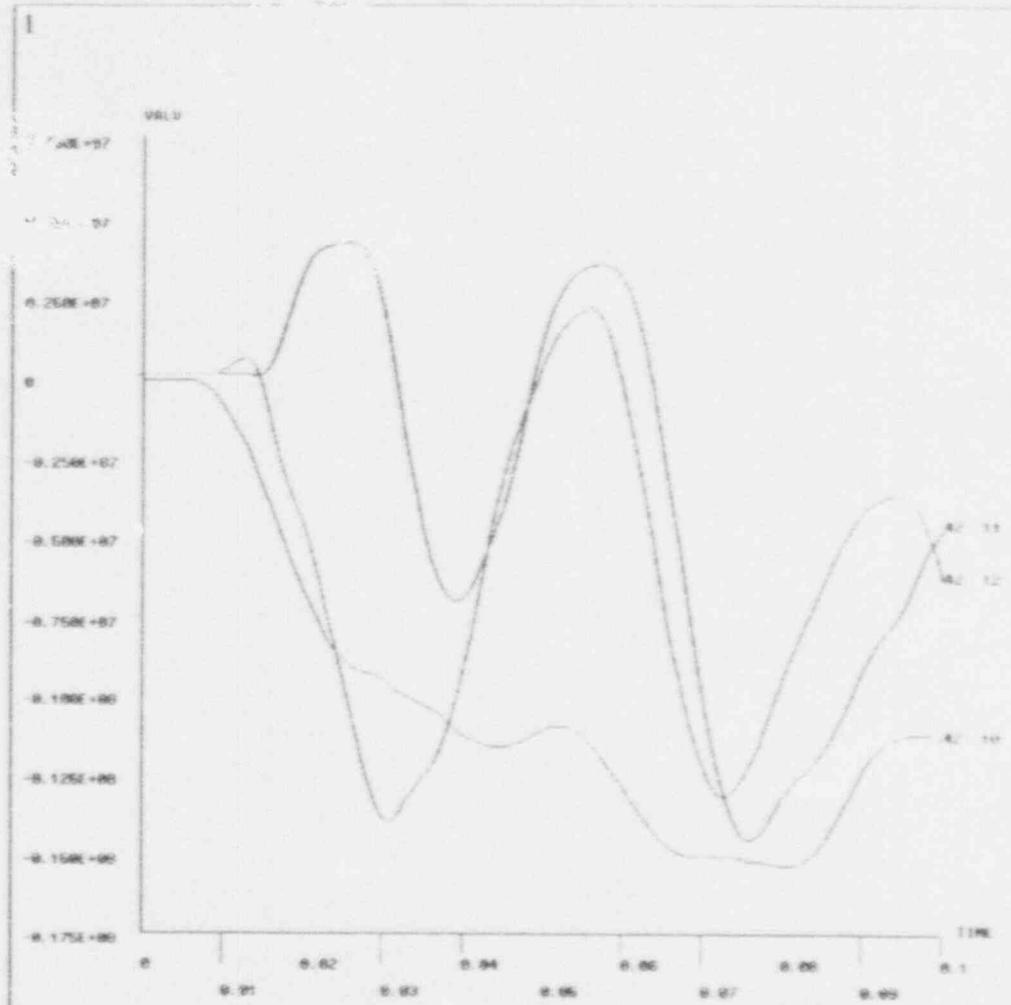
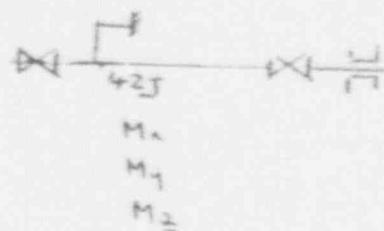


Figure 4 : Displacement time histories. DT=0.001 sec
at the break location

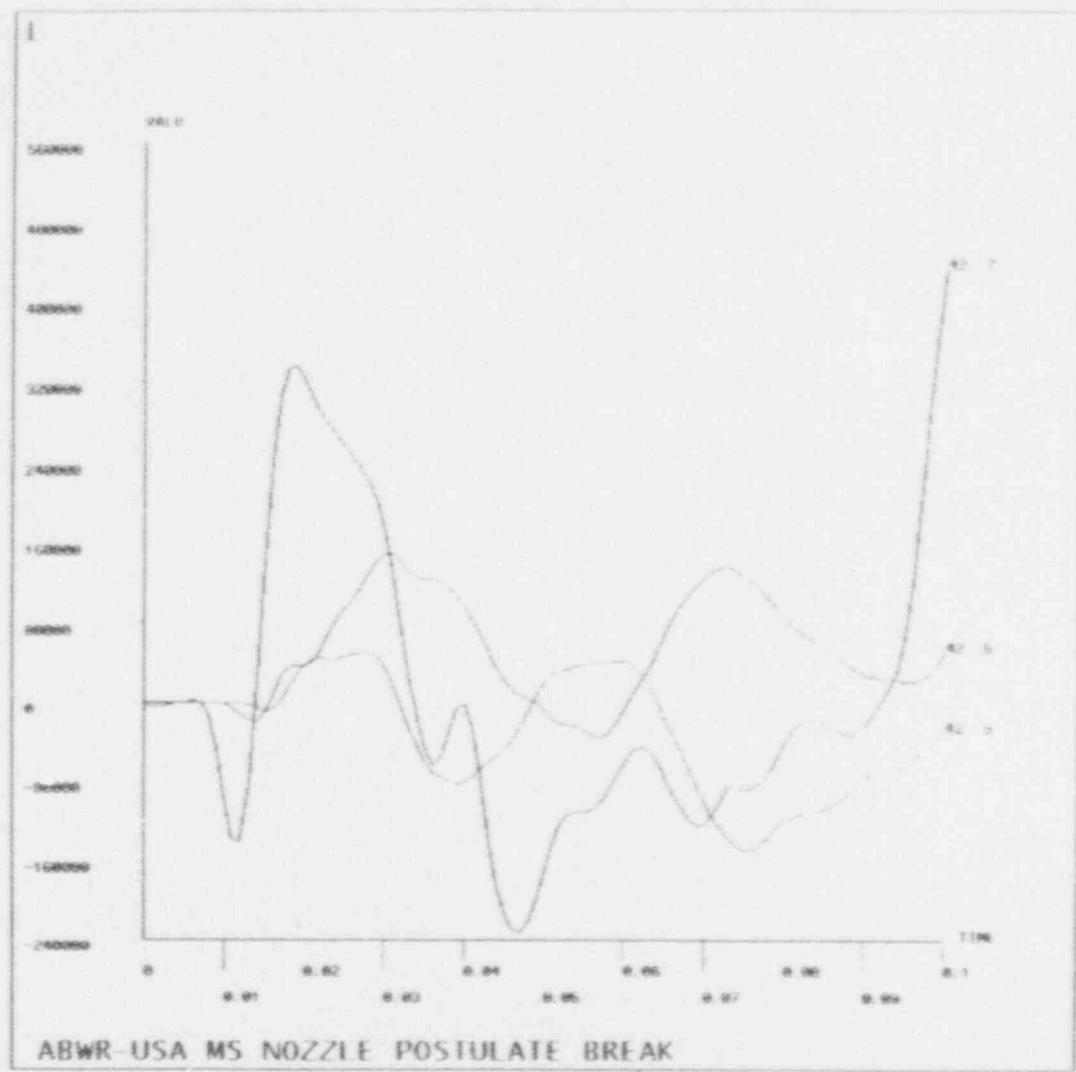


ANSYS 4.4A
AUG 7 1992
14:21:15
POST26



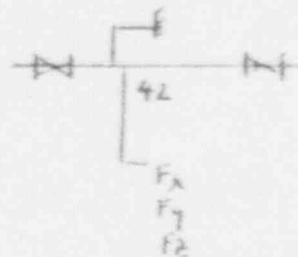
POST26-INP=

Figure 5 : Moment time history at headfitting, (Elm 42J)
DT=0.001 sec.



ANSYS 4.4A
AUG 7 1992
14:27:03
POST26

ZV = 1
DIST = 0.6666
XF = 0.5
YF = 0.5
ZF = 0.5



POST26-INP=

Figure 6 : Force time histories at headfitting. (Elm 42J)
DT=0.001 sec

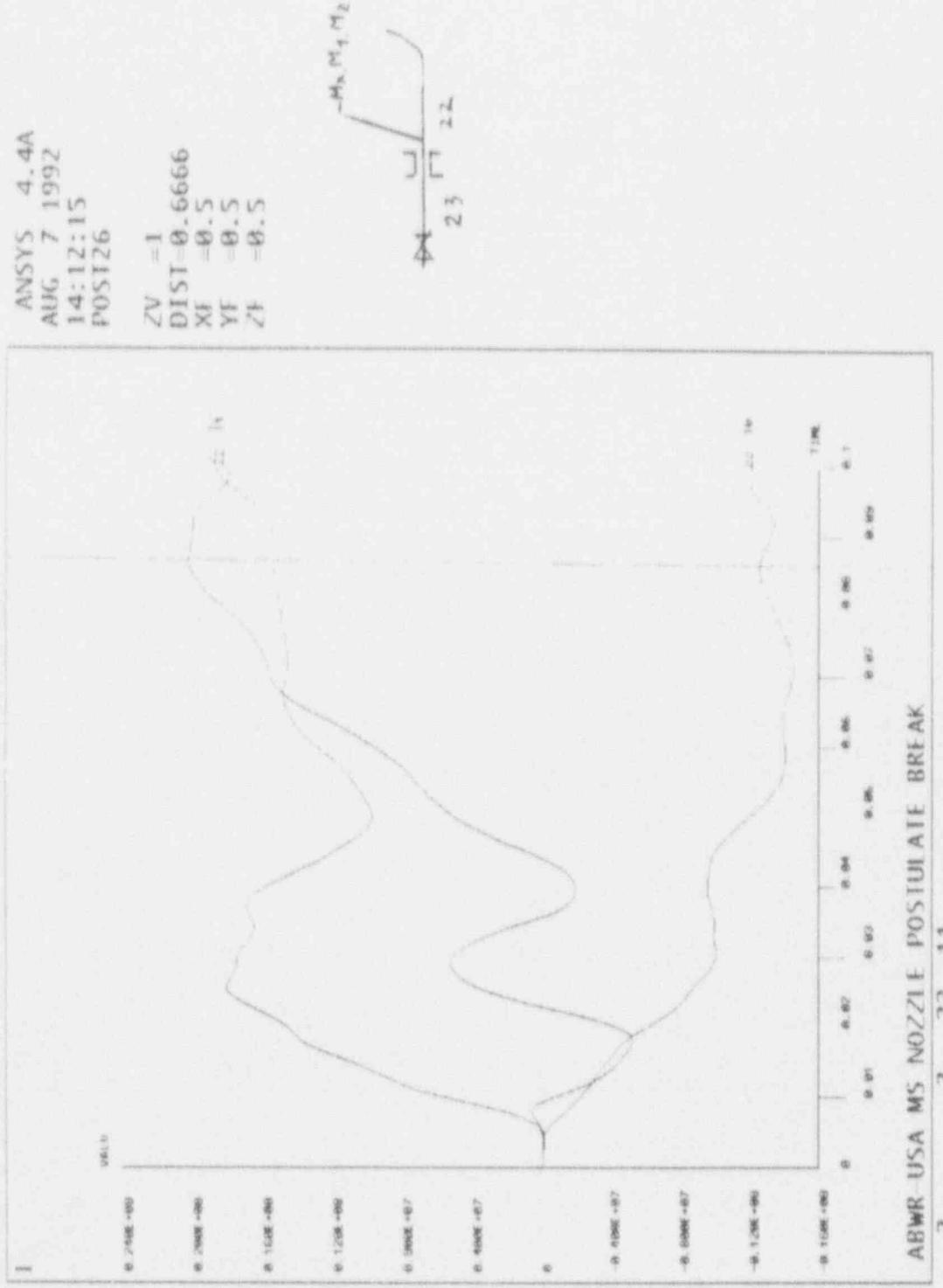
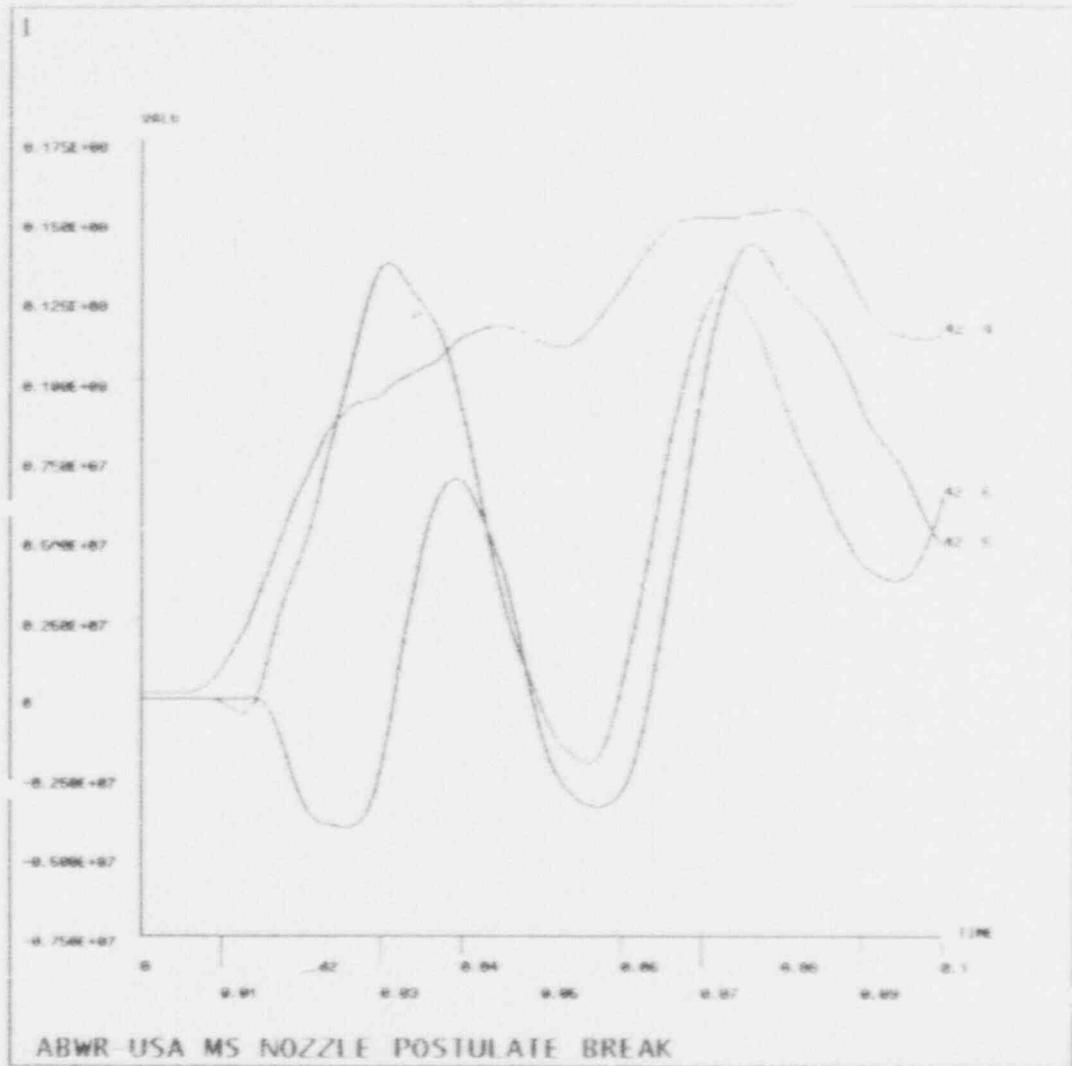


Figure 7 : Bending moment time histories. DT=0.001 sec
at elm 22J , before main steam guide



ANSYS 4.4A
AUG 7 1992
14:16:59
POST26

ZV =1
DIST=0.6666
XF =0.5
YF =0.5
ZF =0.5

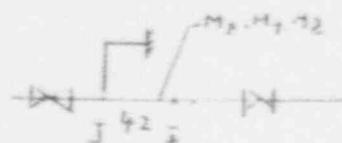


Figure 8 : Bending moment time histories. DT=0.001 sec
at elm 42I ,near headfitting

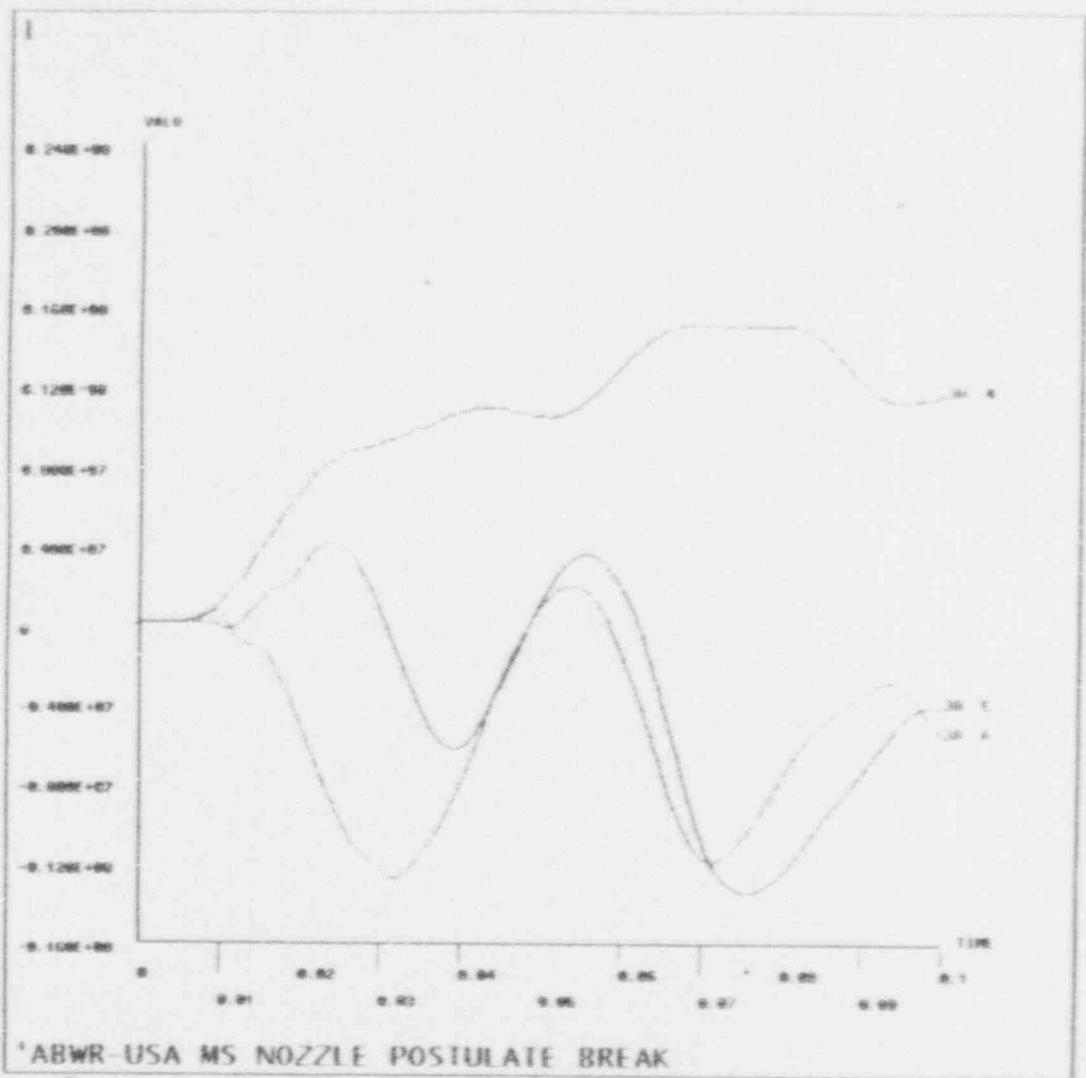
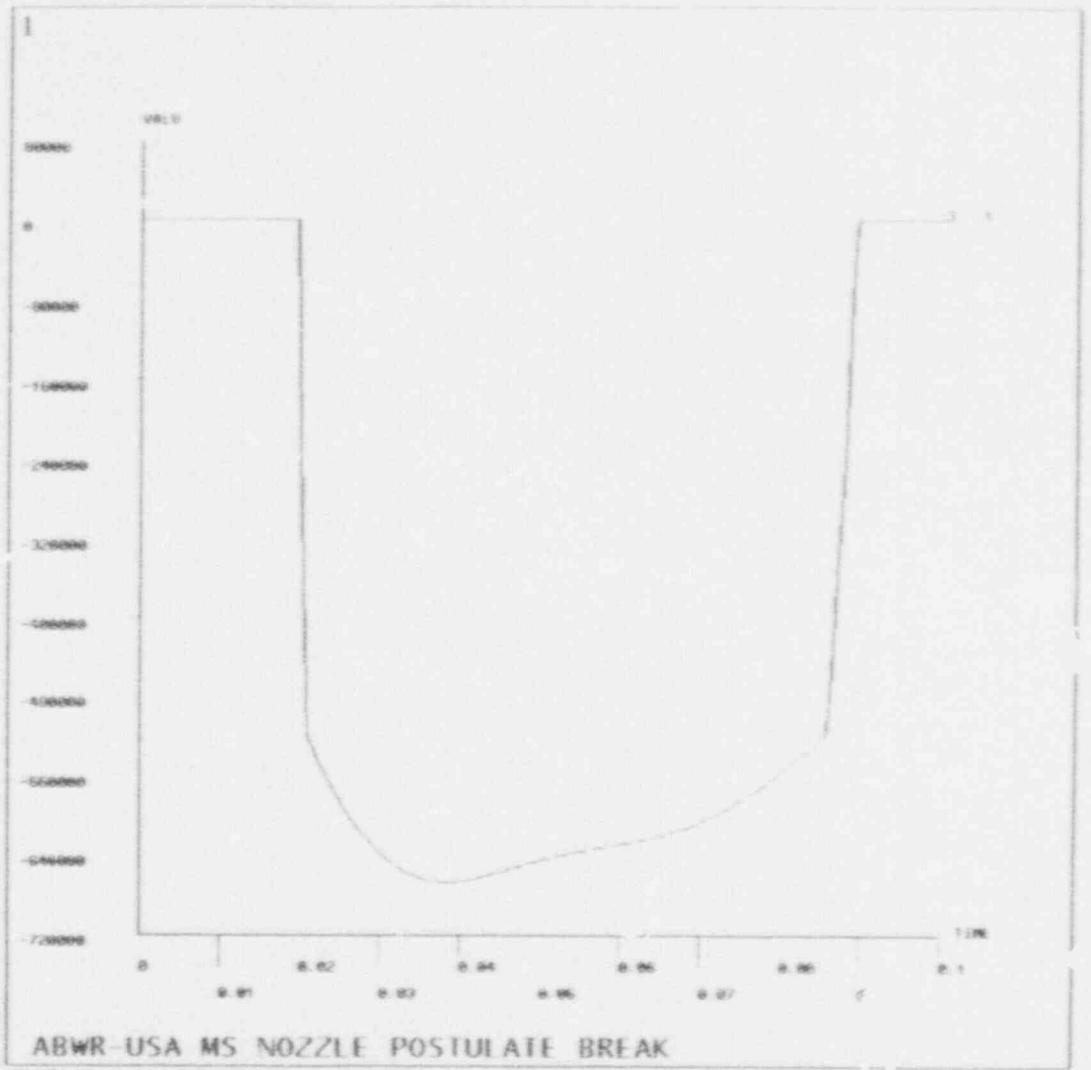


Figure 9 : Bending moment time histories. DT=0.001 sec.
at Elm 38I, 1st elm after MSIV.

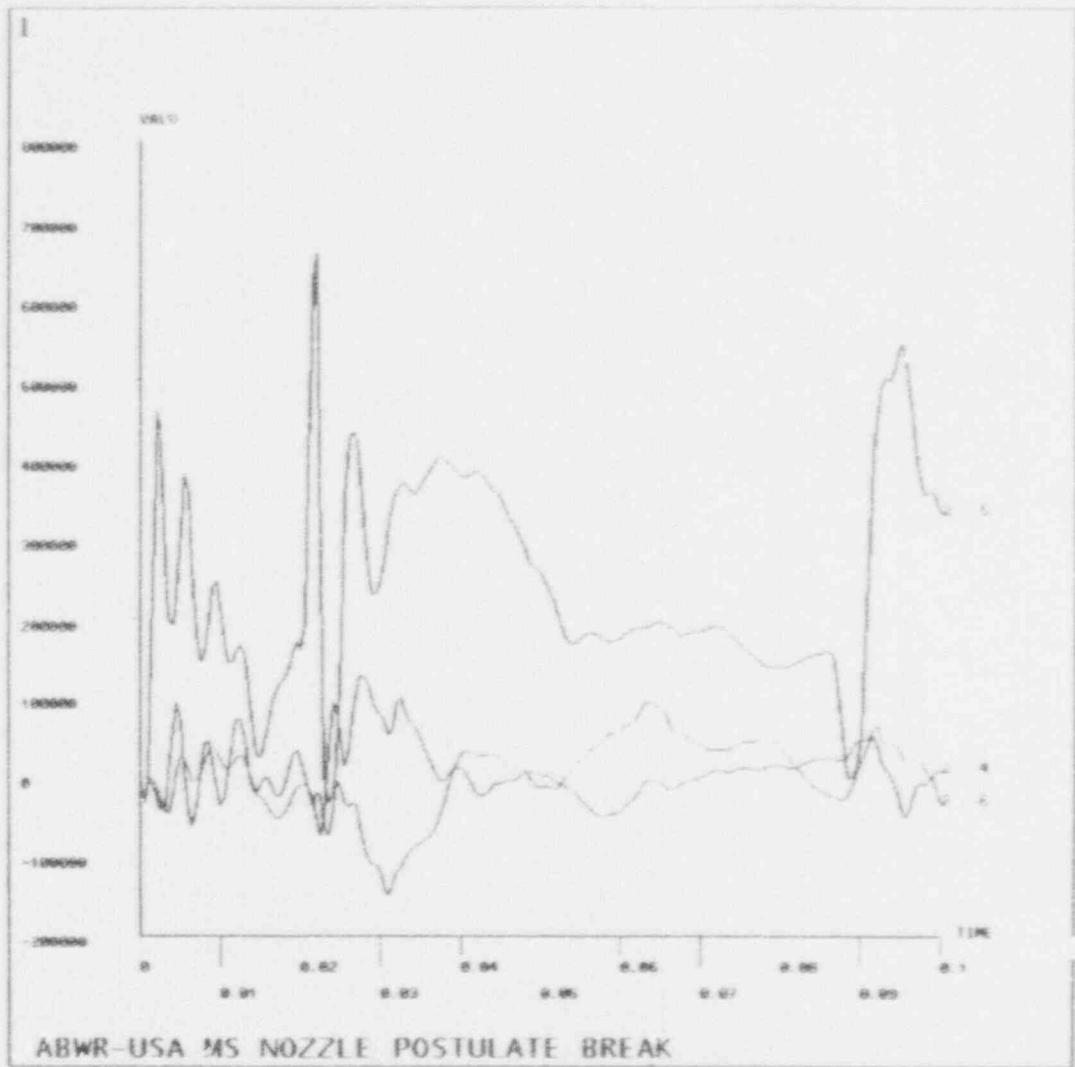


ANSYS 4.4A
AUG 19 1992
11:14:48
POST26

ZV =1
DIST=0.6666
XF =0.5
YF =0.5
ZF =0.5

dt: 0.0005 sec

Figure 2A: Impact force at the pipe whip restraint. DT=0.0005 sec
(pa=373,600 lb, max impact=670,000 lb)



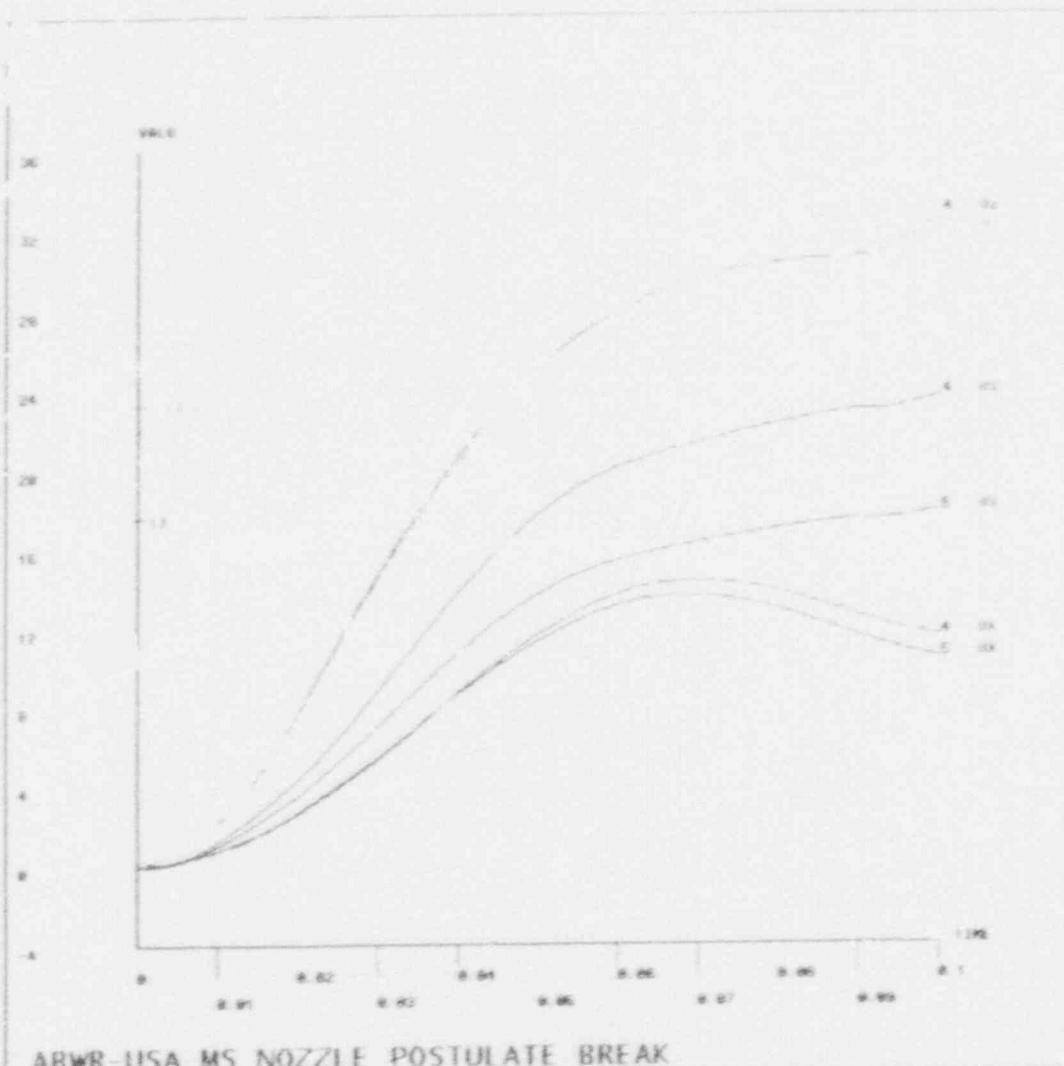
POST26-INP=

Figure 3A: Bending moment time histories. DT=0.0005 sec.
at elm. 2I ,at elbow near break

dt = 0.0005 sec

ANSYS 4.4A
AUG 28 1997
10:28:36
POST26

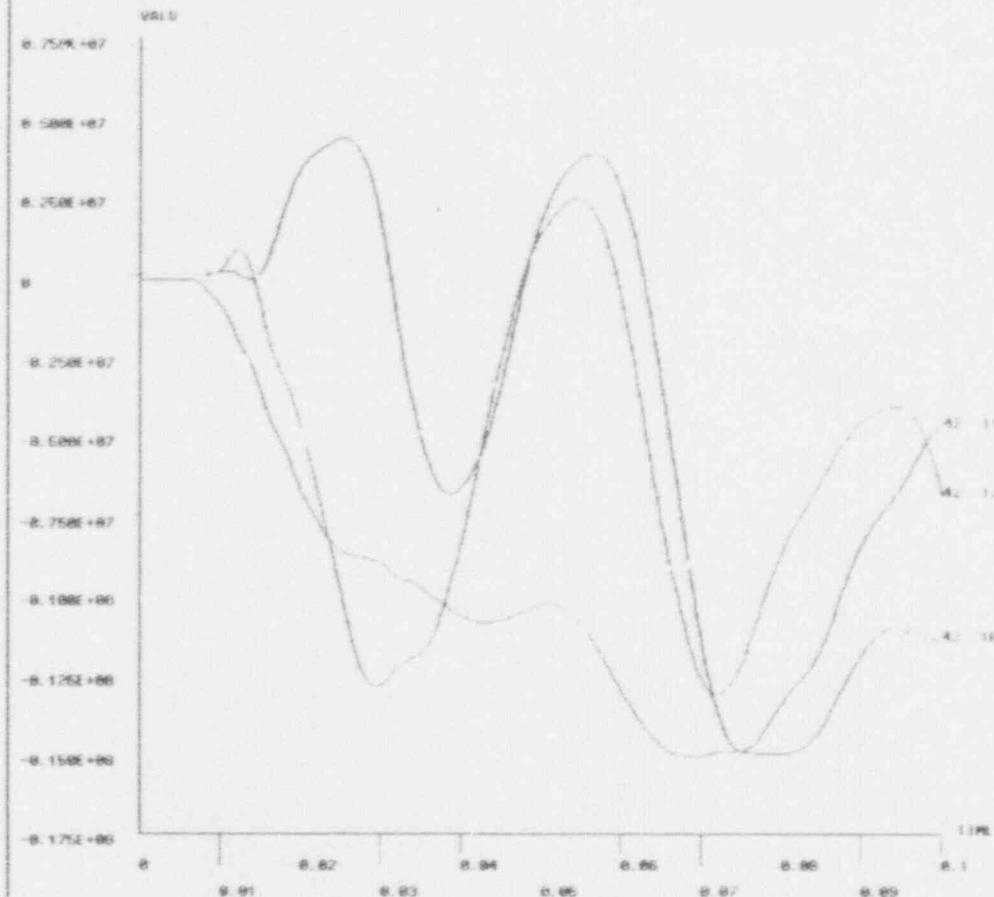
ZV =1
DIST=0.6666
XF =0.5
YF =0.5
ZF =0.5



5 6 5 UY
6 7 5 UZ
POST26-INP=

Figure 4A: Displacement time histories. DT=0.0005 sec
at the break location

1



ANSYS 4.4A
AUG 19 1992
11:30:56
POST26

ZV = 1
DIST=0.6666
XF = 0.5
YF = 0.5
ZF = 0.5

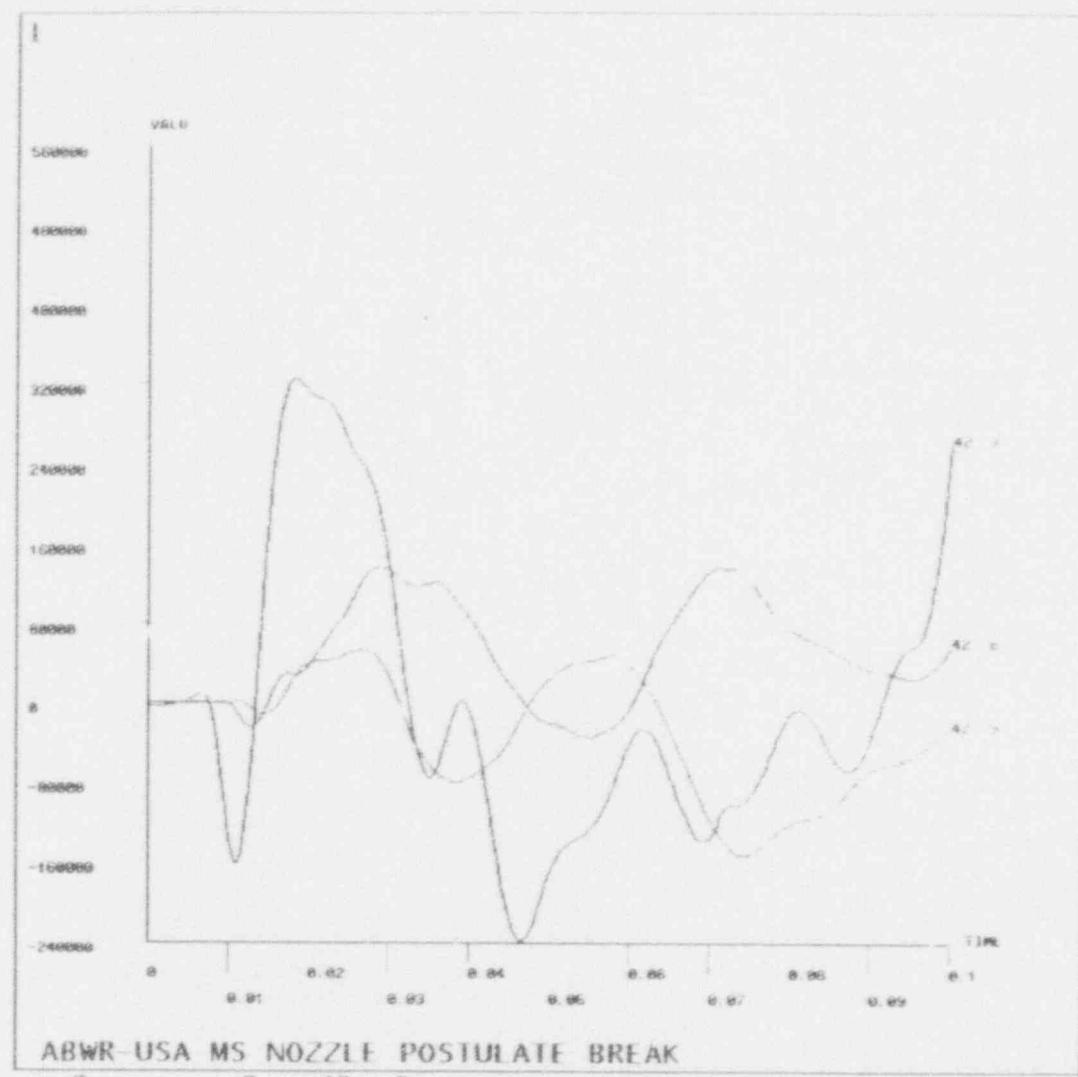
ABWR-USA MS NOZZLE POSTULATE BREAK

2	3	42	11
3	4	42	12

POST26-INP=

Figure 5A: Moment time history at headfitting, (Elm 42J)
DT=0.0005 sec.

$\Delta t = 0.0005 \text{ sec}$

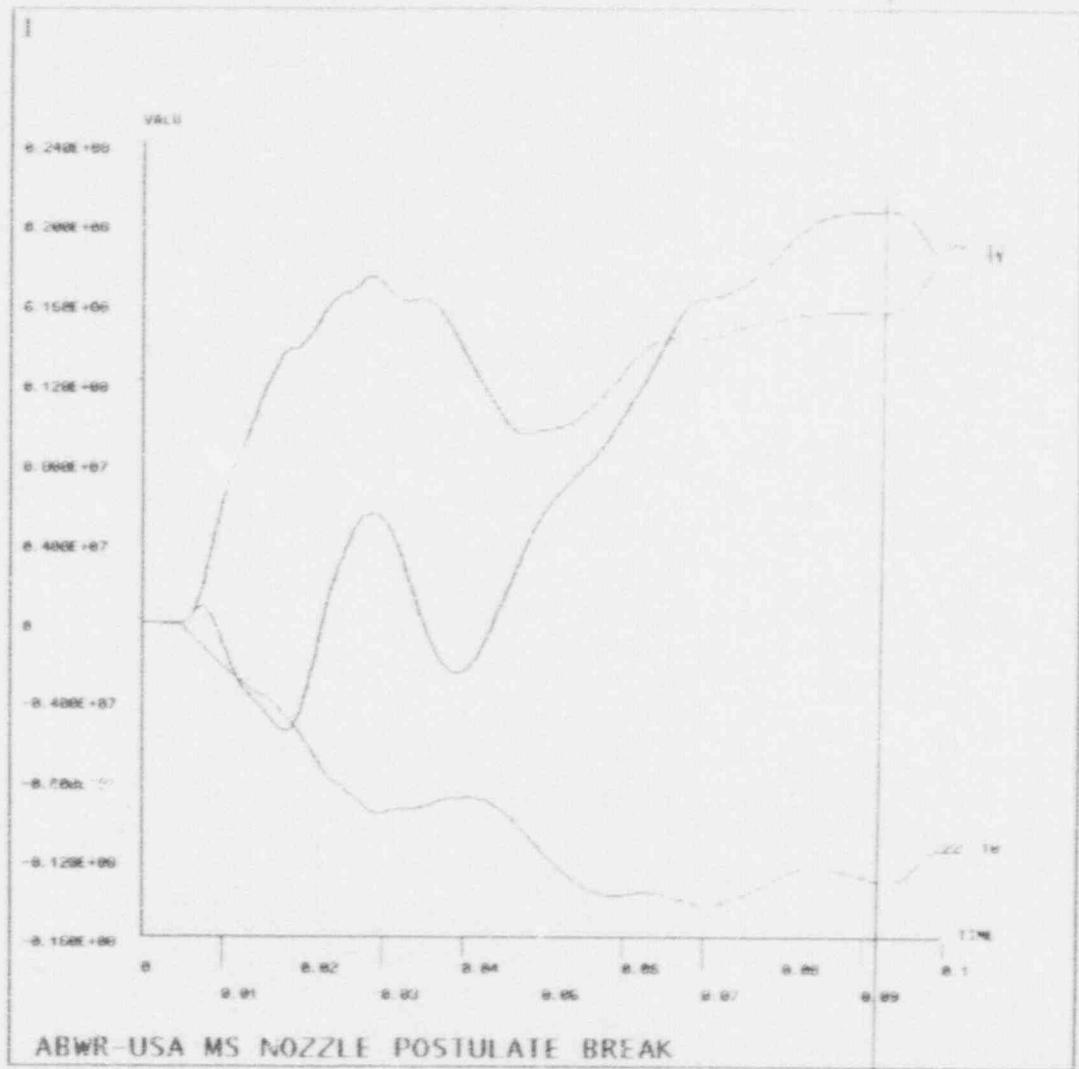


ABWR-USA MS NOZZLE POSTULATE BREAK

2	3	42	8
3	4	42	9

POST26-INP-

Figure 6A: Force time histories at headfitting. (Elm 42J)
 DT=0.0005 sec

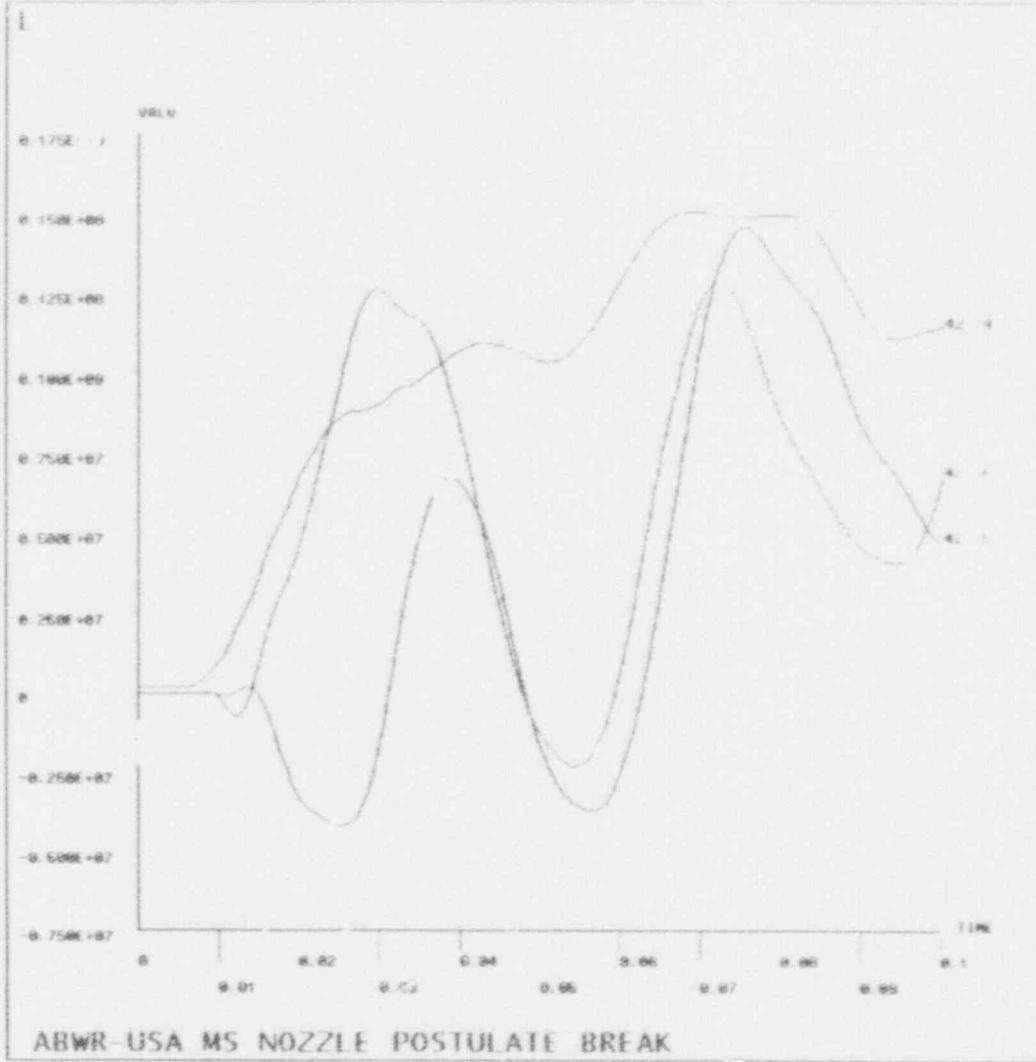


ANSYS 4.4A
AUG 19 1992
11:25:14
POST26

ZV = 1
DIST=0.6666
XF = 0.5
YF = 0.5
ZF = 0.5

$\Delta t = 0.0005 \text{ sec}$

Figure 7A: Bending moment time histories. $\Delta t=0.0005 \text{ sec}$
at elm 22J ,before main steam guide



ANSYS 4.4A
AUG 19 1992
11:28:39
POST26

ZV =1
DIST=0.6666
XF =0.5
YF =0.5
ZF =0.5

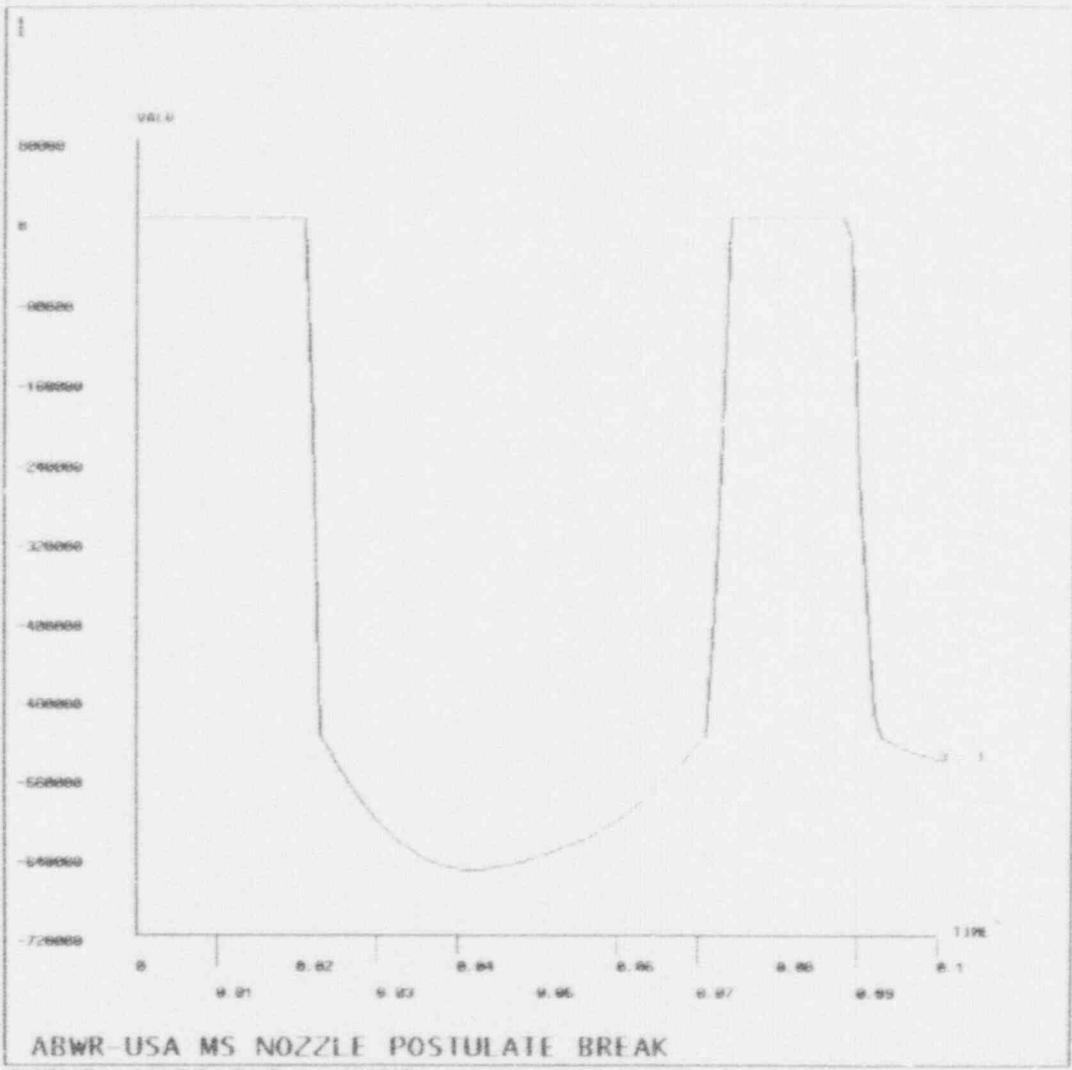
ABWR-USA MS NOZZLE POSTULATE BREAK

2	3	42	5
3	4	42	6

POST26-INP=

Figure 8A: Bending moment time histories. DT=0.0005 sec
at elm 42I ,near headfitting

Δt = 0.0005 sec



ANSYS 4.4A
AUG 28 1992
13:54:08
POST26

ZV =1
DIST=0.6666
XF =0.5
YF =0.5
ZF =0.5

Figure 2B: Impact force at the pipe whip restraint.
($\rho_a=373,600$ lb, max impact=670,000 lb)
(Included rotated blowdown angle)

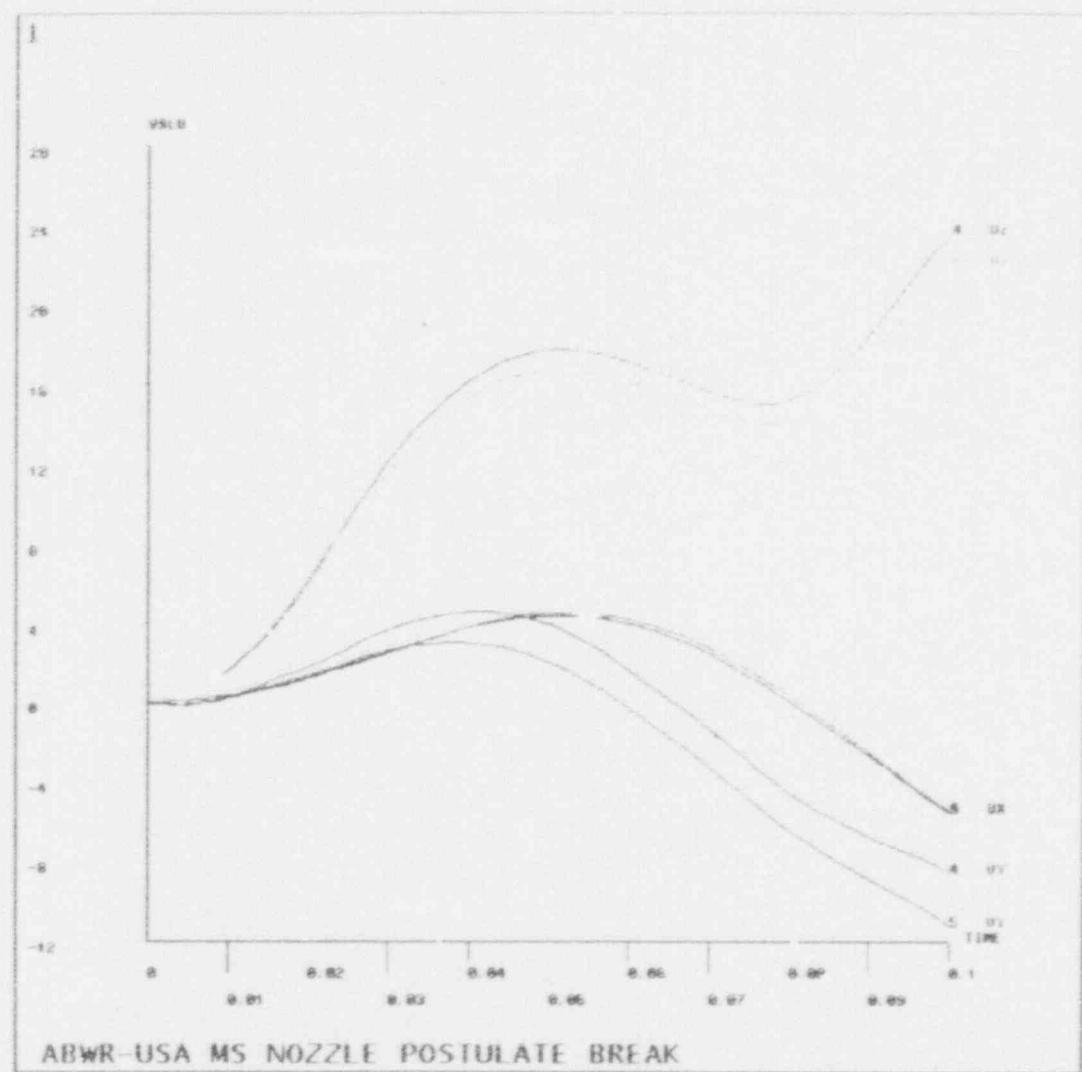
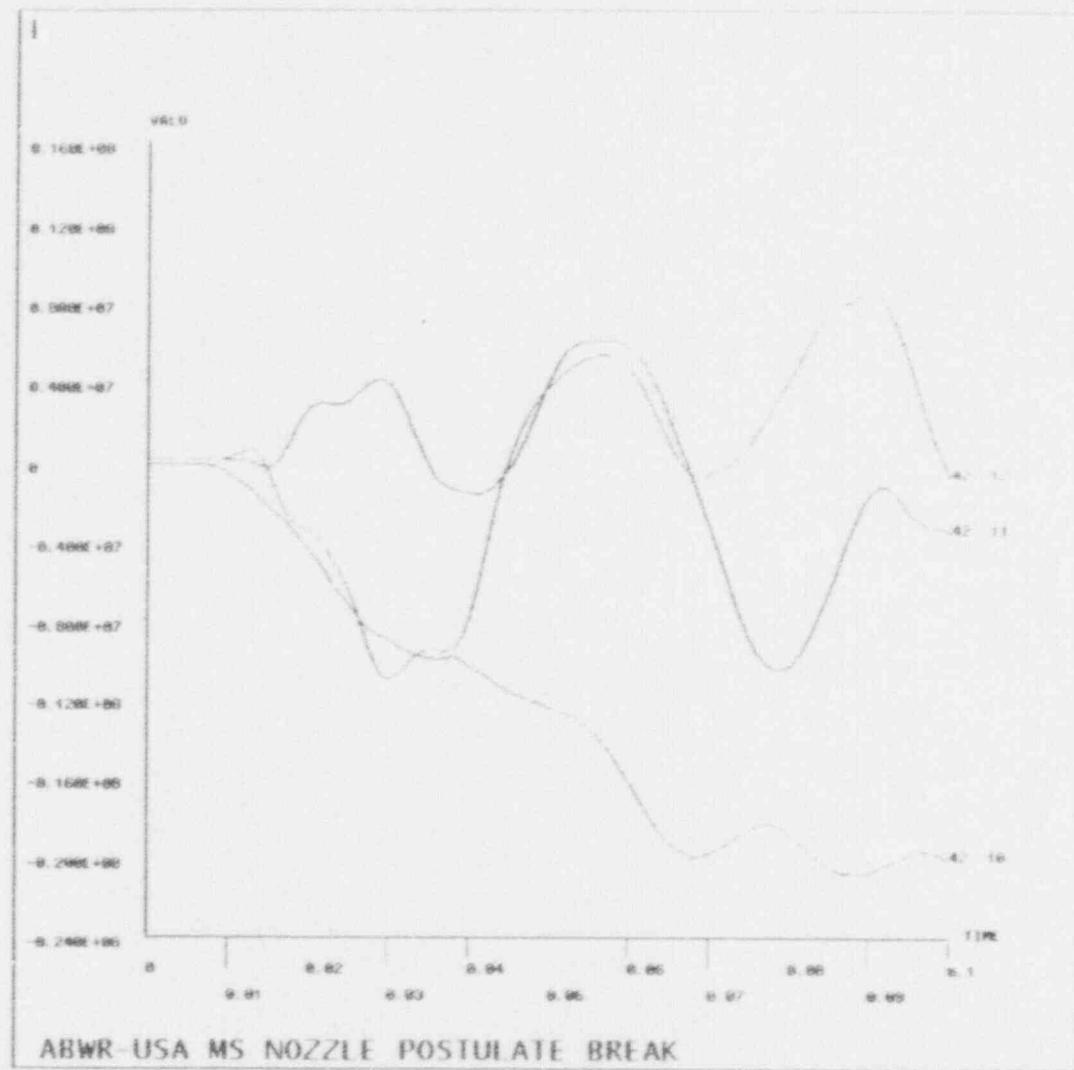
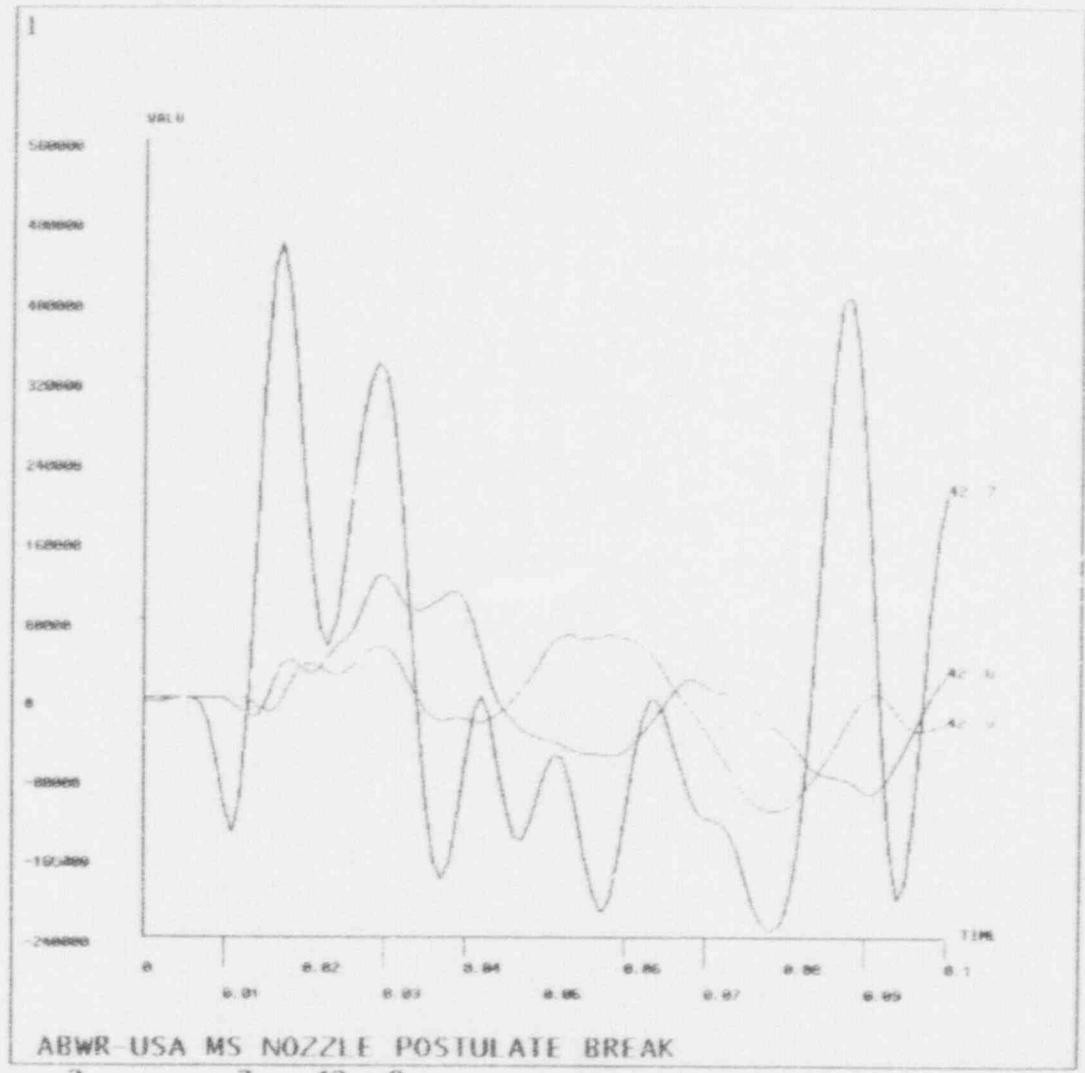


Figure 4B: Displacement time histories.
at the break location
(Included rotated blowdown angle)



POST26 INP-

Figure 5B: Moment time history at headfitting, (Elm 42J)
(Included rotated blowdown angle)

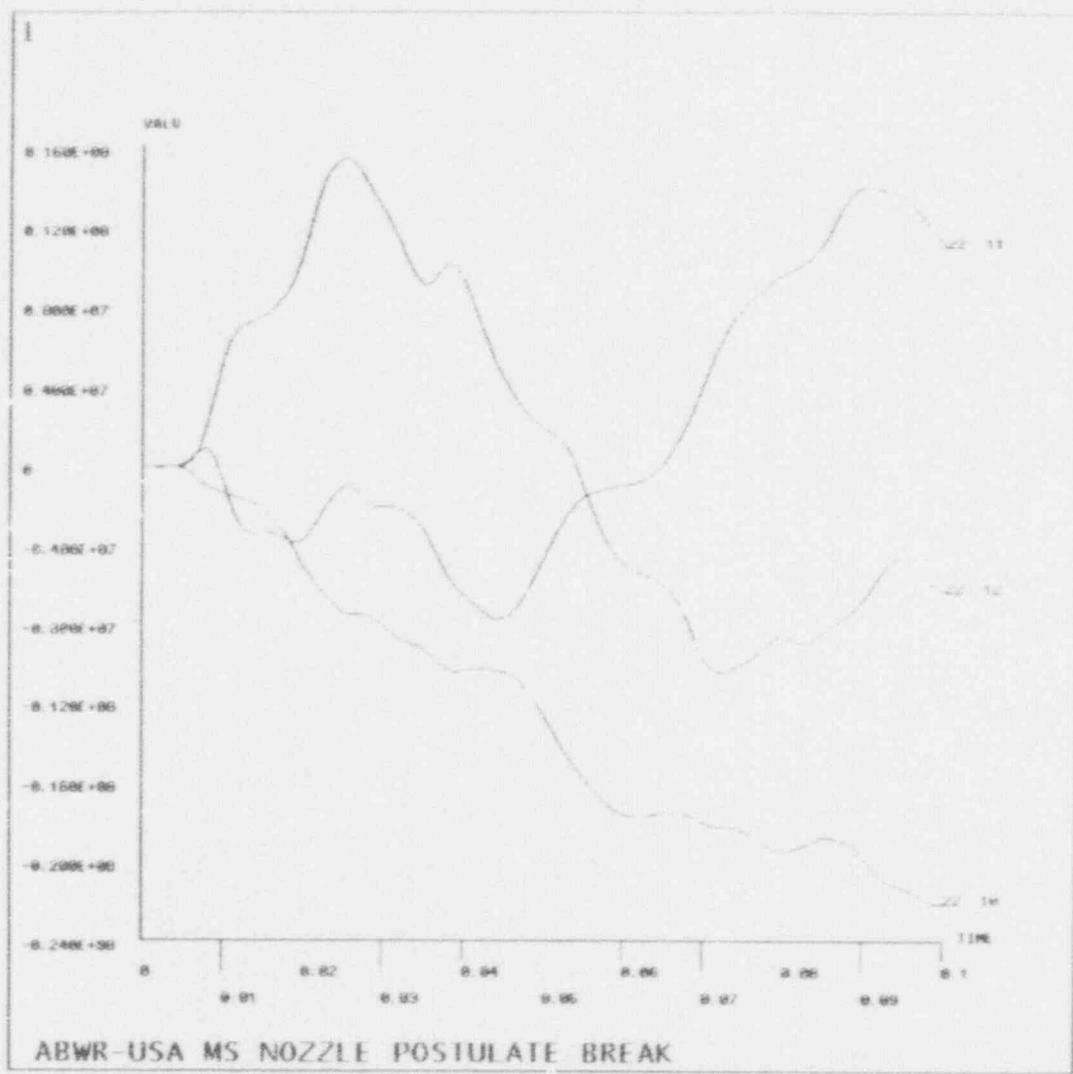


ANSYS 4.4A
AUG 28 1992
14:01:56
POST26

ZV =1
DIST=0.6666
XF =0.5
YF =0.5
ZF =0.5

POST26-TNP=

Figure 6B: Force time histories at headfitting. (Elm 42J)
(Included rotated blowdown angle)

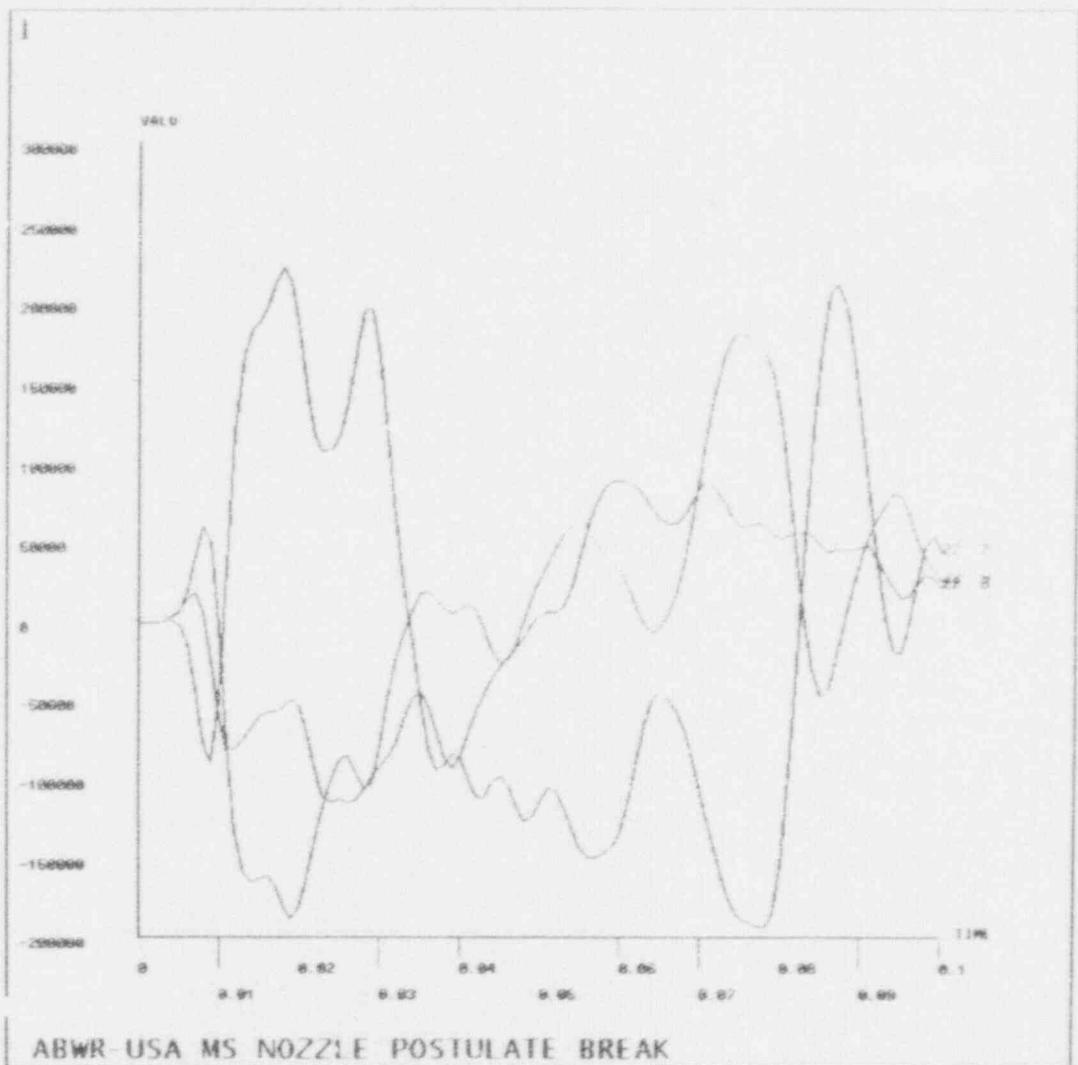


ANSYS 4.4A
AUG 28 1992
14:03:53
POST26

ZV =1
DIST = 0.6666
XF = -0.5
YF = 0.5
ZF = -0.5

Figure 7B: Bending moment time histories. DT=0.001 sec
at elm 22J , before main steam guide
(Included rotated blowdown angle)

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ABWR-USA MS NOZZLE POSTULATE BREAK

2	3	22	8
3	4	22	9

POST26-INP=

Figure 9B: Force time histories.
 at elm 22J ,before main steam guide
 (Included rotated blowdown angle)

/PREP7

/TITLE ABWR-USA HS NOZZLE POSTULATE BREAK

KAN.

KNL

1

ALPHAD

2 464

BETA

0 00009

KAY

4 0

KAY

5 2

KAY

6 1

TREF

70 0

/COM COORDINATE SYSTEMS

CSYS 0

/COM NODE DEFINITIONS

/COM

NODE

DEFINITIONS

N	1	48 13	611 97	148 13
N	2	58 09	611 97	178 79
N	3	61 79	611 97	190 17
N	4	69 75	611 97	214 66
N	5	73 94	611 97	227 56
N	6	73 94	555 97	227 56
N	7	91 24	555 97	280 82
N	8	91 24	517 01	280 82
N	9	91 24	494 35	280 82
N	10	91 24	494 35	280 82
N	11	130 80	494 36	267 97
N	12	130 80	452 35	267 97
N	13	130 80	452 35	267 97
N	14	131 19	452 35	267 84
N	15	143 66	452 22	263 79
N	16	152 57	452 13	260 89
N	17	159 00	452 06	258 79
N	18	165 11	452 00	255 97
N	19	188 44	451 71	241 41
N	20	207 51	451 42	221 64
N	21	214 23	451 29	209 99
N	22	219 96	451 18	201 73
N	23	231 83	450 94	181 13
N	24	243 66	450 71	160 67
N	25	255 46	450 47	140 22
N	26	269 73	450 18	115 50
N	27	288 44	449 81	83 10
N	28	336 93	449 33	83 10
N	29	336 93	449 16	55 12
N	30	354 33	448 99	55 12
N	31	385 83	448 67	55 12
N	32	424 05	448 29	55 12
N	33	473 05	447 80	55 12
N	34	496 05	447 57	55 12
N	35	451 48	463 37	55 12
N	36	432 07	489 61	55 12
N	37	424 94	496 89	55 12
N	38	411 71	513 39	55 12
N	39	408 88	513 27	55 12
N	40	387 29	535 30	55 12
N	41	439 72	511 39	55 12
N	42	437 88	513 27	55 12
N	43	426 85	524 52	55 12
N	44	423 67	527 66	55 12
N	45	544 52	447 09	55 12
N	46	568 18	446 85	55 12
N	47	700 37	445 53	55 12
N	48	706 08	445 47	55 12
N	49	708 25	445 45	55 12
N	50	708 25	445 45	55 12

N.	62.	647	27.	446	06.	55	16.
N.	63.	91.	24.	561	97.	280	82.
N.	66.	58.	13.	611	97.	148	37.
N.	67.	48.	13.	621	97.	148	37.
N.	68.	48.	13.	611	97.	158	37.
N.	69.	657	27.	446	06.	55	12.
N.	70.	647	27.	456	06.	55	12.
N.	71.	647	27.	446	06.	65	12.
N.	72.	190.	43.	470	87.	184	69.
N.	76.	229.	25.	415	04.	152	36.
N.	80.	354.	33.	458	93.	55	12.
N.	81.	354.	33.	448	99.	55	12.
N.	82.	100.	36.	555	97.	308	90.
/COM N.	83.	117.	96.	451.	71.	154.	37.
/COM						0 00000.	72 00.

/COM /COM REAL CONSTANT TABLES FOR PIPE

R.	1.	28	0.	1	41.	66	0
R.	2.	28	0.	1	41.	42	0
R.	3.	28	0.	1	41.	312	0
R.	4.	28	0.	1	41.	312	0
R.	5.	25	60.	2	41.		
R.	6.	27	39.	2	41.		
R.	7.	12	00.	0	90.		
R.	8.	6	35.	0	09.		
R.	9.	3	35.	0	03.		
R.	10.	J.	28	0.	00.		
R.	11.	48	0.	3	00.		
R.	12.	48	0.	1	58.		
R.	13.	3.	14.	0	100.		
R.	14.	0	0	4	54.	10.	4 7.
RHORE.	5.	0.	516340.	20	0.	1197549.	254000.
/COM							

/COM MATERIAL PROPERTY TABLE

EX.	1.	300008000.					
ALPX.	1.	6.07E-06					
NUXY.	1.	0.3					
DENS.	1.	0.000733					
/COM							
NLSIZE							
NL.	1.	1					
NL.	1.	7					
NL.	1.	13.	18				
NL.	1.	14.	0.00097.	0	01.	0.05.	0.10.
NL.	1.	19.	100.	27100.	32565.	44931.	51612.
NL.	1.	25.	200.	27100.	32565.	44931.	51612.
NL.	1.	31.	300.	27100.	32565.	44931.	51612.
NL.	1.	37.	400.	27100.	32565.	44931.	51612.
NL.	1.	43.	500.	27100.	32565.	44931.	51612.
NL.	2.	7					
NL.	2.	13.	18				
NL.	2.	14.	0.4543.	0.47000.	0.5000.	0.7000.	2 000.
/COM							
EX.	2.	200000.					
ALPX.	2.	6.07E-06					
NUXY.	2.	0.3					
DENS.	2.	0.000733					
NL.	2.	1					
NL.	2.	13.	18				
NL.	2.	14.	0.4543.	0.47000.	0.5000.	0.7000.	2 000.
NL.	2.	19.	100.	254000.	516343.	775625.	1197549.
NL.	2.	25.	200.	254000.	516343.	775625.	1197549.
/COM							

/COM HA NOZZLE PIPE WHIP WESTRAIN

/COM							
EX.	2.	200000.					
ALPX.	2.	6.07E-06					
NUXY.	2.	0.3					
DENS.	2.	0.000733					
NL.	2.	1					
NL.	2.	7					
NL.	2.	13.	18				
NL.	2.	14.	0.4543.	0.47000.	0.5000.	0.7000.	2 000.
NL.	2.	19.	100.	254000.	516343.	775625.	1197549.
NL.	2.	25.	200.	254000.	516343.	775625.	1197549.
/COM							

NL, 2, 31, 300, 501.0, 254000, 516343, 775625, 1197549
NL, 2, 37, 400, 501.0, 254000, 516343, 775625, 1197549
NL, 2, 43, 500, 501.0, 254000, 516343, 775625, 1197549
/COM
/COM 1" LONG NL, 2, 14, 4.5430, 4.5698, 5.0000, 7.0000, 20.000
/COM ELEMENT TYPE TABLE
/COM
/COM PLASTIC PIPE
ET, 1, 20, 0, 0, 0, 0, 0, 1
/COM PLASTIC ELBOW
ET, 2, 60, 0, 0, 0, 0, 0, 1
/COM HOR SPRING ELEMENT
ET, 3, 14, 0, 0, 0, 0, 0, 1
/COM VERTICL SPRING
ET, 4, 14, 0, 0, 0, 0, 0, 3
ET, 5, 39, 0, 0, 1, 0, 0
/COM
/COM ELEMENT DEFINITION
/COM
TYPE, 1 \$ REAL, 1 \$ MAT, 1
E, 4, 5
TYPE, 2 \$ REAL, 2 \$ MAT, 1
E, 5, 6, 7
/COM
/COM PIPE WHIP
/COM
TYPE, 5 \$ REAL, 14 \$ MAT, 1
E, 6, 82
TYPE, 1 \$ REAL, 1 \$ MAT, 1
E, 6, 10
E, 10, 12
TYPE, 2 \$ REAL, 3 \$ MAT, 1
E, 12, 13, 11
TYPE, 1 \$ REAL, 1 \$ MAT, 1
E, 13, 14
E, 14, 15
E, 15, 16
TYPE, 1 \$ REAL, 4 \$ MAT, 1
E, 16, 17
TYPE, 1 \$ REAL, 1 \$ MAT, 1
E, 17, 18
TYPE, 1 \$ REAL, 4 \$ MAT, 1
E, 18, 19
TYPE, 1 \$ REAL, 1 \$ MAT, 1
E, 19, 26
E, 26, 27
E, 27, 35
E, 35, 36
E, 36, 37
E, 37, 38
E, 38, 39
E, 39, 40
TYPE, 2 \$ REAL, 2 \$ MAT, 1
E, 40, 41, 64
TYPE, 1 \$ REAL, 1 \$ MAT, 1
E, 41, 42
E, 42, 43
E, 43, 44
TYPE, 1 \$ REAL, 10 \$ MAT, 1
E, 44, 45
E, 45, 56
E, 45, 46
E, 46, 47
TYPE, 1 \$ REAL, 7 \$ MAT, 1
E, 47, 48

39, FX, 0
43, FX, 0
WRITE
COM
ITER, 1, 1, 1
TIME, 00200
62, UX, 0, 0, ..., UY, UZ, ROTX, ROTY, ROTZ
82, UX, 0, 0, ..., UY, UZ, ROTX, ROTY, ROTZ
42, UY, 0, 0, ..., UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, 76511
16, FX, 0
16, FZ, 0
39, FX, 0
39, FZ, 0
43, FX, 0
43, FX, 0.
WRITE
COM
ITER, 1, 1, 1
TIME, 00300
62, UX, 0, 0, ..., UY, UZ, ROTX, ROTY, ROTZ
82, UX, 0, 0, ..., UY, UZ, ROTX, ROTY, ROTZ
42, UY, 0, 0, ..., UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, 145739
16, FX, 0
16, FZ, 0
39, FX, 0
39, FZ, 0
43, FX, 0
43, FX, 0.
WRITE
COM
ITER, 1, 1, 1
TIME, 00400
62, UX, 0, 0, ..., UY, UZ, ROTX, ROTY, ROTZ
82, UX, 0, 0, ..., UY, UZ, ROTX, ROTY, ROTZ
42, UY, 0, 0, ..., UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, 183502
16, FX, -16
16, FZ, 5
39, FX, 0
39, FZ, 0
43, FX, 0
43, FX, 0.
WRITE
COM
ITER, 1, 1, 1
TIME, 00500
62, UX, 0, 0, ..., UY, UZ, ROTX, ROTY, ROTZ
82, UX, 0, 0, ..., UY, UZ, ROTX, ROTY, ROTZ
42, UY, 0, 0, ..., UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, 201414
16, FX, -373
16, FZ, 121
39, FX, -5
39, FZ, 8
43, FX, 0.
WRITE
COM
ITER, 1, 1, 1

```

TIME, 00600
D.62, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.82, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.42, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FX, 26620
F, 16, FX, -2784
F, 16, FZ, 905
F, 39, FX, -95
F, 39, FZ, 165
F, 43, FX, 0
LWRITE
/COM
ITER, 1, 1, 1
TIME, 00700
D.62, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.82, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.42, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FX, 203183
F, 16, FX, -10030
F, 16, FZ, 3259
F, 39, FX, -734
F, 39, FZ, 1272
F, 43, FX, 0
LWRITE
/COM
ITER, 1, 1, 1
TIME, 00800
D.62, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.82, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.42, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FX, 188073
F, 16, FX, -22111
F, 16, FZ, 7181
F, 39, FX, -3064
F, 39, FZ, 5306
F, 43, FX, 0
LWRITE
/COM
ITER, 1, 1, 1
TIME, 00900
D.62, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.82, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.42, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FX, 165330
F, 16, FX, -34687
F, 16, FZ, 11271
F, 39, FX, -8346
F, 39, FZ, 14455
F, 43, FX, 0
LWRITE
/COM
ITER, 1, 1, 1
TIME, 01000
D.62, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.82, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
D.42, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
F, 5, FX, 115440

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F, 5,FZ, 355287
F, 12,FY, 140033
F, 16,FX, -43144
F, 16,FZ, 14018
F, 39,FX, -16812
F, 39,FZ, 29119
F, 43,FX, -10
LWRITE
/COM
ITER,1,1,1
TIME, 01100
D,62,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
D,82,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
D,42,UY,0,0,,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F, 12,FY, 115895
F, 16,FX, -46053
F, 16,FZ, 14963
F, 39,FX, -27391
F, 39,FZ, 47440
F, 43,FX, -77
LWRITE
/COM
ITER,1,1,1
TIME, 01200
D,62,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
D,82,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
D,42,UY,0,0,,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F, 12,FY, 94879
F, 16,FX, -44620
F, 16,FZ, 14498
F, 39,FX, -38466
F, 39,FZ, 66623
F, 43,FX, -392
LWRITE
/COM
ITER,1,1,1
TIME, 01300
D,62,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
D,82,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
D,42,UY,0,0,,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F, 12,FY, 77454
F, 16, , -40760
F, 16, , 13244
F, 39, , -48601
F, 39,FZ, 84178
F, 43,FX, -1429
LWRITE
/COM
ITER,1,1,1
TIME, 01400
D,62,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
D,82,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
D,42,UY,0,0,,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F, 12,FY, 63358
F, 16,FX, -35979
F, 16,FZ, 11690
F, 39,FX, -56752

39, FZ, 98295
43, FX, -4006

WRITE

COM

ITER, 1, 1, 1

TIME, 01500
0, 62, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
0, 82, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
0, 42, UY, 0, 0, ., ., UZ
. 5, FX, 115440
. 5, FZ, 355287
. 12, FY, 52074
. 16, FX, -31166
. 16, FZ, 10126
. 39, FX, -62255
. 39, FZ, 107826
. 43, FX, -9031

WRITE

COM

ITER, 1, 1, 1

TIME, 01600
0, 62, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
0, 82, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
0, 42, UY, 0, 0, ., ., UZ
. 5, FX, 115440
. 5, FZ, 355287
. 12, FY, 43061
. 16, FX, -26745
. 16, FZ, 8690
. 39, FX, -64866
. 39, FZ, 112348
. 43, FX, -17024

WRITE

COM

ITER, 1, 1, 1

TIME, 01700
0, 62, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
0, 82, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
0, 42, UY, 0, 0, ., ., UZ
. 5, FX, 115440
. 5, FZ, 355287
. 12, FY, 35844
. 16, FX, -22870
. 16, FZ, 7431
. 39, FX, -64781
. 39, FZ, 112200
. 43, FX, -27717

WRITE

COM

ITER, 1, 1, 1

TIME, 01800
0, 62, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
0, 82, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
0, 42, UY, 0, 0, ., ., UZ
. 5, FX, 115440
. 5, FZ, 355287
. 12, FY, 30037
. 16, FX, -19557
. 16, FZ, 6354
. 39, FX, -62539
. 39, FZ, 108318
. 43, FX, -40041

WRITE

COM

ITER, 1, 1, 1

```

TIME 01900
0.62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
0.42, UX, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 25335
F, 16, FX, -16755
F, 16, FZ, 5444
F, 39, FX, -588828
F, 39, FZ, 101890
F, 43, FX, -52464
LWRITE
/COM
ITER, 1, 1, 1 02000
TIME 02100
0.62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
0.42, UX, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 21500
F, 16, FX, -14402
F, 16, FZ, 4679
F, 39, FX, -54297
F, 39, FZ, 94043
F, 43, FX, -63463
LWRITE
/COM
ITER, 1, 1, 1 02100
TIME 02200
0.62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
0.42, UX, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 18349
F, 16, FX, -12426
F, 16, FZ, 4037
F, 39, FX, -49456
F, 39, FZ, 85658
F, 43, FX, -71918
LWRITE
/COM
ITER, 1, 1, 1 02300
TIME 02300
0.62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
0.42, UX, 0, 0, ., UZ

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F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 13572
F, 16, FX, -9367
F, 16, FZ, 3043
F, 39, FX, -40102
F, 39, FZ, 69457
F, 43, FX, -79679
LWRITE
/COM
ITER, 1, 1, 1
TIME, 02400
D, 62, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
D, 82, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
D, 42, UY, 0, 0, ., ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 11750
F, 16, FX, -8183
F, 16, FZ, 2659
F, 39, FX, -35907
F, 39, FZ, 62191
F, 43, FX, -79475
LWRITE
/COM
ITER, 1, 1, 1
TIME, 02500
D, 62, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
D, 82, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
D, 42, UY, 0, 0, ., ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 10213
F, 16, FX, -7178
F, 16, FZ, 2332
F, 39, FX, -32110
F, 39, FZ, 55615
F, 43, FX, -77312
LWRITE
/COM
ITER, 1, 1, 1
TIME, 02600
D, 62, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
D, 82, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
D, 42, UY, 0, 0, ., ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 6908
F, 16, FX, -6322
F, 16, FZ, 2054
F, 39, FX, -28714
F, 39, FZ, 49732
F, 43, FX, -73813
LWRITE
/COM
ITER, 1, 1, 1
TIME, 02700
D, 62, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
D, 82, UX, 0, 0, ., ., UY, UZ, ROTX, ROTY, ROTZ
D, 42, UY, 0, 0, ., ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 7792
F, 16, FX, -5587
F, 16, FZ, 1815

F, 39, FX, -25695.
 F, 39, FZ, 44504.
 F, 43, FX, -69514.
 LWRITE
 /COM
 LITER, 1, 1, 1
 TIME, 0 02800
 D, 62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
 D, 82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
 D, 42, UX, 0, 0, ., UZ
 F, 5, FX, 115440.
 F, 5, FZ, 355287.
 F, 12, FY, 6834.
 F, 16, FX, -4955.
 F, 16, FZ, 1610.
 F, 39, FX, -23024.
 F, 39, FZ, 39878.
 F, 43, FX, -64829.
 LWRITE
 /COM
 LITER, 1, 1, 1
 TIME, 0 02900
 D, 62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
 D, 82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
 D, 42, UX, 0, 0, ., UZ
 F, 5, FX, 115440.
 F, 5, FZ, 355287.
 F, 12, FY, 6007.
 F, 16, FX, -4409.
 F, 16, FZ, 1432.
 F, 39, FX, -20666.
 F, 39, FZ, 35794.
 F, 43, FX, -60047.
 LWRITE
 /COM
 LITER, 1, 1, 1
 TIME, 0 03000
 D, 62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
 D, 82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
 D, 42, UX, 0, 0, ., UZ
 F, 5, FX, 115440.
 F, 5, FZ, 355287.
 F, 12, FY, 5290.
 F, 16, FX, -3934.
 F, 16, FZ, 1278.
 F, 39, FX, -18584.
 F, 39, FZ, 32188.
 F, 43, FX, -56363.
 LWRITE
 /COM
 LITER, 1, 1, 1
 TIME, 0 03100
 D, 62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
 D, 82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTZ
 D, 42, UX, 0, 0, ., UZ
 F, 5, FX, 115440.
 F, 5, FZ, 355287.
 F, 12, FY, 4664.
 F, 16, FX, -3521.
 F, 16, FZ, 1144.
 F, 39, FX, -16746.
 F, 39, FZ, 29005.
 F, 43, FX, -50891.
 LWRITE
 /COM

ITER, 1, 1, 1
TIME, 03200
D, 62, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 82, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 42, UY, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 4118
F, 16, FX, -3160
F, 16, FZ, 1027
F, 39, FX, -15122
F, 39, FZ, 26190
F, 43, FX, -46700
LWRITE
/COM
ITER, 1, 1, 1
TIME, 03300
D, 62, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 82, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 42, UY, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 3637
F, 16, FX, -2842
F, 16, FZ, 923
F, 39, FX, -13683
F, 39, FZ, 23699
F, 43, FX, -42818
LWRITE
/COM
ITER, 1, 1, 1
TIME, 03400
D, 62, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 82, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 42, UY, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 3213
F, 16, FX, -2563
F, 16, FZ, 833
F, 39, FX, -12407
F, 39, FZ, 21489
F, 43, FX, -39250
LWRITE
/COM
ITER, 1, 1, 1
TIME, 03500
D, 62, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 82, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 42, UY, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, 2838
F, 16, FX, -2314
F, 16, FZ, 752
F, 39, FX, -11273
F, 39, FZ, 19524
F, 43, FX, -35988
LWRITE
/COM
ITER, 1, 1, 1
TIME, 03600
D, 62, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 82, UX, 0, 0, ., UY, UZ, R_{OTX}, R_{OTY}, R_{OTZ}
D, 42, UY, 0, 0, ., UZ

, 5,FX, 115440
, 5,FZ, 355287
, 12,FY, 2504
, 16,FX, -2094
, 16,FZ, 680
, 39,FX, -10261
, 39,FZ, 17772
, 43,FX, -33018

LWRITE

/COM

IITER,1,1,1

TIME, 03700
D,62,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D,82,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D,42,UY,0.0.,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F,12,FY, 2207
F,16,FX, -1899
F,16,FZ, 617
F,39,FX, -9360
F,39,FZ, 16211
F,43,FX, -30318

LWRITE

/COM

IITER,1,1,1

TIME, 03800
D,62,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D,82,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D,42,UY,0.0.,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F,12,FY, 1941
F,16,FX, -1724
F,16,FZ, 560
F,39,FX, -8552
F,39,FZ, 14812
F,43,FX, -27867

LWRITE

/COM

IITER,1,1,1

TIME, 03900
D,62,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D,82,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D,42,UY,0.0.,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F,12,FY, 1703
F,16,FX, -1567
F,16,FZ, 509
F,39,FX, -7827
F,39,FZ, 13557
F,43,FX, -25646

LWRITE

/COM

IITER,1,1,1

TIME, 04000
D,62,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D,82,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D,42,UY,0.0.,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F,12,FY, 1489
F,16,FX, -1426
F,16,FZ, 463

```

F. 39, FX, -7176
F. 39, FZ, 12428
F. 43, FX, -23628
LWRITE
/COM
ITER, 1, 1, 1
TIME, 04100
0.62, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
D.42, UX, 0, 0, ,UZ, ROTX, ROTY, ROTZ
F. 5, FX, 115440
F. 5, FZ, 355287
F. 12, FY, 1296
F. 16, FX, -1300
F. 16, FZ, -422
F. 39, FX, 6589
F. 39, FZ, 11412
F. 43, FX, -21796
LWRITE
/COM
ITER, 1, 1, 1
TIME, 04200
0.62, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
D.42, UX, 0, 0, ,UZ, ROTX, ROTY, ROTZ
F. 5, FX, 115440
F. 5, FZ, 355287
F. 12, FY, 1122
F. 16, FX, -1185
F. 16, FZ, 385
F. 39, FX, -6059
F. 39, FZ, 10495
F. 43, FX, -20132
LWRITE
/COM
ITER, 1, 1, 1
TIME, 04300
0.62, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
D.42, UX, 0, 0, ,UZ, ROTX, ROTY, ROTZ
F. 5, FX, 115440
F. 5, FZ, 355287
F. 12, FY, 964
F. 16, FX, -1082
F. 16, FZ, 351
F. 39, FX, -5579
F. 39, FZ, 9664
F. 43, FX, -18617
LWRITE
/COM
ITER, 1, 1, 1
TIME, 04400
0.62, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
D.82, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
D.42, UX, 0, 0, ,UZ, ROTX, ROTY, ROTZ
F. 5, FX, 115440
F. 5, FZ, 355287
F. 12, FY, 820
F. 16, FX, -987
F. 16, FZ, 321
F. 39, FX, -5144
F. 39, FZ, 8910
F. 43, FX, -17241
LWRITE
/COM

```

TER, 1, 1, 1
TIME, 04500
0, 62, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 82, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 42, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, 690
16, FX, -902
16, FZ, 293
39, FX, -4749
39, FZ, 8225
43, FX, -15983
WRITE

COM

TER, 1, 1, 1
TIME, 04600
0, 62, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 82, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 42, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, 571
16, FX, -825
16, FZ, 268
39, FX, -4389
39, FZ, 7602
43, FX, -14836
WRITE

COM

TER, 1, 1, 1
TIME, 04700
0, 62, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 82, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 42, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, 463
16, FX, -754
16, FZ, 245
39, FX, -4061
39, FZ, 7033
43, FX, -13787
WRITE

COM

TER, 1, 1, 1
TIME, 04800
0, 62, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 82, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 42, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, 363
16, FX, -689
16, FZ, 224
39, FX, -3760
39, FZ, 6512
43, FX, -12830
WRITE

COM

TER, 1, 1, 1
TIME, 04900
0, 62, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 82, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ
0, 42, UX, 0, 0, UY, UZ, ROTX, ROTY, ROTZ

5,FX, 115440
5,FZ, 355287
12,FY, 273
16,FX, -629
16,FZ, 204
39,FX, -3485
39,FZ, 6137
43,FX, -11947
WRITE
COM
TER,1,1,1
IME, 05000
62,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
82,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
42,UY,0,0,,,UZ
5,FX, 115440
5,FZ, 355287
12,FY, 190
16,FX, -574
16,FZ, 187
39,FX, -3233
39,FZ, 5600
43,FX, -11141
WRITE
COM
TER,1,1,1
IME, 05100
62,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
82,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
42,UY,0,0,,,UZ
5,FX, 115440
5,FZ, 355287
12,FY, 113
16,FX, -524
16,FZ, 170
39,FX, -3001
39,FZ, 5198
43,FX, -10397
WRITE
COM
TER,1,1,1
IME, 05200
62,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
82,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
42,UY,0,0,,,UZ
5,FX, 115440
5,FZ, 355287
12,FY, 43
16,FX, -477
16,FZ, 155
39,FX, -2788
39,FZ, 4828
43,FX, -9714
WRITE
COM
TER,1,1,1
IME, 05300
62,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
82,UX,0,0,,,UY,UZ,ROTX,ROTY,ROTZ
42,UY,0,0,,,UZ
5,FX, 115440
5,FZ, 355287
12,FY, -21
16,FX, -435
16,FZ, 141

F -39, FX, -2591
F -39, FZ, 4488
F -43, FX, -9084
LWRITE
/COM
ITER, 1, 1, 1 05400
TIME, 0.62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTY, ROTZ
0, 82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTY, ROTZ
0, 42, UX, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, -81
F, 16, FX, -395
F, 16, FZ, 128
F, 39, FX, -2410
F, 39, FZ, 4175
F, 43, FX, -8502
LWRITE
/COM
ITER, 1, 1, 1 05500
TIME, 0.62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTY, ROTZ
0, 82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTY, ROTZ
0, 42, UX, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, -137
F, 16, FX, 358
F, 16, FZ, 116
F, 39, FX, -2242
F, 39, FZ, 3884
F, 43, FX, -7965
LWRITE
/COM
ITER, 1, 1, 1 05600
TIME, 0.62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTY, ROTZ
0, 82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTY, ROTZ
0, 42, UX, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, -187
F, 16, FX, -329
F, 16, FZ, 105
F, 39, FX, -2086
F, 39, FZ, 3614
F, 43, FX, -7466
LWRITE
/COM
ITER, 1, 1, 1 05700
TIME, 0.62, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTY, ROTZ
0, 82, UX, 0, 0, ., UY, UZ, ROTX, ROTY, ROTY, ROTZ
0, 42, UX, 0, 0, ., UZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, -235
F, 16, FX, -293
F, 16, FZ, 95
F, 39, FX, -1943
F, 39, FZ, 3365
F, 43, FX, -7005
LWRITE
/COM

TIME 05800
 0.62 UX 0 0 .UY UZ ROTX ROTY ROTZ
 0.82 UX 0 0 .UY UZ ROTX,ROTY,ROTZ
 0.42 UX 0 0 .UZ
 F. 5 FX 115440
 F. 5 FZ 355287
 F. 12 FY -277
 F. 16 FX -264
 F. 16 FZ -86
 F. 39 FX 1809
 F. 39 FZ -3135
 F. 43 FX -6576
 LWRITE
 /COM
 ITER 1 1.1
 TIME 05900
 0.62 UX 0 0 .UY UZ ROTX,ROTY,ROTZ
 0.82 UX 0 0 .UY UZ,ROTX,ROTY,ROTZ
 0.42 UX 0 0 .UZ
 F. 5 FX 115440
 F. 5 FZ 355287
 F. 12 FY -318
 F. 16 FX -237
 F. 16 FZ -77
 F. 39 -Y -1685
 F. 39 +Y 2918
 F. 43 FX -6178
 LWRITE
 /COM
 ITER 1 1.1
 TIME 06000
 0.32 UX 0 0 .UY UZ,ROTX,ROTY,ROTZ
 0.82 UX 0 0 .UY UZ,ROTX,ROTY,ROTZ
 0.42 UX 0 0 .UZ
 F. 5 FX 115440
 F. 5 FZ 355287
 F. 12 FY -355
 F. 16 FX -211
 F. 16 FZ -69
 F. 39 FX -1569
 F. 39 FZ 2717
 F. 43 FX -5809
 LWRITE
 /COM
 ITER 1 1.1
 TIME 06100
 0.62 UX 0 0 .UY UZ,ROTX,ROTY,ROTZ
 0.82 UX 0 0 .UY UZ,ROTX,ROTY,ROTZ
 0.42 UX 0 0 .UZ
 F. 5 FX 115440
 F. 5 FZ 355287
 F. 12 FY -330
 F. 16 FX -87
 F. 16 FZ -61
 F. 39 FX -1461
 F. 39 FZ 2531
 F. 43 FX -5463
 LWRITE
 /COM
 ITER 1 1.1
 TIME 06200
 0.62 UX 0 0 .UY UZ,ROTX,ROTY,ROTZ
 0.82 UX 0 0 .UY UZ,ROTX,ROTY,ROTZ
 0.42 UX 0 0 .UZ

S, 5, FX, 1154.69
 F, 5, FZ, 355287
 F, 12, FY, -422
 F, 16, FX, -165
 F, 16, FZ, -1361
 F, 39, FX, 2357
 F, 39, FZ, -5145
 LWRITE
 /COM
 ITER 1, 1, 1 TIME 06300
 D, 62, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 D, 82, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 D, 42, UX, 0, 0, , UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -452
 F, 16, FX, -144
 F, 16, FZ, -47
 F, 39, FX, -1267
 F, 39, FZ, 2194
 F, 43, FX, -4843
 LWRITE
 /COM
 ITER 1, 1, 1 TIME 06400
 D, 62, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 D, 82, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 D, 42, UX, 0, 0, , UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -479
 F, 16, FX, -124
 F, 16, FZ, -40
 F, 39, FX, -1179
 F, 39, FZ, 2041
 F, 43, FX, -4563
 LWRITE
 /COM
 ITER 1, 1, 1 TIME 06500
 D, 62, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 D, 82, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 D, 42, UX, 0, 0, , UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -506
 F, 16, FX, -107
 F, 16, FZ, -35
 F, 39, FX, -1097
 F, 39, FZ, 1899
 F, 43, FX, -4301
 LWRITE
 /COM
 ITER 1, 1, 1 TIME 06600
 D, 62, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 D, 82, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 D, 42, UX, 0, 0, , UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -529
 F, 16, FX, -89
 F, 16, FZ, -29

F-39, FX, -1019
 F-39, FZ, -1766
 F-43, FX, -4057
 LWRITE
 /COM
 ITER. 1, 1, 1
 TIME, 06700
 D-62, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
 D-82, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
 D-42, UX, 0, 0, ,UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, 5552
 F, 16, FX, -74
 F, 16, FZ, 24
 F, 39, FX, -947
 F, 39, FZ, 1640
 F, 43, FX, -3827
 LWRITE
 /COM
 ITER. 1, 1, 1
 TIME, 06800
 D-62, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
 D-82, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
 D-42, UX, 0, 0, ,UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -571
 F, 16, FX, -58
 F, 16, FZ, 19
 F, 39, FX, -879
 F, 39, FZ, 1523
 F, 43, FX, -3610
 F, 43, FZ, -3408
 LWRITE
 /COM
 ITER. 1, 1, 1
 TIME, 06900
 D-62, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
 D-82, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
 D-42, UX, 0, 0, ,UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -5
 F, 16, FX, -7
 F, 16, FZ, 14
 F, 39, FX, -815
 F, 39, FZ, 1412
 F, 43, FX, -3408
 LWRITE
 /COM
 ITER. 1, 1, 1
 TIME, 07000
 D-62, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
 D-82, UX, 0, 0, ,UY, UZ, ROTX, ROTY, ROTZ
 D-42, UX, 0, 0, ,UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -608
 F, 16, FX, -31
 F, 16, FZ, 10
 F, 39, FX, -755
 F, 39, FZ, 1309
 F, 43, FX, -3218
 LWRITE
 /COM

TER 1 1 1 07100
 TIME 0 0 0 UY UZ ROTX ROTY ROTZ
 0 62 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 82 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 42 UY 0 0 ... UY UZ ROTX ROTY ROTZ
 5 FX 115440
 5 FZ 355287
 12 FY -624
 16 FX -17
 16 FZ 6
 39 FX -698
 39 FZ 1209
 43 FX -3040
 WRITE
 COM
 TER 1 1 1 07200
 TIME 0 0 0 UY UZ ROTX ROTY ROTZ
 0 62 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 82 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 42 UY 0 0 ... UY UZ ROTX ROTY ROTZ
 5 FX 115440
 5 FZ 355287
 12 FY -641
 16 FX -6
 16 FZ 2
 39 FX -645
 39 FZ 1117
 43 FX -2871
 WRITE
 COM
 TER 1 1 1 07300
 TIME 0 0 0 UY UZ ROTX ROTY ROTZ
 0 62 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 82 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 42 UY 0 0 ... UY UZ ROTX ROTY ROTZ
 5 FX 115440
 5 FZ 355287
 12 FY -654
 16 FX 4
 16 FZ -1
 39 FX -595
 39 FZ 1001
 43 FX -2711
 WRITE
 COM
 TER 1 1 1 07400
 TIME 0 0 0 UY UZ ROTX ROTY ROTZ
 0 62 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 82 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 42 UY 0 0 ... UY UZ ROTX ROTY ROTZ
 5 FX 115440
 5 FZ 355287
 12 FY -666
 16 FX 15
 16 FZ -5
 39 FX -547
 39 FZ 948
 43 FX -2563
 WRITE
 COM
 TER 1 1 1 07500
 TIME 0 0 0 UY UZ ROTX ROTY ROTZ
 0 62 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 82 UX 0 0 ... UY UZ ROTX ROTY ROTZ
 0 42 UY 0 0 ... UY UZ ROTX ROTY ROTZ

F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -678
 F, 16, FX, 25
 F, 16, FZ, -8
 F, 39, FX, -502
 F, 39, FZ, 870
 F, 43, FX, -2420
 LWRITE
 /COM
 ITER, 1, 1, 1
 TIME, 07600
 0.62, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 0.82, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 0.42, UY, 0, 0, , UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -690
 F, 16, FX, 34
 F, 16, FZ, -11
 F, 39, FX, -460
 F, 39, FZ, 796
 F, 43, FX, -2288
 LWRITE
 /COM
 ITER, 1, 1, 1
 TIME, 07700
 0.62, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 0.82, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 0.42, UY, 0, 0, , UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -700
 F, 16, FX, 44
 F, 16, FZ, -14
 F, 39, FX, -420
 F, 39, FZ, 727
 F, 43, FX, -2160
 LWRITE
 /COM
 ITER, 1, 1, 1
 TIME, 07800
 0.62, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 0.82, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 0.42, UY, 0, 0, , UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -709
 F, 16, FX, 51
 F, 16, FZ, -17
 F, 39, FX, -381
 F, 39, FZ, 661
 F, 43, FX, -2042
 LWRITE
 /COM
 ITER, 1, 1, 1
 TIME, 07900
 0.62, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 0.82, UX, 0, 0, , UY, UZ, ROTX, ROTY, ROTZ
 0.42, UY, 0, 0, , UZ
 F, 5, FX, 115440
 F, 5, FZ, 355287
 F, 12, FY, -718
 F, 16, FX, 60
 F, 16, FZ, -20

TER 1.1.1 08400
TIME 0.62.0X.0 0...UY.UZ.ROTX.ROTY.RO12
0.82.0X.0 0...UY.UZ.RO1X.ROTY.RO12
0.42.0Y.0 0...UY.UZ.
5.FX. 115440
5.FZ. 355287
12.FY. -751
16.FX. -94
16.FZ. -31
39.FX. -191
39.FZ. -331
43.FX. -1441

WHITE

COM

TER 1.1.1 08500
TIME 0.62.0X.0 0...UY.UZ.ROTX.ROTY.RO12
0.82.0X.0 0...UY.UZ.RO1X.ROTY.RO12
0.42.0Y.0 0...UY.UZ.
5.FX. 115440
5.FZ. 355287
12.FY. -756
16.FX. -99
16.FZ. -32
39.FX. -164
39.FZ. -284
43.FX. -1357

WHITE

COM

TER 1.1.1 08600
TIME 0.62.0X.0 0...UY.UZ.ROTX.ROTY.RO12
0.82.0X.0 0...UY.UZ.RO1X.ROTY.RO12
0.42.0Y.0 0...UY.UZ.
5.FX. 115440
5.FZ. 355287
12.FY. -760
16.FX. -104
16.FZ. -34
39.FX. -139
39.FZ. -240
43.FX. -1272

WHITE

COM

TER 1.1.1 08700
TIME 0.62.0X.0 0...UY.UZ.ROTX.ROTY.RO12
0.82.0X.0 0...UY.UZ.RO1X.ROTY.RO12
0.42.0Y.0 0...UY.UZ.
5.FX. 115440
5.FZ. 355287
12.FY. -764
16.FX. -110
16.FZ. -36
39.FX. -114
39.FZ. -198
43.FX. -1189

WHITE

COM

TER 1.1.1 08800
TIME 0.62.0X.0 0...UY.UZ.ROTX.ROTY.RO12
0.82.0X.0 0...UY.UZ.RO1X.ROTY.RO12
0.42.0Y.0 0...UY.UZ.

```

F, S, FX, 115440
F, S, FZ, 355287
F, 12, FY, -768
F, 16, FX, 114
F, 16, FZ, -37
F, 39, FX, -90
F, 39, FZ, 156
F, 43, FX, -1103
LWRITE
/COM
ITER 1,1,1
TIME 08900
0.62 UX,0,0.,UY,UZ,ROTX,ROTY,ROTZ
0.82 UX,0,0.,UY,UZ,ROTX,ROTY,ROTZ
D,42 UY,0,0.,UY,UZ,ROTX,ROTY,ROTZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, -771
F, 16, FX, 119
F, 16, FZ, -39
F, 39, FX, -67
F, 39, FZ, 116
F, 43, FX, -1014
LWRITE
/COM
ITER 1,1,1
TIME 09000
0.62 UX,0,0.,UY,UZ,ROTX,ROTY,ROTZ
0.82 UX,0,0.,UY,UZ,ROTX,ROTY,ROTZ
D,42 UY,0,0.,UY,UZ,ROTX,ROTY,ROTZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, -773
F, 16, FX, 123
F, 16, FZ, -40
F, 39, FX, -43
F, 39, FZ, 74
F, 43, FX, -916
LWRITE
/COM
ITER 1,1,1
TIME 09100
0.62 UX,0,0.,UY,UZ,ROTX,ROTY,ROTZ
0.82 UX,0,0.,UY,UZ,ROTX,ROTY,ROTZ
D,42 UY,0,0.,UY,UZ,ROTX,ROTY,ROTZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, -776
F, 16, FX, 128
F, 16, FZ, -42
F, 39, FX, -18
F, 39, FZ, 31
F, 43, FX, -806
LWRITE
/COM
ITER 1,1,1
TIME 09200
0.62 UX,0,0.,UY,UZ,ROTX,ROTY,ROTZ
0.82 UX,0,0.,UY,UZ,ROTX,ROTY,ROTZ
D,42 UY,0,0.,UY,UZ,ROTX,ROTY,ROTZ
F, 5, FX, 115440
F, 5, FZ, 355287
F, 12, FY, -778
F, 16, FX, 132
F, 16, FZ, -43

```

F, 39,FX, 8
F, 39,FZ, -14
F, 43,FX, -679
LWRITE
/COM
ITER,1,1,1
TIME, 09300
D, 62,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D, 82,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D, 42,UY,0.0.,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F, 12,FY, -781
F, 16,FX, 137
F, 16,FZ, -44
F, 39,FX, 39
F, 39,FZ, -67
F, 43,FX, -533
LWRITE
/COM
ITER,1,1,1
TIME, 09400
D, 62,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D, 82,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D, 42,UY,0.0.,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F, 12,FY, -784
F, 16,FX, 142
F, 16,FZ, -46
F, 39,FX, 73
F, 39,FZ, -127
F, 43,FX, -364
LWRITE
/COM
ITER,1,1,1
TIME, 09500
D, 62,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D, 82,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D, 42,UY,0.0.,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F, 12,FY, -788
F, 16,FX, 147
F, 16,FZ, -48
F, 39,FX, 116
F, 39,FZ, -201
F, 43,FX, -166
LWRITE
/COM
ITER,1,1,1
TIME, 09600
D, 62,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D, 82,UX,0.0.,,UY,UZ,ROTX,ROTY,ROTZ
D, 42,UY,0.0.,,UZ
F, 5,FX, 115440
F, 5,FZ, 355287
F, 12,FY, -795
F, 16,FX, 155
F, 16,FZ, -50
F, 39,FX, 168
F, 39,FZ, -291
F, 43,FX, 59
LWRITE
/COM

TER, 1, 1, 1 09700
TIME, 0.0, .UY, UX, C 0, .UY, UZ, ROTX, ROTY, ROTZ
0.62, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
0.42, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, -804
16, FX, 164
16, FZ, -53
39, FX, 234
39, FZ, -405
43, FX, 315
WRITE

COM

TER, 1, 1, 1 09800
TIME, 0.0, .UY, UX, C 0, .UY, UZ, ROTX, ROTY, ROTZ
0.62, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
0.42, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, -817
16, FX, 178
16, FZ, -58
39, FX, 312
39, FZ, -540
43, FX, 596
WRITE

COM

TER, 1, 1, 1 09900
TIME, 0.0, .UY, UX, C 0, .UY, UZ, ROTX, ROTY, ROTZ
0.62, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
0.42, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, -837
16, FX, 194
16, FZ, -63
39, FX, 407
39, FZ, -705
43, FX, 895
WRITE

COM

TER, 1, 1, 1 10000
TIME, 0.0, .UY, UX, C 0, .UY, UZ, ROTX, ROTY, ROTZ
0.62, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
0.82, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
0.42, UX, 0, 0, .UY, UZ, ROTX, ROTY, ROTZ
5, FX, 115440
5, FZ, 355287
12, FY, -868
16, FX, 215
16, FZ, -70
39, FX, 520
39, FZ, -901
43, FX, 1201
WRITE

A/FORMATTE
FINISH
INPUT, 27
FINISH

IE/80/2664-3

63314 VAX0162-5032 REEL
1 MVS1078VX016292244028120220
INBOUND STATUS NORMAL TERM
OUTBOUND STATUS NORMAL END OF JOB

833413 START 0837 18 STOP 0837 28 TYPE D
PAGES 000034 SHEETS 000017
NO INPUT BLKS SKIPPED

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BOUND STATUS NORMAL INBOUND TERM NO INPUT BLKS SKIPPED
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