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Component Flooding Evaluation Laboratory

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Objective

Support development of deeper comprehension of nuclear power plant flooding risks through three pathways:

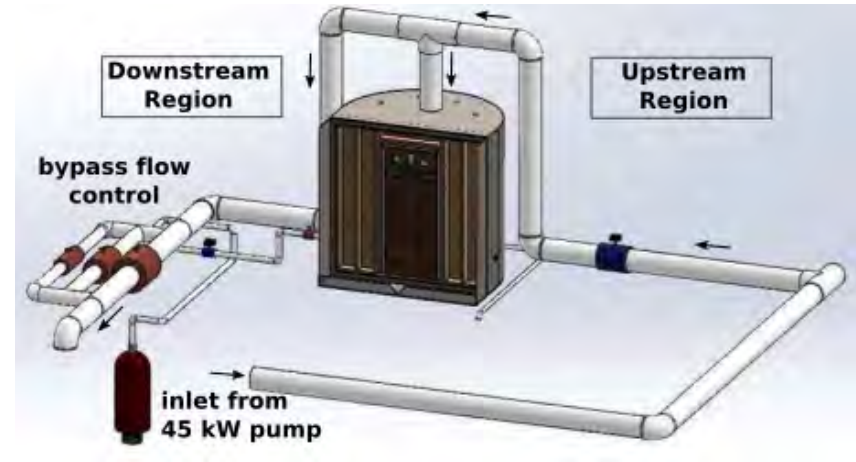
1. Execution of component flooding experiments
2. Comprehensive data analysis and component fragility curve development
3. Integration of component fragility into flooding simulation



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Portal Evaluation Tank

- 2,000-gal tank
- 8,000-gal reservoir
- 4500 gpm pump
- 8 ft x 8 ft opening for components

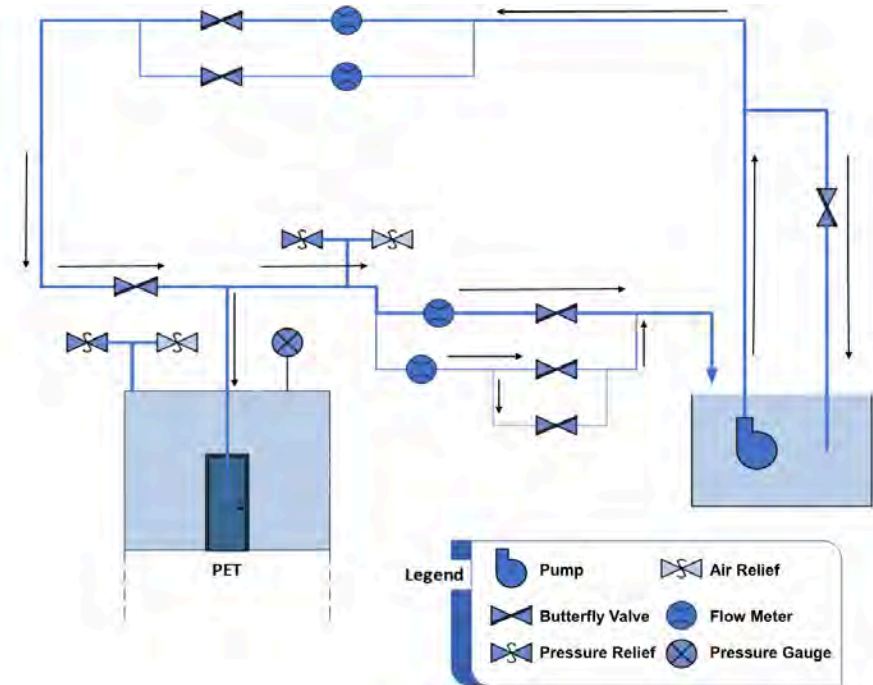


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Instrumentation

- 2 inlet flowmeters
- 2 outlet flowmeters
- 2 pressure based depth measurement
- Small leakage measurement using V-notch weir





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Hollow-core Door Experiments

- Inexpensive
- Rapid
- Learning to build
- Learning to operate
- Learning to collect data



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Steel Door Experiments



- Representative of industrial setting
- Required strengthened construction
- Outward swinging
- Inward swinging
- With and without dead-bolt

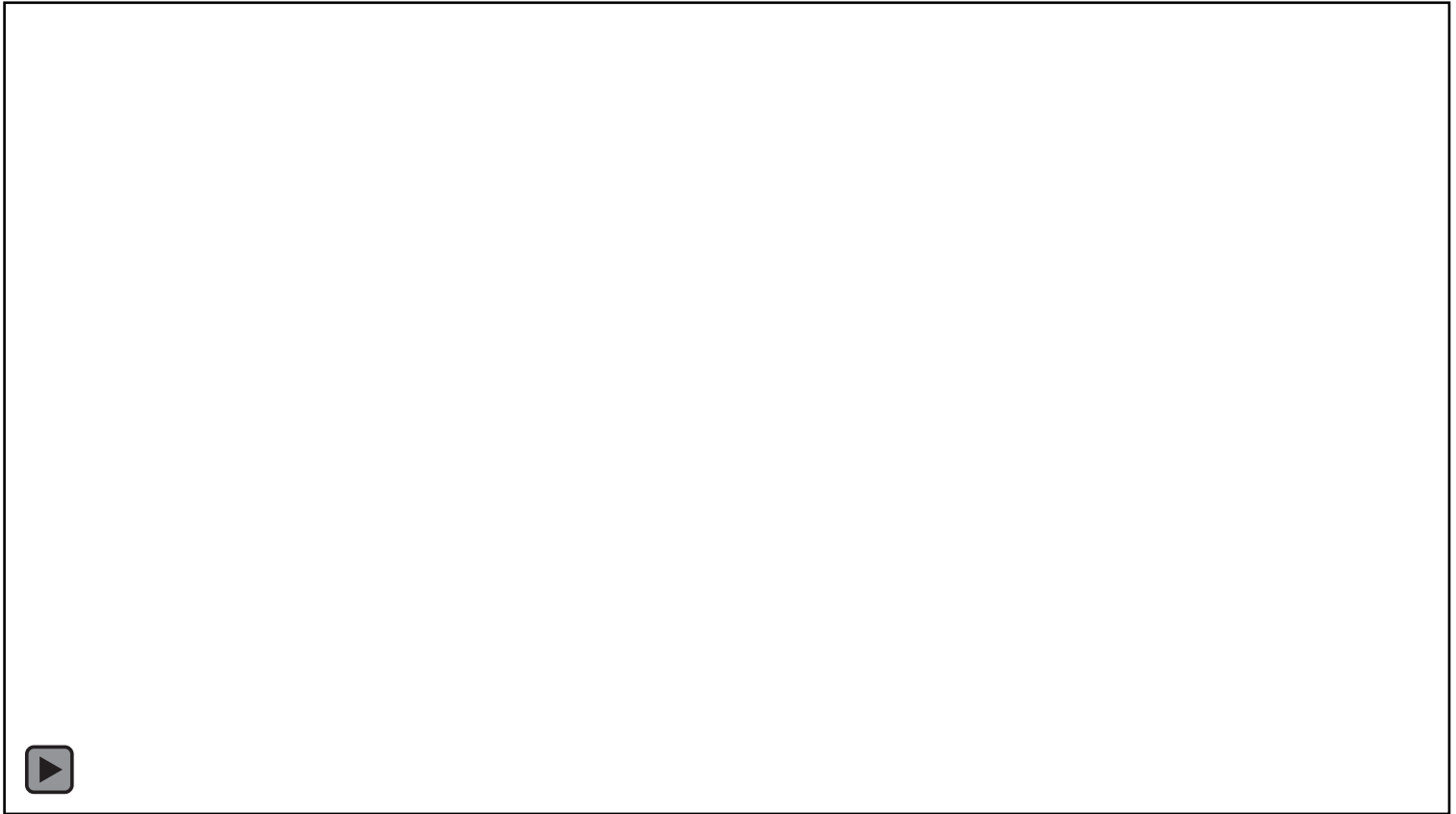


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Inward Swing Steel Door

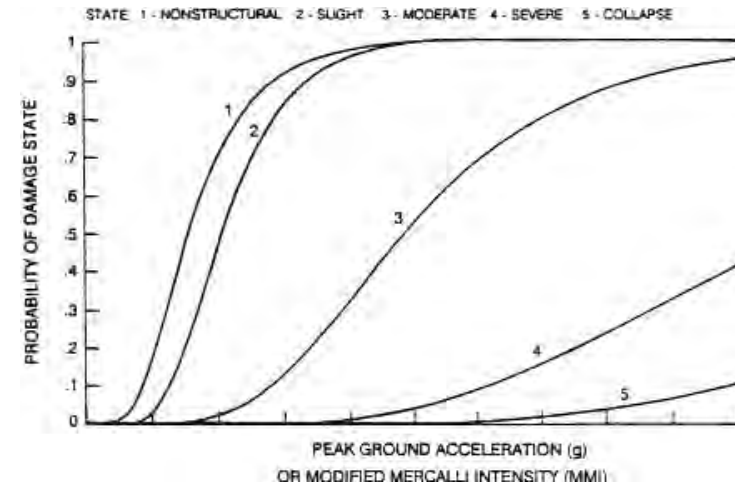


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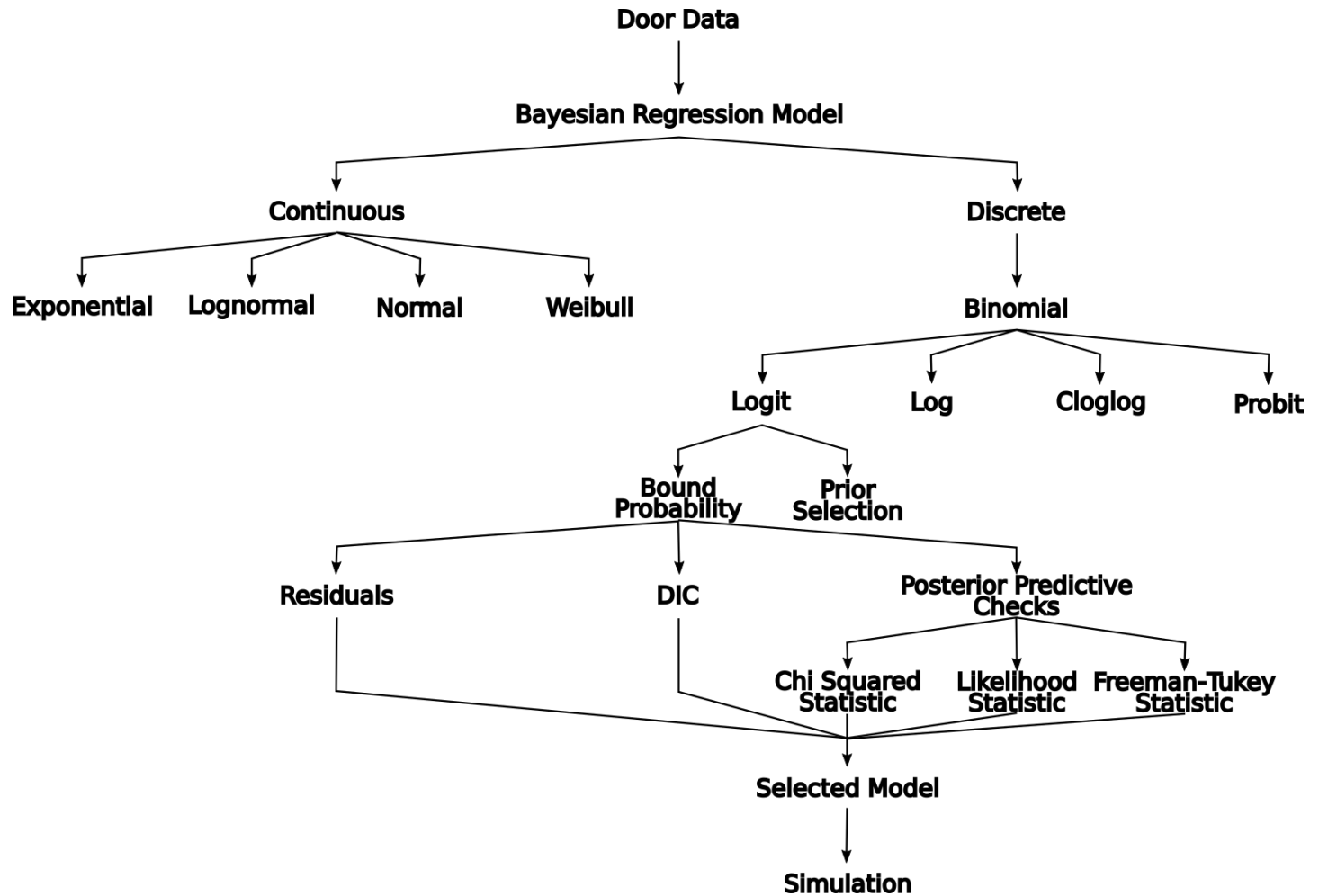
Fragility Modeling Approach

- Most fragility modeling has focused on seismic component fragility determination
- Additional observables may be better indicators for the potential of failures
 - X, Y, and Z parts of the ground motion
 - Frequency of the wave
 - Age of component
 - Anchorages of the component
 - Specifics of the component type
- Limitations can be avoided by moving to a more flexible, data-informed approach
 - Bayesian fragility modeling through experiment-driven regression modeling





Model Development





Bayesian Inference

- Need a model that represents the failure of a component during a flooding event
 - Binomial model
 - Key variable is probability of failure, p
- Determine what observable phenomena drive failure
 - Turn the parameter p into its own regression model
 - p is possibly a function of the water depth, flow rate, and even temperature

```
model {
  for(i in 1:tests){
    failure[i] ~ dbin(p.bound[i], numtested)
    logit(p[i]) <- a + b*Depth[i]
  }
  #Prior Distributions
  a ~ dnorm(0, .000001)
  b ~ dnorm(0, .000001)
}

data
list(
  tests= 19,
  numtested= 1,
  failure= c(1, 1, 1, 1, 1, 1, 1, 1, 1, 0, 0, 0, 0, 0, 0, 0, 0, 1),
  Depth= c(46.1, 39.0, 37.1, 37.8, 37.5, 37.6, 37.7, 37.1, 44.5, 25.7, 17.0, 27.4, 30.9, 32.3, 24.3, 34.8, 37.5, 38.0, 41.4)
)

inits
list(a= 0, b= 0)
```

Model (bracketed next to the for loop)

Prior Distributions (bracketed next to the a and b distributions)

Data (bracketed next to the data list)



Steel Door Results

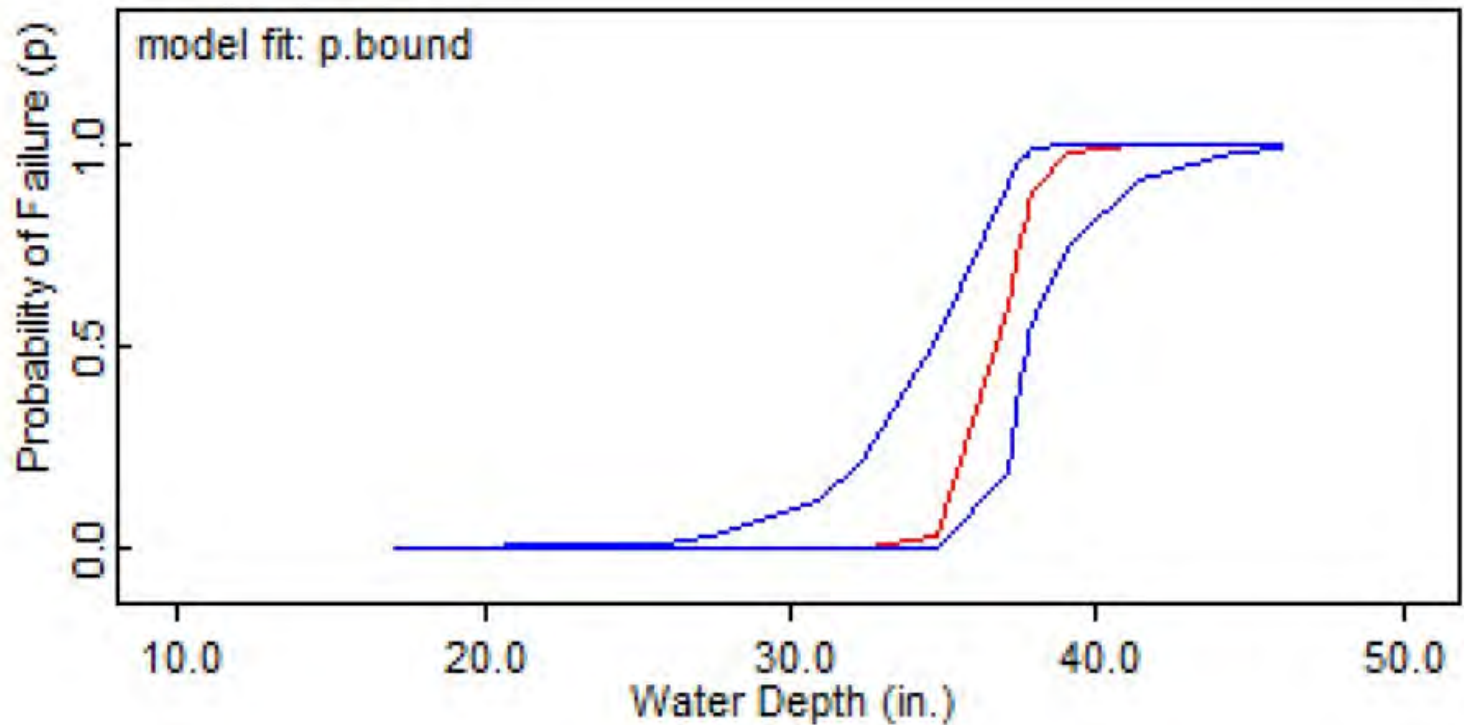
Parameter	Depth	Flow Rate	Depth & Flow Rate
a (intercept)	-75.68	-8.51	-72.5
b (depth coeff.)	2.05	na	1.83
c (flow rate coeff.)	na	0.01	0.007
sat. deviance	12.88 (10.65, 17.43)	14.29 (12.07, 18.92)	13.31 (10.1, 18.82)
Chi-square p-value	0.19	0.26	0.14
Likelihood ratio p-value	0.38	0.36	0.29
Freeman-Tukey P-value	0.33	0.23	0.21
DIC	14.42	16.01	15.66

- Posterior estimates can be used with the fragility model to calculate the failure probability for a steel door:

$$p = \frac{1}{e^{-(-75.68+2.05D)} + 1}$$



Steel Door Fragility Curve





Smoothed Particle Hydrodynamics

- Theory

- Particle based, Lagrangian, method
- Interpolation method
- A particle's property depends on the particles surrounding it
- Equations of motion

- Time stepping scheme

$$\mathbf{v}_{t+\Delta t} = \mathbf{v}_t + \Delta t \mathbf{a}_t$$

$$\mathbf{r}_{t+\Delta t} = \mathbf{r}_t + \Delta t \mathbf{v}_{t+\Delta t}$$

- Momentum

$$\frac{d\mathbf{v}_i}{dt} = - \sum_j m_j \left(\frac{P_j}{\rho_j^2} + \frac{P_i}{\rho_i^2} + \Pi_{ij} \right) \nabla_i W_{ij} + \mathbf{g}$$

- Compressibility model

$$\mathbf{v}_i^* = \mathbf{v}_i(t) + \Delta t \left(- \sum_j m_j \Pi_{ij} \nabla W_{ij}(t) + \mathbf{g} \right)$$

$$\rho_i^* = \rho_i(t) + \Delta t \sum_j m_j (\mathbf{v}_i^* - \mathbf{v}_j^*) \cdot \nabla W_{ij}(t)$$

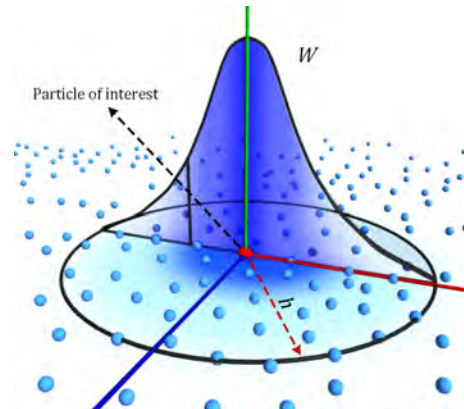
- Continuity

$$\frac{d\rho_i}{dt} = \sum_j m_j \mathbf{v}_{ij} \cdot \nabla_i W_{ij}$$

$$\nabla^2 p_i(t) = \frac{\rho_0 - \rho_i^*}{\Delta t^2}$$

- Moving particles

$$\frac{d\mathbf{r}_i}{dt} = \mathbf{v}_i + \frac{1}{2} \sum_j \frac{m_j}{\rho_{ij}} \mathbf{v}_{ij} W_{ij}$$

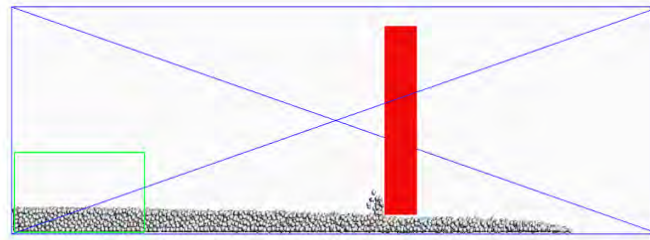




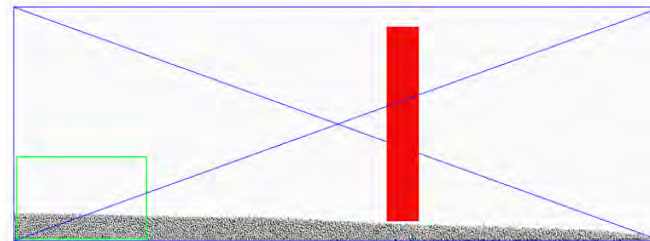
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Particle Spacing Selection

- 0.0625 m particle spacing



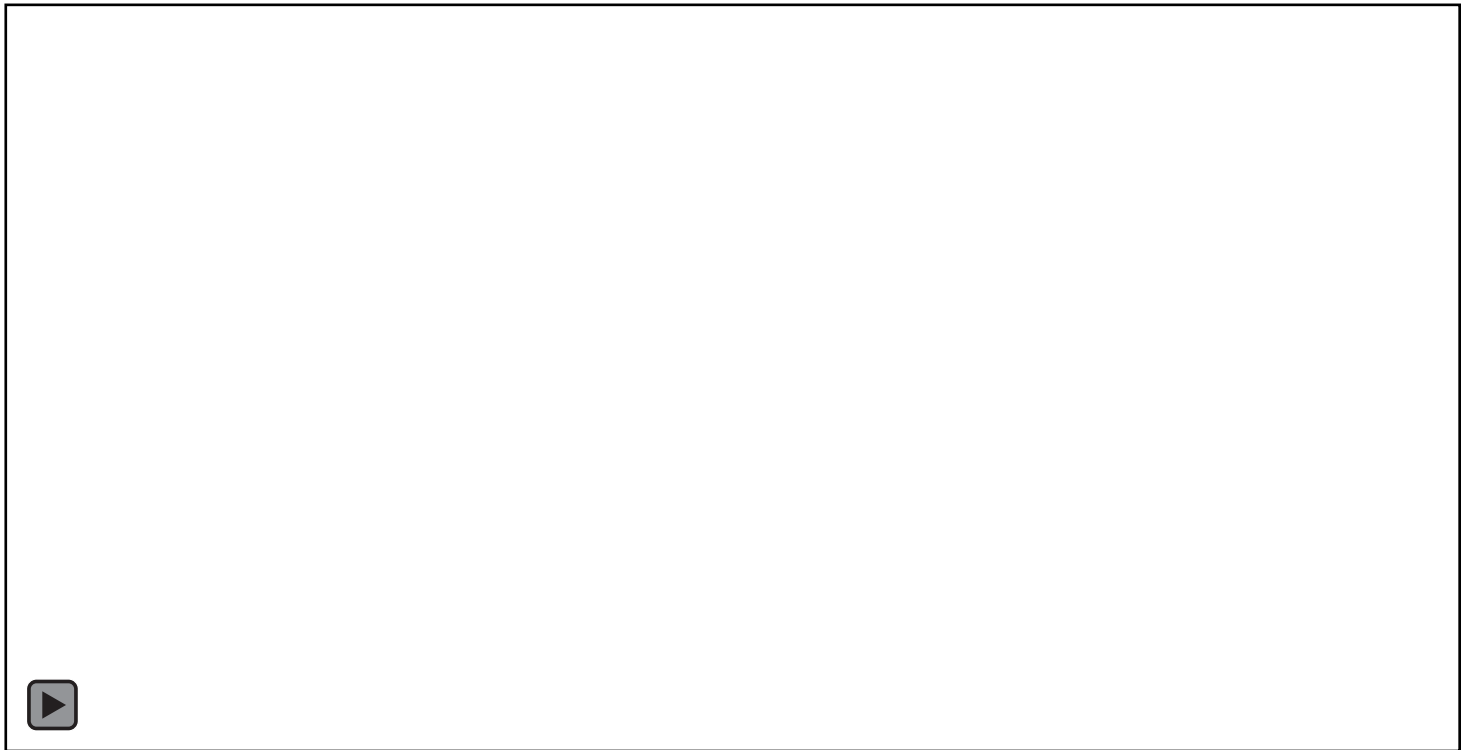
- 0.03125 m particle spacing





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Simulation Overlay

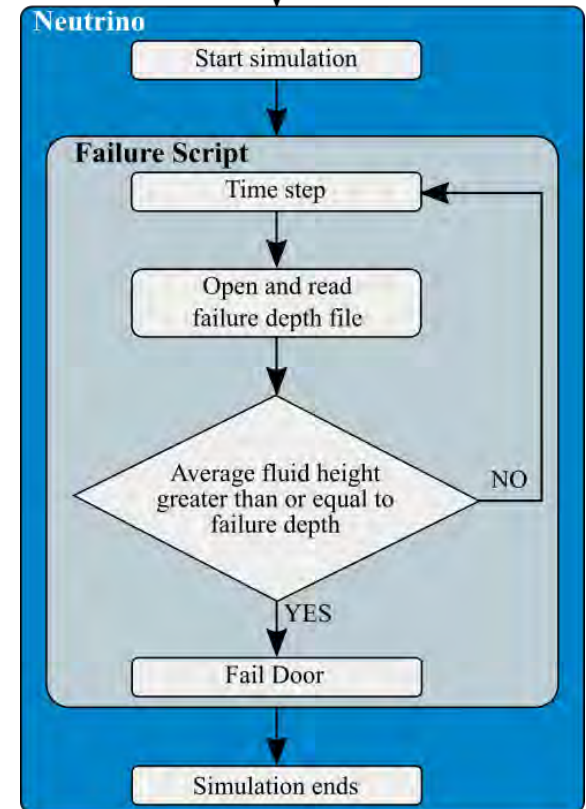
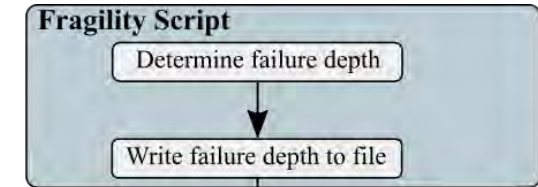
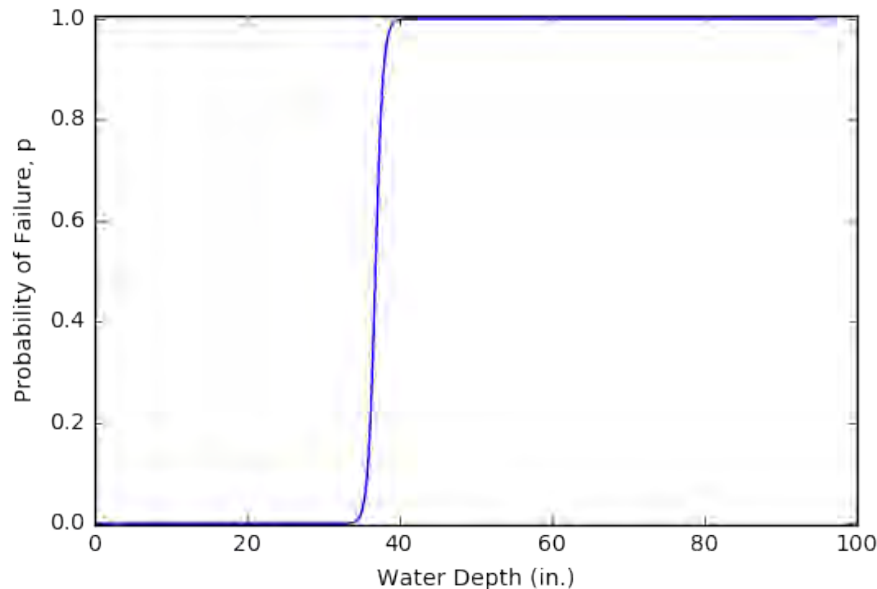


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Fragility Integration

- Flooding fragility can improve simulation to realistically model component behavior
- Couple fragility model to Neutrino via Python dynamic expression scripts





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Simulation with Fragility



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Conclusion

- Significant progress has been made in all three pathways
 - Walk-then-run approach for experiment activities
 - Detailed research on SPH validation and particle spacing selection
 - Detailed research on fragility model development
 - Coupling of fragility models and flooding simulation



References

PUBLICATIONS

- E. D. Ryan, C. L. Pope, Coupling of the Smoothed Particle Hydrodynamic Code Neutrino and the Risk Analysis Virtual Environment for Particle Spacing Optimization, *Nuclear Technology*, DOI: 10.1020/00295450.2019.1704576.
- A. Wells, E. Ryan, B. Savage, A. Tahhan, S. Suresh, C. Muchmore, C. L. Smith, and C. L. Pope, “Non-watertight Door Performance Experiments and Analysis Under Flooding Scenarios,” *Results in Engineering*, **3** (2019)
- E. D. Ryan, B. M. Savage, C. L. Smith, C. L. Pope, “Comparison of Free Surface Flow Measurements and Smoothed Particle Hydrodynamic Simulation for Potential Nuclear Power Plant Flooding Simulation,” *Annals of Nuclear Energy* **126** (2019).
- A. Tahhan, C. Muchmore, L. Nichols, A. Wells, G. Roberts, E. Ryan, S. Suresh, B. Bhandari, C. L. Pope, “Development of Experimental and Computational Procedures for Nuclear Power Plant Components Under Flooding Conditions,” *Proceedings of the 2017 25th International Conference on Nuclear Engineering* (2017).



References

TECHNICAL REPORTS

- *Nuclear Power Plant Component Flooding Fragility Research*, C. L. Pope, B. Savage, S. Jash, B. Johnson, C. Muchmore, L. Nichols, E. Ryan, S. Suresh, A. Tahhan, R. Tuladhar, A. Wells, C. L. Smith, INL/EXT-18-45247, Idaho National Laboratory, Research Report (2018).
- *Nuclear Power Plant Mechanical Component Flooding Fragility Experiments FY-2017 Report*, C. L. Pope., B. Savage, B. Johnson, C. Muchmore, L. Nichols, G. Roberts, E. Ryan, S. Suresh, A. Tahhan, R. Tuladhar, A. Wells, C. Smith, INL/EXT-17-43439, Idaho National Laboratory, Research Report (2017).
- *Nuclear Power Plant Mechanical Component Flooding Fragility Experiments Status*, C. L. Pope, B. Savage, B. Johnson, C. Muchmore, L. Nichols, G. Roberts, E. Ryan, S. Suresh, A. Tahhan, R. Tuladhar, A. Wells, C. Smith, INL/EXT-17-42728, Idaho National Laboratory, Research Report (2017).
- *Flooding Fragility Experiments and Prediction*, C. Smith, B. Bhandari, C. Muchmore, A. Tahhan, A. Wells, L. Nichols, C. L. Pope, INL/EXT-16-39963, Idaho National Laboratory, Research Report (2016).
- *Status of the Flooding Fragility Testing Development*, C. L. Pope, B. Savage, A. Sorensen, B. Bhandari, D. A. Kamerman, A. Tahhan, C. Muchmore, G. Roberts, E. Ryan, S. Suresh, A. Wells, C. Smith, INL/EXT-16-39115, Idaho National Laboratory, Research Report (2016).
- *Progress on the Industry Application External Hazard Analyses Early Demonstration*, C. L. Smith, S. Prescott, J. Coleman, E. Ryan, B. Bhandari, S. Sludern, C. L. Pope, R. Sampath, INL/EXT-15-36749, Idaho National Laboratory, Research Report (2015).
- *Industry Application External Hazard Analyses Problem Statement*, R. H. Szilard, J. Coleman, C. L. Smith, S. Prescott, A. Kammerer, R. Youngblood, C. L. Pope, INL/EXT-15-36101, Idaho National Laboratory, Research Report (2015).



References

PHD STUDENTS

- Alison Wells, PhD, *Assessing Nuclear Power Plant Component Fragility in Flooding Events using Bayesian Regression Modeling with Explanatory Variables* (defense scheduled for April 3, 2020)
- Emerald Ryan, PhD, *Determination, Development, and Validation of a Fluid Height Analysis Method and Particle Spacing Protocol for the Smoothed Particle Hydrodynamic Code Neutrino* (2019)

MS STUDENTS

- Cody Muchmore, MS, *Categorization and Evaluation of Spray Patterns from Pipe Leaks*, (2018)
- Antonio Tahhan, MS, *Performance Improvements to the Portal Evaluation Tank, Characterization Analysis of Nuclear Power Plant Component Flooding Tests* (2018)
- Soumadipta Jash, MS, *Instrumentation for Measuring Velocity of Wave Produced by Wave Impact Simulation Device for the Idaho State University Component Flooding Evaluation Laboratory* (2018)
- Sneha Suresh, MS, *Development of an Interior Component Flooding Fragility Model and Design of Component Evaluation Flooding Laboratory Safety Circuit* (2017)
- Emerald Ryan, MS, *Construction of a Smoothed Particle Hydrodynamic Model for Flow Over an Ogee Spillway Comparison to Determine Viability in Modeling Flooding Scenarios* (2016)
- Bishwo Bhandarai, MS, *Full Scale Door Testing Under Flooding Conditions to Develop Testing Protocol* (2016)
- David Kamerman, MS, *The Use of Flooding Fragility Curves in Nuclear Power Plant Risk Analysis* (2016)