

QUAD-CITIES NUCLEAR POWER STATION

UNITS 1 AND 2

MONTHLY PERFORMANCE REPORT

AUGUST 1984

COMMONWEALTH EDISON COMPANY

AND

IOWA-ILLINOIS GAS & ELECTRIC COMPANY

NRC DOCKET NOS. 50-254 AND 50-265

LICENSE NOS. DPR-29 AND DPR-30

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I. INTRODUCTION

Quad-Cities Nuclear Power Station is composed of two Boiling Water Reactors, each with a Maximum Dependable Capacity of 769 MWe Net, located in Cordova, Illinois. The Station is jointly owned by Commonwealth Edison Company and Iowa-Illinois Gas & Electric Company. The Nuclear Steam Supply Systems are General Electric Company Boiling Water Reactors. The Architect/Engineer was Sargent & Lundy, Incorporated, and the primary construction contractor was United Engineers & Constructors. The Mississippi River is the condenser cooling water source. The plant is subject to license numbers DPR-29 and DPR-30, issued October 1, 1971, and March 21, 1972, respectively; pursuant to Docket Numbers 50-254 and 50-265. The date of initial Reactor criticalities for Units One and Two, respectively were October 18, 1971, and April 26, 1972. Commercial generation of power began on February 18, 1973 for Unit One and March 10, 1973 for Unit Two.

This report was compiled by Becky Brown and Dave Kimler, telephone number 309-654-2241, extensions 127 and 192.

II. SUMMARY OF OPERATING EXPERIENCE

A. Unit One

August 1-17: Unit One began the month shutdown for End of Cycle Seven Refueling and Maintenance. On August 16, at 0940 hours, the unit was critical and on August 17, at 1900 hours, the unit was on line.

August 18-31: On August 25, at 0726 hours, the unit scrambled on high APRM flux caused by a pressure spike that was generated by the rapid opening and closing of a Turbine Bypass Valve. On August 26, at 1914 hours, the unit was critical and on August 27, at 0503 hours, the unit was on line. On August 28, at 1352 hours, the unit scrambled on Main Steam Line High Flow caused by an Instrument Mechanic's failure to fill the reference leg of the transmitter. At 2139 hours the unit was critical and on August 29, at 0314 hours, the unit was on line.

B. Unit Two

August 1-6: Unit Two began the month operating at full power. On August 4, at 2105 hours, load was dropped to 400 MWe to perform MSIV quarterly testing. On August 5, at 1044 hours, the unit scrambled due to a one-half scram from loss of the 2B RPS MG Set coupled with a one-half scram from the partial closure of two MSIV's. On August 6, at 0204 hours, the unit was critical and at 0852 hours, the unit was on line.

August 7-19: On August 12, at 2300 hours, load was dropped to 700 MWe for weekly Turbine tests. At 0715 hours the unit began a normal load increase to full power. On August 19, at 0135 hours, load was dropped to 700 MWe for weekly Turbine tests. At 0700 hours the unit began a normal load increase to full power.

August 20-31: On August 24, at 0045 hours, load was dropped to 700 MWe for Reactor Feed Pump changeover. At 0155 hours, the unit began a normal load increase to full power. On August 26, at 0225 hours, load was dropped to 700 MWe to perform weekly Turbine tests. At 0800 hours, the unit began a normal load increase to full power.

III. PLANT OR PROCEDURE CHANGES, TESTS, EXPERIMENTS, AND SAFETY RELATED MAINTENANCE

A. Amendments to Facility License or Technical Specifications

On June 6, 1984, the NRC issued Amendment 88 to License DPR-29 and Amendment 83 to License DPR-30. These Amendments establish time delays on Trip Level Settings for initiation of Primary Containment Isolation by means of High RCIC Steamline Flow and High HPCI Steamline Flow. A time delay of greater than or equal to 3 seconds, but less than or equal to 10 seconds was implemented. These Amendments also establish changes to the Minimum Test and Calibration Frequency Tables pertinent to these Core Cooling Systems including a verification of the time delay setting.

On August 8, 1984, the NRC issued Amendment 90 to License DPR-29. This Amendment establishes the implementation of Analog Trip Systems in the Reactor Low Water Level, Reactor Water Level, HPCI High Steam Flow and HPCI Steamline Low Pressure Instrumentation. It also establishes the installation of level switches and related instrumentation in the Scram Discharge Volumes. This includes changes to the pertinent Reactor Protection System Instrumentation Requirements, Logic Systems Functional Tests, and Minimum Calibration Frequencies Tables.

B. Facility or Procedure Changes Requiring NRC Approval

There were no Facility or Procedure changes requiring NRC approval for the reporting period.

C. Tests and Experiments Requiring NRC Approval

There were no Tests or Experiments requiring NRC approval for the reporting period.

D. Corrective Maintenance of Safety Related Equipment

The following represents a tabular summary of the major safety related maintenance performed on Unit One and Unit Two during the reporting period. This summary includes the following headings: Work Request Numbers, LER Numbers, Components, Cause of Malfunctions, Results and Effects on Safe Operation, and Action Taken to Prevent Repetition.

UNIT ONE MAINTENANCE SUMMARY

W. R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q35034	84-2	Outboard 'B' Feedwater Check Valve	Valve leaks; not seating properly.	Reference LER 84-2.	Cleaned the seat and tested satisfactorily.
Q35135	84-7	RHR Service Water Vault Penetrations	Leak; pipe vibration.	The leakage encountered was small enough that the vault sump pump could easily handle the flow in the unlikely event of condensate pit flooding.	The penetrations were repaired for startup.
Q36392	84-2	Valve A0 1- 2001-4	Leak; improperly adjusted stroke.	The in-line valve, A0 1-2001-3, would have performed PCI function. Reference LER 84-2.	Adjusted stroke.
Q36585		1/2 Diesel Generator Voltage Pegged High	Terminal connection on the 'A' phase of the power transformer burned. See DVR 84-43.	The results of this deviation were minimized because two off-site lines and the Unit 1 and Unit 2 Diesel Generators were available.	The terminals were relocated to a larger box to prevent over- heating on all three Diesel Generators.
Q28421		RHR Service Water Pump Discharge Check Valve 'A'	Improper seating of the valve disc.	If backflow through the pump was detected, the pump could have been isolated with the 1- 1001-3A valve.	The Check Valve was replaced.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
W28423		RHR Service Water Pump Discharge Check Valve 'C'	Improper seating of the valve disc.	If backflow through the pump was detected, the pump could have been isolated with the 1-1001-3C valve.	The Check Valve was replaced.
Q31467		HPCI Testable Check Valve (Disassemble & Rebuild)	Disc would "hang- up" during testing.	This line could be isolated remotely using valves M0 1- 2301-9 or M0 1-2301-8.	Rebuilt valve, lapped seats and relocated hinge pin bearing inserts.
Q3196		Replace Cables to Standby Liquid Control Squib Valves	Cracked insulation on cables to SBLC Squib Valves.	Both Squib Valves maintained continuity, therefore, the safety consequences of this occurrence were minimal.	Replaced cables with cracked insulation.
Q32927	84-2	Valve M0 1- 220-1	Leaks; improper seating of valve disc.	Reference LER 84-2.	Valve was cleaned and leakage was reduced to an acceptable value for startup.
Q33174	84-2	2D MSIV	Leaks; improper seating of the valve plug.	The other in-line MSIV would have limited the leakage to an acceptable value. Reference LER 84-2.	Valve was rebuilt and leakage through this valve was reduced to an acceptable value for startup.
Q33176	84-2	1C MSIV	Leaks; improper seating of the valve plug.	Reference LER 84-2.	Valve was rebuilt and leakage was reduced to an acceptable value for startup.

UNIT ONE MAINTENANCE SUMMARY

W. R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q33178	84-2	1B MSIV	Leaks; improper seating of the valve plug.	Reference LER 84-2.	Valve was rebuilt and leakage was reduced to an acceptable value for startup.
Q33183	84-2	M0 1-220-2	Leaks; improper seating of valve disc.	Reference LER 84-2.	Valve was rebuilt and leakage was reduced to an acceptable value for startup.
Q36594	84-2	2C MSIV	Leaks; improper seating of valve plug.	Reference LER 84-2.	Valve leakage was reduced to an acceptable value for startup.
Q36674		Unit 1/2 250 Volt Battery Charger (trips when turned on; install new Silicone Controlled Rectifiers and Diodes)	Battery charger would not give correct output.	The consequences of this occurrence were minimized because Unit 1 was shutdown. The Unit 2 battery charger was cross-tied to Unit 1. The 1/2 battery charger was returned to service within 72 hours.	Installed new silicone controlled rectifiers and diodes; adjusted charger for correct output.
Q36690	84-12	1/2 'B' Standby Gas Treatment Heater - replace control transformer & rewire.	Incorrectly placed jumpers caused secondary side of control transformer to be grounded.	Reference LER 84-12.	Rewired and replaced control transformer. Performed a Drawing Change Request so drawings would reflect more accurately what existed at the heater.

UNIT ONE MAINTENANCE SUMMARY

W. R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q36767		1-1601-33C Vacuum Breaker	Leaks; dirt and sand in seating surface.	No effects on safe operation. Leak was found during testing. Test (QOS 1600-5) was successfully conducted the next day.	Seat was cleaned. Test was performed again on the following day.
Q36833		Relay 590-102D of MSIV IC - Does not "pick-up" During Testing	An out of adjustment lever arm on 2B switch.	Defect was found during testing. No effect on safe operation. Test was successfully performed later on the same day. Unit 1 was shutdown.	Adjusted lever arm on 2B switch and MSIV scram functional was performed.
Q29142		1B RHR Service Water Pump Casing - Replace	Cavitation.	Pump still performed its intended function.	Replaced pump casing.
Q32777		HPCI Oil Sump - Investigate & repair--overflowing and is white & milky.	Water infiltration from gasket between tube and shell of heat exchanger.	The unit was shutdown for refuel and HPCI was not required to be operable.	Replaced gasket.
Q32815	84-13	1-203-3E Electromatic Relief Valve Failed to Open During Manual Actuation	Coil failure from excessive vibration.	The other Electromatic Relief Valves would have provided an adequate flowpath.	Rebuilt actuator.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q33365	84-21	Perform IHSI on Specified Welds on Reactor Recirculation and RHR Piping	Believed to be IGSCC induced indications.	Welds treated with IHSI were not 100% through-wall. Reference LER 84-21.	All welds, except three, had IHSI performed on them, as per NUTECH, Inc. Engineers.
Q36130	84-2	A0 1-2001-16	Stroke was out of adjustment causing valve to fail LLRT.	Reference LER 84-2.	The leakage was brought to an acceptable value prior to startup.
Q36629	84-2	A0 1-203-2B (MSIV)	Improper seating of valve disc caused valve to fail LLRT.	Reference LER 84-2.	Leakage was reduced to an acceptable value prior to startup.
Q36892		1A RHR Pump Seal	Leaks; seal faces worn.	Unit was shutdown & leakage was minimal.	Replaced mechanical seal.
Q36982		Valve M0 1-2301-48 - Motor Mount is Broken	Motor mount for valve M0 1-2301-48 was found to be broken.	Unit 1 was coming up from refueling and HPCI was not needed.	Installed new motor.

UNIT TWO MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q36691	84-12	1/2 'A' Standby Gas Treatment Train Heater	Poor drawings caused improper placement of a temporary jumper.	The SGBT Trains were repaired within the required 36 hours. Reference LER 84-12.	Replaced control transformer and changed prints to reflect what actually exists.
Q36743	84-9	DC Solenoids on the Outboard 'A' & 'B' MSIV's (2-203-2A & 2B)	Air solenoid valves had failed DC coils.	The coils failed in a safe direction. When the 'B' RPS bus failed, these valves went shut causing a Reactor scram. Reference LER 84-9.	The faulty coils were replaced and all MSIV DC solenoids were tested.
Q36870		Valve MO 2- 1001-29A (rewire)	An undetected mistake was found in the anti-hammer circuit when a new EQ operator (without brakes) was installed.	The valve did not fail, it just had the potential for hammering. Reference Unit 1 LER 84-14.	The valve was rewired correctly.
Q36871		Valve MO 2- 1001-29B (rewire)	An undetected mistake was found in the anti-hammer circuit when a new EQ operator (without brakes) was installed.	The valve did not fail, it just had the potential for hammering. Reference Unit 1 LER 84-14.	The valve was rewired correctly.
Q36981		MO 2-2301-10 Will Not Close	Motor pinion gear on Limiter torque operator had loose set screw which allowed key to fall out.	Unusual Event (GSEP) was declared due to RCIC being inoperable and there was a delay in testing & PCI due to this valve. Reference DVR 4-2-84-46.	Shaft and keyway were drilled with an in- dentation to lock key on shaft.

UNIT TWO MAINTENANCE SUMMARY

W. R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q30933		595-112B (PCI Group I Relay)	Relay was stuck in de-energized position.	Relay failed in the safe direction by giving a 1/2- isolation signal. Relay for the other channel prevented a full isolation.	Replaced the relay.

IV. LICENSEE EVENT REPORTS

The following is a tabular summary of all licensee event reports for Quad-Cities Units One and Two occurring during the reporting period, pursuant to the reportable occurrence reporting requirements as set forth in sections 6.6.B.1. and 6.6.B.2. of the Technical Specifications.

<u>Licensee Event Report Number</u>	<u>Date</u>	<u>Title of Occurrence</u>
84-12	8-2-84	Standby Gas Treatment System 'A' and 'B' Trains Inoperable
84-13	8-8-84	ECCS Signal From Improper Backfilling of Instrument Lines
84-14	8-8-84	MO 1-1001-29A and 29B Failure
84-15	8-25-84	Reactor scram -- APRM Hi Flux Due to Pressure Spike
84-16	8-28-84	Reactor scram -- Main Steamline Hi Flow
84-17	8-17-84	South SJAE Valves Incorrectly Installed
<u>UNIT TWO</u>		
84-9	8-5-84	Reactor scram -- 2B Reactor Protection System MG Set Trip

V. DATA TABULATIONS

The following data tabulations are presented in this report:

- A. Operating Data Report
- B. Average Daily Unit Power Level
- C. Unit Shutdowns and Power Reductions

OPERATING DATA REPORT

DOCKET NO. 50-254

UNIT ONE

DATE Sept. 12

COMPLETED BY DAVE KIMLER

TELEPHONE 309-654-2241X192

OPERATING STATUS

0090 00104

1. Reporting period: 2400 063.84 Gross hours in reporting period: 744

2. Currently authorized power level (MWt): 2511 Max. Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted (if any) (MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr. to Date	Cumulative
5. Number of hours reactor was critical	<u>330.8</u>	<u>1892.9</u>	<u>85448.5</u>
6. Reactor reserve shutdown hours	<u>0.0</u>	<u>0.0</u>	<u>3421.9</u>
7. Hours generator on line	<u>282.0</u>	<u>1843.2</u>	<u>82191.1</u>
8. Unit reserve shutdown hours.	<u>0.0</u>	<u>0.0</u>	<u>909.2</u>
9. Gross thermal energy generated (MWH)	<u>436851</u>	<u>4096583</u>	<u>169203289</u>
10. Gross electrical energy generated (MWH)	<u>147522</u>	<u>1360670</u>	<u>54619286</u>
11. Net electrical energy generated (MWH)	<u>136965</u>	<u>1281172</u>	<u>50887139</u>
12. Reactor service factor	<u>44.5</u>	<u>32.3</u>	<u>79.2</u>
13. Reactor availability factor	<u>44.5</u>	<u>32.3</u>	<u>82.4</u>
14. Unit service factor	<u>37.9</u>	<u>31.5</u>	<u>76.2</u>
15. Unit availability factor	<u>37.9</u>	<u>31.5</u>	<u>77.0</u>
16. Unit capacity factor (Using MDC)	<u>23.9</u>	<u>28.5</u>	<u>61.3</u>
17. Unit capacity factor (Using Des. MWe)	<u>23.3</u>	<u>27.7</u>	<u>59.8</u>
18. Unit forced outage rate	<u>13.4</u>	<u>2.3</u>	<u>5.2</u>
19. Shutdowns scheduled over next 6 months (Type, Date, and Duration of each):			
20. If shutdown at end of report period, estimated date of startup			<u>NA</u>

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

*UNOFFICIAL COMPANY NUMBERS ARE USED IN THIS REPORT

OPERATING DATA REPORT

DOCKET NO. 50-265

UNIT TWO

DATE Sept. 12

COMPLETED BY DAVE KIMLER

TELEPHONE 309-J54-2241X192

OPERATING STATUS

0000 080184

1. Reporting period: 2400 083184 Gross hours in reporting period: 744

2. Currently authorized power level (MWt): 2511 Max. Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted (if any) (MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr. to Date	Cumulative
5. Number of hours reactor was critical	<u>728.7</u>	<u>4293.8</u>	<u>82211.3</u>
6. Reactor reserve shutdown hours	<u>0.0</u>	<u>0.0</u>	<u>2985.8</u>
7. Hours generator on line	<u>721.9</u>	<u>4176.9</u>	<u>79386.6</u>
8. Unit reserve shutdown hours.	<u>0.0</u>	<u>0.0</u>	<u>702.9</u>
9. Gross thermal energy generated (MWH)	<u>1749867</u>	<u>9849890</u>	<u>165231978</u>
10. Gross electrical energy generated (MWH)	<u>554982</u>	<u>3174072</u>	<u>52609852</u>
11. Net electrical energy generated (MWH)	<u>528825</u>	<u>3023454</u>	<u>49357514</u>
12. Reactor service factor	<u>97.9</u>	<u>73.3</u>	<u>76.8</u>
13. Reactor availability factor	<u>97.9</u>	<u>73.3</u>	<u>79.6</u>
14. Unit service factor	<u>97.0</u>	<u>71.3</u>	<u>74.2</u>
15. Unit availability factor	<u>97.0</u>	<u>71.3</u>	<u>74.9</u>
16. Unit capacity factor (Using MDC)	<u>92.4</u>	<u>67.2</u>	<u>60.0</u>
17. Unit capacity factor (Using Des. MWe)	<u>90.1</u>	<u>65.4</u>	<u>58.5</u>
18. Unit forced outage rate	<u>2.1</u>	<u>3.8</u>	<u>8.4</u>

19. Shutdowns scheduled over next 6 months (Type, Date, and Duration of each):

20. If shutdown at end of report period, estimated date of startup NA

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-254

UNIT ONE

DATE Sept. 12

COMPLETED BY DAVE KIMLER

TELEPHONE 309-654-2241X192

MONTH August 1984

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

1.	<u>-7.4</u>
2.	<u>-8.0</u>
3.	<u>-8.3</u>
4.	<u>-7.7</u>
5.	<u>-8.7</u>
6.	<u>-10.0</u>
7.	<u>-11.7</u>
8.	<u>-11.6</u>
9.	<u>-11.0</u>
10.	<u>-10.0</u>
11.	<u>-10.1</u>
12.	<u>-10.2</u>
13.	<u>-10.0</u>
14.	<u>-9.5</u>
15.	<u>-9.3</u>
16.	<u>-13.1</u>

17.	<u>-18.8</u>
18.	<u>74.7</u>
19.	<u>274.3</u>
20.	<u>413.3</u>
21.	<u>533.0</u>
22.	<u>617.5</u>
23.	<u>695.1</u>
24.	<u>608.3</u>
25.	<u>170.7</u>
26.	<u>-12.8</u>
27.	<u>279.5</u>
28.	<u>260.7</u>
29.	<u>432.3</u>
30.	<u>647.2</u>
31.	<u>726.8</u>

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly.

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-265

UNIT TWO

DATE Sept. 12

COMPLETED BY DAVE KIMLER

TELEPHONE 309-654-2241X192

MONTH August 1984

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

1. 761.3
2. 759.8
3. 756.7
4. 738.0
5. 158.1
6. 256.1
7. 594.8
8. 716.5
9. 746.5
10. 752.1
11. 752.3
12. 724.8
13. 746.3
14. 755.5
15. 758.7
16. 759.5

17. 756.8
18. 766.3
19. 730.9
20. 751.9
21. 762.5
22. 756.2
23. 768.6
24. 755.6
25. 762.3
26. 736.0
27. 767.9
28. 780.0
29. 755.0
30. 760.0
31. 768.4

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt. These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly.

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 050-254UNIT NAME Quad-Cities Unit OneCOMPLETED BY D. KimlerDATE September 4, 1984REPORT MONTH AUGUST 1984TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
84-15	840824	S	0.0	B	5		CH	VALVEX	Reduced load to 600 MWe for Heater Control Valve Adjustment.
84-16	840825	F	35.2	A	3	84-15	HE	VALVEX	Reactor scram - Turbine Bypass Valve opened and shut rapidly causing pressure spike and Hi APRM Flux.
84-17	840828	F	7.8	H	3	84-16	CC	INSTRU	Reactor scram - Instrument Mechanic failed to fill reference leg of flow transmitter on Main Steam Line.

APPROVED
AUG 16 1982

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 050-265UNIT NAME Quad-Cities Unit TwoCOMPLETED BY D. KimlerDATE September 4, 1984REPORT MONTH AUGUST 1984TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
84-29	840804	S	0.0	B	5		CD	VALVEX	Reduced load to 400 MWe to perform Main Steam Isolation Valve Quarterly Tests.
84-30	840805	F	15.3	A	3	84-9	CD	VALVEX	Reactor scram due to 2B Reactor Protection System MG Set trip and MSIV closure.
84-31	840812	S	0.0	B	5		HA	TURBIN	Reduced load to perform weekly Turbine tests.
84-32	840819	S	0.0	B	5		HA	TURBIN	Reduced load to perform weekly Turbine tests.
84-33	840824	S	0.0	H	5		CH	PUMPXX	Reduced load to changeover Reactor Feed Pump
84-34	840826	S	0.0	B	5		HA	TURBIN	Reduced load to perform weekly Turbine tests.

APPROVED

AUG 16 1982

VI. UNIQUE REPORTING REQUIREMENTS

The following items are included in this report based on prior commitments to the commission:

A. Main Steam Relief Valve Operations

Relief valve operations during the reporting period are summarized in the following table. The table includes information as to which relief valve was actuated, how it was actuated, and the circumstances resulting in its actuation.

<u>Unit</u>	<u>Date</u>	<u>Valves Actuated</u>	<u>No. & Type Actuations</u>	<u>Plant Conditions</u>	<u>Description of Events</u>
1	8-17-84	1-203-3A	1 Manual	Rx Press	Surveillance Technical
		1-203-3B	1 Manual	940	Specification 4.5.D.1.b
		1-203-3C	1 Manual		(Post Maintenance)
		1-203-3D	1 Manual		(Replaced Pilot Valves)
		1-203-3E	1 Manual		

VI. UNIQUE REPORTING REQUIREMENTS

(continued)

B. Control Rod Drive Scram Timing Data for Units One and Two

The basis for reporting this data to the Nuclear Regulatory Commission are specified in the surveillance requirements of Technical Specifications 4.3.C.1 and 4.3.C.2.

The following table is a complete summary of Units One and Two Control Rod Drive Scram Timing for the reporting period. All scram timing was performed with Reactor pressure greater than 800 psig.

RESULTS OF SCRAM TIMING MEASUREMENTS

PERFORMED ON UNIT 1 & 2 CONTROL

ROD DRIVES, FROM 1-1 TO 12-31-84

DATE	NUMBER OF RODS	AVERAGE TIME IN SECONDS AT % INSERTED FROM FULLY WITHDRAWN				Max. Time For 90% Insertion	DESCRIPTION
		5	20	50	90		
		0.375	0.900	2.00	3.5	7 sec.	Technical Specification 3.3.C.1 & 3.3.C.2 (Average Scram Insertion Time)
8-19	177	0.28	0.67	1.45	2.55	3.39 (P-5)	Unit 1 Hot Scram Timing - A & B Sequence

VII. REFUELING INFORMATION

The following information about future reloads at Quad-Cities Station was requested in a January 26, 1978, licensing memorandum (78-24) from D. E. O'Brien to C. Reed, et al., titled "Dresden, Quad-Cities, and Zion Station--NRC Request for Refueling Information", dated January 18, 1978.

QUAD-CITIES REFUELING
INFORMATION REQUEST

QTP 300-S32
Revision 1
March 1978

- *
1. Unit: Q1 Reload: 7 Cycle: 8
2. Scheduled date for next refueling shutdown: 11-11-85
3. Scheduled date for restart following refueling: 1-20-86
4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:
NOT AS YET DETERMINED.
5. Scheduled date(s) for submitting proposed licensing action and supporting information:
SEPTEMBER 13, 1985, IF LICENSING ACTION REQUIRED.
6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
NONE PLANNED AT PRESENT TIME.
7. The number of fuel assemblies.
- a. Number of assemblies in core: 724
- b. Number of assemblies in spent fuel pool: 2062
8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:
- a. Licensed storage capacity for spent fuel: 3657
- b. Planned increase in licensed storage: 0
9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

APPROVED

APR 20 1978

Q. C. O. S. R.

QUAD-CITIES REFUELING
INFORMATION REQUEST

QTP 300-S32
Revision 1
March 1978

- *
1. Unit: Q2 Reload: 7 Cycle: 8
2. Scheduled date for next refueling shutdown: 3-18-85
3. Scheduled date for restart following refueling: 5-26-85
4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:
Not as yet determined.
5. Scheduled date(s) for submitting proposed licensing action and supporting information:
January 18, 1985, if licensing action required.
6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
1) All new fuel assemblies will be GE7B-type (barrier clad, extended exposure design).
2) A generic methodology was used for the analysis of the Control Rod Drop Accident and Rod Withdrawal Error events.
7. The number of fuel assemblies.
a. Number of assemblies in core: 724
b. Number of assemblies in spent fuel pool: 278
8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:
a. Licensed storage capacity for spent fuel: 3897
b. Planned increase in licensed storage: 0
9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

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APR 20 1978

Q. C. O. S. R.

VIII. GLOSSARY

The following abbreviations which may have been used in the Monthly Report, are defined below:

ACAD/CAM	-	Atmospheric Containment Atmospheric Dilution/Containment Atmospheric Monitoring
ANSI	-	American National Standards Institute
APRM	-	Average Power Range Monitor
ATWS	-	Anticipated Transient Without Scram
BWR	-	Boiling Water Reactor
CRD	-	Control Rod Drive
EHC	-	Electro-Hydraulic Control System
EOF	-	Emergency Operations Facility
GSEP	-	Generating Stations Emergency Plan
HEPA	-	High-Efficiency Particulate Filter
HPCI	-	High Pressure Coolant Injection System
HRSS	-	High Radiation Sampling System
IPCLRT	-	Integrated Primary Containment Leak Rate Test
IRM	-	Intermediate Range Monitor
ISI	-	Inservice Inspection
LER	-	Licensee Event Report
LLRT	-	Local Leak Rate Test
LPCI	-	Low Pressure Coolant Injection Mode of RHRS
LPRM	-	Local Power Range Monitor
MAPLHGR	-	Maximum Average Planar Linear Heat Generation Rate
MCPR	-	Minimum Critical Power Ratio
MFLCPR	-	Maximum Fraction Limiting Critical Power Ratio
MPC	-	Maximum Permissible Concentration
MSIV	-	Main Steam Isolation Valve
NIOSH	-	National Institute for Occupational Safety and Health
PCI	-	Primary Containment Isolation
PCOMR	-	Preconditioning Interim Operating Management Recommendations
RBCCW	-	Reactor Building Closed Cooling Water System
RBM	-	Rod Block Monitor
RCIC	-	Reactor Core Isolation Cooling System
RHRS	-	Residual Heat Removal System
RPS	-	Reactor Protection System
RWM	-	Rod Worth Minimizer
SBGTS	-	Standby Gas Treatment System
SBLC	-	Standby Liquid Control
SDC	-	Shutdown Cooling Mode of RHRS
SDV	-	Scram Discharge Volume
SRM	-	Source Range Monitor
TBCCW	-	Turbine Building Closed Cooling Water System
TIP	-	Traversing Incore Probe
TSC	-	Technical Support Center



Commonwealth Edison

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NJK-84-260

September 4, 1984

Director, Office of Inspection & Enforcement
United States Nuclear Regulatory Commission
Washington, D. C. 20555
Attention: Document Control Desk

Gentlemen:

Enclosed for your information is the Monthly Performance Report covering the operation of Quad-Cities Nuclear Power Station, Units One and Two, during the month of August 1984.

Very truly yours,

COMMONWEALTH EDISON COMPANY
QUAD-CITIES NUCLEAR POWER STATION

N. J. Kalivianakis
Station Superintendent

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Enclosure

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