## SAN ONOFRE

1984 AUG 30 PH 1:04
NUCLEAR GENERATING STATION

## UNITS 2 \& 3



## SEMIANNUAL EFFLUENT REPORT

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## SEMIANNUAL EFFLUENT REPORT

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January - June 1984
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## SECTION A. INTRODUCTION

This Semiannual Report summarizes the gaseous and liquid radioactive effluent releases and solid waste shipments made from the San Onofre Nuclear Generating Station, Units 2 and 3. This report is prepared in the general format of USNRC Regulatory Guide 1.21 and includes:

1. Quarterly summaries of liquid and gaseous effluents for "batch" and "continuous" modes of release;
2. Percent of Technical Specification Limits;
3. Estimated total percent error;
4. Lower limit of detection concentrations;
5. Meteorological data;
6. 10 CFR 50 Appendix I considerations;
7. 40 CFR 190 considerations;
8. Radwaste shipments.

## SECTION B. GASEOUS EFFLUENTS

Table 1A, "Gaseous Effluents - Summation of All Releases," provides a detailed listing of gaseous effluents released quarterly in four categories: fission and activation gases, iodine-131, particulates with half-lives greater than eight days, and tritium. Listed are the total releases of each category, the average release rate for the quarter, and the percent of Technical Specification Limit (TSL).

The percent estimated total error is listed in Table $1 A$ for each of the four gaseous effluent categories. The methodology used for error analysis is described in Section F of this report.

Table 1B, "Gaseous Effluents - Elevated Release," has not been included in this report since it is assigned to elevated releases and San Onofre Nuclear Generating Station Units 2 and 3 do not have elevated releases.

Table 1C, "Gaseous Effluents - Ground-Level Releases," provides the systematic listing by radionuclide for the quantity of radioactivity released in three categories: fission gases, iodines, and particulates. The total radioactivity for each radionuclide is listed for each quarterly period by both "continuous" and "batch" modes of release.

Waste gas decay tank and calibration releases are considered to be "batch" releases. Containment purges, steam jet air ejector and plant stack releases are considered to be "continuous" releases.

Table 10, "Gaseous Effluents - Lower Limit of Detection," provides the listing of lower limit of detection concentrations for radionuclides not detected in Table 1C.

Table 1E, "Gaseous Effluents - Radiation Doses at Site Boundary," provides a summary of doses at the site boundary for this reporting period, by quarter.

The values for the composite gross alpha, $\mathrm{Sr}-89$ and $\mathrm{Sr}-90$, (Tables 1 A and Table 1C Gaseous Effluents), for the July - Decemioer 1983 Semiannual Report were incomplete because data was not available prior to reporting time. The Fe-55 values are for the months of November and December; the October values were reported in the last Semiannual Report. The values not reported were for the fourth quarter, 1983. The values not reported are as follows:

Unit

| Gross alpha | Ci | $6.66 \mathrm{E}-7$ |
| :--- | :--- | :--- |
| $\mathrm{FE}-55$ | Ci | $5.37 \mathrm{E}-5$ |
| $\mathrm{Sr}-89$ | Ci | $5.19 \mathrm{E}-6$ |
| $\mathrm{Sr}-90$ | Ci | $4.12 \mathrm{E}-7$ |


| Unit | Quarter <br> First | Quarter <br> Second |
| :--- | :--- | :--- | | Est. Total |
| :--- |
| Error, \% |

A. Fission \& activation gases

| 1.Tctal release Ci $6.34 \mathrm{E}+3$ $1.28 \mathrm{E}+4$ | $2.50 \mathrm{E}+1$ |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 2.Average release <br> rate for period | $\mu \mathrm{Ci} / \mathrm{sec}$ | $8.07 \mathrm{E}+2$ | $1.63 \mathrm{E}+3$ |  |
| 3.Percent of technical <br> specification limit | $\%$ | $6.55 \mathrm{E}+0$ | $1.31 \mathrm{E}+1$ |  |

B. Iodines

1. Total iodine-131
Ci
2. $32 \mathrm{E}-2$
3. $25 \mathrm{E}-1$
4. $90 \mathrm{E}+1$
5. Average reiease rate for period
$\mu \mathrm{Ci} / \mathrm{sec}$
1.19E-2
6. 13E-2
7. Percent of technical specification limit
\%
$2.38 \mathrm{E}-1$
$8.76 \mathrm{E}-1$
C. Particulates
8. Particulates with
half-lives $>8$ days
Ci
$1.01 \mathrm{E}-3$
9. $30 \mathrm{E}-4$
10. $60 \mathrm{E}+1$
11. Average release rate for period
$\mu \mathrm{Ci} / \mathrm{sec}$
12. $28 \mathrm{E}-4$
1.06E-4
13. Percent of technical specification limit
\%
1.22E-3
14. $21 \mathrm{E}-3$
15. Gross alpha
radioactivity
Ci
16. 68E-6
5.00E+1
D. Tritium
17. Total release
Ci
$1.79 E+2$
$2.76 \mathrm{E}-1$
18. $50 \mathrm{E}+1$
19. Average release rate for period
$\mu \mathrm{Ci} / \sec$
20. $28 \mathrm{E}+1$
$3.51 \mathrm{E}-2$
21. Percent of technical
specification limit $\quad$ 2.73E-1 $22 \mathrm{E}-4$
*Second quarter analyses not available at report time; analysis will be included in the following Semiannual Report.

TABLE IC
EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1984)
GASEOUS EFFLUENTS - GROUND-LEVEL RELEASES

|  | Continuous Mode |  |  | Batch Mode |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Nuclides Released | Unit | Quarter First | Quarter <br> Second | Quarter First | Quarter Second |

1. Fission Gases

| argon-41 | Ci | 2.25E+0 | 4. $39 \mathrm{E}+0$ | LLD | LLD |
| :---: | :---: | :---: | :---: | :---: | :---: |
| krypton-85 | Ci | LLD | LLD | $5: 68 \mathrm{E}+0$ | 1.87E+1 |
| krypton-85m | Ci | $3.41 E+0$ | 3.60E-1 | 2.53E-2 | 9.87E-3 |
| krypton-87 | Ci | LLD | 7.66E-3 | 1.54E-3 | LLD |
| krypton-88 | Ci | 2.69E-9 | 1.20E-1 | $1.69 \mathrm{E}-2$ | LLD |
| xenon-131m | Ci | 1.18E+1 | $1.71 \mathrm{E}+1$ | $1.09 \mathrm{E}+1$ | $2.90 \mathrm{E}+1$ |
| xenon-133 | Ci | $5.97 \mathrm{E}+3$ | 1. $23 \mathrm{E}+4$ | 2. $62 \mathrm{E}+2$ | $4.90 \mathrm{E}+2$ |
| xenon-133m | Ci | $3.64 \mathrm{E}+1$ | $1.64 \mathrm{E}+1$ | $1.93 \mathrm{E}-1$ | $6.09 \mathrm{E}-1$ |
| xenon-135 | Ci | $404 \mathrm{E}+1$ | 6.80 [+0 | 1. $28 \mathrm{E}-1$ | 5.04E-1 |
| xenon-135m | Ci | LLD | LLD | LLD | LLD |
| xenon-138 | Ci | LLD | LLD | LLD | LLD |
| Total | Ci | $6.06 E+3$ | 1. $23 \mathrm{E}+4$ | $2.79 \mathrm{E}+2$ | $5.39 \mathrm{E}+2$ |

2. Iodines

| iodine-131 | Cl | $7.31 \mathrm{E}-2$ | 2.77E-1 | LLD | LLD |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Iodine-132 | Ci | $1.46 \mathrm{E}-4$ | 8.02E-4 | LLD | LLD |
| iudine-133 | C! | 855-? | 4.40E-2 | LLD | LLD |
| fodine-135 | C? | $1.44 \mathrm{E}-3$ | 3. $28 \mathrm{E}-3$ | LLD | LLD |
| Total | Ci | 9.32E-2 | 3. $25 \mathrm{E}-1$ | LLD | LLD |

TABLE IC (Continued)
EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1984)
GASEOUS EFFLUENTS - GROUND-LEVEL RE EASES

| Nuclides Released | Continuous Mode |  |  | Batch Mode |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unit | Quarter First | Quarter Second | Quarter First | Quarter Second |
| 3. Particulates |  |  |  |  |  |
| barium-139 | Ci | LLD | 6.14E-6 | LLO | LLD |
| barium-140 | C1 | LLD | LLD | LLD | LLD |
| bromine-82 | Ci | 1.99E-4 | 5.91E-5 | LLD | LLD |
| cerium-139 | Ci | LLD | 7.00E-7 | LLD | LLD |
| cesium-134 | Ci | $1.77 \mathrm{E}-7$ | $3.68 \mathrm{E}-5$ | LLD | LLD |
| cesium-136 | Ci | 1.70E-7 | 6.1.6E-5 | LLD | LLD |
| cesium-137 | Ci - | 5.12E-6 | 2.07E-4 | LLD | LLD |
| cesium-138 | Ci | $3.76 \mathrm{E}-6$ | 4.33E-5 | LLD | LLD |
| chromium-51 | Ci | 1.80E-4 | LLD | LLD | LLD |
| cobalt-58 | Ci | 7.75E-4 | 4.88E-4 | LLD | LLD |
| cobalt-60 | Ci | 2. $23 \mathrm{E}-5$ | 1.40E-5 | LLD | LLD |
| iron-55 | Ci | 4.32E-5 | ** | * | * |
| lanthanum-140 | Ci | LLD | LLD | LLD | LLD |
| lanthanum-142 | Ci | 6.01E-6 | LLD | LLD | LLD |
| manganese-54 | Ci | 2.55E-5 | $9.48 \mathrm{E}-8$ | LLD | LLD |
| molybdenum-99 | Ci | 1.10E-5 | 5.28E-4 | LLD | LLD |
| niobium-94 | Ci | LLD | 2. $45 \mathrm{E}-6$ | LLD | LLD |
| niobium-95 | Ci | 1.94E-4 | $4.33 \overline{\mathrm{E}}-5$ | LLD | LLD |
| rubidium-88 | Ci | $4.56 \mathrm{E}-3$ | 3.80E-3 | LLD | LLD |
| scandium-47 | Ci | $8.73 \mathrm{E}-5$ | LLD | LLD | LLD |
| sodium-24 | Ci | 5.15E-5 | 8.91E-5 | LLD | LLD |
| strontium-89 | Ci | $7.65 \mathrm{E}-6$ | ** | , | * |
| strontium-90 | Ci | LLD | ** | * | * |
| strontium-92 | Ci | LLD | $8.25 \mathrm{E}-6$ | LLD | LLD |
| technetium-99m | Ci | 1. $97 \mathrm{E}-5$ | 6.15E-4 | LLD | LLD |
| tellurium-132 | Ci | LLD | 1.32E-6 | LLD | LLD |
| zirconium-95 | Ci | LLD | 1.90E-5 | LLD | LLD |
| zirconium-97 | Ci | 3. 17E-5 | $1.72 \mathrm{E}-6$ | LLD | LLD |

*Batch releases are not reported separatsly. All batch releases are vented through the Plant Vent Stack, therefore $\mathrm{S} \cdot 89$, Srg 9 and Fe 55 are analyzed by the "Continuous" mode only.
**Second quarter analyses were not available at time of report and will be
reported in the following Semiannual report.
LLD - Lower Limit of Detection; See lable 10.

## EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1984)

 GASEOUS EFFLUENTS - LOWER LIMIT OF DETECTIONNUCLIDE
CONTINUOUS MODE ( $\mu \mathrm{Ci} / \mathrm{cc}$ )
BATCH MODE ( $\mu \mathrm{Ci} / \mathrm{cc}$ )

| argon-41 | * | $<7.53 \mathrm{E}-6$ |
| :---: | :---: | :---: |
| barium-139 | <9.95E-13 | NA |
| barium-140 | <1.57E-12 | NA |
| bromine-82 | * | NA |
| cerium-139 | <1.00E-11 | NA |
| Cesium-134 | * | NA |
| cesium-136 | * | NA |
| cesium-137 | * | NA |
| cesium-138 | * | NA |
| chromium-51 | <1.00E-11 | NA |
| cobalt-58 | * | NA |
| cobalt-60 | * | NA |
| Todine-131 | * | NA |
| Todine-132 | * | NA |
| Iodine-133 | * | NA |
| Todine-135 | * | NA |
| krypton-85 | $<1.07 \mathrm{E}-5$ | * |
| krypton-87 | $<7.45 \mathrm{E}-8$ | <2.10E-6 |
| krypton-88 | * | $<4.76 E-5$ |
| lanthanum-140 | <6.11E-12 | NA |
| lanthanum-142 | <1.00E-11 | NA |
| manganese-54 | * | NA |
| molybdenum-99 | * | NA |
| niobium-94 | <1.00E-11 | NA |
| niobium-95 | * | NA |
| rubidium-88 | * | NA |
| scandium-47 | $<5.40 E-13$ | NA |
| sodium-24 | A | NA |
| strontfum-90 | $<2.50 E-16$ | NA |
| strontium-92 | $<5.80 \mathrm{E}-13$ | NA |
| technetium-99m | * | NA |
| tellurium-132 | <4.57E-13 | NA |
| xenon-135m | <1.19E-5 | -5.91E-6 |
| xenon-138 | $<9.70 \mathrm{E}-8$ | $<8.01$ E-6 |

*     - Nuclide detected in Table 1C.

NA - Iodines and particulates are not analyzed prior to release.

EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1984) GASEOUS EFFLUENTS-RADIATION DOSES AT THE SITE BOUNDARY

|  | Unit | First Quarter | Second Quarter |
| :---: | :---: | :---: | :---: |
| A. Noble Gas |  |  |  |
| 1. Gamma air dose | mrad | $1.71 \mathrm{E}+0$ | 7.22E-1 |
| 2. Percent Technica? Specification Limit | \% | 1.17E+1 | 7.22E+0 |
| 3. Beta air dose | mrad | $3.39 \mathrm{E}+0$ | 2.10E+0 |
| 4. Percent Technical Specification Limit | \% | 1.70E+1 | 1.05E+1 |
| B. Tritium, Iodine, Particulate |  |  |  |
| 1. Organ dose | mrem | 9.00E-1 | 1.79E+0 |
| 2. Percent Technical Specification Limit | \% | $6.00 \mathrm{E}+0$ | 1.19E+1 |

NOTE: Calculations performed in accordance with the ODCM utilizing the historical $X / Q$.

## SECTION C. LIQUID EFFLUENTS

Table 2A, "Liquid Effluents - Summation of All Releases," provides a detailed listing of liquid effluent releases in three categories: Fission and activation products, tritium, and dissolved and entrained gases. Listed are (1) the total release of each category, (2) the average diluted concentration at the point of discharge during each quarterly period, and (3) the percent of Technical Specification Limit. Also listed are the gross alpha radioactivity, the volume of actual waste released (prior to dilution by the circulating water), and the volume of dilution water (the volume of circulating water) used to dilute the batch releases.

The methodology used in calculating the percent of applicable limit is presented in Section $E$ of this report. The percent estimated total error is listed in Table 2A for each of the three liquid effluent categories. The methodology used for error analysis is described in Section F of this report.

Table $2 B$, "Liquid Effluents," provides the systematic listing by radionuclide for the quantity of radioactivity released in each category. The total radioactivity of each radionuclide released is listed for each quarterly period by both "continuous" and "batch" modes of release.

Table 2C, "Liquid Effluents - Lower Limit of Detection," provides a listing of lower limit of detection concentrations for radionuclides not detected in Table 28.

Table 2D, "Liquid Effluents - Radiation Doses at Site Boundary," provides a summary of doses at the site boundary for this reporting period, by quarter.

The values for the composite gross alpha, $\mathrm{Fe}-55, \mathrm{Sr}-89$ and $\mathrm{Sr}-90$ in Table 2A and Table 2B Liquid Effluents, for the July - December Semiannual Report were incomplete because data was not available at reporting time. The values not reported were for the fourth quarter, 1983. The values not reported are as follows:
Unit

| Gross alpha | Ci | LLD |
| :--- | :--- | :--- |
| $\mathrm{Fe}-55$ | Ci | $2.24 \mathrm{E}-2$ |
| $\mathrm{Sr}-89$ | Ci | $4.36 \mathrm{E}-4$ |
| $\mathrm{Sr}-90$ | Ci | $2.18 \mathrm{E}-5$ |

Gross alpha $L L D=<3.00 E-8 \mu \mathrm{Ci} / \mathrm{ml}$

EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1984) LIQUID EFFLUENTS-SUMMATION OF ALL RELEASES

|  | Unit | First <br> Quarter | Second <br> Quarter |  | Estimated <br> Total Error, |
| :--- | :---: | :---: | :---: | :---: | :---: |
| A. Fission and activation products |  |  |  |  |  |

D. Gross alpha radioactivity

1. Total release Ci LLD * 5.00E+1

E. Volume of waste released
(prior to dilution) liters $\quad 6.04 \mathrm{E}+6 \quad 1.83 \mathrm{E}+6 \quad 5.00 \mathrm{E}+0$

F. Volume of dilution water
$\begin{array}{lllll}\text { used during period } & \text { liters } & 2.16 \mathrm{E}+10 & 6.61 \mathrm{E}+10 & 5.00 \mathrm{E}+0\end{array}$

*     - Second quarter analyses not available at report time; analyses will be included in the following Semiannual Report.

LLD - Lower Limit of Detection; see Table 2C.

EFFLUENT ANT WASTE DISPOSAL SEMIANNUAL REPORT (1984) LIQUID EFFLUENTS

|  | Continuous Mode |  |  | Batch Mode |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | First | Second | First | Second |
| Nuclides Released | Unit | Quarter | Quarter | Quarter | Quarter |


| antimony-122 | Ci | LLD | LLD | LLD | 6.73E-3 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| antimony-124 | Ci | LLD | LLD | $5.46 E-3$ | LLD |
| antimony-125 | Ci | LLD | LLD | LLD | 8.83E-5 |
| barium-140 | Ci | LLD | LLD | 2.56E-3 | 2.36E-4 |
| cerium-141 | Ci | LLD | LLD | 5.37E-5 | $1.53 \mathrm{E}-4$ |
| cerium-144 | Ci | LLD | LLD | $8.44 E-4$ | 1.73E-4 |
| cesium-134 | Ci | LLD | 7.30E-5 | 4.49E-3 | 1.23E-1 |
| cesium-136 | Ci | LLD | 3.60E-5 | 3.33E-3 | 2.37E-2 |
| cesium-137 | Ci | LLD | 1.28E-4 | 1.79E-1 | $6.95 \mathrm{E}-1$ |
| chromium-51 | Ci | LLD | LLD | $4.88 \mathrm{E}-1$ | $3.74 \mathrm{E}-1$ |
| cobalt-57 | Ci | LLD | LLD | 8.60E-4 | 3.28E-4 |
| cobalt-58 | Ci | LLD | 1.22E-4 | 6.60E-1 | $5.15 \mathrm{E}-1$ |
| $\text { cobalt }-60$ | Ci | LLD | LLD | 1.11E-1 | 7.31E-2 |
| Iodine-131 | $\mathrm{Ci}$ | LLD | 1.53E-3 | 1.11E-1 | 3.91E-1 |
| iodine-132 | $\mathrm{Ci}$ | LLD | LLD | 8.28E-4 | LLD |
| iodine-133 | $\mathrm{Ci}$ | LLD | $4.66 E-5$ | 1.12E-2 | $2.11 E-2$ |
| iodine-135 | Ci | LLD | LLD | LLD | $9.37 E-4$ |
| iron-55 | Ci | LLD | LLD |  |  |
| iron-59 | Ci | LLD | LLD | $9.81 \mathrm{E}-2$ | 4.33E-2 |
| 1 anthanum-140 | Ci | LLD | LLD | $1.64 E-3$ | $2.34 E-3$ |
| manganese-54 | Ci | LLD | $1.52 E-4$ | $4.83 E-2$ | $3.15 E-2$ |
| molybdenum-99 | Ci | LLD | $2.39 E-4$ | $2.14 E-2$ | $7.70 E-2$ |
| neptunium-239 | Ci | LLD | LLD | $7.93 E-4$ | $4.85 E-5$ |
| niobium 95 | Ci | LLD | LLD | $6.50 E-2$ | $4.79 E-2$ |
| niobium 97 | Ci | LLD | LLD | $\text { 2. } 37 E-2$ | 2. 12E-4 |
| ruthenium-103 | Ci | LLD | LLD | $4.57 E-3$ | $7.31 E-4$ |
| sodium-24 | Ci | LLD | 3.69E-5 | $2.40 E-3$ | $3.85 E-3$ |
| strontium-89 | Ci | LLD | LLD | 1.29E-4 |  |
| strontium-90 | Ci | LLD | LLD | LLD | ** |
| technetium-99m | Ci | LLD | 1.59E-4 | 2.79E-2 | 1.02E-1 |
| tellurium-132 | Ci | LLD | LLD | LLD | 1.62E-4 |
| tin-113 | Ci | LLD | LLD | LLD | $5.15 E-4$ |
| zinc-65 | Ci | LLD | LLD | $4.05 E-3$ | $1.64 \mathrm{E}-3$ |
| zirconium-95 | Ci | LLD | LLD | 5.73E-2 | 5.10E-2 |
| zirconium-97 | Ci | LLD | LLD | LLD | $1.66 E-5$ |
| Total for period | Cl | LLD | 2.52E-3 | $1.93 E+0$ | $2.59 \mathrm{E}+0$ |

[^0]
## EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1983) LIQUID EFFLUENTS

|  |  | Continuous Mode |  | Batch Mode |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Nuclides Released | Unit | First Quarter | Second Quarter | First <br> Quarter | Second Quarter |
| argon-41 | Ci | LLD | LLD | 8.02E-3 | 2. $14 \mathrm{E}-5$ |
| krypton-85 | Ci | LLD | LLD | LLD | 4.47E-3 |
| krypton-85m | Ci | LLD | LLD | LLD | 3.90E-3 |
| krypton-88 | Ci | LLD | LLD | LLD | 6. $55 \mathrm{E}-4$ |
| xenon-131m | Ci | LLD | LLD | $7.12 \mathrm{E}-2$ | 1. $33 \mathrm{E}+0$ |
| xenon-133 | Ci | LLD | 8.69E-4 | $8.66 \mathrm{E}+0$ | 2.82E+2 |
| xenon-133m | Ci | LLD | LLD | $8.31 \mathrm{E}-2$ | $5.05 \mathrm{E}+0$ |
| xenon-135 | Ci | LLD | 7.41E-6 | 2.19E-2 | $3.91 \mathrm{E}+0$ |
| xenon-135m | Ci | LLD | LLD | LLD | 2.36E-5 |

*     - First quarter analysis not available at report time; analysis will be reported in the following semiannual report.
** - Second auarter analyses not available at report time; analyses will be included in the following Semiannual Report.

LLD - Lower Limit of Detection; see Table $2 C$.

## TABLE 2C

EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1984) LIQuid effluents - LOWER limit of detection

| RADIONUCLIDES | CONTINUOUS MODE ( $\mu \mathrm{Ci} / \mathrm{ml}$ ) | BATCH MODE ( $\mu \mathrm{Ci} / \mathrm{ml}$ ) |
| :---: | :---: | :---: |
| antimony-122 | $<2.58 \mathrm{E}-7$ | $<6.12 \mathrm{E}-8$ |
| antimony-124 | $<1.09 \mathrm{E}-7$ | $<8.00 \mathrm{E}-8$ |
| antimony-125 | $<2.24 E-7$ | $<1.85 \mathrm{E}-7$ |
| argon-41 | $<4.00 E-8$ | * |
| barium-140 | $<2.27 \mathrm{E}-7$ | * |
| cerium-141 | $<2.33 \mathrm{E}-7$ | * |
| cerium-144 | <1.00E-6 | * |
| cesium-134 | $<1.09 \mathrm{E}-7$ | * |
| cesium-136 | $<1.13 \mathrm{E}-7$ | * |
| cesium-137 | $<1.11 \mathrm{E}-7$ | * |
| chromium-51 | $<1.14 \mathrm{E}-6$ | * |
| cobalt-57 | $<1.28 \mathrm{E}-7$ | * |
| cobalt-58 | $<1.17 \mathrm{E}-7$ | * |
| cobalt-60 | $<9.42 \mathrm{E}-8$ | * |
| krypton-85 | $<1.69 \mathrm{E}-5$ | $<1.11 \mathrm{E}-5$ |
| krypton-88 | $<1.63 \mathrm{E}-7$ | * |
| fodine-131 | $<4.09 \mathrm{E}-8$ | * |
| Iodine-132 | $<5.01 \mathrm{E}-8$ | $<8.13 \mathrm{E}-8$ |
| fodine-133 | <1.11E-6 | * |
| Iodine-135 | <1.31E-5 | * |
| iron-55 | $<3.00 \mathrm{E}-8$ | $<3.00 E-8$ |
| iron-59 | $<6.07 \mathrm{E}-8$ | * |

EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1984) LIQUID EFFLUENTS - LOWER LIMIT OF DETECTION

| RADIONUCLIDES | CONTINUOUS MODE ( $\mu \mathrm{Ci} / \mathrm{ml}$ ) | BATCH MODE ( $\mu \mathrm{Ci} / \mathrm{ml}$ ) |
| :---: | :---: | :---: |
| 1anthanum-140 | $<1.99 \mathrm{E}-7$ | * |
| manganese-54 | $<4.39 E-8$ | * |
| molybdenum-99 | $<3.31 \mathrm{E}-7$ | * |
| neptunium-239 | $<1.54 \mathrm{E}-6$ | * |
| nlobium-95 | $<5.00 E-8$ | * |
| niobium-97 | $<9.53 \mathrm{E}-8$ | * |
| ruthenium-103 | $<6.14 \mathrm{E}-8$ | * |
| sodium-24 | $<3.20 E-8$ | * |
| strontium-89 | $<4.00 E-8$ | * |
| stront fum-90 | $<1.00 E-8$ | $<1.00 \mathrm{E}-8$ |
| tellurium-132 | $<2.43 \mathrm{E}-7$ | $<1.12 \mathrm{E}-7$ |
| tin-113 | $<1.02 \mathrm{E}-7$ | <5.01E-8 |
| zinc-65 | $<6.45 \mathrm{E}-8$ | * |
| zirconium-95 | $<8.65 \mathrm{E}-7$ | * |
| zirconium-97 | $<2.11 \mathrm{E}-6$ | $<5.22 \mathrm{E}-8$ |
| xenon-131m | $<7.46 \mathrm{E}-6$ | * |
| xenon -133 m | $<3.21 E-6$ | * |
| xenon-135 | $<3.81 \mathrm{E}-7$ | <1.90E-6 |
| xenon-135m | $<6.08 \mathrm{E}-7$ | $<5.10 \mathrm{E}-6$ |
| gross-alpha | <1.50E-7 | * |

[^1]
## TABLE 20

EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1984) LIQUID EFFLUENT-RADIATION DOSES AT THE SITE BOUNDARY

|  |  | Unit | First <br> Quarter | Second <br> Quarter |
| :--- | :--- | :---: | :---: | :---: |
| A. 1. Total body dose | mrem | $1.01 \mathrm{E}-1$ | $7.81 \mathrm{E}-2$ |  |
| 2. Percent Technical Specification Limit | $\%$ | $3.37 \mathrm{E}+0$ | $2.60 \mathrm{E}+0$ |  |
| B. | 1. | Limiting organ dose | mrem | $2.05 \mathrm{E}+0$ |

NOTE: The limiting organ for this reporting period is GI-LLI.

## TABLE 3

EFFLUENT AND WASTE DISPOSAL SEMIANNUAL REPORT (1984) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS
A. Solid Waste Shipped Offsite for Burial or Disposal (Not irradiated fuel)

| 1. Type of Waste | Unit | $\begin{aligned} & \text { 6-month } \\ & \text { period } \end{aligned}$ | Est. Total Error, \% |
| :---: | :---: | :---: | :---: |
| a. Spent resins, filter sludges, | $\stackrel{\mathrm{m}^{3}}{\mathrm{Cf}}$ | $\begin{aligned} & 4.93 \mathrm{E}+0 \\ & 9.99 \mathrm{E}+1 \end{aligned}$ | $3.00 \mathrm{E}+1$ |
| b. Dry compressible waste, contaminated equip., etc. | $\mathrm{m}^{3} \mathrm{Ci}^{3}$ | $\begin{aligned} & 3.19 \mathrm{E}+1^{*} \\ & 7.07 \mathrm{E}-1 \end{aligned}$ | 3. $000+1$ |
| c. Irradiated components, control rods, etc. | $\begin{aligned} & \mathrm{m}^{3} \\ & \mathrm{Ci} \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+0 \\ & 0.00 \mathrm{E}+0 \end{aligned}$ | $3.00 \mathrm{E}+1$ |
| d. Other (filters, sludge, sand/ rubble, wet trash) | $\mathrm{m}^{\mathbf{C}}$ | $\begin{aligned} & 0.00 \mathrm{E}+0 \\ & 0.00 \mathrm{E}+0 \end{aligned}$ | $3.00 \mathrm{E}+1$ |

[^2]
## SECTION ${ }^{\circ}$. RADWASTE SHIPMENTS (Continued)

A. Solid Waste Shipped Offsite for Buriai or Disposal (Continued)
2. Estimate of major nuclide composition (by type of waste)

| carbon-14 | \% | 1.46E-1 |
| :---: | :---: | :---: |
| cesium-134 | \% | $3.61 \mathrm{E}+0$ |
| cesium-137 | \% | $2.86 \mathrm{E}+1$ |
| cobalt-57 | \% | 1.27E-1 |
| cobalt-58 | \% | $4.03 \mathrm{E}+1$ |
| cobalt-60 | \% | $7.54 \mathrm{E}+0$ |
| hydrogen-3 | \% | $7.64 \mathrm{E}-4$ |
| iodine-129 | \% | 1.65E-5 |
| iron-59 | \% | 2.26E-1 |
| manganese-54 | \% | 1. $62 \mathrm{E}+1$ |
| nickel-63 | \% | 3. $25 \mathrm{E}+0$ |
| strontium-90 | \% | 1.17E-2 |
| technetium-99 | \% | 8.93E-5 |
| b. Carbon-14 | \% | 1. $37 \mathrm{E}+1$ |
| cesium-137 | \% | 1.20E-2 |
| chromfum-51 | \% | $1.48 \mathrm{E}+1$ |
| cobalt-58 | \% | $4.31 \mathrm{E}+1$ |
| cobalt-60 | \% | 6.22E+0 |
| hydrogen-3 | \% | 2. $30 \mathrm{E}+0$ |
| iodine-129 | \% | $1.94 \mathrm{E}-4$ |
| iran-59 | \% | $2.50 \mathrm{E}+0$ |
| manganese-54 | \% | $2.49 E+0$ |
| nickel-63 | \% | $4.03 \mathrm{E}+0$ |
| ntobium-95 | \% | $6.77 \mathrm{E}+0$ |
| technet f um-99 | \% | $6.25 \mathrm{E}-4$ |
| zirconium-95 | $\%$ | $4.07 \mathrm{E}+0$ |
| c. Not Applicable | \% | $0.00 \mathrm{E}+0$ |
| d. Not Applicable | \% | $0.00 \mathrm{E}+0$ |

## 3. Solid Waste Disposition

Number of Shipments
2

Mode of Transportation
Chem-Nuclear Systems Inc. Truck
8. Irradiated Fuel Shipments (Disposition)

Number of Shipments Mode of Transportation Destination
None
N/A
N/A

## Gaseous Effluents

The percent of Technical Specification Limit, tabulated in Table 1A, was determined by calculation of the following parameter:


The \% TSL is placed in Parts A.3, B.3, C.3 and D.3 of Table 1A.

The percent of applicable limit, tabulated in Table 2A, was determined by calculation of the following parameter:

| \% TSL $=$ | $\frac{(D i l \text { Conc)(100) }}{M P C}$ |
| ---: | :--- |
| Where: Dil Conc $=$ | total curies released in each category and <br> each quarter, converted to microcuries, <br> divided by the total volume released (sum <br> of Part E and F in Table 2A) converted to <br> milliliters. This number is the value in <br> Part A.2, B.2 and C.2 of Table 2A. |

The MPC ${ }_{\text {eff }}$ is defined:

## 1

|  |  | $\sum_{i=1}^{n} \quad \frac{F_{i}}{i-M P C_{i}}$ |
| :---: | :---: | :---: |
| Where: $F_{i}$ | $=$ | fractional abundance of the 1 th radionuclide obtained by diyiding the activity in curies for each radionuclide, $C_{i}$, by the sum of all such activities, $\mathrm{C}_{\mathrm{T}}$. |
| ก | $=$ | total number of radionuclides identified |
| MPC ${ }_{1}$ | $=$ | MPC of the ith radionuctide |

The \% TSL is placed in Parts A.3, B. 3 and C. 3 of Table 2A.

## SECTION F. ESTIMATION OF ERROR

Estimations of the error in reported values of gaseous and liquid effluent releases have been made. Sources of error considered for gaseous effluents - batch releases are: (1) tank volumes, (2) sampling errors, (3) counting errors, and (4) calibration errors. Sources of error for gaseous effluents - continuous releases are: (1) fan flow rate, (2) sampling, (3) counting, (4) calibration and (5) differential pressure drop.

Sources of error for 1 qquid effluents - batch releases are: (1) tank volumes, (2) sampling, (3) counting and (4) calibration. Sources of error for liquid effluents - continuous releases are: (1) dilution water flow rate, (2) sampling, (3) counting and (4) calibration.

These sources of error are independent, and thus the total error is calculated according to the formula:

$$
\text { Total Error }=\sqrt{\begin{array}{r}
\sigma^{2}+\sigma^{2}+\sigma^{2} \ldots+\sigma^{2} \\
1 \\
2
\end{array} \quad 3 \begin{array}{l}
i
\end{array}}
$$

Where: $\quad \sigma_{i}=$ Error associated with each component

The meteorology of the SONGS-2/3 site for the first and second quarter of 1984 is described in this section. Meteorological measurements have been made according to the guidance set forth in USNRC Regulatory Guide 1.23, "Onsite Meteorological Programs." A summary report of the meteorological measurements taken during each calendar quarter are presented in Table 4A as joint frequency distribution (JFD) of wind direction and wind speed by atmospheric stability class.

Hourly meteorological data for batch releases have been recorded for the periods of actual release. This data is avallable, as well as the hourly data for the Semiannual report, but has not been included in this report because of the bulk of data recorded.

Table 4A lists the joint frequency distribution for the first and second quarter of 1984. Each page of Table 4A represents the data for the Stability Classes: $A, B, C, D, E, F$, and $G$; the last page of each table is the JFD with the combined stability classes. Each page is also divided into two parts; the upper part lists the number of hourly periods when each meteorology condition occurred, and the lower part lists the frequency of each classification by percent. The wind speeds have been measured at the 10 -meter level, and the stability classes are defined by the temperature differential between the 10 and 40 -meter levels.

## TABLE 4A

```
SOUTHERN CALIFORNIA EDISON COMPANY
    25-JUL-84
    SAN DNOFGE NUCLFAR QENEGATING STATION
    13T GUARTER, 1%E4
    DAMES AND MOORE JOB ND - 00377-084-09
    DATA PERIOD- 01/01/84 TO 03/31/94
    STABILITY CLAGS #AN (10-MO METERS )
WINDS AT 10 METER LEVEL
```

WIND FREGUENCY DISTRIBUTIDN
(FREQUENCY IN NUMBER OF OCCURRENCES)


WIND FREQUENCY DIGTRTBUTION (FREQUENCY IN PERCENT OF TOTAL.)

| WIND |  |  |  |  |  | UPPER CLASS |  |  |  |  | INTERVALS |  |  |  | $\begin{array}{r} 0 \mathrm{~F} \\ \hline \end{array}$ |  | \% | SPEED | $D$ (MPH) |  |  | 11 |  | 711 |  | total |  | MEAN <br> SPEED |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTI | ON | 1 |  | 2 |  | 3 |  | 4 |  | 5 |  |  | 6 |  |  |  |  |  | 9 |  | 10 |  |  |  |  |  |  |  |  |
| NNE | c | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 08 | 5 | 0 | 00 | 0 | 05 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 19 |  | 20 |
| HE | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 0 | 00 | - | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 05 | 4 | 40 |
| Ent | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 000 | 0 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 03 | 6 | 90 |
| E | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 05 | 12.4 | 40 |
| E3E | - | 00 | - | 00 | 0 | 00 | 0 | 00 | 0 | 00 | $\bigcirc$ | 000 | 0 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 |
| SE | 0 | 00 | 0 | 00 | 0 | 00 | 0 | O0 | 0 | 00 | 0 | 09 | 5 | 0 | 05 | 0 | 05 | 0 | 09 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 23 | 7 | 16 |
| 558 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 14 | 0 | 23 | 0 | 09 | 9 | 0 | 14 | 0 | 19 | 0 | 19 | 0 | 14 | 0 | 00 | - | 00 | 1 | 07 | 6. | 53 |
| 5 | 0 | 00 | 0 | 00 | 0 | 14 | 0 | 37 | - | 23 | 0 | - 51 | 1 | 0 | 69 | 0 | 60 | 0 | 19 | 0 | 05 | 0 | 14 | 0 | 00 | 2 | 80 | 6. | 23 |
| S0w | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 37 | 0 | 46 | 0 | 51 | 1 | 0 | 28 | 0 | 19 | 0 | 42 | 0 | 09 | 0 | 00 | 0 | 05 | 2 | 37 | 6 | 09 |
| 54 | 0 | 00 | 0 | 30 | 0 | 23 | 0 | 65 | 0 | 93 | 0 | 70 | 0 | 0 | 33 | 0 | 37 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 3 | 25 | 4. | ต日 |
| W9\% | 0 | 00 | 0 | on | 0 | 07 | 0 | 88 | 1 | 21 | 0 | 88 | 8 | 0 | 74 | 0 | 19 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 19 | 4 | 23 | 5.4 | 46 |
| $\cdots$ | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 46 | 1 | $4{ }^{4}$ | 2 | 209 | 9 | 1 | 30 | 0 | 93 | 0 | 33 | 0 | 23 | $\bigcirc$ | 19 | 0 | 09 | , | in | 61 |  |
| UNW | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 14 | - | 33 | 0 | . 60 | 0 | 0 | 74 | 0 | 42 | 0 | 33 | 0 | 46 | 0 | 14 | 0 | 42 | 3 | 50 | 7 | 08 |
| Tow | 9 | 00 | 0 | 06 | 0 | 00 | 0 | 20 | 0 | 00 | 0 | 00 | 0 | 0 | 00 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 05 | 0 | 14 | 101 | 13 |
| NeNW | 0 | 00 | 0 | an | 0 | 00 | 0 | 00 | $\bigcirc$ | 09 | 0 | 000 | 0 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | oo | 0 | 05 | 4 \% | 20 |
| $\stackrel{N}{4}$ | 0 | 00 | 0 | 02 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 |
| Vantatie |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | Ot | 0 | 00 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 00 |  |  |
| taral. | 2 | 00 | 0 | 90 | 0 | 96 | 3 | 02 | 4 | 93 |  | 3 44 |  |  | 28 |  | 07 | 1 | 63 | 0 | 98 | 0 | 91 | 0 | 68 | 25 | 29 | 6. | 20 |

TOTAL NUMBER OF POSSIBLE OBSERVATIONS - 2184
TOTAL RUMBEM DC DESERVATIONS WITH VALID SPEED. DIRECTION AND STABILITY - 2192

```
SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLEAR GENERATING STATION 1ST QUARTER. 1984
DAMES AND MODRE JOB NO - 00377-084-09
DATA PERIOD- 01/01/94 TO 03/31/94
STABILITY CLASS NBE (10-40 METERS)
WINDS AT 10 MEIER LEVEL
```

25-M1-84

WIND FREQUENCY DISTRIBUTION
(FREQUENCY IN NUMBER OF OCCURRENCES)

| WIND |  |  | UPPER CLASS |  |  | INTERVALS | OF | WIND SPEED (MPH) |  |  | 11 | >11 | total |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTION | 1 | 2 | 3 | 4 | 5 | 6 |  | 8 | 9 | 10 |  |  |  |  |  |
| NINE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1. | 0 | 0 | 1 | 2 | 17 | 40 |
| THE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 8 | so |
| ENE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 00 |
| E | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| ESE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| SE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| S5E | 0 | 0 | 2 | 0 | 0 | 0 | z | 0 | 0 | 0 | 1 | 0 | 5 | 5 | 72 |
| 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| 55w | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 00 |
| SW | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 |
| WS\% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 |
| $\cdots$ | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 5 | 49 |
| WNW | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 3 | 6 | 43 |
| HM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| NNW | c | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 5 | ¢0 |
| N | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| VARTAALE |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 | 00 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 |  |
| total | 0 | 0 | 3 | 1 | 2 | 0 | 4 | 2 | 2 | 0 | 1 | 1 | 16 | 7 | 31 |

> WIND FREQUENCY DISTR IBlITION (FREQUENCY IN PERCENT OF TOTAL.)


TDTAL NUMBER DF POSSIBLE OBSERVATIONA - 2184
TOTAL NUMBEN OC OBSERVATIOHS WITH VALID SPEED. DIRECTION AND STABILITY - 2152

## TABLE 4A

| SOUTHERN CALIFORNIA EDISON COMPANY |  |
| :---: | :---: |
| San onofre mullear | GENERATING STATION |
| IST QUARTER. 1984 |  |
| DAMES AND MODRE JOD NO - 00377-084-09 |  |
| DATA PERIOD-01/01/ | 134 T0 03/31/04 |
| STABILITY CLASS ac* | (10-40 METEAS |
| WINDS AT 10 METER | LEVEL |

WIND FREQUENCY DISTRIBUTION
(FREQUENCY IN NUMBER OF OCCURRENCES)


WIND FREQUENCY DISTRIBUTION (FAEGUENCY IN PERCENT OF TOTAL)


TOTAL NUMBER DF POSSIBL OBSERVATIONS - 2184
TOTAL RUMBER OC ORSERVATIONE WITH VALID SPEED. DIRECTION AND STABILITY - 2192

```
SOUTMERN CALIFORNIA EDISON GIMPANY
    SAN THDOFRE NUCLEAR GENERATING STATION
    IST QuaNTER. 1 वga 
DAMES AND MOORE JOD NO - 00377-0B4 -09
DATA PERIOD- 01/01/04 10 03/31/04
STABILITY CLASS ND (10-40 METERS )
WINDS AT 10 MEIER LEVEL
```

    23-JUl-84
    WIND FREGUENCY DISTRIBUTION
(FREQUENCY IN NUMBER OF OCCURRENCES)


## WIND FREGUENCY DISTRTBUTION

 (FREQUENCY IN PERCENT OF TOTAL.)

TOTAL MEMBEA OF pOSSTBLE OBSERVATIONE - 2184
TOTAL NUM3EH OC BBSERVATIDNS WITH VALID SPEED. DIMECTION AND STABILITY - 2192

## TABLE 4A

STUTHERN CALIFORNIA EDISON CTMPANY
25- $9 \mathrm{ML}-84$
SAN DNOFRE NUCLEAR OENERATINS STATION
157 GUAHTER. 190.
DAMES AND MOORE JOB NO - 00377-084-09
DATA PERIOD- 01/01/84 T0 03/31/04 SNABILITY CLAAS aE (10-40 METEAS , WINDS AT 10 NEIER LEVEL

WIND FREOUENCY DIGTRIBUTION
(FREGUENCY IN NUMEER OF OCCURRENCES)

| WIND |  |  | UPPER |  | CLa3s | INTERVALS | $\begin{gathered} \text { OF } \\ \hline \end{gathered}$ | WIND GPEED (MPH) |  |  | 11 | 311 | TOTAL. | NEAN |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIAECTIOR | 1 | 2 | 3 | 4 | 5 | b |  | 8 | 9 | 10 |  |  |  | SPE | E0 |
| --* - |  |  |  |  | \#** | $=$ |  | *** |  | - |  |  | - |  |  |
| Ne Ne | 0 | 2 | 18 | 18 | 22 | 16 | 3 | 1 | $\theta$ | 4 | 1 | 5 | 92 | 4 | 99 |
| NE | 0 | 2 | 3 | 3 | 2 | 3 | 0 | 0 | 1 | 0 | 0 | 8 | 22 | 7 |  |
| Enes | 0 | 1 | 2 | 2 | 1 | 1 | 2 | 0 | $t$ | 1 | 0 | 0 | 11 | * | 00 |
| E | 0 | 0 | 2 | 0 | 4 | 3 | 0 | $\bigcirc$ | 0 | 1 | 0 | 0 | 10 | 4 | 48 |
| Ebe | 0 | 0 | 1 | 2 | 1 | 2 | 1 | 0 | e | $\theta$ | - | ¢ | $\stackrel{ }{ }$ | 4 | 4) |
| SE | 0 | 0 | 0 | 1 | 4 | 3 | 1 | 0 | 0 | $\theta$ | 0 | ${ }^{6}$ | $\stackrel{\square}{ }$ | 9 | al |
| Sse | 0 | 0 | 1 | 2 | 3 | 4 | 1 | 0 | 0 | 0 | 6 | 0 | 11 | $\stackrel{*}{*}$ | 7 |
| 5 | $\theta$ | 0 | 2 | 1 | 0 | $\theta$ | 1 | 0 | 0 | $\theta$ | 0 | 6 | 4 | 3 | 75 |
| 30w | 0 | 0 | \% | 0 | 0 | 0 | - | 0 | $\theta$ | 0 | $\theta$ | 0 | \% | \% | 91 |
| 5 w | 0 | 0 | 3 | 0 | 1 | 6 | 1 | $\theta$ | 0 | $\theta$ | 0 | ${ }_{0}$ | 5 | 3 | 70 |
| Why | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | $t$ | $\bigcirc$ | 0 | 0 | 3 | 5 | 90 |
| 4 | * | 0 | 0 | 4 | 1 | 4 | e | e | 0 | 0 | 0 | 0 | $\stackrel{\square}{*}$ | 4 | 48 |
| Lenew | 0 | $\theta$ | 1 | 2 | 6 | 3 | 3 | 1 | $t$ | 0 | $\theta$ | a | 17 | 9 | 10 |
| गW | 0 | 0 | 1 | 0 | 1 | 3 | 4 | 0 | 0 | 1 | 0 | 0 | 10 | 5 | 80 |
| N(TaH | 0 | 1 | 1 | \% | 1 | 4 | 7 | 2 | 1 | 1 | 0 | 1 | 26 | 5 | 45 |
| " | $\sigma$ | 3 | 1 | \% | 4 | * | 7 | 1 | 1 | 0 | 1 | 1 | 31 | 5 |  |
| VAAIARLE 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ¢AL. ${ }^{\text {a }}$ |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 | 00 |
| Totac | 0 | 9 | 39 | 50 | 92 | 50 | 33 | 3 | * | 8 | 2 | 15 | $26 \%$ |  |  |

WINE FRE Zuency binteinution (EAEOUENCY IN PERCENT OF TOTAL)


TOTAL mmber or possibif obst Ryattoms - z184


```
SOUTIERN CALIFOMNIA EDISON COMBANY
SAN ONOFRE FHCLEAR GENERATING STATION
Ist OUAATER, IqA4
IDt aUARTER, IVE4
DAMES AND mDOQE JOE NO = 00377-004
STABILITY CLABS &Fe (10-40 NETERS )
UINDS AT IO NEIER LEVEL
```

$25-$ 月4. 84

WIND FREQUNCY DISTRIBUTION
(FaEOUENCY IN MUMBER OF OCCURRENCES)





## TABLE 4A

```
SOUTHERN CALIFORNIA EDISON CIOMPANY 25-JUL-84
SAN ONOFRE RUCLEAR GENERATING STATION
IST GUARTER, 19@A
DAMES AND MOORE JOB ND - 00377-OA4-09
DATA PERIOO- 01/01/A4 TO 03/31/R4
STABILITY CLAS5 GG* (10-40 METERS )
WINDG AT 10 MEIER LEVEL
```

WIND FREJUENCY DISTRIBUTION
(FREGUENCY IN NUMBER OF OCCURRENCES)

| WIND |  |  | UPPER CLAGS INTERVALS OF WIND BPEED (MPH) |  |  |  |  |  |  |  | 11 | 211 | TOTAL | MEAN |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  | 10 |  |  |  |  | EED |
| NNE | 0 | 1. | 4 | 15 | 14 | 46 | 71 | 90 | 月0 | 111 | 72 | 79 | 383 | B | 63 |
| NE | 0 | 1. | 1. | 4. | 1 | 6. | 4 | 4 | 0 | 2 | 0 | 3 | 26 | 6 | 62 |
| ENE | 0 | 1 | 0 | 0 | 2 | 0 | 1. | 0 | 0 | 0. | 0 | 0 | 4 | 4 | 47 |
| E | 0 | 0 | 1 | 1. | 1 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 3 | 3. | 53 |
| ETE | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2. | 70 |
| SE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 00 |
| S5E | ? | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 00 |
| 5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5. | 00 |
| S3W | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| 5w | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| WSW | 0. | 0 | 0 | 0. | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 00 |
| W | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| LINH | 0 | 0 | 0 | 0 | $\checkmark$ | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 | 5 | 20 |
| NW | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 6. | 50 |
| NNIT | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0. | 0. | 0 | 2 |  |  |
| N | 0 | 0 | 0 | 2 | 1 | 3 | 6 | 4 | 10 | 6 | 3 | 4 | 37 |  |  |
| Var IAsLE |  |  |  |  |  |  |  |  |  |  |  |  | 0 |  | 00 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 | 00 |
| TOTAL | 0 | 4 | 7 | 22 | 21. | 36 | ab | 98 | 70 | 119 | 73 | 86. | 904 |  | 43 |

WIND FREGUENCY DISTRIEUT SCOW
(FREqUENCY IN PERCENT OF TOTA,)


TOTAL NUMBER OF POCSIDLE OBSERVATIONS - 2184
TOTAL NUMBER IC ORSERVAY TOHS WITH VALID SPEED, DIRECTION AND STABILITY - 2192

$$
\begin{aligned}
& \text { SOUTHEAN CALIFORNIA EDISON COMI ANY } \\
& \text { SAN ONOFRE NUCLEAR GENERATING STATION } \\
& \text { ISY QUARTER, } 1984 \\
& \text { DAMES AND MOORE JOB NO - OO377-084-O9 } \\
& \text { DATA PERIOD- O1/O1/B4 TO O3/31/B4 } \\
& \text { STA3ILITY CLASS ALL IIO-4O METERS, } \\
& \text { WINDS AT IO MEIER LEVEL. }
\end{aligned}
$$

$$
25-J u-84
$$

WIND FREQUENCY DIGTRIBUTION
(FREQUENCY IN NUMBER OF OCCURRENCEG)

| WIND |  |  | UPPER CLABS INTERVALS OF WIND BPEED (MPH) |  |  |  |  |  |  |  | 11 | \$11 | thtal | MEAN SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OIRECTIDN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | $\bullet$ | 10 |  |  |  |  |
| NINE | 0 | 7 | 37 | 72 | 79 | 100 | 109. | 106 | 69. | 120 | 79 | 100 | 394 | 7. 60 |
| HE | 0 | 3 | 15. | 15 | 7 | 14 | 7 | 6 | 3 | 3 | 1 | 18 | 92. | 6.61 |
| ENE | 0 | 6. | 3. | 6 | 6. | 3 | 6 | 1 | 1. | 1 | 0 | 0 | 33. | 4.54 |
| E | 1. | 0. | 4 | 2 | $\theta$ | 6 | 4 | 2 | 0 | 1 | 0 | 2 | 30 | 539 |
| E3E | 1 | 1 | 6 | 4 | 1 | 4. | 8 | 5 | 1 | c | 0 | 0 | 31 | 5.06 |
| SE | 0 | 0 | 0 | 9 | 9 | 13 | 9 | 7 | E | 8 | 4 | 1 | 68 | 6. 75 |
| SSE | 0 | 1 | 9 | 15 | 14 | 12 | 9 | 8 | 7 | 9 | 1 | 0 | 83 | 5. 70 |
| S | 0 | 0 | 13 | 10 | 12 | 15 | 16 | 18 | 5 | 3 | 4 | 0. | 96. | 5. 99 |
| 55W | 0 | 0 | 7 | 9 | 13 | 12 | 7 | 7 | 10 | 2 | 0 | 2 | 69 | 5.83 |
| SW | 0 | 2 | 13 | 17 | 23. | 16 | B | 8 | 0 | 0 | 0. | 0 | 89 | 459 |
| WSW | 0 | 2 | 7 | 22 | 30 | 19 | 17 | 4 | 2 | 3 | 1 | 6 | 113 | 5. 51 |
| W | 0. | 0 | 5 | 19 | 41 | 53 | 30 | 20 | 7 | 5 | 4 | 5 | 189 | 6.02 |
| WNW | 0 | 1 | 3 | 10. | 21 | 27. | 26. | 12 | 10 | 11 | 4 | 14 | 139 | 716 |
| NW | 0 | 0 | 6 | 8. | 6 | 11. | 13. | 5 | 0 | 1 | 1. | 2 | 53. | 5. 65 |
| NNW | 0 | 2 | 4 | 12. | 10 | 11 | 10 | 4 | 1 | 1 | 0 | 1 | 57. | 5.09 |
| N | 0 | 6 | 3 | 15. | 19 | 16. | 18. | 11. | 12 | 11 | 4 | 6 | 121. | 6. 39 |
| VARIABLE |  |  |  |  |  |  |  |  |  |  |  |  | 0 | - 00 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  | 0. | 0. 00 |
| TOTAL | 2 | 31. | 139 | 246. | 297 | 332 | 297 | 224 | 136 | 179 | 103 | 157 | 2159 | 6. 63 |

WIMD FREGUENCY DISTRIBUYIDN (FREQUENCY IN PERCENT OF TOTAL)

| $\begin{aligned} & \text { WIND } \\ & \text { OIRECTION } \end{aligned}$ |  | 1 | 2 |  |  | 3 UPPER |  | ${ }_{4}$ | As |  | $\begin{aligned} & \text { ATERVAL.S } \\ & 6 \end{aligned}$ |  |  | $\begin{array}{r} 0 \mathrm{~F} \\ 7 \end{array}$ |  | ${ }_{8}$ | BPEED |  | MPH) |  |  | 11 | >11 |  | total |  | MEAN SPEED |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | 10 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NNE | 0. |  | 00 | 0 | 32 | 1 | 71 |  | 3. | 33 |  |  |  | 3 | 47 |  | 63 | 5 | 05 | 4 | 91 | 4. | 12 | 9 | 56 | 3 | 66 | 4 | 63 |  | 41 | 7 | 60 |
| NE | 0 | 00 | 0 | 14 | 0 | 69 | 0 | 69 | 0. | 32 | 0 | 65 | 0 | 32 | 0 | 28 | 0. | 14 | 0 | 14 | 0 | 05 | 0 | 83 | 4 | 26 | 6. | 61 |
| ENE | 0 | 00 | 0 | 28 | 0 | 14 | 0 | 28 | 0 | 28 | 0 | 14 | 0 | 28 | 0 | 05 | 0 | 55 | 0. | 05 | 0 | 00 | 0 | 00 | 1 | 53 | + | 54 |
| E | 0 | 05 | 0 | 00 | 0 | 19 | 0 | 09 | 0. | 37 | 0 | 28 | 0 | 19 | 0 | 09 | 0 | 00 | 0. | 05 | 0 | 00 | 0 | 09 | 1 | 37 | 3 | 39 |
| ESE | 0 | 05 | 0 | 05 | 0 | 28 | 0 | 19 | 0. | 05 | 0 | 19 | 0. | 37 | 0 | 23 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 1. | 44 | 5 | 06 |
| SE | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 42 | 0 | 42 | 0. | 60 | 0 | 42 | 0 | 32 | 0 | 37 | 0 | 37 | 0 | 19 | 0 | 05 | 3 | 15 | 6. | 75 |
| S3E | 0. | 00 | 0. | 05 | 0 | 42 | 0 | 69 | 0 | 65 | 0. | 36 | 0 | 42 | 0 | 37 | 0. | 32 | 0 | 42 | 0 | 05 | 0 | 00 | 3 | 94 | 5. | 70 |
| $\varepsilon$ | 0 | 00 | 0 | 00 | 0 | 60 | 0 | 46 | 0 | 56 | 0. | 69 | 0 | 74 | 0 | 83 | 0 | 23 | 0 | 14 | 0 | 19 | 0 | 00 | 4 | 45 | 5 | 89 |
| 551. | 0 | 00 | 0 | 00 | 0 | 32 | 0 | 42 | 0 | 60 | 0 | 36 | 0 | 32 | 0 | 32 | 0 | 46 | 0. | 09 | 0 | 00 | 0 | 09 | 3 | 20 | 5 | 83 |
| SW | 0 | 00 | 0 | 09 | 0 | 60 | 0 | 79 | 1 | 16 | 0. | 74 | 0 | 37 | 0 | 37 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 4 | 12 | 4. | S5 |
| WSH | 0 | 00 | 0 | 09 | 0 | 32 | 1 | 02 | 1. | 39 | 0 | 88 | 0 | 79 | 0 | 19 | 0 | 09 | 0 | 14 | 0. | 05 | 0 | 28 | 5 | 23 | 5 | 51 |
| 4 | 0 | 00 | 0 | 00 | 0 | 23 | 0 | 88 | 1. | 90 | 2 | 45 | 1. | 39 | 0 | 93 | 0 | 32 | 0 | 23 | 0 | 19 | 0 | 23 | 0 | 75 | 6. | 02 |
| WNW | 0 | 00 | 0 | 05 | 0 | 14 | 0 | 46 | 0 | 97 | 1 | 29 | 1 | 20 | 0 | 56 | 0 | 46 | 0 | 51 | 0 | 19 | 0 | 69 | 5 | 44 | 7 | 16 |
| NW | 0 | 00 | 0 | 00 | 0 | 28 | 0 | 37 | 0 | 28 | 0 | 51 | 0 | 60 | 0 | 23 | 0 | 00 | 0 | 03 | 0 | 09 | 0 | 09 | 2 | 45 | 5 | 65 |
| Noviw | 0 | 00 | 0 | 09 | 0 | 19 | 0 | 60 | 0 | 45 | 0 | 51 | 0 | 45 | 0 | 19 | 0 | 05 | 0 | 05 | 0 | 00 | 0 | os | 2 | 64 | 5 | 09 |
| $N$ |  | 00 | 0 | 28 | 0 | 14 | 0 | 69 | 0 | 88 | 0 | 74 | 0 | 83 | 0. | 51 | 0 | 56 | 0 | 51 | 0 | 19 | 0 | 28 | 5 | 60 | 6 |  |
| VAAIABLE 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 00 | 0 |  |
| TOTAL | 0. | 09 | 1. | 44 | 6 | 25 | 11 | 39 | 13 | 76 | 15 | 38 | 13 | 76 | 10 | 38 |  | 23 | e | 29 | 4 | 77 | 7 | 27 | 00 | 00 |  | 63 |

TOTAL NUMBER OF POSSIBLE ORSERVATIONS - $2: 84$
TOTAL NUMDER OC OBSERVATIONS WITH VALID SPEED, DIRECTION AND STADILITY - 2192

| OUTHERN CALIFORNIA EDISON COMPANY | UL-84 |
| :---: | :---: |
| SAN ONOFRE NUCLFAR GENERATING STATION |  |
| 2ND QUARTER. 1984 |  |
| DAMES AND MOORE JOD NO - 00377-084-09 |  |
| DATA PERILDD-04/01/34 TO 06/30/04 |  |
| STABILITY CLASS *A* (10-40 METERS |  |
| WINDS AT 10 METER LEVEL |  |

WIND FREQUENCY DISTRIBUTION
(FREGUENCY IN NUMBER OF OCCURRENCES)

| HIND |  |  | IJPPER CLASS |  |  | INTERVALS OF |  | WIND SPEED (MPH) |  |  | 11 | 311 | total | MEAN |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 日 | 9 | 10 |  |  |  | SPE |  |
| NNE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| NE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 00 |
| ENE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 00 |
| E | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| ESE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | - | 6 | 0. | 0. | 0 | 00 |
| SE | 0 | 0 | 0. | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 1. | 4 | 8 | 57 |
| SOE | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 5 | 6 | 2 | 3 | 20. | 41. | 11. | 17 |
| 5 | 0 | 0 | 2 | 4 | 8 | 9 | 11 | 16 | 21 | 20 | 9 | 21 | 121. | 8. | 54 |
| S5W | 0. | 0 | 1 | 5 | 13. | 19 | 23 | 25. | 28 | 9 | 2 | 4. | 129 | 7 | 17 |
| 5w | 0. | 0 | 2 | 11. | 22. | 32 | 42. | 32 | 13 | 5 | 2 | 1 | 162 | 6 | 41 |
| WSW | 0 | 0 | 1 | 6 | 17. | 39 | 45 | 25. | 12. | 7 | 3 | 1 | 156 | 6. | 53 |
| $\omega$ | 0 | 0 | 0 | 1 | 20 | 27 | 27 | 19 | 26 | 15 | 8 | 12 | 153. | 7. | 64 |
| WNW | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 2 | 4 | 2 | 2 | 21 | 36 | 11 | 25 |
| NW | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 1 | 0 | 0 | 1 | 2 | 11 | 90 |
| NINW | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| N | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 00 |
| VARIABLE |  |  |  |  |  |  |  |  |  |  |  |  | 0. | 0 | 00 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0 | 00 |
| TOTAL | 0 | 0 | 6. | 27 | ni. | 132 | 193 | 125 | 111 | 61 | 29 | A2 | 906 | 7 | 39 |

WIND FREGUENCY DISTRIBUTION
(FREGUENCY IN PERCENT OF TOTAL)

| W1ND |  |  |  |  | UPPER |  |  | CLABS |  | NTERVALS |  |  | $\begin{gathered} \text { OF } \\ 7 \end{gathered}$ | WIN | 8 | 9 |  | MPH) |  | 11 |  | >11 |  | total |  | MEAN |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIPECTION | ON |  | 2 |  | 3 |  | 4 |  |  |  | 6 |  |  |  |  |  |  |  | 10 |  |  | SPE |  |  |  |
| NNE | 0.00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 |  |  |  | 00 | 0 | 00 |  | 00 |
| NE | 0.00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | . | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 |
| ENE | 000 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 |
| E | 0.00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 |  | 00 | 0 | 00 | 0 | 00 |
| ESE | 000 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 09 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 |
| SE | 000 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 09 | 0. | 00 | 0 | 05 | 0 | 00 | 0 | 05 | 0 | 19 | 8 | 57 |
| BSE | 000 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 14 | 0 | 09 | 0 | 24 | 0. | 28 | 0 | 09 | 0 | 14 | 0 | 94 | 1 | 93 | 11 | 17 |
| 5 | - 00 | - | 00 | 0 | 09 | 0 | 19 | 0 | 38 | 0 | 42 | 0 | 52 | 0 | 73 | 0 | 99 | 0 | 94 | 0 | 42 | 0 | 99 | 5 | 71 | B. | 54 |
| 55w | 000 | 0 | 00 | 0 | 05 | 0 | 24 | 0 | 61 | 0 | 90 | 1 | O8 | 1 | 18 | 1 | 32 | 0 | 42 | 0 | 09 | 0 | 19 | 6 | O8 | 7. | 17 |
| SW | - 00 | 0 | 00 | 0 | 09 | 0 | 52 | 1 | 04 | 1 | 51 | 1 | 98 | 1 | 51 | 0 | 61 | 0 | 24 | 0 | 09 | 0 | Os | 7 | 64 | 6. | 41 |
| W5W | 000 | 0 | 00 | 0 | 05 | 0 | 29 | 0 | 80 | 1 | 84 | 2 | 12 | 1 | 18 | 0 | 57 | 0 | 33 | 0. | 14 | 0 | 05 | 7 | 3s | 6 | 53 |
| W | 0.00 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 94 | 1 | 27 | 1 | 27 | 0 | 90 | 1 | 23 | 0 | 71 | 0 | 38 | 0 | 57 | 7 | 31 | 7 | 64 |
| WNW | 000 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 14 | 0 | 09 | . | 09 | 0 | 19 | 0 | 09 | 0 | 09 | 0 | 95 | 1 | 70 |  | 25 |
| NW | 000 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | - | 00 |  | 00 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 07 | 11 | 00 |
| NNW | 0.00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | $c$ | 00 | 0 | 00 | 0 | 00 |
| N | 0.00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | $\bigcirc$ | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 |  | 00 |
| VARTABLE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 00 | 0 | 00 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\bigcirc$ | 00 | 0 |  |
| tal | 000 |  |  |  |  |  |  |  | 77 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

[^3]```
SOUTHERN CALIFOPNIA EDISON CORIPANY
    SAN ONOFRE NUCLEAR GENERATING STATION
    2ND GUARTER, 1994
    DAMES AND MOORE JOB NO - 00377-084-09
    DATA PERIOD- 04/01/94 TO 06/30/94
    STABILITY CLASS NB* (10-40 METERS,
    WINDS AT 10 METER LEVEL
```

                                    25-JUL-84
    WIND FREQUENCY DIGTRIBUTION
(FREGUSNCY IN NUMBER OF OCCURRENCES)

| WIND |  |  | UPPER CLASS INTERVALS OF WIND GPEED (MPH) |  |  |  |  |  |  |  |  |  |  | MEAN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 311 | total | SPEED |
| Nene | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | O. 00 |
| NE | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0.00 |
| ENE | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. 00 |
| E | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. 00 |
| ESE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - 00 |
| SE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 3 | 963 |
| SSE | 0 | 0 | 0 | 0 | 0 | 1. | 1 | 2 | 0. | 1 | 0 | 3 | 8 | 9.61 |
| 5 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 1 | 5 | 716 |
| 55w | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 3 | 7.13 |
| SW | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 5 | 6. 00 |
| W5W | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1. | 3. 70 |
| $\omega$ | 0. | 0 | 0 | 0 | 0. | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 7. 80 |
| WNW | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 1. | 0 | 0 | 0 | 0 | 1 | 7.70 |
| NW | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1. | 12. 40 |
| NNW | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. 00 |
| N | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - 00 |
| VARTABLE |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 000 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 000 |
| TOTAL | 0 | 0 | 1 | 1 | 2 | 2 | 6 | 6 | 2 | 2 | 0 | 6 | 28 | 8. 02 |

WIND FREQUENCY DISTRIBUTION
(FREQUENCY IN PERCENT OF TOTAL)


TOTAL NUMBER OF POSSIBLE OBSERVAIIONS - 2184
TOTAL NUMBER DC GESEAVATIDNS WITH VALID SPEED. DIRECTION AND STABILITY - 2120
SOUTHERN CALIFORNIA EDISON COMPANY
SAN INOFRE NUCLEAR GENENATING STATION
ZND GUARTER. 1984
D.AIAES AND MOORE JOR ND- $00377-084-09$
DATA PERIOD- $04 / 01 / 84$ TO $06 / 30 / 04$
STABILITY CLASS \#C (10-4O METERS ,
WINDS AT 10 METER LEVEL.

WIND FREQUENCY DISTRIBUTION
(FREQUENCY IN NUMBER OF OCCURRENCES)

| WIND |  |  | UPPER CLASS INTERVALS OF WIMD SPEED (MPH) |  |  |  |  |  |  |  |  |  |  | MEAN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OIRECTION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 711 | total | SPEED |
| NNE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0. | 0. 00 |
| NE | 0. | 0 | 0. | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 000 |
| ENE | 0. | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| E | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0. 00 |
| EsE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0. | 0. 00 |
| SE | 0 | 0 | 0. | 0 | 0 | 1. | 0 | 2 | 1 | 0 | 0 | 2 | 6 | 9. 78 |
| SSE | 0 | 0 | 0 | 2 | 1 | 3 | 1. | 4 | 0 | 2 | 1 | 5 | 19 | 9.03 |
| 5 | 0 | 0 | 1 | 1. | 3 | 1 | 0 | 2 | 2. | 1 | 2 | 1. | 14 | 720 |
| 35w | 0 | 0 | 1 | 1 | 1 | 3 | 2 | 2 | 0 | 0 | 0 | 0 | 10 | 570 |
| Sw | 0 | 0 | 1 | 1. | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 4 | 5.65 |
| W5W | 0 | 0 | 1 | 4 | 5 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 12 | 4.28 |
| W | 0 | 0 | 3 | 3 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 11. | 4 O 0 |
| WNW | 0 | 0 | 0 | 3 | 3 | 0 | 3 | 2 | 1 | 1 | 0 | 0 | 13 | 606 |
| NW | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 000 |
| NNW | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1. | 10 S0 |
| N | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | O. 00 |
| VARIABLE |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 0.00 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 000 |
| total | 0 | 0 | 7 | 15 | 16. | 10. | 9 | 12 | 4 | 4 | 5 | B | 90 | 6.63 |

WIND FREGUENCY DISTRIBUTION
(FREQUENCY IN PERCENT OF TOTAL)

| HIND |  |  |  |  |  | $3{ }_{3}$ UPPER ${ }_{4}$ |  |  | CLASS |  | INTERVALS |  |  | $\stackrel{\mathrm{OF}}{7}$ |  | ${ }^{1}$ | SPEE | ED (MPH) |  |  | 11 |  | 311 |  | TOTAL |  | MEAN SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECT1 | ON | 1 |  | 2 |  |  |  |  |  | 5 |  | 6 |  |  |  |  |  | 9 |  | 10 |  |  |  |  |  |  |  |
| NNE | - | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 |  | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | - | 00 | 0 | 00 |  | 00 | 0.00 |
| NE | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. 00 |
| ENE | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. 00 |
| E | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 000 |
| ESE | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0. | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0.00 |
| SE | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 00 | 0 | 09 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 09 | 0 | 29 | 9.78 |
| SSE | 0 | 00 | $\bigcirc$ | 00 | 0 | 00 | 0 | 09 | 0 | 05 | 0 | 14 | 0. | 05 | 0 | 17 | 0 | 00 | 0 | 09 | 0 | 05 | 0 | 24 | 0 | 90 | 9. 03 |
| 5 | 0. | 00 | 0 | 00 | 0 | 09 | 0 | 05 | 0 | 14 | 0 | 05 | 0. | 00 | 0 | 09 | 0. | 09 | 0 | 03 | 0 | 09 | 0 | 05 | 0. | 66 | 7.20 |
| S5w | $\bigcirc$ | 00 | 0 | 00 | 0 | 05 | 0 | 09 | 0 | 05 | 0 | 14 | 0 | 09 | 0. | 09 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 47 | 5. 70 |
| Sw | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 05 | 0 | 00 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 00 | 0 | 19 | 545 |
| W5W | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 19 | 0. | 24 | 0 | 05 | 0 | 05 | 0. | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 57 | 428 |
|  | 0 | 00 | 0 | 00 | 0 | 14 | 0 | 14 | 0 | 14 | 0. | 00 | 0 | 09 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 52 | 4 OB |
| WNW | $\bigcirc$ | 00 | 0 | 00 | 0 | 00 | $\bigcirc$ | 14 | 0 | 14 | 0 | 00 | 0 | 14 | 0 | 09 | 0 | 05 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 61 | 606 |
| NW | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 5 | 00 | 000 |
| nenh | 0 | 00 | 0 | 0 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 00 | - | 05 | 10 no |
| N | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | - |  |  |
| VARIABLE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 00 | 000 |
| CAL.MTOTAL. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 000 |
|  |  |  | 0 | 00 | 0 | 33 | 0 | 71 |  | 79 | 0 | 47 | 0 | 42 | 0 | 57 | 0 | 19 | 0 | 19 | 0 |  |  | 38 | 4 | 25 | 6.33 |

TOTAL NUMDER OF POSSISLE OBSERVATIONS - 2184
TOTAL NUMBER OC OBSERVATIONS WITH VALID SPEED. DIRECTION AND STABILITY - 2120

## TABLE 4A

| SAN ONOFRE NUCLEAR GENERATING STAZND GUARTER. 1984DAMES AND MOORE JOS NO- $00377-08$DATA PERIOD- $04 / 01 / 94$ TO $06 / 30 / 94$ |  |  |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |

25-JUL-84
SAN ONOFRE NUCLEAR GENERATING STATION
DAMES AND MOORE JOB NO - 00377-084-09
DATA PERIOD- 04/01/94 TO 06/30/94
WINDS AT 10 METER LEVEL

WIND FREQUENCY DIBTRIBUTION
(FREGUENCY IN NUMDER OF OCCURRENCES)


WIND FREQUENCY DISTRIBUTION (FREQUENCY IN PERCENT OF TOTAL)

| WIND |  |  |  |  |  |  |  | ${ }_{4}$ | ASS |  | 6 |  | $\begin{array}{r} \text { OF } \\ 7 \end{array}$ |  |  | 4D | EED |  | (MPH) |  | 11 |  | 311 |  | TOTAL |  | MEAN |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTIO | ON | 1 |  | 2 |  |  |  |  |  |  | 10 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NNE | 0 | 00 | 0 | 00 | 0 | 09 |  |  | 28 |  |  |  | 28 | 0 | 19 | 0 | 09 |  | 09 | 0 | 00 | 0 | 00 |  | 00 | 0 | 00 |  | 04 | 4 | 72 |
| NE | 0 | 00 | 0. | 00 | 0 | 05 | 0 | 24 | 0 | 09 | 0 | 05 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 42 | 3 | 70 |
| ENE | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 09 | 0. | $00^{\circ}$ | 0 | 28 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 57 | 4 | 38 |
| E | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 09 | 0 | 47 | 0 | 05 | 0 | 09 | 0 | 05 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 80 | 4 | 79 |
| ESE | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 33 | 0 | 19 | 0 | 61 | 0 | 57 | 0 | 28 | 0 | 42 | 0 | 19 | 0 | 00 | 0 | 00 | 2 | 64 | 6. | 34 |
| EE | 0 | 00 | 0 | 00 | 0 | 19 | 0 | 61 | 0 | 75 | 0 | 94 | 1 | 08 | 1. | 51 | 1. | 18 | 0 | 85 | 0 | 61 | 0. | 90 | 8 | 63 | 7 | 67 |
| SSE | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 47 | 0. | 38 | 0 | 47 | 0 | 19 | 0 | 47 | 0 | 42 | 0 | 28 | 0 | 14 | 0 | 33 | 3 | 21 | 7 | 27 |
| 5 | 0 | 00 | 0 | 00 | 7 | 38 | 0 | 33 | 0 | 47 | 0 | 33 | 0 | 28 | 0 | 19 | 0 | 28 | 0 | 14 | 0 | 14 | 0 | 05 | 2 | 57 | 5 |  |
| 93W | 0 | 00 | 0 | C5 | 0 | 09 | 0 | 28 | 0 | 38 | 0 | 33 | 0 | 05 | 0 | 14 | 0 | 09 | 0 | 05 | 0 | 09 | 0 | 09 | 1 | 69 | 5 | 02 |
| 5w | 0 | 00 | 0 | 00 | 0 | 09 | 0 | 19 | 0 | 24 | - | 24 | 0 | 14 | 0. | 24 | 0 | 09 | 0 | 05 | 0 | 09 | 0 | 00 | 1 | 32 | 5 | 94 |
| WSW | 0 | 00 | $\bigcirc$ | 09 | 0 | 24 | 0 | 19 | 0 | 09 | 0 | 04 | 0 | 09 | 0. | 00 | 0 | 00 | - | 05 | 0 | 00 | 0 | 05 | 0 | 89 | 4 | 90 |
| $\omega$ | 0 | 00 | 0 | 05 | 0 | 28 | 0 | 14 | 0 | 24 | - | 09 | 0 | 05 | 0 | 00 | 0. | 05 | 0 | 05 | 0 | 00 | 0 | 04 | 1 | 04 | 5 | 32 |
| WNW | 0 | 00 | 0 | 00 | 0 | 09 | 0 | 09 | 0 | 19 | 0 | 09 | 0 | 09 | 0 | 19 | 0 | 09 | 0 | 00 | 0 | 05 | 0 | 19 | 0 | 94 | 7 | 54 |
| NW | 0. | 00 | 0 | 00 | 0 | 09 | 0 | 14 | 0 | 09 | 0 | 14 | 0 | 09 | 0. | 09 | 0 | 09 | $\bigcirc$ | 09 | 0 | 00 | 0 | 28 | 1 | 13 | B |  |
| NNW | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 24 | 0 | 00 | 0 | 05 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | oo | 0 | oo | 0 | 33 | 3 | 66 |
| N | 0 | 00 | 0 | 14 | 0 | 24 | 0 | 42 | 0 | 24 | 0 | 14 | 0 | $0{ }^{\circ}$ | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | , | 32 |  |  |
| VARIABLE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 00 |  |  |
| TOTAL | 0 | 00 |  | 28 | 2 | 03 | 4 | 15 |  | 20 | 4 | 10 | 2 | 92 | 3 | 30 | 2 | 74 | 1 | 75 | 1 | OB | 1 | 96 | 28 | 54 |  | 48 |

TOTAL NUMBER OF POSSIBLE OBSERVATIONS - 2184
TOTAL NUMBER OC OBSERVATIONS WITH VALID SPEED, DIRECTION AND STABILITY - 2120

```
SOUTHERN CALIFGRNIA EDISON COMPANY
SAN ONOFRE NUCLFAR GENERATING STATION
2ND GUARTER, 1984
DAME!3 AND MDORE JOB NO - 00377-084-09
DATA PERIOD- 04/01/94 TO 06/30/94
STABILITY CLASS MEN (10-40 METERS )
WINDS AT 10 MEIER LEVEL
```

25-JUL-84

WIND FREQUENCY DISTRIBUTION
(FREQUENCY IN NUMBER OF OCCURRENCES)

| WIND |  |  | UPPER CLASS INTERVALS OF WIND SPEED (MPH) |  |  |  |  |  |  |  |  |  |  | MEAN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIMECTION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 311 | TOTAL | SPEED |
| NNE | 0 | 2. | 6 | 18. | E | 4. | 5 | 5 | 0 | 2 | 0 | 0 | 50. | 469 |
| NE | 0 | 1 | 2 | 1. | 3 | 0 | 0. | 0. | 0 | 0 | 0 | 0 | 7 | 3.49 |
| ENE | 0 | 0 | 1 | 3 | 2. | 1 | 0 | 0. | 0 | 0 | 0 | 0. | 7 | 3. 99 |
| $E$ | 0 | 0. | 2 | 2. | 3. | 4 | 1. | 1 | 1 | 1. | 0. | 0 | 15. | 9. 33 |
| ESE | 0 | 0 | 3 | 3 | 4 | 6 | 1 | 0 | 1 | 0 | 0 | 0. | 18. | 4.64 |
| SE | 0 | 0 | 3. | 10. | 6 | 6 | 7 | 2. | 2 | 0 | 0. | 0 | 36. | 5.13 |
| SJE | $\bigcirc$ | 1 | 6 | 9 | 2 | 5 | 2 | 2 | 0 | 0 | 0 | 0 | 27 | 420 |
| 5 | 0. | 0 | 3 | 2 | 2. | 1 | 3 | 0 | 0 | 0. | 0 | 0 | 11 | 459 |
| 83W | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1. | 0 | 0 | 0 | 0 | 4 | 6.30 |
| SW | 0 | 0 | 1 | 2 | 1. | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 6 | 4.52 |
| WSW | 0 | 0 | 0 | 2. | 0. | 0 | 0 | 1 | 0 | 1. | 0 | 0 | 4 | 578 |
| $\cdots$ | 0 | 0 | 1. | 3. | 2 | 0 | 0 | 0 | 0 | 0. | 0 | 0. | 6 | 3.68 |
| WNW | 0 | 1 | 1. | 1 | 2 | 1 | 2 | 1 | 0 | 0 | 0 | 1 | 10. |  |
| NW | 0 | 1 | 3. | 1. | 2 | 2 | 1 | 0 | 1 | 0 | 1 | 5 | 17. |  |
| NNW | 0. | 1 | 2 | 3. | 0 | 0 | 1 | 1 | 1. | 0 | 0 | 0 | 9 | 4 ¢3 |
| N | 0 | 2 | 12. | 5 | 3 | 2 | 2 | 2 | 0 | 1 | 0 | 0 | 29 |  |
| VAR IABLE |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 000 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  | 0 |  |
| TOTAL | 0 | 9 | 46. | 59. | 40 | 35 | 27 | 16. | 6. | 5 | 1 | 6 | 236 | 4.91 |

WIND FREQUENCY DISTRIBUTION
(FREQUENCY IN PERCENT OF TOTAL)


TOFAL NUMBER OF POSSIBLE OBSERVATIONS - 2184
TO:AL NUMBEH OC OBSERVATIONS WITH VALID SPEED. DIRECTION AND STABILITY - 2120

## TABLE 4A



WIND FREQUENCY DISTRIBUTION
(FREQUENCY IN NUMBER OF OCCURRENCES)


WIND FREGUENCY DISTRIBUTION
(FREQUENCY IN PERCENT OF TOTAL.)

| HIND |  |  |  |  |  | UPPER |  |  | LASS | 5 | INTERVALS 6 |  |  | $8$ |  | ND ${ }^{\text {c }}$ | SPEE | $\square^{9}$ | $\begin{array}{r} \mathrm{MPH})_{10} \end{array}$ |  | 11 |  | 711 |  | TOTAL |  | MEAN SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTI | ON | 1 |  | 2 |  | 3 |  | 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NNE | 0 | 00 | 0 | 05 | 0 | 33 | 1 | 18 |  | 98 | 1 | 32 | 1. | 04 |  | 24 | 0 | 24 | 0 | 09 | 0 | 00 | 0 | 00 | 6. | 42 | 512 |
| NE | 0 | 00 | 0 | 09 | 0 | 14 | 0 | 28 | 0 | 14 | 0 | 09 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 71 | 375 |
| ENE | 0 | 00 | 0 | 00 | 0 | 09 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 17 | 373 |
| E | c. | 00 | 0 | 05 | 0 | 14 | 0 | 00 | 0 | 05 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | - | 00 | 0. | 28 | 3 |
| Ese | 0 | 00 | 0 | 00 | 0 | 09 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 14 | 2 |
| SE | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 5 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 05 | 2 |
| SSE | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 05 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | OC | 0. | 09 | 2.9 |
| 5 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 05 | 2 |
| 55w | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 |
| SW | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | о0 | 0 | 00 | 0 | 00 | 0. | 00 | - | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 |
| WSW | 0 | 00 | 0 | 00 | 0 | 14 | 0 | 05 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 19 | 2 |
| W | 0 | 00 | 0 | 00 | 0 | on | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 |
| WNW | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 09 | 0 | 00 | 0. | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0. | 05 | 7 |
| NW | 0 | 0 | 0 | 00 | 0 | 00 | 0 | 09 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 05 | 0 | 05 | 0 | 05 | 0 | 00 | 0 | 19 | 8 |
| NiNW | $\bigcirc$ | 00 | 0 | 00 | 0 | 05 | 0 | 03 | 0 | 05 | 0 | 05 | 0 | 00 | 0 | 05 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 00 | 0 | 24 | 4 |
| N | 0 | 00 | 0 | 00 | 0 | 19 | 0 | 39 | 0 | 19 | 0 | 14 | 0 | 09 | 0 | 09 | 0 | 09 | 0 | 00 | 0 | 05 | 0 | 00 | 1 | 23 | 4 |
| VARTABLE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0. | 00 | 0 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 00 | 00 |
| TOTAL | 0 | 00 | 0 | 14 | 1 | 32 |  | 12 | 2 | 41 |  | 65 | 1 | 23 |  |  |  |  | 0 | 09 | 0 | $0 \%$ |  |  |  | 81 | 4.3 |

TOTAL NUMBER OF POSSIBLE OBSERVATIONS - 2184
TOTAL NUMBER OC OBSERVATIONS WITH VALID SPEED, DIRECTION AND STABILTTY - 2120

```
SOUTHERN CALIFOPNIA EDISON COMPANY
    25-JUL-34
SAN ONOFRE NUCLEAR GENERATING STATION
IND QUARTER, 1984
DAMES AND MOORE JOB NO - 00377-084-09
DATA PERIOD- 04/01/84 TO 06/30/84
STABILITY CLASS WG* (10-40 METERS)
WINDS AT 10 MEIER LEVEL
```

WIND FREQUENCY DIGTRIBUTION
(FREGUENCY IN NUMBER OF OCCURRENCES)

| WIND |  |  | UPPER |  | CLASS | INTERVALS OF |  | WIND | $8 \text { SPEED }$ | $9{ }_{10}^{(\mathrm{MPH})}$ | 11 | 211 | TOTAL | MEAN SPEED |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIRECTION | 1 | 2 | 3 | 4 |  | 56 | 7 |  |  |  |  |  |  |  |
| NNE | 0. | 0 | 0 | 1. | 9. | 19 | 19 | 27. | 21 | 8 | 4 | 0 | 108 | 719 |
| NE | 0. | 0 | 0. | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0. | 0 | 0 | - 00 |
| Ene | 0. | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1. | 5.40 |
| E | 0. | 0 | 0. | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. 00 |
| Ese | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | o. 00 |
| SE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0. 00 |
| SSE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| 5 | 0. | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0. | - 00 |
| 55w | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | - 00 |
| SW | 0. | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | - 00 |
| WSW | 0. | 0. | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| $\omega$ | 0. | 0. | 0. | 0. | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | - 00 |
| LNW | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1. | 1 | 4 | B 85 |
| NiN | 0 | 0 | 0 | 0. | 0 | 1. | 0 | 0 | 0 | 0. | 3. | 0 | 4 | 9. 33 |
| rand | 0. | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0. | - 00 |
| N | 0 | 0 | 0 | 1. | 0 | 1 | 5 | 3 | 0 | 0 | 0 | 0 | 10 | 6. 50 |
| VAPIABLE |  |  |  |  |  |  |  |  |  |  |  |  | 0. | c. 00 |
| CALM |  |  |  |  |  |  |  |  |  |  |  |  | 0 | 000 |
| TOTAL | 0 | 0 | 0 | 2 | 10. | 22 | 24 | 31 | 21. | E | 8 | 1 | 127 | 7.24 |

WIND FREQUENCY DISTRIBUTION (FREQUENCY IN PERCENT OF TOTAL.)


TOTAL NUMBER OF POSSIBLE ORSERVATIONS - 2184
TOTAL NUMBER DC OBSERVATIONS WITH VALID SPEED. DIRECTION AND STABILITY - 2120

## TABLE 4A

```
SOUTHERN CALIFORNIA EDISON COMPANY
SAN ONOFRE NUCLFAR GENERATING STATION
ZND GUARTER, 1984
DAMES AND MOORE JOB NO - 00377-084-0%
DATA PERIOD- 04/O1/B4 TO 06/30/34
STABILITY CLAGS ALL (10-40 METERS )
WINDS AT 10 MEIER LEVEL
```

25-JUL-84

WIND FREGUENCY DIGTRIBUTION
(FREQUENCY IN NUMBER OF OCCURRENCES)


WIND FREQUENCY DIGTRIBUTION
(FREQUENCY IN PERCENT OF TOTAL)


TOTAL NUMBER OF POSSIBLE OBSERVATIONS - 2184
TOTAL NUMBER OG OBSERVATIONS WITH VALID SPEED. DIRECTION AND STABILITY - 2120

## SECTION H. 10 CFR 50 APPENDIX I AND 40 CFR 190 CONSIDERATIONS

The table in Section $H$ presents the maximum dose to an individual for the first and second quarters. Six different categories are presented: (1) Liquid Effluerts - Whole Body, (2) Liquid Effluents - Organ, (3) Airborne Effluents Iodines and Particulates, (4) Noble Gases - Gamma, (5) Noble Gases - Beta, and (6) Direct Radiation.

The doses for categories 1 and 2 were calculated using the methodology of the ODCM, this data is also presented in Table $2 D$ for the first and second quarters. Categories 3, 4 , and 5 were calculated utilizing RRRGS (Radioactive Release Report Generating System) software, Reg. Guide 1.109 methodology, and concurrent meteorology. Table 1E lists data similar to categories 3, 4, and 5 covering the first and second quarters using methods described in the ODCM and the historical meteorology $(X / Q)$. Category 6 presents direct dose data measured by TLD dosimeters. Each portion of each category is footnoted to briefly describe each maximum individual dose presented.

10 CFR 50 APPENDIX I AND 40 CFR 190 CONSIDERATIONS

|  | Dose* (millirems) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SOURCE | 1st Q | 2nd Q | 3 rd Q | 4th Q | YEAR |
| Liquid Effluents | $\begin{aligned} & \text { 1) } \\ & \text { 1.01E-1 } \end{aligned}$ | 2) <br> $7.81 \mathrm{E}-2$ | 3) | 4) | 5) |
|  | 6) $2.05 E+0$ | $\begin{aligned} & \text { 7) } \\ & \text { 8. } 40 \mathrm{E}-1 \end{aligned}$ | 8) | 9) | 10) |
| Airborne Effluents Iodines and Particulates | $\begin{aligned} & \text { 11) } \\ & 3.24 \mathrm{E}-2 \end{aligned}$ | $\begin{aligned} & \text { 12) } \\ & 5.64 \mathrm{E}-2 \end{aligned}$ | 13) | 14) | 15) |
| Noble Gases** | $\begin{aligned} & \text { 16) } \\ & 1.03 \mathrm{E}-1 \end{aligned}$ | $\begin{aligned} & \text { 17) } \\ & \text { 5.48E-1 } \end{aligned}$ | 18) | 19) | 20) |
|  | $\begin{aligned} & \text { 21) } \\ & 3.08 \mathrm{E}-1 \end{aligned}$ | $\begin{aligned} & \text { 22) } \\ & 1.54 \mathrm{E}+0 \end{aligned}$ | 23) | 24) | 25) |
| Direct Radiation | $\begin{aligned} & \text { 26) } \\ & 2.02 \mathrm{E}-1 \end{aligned}$ | $\begin{aligned} & \text { 27) } \\ & 1.64 \mathrm{E}-1 \end{aligned}$ | 28) | 29) | 30) |

* The numbered footnotes below briefly explain how each maximum dose was calculated, including the organ and the predominant pathway(s).
** Noble gas doses due to airborne effluents are in units of mrad reflecting the air dose.

1. This data was calculated using the methodology of the ODCM.
2. This data was calculated using the methodology of the OOCM.
3. This data to be evaluated during the third and fourth quarters.
4. This data to be evaluated during the third and fourth quarters.
5. This data to be evaluated during the third and fourth quarters.
6. This data was calculated using the methodology of the ODCM; the GI-LLI received the maximum dose primarily by the saltwater fish pathway.
7. This data was calculated using the methodology of the ODCM; the GI-LLI received the maximum dose primarily by the saltwater fish pathway.
8. This data to be evaluated during the third and fourth quarters.
9. This data to be evaluated during the third and fourth quarters.
10. This data to be evaluated during the third and fourth quarters.
11. The maximum organ dose was to a child's thyroid and was located in the NNW sector. This was calculated using the activity reported in the January June 1984 Semiannual Report with the assumptions of USNRC Regulatory Guide 1.109.
12. The maximum organ dose was to a child's thyroid and was located in the NNW sector. This was calculated using the activity reported in the January June 1984 Semiannual Report with the assumptions of USNRC Regulatory Guide 1.109
13. This data to be evaluated during the third and fourth quarters.
14. This data to be evaluated during the third and fourth quarters.
15. This data to be evaluated during the third and fourth quarters.
16. A maximum air dose of $2.79 \mathrm{E}-1 \mathrm{mrad}$ for gamma radiation was located in the SSW sector, a seaward direction. The reported maximum air dose for gamma radiation was located in the ENE sector, a landward sector, at the exclusion area boundary and caiculated with the assumptions of USNRC Regulatory Guide 1.109.
17. The maximum air dose for gamma radiation was located in the $E$ sector at the exclusion area boundary and calculated with the assumptions of USNRC Regulatory Guide 1.109.
18. This data to be evaluated during the third and fourth quarters.
19. This data to be evaluated during the third and fourth quarters.
20. This data to be evaluated during the third and fourth quarters.
21. A maximum air dose of $8.33 \mathrm{E}-1 \mathrm{mrad}$ for beta radiation was located in the SSW sector, a seaward direction. The reported maximum air dose for beta radiation was located in the ENE sector, a landward sector, at the exclusion area boundary and calcuiated with the assumptions of the USNRC Regulatory Guide 1.109.
22. The maximum air dose for beta radiation was located in the E sector at the exclusion area boundary and calculated with the assumptions of the USNRC Regulatory Guide 1.109.
23. This data to be evaluated during the third and fourth quarters.
24. This data to be evaluated during the third and fourth quarters.
25. This data to be evaluated during the third and fourth quarters.
26. Measurements were made using TLD dosimeters; values were prorated to 300 hours per year; highest dose was measured at the San Onofre State Beach (Unit 1 North location).
27. Measurements were made using TLD dosimeters; values were prorated to 300 hours per year; highest dose was measured at the San Onofre State Beach (Unit 1 North location).
28. This data to be evaluated during the third and fourth quarters.
29. Tnis data to be evaluated during the third and fourth quarters.
30. This data to be evaluated during the third and fourth quarters.

## SECTION I. 10 CFR 50 APPENDIX I AND 40 CFR 190 , PERCENT TECHNICAL SPECIFICATION LIMITS

The table in Section I corresponds to the table in Section H. Each dose presented in Section $H$ is related to the percent of Technical Specification Limits and this value listed in Section I.

10 CFR 50 APPENDIX I AND 40 CFR 190, PERCENT TECHNICAL SPECIFICATION LIMITS

|  | \% TSL |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SOURCE | 1st Q | 2nd $Q$ | 3 rd Q | 4th Q | YEAR |
| Liquid Effluents WHOLE BODY | $3.40 \mathrm{E}+0$ | 2. $6 \mathrm{E}+0$ |  |  |  |
| ORGAN | $2.05 \mathrm{E}+1$ | $8.40 \mathrm{E}+0$ |  |  |  |
| Airborne Effluents Iodines and Particulates | $2.16 \mathrm{E}-1$ | $3.76 \mathrm{E}-1$ |  |  |  |
| Noble Gases GAMMA | $1.03 \mathrm{E}+0$ | $5.48 \mathrm{E}-1$ |  |  |  |
| BETA | $1.54 \mathrm{E}+0$ | $7.70 \mathrm{E}+0$ |  |  |  |
| Direct Radiation | * | * |  |  |  |

* These sections were left intentionally blank since the 40 CFR 190 limit is based on a "per year" basis only.


## SECTION J. MISCELLANEOUS

## I. UNPLANNED RELEASES

On January 1, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 84 Curies $X e-133$ equivalent was released when the Waste Gas Header was drained of water. The release is described in full detail in Unit 2 LER \#84-001.

On January 12, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 23 Curies of Xe-133 equivalent was released as a release inside the Radwaste Butlding was cleared. This was reported via telephone to the NRC per 50.72 reporting requirements

On March 24, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 7.6 Curies of $\mathrm{Xe}-133$ equivalent was released when a Unit 3 degassification line was cleared. This was reported via telephone to the NRC per 50.72 reporting requirements.

On March 26, 1984, two unplanned but monitored gaseous releases occurred via the Plant Vent Stack. The first release occurred when Unit 3 letdown control valve leaked and released approximately 5.7 Curies of $\mathrm{Xe}-133$ equivalent. The second release occurred when the Waste Gas Decay tanks were sampled and approximately 5.5 Curies of $\mathrm{Xe}-133$ equivalent was released. This was reported via telephone to the NRC per 50.72 reporting requirements.

On March 27, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 3.1 Curies of $\mathrm{Xe}-133$ equivalent was released as a sample was drawn off the Chemical Volume Control ion-exchanger. This was reported via telephone to the NRC per 50.72 reporting requirements.

On March 28, 1984, several unplanned but monitored gaseous releases occurred via the Plant Vent Stack. A total of approximately 12 Curies of $\mathrm{Xe}-133$ equivalent was released during sampling and relief valves lifting on the Waste Gas Header. These were reported via telephone to the NRC per 50.72 reporting requirements.

On March 30, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 0.2 Curies of $\mathrm{Xe}-133$ equivalent was released while dewatering a Crud Tank. This was reported via telephone to the NRC per 50.72 reporting requirements.

On April 1, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 0.1 Curies of Xe-133 equivalent was released while backflushing a radwaste filter. This was reported via telephone to the NRC per 50.72 reporting requirements.

On April 4, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 0.27 Curies of Xe-133 equivalent was released while backflushing a radwaste filter. This was reported via telephone to the NRC per 50.72 reporting requirements.

On April 5, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 1.4 Curies of Xa-133 equivalent was released while backflushing a radwaste filter. This was reported via telephone to the NRC per 50.72 reporting requirements.

On April 6, 1984, an unplanned but monitored gasecus release occurred via the Plant Vent Stack. A total of approximately 0.33 Curies of $\mathrm{Xe}-133$ equivalent was released while pumping 1 iquid radwaste into the Miscellaneous Radwaste tank. This was reported via telephone to the NRC per 50.72 reporting requirements.

On April 12, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 3.7 Curies of $\mathrm{Xe}-133$ equivalent was released while utilizing the Volume Control Tank sample line. This was reported via telephone to the NRC per 50.72 reporting requirements.

On April 17, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 0.36 Curies of $\mathrm{Xe}-133$ equivalent was released while utilizing the Pressurizer Degas System. This was reported via telephone to the NRC per 50.72 reporting requirements.

On April 19, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 0.1 Curies of $\mathrm{Xe}-133$ equivalent was released while draining the Pressurizer Vapor Space. This was reported via telephone to the NRC per 50.72 reporting requirements.

On April 23, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 22.7 Curies of $\mathrm{Xe}-133$ equivalent was released while backflushing a radwaste filter. This was reported via telephone to the NRC per 50.72 reporting requirements.

On April 30, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 1.8 Curies of Xe-133 equivalent was released while backflushing a radwaste filter. This was reported via telephone to the NRC per 50.72 reporting requirements.

On May 1, 1984, an unplanned but monitored gaseous release occurred via the Plant Vent Stack. A total of approximately 2.1 Curies of $X e-133$ equivalent was released while backflushing a radwaste filter. This was reported via telephone to the NRC per 50.72 reporting requirements.

On May 2, 1984, an unplanned but monitored release occurred via the Plant Vent Stack. A total of approximately 107 Curies of $\mathrm{Xe}-133$ equivalent was released when a rupture disc on a Waste Gas Compressor check valve failed. An UNUSUAL EVENT was declared per the Emergency Preparedness Procedure. The release is described in full detail in Unit 2 LER \#84-027.

On May 5, 1984, an unplanned but monitored release occurred via the Plant Vent Stack. A total of approximately 405 Curies of $\mathrm{Xe}-133$ equivalent was released When a Waste Gas Sampling System pressure control valve failed open. An UNUSUAL EVENT was declared per the Emergency Preparedness Procedure. The release is described in full detail in Unit 2 LER \#84-028.

On May 8, 1984, an unplanned but monitored release occurred via the Plant Vent Stack. A total of approximately 1.7 Curies of $\mathrm{Xe}-133$ equivalent was released while flushing a Reactor Coolant System sample line. This was reported via telephone to the NRC per 50.72 reporting requirements.

On May 13, 1984, an unplanned but monitored release occurred via the Plant Vent Stack. A total of approximately 1.4 Curies of $\mathrm{Xe}-133$ equivalent was released when a Waste Gas Header Relief valve lifted. This was reported via telephone to the NRC per 50.72 reporting requirements.

On June 2, 1984, an unplanned but monitored release occurred via the Plant Vent Stack. A total of approximately 427 Curies of $\mathrm{Xe}-133$ equivalent was released when safety relief valves on the Nuclear Sampling System lifted. The release is described in full detail in Unit 3 LER \#84-021.

## SUMMARY

During the 1 st quarter, unplanned but monitored releases by the plant vent stack were evaluated from computer recorded monitor data for the plant vent stack monitors and totaled $3.38 \mathrm{E}+3$ Curies of $\mathrm{Xe}-133$. This activity has been included in the total releases and has been included in the appropriate dose calculations.

During the 2nd quarter, unplanned but monitored releases by the plant vent stack were evaluated from computer recorded monitor data for the plant vent stack monitors and totaled $9.34 \mathrm{E}+3$ Curies of $\mathrm{Xe}-133$. This activity has been included in the total releases and has been included in the appropriate dose calculations.
11. UNIT 2 AND 3 EFFLUENT RADIATION MONITORS OUT OF SERVICE FOR GREATER THAN 30 DAYS



## III. CHANGES TO THE PROCESS CONTROL PROGRAM FOR SAN ONOFRE UNIT 2 AND UNIT 3

Interim approval for the Process Control Program for San Onofre Unit 2 and Unit 3 (Health Physics Procedure SO23-VII-8.5.1, Revision 1) was received on April 24, 1984. There was one revision made to the Process Control Program between the approval date of $4 / 24 / 84$ and $6 / 30 / 84$. On May 9, 1984, a revision of the Process Control Program (Health Physics Procedure S023-VII-8.5.1, Revision 2) was submitted to the Onsite Review Committee for approval in accordance with the Unit 2 and Unit 3 Technical Specifications. Most of the changes were done to comply with step 3.5 of the Process Control Program. The changes for this requirement reflect the new method for transporting the additive material $M-5$ to the disposable liner and the required change to the sample test/preparation requirements. These changes ensure the formula used for solidification is in compliance with the Chem-Nuclear Topical Report CNSI-WF-C-01-NP, "10 CFR 61 Waste Form Certification - Cement,"
November 30, 1983, and the latest cement solidification technology. The balance of the changes were a result of an April 13, 1984, meeting between SCE and the NRC. The Unit 2 and Unit 3 Process Control Program was modified to specifically state that the Process Control Program complies with 20.311 requirements for shipment and disposal. In addition changes were made to the Process Control Program to further clarify compliance with 10 CFR 61 and the specifically required sampling program. All the above described changes were reviewed and approved by the Onsite Review Committee as documented in Reference 4. The identified changes do not alter the logic or intent of the primary submittal of the Process Control Program.

## REFERENCES

1. Unit 2 and Unit 3 Technical Specifications, Section 6.13.2
2. Letter dated April 24, 1984 from the Nuclear Regulating Commission to Kenneth P. Baskin of SCE and James C. Holcombe of SDG\&E, relating to interim approval of the Unit 2 and Unit 3 Process Control Program.
3. Letter dated April 19, 1984 from Southern California Edison Company (SCE) to George W. Knighton of USNRC relating to a meeting between SCE and NRC in Bethesda, Maryland concerning approval of the Unit 2 and Unit 3 Process Control Program.
4. Memorandum dated May 9, 1984 to W. W. Strom of Nuclear Safety Group from W. C. Moody, Acting Chairman, Onsite Review Committee relating to Special Onsite Review Committee meeting No. 84-012.

## SECTION K. CONCLUSION

- Radioactive releases totaled $1.93 E+4$ Curies for gaseous effluents and 5.29E2 Curies for liquid effluents.
- Gaseous releases were primarily noble gases and totaled 1.93E+4 Curies of which $94.8 \%$ of the noble gases was $\mathrm{Xe}-133$.
- Liquid releases were primarily tritium and accounted for 2.78E +2 Curies or $52.6 \%$ of the total liquid releases.
- There were 2 radwaste shipments for SONGS $2 / 3$ to Richland, Washington. There were 536.8 cubic meters of solid radwaste shipped containing 100. 6 Curies of radioactivity.
- Meteorological conditions during the year were typical of the meteorology at SONGS $2 / 3$. Meteorological dispersion was good $36 \%$ of the time, fair $33 \%$ of the time, and poor $31 \%$ of the time.
- Compliance with 40 CRF 190 dose limits have been demonstrated in Section $H$ of this report and there are no other fuel cycle facilities within 8 kilometers.
- For liquid releases, marine sumple analyses will indicate if any radioactive material has concentrated in marine life. However, detection of any tritium in these sample; is not expected because of the rapid turnover of water in marine life and because of the bulk of ocean water available for dilution.
- The net results from the analysis $f$ these effluent releases indicate the operation of SONGS $2 / 3$ has not produced any detrimental effect on the environment.


## Southern California Edison Company

san onofre nuclear generating stationed 31030 PH $1: 03$

P.O. Box ${ }^{126}$

SAN CLEMENTE. CALIFORNIA 92672

August 29, 1984
U.S. Nuclear Regulatory Commission
Office of Inspection and Enforcement
Region V
1450 Maria Lane, Suite 210
Walnut Creek, California $94596-5368$

| Attention: | Mr. J. B. Martin, Regional Administrator |
| :--- | :--- |


| Dear Sir: |
| :--- |
| Subject: | | Docket Nos. $50-361$ and $50-362$ |
| :--- |
| Semiannual Radioactive Effluent Release Report |
| San Onofre Nuclear Generating Station, Units 2 and 3 |

In accordance with Sections 6.9.1.8 and 6.9.1.9 of Appendix A to Technical Specifications for Facility Operating License Nos. NPF-10 and NPF-15 for San Onofre Nuclear Generating Station, Units 2 and 3 , respectively, enclosed is the semiannual report of the radioactive content of effluents released to unrestricted areas and shipments of solid waste during the period January 1 to June 30, 1984.

This report has been prepared in the general format of NRC Regulatory Guide 1.21 , sections pertinent to SONGS 2 and 3. Included in this report are quarterly effluent summaries, percent of Technical Specification Limits, estimated total percent error, lower limit of detection concentrations, 40 CR 190 considerations, meteorological data and 50 mile radius population doses.

Please contact us if we can be of further assistance.


Enclosure

Units 2 and 3
San Onofre Nuclear Generating Station
cc: A. E. Chaffee (USNRC Resident Inspector, Units 1, 2 and 3) 30 PH 1. 3 ?
J. P. Stewart (USNRC Resident Inspector, Units 2 and 3$)^{-4}$
U.S. Nuclear Regulatory Commission Document Contpol Desk

Institute o: Nuclear Power Operations (INPO)


[^0]:    

[^1]:    *     - Nuclide detected in Table 1C

[^2]:    *Material shipped in 55 gal . D.O.T. 7 A Type A Drums ( $7.5 \mathrm{ft}^{3}$ ea.) and steel boxes (strong tight containers - $98 \mathrm{ft}^{3} \mathrm{ea}$.)

[^3]:    TOTAL NUMBER OF POSSIBLE ODSERVATIONS - 2184
    TOTAL NUMBER OC OBSERVATIONS WITH VALID GPEED. DIRECTION AND GTABILITY - Z:20

