

Public Service  
Electric and Gas  
Company

Steven E. Miltenberger

Public Service Electric and Gas Company P.O. Box 236, Hancocks Bridge, NJ 08038 609-339-1100

Vice President and Chief Nuclear Officer

SEP 03 1992  
NLR-N92120

United States Nuclear Regulatory Commission  
Document Control Desk  
Washington, DC 20555

Gentlemen:

RESPONSE TO GENERIC LETTER 92-01, REVISION 1  
REACTOR VESSEL STRUCTURAL INTEGRITY, 10CFR50.54(f)  
HOPE CREEK GENERATING STATION  
FACILITY OPERATING LICENSE NO. NPF-57  
DOCKET NO. 50-354

PSE&G submitted the response to Generic Letter 92-01, Revision 1 to the NRC in Letter NLR-N92080 dated June 30, 1992. This submittal provided peak and maximum end of life (EOL) fluence levels which were calculated utilizing the methodology of Regulatory Guide 1.99, Rev. 1. PSE&G's response to Generic Letter 88-11 included the revised fluence levels from Revision 2 of the Regulatory Guide. These revised fluence levels were inadvertently excluded from the Generic Letter 92-01 response.

Once PSE&G realized the submitted data was not reflective of the Generic Letter 88-11 submittal, PSE&G contacted Mr. J. Stone, NRR Licensing Project Manager to apprise him of this status.

Although the differences are minor in nature, PSE&G is submitting revised fluence levels to be incorporated into the response to Generic Letter 92-01, Rev. 1 consistent with the values previously submitted. A marked up Table 4 with the corrections annotated as well as a corrected Table 4 are provided for incorporation into the original Generic Letter 92-01 submittal.

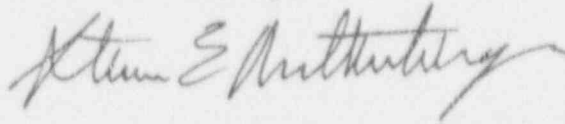
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PSE&G apologizes for any inconvenience this may cause. Should you have any questions regarding this submittal, please do not hesitate to contact us.

Sincerely,



Attachment  
Affidavit

C Mr. T. T. Martin, Administrator - Region I  
U. S. Nuclear Regulatory Commission  
475 Allendale Road  
King of Prussia, PA 19406

Mr. J. Stone, Licensing Project Manager  
U. S. Nuclear Regulatory Commission  
One White Flint North  
11555 Rockville Pike  
Rockville, MD 20852

Ms. A. Keller  
U. S. Nuclear Regulatory Commission  
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Mr. T. P. Johnson (S05)  
USNRC Senior Resident Inspector

Mr. K. Tosch, Chief  
NJ Department of Environmental Protection  
Division of Environmental Quality  
Bureau of Nuclear Engineering  
CN 415  
Trenton, NJ 08625

STATE OF NEW JERSEY )  
 ) SS.  
COUNTY OF SALEM )

Steven E. Miltenberger, being duly sworn according to law deposes and says:

I am Vice President and Chief Nuclear Officer of Public Service Electric and Gas Company, and as such, I find the matters set forth in the above referenced letter, concerning the Hope Creek Generating Station, are true to the best of my knowledge, information and belief.

Steven E. Miltenberger

Subscribed and Sworn to before me  
this 3<sup>rd</sup> day of September, 1992

Kimberly A. Hill  
Notary Public of New Jersey

KIMBERLY A. HILL  
NOTARY PUBLIC OF NEW JERSEY  
My Commission Expires March 9, 1997

My Commission expires on \_\_\_\_\_

NLR-392120

ATTACHMENT

RESPONSE TO GENERIC LETTER 92-01, REVISION 1  
REVISED TABLE 4  
HOPE CREEK GENERATING STATION  
DOCKET NO. 50-354

TABLE 4

RADIATION  $\Delta RT_{NDT}$  AND EOL  $RT_{NDT}$  FOR BELTLINE MATERIALS

Heat Number/Lot	Chemistry		$RT_{NDT}$ ( $^{\circ}F$ )		
	Cu (Wt Percent)	Ni (Wt Percent)	Initial Value	Guide 1.99, R2 Extrapolation	Estimated EOL
Vessel Plate Material (SA533, Gr. B, Cl-1) for Shell Courses 4 and 5					
Peak EOL Fluence at 1/4T - <del>1.1</del> <sup>1.2</sup> $\times 10^{18}$ n/cm <sup>2</sup>					
5K2963-1-2	0.07	0.58	-10	40	+30
5K2930-1-2	0.08	0.56	+19	46	+65
5K3238-1-2 <sup>(1)</sup>	0.09	0.63	+7	52	+59
5K3230-1-2	0.07	0.56	-10	40	+30
6C35-1-2	0.09	0.54	-11	52	+41
6C45-1-2	0.08	0.57	+1	46	+47
Vessel Plate Material (SA533, Gr. B, Cl-1) for Shell Course 3					
Maximum EOL Fluence <sup>(2)</sup> at 1/4T - <del>2.37</del> <sup>2.36</sup> $\times 10^{17}$ n/cm <sup>2</sup>					
5K3025-1	0.15	0.71	+19	45	+64
5K2608-1	0.09	0.58	+19	23	+42
5K2698-1	0.10	0.58	+19	26	+45
Material for Girth and Longitudinal Welds for Shell Courses 4 and 5					
Peak EOL Fluence at 1/4T - <del>1.1</del> <sup>1.2</sup> $\times 10^{18}$ n/cm <sup>2</sup>					
510-01205 <sup>(3)</sup>	0.09	0.54	-40	98	+58
D53040/1125-02205 <sup>(2,5)</sup>	0.08	0.63	-30	96	+66

TABLE 4 (Cont)

Heat Number/Loc	Chemistry		RT <sub>NDT</sub> (*F)		
	Cu (Wt Percent)	Ni (Wt Percent)	Initial Value	Guide 1.99R2 Extrapolation	Estimated EOL
Girth Weld Material between Shell Courses 3 and 4					
Maximum EOL Fluence <sup>(2)</sup> (Shell Course 3) at 1/4T $\times 10^{17}$ n/cm <sup>2</sup>					
				2.37 2.36	
519-01205 <sup>(4)</sup>	0.010	0.53	-49	8	-41
504-01205 <sup>(4)</sup>	0.010	0.51	-31	8	-23
D55733/1810-02205	0.100	0.68	-40	51	+11
D53040/1810-02205	0.100	0.68	-49	51	+2

LPCI Nozzle Weld Material (Lotter of Nozzles)					
Maximum EOL Fluence <sup>(2)</sup> at 1/4T $\times 10^{17}$ n/cm <sup>2</sup>					
				1.6 1.7	
001-01205	0.02	0.51	-40	9	-31

(1) Surveillance test plate material.

(2) Axial and radial distributions included.

(3) These materials were also used in the longitudinal seams shell course 3 and in the girth welds between shell courses and 4.

(4) These materials were also used for the LPCI nozzle welds.

(5) Surveillance weld material.

TABLE 4

RADIATION  $\Delta RT_{NDT}$  AND EOL  $RT_{NDT}$  FOR BELTLINE MATERIALS

Heat Number/Lot	Chemistry		$RT_{NDT}$ ( $^{\circ}F$ )		
	Cu (Wt Percent)	Ni (Wt Percent)	Initial Value	Guide 1.99, R2 Extrapolation	Estimated EOL

 $\Delta$  from Reg.

Vessel Plate Material (SA533, Gr. B, Cl-1) for Shell Courses 4 and 5  
Peak EOL Fluence at  $1/4T = 1.2 \times 10^{18}$  n/cm<sup>2</sup>

5K2963-1-2	0.07	0.58	-10	40	+30
5K2530-1-2	0.08	0.56	+19	46	+65
5K3238-1-2 <sup>(1)</sup>	0.09	0.63	+7	52	+59
5K3230-1-C	0.07	0.56	-10	40	+30
6C35-1-2	0.09	0.54	-11	52	+41
6C45-1-2	0.08	0.57	+1	46	+47

Vessel Plate Material (SA533, Gr. B, Cl-1) for Shell Course 3  
Maximum EOL Fluence<sup>(2)</sup> at  $1/4T = 2.36 \times 10^{17}$  n/cm<sup>2</sup>

5K3025-1	0.15	0.71	+19	45	+64
5K2608-1	0.09	0.58	+19	23	+42
5K2698-1	0.10	0.58	+19	26	+45

Material for Girth and Longitudinal Welds for Shell Courses 4 and 5  
Peak EOL Fluence at  $1/4T = 1.2 \times 10^{18}$  n/cm<sup>2</sup>

510-01205 <sup>(3)</sup>	0.09	0.54	-40	98	+58
D53040/1125-02205 <sup>(2,5)</sup>	0.08	0.63	-30	96	+66

TABLE 4 (Cont)

Heat Number/Lot	Chemistry		RT <sub>NDT</sub> (°F)		
	Cu (Wt Percent)	Ni (Wt Percent)	Initial Value	Guide 1.99 R2 Extrapolation	Estimated EOL
Δ from Reg.					
Girth Weld Material between Shell Courses 3 and 4					
Maximum EOL Fluence <sup>(2)</sup> (Shell Course 3) at 1/4T = $2.36 \times 10^{17}$ n/cm <sup>2</sup>					
519-01205 <sup>(4)</sup>	0.010	0.53	-49	8	-41
504-01205 <sup>(4)</sup>	0.010	0.51	-31	8	-23
D55733/1810-02205	0.100	0.68	-40	51	+11
D53040/1810-02205	0.100	0.68	-49	51	+2

LPCI Nozzle Weld Material (Bottom of Nozzles)

Maximum EOL Fluence<sup>(2)</sup> at 1/4T =  $1.7 \times 10^{17}$  n/cm<sup>2</sup>

001-01205	0.02	0.51	-40	9	-31
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(1) Surveillance test plate material.

(2) Axial and radial distributions included.

(3) These materials were also used in the longitudinal seams of shell course 3 and in the girth welds between shell courses 3 and 4.

(4) These materials were also used for the LPCI nozzle welds.

(5) Surveillance weld material.