



UNITED STATES  
NUCLEAR REGULATORY COMMISSION

WASHINGTON, D.C. 20555-0001

December 28, 1995

Mr. Nicholas J. Liparulo  
Nuclear Safety and Regulatory Activities  
Westinghouse Electric Corporation  
P.O. Box 355  
Pittsburgh, Pennsylvania 15230

Dear Mr. Liparulo:

SUBJECT: FOLLOWON QUESTIONS ON THE AP600 WOBRA/TRAC LONG TERM COOLING  
ANALYSIS

As a result of its review of the June 1992 application for design certification of the AP600, the staff has determined that it needs additional information in order to complete its review. The enclosed questions were developed as a result of the WCOBRA/TRAC-Oregon State University Long Term Cooling Preliminary Validation Report. A preliminary version of these questions were discussed with Westinghouse during a meeting with the Nuclear Regulatory Commission staff on December 18, 1995.

You have requested that portions of the information submitted in the June 1992 application for design certification be exempt from mandatory public disclosure. While the staff has not completed its review of your request in accordance with the requirements of 10 CFR 2.790, that portion of the submitted information is being withheld from public disclosure pending the staff's final determination. The staff concludes that these followon questions do not contain those portions of the information for which exemption is sought. However, the staff will withhold this letter from public disclosure for 30 calendar days from the date of this letter to allow Westinghouse the opportunity to verify the staff's conclusions. If, after that time, you do not request that all or portions of the information in the enclosures be withheld from public disclosure in accordance with 10 CFR 2.790, this letter will be placed in the NRC's Public Document Room.

These followon questions affect nine or fewer respondents, and therefore is not subject to review by the Office of Management and Budget under P.L. 96-511.

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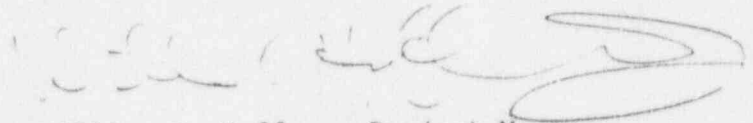
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Mr. Nicholas J. Liparulo

- 2 -

If you have any questions regarding this matter, you can contact me at  
(301) 415-1141.

Sincerely,

A handwritten signature in black ink, appearing to read "William C. Huffman". The signature is fluid and cursive, with a large, sweeping flourish at the end.

William C. Huffman, Project Manager  
Standardization Project Directorate  
Division of Reactor Program Management  
Office of Nuclear Reactor Regulation

Docket No. 52-003

Enclosure: As stated

cc w/enclosure:  
See next page

Mr. Nicholas J. Liparulo

- 2 -

December 28, 1995

If you have any questions regarding this matter, you can contact me at (301) 415-1141.

Sincerely,

Original signed by

William C. Huffman, Project Manager  
Standardization Project Directorate  
Division of Reactor Program Management  
Office of Nuclear Reactor Regulation

Docket No. 52-003

Enclosure: As stated

cc w/enclosure:  
See next page

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Mr. Nicholas J. Liparulo  
Westinghouse Electric Corporation

Docket No. 52-003  
AP600

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Enclosure to be distributed to the following addressees after the result of the proprietary evaluation is received from Westinghouse:

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**REQUEST FOR ADDITIONAL INFORMATION  
CONCERNING THE AP600 WCOBRA/TRAC LONG TERM COOLING  
PRELIMINARY VALIDATION REPORT (LTCT-GSR-003)**

- 440.554 The containment is not part of the OSU simulation, the steam produced during the LTC was reintroduced as condensate into the IRWST. Containment condensation is a major part of the LTC cooling cycle. There is no discussion in LTCT-GSR-003 of the process which establishes the adequacy of the containment as a heat exchanger. In particular there is no discussion on: (1) the adequacy of the primary water to fill the containment with steam without core uncover throughout the transient (2) the interface of the GOTHIC code and WCOBRA/TRAC regarding the time dependent condensation process and (3) the coolant inventory distribution as a function of time during the transient until steady state condensation rate is achieved.
- 440.555 The LTC window is supposed to represent a stable set of conditions demonstrating that the core remains covered and the system is able to dissipate the decay heat. Yet this does not seem to be the case in that there are still evolutions in the system parameters for the following figures: (1) the break flow integrals (Figures 5.5-4, 5.6-4, 5.7-4 and 5.8-5) (2) the ADS flow integrals (Figures 5.5-16, 5.6-16, 5.7-12 and 5.8-17) and the steam flow generated in the core (Figures 5.5-23, 5.6-23 and 5.7-19). In view of the above: why is the code converging?, why is the code stable? and why is the code suitable for the problem?
- 440.556 Section 15.6.5.4C.1.0 states that an entire transient was modeled. Please show the results of such a transient if it is available. If not why not?
- 440.557 On page 5.2-3 the presence of non condensable (air) caused a 500 sec delay to CMT draindown initiation. Is the presence of the accumulator cover gas accounted in the system during the transient?
- 440.558 The upper head water level in Figures 5.2-27, 5.3-30 and 5.4-28 for the last 3 simulations are missing. Why?
- 440.559 There is a significant discrepancy from 320 sec to 440 sec in the CMT injection flow rate Fig. 5.4-12. In addition the direction of the simulation is opposite to that of the calculation. The same trend is manifested in Figures 5.3-14, 5.2-12 and 5.1-8. What caused the discrepancy and what does it mean for the code?
- 440.560 What is the consequence of the systematic underprediction of the IRWST level in Figures 5.5-1, 5.6-1 and 5.7-1?

Enclosure

- 440.561 The WC/T ADS 1,2,3 flow integrals in Figures 5.5-16, 5.7-12 and 5.8-17 disagree with the OSU results and in addition show inconsistent trends. The trends do not point to a stabilized regime as expected for LTC. Please comment.
- 440.562 There is a large initial discrepancy (which persists throughout the window) in the core level estimates as shown in Figures 5.5-24, 5.6-24, 5.7-20 and 5.8-25. Please comment on this phenomenon and its significance.
- 440.563 The upper plenum pressure is underpredicted in Figures 5.6-2, 5.7-2 and 5.8-3. The corresponding break flows in Figures 5.6-4, 5.7-4 and 5.8-5 are inconsistent in that they should all be overpredictions. Aren't pressure predictions crucial for the core LTC behavior in that small pressure differences (from the real ones) can change the outcome of the transient? What are the step decreases in the beginning of these windows?
- 440.564 Figure 5.7-21 indicates the upper plenum level to increase while in this window the inventory should have stabilized. Please explain. In the remaining upper plenum data, there is a step level change. What is this due to?
- 440.565 In Figure 5.8-14 there is a significant DVI nozzle temperature underprediction, attributed to the contribution of the IRWST water. Is IRWST still operating this late in the transient?