DAVIS-BESSE NUCLEAR POWER STATION UNIT NO. 1

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REACTOR CONTAINMENT BUILDING INTEGRATED LEAK RATE TEST

DECEMBER 1984

TOLEDO EDISON COMPANY

Prepared	by:	John J Blessing
Reviewed	by:	R.S. Shirk U ILRT Engineer
Approved	by:	Stephen merenneng
	85 PD	03150178 850308 R ADOCK 05000346 PDR

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TABLE OF CONTENTS

Sect.	Item	Title	Page
1.0		SYNOPSIS	1
2.0		INTRODUCTION	2
3.0		GENERAL, TECHNICAL, AND TEST DATA	3
4.0		ACCEPTANCE CRITERIA	5
	4.1	TECHNICAL SPECIFICATION ACCEPTANCE CRITERIA	5
같이?	4.2	SHORT DURATION TESTING ACCEPTANCE CRITERIA	5
5.0		TEST INSTRUMENTATION	6
	5.1	SUMMARY OF INSTRUMENTS	6
	5.2	SCHEMATIC ARRANGEMENT	7
	5.3	CALIBRATION CHECKS	7
	5.4	INSTRUMENTATION PERFORMANCE	7
	5.5	VOLUME WEIGHTING FACTORS	8
	5.6	SYSTEM ERROR ANALYSIS	9
	5.7	SUPPLEMENTAL VERIFICATION	11
6.0		TEST PROCEDURE	13
	6.1	PREREQUISITES	13
	6.2	GENERAL DISCUSSION	13
	6.3	TEST PERFORMANCE	15
7.0		METHODS OF ANALYSIS	16
	7.1	GENERAL DISCUSSION	16
	7.2	STATISTICAL EVALUATION	19
8.0		DISCUSSION OF RESULTS	21
	8.1	RESULTS AT P	21
	8.2	SUPPLEMENTAL TEST RESULTS	23
	8.3	AS FOUND ANALYSIS	23
9.0		REFERENCES	25

TABLE OF CONTENTS (Cont'd)

APPENDICES

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Appendix	A	-	Schematic Arrangement of Test Instrumentation
Appendix	B	-	Reduced Leakage Rate Data
Appendix	с	-	Weight of Containment Air and Average Containment Temperature Versus Time
Appendix	D	-	Computer Printout
Appendix	E	-	Summary of Measured Data
Appendix	F	-	Type B and C Leakage Rate Histories

1.0 SYNOPSIS

The Davis-Besse Nuclear Power Station Unit No. 1 reactor containment building was subjected to a periodic integrated leak rate test during the period of December 9, 1984 to December 10, 1984. The purpose of this test was to demonstrate the acceptability of the building leakage rate at an internal pressure of 38 psig (P). Testing was performed in conformance with the requirements of 10CFR50 Appendix J, ANSI N45.4-1972, Bechtel Topical Report BN-TOP-1, and the Davis-Besse Technical Specifications.

The Mass Point method of analysis resulted in a measured leakage rate of 0.000% by weight per day at 39 psig. The leakage rate at the upper bound of the 95% confidence interval was 0.003% by weight per day.

Utilizing the Total Time method of analysis, the measured leakage rate was found to be -0.019% by weight per day and 0.087% by weight per day at the upper bound of the 95% confidence interval at the 39 psig pressure level. The mean of the measured leakage rates based on the total time calculations for the last five hours of the test was -0.002% by weight per day. All total time analyses are below the allowable leakage rate of 0.375% by weight per day and meet the criteria set forth in Bechtel Topical Report BN-TOP-1 for conduct of a short duration integrated leakage rate test.

An equivalent leakage rate reduction of 0.175% by weight per day was achieved by performing Type B and Type C tests prior to the integrated leakage rate test (see Section 8.3). Therefore, the 'as found' reactor containment integrated leakage rate is the measured leakage rate of 0.003% by weight per day plus the 0.175% by weight per day or 0.178% by weight per day using the Mass Point method of analysis. Utilizing the Total Time method, the 'as found' leakage rate is the measured upper confidence leakage rate of 0.087% by weight per day plus the 0.175% by weight per day or 0.262% by weight per day. These values are well below the allowable 'as found' leakage rate of 0.375% by weight per day (see Appendix F).

The supplemental instrumentation verification test at P demonstrated an agreement between measured reactor containment building integrated leakage rates of 1% using the Mass Point method and 4% using the Total Time Method which are within the 25% requirement of 10CFE50, Appendix J, Section III A.3.b.

Testing was performed by Toledo Edison with the technical assistance of Gilbert/Commonwealth, Inc. Procedural and calculational methods were witnessed by Nuclear Regulatory Commission personnel.

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2.0 INTRODUCTION

The objective of the integrated leakage rate test was the verification of the overall leak tightness of the reactor containment building at the calculated design basis accident pressure of 38 psig. The allowable leakage is defined by the design basis accident applied in the safety analysis in accordance with site exposure guidelines specified by 10CFR100. For Davis-Besse, the maximum allowable integrated leak rate at the design basis accident pressure of 38 psig (P_a) is 0.5% by weight per day (L_a).

Testing was performed in accordance with the procedural requirements as stated in Davis-Besse Nuclear Power Station Unit No. 1 Surveillance Procedure ST-5061.01. This procedure was approved by the station superintendent prior to commencement of the test.

Leakage rate testing was accomplished at the pressure level of 39 psig for a period of 15.75 hours. The 15.75 hour period was followed by a one hour stabilization period and four hour supplemental test for a verification of test instrumentation.

3.0 GENERAL, TECHNICAL, AND TEST DATA

3.1 GENERAL DATA

Owner:

Docket No .:

Lccation:

Containment Type:

Date Test Completed:

3.2 TECHNICAL DATA

Containment Net Free Volume:

Design Pressure:

Design Temperature:

Calculated Accident Peak Pressure:

Calculated Accident Peak Temperature:

3.3 TEST DATA

Test Method:

Data Analysis:

Test Pressure:

Max Allowable Leakage Rate (L_)

Measured Leakage Rate:

Mass Point Total Time

Measured Leakage Rate at UCL:

Mass Point Total Time Toledo Edison Company 50-346 Oak Harbor, Ohio Steel

December 10, 1984

2.834 x 10^6 cubic feet 36 psig/40 psig (max) $265^{\circ}F$

38 psig

255°F

Absolute

Mass Point and Total Time 39 psig

0.500 wt & per day

0.000 wt * per day -0.019 wt * per day

0.003 wt % per day 0.087 wt % per day

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Suppremental	lest flow Rate:	0.3968	per	day	
Supplemental Leak Rate:	Test Measured				
Mass Point Total Time		0.391 0.397	wt % wt %	per per	day day
Supplemental Agreement:	Test and L am		*		
Mass Point		18			
Total Time		4*			

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4.0 ACCEPTANCE CRITERIA

4.1 TECHNICAL SPECIFICATION ACCEPTANCE CRITERIA

Acceptance criteria established prior to the test, and as specified by 10CFR50, Appendix J, ANSI N45.4-1972 and the Davis-Besse Nuclear Power Station Unit No. 1 Technical Specifications are as follows:

5

 The measured leakage rate (L) at the calculated design basis accident pressure of 38 psig (P) shall be less than 75% of the maximum allowable leakage rate (L) specified at 0.5% by weight of the building atmosphere per day. The acceptance criteria is determined as follows:

> $L_a = 0.5 \frac{1}{day}$ 0.75 $L_a = 0.375 \frac{1}{day}$

2. The test instrumentation shall be verified by means of a supplemental test. Agreement between the containment leakage measured during the Type A test and the containment leakage measured during the supplemental test shall be within 25% of L.

4.2 SHORT DURATION TESTING ACCEPTANCE CRITERIA

In addition to the acceptance criteria mentioned above, the following short duration testing acceptance criteria contained in Bechtel Topical Report BN-TOP-1, Revision 1 dated November 1, 1972 was used:

- The trend report based on total time calculations shall indicate that the magnitude of the calculated leak rate is tending to stabilize at a value less than the maximum allowable leak rate (L_a).
- The end of test upper 95% confidence limit for the calculated leak rate based on total time calculations shall be less than the maximum allowable leak rate.
- 3. The mean of the measured leak rates based on total time calculations over the last five hours of test or last 20 data points, whichever provides the most data, shall be less than the maximum allowable leak rate.
- At least 20 data points shall be provided for statistical analysis.

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5.0 TEST INSTRUMENTATION

5.1 SUMMARY OF INSTRUMENTS

Test instruments employed are described, by system, in the following subsections.

5.1.1 Temperature Indicating System

Resistance Temperature Detectors

Quantity Manufacturer Type Range, ^OF (calibrated) Accuracy, ^OF Sensitivity, ^OF

20 Burns 100 ohm platinum 32 - 100 +0.5 +0.5

5.1.2 Dawpoint Indicating System

Dewcell Elements

Quantity Manufacturer Type Range, °F Accuracy, °F Sensitivity, °F Repeatability, °F

5 EG&G Model 660 -58 to 212 +0.54 +0.01 +0.1

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5.1.3 Pressure Monitoring System

Precision Pressure Gauges

Quantity Manufacturer Type

Range, psia Accuracy, psia

Sensitivity, psia Repeatability, psia

2 Mensor Dual Quartz Manometer 0 - 60 +0.01% of reading plus 0.002% full scale +0.005 psia +0.005 psia

6

5.1.4 Supplemental Test Flow Monitoring System

Mass Flow Meter

Quantity Manufacturer Type Range, scfm Accuracy

2 Brooks Model 5812 0 - 14 +1% of full scale

5.2 SCHEMATIC ARRANGEMENT

The arrangement of the four measuring systems summarized in Section 5.1 is depicted in Appendix A.

Drybulb tamperature sensors were placed throughout the reactor containment vessel volume to permit monitoring of internal temperature variations at 20 locations. Dewpoint temperature sensors were placed at five locations to permit monitoring of the reactor containment partial pressure of water vapor. A temperature modeling survey was performed after the sensors were installed which verified that the sensors were monitoring representative volumes and that there were no large areas of temperature variation.

5.3 CALIBRATION CHECKS

Temperature, dewpoint, and pressure measuring systems were checked for calibration before the test as recommended by ANSI N45.4-1972, Section 6.2 and 6.3. The results of the calibration checks are on file at Davis-Besse Nuclear Power Station Unit No. 1. The supplemental test at 38 psig confirmed the instrumentation acceptability.

5.4 INSTRUMENTATION PERFORMANCE

During the pressurization phase, one dewpoint instrument exhibited abnormal behavior and was not used for the test. The volume weighting fraction assigned to the defective dewpoint instrument was then assigned to the other dewpoint instrument on the same elevation. The remaining five dewpoint instruments, 20 RTDs, two precision pressure gauges, and two mass flowmeters performed satisfactorily throughout the performance of the integrated leak rate test and provided more than adequate coverage of containment.

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5.5 VOLUME WEIGHTING FACTORS

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Weighting factors were assigned to each operable drybulb temperature sensor and dewpoint temperature sensor based on the calculated volume of the reactor containment building each sensing device monitored. Drybulb and dewpoint temperature sensors elevation and weighting factors for the test were as follows:

8

Elevation/ Azimuth	Temperature Element	Weighting Factor
782/0°	TE-5056A	.056
782/1800	TE-5056B	.056
760/270°	TE-5056C	.056
760/90°	TE-5056D	.056
739/0°	TE-5056E	.056
739/1800	TE-5056F	.056
714/2700	TE-5056G	.056
714/90	TE-5056H	.056
689/00	TE-50561	.056
689/180	TE-5056J	.056
664/270	TE-5056K	.056
664/90°	TE-5056L	.056
634/0°	TE-5056M	.051
634/180	TE-5056N	.051
603/270°	TE-50560	.051
603/90	TE-5056P	.051
590/270°	TE-5056S	.031
590/90	TE-5056T	.031
584/0	TE-50560	.031
584/180	TE-5056R	.031
760/90°	TE-5057D	. 334
689/0°	TE-50571	.169
689/180°	TE-5057J	.169
603/270°	TE-50570	164
603/90°	TE-5057P	.164

5.6 SYSTEM ERROR ANALYSIS

Systematic error, in this test, is induced by the operation of the temperaure indicating system, dewpoint indicating system, and the pressure indicating system.

Justification of instrumentation selection was accomplished using manufacturer's sensitivity and repeatability tolerances, stated in Section 5.1, by computing the instrumentation selection guide (ISG) formula.

Containment leakage determined by the Absolute Method requires accurate measurement of small changes in containment pressure with suitable corrections for temperature and water vapor. Since the Absolute Method utilizes the change in a reading (i.e., pressure and temperature) to calculate leak rate, the repeatability, sensitivity, and readability of the instrument system is of more concern than the accuracy. To perform the ISG calculation, the sensitivity error of the sensor and the repeatability error of the measurement system must be used.

Sensitivity is defined as 'the capability of a sensor to respond to change.' Sensitivity is usually a function of the system measuring the sensor output. When the sensor energy state is raised or lowered an amount equal to the smallest value which the entire system will process, a change of indication will occur. To determine sensitivity for ILRT sensors, it is necessary to analyze the smallest value of the analog sensor output which will cause a one digit change in the digital display.

Repeatability is defined as 'the capability of the measurement system to reproduce a given reading from a constant source.'

Utilizing the methods, techniques, and assumptions in Appendix G to ANS 56.8-1981, the ISG formula was computed for the Absolute Method as follows:

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- 1. Conditions:
 - L = 0.5%/day
 - P = 53.7 psia
 - T = 525°R arybulb
 - T_{dp} = 49°F dewpoint
 - t = 15.75 hours

2.

Total Absolute Pressure: ep

Range = 0 - 60 psia

No. of sensors - 2

Sensor sensitivity error $(E_p) = \pm 0.005$ psia Measurement system error $\binom{\varepsilon}{p} = \pm 0.005$ psia

$$e_{p} = \pm \left[\left(E_{p} \right)^{2} + \left(\epsilon_{p} \right)^{2} \right]^{1/2} / [no. of sensors]^{1/2}$$

$$e_{p} = \left[\left(5 \times 10^{-3} \right)^{2} + \left(5 \times 10^{-3} \right)^{2} \right]^{1/2} / [2]^{1/2}$$

$$e_{p} = \pm 5 \times 10^{-3} \text{ psia}^{1/2}$$

3. Water Vapor Pressure: e

No. of sensors = 5 Sensor sensitivity error (E) = +0.01°F Measurement system error (ϵ), excluding sensor pv = +0.1°F

At a dewpoint temperature of 49°F, the equivalent water vapor pressure change (as determined from steam tables) is 0.0065 psia/°F

 $E_{pv} = \pm 0.01^{\circ} F (0.0065 \text{ psia}^{\circ} F)$ $E_{pv} = 6.5 \times 10^{-5}$ psia $\epsilon_{\rm DV} = \pm 0.1^{\circ} F (0.0065 \text{ psia}/^{\circ} F)$ $\epsilon_{\rm pv} = 6.5 \times 10^{-4} \text{ psia}$ $e_{pv} = \pm \left[(E_{pv})^2 + (\epsilon_{pv})^2 \right]^{1/2} / [no. of sensors]^{1/2}$ $e_{pv} = \pm \left[(6.5 \times 10^{-5})^2 + (6.5 \times 10^{-4})^2 \right]^{1/2} / (5)^{1/2}$ $e_{pv} = \pm 2.92 \times 10^{-4} \text{ psia}$

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4. Temperature: em

No. of sensors = 20

Sensor sensitivity error $(E_T) = \pm 0.5^{\circ}F = \pm 0.5^{\circ}R$ Measurement system error $(\epsilon_T) = \pm 0.1^{\circ}F = \pm 0.1^{\circ}R$

 $e_{T} = \pm \left[(E_{T})^{2} + (e_{T})^{2} \right]^{1/2} / [\text{no. of sensors}]^{1/2}$ $e_{T} = \pm \left[(0.5)^{2} + (0.1)^{2} \right]^{1/2} / [20]^{1/2}$ $e_{T} = \pm 0.114^{0} R$

5. Instrument Selection Guide (ISG):

ISG =
$$\pm \frac{2400}{t} \left[2\left(\frac{p}{p}\right)^2 + 2\left(\frac{e}{pv}\right)^2 + 2\left(\frac{e}{T}\right)^2 \right] \frac{1}{2}$$

$$ISG = \frac{+2400}{15.75} \left[2\left(\frac{5 \times 10^{-3}}{53.7}\right)^2 + 2\left(\frac{2.92 \times 10^{-4}}{53.7}\right)^2 + 2\left(\frac{0.114}{525}\right)^2 \right] \frac{1}{2}$$

$$ISG = \frac{+152.4}{1.734 \times 10^{-8}} + 5.914 \times 10^{-11} + 9.430 \times 10^{-8} \right] \frac{1}{2}$$

$$ISG = \frac{+0.0518}{day}$$

The ISG value does not exceed 0.25 L (0.125%/day) and it is therefore concluded that the instrumentation selected was acceptable for use in determining the reactor containment integrated leakage rate.

5.7 SUPPLEMENTAL VERIFICATION

In addition to the calibration checks described in Section 5.3, test instrumentation operation was verified by a supplemental test subsequent to the completion of the 15.75 hour leakage rate test. This test consisted of imposing a known calibrated leakage rate on the reactor containment building. After the flow rate was established, it was not altered for the duration of the test.

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During the supplemental test, the measured leakage rate was:

$$L_c = L_v' + L_o$$

Where:

- L = Measured composite leakage rate consisting of the reactor containment building leakage rate plus the imposed leakage rate
- L = Imposed leakage rate
- L' = Leakage rate of the reactor containment building during the supplemental test phase

Rearranging the above equation,

$$L_v' = L_c - L_o$$

The reactor containment building leakage during the supplemental test can be calculated by subtracting the known superimposed leakage rate from the measured composite leakage rate.

The reactor containment building leakage rate during the supplemental test (L') was then compared to the measured reactor containment building leakage rate during the preceding 15.75 hour test (L) to determine instrumentation acceptability. Instrumentation is considered acceptable if the difference between the two building leakage rates is within 25% of the maximum allowable leakage rate (L).

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6.0 TEST PROCEDURE

6.1 PREREQUISITES

Prior to commencement of reactor containment building pressurization, the following prerequisites were satisfied:

- Proper operation of all test instrumentation was verified.
- All reactor containment building isolation valves were closed using the normal mode of operation. All associated system valves were placed in post-accident positions.
- 3. Equipment within the reactor containment building, subject to damage, was protected from external differential pressures.
- Porticus of fluid systems, which under post-accident conditions become extensions of the containment boundary, were drained and vented.
- Type B and C testing was completed with a leakage value less than 0.6 L.
- 6. Containment pressurization system was operational.
- Potential pressure sources were removed or isolated from the containment.
- 8. Containment recirculation fans were in operation.
- 9. A general inspection of the accessible interior and exterior areas of the containment was completed.

6.2 GENERAL DISCUSSION

Following the satisfaction of the prerequisites stated in Section 6.1, the reactor containment building pressurization was initiated at a rate of approximately 2.2 psi per hour. After the containment was stabilized, leak rate testing was initiated at the 39.0 psig pressure level. For the duration of the 15.75 hour leak test and the four hour supplemental test, average internal containment temperature remained within a band of +0.6°F.

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During the test, the following occurred at 15 minute intervals (see Appendix B and Appendix E):

- Readings indicated by the precision pressure gauges were recorded and entered into the computer. The computer then computed the average pressure in psia.
- 2. Readings indicated by the 20 RTDs were recorded and entered into the computer. The computer program calculated the average containment building drybulb temperature by use of a weighting factor that was assigned to each RTD. This value was subsequently converted to degrees Rankine for use in the ideal gas law equation to calculate containment building weight of air.
- 3. Readings indicated by the five dewpoint temperature sensors were recorded and entered into the computer. The computer program then calculated the average containment dewpoint temperature by use of a weighting factor assigned to each sensor. This weighted average dewpoint temperature was then converted to a partial pressure of water vapor.

The use of water vapor pressure (P), temperature (T), and the total pressure (P) is described in more detail in Section 7.1. All original data is on file at Davis-Besse Nuclear Power Station Unit No. 1.

Data was entered into an Atrona attache microcomputer located in the plant computer room. The ILRT computer program utilized for the test had been previously checked with sample data of known results and certified prior to the test at Davis-Besse Unit No. 1. The computer program then calculated the following at 15 minute intervals:

- . Total weight of containment air.
- Mass point least squares fit leakage rate.
- 3. Mass point 95% upper confidence level leakage rate.
- 4. Observed total time leakage rate.
- 5. Total time mean leakage rate.
- 6. Total time least squares fit leakage rate.
- 7. Total time 95% upper confidence level leakage rate.

A plot of weighted average containment temperature, containment total pressure, containment average dewpoint temperature, and weight of air was performed for each 15 minute data set (see Appendix C).

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Immediately following the 15.75 hour leak test, a superimposed leakage rate was established for a one hour stabilization period and four hour test period. During this time, temperature, pressure, and vapor pressure were monitored as described above.

6.3 TEST PERFORMANCE

6.3.1 Pressurization and Stabilization Phase

Pressurization of the reactor containment building was started on December 8, 1984 at 2145. The pressurization rate was approximately 2.2 psi per hour. When containment internal pressure reached 39.0 psig at approximately 1630 on December 9, pressurization was secured. By 2100 on December 9, temperature stabilization criteria had been met and leakage rate data recording, reduction, and analysis began.

6.3.2 Integrated Leak Rate Testing Phase

Fifteen minute frequency test data showed that stable conditions existed within the containment. Test duration for the ILRT was extended to 15.75 hours to ensure that a stable leakage rate had been established prior to the start of the superimposed test. For the 15.75 hour period from 2100 on December 9 to 1245 on December 10, an acceptable leakage rate of 0.000%/day with an associated 95% confidence interval of 0.003% by weight per day was obtained using the Mass Point method of analysis. Utilizing the Total Time method, the measured leakage rate was -0.019%/day and 0.087% by weight per day at the upper bound of the 95% confidence interval.

6.3.3 Supplemental Leakage Rate Test Phase

Following completion of the 15.75 hour integrated leak rate test, a leakage rate of 28.64 scfm was imposed on the containment building through two mass flowmeters at 1300 on December 10. After a one hour stablization period, leakage rate data was again collected at 15 minute intervals for a period of four hours. With an imposed leak rate of 0.396% per day, a measured composite leakage rate of 0.391% per day was obtained using the Mass Point method. This results in a containment building leakage rate agreement of 1% of L with the results of the 15.75 hour test. Using the Total Time method of analysis, the measured composite leakage rate was 0.397% per day, resulting in an agreement of 4% of L with the results of the 15.75 hour test. These values are both well within the acceptance limit of 25% of L

6.3.4 Depressurization Phase

After all required data was obtained and evaluated, containment building depressurization to 0 psig was started. A post test inspection of the reactor containment building interior revealed no unusual findings.

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7.0 METHODS OF ANALYSIS

7.1 GENERAL DISCUSSION

The Absolute Method of leakage rate determination was employed during testing at the 38.0 psig pressure level. The Gilbert/Commonwealth, Inc. ILRT computer code calculates the percent per day leakage rate for the mass point and total time methods.

7.1.1 Mass Point Analysis

The mass point method of computing leakage rates uses the following ideal gas law equation to calculate the weight of air inside containment for each 15 minute interval:

$$W = \frac{144 \text{ PV}}{\text{RT}} = \frac{\text{KP}}{\text{T}}$$

Where:

W = Mass of air inside containment, 1bm K = 144 V/R = 7.64941 x 10⁶ $\frac{1bm - {}^{O}R - in.^2}{1bf}$ P = Partial pressure of air, psia T = Average internal containment temperature, ${}^{O}R$ V = 2.834 x 10⁶ ft³

$$R = 53.35 \frac{1bf - ft}{1bm - R}$$

The partial pressure of air, P, is calculated as follows:

$$P = P_T - P_{WV}$$

Where:

- P_T = True corrected pressure by converting pressure gauge readings and averaging, psia
- P = Partial pressure of water vapor determined by averaging the five dewpoint temperatures and converting to partial pressure of water vapor, psia

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The average internal containment temperature, T, is calculated as follows:

T = Sum of the products of each RTD x assigned weighting factor + 459.69°R

The weight of air is plotted versus time for the 15.75 hour test and for the four hour supplemental test. The Gilbert/Commonwealth, Inc. ILRT computer code fits the locus of these points to a straight line using a linear least squares fit. The equation of the linear least squares fit line is of the form $W = A_t + B$, where A is the slope in lbm per hour and B is the initial weight at time zero. The least squares parameters are calculated as follows:

$$A = \frac{N (\Sigma_{i} W_{i}) - (\Sigma_{i}) (\Sigma_{i})}{S_{xx}}$$
$$B = \frac{(\Sigma_{i}^{2}) (\Sigma_{i}) - (\Sigma_{i}) (\Sigma_{i} W_{i})}{S_{xx}}$$

Where:

$$s_{xx} = N (Et_i^2) - (Et_i)^2$$

The weight percent leakage per day can then be determined from the following equation:

$$L_{am} = \frac{-2400 \text{ A}}{\text{B}}$$

where the negative sign is used since A is a negative slope to express the leakage rate as a positive quantity.

7.1.2 Total Time Analysis

The total time method utilizes the following equation to determine the leakage rate of the reactor containment building:

$$L = \frac{2400}{t} \left[1 - \frac{T_1 P_2}{T_2 P_1} \right]$$

Where:

Measured leak rate in weight percent per day

t

L

- = Time interval, in hours, between measurements
- T₁, T₂ = Average internal containment temperature, ^OR, at the beginning and the end of the test interval respectively.
- P1, P2 = Average containment pressure (corrected for water vapor pressure) at the beginning and end of the test interval respectively.

The mean total time leakage rate is derived from the above individual total time calculations. The equation for the mean leakage rate is in the form:

$$\overline{L} = \frac{\sum_{i} L_{i}}{n}$$

Where:

L_i = Individual total time leakage rates

n = Number of total time leakage rates

The individual leakage rates are then plotted against time for the duration of the 15.75 hour test. The Gilbert/Commonwealth, Inc. ILRT computer code fits the locus of these points to a straight line using a linear least squares fit. The equation is of the form $L = L + L_t$ where L is the slope in percent per hour and L is the initial leakage rate at time zero. The least squares parameters are calculated as follows:

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$$L_{0} = \frac{\Sigma L_{i}^{2} \Sigma L_{i}^{2} - \Sigma L_{i}^{2} \Sigma L_{i}^{2}}{S_{xx}}$$

$$L_{1} = \frac{N \Sigma L_{i}^{2} \Sigma L_{i}^{2} - \Sigma L_{i}^{2} \Sigma L_{i}^{2}}{S_{xx}}$$

Where:

 $S_{xx} = N Et_i^2 - (Et_i)^2$

7.2 STATISTICAL EVALUATION

7.2.1 General

After performing the least squares fit, the ILRT computer code calculates the following statistical parameters:

- Limits of the 95% confidence interval for the mass point leakage rate (C_u).
- 2. Limits of the 95% confidence interval for the total time leakage rate (C_{L}) .

These statistical parameters are then used to determine that the measured leakage rate plus the 95 UCL meet the acceptance criteria.

7.2.2 Mass Point Confidence

The upper 95% confidence limit for the mass point leakage rate is calculated as follows:

$$C_{M} = 2400 t_{05} (S_{A}/B)$$

Where:

- C_M = Upper 95% confidence limit
- tos = Student's t distribution with N-2 degrees of freedom
- S_A = Standard deviation of the slope of the least squares
 fit line
- B = Intercept of the least squares fit line

The standard deviation of the slope of the least squares fit line (S_A) is calculated as follows:

$$\mathbf{x} = \frac{S(N)^{1/2}}{(N(\Sigma t_i^2) - (\Sigma t_i^2)^2)^{1/2}}$$

Where:

S

S = Common standard deviation of the weights from the least squares fit line

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- N = Number of data points
- t, = Time interval of the ith data point

The common standard deviation (S) is defined by:

$$s = \left[\frac{\Sigma(W_i - W)^2}{N-2}\right] \frac{1}{2}$$

Where:

W, = Observed mass of air

W = Least squares calculated mass of air

The ILRT computer code calculates an upper 95% confidence leakage rate as follows:

UCL = L + 2400 t 95 (SA/B)

This UCL value is then used to determine that the measured leakage rate at the upper 95% confidence limit meets the acceptance criteria.

7.2.3 Total Time Confidence

The 95% confidence limit for the total time leakage rate is calculated as follows:

$$C_{L} = t_{95} Se \left[1 + \frac{1}{n} + \frac{(t - \overline{t})^{2}}{\Sigma(t_{1} - t)^{2}} \right] \frac{1}{2}$$

Where:

t = Total time interval

$$\bar{t} = \frac{\Sigma t_i}{D}$$

t = Time interval for each data point

n = Number of individual total time leakage rates

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20

8.0 DISCUSSION OF RESULTS

8.1 RESULTS AT P

8.1.1 Mass Point Method of Analysis

Data obtained during the leak rate test at P indicated the following changes (highest to lowest) during the 15.75 hour test.

Variable	Maximum Change
P _T	0.104 psia
Pwv	0.004 psia
T	1.07°F

The method used in calculating the Mass Point leakage rate is described in Section 7.1.1. The results of this calculation is a mass point leakage rate of 0.000%/day (see Appendix D).

The 95% confidence limit associated with this leakage rate is 0.003% per day. Thus, the leakage rate at the upper bound of the 95% confidence level becomes:

UCL = 0.000 + 0.003

UCL = 0.003%/day

Additional leakage rates must be applied to the measured leakage rate at the upper 95% confidence level to account for changes in the net free volume of the containment due to water level changes, penetration paths not exposed to the test pressure, and for nitrogen additions to the electrical penetrations during the test. Penetration paths not exposed to the test pressure and the corresponding leakage rates based on analysis of minimum pathway local leakage rate testing are as follows.

System	Isolation Valve	Type C Leakage (sccm)
ILRT Pressurization	CV-343	119
Ctmt Spray	CS-33, CS-17	0
Ctmt Spray	CS-36, CS-18	0
Seal Return	MU-59A-D, MU-38	0
ILRT Pressure Sensing	CV-5094	0

The total applicable local leakage rate is 119 sccm which is equivalent to 6 x 10^{-5} %/day. The addition of this negligible value does not change the results of the integrated leakage rate test.

Water level changes in the containment during the 15.75 hour integrated leakage rate test are summarized below:

Containment Sump Water Level:

1500	12-08-84	0.35'
1325	12-10-84	0.61'

Pressurizer and Hot Leg Level:

2100	12-09-84	268*	
1800	12-10-84	263*	

During the test, no makeup water was introduced into the reactor coolant system. Therefore, the volume change associated with the change in pressurizer/hot leg water level showed an increase in the net free volume of 44 cubic feet in 21 hours or 50.3 cubic feet extrapolated out to 24 hours. This corresponds to a reduction in the measured containment leakage rate of 0.0017%/day. However, it is conservatively assumed that the water level decrease was not lost out of containment and no change in net free volume occurred.

The level change in the containment sump showed a decrease in the net free volume of 12.5 cubic feet in 15.75 hours or 19 cubic feet when extrapolated out to 24 hours. This corresponds to an additional leakage rate of 0.00067%/day.

The nitrogen addition to the electrical penetrations is conservatively assumed to have gone into containment. The amount of nitrogen used was measured to be 8.472 cubic feet from 2100 on December 9 to 1400 on December 10. This is equivalent to 11.96 cubic feet for a 24 hour period. This corresponds to an additional leakage rate of 0.0001%/day.

The addition of these very small leakage rates due to water level changes, Type C penalties, and nitrogen additions have no significant effect on the results of the integrated leakage rate test.

The measured leakage rate and the measured leakage rate at the upper bound of the 95% confidence level are well below the acceptance criteria of 0.375%/day (0.75 L).

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8.1.2 Total Time Method of Analysis

The method used in calculating the total time leakage rates is defined in Section 7.1.2. The results of these calculations are as follows:

- The mer gred total time leakage rate for the 15.75 hour test was -0.019% by weight per day.
- The 95% confidence limit associated with this leakage rate is 0.106% per day. Thus, the leakage rate at the upper bound of the 95% confidence level becomes:

UCL = -0.019 + 0.106 $UCL = 0.087 \frac{1}{day}$

 The mean of the measured leakage rates based on the last five hours of the test was -0.002 percent by weight per day.

The total time measured leakage rate, the measured leakage rate at the upper bound of the 95% confidence level and the mean of the measured leakage rates based on the last five hours of testing are below the acceptance criteria of 0.375%/day.

Therefore, the reactor containment building leakage rate, based on both the mass point method and total time method of analysis, at the calculated design basis accident pressure (P_a) of 38.0 psig is acceptable.

8.2 SUPPLEMENTAL TEST PESULTS

After conclusion of the 15.75 hour test at 38.0 psig (P), the mass flowmeters were placed in service and a flow rate of 28.64 scfm was established. This flow rate is equivalent to a leakage rate of 0.396*/day. After the flow rate was established, it was not altered for the duration of the supplemental test. The measured leakage rate (L) during the supplemental test was calculated to be 0.391*/day using the Mass Point muthod of analysis and 0.397*/day using the Total Time Method.

The building leakage rate during the supplemental test is then determined as follows:

	Ma	lass Point			Total Time		
r'	-	L _c - L _o	r^,	•	L _c - L _o		
r^,	-	0.391 - 0.396	L,'	1	0.397 - 0.396		
r,	-	-0.005%/day	r".	-	0.001%/day		

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Comparing this leakage rate with the building leakage rate measured during the 15.75 hour test yields the following:

Mass Point =
$$\left|\frac{L_{am} - L_{v'}}{L_{a}}\right| = \left|\frac{0.000 - (-0.005)}{0.000}\right| = .000$$

Total Time = $\left|\frac{L_{am} - L_{v'}}{L_{a}}\right| = \left|\frac{-0.019 - 0.001}{0.5}\right| = .004$

The building leakage rates agree within 1% of L using the Mass Point method and 4% using Total Time which are well below the acceptance criteria of 25%.

Using the formulation of ANS 56.8-1981,

 $(L_{o} + L_{am} - 0.25 L_{a}) \leq L_{c} \leq (L_{o} + L_{am} + 0.25 L_{a})$ (0.396 + 0 - 0.125) $\leq L_{c} \leq (0.396 + 0 + 0.125)$

0.271 <L <0.521

Since L was measured to be 0.391%/day, this value falls within the acceptable range of 0.271% to 0.521% per day. Therefore, the acceptability of the test instrumentation is considered to have been verified.

8.3 AS FOUND ANALYSIS

To determine the as-found containment leakage rate, an analysis was performed to evaluate any leakage savings from repairs of containment isolation barriers. Leakage savings are realized when containment isolation barrier repairs result in a lower minimum pathway leakage which is the minimum leakage value that can be quantified through a penetration leakage path.

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Repairs were performed on eight penetrations during the 1984 outage with only two resulting in a minimum pathway leakage (MPL) savings. The results of these eight penetrations (in sccm) are listed below.

Penet.	As Found	As Left	MPL Pre-Maint	MPL Post-Maint	Leakage Savings
3	(1)	423	212	212	0
33	700,000	504	350,000	252	349,748
34	371	1188	186	594	0
41	34,400	. 0		0	368
	368	368	368		-
42A	11,814	280			
	89	89	89	89	0
44A	(2)	1869			
만보험	775	775	775	775	0
81	(3)	1743	872	872	0

 Valves tested in parallel, penetration would not pressurize, maintenance performed on only one.valve.

(2) Valves tested in series, one valve would not pressurize, maintenance performed on only one valve.

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(3) Personnel lock would not pressurize, maintenance performed on one handwheel shaft seal.

The leakage savings due to performing Type B and C tests prior to the Type A test is 350,116 sccm. This value is equivalent to 0.175% by weight per day.

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9.0 REFERENCES

- Surveillance Test ST 5061.01 Containment Integrated Leak Rate Test.
- Davis-Besse Nuclear Power Station Unit No. 1 Updated Safety Analysis Report.
- 3. Code of Federal Regulations, Title 10, Part 50, Appendix J.
- ANSI N45.4-1972, Leakage Rate Testing of Containment Structures for Nuclear Reactors, American Nuclear Society, March 16, 1972.
- ANS-56.8-1981, Containment System Leakage Testing Requirements, American Nuclear Society.
- 6. ILRT Computer Code, Gilbert/Commonwealth, Inc.
- 7. Steam Tables, American Society of Mechanical Engineers, 1967.
- BN-TOP-1, Testing Criteria for Integrated Leakage Rate Testing of Primary Containment Structures for Nuclear Power Plants, Revision 1, November 1, 1972.

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APPENDICES

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10

APPENDIX A

SCHEMATIC ARRANGEMENT OF TEST INSTRUMENTATION

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APPENDIX A SCHEMATIC ARRANGEMENT OF TEST INSTRUMENTATION

TAG NUMBERS

TE-5056T

PI-5094

PT-5094A & B

FT-4912A & B

TE-5057 D,I,J,

TE-5056A thru

O,P

APPENDIX B

REDUCED TEST DATA

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APPENDIX B

REDUCED TEST DATA

Date	Time	PAVG	PWV	TAVG	Weight
12-09-84	2100	53.778	.171	65.52	780752
	2115	53.773	.172	65.49	780721
	2130	53.77	.172	65.45	780735
	2145	53.766	.172	65.41	7.80735
	2200	53.764	.172	65.37	780759
	2215	53.76	.172	65.35	780738
	2230	53.758	.172	65.31	780761
	2245	53.755	.172	65.29	780751
	2300	53.753	.172	65.26	780757
승규가 있는 것이 없다.	2315	53.751	.172	65.23	780776
	2330	53.749	.173	65.22	780746
	2345	53.746	.172	65.20	780756
12-10-84	0000	53.744	.172	65.19	780747
	0015	53.743	.173	65.16	780756
	0030	53.741	.172	65.13	780782
	0045	53.739	.173	65.10	780783
	0100	53.738	.173	65.10	780776
	0115	53.737	.172	65.08	780790
	0130	53.736	.173	65.06	780796
	0145	53.734	.173	65.05	780793
	0200	53.732	.173	65.04	780781
	0215	53.731	.172	65.03	780786
	0230	53.731	.172	65.02	780783
	0245	53.729	.172	65.00	780797
	0300	53.728	.172	64.98	780807
	0315	53.727	.173	64.97	780791
	0330	53.725	.173	64.97	780763
	0345	53.723	.173	64.95	780771
	0400	53.721	.173	64.92	780795
	0415	53.719	.173	64.90	780785
	0430	53.716	.174	64.90	780729
	0445	53.715	.174	64.87	780759
	0500	53.712	.173	64.85	780762
	0515	53.71	.174	64.82	780771
	0530	53.709	.173	64.80	780779
	0545	53.706	.173	64.77	780789
	0600	53.705	.173	64.77	780772
	0615	53.703	.174	64.75	780772
	0630	53.702	.174	64.73	780775
	0645	53.699	.174	64.71	780758

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APPENDIX B (Cont'd)

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Date	Time	PAVG	PWV	TAVG	Weight
12-10-84	0700	53.697	.173	64.69	780785
	0715	53.696	.174	64.68	780775
	0730	53.695	.173	64.66	780786
	0745	53.693	.174	64.66	780759
	0800	53.692	.174	64.63	780784
	0815	53.69	.174	64.64	780742
	0830	53.689	.174	64.62	780745
	0845	53.687	.174	64.60	780752
	0900	53.686	.174	64.58	780769
	0915	53.685	.174	64.56	780785
	0930	53.684	.175	64.55	780770
	0945	53.682	-174	64.55	780753
	1000	53.681	.174	64.53	780764
	1015	53.679	.175	64.51	780765
	1030	53.679	.175	64.51	780771
	1045	53.678	.175	64.49	780776
	1100	53.677	-174	64.48	780780
	1115	53.676	.175	64.47	780773
	1130	53.675	.174	64.47	780762
	1145	53.673	.175	64.47	780726
	1200	53.672	.176	64.45	780752
	1215	53.672	.175	64.45	780737
	1230	53.670	.175	64.42	780761
	1245	53.669	.175	64.43	780724
VERIFICATIO	ON TEST				
	1400	53.654	.175	64.38	780596
	1415	53.650	.176	64.36	780565
	1430	53.648	.175	64.35	780535
	1445	53.645	.176	64.34	780511
	1500	53.642	.175	64.35	780470
	1515	53.639	.175	64.33	780431
	1530	53.636	.176	64.31	780405
	1545	53.633	.176	64.31	780379
	1600	53.63	.176	64.31	780335
	1615	53.627	.176	64.32	780280
	1630	53.624	.175	64.29	780271
	1645	53.620	.175	64.28	780239
	1700	53.618	.175	64.27	780231
	1715	53.615	.175	64.28	780168
	1730	5.612	.175	54.26	780163
	1745	53.609	.175	64.26	780113
	1800	53.606	.175	64.24	780101

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APPENDIX C

LEAKAGE RATE TEST GRAPHS

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APPENDIX C

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WEIGHT OF CONTAINMENT AIR AND AVERAGE CONTAINMENT TEMPERATURE VERSUS TIME



APPENDIX D

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COMPUTER RESULTS

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APPENDIX D

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COMPUTER RESULTS

1.	Mass Point Results
	<pre>A = Slope of least squares line (lbs/hr) is 0.07</pre>
	B = Intercept of least squares line (lbs) is 780765.5
	L = Measured leak rate is 0.000%/day
	UCL = 95% upper confidence leakage rate is 0.003%/day
2.	Total Time Results
	A = Slope of least squares line (%/day/hr) is 0.021
	B = Intercept of least squares line (%/day) is -2.479
	L_{am} = Measured leak rate is -0.009
	UCL = 95% upper confidence leakage rate is 0.087%/day
	Mean leakage rate for last five hours is -0.002%/day
3.	Verification Test
	<pre>A = Slope of least squares line (lbs/hr) is -127.19</pre>
	B = Intercept of least squares line (lbs) is 780595
	$L_c = Composite leakage rate is 0.391%/day$

APPENDIX E

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SUMMARY OF MEASURED DATA

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READINGS	TAKEN	AT	TIME	PERIOD	:	2100	

DATE : 12/9/84

RTD	1	64.9	RTD	11	65.74	
RTD	2	65.38	RTD	12	65.53	
RTD	3	65.46	RTD	13	65.81	
RTD	4	65.24	RTD	14	66.19	
RTD	5	65.47	RTD	15	65.71	
RTD	6	64.83	RTD	16	65.96	
RTD	7	65.53	RTD	17	64.55	
RTD	8	65.35	RTD	18	65.41	
RTD	9	65.62	RTD	19	65.03	
RTD	10	65.53	RTD	20	67.33	

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.5156 IN F = 525.206 IN R

PRESS	1	53.789	PRESS	2	53.766
	•				

THE AVE PRESSURE IS = 53.7775 PSIA

DEWPT 1 48.75 DEWPT 4 49.58 DEWPT 2 49.54 DEWPT 5 48.64 DEWPT 3 48.65

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 48.9847 THE PWV IS = .171401 PSIA

THE MASS WEIGHT IS = 780751.5 LBM

READINGS TAKEN AT TIME PERIOD : 2115 DATE : 12/9/84

RTD	1	64.9	RTD	11	65.71
RTD	2	65.33	RTD	12	65.44
RTD	3	65.46	RTD	13	65.75
RTD	4	65.18	RTD	14	66.18
RTD	5	65.35	RTD	15	65.71
RTD	6	64.83	RTD	16	65.96
RTD	7	65.49	RTD	17	64.55
RTD	8	65.35	RTD	18	65.41
RTD	9	65.56	RTD	19	65.15
RTD	10	65.5	RTD	20	67.22

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.4854 IN F = 525.175 IN R

PRESS 1 53.784 PRESS 2 53.761

THE AVE PRESSURE IS = 53.7725 PSIA

DEWPT 1 48.82 DEWPT 2 49.71 DEWPT 4 49.62 DEWPT 5 48.31 DEWPT 3 48.79

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.0129 THE PWV IS = .171582 PSIA

THE MASS WEIGHT IS = 780720.8125 LBM

READINGS TAKEN AT TIME PERIOD : 2130

DATE : 12/9/84

 RTD
 1
 64.84
 RTD
 11
 65.68

 RTD
 2
 65.33
 RTD
 12
 65.38
 RTD 12 65.38 RTD 13 65.75 RTD 3 65.4 RTD 4 65.18 RTD 14 66.18 RTD 15 65.71 RTD 5 65.35 RTD 6 64.71 RTD 16 65.9 RTD 7 65.43 RTD 17 64.55 RTD 8 65.28 RTD 9 65.47 RTD 18 65.35 RTD 19 65.21 RTD 10 65.47 RTD 20 67.22

> THE AVE RTD WITH WEIGHTING FACTORS IS = 65.4499 IN F = 525.14 IN R

PRESS 1 53.781 PRESS 2 53.759

THE AVE PRESSURE IS = 53.77 PSIA

DEWPT 1 48.82 DEWPT 4 49.65 DEWPT 2 49.63 DEWPT 5 48.37 DEWPT 3 48.9

0

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.0327 THE PWV IS = .171709 PSIA

THE MASS WEIGHT IS = 780735.375 LBM

READINGS TAKEN AT TIME PERIOD : 2145

DATE : 12/9/84

RTD 1 64.78 RTD 11 65.6 RTD 2 65.27 RTD 12 65.27 RTD 3 65.34 RTD 13 65.69 RTD 4 65.12 RTD 14 66.1 RTD 5 65.3 RTD 6 64.7 RTD 15 65.71 RTD 16 65.96 RTD 7 65.41 RTD 17 64.55 RTD 8 65.28 RTD 18 65.35 RTD 9 65.47 RTD 19 65.27 RTD 10 65.3 RTD 20 67.22

> THE AVE RTD WITH WEIGHTING FACTORS IS = 65.4096 IN F = 525.1 IN R

PRESS 1 53.777 PRESS 2 53.755

THE AVE PRESSURE IS = 53.766 PSIA

DEWPT 1 48.81 DEWPT 2 49.63 DEWPT 3 48.82

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DEWPT 4 49.63 DEWPT 5 48.64

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.0569 THE PWV IS = .171864 PSIA

THE MASS WEIGHT IS = 780734.75 LBM

READINGS TAKEN AT TIME PERIOD : 2200 DATE : 12/9/84

. .

RTD	1	64.72	RTD	11	65.53
RTD	2	65.21	RTD	12	65.27
RTD	3	65.34	RTD	13	65.63
RTD	4	65.06	RTD	14	66.1
RTD	5	65.24	RTD	15	65.65
RTD	6	64.7	RTD	16	65.96
RTD	7	65.35	RTD	17	64.49
RTD	8	65.22	RTD	18	65.3
RTD	9	65.41	RTD	19	65.33
RTD	10	65.37	RTD	20	67.1

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.3747 IN F = 525.065 IN R

PRESS 1 53.775 PRESS 2 53.753

THE AVE PRESSURE IS = 53.764 FSIA

DEWPT 1 48.65 DEWPT 4 49.62 DEWPT 2 49.64 DEWPT 5 48.71 DEWPT 3 48.99

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.0437 THE PWV IS = .171779 PSIA

THE MASS WEIGHT IS = 780758.75 LBM

READINGS TAKEN AT TIME PERIOD : 2215

DATE : 12/9/84

RTD	1	64.72	RTD	11	65.56
RTD	2	65.21	RTD	12	65.27
RTD	3	65.28	RTD	13	65.57
RTD	4	65	RTD	14	66.12
RTD	5	65.24	RTD	15	65.65
RTD	6	64.7	RTD	16	65.96
RTD	7	65.22	RTD	17	64.49
RTD	8	65.16	RTD	18	65.3
RTD	9	65.41	RTD	19	65.27
RTD	10	65.3	RTD	20	67.1

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.3512 IN F = 525.041 IN R

PRESS 1 53.771 PRESS 2 53.749

THE AVE PRESSURE IS = 53.76 PSIA

DEWPT 1 48.82 DEWPT 4 49.63 DEWPT 2 49.65 DEWPT 5 48.55 DEWPT 3 48.64

0

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.0184 THE PWV IS = .171617 PSIA

THE MASS WEIGHT IS = 780737.875 LBM

READINGS TAKEN AT TIME PERIOD : 2230

DATE : 12/9/84

RTD	1	64.67	RTD	11	65.49
RTD	2	65.15	RTD	12	65.21
RTD	3	65.22	RTD	13	65.57
RTD	4	65	RTD	14	65.91
RTD	5	65.18	RTD	15	65.65
RTD	6	64.56	RTD	16	65.96
RTD	7	65.28	RTD	17	64.49
RTD	8	65.11	RTD	18	65.24
RTD	9	65.35	RTD	19	65.33
RTD	10	65.24	RTD	20	67.1

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.3063 IN F = 524.996 IN R

PRESS 1 53.768 PRESS 2 53.747

THE AVE PRESSURE IS = 53.7575 PSIA

 DEWPT 1
 48.77
 DEWPT 4
 49.6

 DEWPT 2
 49.74
 DEWPT 5
 48.71
 DEWPT 3 48.97

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0

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.094 THE PWV IS = .172102 PSIA

THE MASS WEIGHT IS = 780761 LBM

READINGS TAKEN AT TIME PERIOD : 2245

DATE : 12/9/84

RTD	1	64.61	RTD	11	65.56
RTD	2	65.09	RTD	12	65.21
RTD	3	65.22	RTD	13	65.52
RTD	4	64.94	RTD	14	65.87
RTD	5	65.18	RTD	15	65.63
RTD	6	64.5	RTD	16	65.96
RTD	7	65.25	RTD	17	64.43
RTD	8	65.11	RTD	18	65.24
RTD	9	65.3	RTD	19	65.33
RTD	10	65.27	RTD	20	67.05

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.285 IN F = 524.975 IN R

PRESS 1 53.766 PRESS 2 53.744

THE AVE PRESSURE IS = 53.755 PSIA

 DEWT 1
 48.87
 DEWPT 4
 49.69

 DEWPT 2
 49.65
 DEWPT 5
 48.86
 DEWPT 3 48.94

(

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1465 THE PWV IS = .172439 PSIA

THE MASS WEIGHT IS = 780751.4375 LBM

READINGS TAKEN AT TIME PERIOD : 2300

DATE : 12/9/84

64.61 RTD 1 RTD 11 65.49 65.09 RTD 2 RTD 12 65.15 RTD 3 65.16 65.52 RTD 13 RTD 4 64.94 RTD 14 65.88 RTD 5 65.06 RTD 15 65.57 64.52 RTD 6 RTD 16 65.96 RTD 7 65.18 RTD 17 64.43 RTD 8 65.05 RTD 18 65.18 RTD 9 65.3 RTD 19 65.33 RTD 10 65.28 RTD 20 67.03

> THE AVE RTD WITH WEIGHTING FACTORS IS = 65.257 IN F = 524.947 IN R

PRESS 1 53.763 PRESS 2 53.742

THE AVE PRESSURE IS = 53.7525 PSIA

DEWPT 1 49.05
 DEWPT 1
 49.05
 DEWPT 4
 49.66

 DEWPT 2
 49.68
 DEWPT 5
 48.65
 DEWPT 3 48.79

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.147 THE PWV IS = .172443 PSIA

THE MASS WEIGHT IS = 780756.6875 LBM

READINGS TAKEN AT TIME PERIOD : 2315 DATE : 12/9/84

RTD	1	64.61	RTD	11	65.44
RTD	2	65.03	RTD	12	65.09
RTD	3	65.11	RTD	13	65.46
RTD	4	64.89	RTD	14	65.87
RTD	5	65.12	RTD	15	65.57
RTD	6	64.46	RTD	16	65.9
RTD	7	65.18	RTD	17	64.43
RTD	8	65.05	RTD	18	65.18
RTD	9	65.3	RTD	19	65.38
RTD	10	65.15	RTD	20	66.97

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.2276 IN F = 524.918 IN R

PRESS 1 53.761 PRESS 2 53.74

THE AVE PRESSURE IS = 53.7505 PSIA

 DEWPT 1
 48.82
 DEWPT 4
 49.73

 DEWPT 2
 49.71
 DEWPT 5
 48.48
 DEWPT 3 48.98

(

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.0909 THE PWV IS = .172082 PSIA

THE MASS WEIGHT IS = 780776.375 LBM

READINGS TAKEN AT TIME PERIOD : 2330	DA
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DATE : 12/9/84

RTD	1	64.55	RTD	11	65.43
RTD	2	65.03	RTD	12	65.09
RTD	3	65.11	RTD	13	65.46
RTD	4	64.89	RTD	14	65.78
RTD	5	65.06	RTD	15	65.57
RTD	6	64.52	RTD	16	65.96
RTD	7	65.12	RTD	17	64.43
RTD	8	65.05	RTD	18	65.18
RTD	9	65.3	RTD	19	65.33
RTD	10	65.24	RTD	20	66.97

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.2223 IN F = 524.912 IN R

PRESS 1 53.759 PRESS 2 53.738

THE AVE PRESSURE IS = 53.7485 PSIA

DEWPT 1 48.91 DEWPT 4 49.77 DEWPT 2 49.76 DEWPT 5 48.76 DEWPT 3 49.03

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1904 THE PWV IS = .172722 PSIA

THE MASS WEIGHT IS = 780745.6875 LBM

READINGS TAKEN AT TIME PERIOD : 2345

DATE : 12/9/84

RTD	1	64.55	RTD	11	65.35
RTD	2	65.03	RTD	12	65.09
RTD	3	65.11	RTD	13	65.4
RTD	4	64.83	RTD	14	65.82
RTD	5	65.06	RTD	15	65.57
RTD	6	64.53	RTD	16	65.9
RTD	7	65.09	RTD	17	64.37
RTD	8	64.99	RTD	18	65.18
RTD	9	65.24	RTD	19	65.33
RTD	10	65.27	RTD	20	66.97

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.2024 IN F = 524.892 IN R

PRESS -1 53.756 PRESS 2 53.736

THE AVE PRESSURE IS = 53.746 PSIA

DEWPT 1 48.92 DEWPT 2 49.7 DEWPT 3 48.79 DEWPT 4 49.73 DEWPT 5 47.97

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.0069 THE PWV IS = .171543 PSIA

THE MASS WEIGHT IS = 780756.1875 LBM

READINGS TAKEN AT TIME PERIOD : 0 DATE : 12/10/84

RTD	1	64.55	RTD	11	65.33
RTD	2	64.97	RTD	12	65.03
RTD	3	65.11	RTD	13	65.4
RTD	4	64.83	RTD	14	65.79
RTD	5	65.06	RTD	15	65.63
RTD	6	64.46	RTD	16	65.84
RTD	7	65.09	RTD	17	64.37
RTD	8	64.99	RTD	18	65.18
RTD	9	65.24	RTD	19	65.33
RTD	.10	65.21	RTD	20	66.97

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.1857 IN F = 524.876 IN R

PRESS 1 53.754 PRESS 2 53.734

THE AVE PRESSURE IS = 53.744 PSIA

 DEWPT 1
 48.82
 DEWPT 4
 49.81

 DEWPT 2
 49.69
 DEWPT 5
 48.27
 DEWPT 3 48.93

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.0578 THE PWV IS = .171869 PSIA

THE MASS WEIGHT IS = 780747 LBM

READINGS TAKEN AT TIME PERIOD : 15

DATE : 12/10/84

RTD	1	64.49	RTD	11	65.33
RTD	2	64.97	RTD	12	65.03
RTD	3	65.05	RTD	13	65.34
RTD	4	64.83	RTD	14	65.75
RTD	5	65	RTD	15	65.63
RTD	6	64.46	RTD	16	65.78
RTD	7	65.09	RTD	17	64.37
RTD	8	64.93	RTD	18	65.12
RTD	9	65.18	RTD	19	65.33
RTD	10	65.21	RTD	20	66.91

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.1571 IN F = 524.847 IN R

PRESS 1 53.753 PRESS 2 53.732

THE AVE PRESSURE IS = 53.7425 PSIA

 DEWPT 1
 48.96
 DEWPT 4
 49.76

 DEWPT 2
 49.77
 DEWPT 5
 48.69

 DEWPT 3
 48.98
 48.69

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1872 THE PWV IS = .172702 PSIA

THE MASS WEIGHT IS = 780755.75 LBM

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READINGS TAKEN AT TIME PERIOD : 30

DATE : 12/10/84

RTD	1	64.49	RTD	11	65.31
RTD	2	64.97	RTD	12	64.97
RTD	3	65.05	RTD	13	65.34
RTD	4	64.77	RTD	14	65.62
RTD	5	65	RTD	15	65.56
RTD	6	64.93	RTD	16	65.84
RTD	7	65.03	RTD	17	64.37
RTD	8	64.93	RTD	18	65.12
RTD	9	65.18	RTD	19	65.27
RTD	10	65.15	RTD	20	66.88

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.1589 IN F = 524.849 IN R

PRESS -1 53.751 PRESS 2 53.731

THE AVE PRESSURE IS = 53.741 PSIA

DEWPT 148.82DEWPT 449.82DEWPT 249.66DEWPT 548.48 DEWPT 3 49.14

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1243 THE PWV IS = .172297 PSIA

THE MASS WEIGHT IS = 780737.0625 LBM

READINGS TAKEN AT TIME PERIOD : 45

65.12

RTD	1	64.43	RTD	11	65.31
RTD	2	64.92	RTD	12	64.92
RTD	3	64.99	RTD	13	65.34
RTD	4	64.77	RTD	14	65.72
RTD	5	64.94	RTD	15	65.56
RTD	6	64.33	RTD	16	65.84
RTD	7	65.03	RTD	17	64.31
RTD	8	64.87	RTD	18	65.06
RTD	9	65.12	RTD	19	65.33

RTD

THE	AVE	RTD	WITH	WEIGHTING	FACTORS	IS	=	65.1045	IN
							-	EDA 704	TRI

20

66.88

IN R 524.794

F

DATE : 12/10/84

THE AVE PRESSURE IS = 53.739 PSIA

DEWPT 1 48.96
 DEWPT 1
 48.96
 DEWPT 4
 49.82

 DEWPT 2
 49.74
 DEWPT 5
 48.7
 DEWPT 3 48.96

RTD 10

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1902 THE PWV IS = .172721 PSIA

THE MASS WEIGHT IS = 780782.6875 LBM

READINGS TAKEN AT TIME PERIOD : 100 DATE : 12/10/84

RTD	1	64.43	, RTD	11	65.28
RTD	2	64.92	RTD	12	64.92
RTD	3	64.99	RTD	13	65.28
RTD	4	64.77	RTD	14	65.68
RTD	5	64.94	RTD -	15	65.56
RTD	6	64.4	RTD	16	65.84
RTD	7	65.03	RTD	17	64.31
RTD	8	64.87	RTD	18	65.06
RTD	9	5.12	RTD	19	65.27
RTD	10	65.08	RTD	20	. 66.82

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.0956 IN F = 524.786 IN R

PRESS -1 53.747 PRESS 2 53.728

THE AVE PRESSURE IS = 53.7375 PSIA

DEWPT 1 48.98 DEWPT 4 49.77 DEWPT 2 49.74 DEWPT 5 48.69 DEWPT 3 48.88

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1735 THE PWV IS = .172614 PSIA

THE MASS WEIGHT IS = 780775.5 LBM

READINGS TAKEN AT TIME PERIOD : 115 DATE : 12/10/84

RTD	1	64.37	RTD	11	65.3
RTD	2	64.92	RTD	12	64.92
RTD	3	64.93	RTD	13	65.28
RTD	4	64.74	RTD	14	65.57
RTD	5	64.94	RTD	15	65.56
RTD	6	64.34	RTD	16	65.84
RTD	7	64.97	RTD	17	64.26
RTD	8	64.87	RTD	18	65.06
RTD	9	65.12	RTD	19	65.27
RTD	10	65.18	RTD	20	66.83

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.0804 IN F = 524.77 IN R

PRESS -1 53.746 PRESS 2 53.727

THE AVE PRESSURE IS = 53.7365 PSIA

 DEWPT 1
 48.96
 DEWPT 4
 49.77

 DEWPT 2
 49.8
 DEWPT 5
 48.86
 DEWPT 3 48.3

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1069 THE PWV IS = .172185 PSIA

THE MASS WEIGHT IS = 780790 LBM

READINGS TAKEN AT TIME PERIOD : 130 DATE : 12/10/84

RTD	1	64.43	RTD	11	65.25
RTD	2	64.86	RTD	12	64.92
RTD	3	64.93	RTD	13	65.22
RTD	4	64.74	RTD	14	65.53
RTD	5	64.89	RTD	15	65.56
RTD	6	64.34	RTD	16	65.82
RTD	7	64.97	RTD	17	64.26
RTD	8	64.87	RTD	18	65.06
RTD	9	65.06	RTD	19	65.27
RTD	10	65.12	RTD	20	66.81

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.0613 IN F = 524.751 IN R

PRESS 1 53.745 PRESS 2 53.726

THE AVE PRESSURE IS = 53.7355 PSIA

 DEWPT 1
 48.97
 DEWPT 4
 49.75

 DEWPT 2
 49.84
 DEWPT 5
 48.8
 DEWPT 3 48.79

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1867 THE PWV IS = .172699 PSIA

THE MASS WEIGHT IS = 780796.25 LBM

READINGS TAKEN AT TIME PERIOD : 145

DATE : 12/10/84

RTD	1	64.37	RTD	11	65.25
RTD	2	64.86	RTD	12	64.86
RTD	3	64.93	RTD	13	65.22
RTD	4	64.68	RTD	14	65.59
RTD	5 .	64.89	RTD	15	65.56
RTD	6	64.29	RTD	16	65.82
RTD	7	64.97	RTD	17	64.26
RTD	8	64.81	RTD	18	65
RTD	9	65.06	RTD	19	65.27
RTD	10	65.15	RTD	20	66.81

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.048 IN F = 524.738 IN R

PRESS 1 53.744 PRESS 2 53.724

THE AVE PRESSURE IS = 53.734 PSIA

DEWPT 1 48.94 DEWPT 4 47.55 DEWPT 2 49.74 DEWPT 5 48.86

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.2047 THE PWV IS = .172815 PSIA

THE MASS WEIGHT IS = 780792.5 LBM

READINGS TAKEN AT TIME PERIOD : 200 DATE : 12/10/84

RTD	1	64.37	RTD	11	65.3
RTD	2	64.86	RTD	12	64.86
RTD	3	64.93	RTD	13	65.22
RTD	4	64.68	RTD	14	65.56
RTD	5	64.89	RTD	15	65.5
RTD	6	64.3	RTD	16	65.82
RTD	7	64.97	RTD	17	64.26
RTD	8	64.81	RTD	18	65
RTD	9	65.06	RTD	19	65.21
RTD	10	65.09	RTD	20	66.67

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.0372 IN F = 524.727 IN R

PRESS -1 53.74 PRESS 2 53.724

THE AVE PRESSURE IS = 53.732 PSIA

DEWPT 148.92DEWPT 449.82DEWFT 249.86DEWPT 548.57 DEWPT 1 48.92 DEWPT 3 49.05

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.191 THE PWV IS = .172727 PSIA

THE MASS WEIGHT IS = 780780.75 LBM

READINGS TAKEN AT TIME PERIOD : 215 DATE : 12/10/84

RTD	1	64.37	RTD	11	65.24
RTD	2	64.86	RTD	12	64.87
RTD	3	64.87	RTD	13	65.22
RTD	4	64.68	RTD	14	65.56
RTD	5	64.89	RTD	15	65.5
RTD	6	64.3	RTD	16	65.76
RTD	7	64.94	RTD	17	64.26
RTD	8	64.81	RTD	18	65
RTD	9	65.06	RTD	19	65.27
RTD	10	65.03	RTD	20	66.79

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.0285 IN F = 524.719 IN R

PRESS 1 53.741 PRESS 2 53.721

THE AVE PRESSURE IS = 53.731 PSIA

 DEWPT 1
 43.92
 DEWPT 4
 49.86

 DEWPT 2
 49.86
 DEWPT 5
 48.26
 DEWPT 3 48.9

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1214 THE PWV IS = .172278 PSIA

THE MASS WEIGHT IS = 780785.5625 LBM

READINGS TAKEN AT TIME PERIOD : 230

1

DATE : 12/10/84

RTD 1 64.36 RTD 2 64.86 RTD 11 65.3 RTD 12 64.87 RTD 3 64.93 RTD 13 65.16 RTD 4 64.68 RTD 14 65.52 64.89 RTD 5 RTD 15 65.5 64.3 RTL 6 RTD 16 65.71 RTD 7 64.92 RTD 17 64.26 RTD 8 64.81 RTD 18 65 RTD 9 65.06 RTD 19 65.21 RTD 10 65.03 RTD 20 66.76

> THE AVE RTD WITH WEIGHTING FACTORS IS = 65.0231 IN F = 524.713 IN R

PRESS 1 53.74 PRESS 2 53.721

THE AVE PRESSURE IS = 53.7305 PSIA

DEWPT 1 49.05 DEWPT 2 49.76 DEWPT 3 48.98

DEWPT 4 49.86 DEWPT 5 48.22

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1549 THE PWV IS = .172494 PSIA

THE MASS WEIGHT IS = 780783.25 LBM

READINGS TAKEN AT TIME PERIOD : 245

1

DATE : 12/10/84

RTD	1	64.36	RTD	11	65.27
RTD	2	64.8	RTD	12	64.8
RTD	3	64.87	RTD	13	65.16
RTD	4	64.68	RTD	14	65.47
RTD	5	64.89	RTD	15	65.5
RTD	6	64.29	RTD	16	65.76
RTD	7	64.86	RTD	17	64.26
RTD	8	64.81	RTD	18	64.94
RTD	9	65	RTD	19	65.27
RTD	10	65.03	RTD	20	66.7

THE AVE RTD WITH WEIGHTING FACTORS IS = 65.0016 IN F = 524.692 IN R

PRESS 1 53.738 PRESS 2 53.72

THE AVE PRESSURE IS = 53.729 PSIA

 DEWPT 1
 49.08
 DEWPT 4
 49.85

 DEWPT 2
 49.86
 DEWPT 5
 47.98
 DEWPT 3 48.81

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1121 THE PWV IS = .172218 PSIA

THE MASS WEIGHT IS = 780797.25 LBM

READINGS TAKEN AT TIME PERIOD : 300

DATE : 12/10/84

RTD	1	64.3	RTD	11	65.19
RTD	2	64.86	RTD	12	64.86
RTD	3	64.87	RTD	13	65.16
RTD	4	64.62	RTD	14	65.53
RTD	5	64.81	RTD	15	65.5
RTD	6	64.29	RTD	16	65.63
RTD	7	64.86	RTD	17	64.2
RTD	8	64.75	RTD	18	64.94
RTD	9	65	RTD	19	65.21
RTD	10	64.97	RTD	20	66.73

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.9796 IN F = 524.67 IN R

PRESS -1 53.737 PRESS 2 53.718

THE AVE PRESSURE IS = 53.7275 PSIA

DEWPT 149.07DEWPT 449.84DEWPT 249.75DEWPT 548.25 DEWPT 3 48.79

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.1294 THE PWV IS = .17233 PSIA

THE MASS WEIGHT IS = 780806.625 LBM

READINGS TAKEN AT TIME PERIOD : 315 DATE : 12/10/84

RTD	1	64.3	RTD	11	65.21
RTD	2	64.8	RTP	12	64.86
RTD	3	64.81	RTD	13	65.16
RTD	4	64.62	RTD	14	65.43
RTD	5	64.81	RTD	15	65.5
RTD	6	64.27	RTD	16	65.71
RTD	7	64.86	RTD	17	64.2
RTD	8	64.75	RTD	18	64.94
RTD	9	65	RTD	19	65.15
RTD	10	65.03	RTD	20	66.76

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.9743 IN F = 524.664 IN R

PRESS 1 53.736 PRESS 2 53.717

THE AVE PRESSURE IS = 53.7265 PSIA

DEWPT 1 49.07 DEWPT 4 49.88 DEWPT 2 49.93 DEWPT 5 48.37 DEWPT 3 49.03

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.2266 THE PWV IS = .172956 PSIA

THE MASS WEIGHT IS = 780790.75 LBM

READINGS TAKEN AT TIME PERIOD : 330 DATE : 12/10/84

RTD	1	64.3	RTD	11	65.15	
RTD	2	64.8	RTD	12	64.8	
RTD	3	64.81	RTD	13	65.16	
RTD	4	64.62	RTD	14	65.41	
RTD	5	64.81	RTD	15	65.5	
RTD	6	64.27	RTD	16	65.76	
RTD	7	64.94	RTD	17	64.2	
RTD	8	64.75	RTD	18	64.94	
RTD	9	65	RTD	19	65.21	
RTD	10	64.97	RTD	20	66.76	

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.9721 IN F = 524.662 IN R

PRESS 1 53.734 PRESS 2 53.715

THE AVE PRESSURE IS = 53.7245 PSIA

DEWPT 1 49.19 DEWPT 4 49.86 DEWPT 2 49.82 DEWPT 5 48.43 DEWPT 3 48.96

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.2428 THE PWV IS = .173061 PSIA

THE MASS WEIGHT IS = 780763.4375 LBM

READINGS TAKEN AT TIME PERIOD : 345 DATE : 12/10/84

RTD	1	64.3		RTD	11	65.24
RTD	2	64.74		RTD	12	64.8
RTD	3	64.81		RTD	13	65.11
RTD	4	64.56		RTD	14	65.47
RTD	5	64.81	•	RTD	15	65.43
RTD	6	64.27		RTD	16	65.72
RTD	7	64.89		RTD	17	64.14
RTD	8	64.75		RTD	18	64.93
RTD	9	64.94		RTD	19	65.21
RTD	10	64.92		RTD	20	66.63

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.9501 IN F = 524.64 IN R

PRESS 1 53.732 PRESS 2 53.713

THE AVE PRESSURE IS = 53.7225 PSIA

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 DEWPT 1
 49.15
 DEWPT 4
 49.88

 DEWPT 2
 49.9
 DEWPT 5
 48.19
 DEWPT 3 48.93

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.2019 THE PWV IS = .172796 PSIA

THE MASS WEIGHT IS = 780770.75 LBM

READINGS TAKEN AT TIME PERIOD : 400 DATE : 12/10/84

RTD	1	64.24	RTD	11	65.18
RTD	2	64.74	RTD	12	64.71
RTD	3	64.75	RTD	13	65.11
RTD	4	64.56	RTD	14	65.38
RTD	5	64.75	RTD	15	65.43
RTD	6	64.27	RTD	16	65.75
RTD	7	64.83	RTD	17	64.07
RTD	8	64.7	RTD	18	64.87
RTD	9	64.94	RTD	19	65.15
RTD	10	64.94	RTD	20	66.57

THE AVE RTD WITH WEIGHTING FACTURS IS = 64.9158 IN F = 524.606 IN R

PRESS 1 53.73 PRESS 2 53.712

THE AVE PRESSURE IS = 53.721 PSIA

 DEWPT 1
 49.15
 DEWPT 4
 49.71

 DEWPT 2
 49.95
 DEWPT 5
 48.57
 DEWPT 3 48.98

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.2532 THE PWV IS = .173128 PSIA

THE MASS WEIGHT IS = 780795.125 LBM

READINGS TAKEN AT TIME PERIOD : 415

DATE : 12/10/84

RTD	1	64.24	RTD	11	65.09
RTD	2	64.74	RTD	12	64.71
RTD	3	64.81	RTD	13	65.05
RTD	4	64.56	RTD	14	65.4
RTD	5	64.75	RTD	15	65.43
RTD	6	64.12	RTD	16	65.63
RTD	7	64.84	RTD	17	64.07
RTD	8	64.7	RTD	18	64.86
RTD	9	64.89	RTD	19	65.21
RTD	10	64.89	RTD	20	66.64

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.8962 IN F = 524.586 IN R

PRESS 1 53.728 PRESS 2 53.709

THE AVE PRESSURE IS = 53.7185 PSIA

DEWPT 1 49.07 DEWPT 4 49.91 DEWPT 2 49.88 DEWPT 5 48.88 DEWPT 3 48.86

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.278 THE PWV IS = .173288 PSIA

THE MASS WEIGHT IS = 780785.375 LBM

READINGS TAKEN AT TIME PERIOD : 430 DATE : 12/10/84 RTD 1 64.24 RTD 11 65.09 RTD 2 64.74 RTD 12 64.77 RTD 3 64.75 RTD 13 65.05 RTD 4 64.56 RTD 14 65.35 RTD 5 64.75 RTD 15 65.43 64.23 RTD 6 RTD 16 65.76 RTD 7 64.77 RTD 17 64.07 RTD 8 64.64 RTD 18 64.86 RTD 9 64.89 RTD 19 65.21 RTD 10 64.96 RTD 20 66.64 THE AVE RTD WITH WEIGHTING FACTORS IS = 64.9031 IN F = 524.593 IN R

PRESS 1 53.725 PRESS 2 53.707

THE AVE PRESSURE IS = 53.716 PSIA

DEWPT 1 49.11 DEWPT 4 49.86 DEWPT 2 50.01 DEWPT 5 48.99 DEWPT 3 49.2

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3806 THE PWV IS = .173952 PSIA

THE MASS WEIGHT IS = 780728.9375 LBM

READINGS TAKEN AT TIME PERIOD : 445 DATE : 12/10/84

RTD 1 64.24 RTD 11 64.96 RTD 2 64.68 RTD 12 64.71 RTD 3 64.75 RTD 13 65.05 RTD 4 64.5 RTD 14 65.38 RTD 5 64.7 RTD 15 65.37 RTD 6 64.17 RTD 16 65.71 RTD 7 64.83 RTD 17 64.07 RTD 8 64.64 RTD 18 64.86 RTD 9 64.89 RTD 19 65.15 RTD 10 64.92 RTD 20 66.57

> THE AVE RTD WITH WEIGHTING FACTORS IS = 64.8726 IN F = 524.563 IN R

PRESS 1 53.724 PRESS 2 53.706

THE AVE PRESSURE IS = 53.715 PSIA

DEWPT 1 49.09 DEWPT 4 49.96 DEWPT 2 49.91 DEWPT 5 49.05 DEWPT 3 49.22

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3867 THE PWV IS = .173992 PSIA

THE MASS WEIGHT IS = 780759.25 LBM
READINGS	TAKEN	AT	TIME	PERIOD	:	500	D

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DATE : 12/10/84

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RTD	1	64.18	RTD	11	65.03	
RTD	2	64.68	RTD	12	64.71	
RTD	3	64.75	RTD	13	64.99	
RTD	4	64.5	RTD	14	65.3	
RTD	5	64.7	RTD	15	65.37	
RTD	6	64.11	RTD	16	65.63	
RTD	7	64.81	RTD	17	64.07	
RTD	8	64.64	RTD	18	64.78	
RTD	9	64.83	RTD	19	65.22	
RTD	10	64.86	RTD	20	66.53	

- 504 57				ALL REAL PROPERTY AND ADDRESS OF A DESCRIPTION OF A DESCR	 	 	a a then	
= 524.55	IN R	524.539	=					

TEDD & 00.721 FREDD 2 00.700	PRESS	-1	53.721	PRESS 2	53.703
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THE AVE PRESSURE IS = 53.712 PSIA

DEWPT	1	49.09	DEWPT	4	49.92
DEWPT	2	50.02	DEWPT	5	48.63
DEWPT	3	48.82			

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.2622 THE PWV IS = .173186 PSIA

THE MASS WEIGHT IS = 780762.125 LBM

READINGS TAKEN AT TIME PERIOD : 515 DATE : 12/10/84

8

RTD	1	64.18	RTD	11	65.09
RTD	2	64.68	RTD	12	64.68
RTD	3	64.7	RTD	13	64.99
RTD	4	64.45	RTD	14	65.18
RTD	5	64.64	RTD	15	65.31
RTD	6	64.09	RTD	16	65.57
RTD	7	64.75	RTD	17	63.99
RTD	8	64.58	RTD	18	64.78
RTD	9	64.83	RTD	19	65.21
RTD	10	64.86	RTD	20	66.53

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.8191 IN F = 524.509 IN R

PRESS -1 53.719 PRESS 2 53.701

THE AVE PRESSURE IS = 53.71 PSIA

DEWPT 1 49.15 DEWPT 2 49.86 DEWPT 3 49.18

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DEWPT 4 49.86 DEWPT 5 48.8

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 19.3341 THE PWV IS = .173651 PSIA

THE MASS WEIGHT IS = 780771.125 LBM

READINGS TAKEN AT TIME PERIOD : 530

DATE : 12/10/84

RTD	1	64.18	RTD	11	65.03
RTD	2	64.68	RTD	12	64.56
RTD	3	64.7	RTD	13	64.93
RTD	4	64.45	RTD	14	65.25
RTD	5	64.64	RTD	15	65.31
RTD	6	04.09	RTD	16	65.65
RTD	7	64.7	RTD	17	63.99
RTD	8	64.58	RTD	18	64.78
RTD	9	64.83	RTD	19	65.15
RTD	10	64.77	RTD	20	66.53

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.8039 IN F = 524.494 IN R

PRESS 1 53.717 PRESS 2 53.7

THE AVE PRESSURE IS = 53.7085 PSIA

DEWPT 1 49.14 DEWPT 4 49.87 DEWPT 2 50.04 DEWPT 5 48.33 DEWPT 3 49.05

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.2638 THE PWV IS = .173196 PSIA

THE MASS WEIGHT IS = 780778.5625 LBM

READINGS TAKEN AT TIME PERIOD : 545 DATE : 12/10/84

RTD	1	64.12	PTD	11	64.92
RTD	2	64.62	RTD	12	64.56
RTD	3	64.64	RTD	13	64.93
RTD	4	64.39	RTD	14	65.19
RTD	5	64.64	RTD	15	65.25
RTD	6	64.17	RTD	16	65.69
RTD	7	64.62	RTD	17	63.93
RTD	8	64.52	RTD	18	64.72
RTD	9	64.77	RTD	19	65.09
RTD	10	64.86	RTD	20	66.44

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.7701 IN F = 524.46 IN R

PRESS 1 53.715 PRESS 2 53.697

THE AVE PRESSURE IS = 53.706 PSIA

DEWPT 149.09DEWFT 449.92DEWPT 249.99DEWPT 548.68 DEWPT 3 49.08

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3093 THE PWV IS = .17349 PSIA

THE MASS WEIGHT IS = 780787.9375 LBM

READINGS TAKEN AT TIME PERIOD : 600

DATE : 12/10/84

RTD 1 64.12 RTD 2 64.62 RTD 11 65.09 RTD 12 64.62 64.64 RTD 3 RTD 13 64.93 RTD 4 64.39 RTD 14 65.15 RTD 5 64.64 RTD 15 65.25 64.11 RTD 16 65.55 RTD 17 63.93 RTD 6 RTD 7 64.72 RTD 8 64.52 RTD 18 64.72 RTD 19 65.15 RTD 9 64.77 RTD 10 64.74 RTD 20 66.5

> THE AVE RTD WITH WEIGHTING FACTORS IS = 64.7731 IN F = 524.463 IN R

PRESS 1 53.714 PRESS 2 53.696

THE AVE PRESSURE IS = 53.705 PSIA

DEWPT 1 49.11 DEWPT 4 49.97 DEWPT 2 49.99 DEWPT 5 48.42 DEWPT 3 49.05

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.2765 THE PWV IS = .173278 PSIA

THE MASS WEIGHT IS = 780772.0625 LBM

READINGS TAKEN AT TIME PERIOD : 615

DATE : 12/10/84

RTD	1	64.12	RTD	11	65
RTD	2	64.62	RTD	12	64.56
RTD	3	64.64	RTD	13	64.93
RTD	4	64.39	RTD	14	65.09
RTD'	5	64.58	RTD	15	65.25
RTD	6	64.11	RTD	16	65.49
RTD	7	64.62	RTD	17	63.87
RTD	8	64.52	RTD	18	64.72
RTD	9	64.77	RTD	19	65.15
RTD	10	64.8	RTD	20	66.44

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.7492 IN F = 524.439 IN R

PRESS 1 53.712 PRESS 2 53.694

THE AVE PRESSURE IS = 53.703 PSIA

 DEWPT 1
 49.13
 DEWPT 4
 49.93

 DEWPT 2
 50.01
 DEWPT 5
 48.8

 DEWPT 3
 49.03
 49.03
 48.8

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3389 THE PWV IS = .173682 PSIA

THE MASS WEIGHT IS = 780772.4375 LBM

READINGS TAKEN AT TIME PERIOD : 630

DATE : 12/10/84

RTD	1	64.07	RTD	11	65
RTD	2	64.56	RTD	12	64.56
RTD	3	64.58	RTD	13	64.87
RTD	4	64.33	RTD	14	65.24
RTD	5	64.58	RTD	15	65.19
RTD	6	64.11	RTD	16	65.49
RTD	7	64.65	RTD	17	63.79
RTD	8	64.46	RTD	18	64.72
RTD	9	64.77	RTD	19	65.15
RTD	10	64.78	RTD	20	66.44

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.7326 IN F = 524.423 IN R

PRESS 1 53.71 PRESS 2 53.693

THE AVE PRESSURE IS = 53.7015 PSIA

 DEWPT 1
 49.16
 DEWPT 4
 49.97

 DEWPT 2
 50.01
 DEWPT 5
 48.37

 DEWPT 3
 49.35
 49.35

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.339 THE PWV IS = .173683 PSIA

THE MASS WEIGHT IS = 780775.3125 LBM

READINGS TAKEN AT TIME PERIOD : 645 DATE : 12/10/84

RTD	1	64. 01	RTD	11	65
RTD	2	64.56	RTD	12	64.56
RTD	3	64.58	RTD	13	64.87
RTP	4	64.33	RTD	14	65.09
RTD	5	64.58	RTD	15	65.19
RTD	6	64.04	RTD	16	65.56
RTD	7	64.58	RTD	17	63.85
RTD	8	64.46	RTD	18	64.67
RTD	9	64.71	RTD	19	65.15
RTD	10	64.77	RTD	20	66.37

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.7115 IN F = 524.402 IN R

PRESS -1 53.708 PRESS 2 53.689

THE AVE PRESSURE IS = 53.6985 PSIA

DEWPT 149.24DEWPT 450.01DEWPT 249.97DEWPT 548.72 DEWPT 3 49.14

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3875 THE PWV IS = .173997 PSIA

THE MASS WEIGHT IS = 780758.3125 LBM

READINGS TAKEN AT TIME PERIOD : 700 DATE : 12/10/84

RTD	1	64.01	RTD	11	64.96
RTD	2	64.5	RTD	12	64.56
RTD	3	64.58	RTD	13	64.81
RTD	4	64.33	RTD	14	65.06
RTD	5	54.52	RTD	15	65.19
RTD	6	64.02	RTD	16	65.49
RTD	7	64.68	RTD	17	63.85
RTD	8	64.46	RTD	18	64.61
RTD	9	64.71	RTD	19	65.15
RTD	10	64.65	RTD	20	66.37

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.6903 IN F = 524.38 IN R

PRESS	-1	53.706	PRESS	2	53.68	38

THE AVE PRESSURE IS = 53.697 PSIA

DEWPT 1 49.19 DEWPT 4 49.9 DEWPT 2 49.95 DEWPT 5 48.16 DEWPT 3 48.86

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.2102 THE PWV IS = .17285 PSIA

THE MASS WEIGHT IS = 780784.75 LBM

READINGS TAKEN AT TIME PERIOD : 715 DATE : 12/10/84

RTD	1	64.01	RTD	11	64.86
RTD	2	64.5	RTD	12	64.56
RTD	3	64.58	RTD	13	64.81
RTD	4	64.33	RTD	14	65.02
RTD	5	64.52	RTD	15	65.19
RTD	6	64.02	RTD	16	65.59
RTD	7	64.56	RTD	17	63.79
RTD	8	64 4	RTD	18	64.67
RTD	9	64.65	RTD	19	65.09
RTD	10	64.77	RTD	20	66.34

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.6783 IN F = 524.368 IN R

PRESS 1 53.705 PRESS 2 53.687

THE AVE PRESSURE IS = 53.696 PSIA

DEWPT 1 49.21 DEWPT 4 49.97 DEWPT 2 49.95 DEWPT 5 48.44 DEWPT 3 49.32

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.352 THE PWV IS = .173767 PSIA

THE MASS WEIGHT IS = 780774.75 LBM

READINGS TAKEN AT TIME PERIOD : 730 DATE : 12/10/84

RTD	1	63.95	RTD	11	64.9
RTD	2	64.5	RTD	12	64.5
RTD	3	64.52	RTD	13	64.81
RTD	4	64.27	RTD	14	65.06
RTD	5	64.52	RTD	15	65.13
RTD	6	64.02	RTD	16	65.46
RTD	7	64.56	RTD	17	63.79
RTD	8	64.4	RTD	18	64.61
RTD	9	64.65	RTD	19	65.09
RTD	10	64.77	RTD	20	66.39

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.6591 IN F = 524.349 IN R

PRESS -1 53.703 PRESS 2 53.686

THE AVE PRESSURE IS = 53.6945 PSIA

DEWPT 1 49.09 DEWPT 4 49.99 DEWPT 2 50.09 DEWPT 5 48.44 DEWPT 3 49.13

0

DEWPT 5 48.44

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3068 THE PWV IS = .173474 PSIA

THE MASS WEIGHT IS = 780785.625 LBM

READINGS TAKEN AT TIME PERIOD : 745 DATE : 12/10/84

RTD	1	64.01	RTD	11	64.96
RTD	2	64.5	RTD	12	64.5
RTD	3	64.52	RTD	13	64.81
RTD	4	64.27	RTD	14	65.03
RTD	5	64.52	RTD	15	65.13
RTD	6	64.01	RTD	16	65.53
RTD	7	64.56	RTD	17	63.79
RTD	8	64.4	RTD	18	64.61
RTD	9	64.65	RTD	19	65.09
RTD	10	64.65	RTD	20	66.41

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.6612 IN F = 524.351 IN R

PRESS 1 53.702 PRESS 2 53.684

THE AVE PRESSURE IS = 53.693 PSIA

 DEWPT 1
 49.21
 DEWPT 4
 50.01

 DEWPT 2
 50.02
 DEWPT 5
 48.37
 DEWPT 3 49.13

0

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3268 THE PWV IS = .173604 PSIA

THE MASS WEIGHT IS = 780758.8125 LBM

READINGS TAKEN AT TIME PERIOD : 800

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DATE : 12/10/84

RTD	1	64.01	RTD	11	64.84
RTD	2	64.52	RTD	12	64.45
RTD	3	64.52	RTD	13	64.81
RTD	4	64.27	RTD	14	65
RTD	5	64.46	RTD	15	65.08
RTD	6	63.95	RTD	16	65.4
RTD	7	64.56	RTD	17	63.79
RTD	8	64.4	RTD	18	64.61
RTD	9	64.65	RTD	19	65.03
RTD	10	64.68	RTD	20	66.32

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.6324 IN F = 524.322 IN R

PRESS -1 53.701 PRESS 2 53.683

THE AVE PRESSURE IS = 53.692 PSIA

DEWPT 1 49.21 DEWPT 4 50.03 DEWPT 2 50.08 DEWPT 5 48.39 DEWPT 3 49.2

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3553 THE PWV IS = .173788 PSIA

THE MASS WEIGHT IS = 780784.375 LBM

READINGS TAKEN AT TIME PERIOD : 815 DATE : 12/10/84

RTD	1	64.01	RTD	11	64.8
RTD	2	64.45	RTD	12	64.45
RTD	3	64.52	RTD	13	64.75
RTD	4	64.27	RTD	14	65.16
RTD	5	64.46	RTD	15	65.13
RTD	6	63.9	RTD	16	65.52
RTD	7	64.59	RTD	17	63.73
RTD	8	64.34	RTD	18	64.61
RTD	9	64.65	RTD	19	65.09
RTD	10	64.67	RTD	20	66.34

THE	AVE	RTD	WITH	WEIGHTING	FACTORS	IS	=	64.6356	IN	F
							=	524.326	IN	R

PRESS	1 53.699			PRESS 2 53.681				53.681
	THE	AVE	PRESSURE	IS	83	53.	. 69	PSIA

DEWPT 1 49.26 DEWPT 4 50.01 DEWPT 2 50.13 DEWPT 5 48.59 DEWPT 3 49.37

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4388 THE PWV IS = .17433 PSIA

THE MASS WEIGHT IS = 780742.4375 LBM

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READINGS TAKEN AT TIME PERIOD : 830

DATE : 12/10/84

RTD	1	63.95	RTD	11	64.92
RTD	2	64.45	RTD	12	64.45
RTD	3	64.46	RTD	13	64.75
RTD	4	64.21	RTD	14	65.02
RTD	5	64.46	RTD	15	65.13
RTD	6	63.99	RTD	16	65.52
RTD	7	64.55	RTD	17	63.73
RTD	8	64.4	RTD	18	64.59
RTD	9	64.59	RTD	19	65.03
RTD	10	64.59	RTD	20	66.28

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.6191 IN F = 524.309 IN R

PRESS -1 53.697 PRESS 2 53.68

THE AVE PRESSURE IS = 53.6885 PSIA

DEWPT 1 49.29 DEWPT 4 50.02 DEWPT 2 49.99 DEWPT 5 48.91 DEWPT 3 49.15

0

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.442 THE PWV IS = .174351 PSIA

THE MASS WEIGHT IS = 780745 LBM

ADINGS TAKEN AT TIME PERIOD : 845

DINGS	TAKE	N AT TIME P	ERIOD : 8	45			DATE : 1	2/10/84
RTD	,	63.95	RTD		44 03			
RTD	2	64.45	RTD	12	64.65			
RTD	3	64.46	RTD	13	64.75			
RTD	4	64.21	RTD	14	65.03			
RTD	5	64.46	RTD	15	65.08			
RTD	6	63.99	RTD	16	65.46			
RTD	7	64.45	RTD	17	63.73			
RTD	8	64.34	RTD	18	64.53			
RTD	9	64.59	RTD	19	65.09			
RTD	10	64.65	RTD	20	66.29			
	THE	AVE RTD WI	TH WEIGHTI	NG	FACTORS	IS =	64.6036	INF

= 524.294 IN R

PRESS 1 53.696 PRESS 2 53.678

THE AVE PRESSURE IS = 53.687 PSIA

DEWPT 1 49.18 DEWPT 4 50.08 DEWPT 2 50.09 DEWPT 5 48.64 DEWPT 3 49.09

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3776 THE PWV IS = .173933 PSIA

THE MASS WEIGHT IS = 780752.1875 LBM

READINGS TAKEN AT TIME PERIOD : 900 DATE : 12/10/84

RTD	1	63.95	RTD	11	64.71
RTD	2	64.39	RTD	12	64.45
RTD	3	64.46	RTD	13	64.7
RTD	4	64.21	RTD	14	64.94
RTD	5	64.4	RTD	15	65.08
RTD	6	63.83	RTD	16	65.46
RTD	7	64.62	RTD	17	63.66
RTD	8	64.34	RTD	18	64.53
RTD	9	64.59	RTD	19	65.09
RTD	10	64.61	RTD	20	66.23

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.5774 IN F = 524.267 IN R

PRESS 1 53.695 PRESS 2 53.677

THE AVE PRESSURE IS = 53.686 PSIA

DEWPT 1 49.11 DEWPT 4 50.05 DEWPT 2 50.16 DEWPT 5 49.11 DEWPT 3 49.2

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4568 THE PWV IS = .174447 PSIA

THE MASS WEIGHT IS = 780769.25 LBM

READINGS TAKEN AT TIME PERIOD : 915 DATE : 12/10/84

RTD	1	63.89	RTD	11	64.72
RTD	2	64.39	RTD	12	64.33
RTD	3	64.46	RTD	13	64.7
RTD	4	64.21	RTD	14	65
RTD	5	64.4	RTD	15	45.08
RTD	6	63.89	RTD	16	65.46
RTD	7	64.48	RTD	17	64.64
RTD	8	64.29	RTD	18	64.48
RTD	9	64.53	RTD	19	65.03
RTD	10	64.59	RTD	20	66.29

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.588 IN F 524.278 IN R

PRESS 1 53.694 PRESS 2 53.676

THE AVE PRESSURE IS = 53.685 PSIA

DEWPT 1 49.38 DEWPT 4 50.1 DEWPT 2 49.88 DEWPT 5 48.8 DEWPT 3 49.19

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4554 THE PWV IS = .174438 PSIA

THE MASS WEIGHT IS = 780738.9375 L.BM

READINGS TAKEN AT TIME PERIOD : 930

DATE : 12/10/84

RTD	1	63.89	RTD	11	64.8
RTD	2	64.33	RTD	12	64.33
RTD	3	64.46	RTD	13	64.7
RTD	4	64.15	RTD	14	64.94
RTD	5	64.4	RTD	15	65.08
RTD	6	63.82	RTD	16	65.46
RTD	7	64.53	RTD	17	63.64
RTD	8	64.34	RTD	18	64.48
RTD	9	64.52	RTD	19	65.03
RTD	10	64.61	RTD	20	66.23

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.552 IN F = 524.242 IN R

PRESS 1 53.692 PRESS 2 53.675

THE AVE PRESSURE IS = 53.6835 PSIA

 DEWPT 1
 49.26
 DEWPT 4
 50.08

 DEWPT 2
 50.23
 DEWPT 5
 48.83

 DEWPT 3
 49.13
 48.83

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4659THE PWV IS = .174506 PSIA

THE MASS WEIGHT IS = 780769.5625 LBM

READINGS TAKEN AT TIME PERIOD : 945

DATE : 12/10/84

RTD	1	63.89	RTD	11	64.75
RTD	2	64.39	RTD	12	64.33
RTD	3	64.39	RTD	13	64.04
RTD	4	64.15	RTD	14	65.02
RTD	5	64.34	RTD	15	65.08
RTD	6	63.86	RTD	16	65.49
RTD	7	64.48	RTD	17	63.64
RTD	8	64.29	RTD	18	64.48
RTD	9	64.52	RTD	19	65.09
RTD	10	64.67	RTD	20	66.2

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.5488 IN F = 524.239 IN R

PRESS 1 53.691 PRESS 2 53.673

THE AVE PRESSURE IS = 53.682 PSIA

DEWPT 1 49.2 DEWPT 4 50.09 DEWPT 2 50.12 DEWPT 5 48.81 DEWPT 3 49.32

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4578 THE PWV IS = .174453 PSIA

THE MASS WEIGHT IS = 780753.1875 LBM

READINGS TAKEN AT TIME PERIOD : 1000

DATE : 12/10/84

RTD	1	63.89		RTD	11	64.86
RTD	2	64.33		RTD	12	64.33
RTD	3	64.39		RTD	13	64.64
RTD	4	64.15		RTD	14	64.94
RTD	5	64.34	1.1	RTD	15	65.02
RTD	6	63.86		RTD	16	65.43
RTD	7	64.42		RTD	17	63.64
RTD	8	64.29		RTD	18	64.48
RTD	9	64.52		RTD	19	65.02
RTD	10	64.5		RTD	20	66.2

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.5264 IN F = 524.216 IN R

PRESS 1 53.689 PRESS 2 53.672

THE AVE PRESSURE IS = 53.6805 PSIA

 DEWPT 1
 49.21
 DEWPT 4
 50.08

 DEWPT 2
 50.18
 DEWPT 5
 49.08

 DEWPT 3
 49.03
 49.08
 49.08

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4649 THE PWV IS = .174499 PSIA

THE MASS WEIGHT IS = 780764.1875 LBM

READINGS TAKEN AT TIME PERIOD : 1015

DATE : 12/10/84

RTD	1	63.89	RTD	11	64.71
RTD	2	64.33	RTD	12	64.33
RTD	3	64.39	RTD	13	64.64
RTD	4	64.09	RTD	14	64.9
RTD	5	64.34	RTD	15	65.02
RTD	6	63.8	RTD	16	65.35
RTD	7	64.42	RTD	17	63.58
RTD	8	64.29	RTD	18	64.48
RTD	9	64.52	RTD	19	65.02
RTD	10	64.56	RTD	. 20	66.26

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.5085 IN F = 524.198 IN R

PRESS 1 53.688 PRESS 2 53.67

THE AVE PRESSURE IS = 53.679 PSIA

DEWPT 3 49.27

 DEWPT 1
 49.24
 DEWPT 4
 50.07

 DEWPT 2
 50.04
 DEWPT 5
 49.15

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5016 THE PWV IS = .174739 PSIA

THE MASS WEIGHT IS = 780765.375 LBM

READINGS TAKEN AT TIME PERIOD : 1030 DATE : 12/10/84

RTD	1	63.83	RTD	11	64.89
RTD	2	64.33	RTD	12	64.39
RTD	3	64.39	RTD	13	54.64
RTD	4	64.09	RTD	14	64.81
RTD	5	64.34	RTD	15	65.02
RTD	6	63.85	RTD	16	65.43
RTD	7	64.37	RTD	17	63 58
RTD	8	64.23	RTD	18	64.48
RTD	9	64.52	RTD	19	63.02
RTD	10	64.45	RTD	20	66.15

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.5051 IN F = 524.195 IN R

PRESS 1 53.688 PRESS 2 53.67

THE AVE PRESSURE IS = 53.679 PSIA

DEWPT 1 49.27 DEWPT 4 50.03 DEWPT 2 50.23 DEWPT 5 48.98 DEWPT 3 49.2

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4975 THE PWV IS = .174712 PSIA

THE MASS WEIGHT IS = 780770.75 LBM

READINGS TAKEN AT TIME PERIOD : 1045 DATE : 12/10/84

· 10

RTD	1	63.83	RTD	11	64.78
RTD	2	64.27	RTD	12	64.27
RTD	3	64.33	RTD	13	64.64
RTD	4	64.09	RTD	14	64.92
RTD	5	64.29	RTD	15	65.02
RTD	6	63.7	RTD	16	65.49
RTD	7	64.43	RTD	17	63.85
RTD	8	64.23	RTD	18	64.42
RTD	9	64.45	RTD	19	65.02
RTD	10	64.45	RTD	20	66.2

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.4905 IN F = 524.18 IN R

PRESS 1 53.687 PRESS 2 53.669

THE AVE PRESSURE IS = 53.678 PSIA

DEWPT 1 49.22 DEWPT 4 50.07 DEWPT 2 50.21 DEWPT 5 49.11 DEWPT 3 49.27

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5171 THE PWV IS = .174839 PSIA

THE MASS WEIGHT IS = 780776.125 LBM

READINGS TAKEN AT TIME PERIOD : 1100

DATE : 12/10/84

RTD	1	63.83	RTD	11	64.81
RTD	2	64.33	RTD	12	64.27
RTD	3	64.31	RTD	13	64.58
RTD	4	64.09	RTD	14	64.9
RTD	5	64.34	RTD	15	65.02
RTD	6	63.82	RTD	16	65.37
RTD	7	64.42	RTD	17	63.52
RTD	8	64.23	RTD	18	64.42
RTD	9	64.45	RTD	19	65.02
RTD	10	64.45	RTD	20	66.13

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.4808 IN F = 524.171 IN R

PRESS 1 53.685 PRESS 2 53.668

THE AVE PRESSURE IS = 53.6765 PSIA

 DEWPT 1
 49.27
 DEWPT 4
 50.12

 DEWPT 2
 50.05
 DEWPT 5
 48.39
 DEWPT 3 49.27

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.3969 THE PWV IS = .174058 PSIA

THE MASS WEIGHT IS = 780780.125 LBM

READINGS TAKEN AT TIME PERIOD : 1115

DATE : 12/10/84

RTD	1	63.83	RTD	11	64.74
RTD	2	64.33	RTD	12	64.33
RTD	3	64.31	RTD	13	64.58
RTD	4	64.09	RTD	14	64.9
RTD	5	64.34	RTD	15	64.96
RTD	6	63.74	RTD	16	65.43
RTD	7	64.36	RTD	17	63.52
RTD	8	64.23	RTD	18	64.42
RTD	9	64.46	RTD	19	64.96
RTD	10	64.5	RTD	20	66.13

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.4739 IN F = 524.164 IN R

PRESS 1 53.685 PRESS 2 53.667

THE AVE PRESSURE IS = 53.676 PSIA

 DEWPT 1
 49.27
 DEWPT 4
 50.14

 DEWPT 2
 50.13
 DEWPT 5
 48.66

 DEWPT 3
 49.54
 49.54
 48.66

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5036 THE PWV IS = .174752 PSIA

THE MASS WEIGHT IS = 780773 LBM

READINGS TAKEN AT TIME PERIOD : 1130 DATE : 12/10/84

RTD	1	63.83	RTD	11	64.59
RTD	2	64.33	RTD	12	64.29
RTD	3	64.37	RTD	13	64.58
RTD	4	64.09	RTD	14	64.84
RTD	5	64.34	RTD	15	65.02
RTD	6	63.82	RTD	16	65.43
RTD	7	64.42	RTD	17	63.52
RTD	8	64.23	RTD	18	64.42
RTD	9	64.46	RTD	19	64.97
RTD	10	64.49	RTD	20	66.13

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.4742 IN F = 524.164 IN R

PRESS 1 53.684 PRESS 2 53.666

THE AVE PRESSURE IS = 53.675 PSIA

DEWPT 1 49.3 DEWPT 1 49.3 DEWPT 4 50.12 DEWPT 2 50.08 DEWPT 5 48.65 DEWPT 3 49.32

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4631 THE PWV IS = .174488 PSIA

THE MASS WEIGHT IS = 780761.75 LBM

READINGS TAKEN AT TIME PERIOD : 1145 DATE : 12/10/84

RTD	1	63.83		RTD	11	64.8
RTD	2	64.27		RTD	12	64.27
RTD	3	64.31		RTD	13	64.58
RTD	4	64.09		RTD	14	64.86
RTD	5	64.29		RTD	15	64.96
RTD	6	63.82		RTD	16	65.43
RTD	7	64.34		RTD	17	63.58
RTD	8	64.23		RTD	18	64.42
RTD	9	64.46		RTD	19	65.03
RTD	10	64.45	una de la	RTD	20	66.19

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.4721 IN F = 524.162 IN R

PRESS 1 53.682 PRESS 2 53.664

THE AVE PRESSURE IS = 53.673 PSIA

 DEWPT 1
 49.29
 DEWPT 4
 50.18

 DEWPT 2
 50.2
 DEWPT 5
 48.82

 DEWPT 3
 49.57
 48.82

(

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.56 THE PWV IS = .175119 PSIA

THE MASS WEIGHT IS = 780726.4375 LBM

READINGS	TAKE	EN AT TIME	PERIOD :	1200		DAT
RTD	1	63.77	RTD	11	64.75	
RTD	2	64.27	RTD	12	64.27	
RTD	3	64.31	RTD	13	64.58	
RTD	4	64.04	RTD	14	64.75	
RTD	5	64.29	RTD	15	64.96	
RTD	6	63.71	RTD	16	65.43	
RTD	7	64.3	RTD	17	63.45	
RTD	8	64.23	RTD	18	64.42	
RTD	9	64.46	RTD	19	64.97	
RTD	10	64.56	RTD	20	66.09	

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.4463 IN F = 524.136 IN R

PRESS 1 53.681 PRESS 2 53.664

THE AVE PRESSURE IS = 53.6725 PSIA

DEWPT 1 49.35 DEWPT 4 50.13 DEWPT 2 50.27 DEWPT 5 49.18 DEWPT 3 49.43

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.619 THE PWV IS = .175505 PSIA

THE MASS WEIGHT IS = 780752.0625 LBM

DATE : 12/10/84

READINGS TAKEN AT TIME PERIOD : 1215 DATE : 12/10/84

RTD	1	63.77	RTD	11	64.77
RTD	2	64.21	RTD	12	64.27
RTD	3	64.31	RTD	13	64.58
RTD	4	64.04	RTD	14	64.84
RTD	5	64.29	RTD	15	64.96
RTD	6	63.71	RTD	16	65.46
RTD	7	64.37	RTD	17	63.51
RTD	8	64.17	RTD	18	64.42
RTD	9	64.46	RTD	19	65.03
RTD	10	64.45	RTD	20	66.1

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.4486 IN F = 524.139 IN R

PRESS 1 53.68 PRESS 2 53.663

THE AVE PRESSURE IS = 53.6715 PSIA

 DEWPT 1
 49.31
 DEWPT 4
 50.34

 DEWPT 2
 50.02
 DEWPT 5
 49.21
 DEWPT 3 49.33

(

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5859 THE PWV IS = .175288 PSIA

THE MASS WEIGHT IS = 780737.125 LBM

READINGS TAKEN AT TIME PERIOD : 1230

p.

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DATE : 12/10/84

RTD	1	63.77	RTD	11	64.7
RTD	2	64.21	RTD	12	64.27
RTD	3	64.31	RTD	13	64.52
RTD	4	64.04	RTD	14	64.78
RTD	5	64.29	RTD	15	64.96
RTD	6	63.66	RTD	16	65.46
RTD	7	64.37	RTD	17	63.45
RTD	8	64.17	RTD	18	64.36
RTD	9	64.4	RTD	19	64.97
RTD	10	64.33	RTD	20	66.09

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.4198 IN F = 524.11 IN R

PRESS 1 53.679 PRESS 2 53.661

THE AVE PRESSURE IS = 53.67 PSIA

DEWPT 1 49.44 DEWPT 4 50.14 DEWPT 2 50.19 DEWPT 5 48.9 DEWPT 3 49.21

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5541 THE PWV IS = .175081 PSIA

THE MASS WEIGHT IS = 780761.1875 LBM

READINGS TAKEN AT TIME PERIOD : 1245 DATE : 12/10/84

RTD	1	63.77	RTD	11	64.71
RTD	2	64.29	RTD	12	64.21
RTD	3	64.26	RTD	13	64.52
RTD	4	64.04	RTD	14	64.84
RTD	5	64.29	RTD	15	64.96
RTD	6	63.79	RTD	16	65.4
RTD	.7	64.33	RTD	17	63.52
RTD	8	64.17	RTD	18	64.36
RTD	9	64.4	RTD	19	64.97
RTD	10	64.45	RTD	20	66.09

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.4326 IN F = 524.123 IN R

PRESS 1 53.678 PRESS 2 53.66

THE AVE PRESSURE IS = 53.669 PSIA

DEWPT 1 49.32 DEWPT 4 50.41 DEWPT 2 50.13 DEWPT 5 48.96 DEWPT 3 45.42

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5935 THE PWV IS = .175338 PSIA

THE MASS WEIGHT IS = 780723.6875 LBM

READINGS TAKEN AT TIME PERIOD : 1400

DATE : 12/10/84

RTD	1	63.71	RTD	11	64.75
RTD	2	64.18	RTD	12	64.2
RTD	3	64.29	RTD	13	64.46
RTD	4	63.98	RTD	14	64.68
RTD	5	64.23	RTD	15	64.9
RTD	6	63.68	RTD	16	65.34
RTD	7	64.3	RTD	17	63.41
RTD	8	64.11	RTD	18	64.3
RTD	9	64.34	RTD	19	64.97
RTD	10	64.33	RTD	20	66.07

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.3752 IN F = 524.065 IN R

PRESS	1	53.6	53	F	PRE	SS	2	53.	646
	THE	AVE	PRESSURE	IS	=	53	5.65	45	PSIA

DEWPT 1 49.44 DEWPT 4 50.23 DEWPT 2 50.24 DEWPT 3 49.42

0

DEWPT 5 48.91

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.6145 THE PWV IS = .175475 PSIA

THE MASS WEIGHT IS = 780595.5625 LBM

READINGS TAKEN AT TIME PERIOD : 1415 DATE : 12/10/84

RTD	1	63.71	RTD	11	64.56
RTD	2	64.18	RTD	12	64.09
RTD	3	64.21	RTD	13	64.46
RTD	4	63.98	RTD	14	64.83
RTD	5	64.23	RTD	15	64.9
RTD	6	63.64	RTD	16	65.37
RTD	7	64.24	RTD	17	63.41
RTD	8	64.05	RTD	18	64.3
RTD	9	64.34	RTD	19	65.03
RTD	10	64.36	RTD	20	66.01

THE AVE RTD WITH WEIGHTING FACTORS 15 = 64.3559 IN F = 524.046 IN R

PRESS 1 53.659 PRESS 2 53.642

THE AVE PRESSURE IS = 53.6505 PSIA

 DEWPT 1
 49.46
 DEWPT 4
 50.21

 DEWPT 2
 50.21
 DEWPT 5
 49.09
 DEWPT 3 49.35

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.6305 THE PWV IS = .175579 PSIA

THE MASS WEIGHT IS = 780564.5625 LBM

READINGS TAKEN AT TIME PERIOD : 1430

DATE : 12/10/84

RTD	1	63.71	RTD	11	64.62
RTD	2	64.2	RTD	12	64.15
RTD	3	64.15	RTD	13	64.46
RTD	4	63.98	RTD	14	64.78
RTD	5	64.17	RTD	15	64.84
RTD	6	63.71	RTD	16	65.4
RTD	7	64.2	RTD	17	63.41
RTD	8	64.11	RTD	18	64.3
RTD	9	64.34	RTD	19	65.03
RTD	10	64.3	RTD	20	65.98

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.3536 IN F = 524.044 IN R

PRESS 1	53.657	PRESS 2	53.639

THE AVE PRESSURE IS = 53.648 PSIA

DEWPT	1	49.42	DEWPT	4	50.24
DEWPT	2	50.23	DEWPT	5	48.91
DEWPT	3	49.32			

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5908 THE PWV IS = .17532 PSIA

THE MASS WEIGHT IS = 780535.125 LBM

READINGS TAKEN AT TIME PERIOD : 1445 DATE : 12/10/84

RTD	1	63.71	RTD	11	64.53
RTD	2	64.14	RTD	12	64.21
RTD	3	64.15	RTD	13	64.46
RTD	4	63.92	RTD	14	64.84
RTD	5	64.17	RTD	15	64.84
RTD	6	63.6	RTD	16	65.41
RTD	7	64.2	RTD	17	63.29
RTD	8	64.05	RTD	18	64.3
RTD	9	64.34	RTD	19	64.97
RTD	10	64.37	RTD	20	66

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.3383 IN F = 524.028 IN R

PRESS 1 53.654 PRESS 2 53.636

(

THE AVE PRESSURE IS = 53.645 PSIA

DEWPT 1 49.41 DEWPT 4 50.24 DEWPT 2 50.29 DEWPT 5 48.86 DEWPT 3 49.54

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.6266 THE PWV IS = .175554 PSIA

THE MASS WEIGHT IS = 780510.8125 LBM
READINGS TAKEN AT TIME PERIOD : 1500

DATE : 12/10/84

RTD	1	63.71	RTD	11	64.5
RTD	2	64.2	RTD	12	64.18
RTD	3	64.21	RTD	13	64.46
RTD	4	63.98	RTD	14	64.67
RTD	5	64.17	RTD	15	64.84
RTD	6	63.66	RTD	16	65.43
RTD	7	64.31	RTD	17	63.35
RTD	8	64.05	RTD	18	64.3
RTD	9	64.34	RTD	19	64.97
RTD	10	64.37	RTD	20	65.96

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.3475 IN F 524.038 IN R

PRESS 1 53.651 PRESS 2 53.634

THE AVE PRESSURE IS = 53.6425 PSIA

 DEWPT 1
 49.37
 DEWPT 4
 50.25

 DEWPT 2
 50.34
 DEWPT 5
 48.38

 DEWPT 3
 49.47
 49.47
 48.38

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5328 THE PWV IS = .174942 PSIN

THE MASS WEIGHT IS = 780469.5 LBM

READINGS TAKEN AT TIME PERIOD : 1515

DATE : 12/10/84

RTD	1	63.71		RTD	11	64.61
RTD	2	64.14		RTD	12	64.15
RTD	3	64.21		RTD	13	64.4
RTD	4	63.92		RTD	14	64.77
RTD	5	64.17	•	RTD	15	64.84
RTD	6	63.54		RTD	16	65.34
RTD	7	64.26		RTD	17	63.35
RTD	8	64.05		RTD	18	64.23
RTD	9	64.34		RTD	19	64.97
RTD	10	64.36		RTD	20	66.06

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.3335 IN F = 524.023 IN R

PRESS 1 53.648 PRESS 2 53.63

THE AVE PRESSURE IS = 53.639 PSIA

DEWPT 1 49.44 DEWPT 4 50.3 DEWPT 2 50.36 DEWPT 5 48.76 DEWPT 3 49.42

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.6216 THE PWV IS = .175522 PSIA

THE MASS WEIGHT IS = 780430.75 LBM

READINGS TAKEN AT TIME PERIOD : 1530 DATE : 12/10/84

RTD	1	63.66	RTD	11	64.53
RTD	2	64.14	RTD	12	64.09
RTD	3	64.15	RTD	13	64.4
RTD	4	63.92	RTD	14	64.71
RTD	5	64.17	RTD	15	64.84
RTD	6	63.55	RTD	16	65.4
RTD	7	64.21	RTD	17	63.41
RTD	8	64.05	RTD	18	64.23
RTD	9	64.29	RTD	19	64.97
RTD	10	64.33	RTD	20	66.01

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.3131 IN F = 524.003 IN R

PRESS	-1	53.644	PRESS 2 53.	627

THE AVE PRESSURE IS = 53.6355 PSIA

DEWPT 1 49.46 DEWPT 4 50.27 DEWPT 5 49.18 DEWPT 3 49.44

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.6787 THE PWV IS = .175896 PSIA

THE MASS WEIGHT IS = 780404.5625 LBM

READINGS TAKEN AT TIME PERIOD : 1545

DATE : 12/10/84

RTD 1 63.66 RTD 11 64.55 RTD 2 64.14 RTD 12 64.09 RTD 3 64.15 RTD 13 64.4 RTD 4 63.92 RTD 14 64.71 RTD 15 64.84 RTD 5 64.17 RTD 6 63.67 RTD 16 65.34 RTD 7 64.14 RTD 17 63.29 RTD 8 64.05 RTD 18 64.23 RTD 9 64.29 RTD 19 64.97 RTD 10 64.33 RTD 20 66

> THE AVE RTD WITH WEIGHTING FACTORS IS = 64.3099 IN F = 524 IN R

PRESS 1 53.642 PRESS 2 53.624

THE AVE PRESSURE IS = 53.633 PSIA

DEWPT 1 49.41 DEWPT 2 50.41 DEWPT 3 49.37 DEWPT 4 50.19 DEWPT 5 48.92

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.6198THE PWV IS = .17551 PSIA

THE MASS WEIGHT IS = 780378.5 LBM

READINGS TAKEN AT TIME PERIOD : 1600

DATE : 12/10/84

RTD	1	63.66	RTD	11	64.45
RTD	2	64.14	RTD	12	64.09
RTD	3	64.15	RTD	13	64.4
RTD	4	63.92	RTD	14	64.78
RTD	5	64.17	RTD	15	64.84
RTD	6	63.61	RTD	16	65.4
RTD	7	64.2	RTD	17	63.35
RTD	8	64.05	RTD	18	64.23
RTD	9	64.29	RTD	19	64.97
RTD	10 .	64.27	RTD	20	66

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.3095 IN F = 523.999 IN R

PRESS 1 53.639 PRESS 2 53.621

THE AVE PRESSURE IS = 53.63 PSIA

DEWPT 1 49.42 DEWPT 4 50.31 DEWPT 2 50.36 DEWPT 5 49.03 DEWPT 3 49.19

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.622 THE PWV IS = .175524 PSIA

THE MASS WEIGHT IS = 780335.1875 LBM

READINGS TAKEN AT TIME PERIOD : 1615

DATE : 12/10/84

RTD	1	63.66	RTD	11	64.65
RTD	2	64.14	RTD	12	64.09
RTD	3	64.15	RTD	13	64.4
RTD	4	63.92	RTD	14	64.67
RTD	5	64.17	RTD	15	64.84
RTD	6	63.61	RTD	16	65.4
RTD	7	64.21	RTD	17	63.35
RTD	8	64.05	RTD	18	64.23
RTD	9	64.29	RTD	19	65.03
RTD	10	64.27	RTD	20	65.93

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.3153 IN F = 524.005 IN R

PRESS 1 53.635 PRESS 2 53.619

THE AVE PRESSURE IS = 53.627 PSIA

 DEWPT 1
 49.54
 DEWPT 4
 50.3

 DEWPT 2
 50.51
 DEWPT 5
 48.83

 DEWPT 3
 49.18
 49.18
 48.83

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.6513 THE PWV IS = .175716 PSIA

THE MASS WEIGHT IS = 780279.875 LBM

DATE : 12/1	READINGS	TAKEN AT	TIME PERIOD :	1630	DATE :	12/10/84
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RTD	1	63.66	RTD	11	64.5
RTD	2	64.14	RTD	12	64.04
RTD	3	64.15	RTD	13	64.4
RTD	4	63.92	RTD	14	64.71
RTD	5	64.11	RTD	15	64.77
RTD	6	63.61	RTD	16	65.4
RTD	7	64.15	RTD	17	63.35
RTD	8	64.05	RTD	18	64.23
RTD	9	64.29	RTD	19	64.97
RTD	10	64.27	RTD	20	65.93

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.294 IN F = 523.984 IN R

	PRESS 1	53.632	PRESS 2	53.615
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THE AVE PRESSURE IS = 53.6235 PSIA

DEWPT	1	49.44	DEWPT	4	50.29
DEWPT	2	50.34	DEWPT	5	48.33
DEWPT	3	49.42			

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5461 THE PWV IS = .175029 PSIA

THE MASS WEIGHT IS = 780270.5 LBM

READINGS	TAKEN	AT	TIME	PERIOD	:	1645	

RTD	1	63.6	RTD	11	64.48	
RTD	2	64.14	RTD	12	64.09	
RTD	3	64.15	RTD	13	64.4	
RTD	4	63.92	RTD	14	64.71	
RTD	5	64.11	RTD	15	64.77	
RTD	6	63.6	RTD	16	65.4	
RTD	7	64.15	RTD	17	63.35	
RTD	8	63.99	RTD	18	64.23	
RTD	9	64.23	RTD	19	64.97	
RTD	10	64.21	RTD	20	65.93	

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.2817 IN F = 523.972 IN R

PRESS 1 53.629 PRESS 2 53.612

THE AVE PRESSURE IS = 53.6205 PSIA

DEWPT 1 49.41 DEWPT 4 50.27 DEWPT 2 50.38 DEWPT 5 48.5 DEWPT 3 49.66

RTD 1 63 6

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.608 THE PWV IS = .175433 PSIA

THE MASS WEIGHT IS = 780239.125 LBM

DATE : 12/10/84

READINGS TAKEN AT TIME PERIOD : 1700

DATE : 12/10/84

RTD	1	63.66	R7D	11	64.49
RTD	2	64.07	RTD	12	64.07
RTD	3	64.14	RTD	13	64.34
RTD	4	63.86	RTD	14	64.62
RTD	5	64.11	RTD	15	64.77
RTD	6	63.58	RTD	16	65.41
RTD	7	64.15	RTD	17	63.35
RTD	8	63.99	RTD	18	64.23
RTD	9	64.23	RTD	19	64.97
RTD	10	64.18	RTD	20	65.88

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.2652 IN F = 523.955 IN R

PRESS 1 53.626 PRESS 2 53.609

THE AVE PRESSURE IS = 53.6175 PSIA

DEWPT 1 49.44 DEWPT 2 50.24 DEWPT 3 49.32

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DEWPT 4 50.36 DEWPT 5 48.14

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4926 THE PWV IS = .17468 PSIA

THE MASS WEIGHT IS = 780231 LBM

READINGS TAKEN AT TIME PERIOD : 1715

DATE : 12/10/84

RTD	1	63.66	RTD	11	64.48
RTD	2	64.12	RTD	12	64.04
RTD	3	64.14	RTD	13	64.34
RTD	4	63.92	RTD	14	64.7
RTD	5	64.11	RTD	15	64.77
RTD	6	63.58	RTD	16	65.37
RTD	7	64.15	RTD	17	63.35
RTD	8	63.99	RTD	18	64.23
RTD	9	64.23	RTD	19	64.97
RTD	10	64.26	RTD	20	65.87

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.2753 IN F = 523.965 IN R

PRESS 1 53.623 PRESS 2 53.607

THE AVE PRESSURE IS = 53.615 PSIA

 DEWPT 1
 49.49
 DEWPT 4
 50.36

 DEWPT 2
 50.29
 DEWPT 5
 48.74

 DEWPT 3
 49.33
 48.74

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.6178 THE PWV IS = .175497 PSIA

THE MASS WEIGHT IS = 780167.5625 LBM

READINGS TAKEN AT TIME PERIOD : 1730

DATE : 12/10/84

RTD	1	63.66	RTD	11	64.5
RTD	2	64.07	RTD	12	64.04
RTD	3	64.08	RTD	13	64.34
RTD	4	63.86	RTD	14	64.62
RTD	5	64.11	RTD	15	64.77
RTD	6	63.52	RTD	16	65.37
RTD	7	64.15	RTD	17	63.35
RTD	8	63.79	RTD	18	64.23
RTD	9	64.23	RTD	19	64.92
RTD	10	64.27	RTD	20	65.88

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.2588 IN F = 523.949 IN R

PRESS 1 53.62 PRESS 2 53.604

THE AVE PRESSURE IS = 53.612 PSIA

 DEWPT 1
 49.48
 DEWPT 4
 50.32

 DEWPT 2
 50.42
 DEWPT 5
 47.52
 DEWPT 3 49.54

.

THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.4653 THE PWV IS = .174503 PSIA

THE MASS WEIGHT IS = 780162.6875 LBM

READINGS TAKEN AT TIME PERIOD : 1745

DATE : 12/10/84

RTD	1	63.6		RTD	11	64.64
RTD	2	64.05		RTD	12	64.04
RTD	3	64.12		RTD	13	64.34
RTD	4	63.86		RTD	14	64.55
RTD	5	64.11	•	RTD	15	64.77
RTD	6	63.55		RTD	16	65.31
RTD	7	64.09		RTD	17	63.29
RTD	8	63.99		RTD	18	64.23
RTD	9	64.29		RTD	19	01.97
RTD	10	64.2		RTC	20	65.9

THE AVE RTD WITH WEIGHTING FACTORS IS = 64.2558 IN F = 523.946 IN R

FPESS 1 53.617 PRESS 2 53.601

0

THE AVE PRESSURE IS = 53.609 PSIA

DEWPT 1 49.42 DEWPT 4 50.34 DEWPT 2 50.34 DEWPT 5 48.54 DEWPT 3 49.38

> THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5753 THE PWV IS = .175219 PSIA

> > 5

THE MASS WEIGHT IS = 780113 LBM

REA	ADINGS	TAKE	N AT TIME PER	100: 1	800	0		DA	TE :	12/10	0/84	ł
	RTD	1	63.6	RTD	11	64.64						
	RTD	2	64.05	RTD	12	63.98						
	RTD	3	64.12	RTD	13	64.34						
	RTD	4	63.86	RTD	14	64.53						i.
	RTD	5	64.11	RTD	15	64.77						
	RTD	6	63.55	RTD	16	65.24						
	RTD	7	64.09	RTD	17	63.23						
	RTD	8	63.99	RTD	18	64.17						
	RTD	9	64.23	RTD	19	64.99						
	RTD	10	64.18	RTD	20	65.82						
		THE	AVE RTD WITH	WEIGHTI	NG	FACTORS	IS	= 64	. 237	8 IN	F	
								= 52	3.92	8 IN	R	

PRESS 1 53.614 PRESS 2 53.598

THE AVE PRESSURE IS = 53.606 PSIA

DEWPT	1	49.55	DEWPT	4	50.27
DEWPT	2	50.41	DEWPT	5	47.74
DEWPT	3	49.62		_	

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THE AVE DEWPOINT WITH WEIGHTING FACTORS IS = 49.5284 THE PWV IS = .174913 PSIA

THE MASS WEIGHT IS = 780100.5 LBM

APPENDIX F

TYPE B AND C LEAKAGE RATE HISTORIES

C

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DATE: 1980-1982 CONTAINMENT VESSEL LOCAL LEAK RATE TEST 1982 ST 5061.02 ADDITIONAL TESTS

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D	-	-	-		
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		-	-		

Pent No	Valves	Valve Leakage As Left SCCM	Pent Leakage As Left SCCM	Comments
43B	CV5011E	0	0	10-6-80
44B	NN58	1000	1000	7-11-20
67	CV 210	370	370	7-30-80
80	Emergency Lock (Volumetric)	0	0	11-10-80
80	Emergency Lock (Volumetric)	0	0	5-12-91
80	Emergency Lock (Volumetric)	0	0	9-11-81
81	Personnel Lock (Volumetric)	447	447	
81	Personnel Lock (Volumetric)	791	791	5 20 01
81	Personnel Lock (Volumetric)	800	800	10-12-91
82	Equipment Hatch	50	50	9_29_90
82	Equipment Hatch	0	0	1-25-81
82	Equipment Hatch	0	0	4-20-91
82	Equipment Hatch	0	0	7-14-81
				1-14-01

APPENDIX F

OCAL LEAK RATE TEST Page 2 S	Connents	11-28-81	1-28-81	1-28-81						
NTAINMENT VESSEL I ST 5061.02 ADDITIONAL TEST	Pent Leakage As Left SCCM	0	0	0						
DATE: 1980-82 CO	Valve Leakage As Left SCCM	0	0	0		- 0				
	Valves	Equipment Hatch	Elect Penetration	Elect Penetration						
	Pent No	82	102	101	11. P.D. M4					

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APPENDIX F

D	1	Valve	Leakage	Penetration Leakage			
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments	
1. 1.	RC240A	0	0			1	
1	RC240B	303	303	303	303	10.000	
3	CC 1411A, CC 1411B	> 3800	0	>3800	0	1	
4	CC 1407A, CC 1407B	40	40	. 40	40	1	
88	CV 5070, CV 5080	2000	2000	2000	2000	1 .	
8B	CV 5071, CV 5081	1202	1202	1202	1202	1	
8C	CV 5072, CV 5082	0	0	0	0		
8D	CV 5073, CV 5083	0	0	0	0		
. 8E	CV 5074, CV 5084	180	180	180	180	1	
8F	CV 5075, CV 5085	0	0	0	0		
8G	CV 5076, CV 5086	0	0	0	0		
8H	CV 5077, CV 5087	0	C	0	0	1.6.1.10.0.	
81	CV 5078, CV 5088	0	0	0	0		
8J	CV 5079, CV 5089	0	0	0	0	1	
12	CC 1567A	0	0			1	
	CC 1567B	0	0	0	0		
13	DR 2012A	50	50			1	
	DR 2012B	0	0	30	50		
14	MU 3	0	0				
	MU 2A	0	0	0	0		
16	RC 1719A	0	0				
	RC 1719B	0	0	0	0		
17	CV 343	248	248				
	Blind Flanges	248	248	248	248		
19	MU 33	35	35	35	35		
				A REAL PROPERTY AND A REAL	The second	4	

Page 3

APPENDIX F

		Valve	Leakage	Penetration Leakage			
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SUCM	Comments	
21	DW 6831A	0	0				
	DW 6831B	0	0	0	0		
23	Fuel Trans Flng	0	0			-	
	Fuel Trans Fing	0	0		0	1946년 - 19 ⁴ 년 1947년 19	
24	Fuel Trans Fing	0	0			-	
	Fuel Trans Fing	0	0	0	0		
25	SA 532, SA 536	0	0			-	
CS 33	0	0] 0	0			
	CS 17	0	0		ľ		
	SA 533, SA 535	0	0				
26	CS 36	0	0	0	0		
	CS 18	0	0				
29	DH 23	0	0	0	0	-	
30	Emer. Sump Guard	0	0	0	0	-	
31	Emer. Sump Guard	0	0	0	0	-	
32	RC 1773A	0	0			-	
52	RC 1773B	0	0	0	0		
33	CV 5005, CV 5006	*	17,400	*	17,400	*Penetration could	
34	CV 5007, CV 5008	3,796	3,796	3,796	3 796	- Ized	
37	Feed Wtr Inner Bellows	0	0	1	3,720	-	
	Feed Wir Outer Bellows	0	0	0	0		
38	Feed Wtr Inner Bellows	0	0				
	Feed Wir Outer Bellows	0	0	0	0		
30	Main Steam Inner Bellows	0	0				
Main Steam Outer Bel	Main Steam Outer Bellows	0	0	0	0		
40	Main Steam Inner Bellows	0	0			-	
40	Miln Steam Outer Bellows	0	0	0	0	APPENDIX F	

APPENDIX F

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		Valve	Leakage	Penetration Leakage		
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments
41	RC 113	0	0			
	RC 232	0	0	0	0	
42A	SA 502	> 3,800	1,298	73,800	1.298	-
	SA 2010	>3,800	0		1,250	
42B	CV 124	0	0			1
	CV 5010E	0	. 0	0	0	
43A	IA 501	251	251			1
	TA 2011	198	198	251	251	1.1.1.1.1.1.1.1.1
43B	CV 125	> 3,800	0			1.
	CV 5011E	0	0	> 3,800	0	
44A	CF 15	727	727			1
	CF 1541	> 3,800	, 80	>3,800	727	
44B	NN 58	954	0			
	NN 236	100	100	954	100	
	CF 1545	75	75	7.54	100	
47A	CF 2A	75	75	75	75	
	CF 2B	0	0			
	CF 5A	0	0			
47B	CF 5B	0	0	90	90	
	CF 1542	90	90			
1.9	RC 229A	0	0			
40	RC 229B	0	0	0	0	
49	DH 87	0	0			
	DH 88	0	0	0	0	
51	DH 5037, DH 5038	0	0	0	0	

1.1.1		Valve Leakage		Penetratio	n Leakage	1
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Lett SCCM	Comments
52	MU 242	3,577	238			
	MU 66A	2,096	0	3,577	238	
53	MU 243	0	0			
	MU 66B	1,996	0	1,996	0	
54	MU 244	605	605			
	MU 66C	0	0	605	605	
55	MU 245	0	0			
	MU 66D	25	25	25	25	
56	MU 38, MU 59A, B, C, D	0	0	0	0	-
59	Blind Flanges	0	0	0	- 0	-
67	CV 210	1,447	324	2,500	864	
	CV 5090	2,500	864		004	
68A	SS 235A	90	90			
	SS 235B	0	0	90	90	
68B	CV 5010B, CV 5011B	0	0	0	0	
69	CV 209	361	361			
	CV 5065	601	601	601	601	
718	CV 5010A, CV 5011A	*	20	*	20	*Penetration could
710	CF 16	677	754			Ized
	CF 1544	0	0	677	754	
738	CV 5010C, CV 5011C	0	0	0	0	
74B	CV 5010D, CV 5011D	49	49	49	49	
740	DH 2735	0	0			7
	DH 2736	0	0	0	0	
80	Emer, Lock	0	0	0	0	
81	Personnel Lock	0	0	0	0	
	1					APPENDIX F

DATE:	1982	CONTAINMENT	VESSEL	LOCAL	LEAK	RATE	TEST	
		ST	5061.02					

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.Page 7

Pent No		Valve I	Leakage	Penetration	1.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2	
	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Conments
. 82	Equip. Hatch	0	0	0	0	
101	Elect. Pent.	0	0	0	0	
102	Elect. Pent.	. 0	0	0	0	

LEAKAGE TOTAL

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31,041

Page 8	nts											APPENDIX F
JCAL LEAK RATE TEST	Counte	7-17-82	7-23-82	9-14-82	9-15-82	1-19-83	1-19-83	5-26-83	3-27-83			
ATAINMENT VESSEL LU ST 5061.02 ADDITIONAL TESTS	Pent Leakage As Left SCCM	0	0	266	296	1,016	1,742	0	0			
DATE: 1982-83 CON	Valve Leakage As Left SCCM	0	0	266	296	1,016	1,742	0	0			
	Valves	PTP38X	P2L4GX	Emergency Hatch	Personnel Lock	Emergency Lock	Personnel Lock	Emergency Lock	Personnel Lock			
	Pent No	101	101	80	81	80	81	80	81			

Valve Leakage Penetration Leakage Pent No. Valves As Found As Left As Found As Left Comments SCCM SCCM SCCM SCCM **RC240A** 0 0 1 0 0 **RC240B** 0 0 *Penetration could 3 CC 1411A, CC 1411B * 0 ŵ. 0 not be pressur-Ized 4 CC 1407A, CC 1407B 610,000 2,900 610,000 2,900 On Pen. 3 only A8 CV 5070, CV 5080 CC1411B was 0 0 0 0 worked 8B 0 CV 5071, CV 5081 0 0 0 8C CV 5072, CV 5082 0 0 0 0 8D . CV 5073, CV 5083 0 0 0 0 8E CV 5074, CV 5084 0 0 0 0 8F CV 5075, CV 5085 0 0 0 0 8G CV 5076, CV 5086 0 0 0 0 8H CV 5077, CV 5087 0 0 0 0 81 CV 5078, CV 5088 0 6 0 0 **8**J 0 CV 5079, CV 5089 0 0 0 CC 1567A 0 0 12 0 0 CC 1567B 0 0 DR 2012A 350,000 0 13 350,000 0 DR 2012B 0 0 MU 3 0 0 14 0 0 MU 2A 0 0 RC 1719A 0 16 0 0 0 RC 1719B 0 0 CV 343 250 250 17 270 270 Blind Flanges 270 270 19 MU 33 0 0 0 0

APPENDIX F

e	1 1	Valve	Leakage	Penetratio		
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments
21	DW 6831A	700	700			
	DW 68318	725	725	725	725	
23	Fuel Trans Fing	0	0	1		-
	Fuel Trans Fing	0	0	- 0	0	
24	Fuel Trans Fing	0	0			-
	Fuel Trans Flng	0	0	- 0	0	
25	SA 532, SA 536	50	50		1	-
	CS 33	0	0	50	50	
	CS 17	0	0		50	
	SA 533, SA 535	0	0			-
26	CS 36	0	0	0	0	
	CS 18	0	0			
29	DH 23	0	0	0	0	
30	Emer. Sump Guard	0	0	0	0	-
31	Emer. Sump Guard	0	0	0	0	-
32	RC 1773A	0	0			
	RC 1773B	0	0		0	
33	CV 5005, CV 5006	395	395	395	395	1
34	CV 5007, CV 5008	960	960	960	950	-
37	Feed Wtr Inner Bellows	0	0		200	-
	Feed Wir Outer Bellows	0	0	0	0	
38	Feed Wtr Inner Bellows	0	0			-
	Feed Wtr Outer Bellows	0	0	1 0	0	
39	Hain Steam Inner Bellows	0	0			1
	Main Steam Outer Bellows	0	0	0	0	
40 -	Main Steam Inner Bellows	0	0			
	huln Steam Outer Bellows	0	0	0	0	APPENDIX F

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Burnt Ma		Valve	Leakage	Penetration Leakage		
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments
41	RC 113	0	0			
	RC 232	165	165	165	165	
42A	SA 502	0	0			Comments
	SA 2010	68,600	735	68,600	735	
428	CV 124	260	260	240		1
	CV 5010E	0	. 0	260	260	
43A	IA 501	130	130	176		1
	IA 2011	175	175	175	175	
43B	CV 125	0	0	-		
	CV SOILE	0	0	0	0	
44A	CF 15	0	0			
	CF 1541	0	0	0	0	
44B	NN 58	595	595	705		
	NN 236	795	795	7 /95	795	
	CF 1545	0	0			
47A	CF 2A	0	0	1 0		
	CF 2B	0	0		U	
	CF 5A	0	0			
47B	CF 5B	0	0	60	60	
	CF 1542	60	60	1.1.1.1.1.1.1.1.1	50	
4.8	RC 229A	0	0			
10	RC 229B	0	0	0	0	
49	DH 87	195	195			
	DH 88	0	0	195	195	
51	DH 5037, DH 5038	0	0	0		

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Punt No		Valve Leakage		Penetratio	Penetration Leakage			
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments		
52	MU 242	110	110					
	MU 66A	0	0	110	110			
53	MU 243	0	0					1
	MU 66B	0	0	0	0			
54	MU 244	1,655	1,655			1		
	MU 66C	0	0	1,655	1,655			
55	MU 245	0	0			1		
	MU 66D	0	0	7 0	0			
56	MU 38, MU 59A, B, C, D	0	0	0	0	1		
59	Blind Flanges	0	0	0	0	1		
67	CV 210	365	365	1.005		1		
	CV 5090	1,235	1,235	1,235	1,235	1		
68A	SS 235A	40	40	40	40	1		
	SS 2358	0	0		40			
68B	CV 5010B, CV 5011B	0	0	0	0	1		
69	CV 209	40	40					
	CV 5065	0	0	40	40	1.000		
718	CV 5010A, CV 5011A	0	0	0	0	1		
710	CF 16	420	420	100		1		
	CF 1544	0	0	420	420			
73B	CV 5010C, CV 5011C	0	0	0	0	1		
74B	CV 5010D, CV 5011D	0	0	0	0	1		
74C	DH 2735	0	0]		
	DH 2736	0	0	0	0			
80	Emer. Lock					2 81 & 80 not		
81	Personnel Lock					Included in thi		
						1		

APPENDIX *

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DATE: 1983 CONTAINMENT VESSEL LOCAL LEAK RATE TEST ST 5061.02

· Page 13

٠,		Valve	Leakage	Penetration	1	
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments
82	Equip. Hatch	0	0	0	0	
101	Elect. Pent.	0	0	0	0	1
102	Elect. Pent.	40	40	40	40	1

TOTAL LEAKAGE

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DATE:1983684 CONTAINMENT VESSEL LOCAL LEAK RATE TEST ST 5061.02 ADDITIONAL TESTS	Valve Leakage Pent Leakage As Left As Left Cumaents SCCM SCCM	0 0 9-24-83	pp1y 175 9-28-83	teturn 0 0 9-29-83	0 0 12-6-83	40 40 12-6-83	165 3-3-84	40 4-3-84	0 0 4-4-84			
DA	Valves Valves As	RC 24.3B	CV 5090-H2 dll supply	CTMT Air Sample Return CV 5011E	Emergency Lock	Personnel Lock	Przr Aux Spray DH 2735	Personnel Lock	Emergency Lock			
	Pent No	-	67	438	60	81	74C	18	80			

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Pent No	1	Valve	Leakage	Penetratio	n Leakage	
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments
	RC240A	0*	0			
1	RC240B	0+	0	0	0	
3	CC 1411A, CC 1411B	*	423	*	423	Only CC14118 Was worked
4	CC 1407A, CC 1407B	2,330+	2,330	2,330	2,330	*Penetration could not be
8A	CV 5070, CV 5080	397	397	397	397	pressurized
8B	CV 5071, CV 5081	30	30	30	30	
8C	CV 5072, CV 5082	0	0	0	0	-
8D	CV 5073, CV 5083	0	0	0	0	-
8E	CV 5074, CV 5084	249	249	249	249	
8F	CV 5075, CV 5085	100	100	100	100	
8G	CV 5076, CV 5086	50	50	50	50	
8H	CV 5077, CV 5087	80	80	80	80	
81	CV 5078, CV 5088	100	100	100	100	
8J	CV 5079, CV 5089	100	100	100	100	
12	CC 1567A	0	0			
	CC 1567B	0*	0	0	0	
13	DR 2012A	300	300	220		
	DR 20128	329*	329	329	329	
14	MU 3	400	. 400	400	(00	
	MU 2A	0	0	400	400	
16	RC 1719A	0	0			
	RC 1719B	0	0	0	0	
17	CV 343	199	119	228	168	State State
	Blind Flanges	228	168			_
19	MU 33	0	0	0	0	

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Pent No		Vaive	Leakage	Penetratio	n Leakage	
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments
21	DW 6831A	129	129		-	
	DW 6831B	40	40	129	129	
23	Fuel Trans Flng	0	0			-
	Fuel Trans Fing	0	0	0	0	
24	Fuel Trans Fing	0	0			-
	Fuel Trans Fing	0	0	- 0	0	
25	SA 532, SA 536	0	0			-
	CS 33	73	73	73 73		
	CS 17	0	0		1 "	
26	SA 533, SA 535	100	100			-
	CS 36	0	0	100	100	
	CS 18	0	0	1	100	
29	DII 23	0	0	0	0	-
30	Emer. Sump Guard	0	0	0	0	1
31	Emer. Sump Guard	0	0	0	0	
32	RC 1773A	0	0		1	1
	RC 1773B	0	0	0	0	
33	CV 5005, CV 5006	700,000	504	700.000	50%	
34	CV 5007, CV 5008	371	1,188	371	1 199	-
37	Feed Wtr Inner Bellow:	0	0		1,100	-
	Feed Wtr Outer Bellows	0	0	0	0	
38	Feed Wtr Inner Bellows	0	0			1
50	Feed Wtr Outer Bellows	0	0	0	0	
20	Main Steam Inner Bellows	0	0			-
39	Main Steam Outer Bellows	0	0	0	0	1.0.0
10	Main Steam Inner Bellows	0	0			
40	Miln Steam Outer Bellows	0	0	0	0	APPENDIX F

DATE: 1984

CONTAINMENT VESSEL LOCAL LEAK RATE TEST ST 5061.02

		valve	Leakage	Penetration	1 Leakage		
Pent No	Valves	As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments	
41	RC 113	34,400	0	21 100			
	RC 232	368	368	34,400	368		
42A	SA 502	89	89				
	SA 2010	11,814	280	11,814	280		
42B	CV 124	330	330				
	CV 5010E	0 *	. 0	330	330		
43A	TA 501	90	90		00		
	IA 2011	30	30		90	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	
43B	CV 125	0	0	1. The superior			
	CV 5011E	0	0	0	0		
44A	CF 15	775	775			*Penetration could not be	
	CF 1541	*	1,869	*	1,869	pressurized	
44B	NN 58	0	0				
	NN 236	0	0	0	0		
	CF 1545	100	100				
47A	CF 2A	161	161	161	161 10	161	1
	CF 2B	0	0				
	CF 5A	. 65	65				
47B	CF 5B	60 *	60	125	125		
	CF 1542	100 -	100				
10	RC 229A	0	0				
40	RC 229B	0	0	0	0		
49	DH 87	0	0	0			
49	DH 88	0	0		0	0	
51	DH 5037, DH 5038	C	0	0	0		
	second se		and the second		The second	and the second se	

APPENDIX F

Pent No	Valves	Valve Leakage		Penetration Leakage		1
		As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comfacuts
52	MU 242	1,191	1,191	1,191	1,191	
	MU 66A	0	0			
53	MU 243	0	0	0	0	
	MU 66B	0	0			
54	MU 244	1,494	1,494	1,494	1,494	
	MU 66C	0	0			
55	MU 245	178	178	178	178	
	MU 66D	0	0			
56	MU 38, MU 59A, B, C, D	0	0	0	0	-
59	Blind Flanges	75	75	75	75	
67	CV 210	966	966	966	966	
	CV 5090	247	247			
68A	SS 235A	0	0	0	0	
	SS 235B	0	0			
68B	CV 5010B, CV 5011B	0	0	0	0	-
69	CV 209	0	· 0	0	0	*Penetration could not be pressurized.
	CV 5065	0	0			
718	CV 5010A, CV 5011A	• 0	0	0	0	
710	CF 16	853	853	853	853	
	CF 1544	0	0			
738	CV 5010C, CV 5011C	0	0	0	0	
74B	CV 5010D, CV 5011D	0 *	0	0	0	
74C	DH 2735	0 *	0	. 0	0	
	DH 2736	0 +	0			
80	Emer. Lock	826	826	826	826	
81	Personnel Lock	*	1,743	*	1,743	Only lower interior handwheel on exter-
					APPENDIX F	ed.

Page 19

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Pent No	Valves	Valve Leakage		Penetration Leakage		1
		As Found SCCM	As Left SCCM	As Found SCCM	As Left SCCM	Comments
82	Equip. Hatch	0	0	0	0	
101	Elect. Pent.	0	0	0	0	-
102	Elect. Pent.	0	0	0	1 0	-
73A	Pressure Sensing Line	0	0	0	0	73A tested since
						in 1984.

TOTAL LEAKAGE

17,299

+Maintenance Performed on Valve