# INSERVICE INSPECTION EXAMINATION REPORT

YANKEE ATOMIC ELECTRIC COMPANY YANKEE NUCLEAR POWER STATION

MARCH 31, 1984 THROUGH JUNE 9, 1984

# 8409240318 840914 PDR ADOCK 05000029 Q PDR

# PREFACE

This summary report covers the inservice inspection of Yankee Nuclear Power Station during the period March 31, 1984 through June 9, 1984.

Included in this report is the NIS-1 form as required by the provisions of ASME Section XI.

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# FORM NIS-1 OWNERS' DATA REPORT FOR INSERVICE INSPECTIONS

# As required by the Provisions of the ASME Code Rules

1.	Owner	Yankee	Atomic	Electric	Co.,	1671	Worcester	Road,	Framingham,	Ma.	01701
				(Name	and A	ddress	of Owner)				
					100						

2. Plant \_\_\_\_\_ Yankee Nuclear Power Station, Rowe, Massachusetts 01367 (Name and Address of Plant)

3. Plant Unit Yankee Rowe 4. Owner Certificate of Authorization (if required) DPR-3

5. Commercial Service Date 7/1/61 6. National Board Number for Unit Reactor #NB-23964

7. Components Inspected

Component or Appurtenance	Manufacturer or Installer	Manufacturer or Installer Serial No.	State or Province No.	National Board No.
Reactor Vessel	B&W	610-0011	N/A	23964
Steam Generator	W	N/A	N/A	404E(Z)1
Piping	S&W	N/A	N/A	N/ A
Pressurizer	B&W	610-0011	N/A	2397 4E 22

Note: Supplemental sheets in form of lists, sketches, or drawings may be used provided (1) size is  $8\frac{1}{2}$  in. x 11 in., (2) information in items 1 through 6 on this data report is included on each sheet, and (3) each sheet is numbered and the number of sheets is recorded at the top of this form.

This form (E00029) may be obtained from the Order Dept., ASME, 345 E. 47th St., New York, N.Y. 10017

# FORM NIS-1 (back)

8. Examination Dates 3/31/84 to 6/9/84 9. Inspection Interval from 12/1/74 to 12/1/84

10. Abstract of Examinations. Include a list of examinations and a statement concerning status of work required for current interval. Page 3 of 28

11. Abstract of Conditions Noted Page 6 of 28

12. Abstract of Corrective Measures Recommended and Taken Page 7 of 28

We certify that the statements made in this report are correct and the examinations and corrective measures taken conform to the rules of the ASME Code, Section XI.

9/5 19 84 Signed YANNER ATOMIC By In MSthamed Date

Certificate of Authorization No. (if applicable) DOR-3 Expiration Date 11/4/97 USNRC Facility License No.

# CERTIFICATE OF INSERVICE INSPECTION

I, the undersigned, holding a valid commission issued by the National Board of Boiler and Pressure Vessel Inspectors and/or the State or Province of <u>Massachusetts</u> and employed by <u>HSBI & I Co.</u> of <u>Connecticut</u> have inspected the components described in this Owners' Data Report during the period <u>3/31/84</u> to <u>6/9/84</u>, and state that to the best of my knowledge and belief, the Owner has performed examinations and taken corrective measures described in this Owners' Data Report in accordance with the requirements of the ASME Code, Section XI.

By signing this certificate neither the Inspector nor his employer makes any warranty, expressed or implied, concerning the examinations and corrective measures described in this Owners' Data Report. Furthermore, neither the Inspector nor his employer shall be liable in any manner for any personal injury or property damage or a loss of any kind a sing from or connected with this inspection.

Date	916	1984	
P.J	Lane	Commissions	Mass. 1182
NY	Inspector's Signatur	e .	National Board, State, Province and No.

10. Abstract of Examinations (Safety Class 1)

ASME Code			
Category	No.	Components Examined	Method
B-A		Closure Head Flange Circulation Weld	UT
		Vessel to Flange Weld	UT
B-B	(2)	Welds Steam Generator #3	UT
	(3)	Pressurizer Nozzles	UT
B-D	(4)	Outlet Nozzles	UT, VT
	(4)	Inlet Nozzles	UT,VT
	(4)	Outlet Nozzles to Reducer	UT,VT
	(4)	Inlet Nozzles to Reducer	UT,VT
B-E	(1)	Feed/Bleed Heat Exchanger Nozzle	VT
B-F	(1)	Pressurizer Safe End Weld	PE,UT
B-G-1	(52)	Rx Head Studs, Nuts, and Washers	VT,MT,UT
		Flange Ligaments	UT
B-G-2	(2)	Safety Valves SV-181/182 Bolting	VT
	(20)	Studs/Nuts Main Coolant Check Valve #316	UT, VT
	(16)	Stator Cap Bolts, #2 Main Coolant Pump	UT,MT,VT
	(12)	Studs/Nuts Pressurizer Primary Manway	UT,VT
	(40)	Studs, #2 Steam Generator Primary Manway	UT,MT,VT
	(38)	Studs, #3 Steam Generator Primary Manway	UT, MT, VT
	(40)	Studs, #4 Steam Generator Primary Manway	UT, MT, VT
В-Н	(4)	Welded Supports Feed/Bleed Heat Exchangers	PE
B-J	(34)	Satety Class 1 Pipe Welds	UT, PE, VT
B-K-1	(3)	Integrally Welded Pump Supports	PE
B-K-2	(5)	Nonwelded Supports	VT
B-M-2	(1)	Main Coolant Check Valve #316 Internals	VT
B-N-1		Interior of Reactor Vessel	vT
B-N-3		Upper Core Support Barrel	VT
		Lower Core Support Barrel O.D.	VT
		Flow Baffle Assembly, Spacer Blocks, and Source Vanes	TV
		Shroud Tubes from I.D. of Lower Core Support Barrel	VT
		Bolting Upper Core Support Plate to Baffle Assembly	VT
		Shroud Tube Tie-Plate Bolting	VT
		Lower Core Support Barrel I.D.	VT

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ASME Code			
Category	No.	Components Examined	Method
		Core Barrel Lateral Support Pads	VT
		Thermal Shield Surface, Spacer Pins, Seam Clamps, and Support Lugs	VT
8-0		Control Rod Drive Housings	PT
в-р		System Leakage Test Conducted on all Safety Class 1 Systems	VT

	10.	Abstract	of	Examinations	(Safety	Classes	2	and 3	)
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ASME Code			
Category	No.	Components Examined	Method
C-A	(1)	Weld Low Pressure Surge Tank Heat Exchanger	UT
C-B	(1)	Nozzle Low Pressure Surge Tank Heat Exchanger	PE
CC-CE	(2)	Welded Supports #3 Steam Generator	PE
	(1)	Mechanical Support #1 Steam Generator	VT
	(3)	Charging Pump Supports	VT
	(2)	Nonwelded Supports #3 Steam Generator	VT
	(30)	Nonwelded Supports Shutdown Cooling System	VT
	(1)	Welded Support Shutdown Cooling System	PE
	(15)	Nonwelded Supports, Main Steam Line	VT
	(17)	Nonwelded Supports, Feedwater Line	VT
	(1)	Vapor Container Heating, Welded Support	VT
	(1)	Low Pressure Surge Tank SV Discharge Support	TV
C-F	(14)	Shutdown Cooling System Piping Welds	PE
	(11)	Safety Injection System Piping Welds	PE
	(5)	Feedwater System Piping Welds	MT, VT
	(10)	Main Steam System Piping Welds	UT,MT,VT
C-H	(9)	Safety Class 2 System Leakage Tests	VT
	(13)	Safety Class 2 System Hydrostatic Tests	VT
D-A	(5)	Safety Class 3 System Leakage Tests	VT
	(3)	Safety Class 3 System Hydrostatic Tests	VT

#### 11. Abstract of Conditions Noted

B-D Ultrasonic inner radius examination of pressurizer nozzles PRZN-2, 5, and 6 revealed 1 recordable indication on nozzle PRZN-2.

> Ultrasonic examination of RPV outlet nozzle FF (I.D.) revealed 1 reportable indication in the weld region.

- B-F An unacceptable linear indication was identified by visual testing on the pressurizer drain line weld PRZ-SE-2.
- B-G-1 Examination of 52 reactor head studs revealed a degraded condition of two threads on reactor stud #4.
- B-G-2 Inspection of 16 bolts on #2 main coolant pump stator cap identified a break in the plating on 1 bolt.
- B-J Examination of main coolant piping weld MC-1-4 identified an unacceptable linear indication.
- B-K-2 Inspection of main coolant pump support CRM-H-12 identified one bolt/nut having lack of thread engagement.
- B-N-3 Visual inspection of the flow baffle assembly (lower core barrel I.D.) revealed a reportable condition - cracked tack weld.
- CC-CE Visual examination identified a total of 15 supports with discontinuities on the Shutdown Cooling System.

Visual examination identified a total of 4 supports with discontinuities on the main steam line.

Visual examination identified a total of 4 supports with discontinuities on the Feedwater System.

C-F Ultrasonic examination of main steam line welds MS-1-15 and MS-2-11 identified two recordable indications.

Examination of 4 nonnuclear safety main steam line welds identified a nonservice-induced discontinuity (LAP).

## 12. Abstract of Corrective Measures Recommended and Taken

B-D The ultrasonic indication recorded on PRZN-2 was subsequently evaluated in accordance with IWB-3514.5 and determined to be a geometric reflector.

The indication found in RPV outlet nozzle FF was evaluated and determined to be acceptable. The evaluation of this indication is contained in Attachments A and B to this report.

A reinspection will be conducted on nozzle FF during the next refueling to assure no changes have taken place.

- B-F The linear indication identified on weld PRZN-SE-2 was subsequently removed by light buffing and re-examined as satisfactory.
- B-G-1 The two degraded threads on reactor stud #4 were subsequently evaluated by engineering and found to be acceptable for continued service.
- B-G-2 The bolt on #3 main coolant pump stator cap which had a break in the plating was replaced in kind.
- B-J The indication on main coolant piping weld MC-1-4 was subsequently removed by light buffing and re-examined satisfactory.
- B-K-2 The lack of thread engagement condition identified on main coolant pump support CRM-H-12 was subsequently corrected and re-examined as satisfactory.
- B-N-3 The indication identified on the flow baffle assembly was subsequently evaluated and deemed inconsequential to the structure.
- CC-CE The 15 supports on the Shutdown Cooling System identified as having discontinuities were subsequently corrected and re-examined as satisfactory.

The 4 supports on the main steam line identified as having discontinuities were subsequently corrected and re-examined as satisfactory.

The 4 supports on the Feedwater System identified as having discontinuities were subsequently corrected and re-examined as satisfactory.

C-F The ultrasonic indications recorded on main steam line welds MS-1-5 and MS-2-11 were subsequently evaluated in accordance with IWB-3514.5 and determined to be geometric reflectors.

> The discontinuity on #2 nonnuclear safety main steam line weld was subsequently determined to be nonservice-induced and accepted as is.

### 1.0 INTRODUCTION

This report covers the inservice inspection of Yankee Nuclear Power Station during the period of March 31, 1984 to June 9, 1981.

The examinations performed are those of the third period of the second interval.

The required ten-year reactor pressure vessel examinations were performed this refueling. A summary of the examinations performed and conditions noted are included as part of this report along with attachments.

With the exception of several hydrostatic pressure tests, the examinations performed this refueling complete the required inspections for the third period of the second interval.

### 2.0 NONDESTRUCTIVE EXAMINATION PROCEDURES

Nondestructive examinations were performed in accordance with the procedures contained in the Yankce Atomic Electric Company Engineering Guidelines. Book III, "Inservice Inspection NDE Procedures", and Nuclear Energy Services examination procedures.

The examination procedures were reviewed and approved by personnel certified to Level III per SNT-TC-1A, 1975 Edition, and the authorized Nuclear Inservice Inspector.

These procedures conform to the requirements of the ASME Code, Section XI, "Rules for Inservice Inspection of Nuclear Power Plant Components", 1977 Edition, Summer 1978 Addenda.

The following procedures were used during the 1984 inservice inspections:

- 1. YA-PE-2 Rev. 3 "Liquid Penetrant Examination"
- 2. YA-MP-111 Rev. 0 "Procedure for Magnetic Particle Examination"
- 3. YA-VT-11 Rev. 1 "Visual Examination Procedure"
- 4. YA-RT-111 Rev. 0 "Radiographic Examination"
- 5. OP-4200 Rev. 10 "Main Coolant System Leak Inspection"
- 6. YA-UT-1 Rev. 2 "Ultrasonic Examination, General Requirements"
- 7. YA-UT-7 Rev. 2 "Ultrasonic Examination of Bolting"
- 8. YA-UT-8 Rev. 1 "Ultrasonic Examination of Reactor Closure Nuts"
- 9. YA-UT-9 Rev. 2 "Ultrasonic Examination of Piping Ferritic Welds"
- 10. YA-UT-10 Rev. 4 "Ultrasonic Examination of Piping Austenitic Welds"
- 11. YA-UT-13 Rev. 1 "Ultrasonic Examination of Vessel Nozzles Inner Radius"
- 12. YA-UT-14 Rev. 2 "Ultrasonic Examination of Piping Base Metal and HAZ"
- 13. YA-UT-22 Rev. 0 "Ultrasonic Examination of Vessels Circumferential, Longitudinal, Meridional, and Flange Welds"
- 14. YA-UT-44 Rev. 0 "Ultrasonic Examination of Vessels Nozzle to Vessel Welds"
- 15. YA-UT-116 Rev. 0 Ultrasonic Examination of Full Penetration Welds"
- 16. YA-UT-6 Rev. 2 "Ultrasonic Examination of Flange Ligaments"

17.	83A0314	Rev. 0 "Auto Nozz	omated UT Examination for RPV Nozzle Welds from Le Bore"
18.	65 <b>A</b> 0313	Rev. 0 "UT I	Examination of RPV Closure Head to Flame weld"
19.	83A0312	Rev. 0 "UT I from	Examination of RPV Upper Shell to Flange Weld the Flange Mating Surface"
20.	83A0311	Rev. 0 "Open	ration of NES Mini-Scanner System"
21.	83A0317	Rev. 0 "Visu	al Examination Procedure"
22.	83A0318	Rev. 0 "Visu	al Examination Scan Plan"
The	following	technique sheet	was used to perform the subject examination:
Tec	hnique		
She	et No.	Rev.	Subject
YA-	UT-3, TS-1	1	Flange to Vessel Weld From Flange Face

# 3.0 EVALUATION OF DATA

All inservice examinations were performed, evaluated, and reviewed by personnel certified to Level II in accordance with SNT-TC-1A, 1975 Edition and ASME Section XI, 1977 Edition, Summer 1978 Addenda.

The examination methods, volumes, and evaluation of indications were in accordance with ASME Boiler and Pressure Vessel Code, Section XI, 1977 Edition, Summer 1978 Addenda, except for Class 1 piping ultrasonic calibration. This was conducted in accordance with Article III-2000 of Appendix III, ASME Section XI, Summer 1976 Addenda, as required per Plant Technical Specifications.

Summaries of the examinations that were performed are contained in Section 4.0 of this report. The detailed examination data along with the calibration records, procedures, personnel, and equipment certifications are maintained at the plant site.

Attached is a summary of the examination methods, volumes, and the results and evaluation of test data thereof, including any corrective measures taken.

#### 4.0 SUMMARY REPORT

The following is a summary of all the examinations performed, the conditions noted and corrective measures taken during the 1984 inservice inspections, with the exception of the ten-year RPV examination that is included as part of this report.

### CODE CATEGORY B-B PRESSURE RETAINING WELDS IN VESSELS OTHER THAN REACTOR VESSELS

Ultrasonic examination was performed on two welds on steam generator #3. The longitudinal shell to barrel weld SG-3-8 and the longitudinal barrel to transitional piece SG-3-9 were inspected with no recordable indications.

#### CODE CATEGORY B-D FULL PENETRATION WELDS OF NOZZLES IN VESSELS

Ultrasonic examination was performed on 3 pressurizer nozzle welds. Nozzle welds PRZN-2, , and 6 were examined with no recordable indications. A nozzle inner radius examination was also performed on all 3 nozzles. Only one indication was recorded, on nozzle PRZN-2, which was subsequently evaluated and determined to be a geometric reflector in accordance with IWB-3514.5.

Ultrasonic examination was performed on eight (8) RPV outlet and inlet nozzle I.D.s. Outlet nozzle FF revealed one reportable indication. This was subsequently evaluated and determined to be acceptable (see Attachments A and B).

#### CODE CATEGORY B-E PRESSURE RETAINING PARTIAL PENETRATION WELDS IN VESSELS

No. 1 feed and bleed heat exchanger nozzle FB-1-3 was visually examined during the Main Coolant System leakage inspection (OP-4200). No leakage was noted.

#### CODE CATEGORY B-F PRESSURE RETAINING DISSIMILAR METAL WELDS

An ultrasonic and liquid penetrant examination was performed on pressurizer safe end weld PRZ-SE-1. No indications were recorded. During the examination of PRZ-SE-1, a visual inspection of weld PRZ-SE-2 identified two linear indications.

The areas were lightly buffed and re-examined with liquid penetrant which revealed the indications had been removed. A liquid penetrant examination was also performed on the weld adjacent to PRZ-SE-2. This examination resulted in no unacceptable indications.

#### CODE CATEGORY B-G-1 PRESSURE RETAINING BOLTING LARGER THAN 2" IN DIAMETER

Fifty-two (52) reactor head closure studs, nuts, and washers (Set No. L-43) including 2 reduced diameter studs #1-638-1 and #1-674-1 were inspected. A visual examination of the washers and a visual, magnetic particle, and ultrasonic examination of the nuts resulted in no recordable indications.

A visual and ultrasonic examination was performed on all 52 studs. During the visual examination of stud #4, two threads were found to be degraded. An engineering evaluation was conducted which determined that the stud was still acceptable for use. The subsequent ultrasonic examination did not reveal any indications.

## CODE CATEGORY B-G-2 PRESSURE RETAINING BOLTING 2" AND SMALLER IN DIAMETER

A base line visual examination was performed on 16 new bolts and nuts prior to installation on pressurizer safety valves SV-181 and 182. This inspection resulted in no unacceptable indications noted.

A base line visual examination was also conducted on 6 new bolts installed on PR-MOV-191. No unacceptable indications were noted.

The following bolting/studs and nuts were inspected per I&E Bulletin 83-02, "Bolting in RCPB Closure Connections Greater Than Six Inches":

A visual and ultrasonic examination was performed on 20 studs and nuts from #3 main coolant loop check valve #316. No unacceptable indications were noted.

A visual, magnetic particle and ultrasonic examination was performed on 16 bolts removed from #2 main coolant pump stator cap. A linear indication was noted on one bolt which was determined to be a break in the plating. A new bolt was installed in its place, prior to which a visual, magnetic particle, and ultrasonic examination was performed on it, with no unacceptable indications noted.

Twelve (12) pressurizer primary manway studs were visually and ultrasonically inspected with no unacceptable indications noted.

A visual, ultrasonic, and magnetic particle examination was conducted on 40 studs from steam generator #2 primary manways, 38 studs from steam generator #3 primary manways, and 40 studs from steam generator #4 primary manways. These examinations resulted in no unacceptable indications.

#### CODE CATEGORY B-H VESSEL SUPPORTS

Feed and bleed heat exchanger integrally welded supports BL-H-6, 8, and 10 were liquid penetrant inspected with no unacceptable indications noted.

#### CODE CATEGORY B-J PRESSURE RETAINING WELDS IN PIPING

The following Main Coolant System piping welds were inspected as follows:

Weld No.

MC-1-10	Liquid penetrant examination performed - no unacceptable indications noted.
MC-1-13	Ultrasonic and liquid penetrant examination performed - no unacceptable indications noted.
MC-1-16	Liquid penetrant examination performed - no unacceptable

Weld No.	
MC-1-17	Liquid penetrant examination performed - no unacceptable indications noted.
MC-1-15	Liquid penetrant examination performed - no unacceptable indications noted.
MC-2-15	Liquid penetrant examination performed - no unacceptable indications noted.
MC-2-10	Liquid penetrant examination performed - no unacceptable indications noted.
MCB-2-5	Liquid penetrant and ultrasonic examination performed - no unacceptable indications noted.
MCB-4BR-2	Liquid penetrant and ultrasonic examination performed - no unacceptable indicatiors noted.
MC-1-4	Liquid penetrant examination was performed which identified several unacceptable linear indications. The areas were subsequently buffed and re-examined which verified the indications had been removed. An additional weld was examined in accordance with IWB-2430, which identified no unacceptable indications.
MC-2-3	Liquid penetrant examination performed - no unacceptable indications noted.
Safety Valve 182 Weld	Ultrasonic and liquid penetrant base line examination performed - no unacceptable indications noted.
PRS-206-23	Liquid penetrant base line examination - no unacceptable indications noted.
PRS-206-26	Liquid penetrant base line examination - no unacceptable indications noted.
PRS-206-29	Liquid penetrant examination - no unacceptable indications noted.
PRS-206-39	Visual and liquid penetrant examination - no unacceptable indications noted.
PRS-43	Liquid penetrant examination - no unacceptable indications noted.
PRS-52	Liquid penetrant examination - no unacceptable indications noted.
PRS-50	Liquid penetrant examination - no unacceptable indications noted.

# Weld No.

PRS-206-24A	Liquid penetrant base line examination - no unacceptable indications noted.
PRS-206-24B	Liquid penetrant base line examination - no unacceptable indications noted.
PRS-206-22A	Liquid penetrant base line examination - no unacceptable indications noted.
PRS-206-22B	Liquid penetrant base line examination - no unacceptable indications noted.
PRS-206-40	Liquid penetrant examination - no unacceptable indications noted.

Pressurizer safety valve discharge header weld caps #1 and #2 - liquid penetrant examination - no unacceptable indications noted.

#### SAFETY INJECTION PIPING INSPECTIONS

# Weld No.

SI-3-7	Ultrasonic and liquid penetrant examination performed - no unacceptable indications noted.
SI-3-7A	Ultrasonic and liquid penetrant examination performed - no unacceptable indications noted.
SI-3-8	Ultrasonic and liquid penetrant examination performed - no unacceptable indications noted.
SI-4-1	Ultrasonic and liquid penetrant examination performed - no unacceptable indications noted.
SI-147	Liquid penetrant examination performed - no unacceptable indications noted.
SI-153	Ultrasonic examination performed - no unacceptable indication: noted.
SI-156	Ultrasonic examination performed - no unacceptable indications noted.
SI-137	Liquid penetrant examination performed - no unacceptable indications noted.

CODE CATEGORY B-K-1 SUPPORT MEMBERS FOR PIPING, PUMPS, AND VALVES

A liquid penetrant examination was performed on 3 main coolant pump integrally welded supports, CRM-H-5, CRM-H-12, and CRM-H-26. No unacceptable indications were identified.

A visual examination (VT-3 and VT-4) was performed on the following component supports:

MCB1-H-1	CRM-H-26
CRM-H-5	SDC-H-1
CRM-H-12	BL-H-1

Only one discontinuity was noted. CRM-H-12 was rejected due to a nonserviceinduced condition (lack of thread engagement), which was subsequently corrected and re-examined as satisfactory.

#### CODE CATEGORY B-M-2 PUMP CASINGS AND VALVE BODIES

Main Coolant System loop #3, check valve 316, was disassembled and a visual inspection was performed on the internals. This resulted in no unacceptable indications.

#### CODE CATEGORY B-P ALL PRESSURE RETAINING COMPONENTS

A system hydrostatic pressure test was conducted on all repaired/replaced sections of the Main Coolant System prior to startup.

Plant Procedure OP-4200, Rev. 10, "Main Coolan' System Leak Inspection or ISI Pressure Test", was performed at 2040 psi at 514°F for two hours. The areas inspected were uninsulated. The visual inspection (VT-2) was acceptable.

In conjunction with the above test, the remaining portions of the Reactor Coolant System was subjected to the required system leakage tests.

No serious degradation was noted during the inspection other than normal packing leaks which were corrected at the time of the inspection.

#### SAFETY CLASS 2 COMPONENTS

#### PRESSURE RETAINING WELDS IN PRESSURE VESSELS CODE CATEGORY C-A

An ultrasonic examination was performed on the low pressure surge tank heat exchanger head circumferential weld (LPST-Hx-H-1). No recordable indications were observed.

#### CODE CATEGORY C-B PRESSURE RETAINING NOZZLE WELDS IN VESSELS

The low pressure surge tank heat exchanger nozzles to shell welds #1 and #2 (LPST-Hx-N1 and 2) were subjected to a liquid penetrant examination. No unacceptable indications were recorded.

An ultrasonic inner radius examination was attempted on #3 steam generator main steam outlet nozzle SG-3-SO1. Due to physical limitations of the component, no relevant data could be obtained, therefore the examination was deleted.

### CODE CATEGORY CC-CE

Due to access limitations, a "best effort" liquid penetrant examination was performed on #3 steam generator integrally welded supports (SG-3-E and SG-3-W). No unacceptable indications were identified.

Mechanical support SG-1-236 was functionally tested (VT-4) after removal from steam generator #1. Functional acceptability was verified as satisfactory.

Component supports for charging pumps P-15-1, 2, and 3 and steam generator #3 supports SG-3-SE and SG-3-SW were subjected to a visual examination (VT-3) and found to be acceptable.

The following Shutdown Cooling System support members were subjected to visual examinations with results as follows:

Support No.

- CRT-H-66 Subjected to a VT-3/VT-4 visual examination. VT-3 identified a nonservice-related discontinuity (lack of thread engagement) which was subsequently corrected and re-examined as satisfactory.
- CRT-H-59 Subjected to a VT-3/VT-4 visual examination. VT-3 identified a nonservice-related discontinuity (lack of thread engagement) which was subsequently corrected and re-examined as satisfactory. VT-4 identified an incorrect support setting. This was evaluated by Engineering and found to be acceptable as is. An additional examination was performed per IWC-2430 and found acceptable.
- SDC-H-1 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- PRCL-H-43 Subjected to a VT-3/VT-4 visual examination. VT-3 identified an unacceptable condition (loose nuts). This condition was corrected and re-examined as satisfactory. An additional examination was performed per IWC-2430 and found to be acceptable.
- PRCL-H-53 Subjected to a VT-3/VT-4 visual examination. VT-3 identified a nonservice-induced unacceptable condition (lack of thread engagement). This condition was corrected and subsequently re-examined and found to be acceptable.
- CRT-H-71 Subjected to a VT-3/VT-4 visual examination and found to be acceptable.
- CRT-H-62 Subjected to a VT-3/VT-4 visual examination. VT-3 identified a nonservice-induced unacceptable condition (lack of thread engagement) which was subsequently corrected and re-examined as satisfactory.

#### Support No.

- PRCL-H-54 Subjected to a VT-3/VT-4 visual examination. This was an additional examination as required by IWC-2430(a). This examination resulted in an unacceptable VT-3/VT-4 condition. In accordance with IWC-2430(b) the remaining number of supports within the system were subjected to applicable VT-3/VT-4 examinations with results as follow:
  - PRCL-H-60 Subjected to VT-3/VT-4 examination. VT-3 identified an unacceptable condition (missing bolt). Subsequently corrected and re-examined as satisfactory.
  - PRCL-H-57 Subjected to VT-3/VT-4 examination. VT-3 identified an unacceptable condition (loose nuts). VT-4 identified incorrect support settings. Both conditions were subsequently corrected and reinspected as satisfactory.
  - PRCL-H-58 Subjected to a VT-3/VT-4 visual examination. VT-4 identified an incorrect support setting which was subsequently corrected and re-examined as satisfactory.
  - PRCL-H-61 ¬ Subjected to a VT-3/VT-4 visual examination. VT-3 identified a nonservice related unacceptable condition (lack of thread engagement) which was subsequently corrected and re-examined as satisfactory.
  - PRCL-S-55 Subjected to a VT-3 visual examination and found acceptable.
  - PRCL-H-51 Subjected to a VT-3/VT-4 visual examination and found acceptable.
  - PRCL-H-44 Subjected to a VT-3/VT-4 visual examination. VT-3 identified an unacceptable nonservice-induced condition (lack of thread engagement). VT-4 identified an incorrect support setting. Both items were subsequently corrected and reinspected as satisfactory.
  - PRCL-H-64 Subjected to a VT-3/VT-4 visual examination and found acceptable.
  - PRCL-S-51 Subjected to a VT-3 visual examination and found acceptable.
  - PRCL-S-51B/S-52 Subjected to a VT-3 visual examination which identified an unacceptable condition (loose nuts). Subsequently corrected and re-examined as satisfactory.

## Support No.

- CRT-H-65 Subjected to a VT-3/VT-4 visual examination. VT-3 identified an unacceptable nonservice-induced condition (lack of thread engagement) which was subsequently corrected and re-examined as satisfactory.
- CRT-H-67 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- C°T-H-68 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- CRT-H-69 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- CRT-H-70 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- PRCL-H-40 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- PRCL-H-42 Subjected to a VT-3/VT-4 visual examination. VT-3 identified an unacceptable condition (loose bracket) which was subsequently corrected and re-examined as satisfactory.
- PRCL-H-45 Subjected to a VT-3/VT-4 visual examination. VT-4 identified an incorrect support setting which was subsequently corrected and re-examined as satisfactory.
- PRCL-H-52 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- PRCL-H-56 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- PRCL-H-63 Subjected to a VT-3/VT-4 visual examination. VT-4 identified an unacceptable support setting which could not be adjusted. A new support was replaced in kind. A base line VT-3/VT-4 was conducted and found acceptable.
- PRCL-S-51A- Subjected to a VT-3 visual examination and found acceptable.
- PRCL-H-41 Subjected to a VT-3/VT-4 visual examination. VT-4 identified an incorrect support setting which was subsequently corrected and re-examined as satisfactory.

A reinspection will be conducted on selected supports on the Shutdown Cooling System next refueling to assure no excessive movement has occurred. The following main steam line supports were visually examined as follows:

Support Nc.

- SHP-H-83 Subjected to a VT-3/VT-4 visual examination and found to be acceptable.
- SHP-H-81 Subjected to a VT-3/VT-4 visual examination and found to be acceptable.
- SHP-H-91 Subjected to a VT-3/VT-4 visual examination. VT-3 identified an unacceptable condition (loose bolts) which was subsequently corrected and re-examined as satisfactory. In accordance with ASME IWC-2430 an additional examination was conducted and found to be acceptable.
- SHP-H-3 Subjected to a VT-3/VT-4 visual examination. VT-3 identified an unacceptable condition (lack of thread engagement) which was determined not to be inservice-induced. This condition was corrected and subsequently re-examined as satisfactory.
- SHP-H-65 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- SHP-H-74 Subjected to a VT-3/VT-4 visual examination. VT-3 identified a nonservice-induced unacceptable condition (lack of thread engagement) which was subsequently corrected and re-examined as satisfactory.
- SHP-H-71 Subjected to a VT-3/VT-4 visual examination. VT-3 identified a nonservice-induced unacceptable condition (loose bolt) which was subsequently corrected and re-examined as satisfactory.
- SHP-RH-3 Subjected to a VT-3 visual examination and found acceptable.
- SHP-H-66 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- SHP-H-92 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- SHP-H-91R Subjected to a VT-3 visual examination and found acceptable.
- SHP-H-81R Subjected to a VT-3 visual examination and found acceptable.

SHP-H-65R Subjected to a VT-3 visual examination which identified an unacceptable nonservice-induced condition (lack of thread engagement). Subsequently corrected and re-examined as satisfactory.

SHP-H-71RSubjected to a VT-3 visual examination and found acceptable.SHP-H-75Subjected to a VT-3 visual examination and found acceptable.

The following Feedwater System supports were visually examined as follows: Support No.

WCBD-H-12 Subjected to a VT-3 visual examination and found acceptable.

- Subjected to a VT-3/VT-4 visual examination. VT-3 identified WCBD-H-139 an unacceptable condition (loose nuts) which was subsequently corrected and re-examined as satisfactory. In accordance with IWC-2430, an additional examination was conducted and found acceptable.
- WCBD-H-130-1 Subjected to a VT-3 visual examination and found acceptable.

WCBD-H-3 Subjected to a VT-3/VT-4 visual examination and found acceptable.

- Subjected to a VT-3/VT-4 visual examination. VT-3 identified WCBD-H-138 a nonservice-induced unacceptable condition (improper support installment) which was subsequently corrected and re-examined as satisfactory.
- WCBD-RH-131 Subjected to a VT-3 visual examination and found acceptable.
- WCBD-RH-122 Subjected to a VT-3 visual examination and found acceptable.
- Subjected to a VT-3 visual examination and found acceptable. WCBD-RH-119
- WCBD-H-114 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- WCBD-H-6 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- WCBD-RH-117 Subjected to a VT-3 visual examination which identified an unacceptable condition (loose nuts) which was subsequently corrected and re-examined as satisfactory. An additional examination was performed in accordance with IWC-2430 and found to be acceptable.
- WCBD-H-8 Subjected to a VT-3/VT-4 visual examination and found acceptable.
- WCBD-H-126 Subjected to a VT-3 visual examination. VT-3 examination identified a nonservice induced unacceptable condition (lack of thread engagement) which was subsequently corrected and reinspected satisfactory.

WCBD-H-129 Subjected to a VT-3 visual examination and found acceptable.

WCBD-H-134-1 Subjected to a VT-3 visual examination and found acceptable.

Subjected to a VT-3 visual examination and found acceptable. WCBD-H-134-4

WCPD-H-120-4 Subjected to a VT-3 visual examination and found acceptable. OTHER CC-CE SUPPORTS

VC Heating A 1.	Subjected to a VT-1 visual examination and found acceptable.
Penetration #4-6" BRL (EDCR 83-10)	Subjected to a base line VT-3 visual examination and found acceptable.
CODE CATEGORY C-F	PRESSURE RETAINING WELDS IN PIPING

CODE CATEGORY C-F PRESSURE RETAINING WELDS IN PIPING

The following Shutdown Cooling System piping welds were subject to liquid penetrant examination with no unacceptable indications noted:

SDC-L-15	SDC-4-6
SDC-3-16	SDC-4-21
SDC-3-19	SDC-4-24
SDC-3-22	SDC-4-27
SDC-3-25	SDC-3L-21
SDC-3L-26	SDC-4-39
STREETS OF STREETS	SDC-3L-22

The following Safety Injection System piping welds were liquid penetrant examined with no unacceptable indications noted:

SI-003	SI-093
SI-006	SI-096
SI-009	SI-117
SI-018	SI-120
SI-019	SI-126
SI-027	

Pressurizer piping weld FR-2-26 was liquid penetrant examined with no unacceptable indic tions noted.

The following Freedwater System piping welds were subjected to magnetic particle examination with no unacceptable indications noted:

FW-4-15	FW-4-18
FW-4-17	94-8D

No. 3 feedwater nozzle to pipe weld (MT and VT).

#### MAIN STEAM SYSTEM PIPING WELDS

- MS-4-20 Subjected to a ultrasonic, magnetic particle, and visual examination with no unacceptable indications noted.
- MS-1-15 Subjected to an ultrasonic, magnetic particle, and visual examination. One indication was recorded during the ultrasonic examination which was subsequently evaluated as a geometric reflector.

MS-2-6 Subjected to an ultrasonic, magnetic particle, and visual examination - no indications noted.

- MS-2-7 Subjected to an ultrasonic, magnetic particle, and visual examination no indications noted.
- MS-2-11 Subjected to an ultrasonic, magnetic particle, and visual examination. One indication was recorded during the ultrasonic examination which was subsequently plotted and evaluated as being a geometric reflector in accordance with IWB-3514.5.
- MS-2-12 Subjected to an ultrasonic, magnetic particle, and visual examination no indications noted.

In accordance with the Integrated Safety Assessment Systematic Evaluation Program for Yankee Nuclear Power Station - NUREG 0825 (3-5.6). The first weld downstream of the non-return valves (all four loops) was magnetic particle and visually exemined.

Only one indication was noted. During the magnetic particle examination of loop #2, a lap-like indication was revealed. Subsequently, an area of the indication was blended out to verify in fact it was a processing-related discontinuity. This indication was evaluated and determined to be nons vice-induced and accepted as is.

### CODE CATEGORY C-H ALL PRESSURE RETAINING COMPONENTS

The following systems were subjected to system leakage tests:

- 1. Safety Injection System
- 2. Low Pressure Surge Tank Cooling
- 3. Shutdown Cooling
- 4. Service Water System
- 5. Vapor Container Heating System
- 6. Main Coolant Drain System
- 7. Charging and Volume Control System
- 8. Purification System
- 9. Chemical Shutdown System

No serious degradation or leakage was noted other than packing leaks which were subsequently corrected.

The following system hydrostatic tests were conducted after modification or repair to safety class systems. Testing was performed in accordance with IWA/IWC-5000; no serious degradation or leakage was identified:

System	Test <u>Pressure</u>	Duration	Procedure
Main Coulant Vent System	2200 psi	10 min	OP-2000.136
Low Pressure Safety Injection Header	787 psi	10 min	OF-2000.130
Charging and Volume Control	52 psi	10 min	OP-2000.130
Vapor Container Drain Header	190 pii	10 min	OP-2000.112.4
Pressure Control and Relief System	300 psi	10 min	OP-2000.123
Feedwater System	1214 psi	10 min	OP-2000.126
Bleed Line	3000 psi	10 min	OP-2000.127
Post Accident Hydrogen Vent System	102 psi	10 min	OP-2000.128/129
Valve Stem Leakoff	375 psi	10 min	OP-2000.132
Low Pressure Surge Tank	94 psi	10 min	OP-2000.134
Main Steam System	1035 psi	10 min	OP-2000.135
EBFP Steam Inlet	1170 psi	10 min	OP-2000.137

An Appendix "J" test was conducted on modifications to the low pressure surge tank safety value discharge header. The test was conducted at 32 psi. Reference plant Procedure OP-2000.133. The test was conducted and found acceptable.

# SAFETY CLASS 3

# CODE CATEGORY D-A PRESSURE RETAINING COMPONENTS

Portions of the following systems were subjected to either inservice or system leakage tests and found acceptable:

- 1. Emergency Boiler Feedwater System
- 2. Main Coolant Vent System
- 3. Spent Fuel Pit Cooling
- 4. Primary Pump Seal Water
- 5. Service Water

System hydrostatic tests were conducted on the following systems after repair or modification and found acceptable:

	System	Pressure	Duration	Procedure
1.	Emergency Boiler Feed Pump Steam Inlet	1 188 psi	10 min	OP-2000.137
2.	Primary Pump Seal Water	345/414 psi	15 min	OP-2000.124
3.	Demineralized Water/Service Water Crosstie	165 psi	10 min	OP-2000.125

### ADDITIONAL EXAMINATIONS

4

In addition to the code-required examinations, the following inspections were conducted:

A visual examination was performed on the reactor head underside to monitor the known flaws. This inspection revealed that no change has occurred.

A visual inspection was also performed on the cladding of #3 steam generator hot leg and cold leg. The visual inspection resulted in no unacceptable indications noted.

The pressurizer internals were subjected to a visual inspection. This inspection concluded that no change has occurred since the last visual inspection.

### 5.0 SAFETY VALVE TESTING

The following safety valves were subjected to testing and found to be acceptable:

- SV-215A Low Pressure Surge Tank Safety
- SV-409A Main Steam Safety
- SV-409B Main Steam Safety
- SV-409C Main Steam Safety
- SV-409D Main Steam Safety
- SV-409E Main Steam Safety
- SV-409F Main Steam Safety
- SV-409G Main Steam Safety
- SV-409H Main Steam Safety
- SV-4091 Main Steam Safety
- SV-409L Main Steam Safety
- PRSV-181 Pressure Code Safety Relief Valve
- PRSV-182 Pressure Code Safety Relief Valve replaced this refueling. During plant operation, valve setpoint was found to be out of tolerance. See LER 84-11.

# 6.0 CONCLUSIONS

With the exception of several hydrostatic pressure tests (which will be completed within this second interval), the examinations performed during this outage complete the inservice inspection requirements of the Yankee Nuclear Station Technical Specifications for the third period of the second interval.

	Procedure No. S3A0314
	Subject: RPS LIZZIES
	Page 64 of 253
	Plant/Unit VANKER FRANE
	Cal. Data Pkg. () 3/4-1
EVALUATION SH	HEET FOR RECORDABLE INDICATIONS
	Supplement C
A. Zone number NIA	Evaluation Proc. No. 80A5535
B. Baster No. FEIPOTIA	Weld number RPV-FF-1
C. Indication number $\frac{R_2}{2}$	
D. Applicable ASME Code Star	ndards used for evaluation:
Section XI SUMMER 1	978 Article 1005 3000
E. Size of indication:	
Length SEE BELOW	Depth 1,48 TO CLOSESI POINT
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u>	Depth 1,48 TO CLOSEST POINT Plate thickness (t) 9.75" Norm
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw	Depth 1,48 TO CLOSEST POINT Plate thickness (t) 9.75" Norm Indication per Fara. 1417-3320
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUE</u>	Depth 1.48 TO CLOSEST POINT Plate thickness (t) 9.75" Norm Indication per Fara. 1407-3320 FACE PLANAR
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication:	Depth 1.48 TO CLOSEL POINT Plate thickness (t) 9.75" Nom Indication per Fara. 14A-3320 FACE PLANAR
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CURC DEPTH of C5 )	Depth 1.48 TO CLOSEL POINT Plate thickness (t) 9.75" $nom$ Indication per Fara. 14/A-3320 FACE PLANAR AX CARRENTON FORTOR 14.51 X.57 = 8.27 AX CARENTON FORTOR 2274 X C = 1.84
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C5 y CIRC DEPTH of C1 x	Depth 1.48 TO CLOSELI MINI Plate thickness (t) 9.75" $nom$ Indication per Para. 14A-3320 FACE PLANAR AX CARRENTON FORTOR 14.51 X.57 = 8.27 AX CARRENTON FORTON 2.27 X.81 = 1.84 1.112
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C5 S CIRC DEPTH of C1 X <u>6.43</u> = 1.2''/SD	Depth 1.48 TO CLOSELI MINI Plate thickness (t) 9.75" $nom$ Indication per Para. 14/A-3320 FACE PLANAR * Ax CARRENTON FACTOR 14.51 X.57 = 8.27 Ax CARRENTON FACTOR 2.27 X.81 = 1.84 6.43
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C5 S CIRC DEPTH of C1 X <u>6.43</u> 5:3550 = 1.2''/SD	Depth 1.48 TO CLOSELI MINI Plate thickness (t) 9.75" $nom$ Indication per Fara. 14/A-3320 FACE PLANAR * Ax CARRENTON FACTOR 14.51 X.57 = 8.27 Ax CARRENTON FACTOR 2.27 X.81 = 1.84 6.43
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C5 S CIRC DEPTH of C1 X <u>6.43</u> 5:3550 = 1.2''/SD	Depth 1.48 TO CLOSELI POINT Plate thickness (t) 9.75" $nom$ Indication per Para. 14/A-3320 FACE PLANAR × Ax CARRENTON FACTOR 14.51 X.57 = 8.27 Ax CARRENTON FACTOR 2.27 X.81 = 1.84 6.43
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C5 $\gamma$ CIRC DEPTH of C1 $\chi$ <u>6.43</u> " = 1.2"/SD 3. Flaw characterization	Depth 1.48 TO CLOSELI POINT Plate thickness (t) 9.75" $nom$ Indication per Fara. 14/A-3320 FACE PLANAR × Ax CARRENTION FACTOR 14.51 x.57 = 8.27 Ax CARRENTION FACTOR 2.27 x.81 = 1.84 6.43
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C5 S CIRC DEPTH of C1 X <u>6.43</u> " = $1.2''/SD$ 3. Flaw characteristic ca Q = 1.2A SD - $.6X, T$	Depth 1.48 TO CLOSELI POINT Plate thickness (t) 9.75" $nom$ Indication per Fara. 1407-3320 FACE PLANAR * Ax CARRENTON FACTOR 14.51 x.57 = 8.27 Ax CARRENTON FACTOR 2.27 x.81 = 1.84 6.43 alculations: = .42 ·
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C1 x <u>6.43</u> " = $1.2''/SD$ 3. Flaw characteristic ca Q = 1.2A SD = .6x.7	Depth 1.48 TO CLOSEST POINT Plate thickness (t) 9.75" rom Indication per Fara. 1407-3320 FACE PLANAR * Ax CARRENTON FORTOR 14.51 x.57 = 8.27 Ax CARRENTON FORTON 2.27 x.81 = 1.84 6.43 alculations: = .42 $\frac{\alpha}{\lambda} = .11 \frac{\alpha}{\lambda} = 4.3\frac{7}{6}$
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C5 , CIRC DEPTH of C1 x <u>6.43</u> " = $1.2''/SD$ 3. Flaw characteristic ca Q = 1.2A SD = .6x.7 $Z = 20.28° \chi E(1.38)^2 + 1$	Depth 1.48 TO CLOSEL POINT Plate thickness (t) 9.75" MM Indication per Fara. 1407-3320 FACE PLARAR * Ax CARRENTON FACTOR 14.51 X.57 = 8.27 Ax CARRENTON FACTOR 2.27 X.81 = 1.84 E.43 alculations: = .42 $a_{\pm} = .11$ $a_{\pm} = 4.3\%$ 14.27 = 3.9"
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C5 > CIRC DEPTH of C1 × <u>6.43</u> " = $1.2''/SD$ 3. Flaw characteristic ca Q = 1.2A SD = .6x.7 $L = 20.28^{\circ} \times \overline{C(1.42)^{2}} + C$ G. Comparison of pertinent of	Depth 1.48 TO CLOSEL 1011 Plate thickness (t) 9.75" $nom$ Indication per Para. 1407-3320 FACE PLANAR AX CARRENTON FACTOR 14.51 X.57 = 8.27 AX CARRENTON FACTOR 2.27 X.81 = 1.84 6.43 alculations: =.42 $q = q = 4.3 \frac{7}{6}$ 19.12 $n = 3.9$ " Evaluation standard (Para. 146. 350.1)
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C5 > CIRC DEPTH of C1 × $6.43^{"} = 1.2^{"}/SD$ 3. Flaw characteristic ca q = 1.2A SD = .6x.7 $L = 20.28^{\circ} \times E(1.8)^{2} + 1$ G. Comparison of pertinent to to actual flaw size. ALLO	Depth 1.48 TO CLOSEST POINT Plate thickness (t) 9.75" ADM Indication per Fara. 1407-3320 FACE PLANAR * Ax CORRECTION FORTON 14.51 X.57 = 8.27 Ax CORRECTION FORTON 2.27 X.81 = 1.84 E.43 alculations: = .42 $\frac{4}{2}$ = .11 $\frac{9}{2}$ = 4.3% $\frac{19.12}{2}$ P = 3.9" Evaluation standard (Para. 146. 350.1) ows 2.6% with 90 for 10
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CIRC DEPTH of C.5 x CIRC DEPTH of C.1 x $6.43^{"} = 1.2''/SD$ 3. Flaw characteristic ca Q = 1.2A SD = .6x.7 $L = 20.28^{\circ} \chi E(1.42)^{2} + 1$ G. Comparison of pertinent to to actual flaw size. ALLO	Depth 1.48 TO CLOSELI PONT Plate thickness (t) 9.75" nom Indication per Para. 1407-3320 FACE PLANAR AX CARRENTON FACTOR 14.51 X.57 = 8.27 AX CARRENTON FACTOR 2.27 X.81 = 1.84 6.43 alculations: =.42 $q = q = 4.3\%$ 19.12 $P = 3.9"$ Evaluation standard (Para. 146. 350.1) ows 2.6% with an $\frac{146.350.1}{6.43}$ Description of the formed of the forme
Length <u>SEE BELOW</u> Width <u>SEE BELOW</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: CARC DEPTH of C5 x CARC DEPTH of C1 x $6.43^{"} = 1.2''/SD$ 3. Flaw characteristic ca Q = 1.2A SD = .6x.1 $L = 20.28^{\circ} \chi E(1.4)^{2} + 12$ G. Comparison of pertinent to to actual flaw size. ALLO	Depth 1.48 To CLUSSEL PMUL Plate thickness (t) 9.75" AM Indication per Fara. 14/A - 3320 FACE PLARAR AX CARRENTON FORTON 14.51 X.57 = 8.27 AX CARRENTON FORTON 2.27 X.81 = 1.64 E.43 alculations: =.42 $\frac{4}{2}$ : $\frac{4}{2}$ : $\frac{4}{2}$ : $\frac{4}{3}$ $\frac{1912}{6}$ = 3.9" Evaluation standard (Para. 146 35/2.1) The With 40 A of .10 Mes 2.6% with 40 A of .10
Length <u>SEE Reference</u> Width <u>SEE BELAN</u> F. Characterization of Flaw 1. Type of Flaw: <u>SUBSUR</u> 2. Sketch of indication: $CIRC \ OEPTH \ of CI \times CIRC \ of CIRC $	Depth 1.48 To CLOSEL PART Plate thickness (t) 9.75" ASM Indication per Fara. <u>1404-3320</u> FACE PLANAR AN CAREETTON FORTOR 14.51 X.57 = 8.27 AN CAREETTON FORTON 2.27 X.81 = 1.64 E.43 alculations: =.42 $G = .11 G = 4.3 \%$ E.43 E.43 Evaluation standard (Para. <u>144.350.1</u> ) ows 2.6% with GN & of.10 Depth 1.48 $G = .10$ Reportable SEE ATTRETED SHE Approval ADAM M Joint LUI

and a second

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( Euster No. FFIPCIIH Indication No. R2/3

THIS COULD HAVE BEEN SIZED AS A LAMINAN INDICATION IN ACCORDANCE WITH FIG. I WB 2500-7 (c) AND TABLE I WB -3512-2. THIS WOULD PUT IT WELL WITHIN ACCEPTABLE LIMITS.

THE a WOULD BE REDUCED TO .18 WITH A REALISTIC SIZING ERITERIA USING BEAM SPREAD.

 $\frac{\alpha}{2} = \frac{.18}{3.9} = .05 \qquad \frac{\alpha}{3} = \frac{.18}{9.75} = 1.85\%$ 

THIS WOULD BE ALLOWABLE.

A for at