

#### UNITED STATES NUCLEAR REGULATORY COMMISSION WASHINGTON, D.C. 20655

### SAFETY EVALUATION BY THE OFFICE OF NUCLEAR REACTOR REGULATION

### TEMPORARY EXEMPTION FROM APPENDIX J INTERVAL

#### FOR LOCAL LEAK RATE TESTING OF CONTAINMENT PENETRATIONS

### BROWNS FERRY NUCLEAR PLANT, UNIT 2 DOCKET NO. 50-260

#### 1.0 INTRODUCTION

By letter dated December 20, 1991, the Tennessee Valley Authority, (TVA or the licensee), requested a temporary schedular exemption to extend the interval for Type B and C (local leak rate) testing of certain containment penetrations at the Browns Ferry Nuclear Plant (BFN), Unit 2, beyond the 2-year limit of Appendix J to 10 CFR Part 50.

Appendix J requires these tests to be performed at every refueling outage, but with the interval not to exceed 2 years. Browns Ferry, Unit 2, was in cold shutdown from September, 1984 until May 24, 1991. Type B and C testing began July 30, 1990, in anticipation of a seemingly impending restart. However, the return-to-power sequence took longer than expected, and startup did not occur until May 24, 1991. Leak rate testing was also spread out and was finished in May, 1991, shortly before startup. Since the next refueling outage is scheduled to begin January 29, 1993, the expiration of the 2-year interval for some of the Type B and C tests would force a plant shutdown in July, 1992, because many of the tests cannot be performed at power.

At the time of the restart, the licensee had expected that an extensive mid-cycle outage would be necessary due to problems which usually occur following restart after an extended outage. The licensee planned to conduct Type B and C testing during this expected mid-cycle outage. TVA has since decided that this mid-cycle outage is not necessary. Therefore, the licensee is unable to perform the required testing within required time frames without a shutdown solely for the performance of the testing. The licensee believes a shutdown only to perform the Appendix J testing is unnecessary and expensive in terms of time, money, and radiation exposure. Therefore, the licensee requested a temporary or schedular exemption to extend the test interval for the Type B and C testing for certain components.

Originally, 159 containment boundary components, or approximately 58 percent of the total in the plant, were in need of Type B or C testing before January 29, 1993. However, during two forced outages in October and December, 1991, the licensee was able to perform some of the tests and reduce the number to 121, or approximately 44 percent of the total. This was the number of components for which the licensee requested an exemption in their December 20, 1991, letter. In February 1992, another outage brought the number down to

9206180025 920610 PDR ADOCK 05000260 87 components, or approximately 32 percent. The 87 components (see attached Table 1) include containment isolation valves, expansion bellows, flanges, and valve bonnets/packing. The maximum requested extension of the interval beyond 2 years for any one component is 177 days, or slightly less than 6 months. Sixty-two of the 87 components would be extended no more than 3 months.

Further, the licensee is committed to performing additional Type B and C tests during any forced outages of sufficient duration that may occur before the next refueling outage.

#### 2.0 EVALUATION

The licensee has addressed the following factors to justify the requested exemption.

#### 2.1 Components not testable at power

For the components listed in Table 1, it is either not possible to test with the unit at power, or it is inadvisable to test at power, as discussed below:

- Approximately half of the components cannot be tested without entering the primary containment, which must remain inerted with nitrogen when the unit is operating.
- 2) The 24 expansion bellows are hot (both thermally and radioactively) during unit operation. The high temperature could affect the accuracy of leak rate measurements. The stability of the leak rate data obtained from the testing apparatus could be affected, and the measured leak rate could be different from that which would be obtained under cold conditions, due to expansion/contraction of the test volume. In addition, testing at power would result in significant radiation doses to the testing personnel. For these reasons, testing the bellows at power is inadvisable.
- 3) Eleven components (valves and bonnets/packing) in the HPCI and RCIC systems cannot be tested without entering a Technical Specification Limiting Condition for Operation for the system being tested. In addition, certain Surveillance Instructions must be performed to demonstrate operability before returning the system to service. These constitute avoidable challenges to safety systems. Therefore, testing these components at power is inadvisable.
- 4) For 8 valves in the Residual Heat Removal (RHR) containment spray system and 2 valves in the Pressure Suppression Chamber (PSC) level control line, a system train must be made inoperable to conduct the tests. This degrades safety systems and is inadvisable at power.

- 5) For one bonnet in the High Pressure Coolant Injection (HPCI) turbine exhaust line, 30-ft-high scaffolding must be erected in the HPCI room to allow access to the bonnet for testing, at some hazard to personnel and the HPCI system. The interval extension for this component is only 16 days. This short extension is not significant enough to warrant the scaffolding exercise.
- 6) One flange in the containment ventilation system requires a 3-day interval extension and must have a 20-ft scaffold erected for the iest. This very short extension is insignificant.

#### 2.2 Good leak rate history for components

The licensee has performed a detailed analysis of the past leak rate history of the 87 components in question. Most of these components are historically "good performers," and those few that are not were repaired or replaced during the last extended refueling outage. The licensee has used historical leak rate data to conservatively project the leak rate expected to exist on January 29, 1993, the date to which interval extension is requested. The expected incremental increases in component leakage rates due to the extension are small, less than 18 percent of 0.6 times the maximum allowable leakage rate, La. The quantity 0.6 La is the acceptance criterion set by 10 CFR 50, Appendix J for Type B and C testing. The projected increase in total leakage rate due to the test interval extension reduces the margin between as-left leakage rate and 0.6 La by less than 22 percent. This provides reasonable assurance that the requested test interval extension will not result in the Type B and C leakage rate total exceeding the 0.6 La limit of Appendix J.

#### 2.3 Improvements made to testing program

During the extended outage, numerous actions were taken to upgrade the plant's Appendix J program. The following is a summary of actions taken to upgrade the program:

- Block valves, test connections, and vent valves to enable isolation valves to be tested by flow in the accident direction were added.
- Block valves and test connections were added to simplify testing of bonnet and packing seals.
- Valves were reoriented to allow packing and bonnet seals to be tested during the normal Type C test.
- Lines no longer used were capped to remove potential leak paths.
- Changes in valve type were made to improve leakage characteristics.

Stainless steel overlays were added to ventilation valves to improve leakage characteristics.

Various repairs, replacements, and modifications of historical problem valves to improve leakage performance were conducted during the outage.

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As a result of these upgrades, modifications, and improved maintenance practices, the possibility of significant degradation of containment components is reduced.

# 2.4 Intent of Appendix J

The staff notes that the 2-year interval requirement for Type B and C components is intended to be often enough to prevent significant deterioration from occurring and long enough to permit the tests to be performed during plant outages. Leak rate testing of the penetrations during plant shutdown is preferable because of the lower radiation exposures to plant personnel. Moreover, as noted before, some penetrations cannot be tested at power. For testing at power is inadvisable as discussed above, the increase in confidence to justify a plant shutdown specifically to perform the tests within the above.

## 3.0 CONCLUSION

Based on the above evaluation, the staff finds the requested temporary exemption, to allow the Type B and C test intervals of the 87 components listed in Table 1 to be extended to the refueling outage which will begin no later than January 29, 1993, to be acceptable.

Attachment:

Components Requiring Extension -Table 1

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Date: June 10, 1992

# COMPONENTS REQUIRING EXTENSION

## TYPE & TESTED COMPONENTS

COMPONENT	PENETRATION	DESCRIPTION	EXTENSION Days
			3.2
RELLOWS	X-7A	Inboard Beliows MS Line A	27
BELLOWS	X-7 A	Outboard Bellows MS Line A	10
BELLOWS	X-7B	inboard Bellows MS Line B	10
BEF., LOWS	X-78	Outboard Brilows MS Line B	10
BELLOWS	X.7C	inboard Bellows MS Line C	10
HELLOWS	X-7C	Outboard Bellows MS Line C	10
BELLOWS	X-7D	Inboard Beliows MS Line D	10
BELLOWS	X-7D	Outboard Bellows MS Line D	27
RELLOWS	X - 8	Inboard Bellows MS Drain	27
RELLOWS	X-C	Outboard Bellows MS Drain	111
BELL 1.59WS	X-9A	Inbuard Bellows FW Line A	
BELLOWS	X-9A	Outboard Bellows PW Line A	111
TE LOWS	X-98	Inboard Bellows FW Line B	
/ ALLOWS	X-98	Outboard Bellows FW Line B	111
WOLLOWS	X-10	Inhoard Bellows RCIC Steam	120
HELLOWS	X-10	Outboard Bellows RCIC Steam	120
BELLOWS	X-11	Inboard Bellows HPCI Steam	0
BELLOWS	X-11	Outboard Bellows HPC1 Steem	
HELLOWS	X-12	Inhoard Bellows SDC Suction	4.2
BELLOWS	X-12	Outboard Bellows SDC Suction	4 2 4 2
BELLOWS	X-13A	Inboard Bellows RHR Discharge	
BELLOWS	X-13A	Outboard Bellows RHR Discharge	4.2
BELLOWS	X-13B	Inboard Bellows RHR Discharge	4.2
RELLOWS	X-13B	Outboard Bellows RHR Discharge	4.2
FLANCE	N/A	Shear Lug Access Cover O <sup>e</sup>	1.2
FLANCE	N/A	Shear Lug Access Cover 45"	1.2
FLANCE	N/A	Sear Lug Access Cover 90"	1.5
FLANCE	'/A	Shear Lug Access Cover 135"	13
FLANCE	-/A	Shear Lug Access Cover 270°	12
FLANCE	N/A	Shear Lus Access Cover 315°	12
BONNET/FACKI		2-FCV-71-59/601	9
BONNFT/PACKI	NG X-220	2-FCV-73-64/642	9
BONNET/PACKI	NG 71-32	RCIC Vacuum Pump Discharge	6.4
BONNET PACKI		HPCI Turbine Exhaust Drain	167
BONNET	73-23	HPCI Turbine Exhaust	16
FLANCE	64-19	Containment Ventilation	3

# TABLE 1 (CONTINUED)

# COMPONENTS REQUIRING EXTENSION

### TYPE C TESTED COMPONENTS

COMPONENT	PENETRALION	DESCRIPTION	EXTENSION Pays
2.3.558	X-9A	Reactor Feedwater A	14
2.3.554	X-9A	Reactor Feedwater A	14
2-FCV-73-45	X-9A	HPCI Injection	1.4
2-3-572	X-9B	Reactor Feedwater B	137
2-3-568	X-98	Reactor Feedwater B	137
2-69-579	X-98	RWCU Return	137
2-FCV-71-40	X-98	RCIC Injection	137
2-85-576	X-9B	CRD Return	137
2-63-525	X-42	Standby Liquid Control	175
2-63-526	X-42	Standby Liquid Control	175
2-68-508	X-37C	RCP Seal Water	2.4
2-68-550	X-37C	RCP Seal Water	2.4
2-FCV-69-1	X-14	RWCU Suction	146
2-FCV-69-2	X-14	RWCU Suction	146
2-FCV-70-4%	X-23	RBCCW Return	5.5
2-70-506	X-24	RBCCW Supply	177
2-FCV-71-2/3	X-10	RCIC Sinam Supply	5
2-HCV 73-23/603		HPCI Turbine Exhaust	16
2-FCV-74-47	X-12	RHR Shuidown Cooling	91
2-FCV-74-48	X-12	RHR Shutdown Cooling	91
2-74-661/662	X-12	RHR Shutdown Cooling	91
2-FCV-77-2A	X-18	Drywell Floor Drain Sump	6.0
2-FCV-77-2B	X-18	Drywell Floor Drain Sump	60
2-FCV-77-15A	X-19	Drywell Equipment Drsta 2444	60
2-FCV-77-15B	. 19	Drywell Equipment Dry Sum	60
2-HCV-71-32-59	2 X-221	RCIC Vacuum Pump Dischary	6.4
2-HCV-73-24/60		HPCI Turbine Exhaust Drain	167
2 FCV-71-18	X-227A	RCIC Pump Suction	6
	X-13A	RHR Return	87
2-FCV-74-53	X-13A	RHR Return	87
2-FCV-74-54 2-FCV-74-57/58	X-211A	RHR Containment Spray	8.5
2-FCV-74-60	X-39B	RHR Containment Spray	8.8
2-FCV-74-61	X-39B	RHR Containment Spray	1.8
2-FCV-74-67	X-13B	RHR Return	8.9
2-FCV-74-68	X-13B	RHR Return	81
2-FCV-74-71/72	X-211B	RHR Containment Spray	75
2-FCV-74-74	X-39A	RHR Containment Spray	6.9
2.FCV-74-75	X-39A	RHR Containment Spray	89
2-FCV-75-25	X-16A	Core Spray Injection	173
2-PCV-75-26	X-16A	Core Spray Injection	173
2-FCV-75-53	X-16A	Core Spray Injection	172
2-FCV-75-54	X-16B	Core Spray Injection	157
2-FCV-75-57/58	X-108 X-227 A	PSC Level Control	147
2-LP 4-12-21128	A-641A	1.50 Perci Perci	