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ICSP-LP-FP-1

International Agreement Report

TRAC-PF1 Code Assessment Using OECD LOFT LP-FP-1 Experiment

Prepared by
F. J. Barbero

Centro de Investigaciones Energeticas
Medioambientales y Tecnologicas
Consejo de Seguridad Nuclear
Madrid, Spain

Office of Nuclear Regulatory Research
U.S. Nuclear Regulatory Commission
Washington, DC 20555

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Prepared as part of
The Agreement on Research Participation and Technical Exchange
under the International Thermal-Hydraulic Code Assessment
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ABSTRACT

Document resumes the final calculations of the thermal-hydraulic aspects of the OECD LOFT-LP-FP-1 experiment, with emphasis in those related with the assessment of the TRAC-PF1 code.

LOFT LP-FP-1 experiment was carried out at the LOFT facility in INEL, sponsored by the OECD.

Code used for this simulation was TRAC-PF1/Mod 1 (version 11.0) running on a CDC Cyber 830 (O.S. NOS-BE).

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FOREWORD

This report represents one of the assessment/application calculations submitted in fulfilment of the bilateral agreement for cooperation in thermalhydraulic activities between the Consejo de Seguridad Nuclear of Spain (CSN) and the United States Nuclear Regulatory Commission (US-NRC) in the form of Spanish contribution to the International Code Assessment and Applications Program (ICAP) of the US-NRC whose main purpose is the validation of the TRAC and RELAP system codes.

The Consejo de Seguridad Nuclear has promoted a coordinated Spanish Nuclear Industry effort (ICAP-SPAIN) aiming to satisfy the requirements of this agreement and to improve the quality of the technical support groups at the Spanish Utilities, Spanish Research Establishments, Regulatory Staff and Engineering Companies, for safety purposes.

This ICAP-SPAIN national program includes agreements between CSN and each of the following organizations:

- Unidad Eléctrica (UNESA)
- Unión Iberoamericana de Tecnología Eléctrica (UITESA)
- Empresa Nacional del Uranio (ENUSA)
- Centro de Investigaciones Energéticas y Medioambientales (CIEMAT)
- TECNATOM
- LOFT-ESPAÑA

The program is executed by 12 working groups and a generic code review group and is coordinated by the "Comité de Coordinación". This committee has approved the distribution of this document for ICAP purposes.

1. INTRODUCTION

The fission products release test LP-FP-1 was conducted on Dec 19, 1984. The first trial to conduct the test on Dec 12 had failed because of a defect in the position indicator of the hot leg QOBV (Quick Opening Blowdown Valve). The test was terminated by the PPS (Plant Protection System) action at about 10 s and the transient ended at 50 s. This test is designated as LP-FP-1A.

The thermal-hydraulic transient of the test LP-FP-1 has been initiated by the reactor scram and opening of the QOBV's with one second delay. This experiment simulates large break LOCA in the cold leg with delayed ECC injection to allow pin rupture and fission products release.

LP-FP-1 was specified to be similar to LOFT experiment L2-5 and OECD LOFT experiments LP-02-6 and LP-LB-1, except for initial primary pump operation, closure of the BLCL valve and ECCS operation for core recovery and fuel cladding quench.

From the thermal-hydraulic point of view, the following objectives were considered achievable:

- Determine system thermal-hydraulics and core thermal response for initial and boundary conditions similar to a large break design basis LOCA leading to and limited to fission product release from the fuel cladding gap region.
- Determine the fission product retention effectiveness of the ECCS operating in a mode representative of a German

PWR ECCS in nominal (best estimate) conditions for combined hot leg and cold leg injection.

During the conduct of FP-1, most of the water in the accumulator B line was unintentionally injected into the upper plenum during the blowdown. This water distorted the thermal behaviour of the core and delayed the burst of the pressurized fuel pins by more than 200 s. Also more than 60 % of the rods that were planned to burst, remained intact. The thermal-hydraulic conditions in the core at the time of fission product release are far less definite than was expected. In order to be able to analyse the test results and to carry out post-test calculations using advanced thermal hydraulic codes, one has to know the amount and the rate of water injected.

We have selected a history for this unexpected injection, based on previous studies. We have run a simulation of 400 s, covering blowdown, heat-up and reflood phases in order to compare the obtained results with the data measured along the experiment, both hydraulic and thermal variables.

A brief description of the LOFT facility, system configuration for LP-FP-1 experiment and test evolution are included in Section 2, together with initial conditions and operational set points.

Section 3 contains the input model for TRAC-PF1 code and nodalization details.

In Section 4, results obtained are checked against the measured data for a set of important parameters showing main physical phenomena that occurred during the experiment.

Run statistics in different regions of the transient are shown in Section 5.

Conclusions and recommendations arising from the study are resumed in Section 6.

Appendix A resumes the instrumentation nomenclature and location for the LOFT system, related with the assessment.

2. FACILITY AND TEST DESCRIPTION

2.1 System configuration

The LOFT facility was designed to simulate the major components and system responses of a commercial PWR during a LOCA. The experimental assembly includes five major subsystems which have been instrumented in such a way that the system variables can be measured and recorded during a LOCA simulation. The subsystems include:

- Reactor vessel
- Intact loop
- Broken loop
- Blowdown suppression tank (BST)
- ECC system

Complete information on the LOFT system is provided in ref [1].

The arrangement of the major LOFT components is shown in Figs 2.1 and 2.2. The intact loop simulates three loops of a commercial four-loop PWR and contains a steam generator, two primary coolant pumps in parallel, a pressurizer, a venturi flowmeter and connecting piping.

The broken loop consists of a hot and a cold legs, each of which are connected to the reactor vessel and the BST header. Primary coolant pump and steam generator simulators were installed in the broken loop hot leg to provide the flow resistance normally represented by these components in a

commercial PWR. Each broken leg contains a quick-opening blowdown valve, a recirculation line, an isolation valve, an orifice to represent the break plane, and connecting piping. The recirculation lines establish a small flow through the broken loop to maintain hot fluid conditions in these loops which otherwise are stagnant prior to initiation of the experiment.

The LOFT reactor vessel, shown in Figure 2.3 has an annular downcomer, a lower plenum, lower core support plates, a nuclear core and an upper plenum. The downcomer is connected to the cold legs of the intact and broken loops and the upper plenum is connected to the hot legs.

The core consists of 1300 enriched uranium fuel rods arranged in five square and four triangular fuel assemblies. The fuel rods were designed to commercial PWR specifications except that they are only 1.68 m long and several fuel rods have special instrumentation. Twenty-four fuel rods were enriched to 6 % (wt) U235, and twenty-two of these were pre-pressurized at cold conditions to 2.41 MPa. The other two fuel rods were unpressurized and were designed to be easily removed for PIE. All other fuel rods in the core were unpressurized and enriched to 4 % (wt) U235. Fig 2.4 shows the fuel cladding thermocouple locations and Fig 2.5 shows all the central fuel assembly instrumentation, as well as the locations of the two fuel rods which were removed for PIE. Fig 2.6 shows the location for the thermocouples in the upper plenum. Nomenclature and location of the instruments may be seen in Appendix A.

The ECCS in FP-1 was designed to simulate the hot leg and cold leg ECC injection rates representative of the ECCS operation in a KWU 1300 Mwe reference PWR under nominal conditions. As mentioned, injection have to be delayed to allow fuel rupture and fission product release and transport in a vapour environment. Accumulator A was rooted to the intact loop cold leg (Fig 2.2) and was used to inject ECC scaled to the reference PWR best estimate cold leg accumulators and LPIS injection based on power scaling (1:100).

Accumulator B was rooted to the upper plenum (Fig 2.2) near the top of the center fuel assembly through a special piping configuration convenient to the LOFT system and not related to the reference PWR. Accumulator B was designed to inject ECC scaled to the reference PWR.

As the injection line enters the pressure vessel, it penetrates through the central fuel module and branches in the upper structure (see Fig 2.7). At station 203.17 (3.44 m) above reactor vessel bottom and about 42 cm above the top of fuel pins, 6 reflood injection nozzles are positioned to inject inside the flow shroud in the central fuel module. At station 191.82 (about 13 cm above the top of fuel pins) another 8 reflood nozzles are positioned in such a way as to inject outside the flow shroud and towards the peripheral elements. Details may be found in reference [2].

Accumulator B is connected to the pressure vessel by three lines. Injection in the hot leg, in downcomer or in the upper plenum can be activated. Direct injection in the downcomer is

only activated in case of PPS as happened in LP-FP-1A. The same lines are also used by the low pressure injection system (LPIS). See design of the injection line in Fig 2.8.

The upper plenum injection valve CV-P120-54 which is very near to the pressure vessel was then opened about 90 s before the test while the far valve CV-P120-33 was kept close. This means that the whole line between that valve and the nozzles in the upper plenum was subjected to the system pressure of 14.77 MPa during a period of 90 s before the test.

No accumulator blowdown and no venting of the primary system were performed after the failed experiment and no precautions were taken to prevent nitrogen injection. The injection line of accumulator B included large amount of nitrogen before system pressurization in the transient phase of FP-1. This nitrogen was then compressed to system pressure during the 90 s after opening CV-P120-54 and the gas bubble was moved towards the accumulator B, behind the flowmeter FE-P120-33.

The LOFT steam generator, located in the intact loop, is a vertical U-tube-design steam generator. Operation of the secondary coolant system approximates that of a commercial PWR.

2.2 Test description

LP-FP-1 was defined to consist of four distinct phases which were designated as: fuel preconditioning, pretransient, transient and postransient. The four phases were continuous and had specific beginning and ending definitions.

The purpose of the fuel preconditioning phase, in conjunction with the pretransient phase, was to subject the 24.6% (wt) enriched fuel rods in the new center assembly to the minimum required burnup condition of 1175 MWD/MTU prior to conducting the transient. This burnup is equivalent to power operation at a maximum linear heat generation rate of 52.2 Kw/m for 20 days on the enriched fuel rods. The preconditioning phase started at the beginning of plant heatup prior to power operation and ended with termination of power operation after the calculated burnup fraction had been achieved. An additional period of preconditioning beyond that required for minimum burnup occurred after the first attempt of conducting the experiment. The delay of one week resulted in three more days of power operation, reaching 1417 MWD/MTU.

The pretransient phase consisted of a reactor shutdown interval of approximately five days, followed by a power operation interval. The final plant preparations were completed during the reactor shutdown interval. The power operation interval established the required minimum decay heat level (86% of DH in commercial PWR fuel rods after one year of at 52 Kw/m), and the initial conditions for conducting the experiment. The requirement to build up the short lived

fission product inventory of 40 Equivalent Fission Product Hours was achieved by 70 %. The pretransient phase started at the termination of power operation in the preconditioning phase and ended with initiation of the transient by a reactor scram.

The transient phase of the experiment started with reactor scram, followed by the opening of the QOBV's and ended at the initiation of the closure of the broken loop hot leg (BLHL) QOBV. The BLHL-QOBV was closed at 68 s to ensure that positive core vapour flow existed for the transport of fission products, released from the fuel rod gap, along the intended path for fission product measurements. The unplanned injection of water in the upper plenum due to the expansion of non-condensable gases in the injection line from accumulator B have caused a delay in pin rupture, core reflood and system recovery, which commenced at 344 s instead of the expected value of 100 s on a peak cladding temperature trip of 1037 K in the peripheral fuel assemblies was accomplished with cold leg and upper plenum accumulator ECC injection. The maximum cladding temperature measured in the central fuel assembly was 1210 K.

The final (postransient) phase consisted of a 12 h time from the closure of the BLHL-QOBV, for measuring the redistribution of fission product inventory in gas and liquid in the BST and PCS.

The initial conditions are specified in Table 2.1 together with the measured system conditions immediately prior to the

transient phase of LP-FP-1. The operational setpoints specified are listed in Table 3 together with the measured values. Differences between specified and operational setpoints reflect in some cases the time elapsed between operator action and system response.

As shown in Table 2.2, the break apertures was taken as the initiation time of the experiment. The reactor was scrammed one second prior to the initiation of blowdown. This was done for avoiding early departure from nucleate boiling (DNB) on the 6 % fuel rods which would lead to excessive cladding temperatures early in the transient. The blowdown was the initiated by opening the QOBVs and the pumps were turned off and decoupled from their flywheels within 1 s.

The PCS quickly depressurized to saturation pressure in the upper plenum, broken hot and cold legs by 0.1, 1.1 and 3.5 s, respectively. A bottom-up partial core quench occurred between 6 and 7 s, followed at 12 to 18 s by a total top-down quench of the central fuel assembly. The lower part of some of the peripheral fuel rods did not completely quench at this time. This total top-down quench was the 1st indication that the upper plenum injection line was leaking. The unplanned injection of water in the upper plenum doesn't influence the pressure history.

The cold leg QOBV was closed by 68 s, forcing all break flow out the cold leg and core flow from bottom to top. A sustained heatup of most (not all) of the core started at 90 s, resulting in the rupture of some of the enriched fuel

rods beginning at 325 s. The ECCS was initiated at 344 s and the entire core was quenched by 365 s. A 12 h postexperiment sampling period followed and the experiment was then terminated with plant cleanup and sample removal for PIE.

TABLE 2.1. Initial conditions for experiment LP-FP-1

	Specified ^(a) Value	Measured Value	
<u>PRIMARY COOLANT SYSTEM</u>			
Core delta T (K)		14.4 ± 0.1	
Primary system pressure (hot leg) (MPa)	14.95 ± 0.1	14.77 ± 0.07 ^(b)	(-1.2 %)
Hot leg temperature (K)	577 ± 1.1	577.6 ± 0.8	
Cold leg temperature (K)		563.2 ± 1.1	
Mass flow intact loop (kg/s)	479 ± 19	486.7 ± 2.5 ^(b)	(+1.6 %)
Boron concentration (ppm)		612 ± 15	
Primary coolant pump injection (both pumps) (L/s)	0.127 ± 0.016	0.126 ± 0.003	
<u>REACTOR VESSEL</u>			
Power level (MW)	38 ± 1	37.0 ± 1.2 ^(b)	(-2.6 %)
Maximum linear heat generation rate (kW/m)	52	51.2 ± 3.6	
Control rod position (above full-in position) (m)	1.37 ± 0.01	1.38 ± 0.002	
<u>STEAM GENERATOR</u>			
Secondary system pressure (MPa) .		6.41 ± 0.08	
Water level (m) ^(c)	0.19 ± 0.05	0.15 ± 0.06 ^(b)	(-21 %)
<u>PRESSURIZER</u>			
Liquid volume (m ³)		0.66 ± 0.02	
Steam volume		0.27 ± 0.02	
Water temperature (K)		616.2 ± 5.8	
Pressure (MPa)		14.73 ± 0.11	
Liquid level (m)	1.12 ± 0.1	1.23 ± 0.04 ^(b)	(+9.8 %)
<u>BROKEN LOOP</u>			
Cold leg temperature (K)		561.4 ± 1.5	
Hot leg temperature (K)		564.8 ± 1.8	

... / ...

	<u>Specified^(a) Value</u>	<u>Measured Value</u>
<u>SUPPRESSION TANK</u>		
Liquid level (m)	1.27 ± 0.127	1.52 ± 0.06 ²⁾ (+19.6 %)
Gas volume (m ³)		47.90 ± 2.11
Water temperature (K)		354.4 ± 3
Pressure (gas space) (kPa)		99.5 ± 3
Boron concentration (ppm)		3898 ± 15

EMERGENCY CORE COOLING SYSTEM

Borated water storage tank temperature (K)	303 ± 3	303.4 ± 7
Accumulator A liquid level (m) ..	2.15 ± 0.03	2.11 ± 0.01 ²⁾ (-1.8 %)
Accumulator A standpipe position (above inside bottom of tank) (m)		0.4 ± 0.03
Accumulator A pressure (MPa)	4.14 ± 0.17	4.30 ± 0.06 ²⁾ (+3.8 %)
Accumulator A liquid temperature (K)	303 ± 3	300 ± 6 ²⁾ (-0.99 %)
Accumulator B liquid level (m) ..	2.1 ± 0.03	2.08 ± 0.01 ²⁾ (-0.9 %)
Accumulator B pressure (MPa)	4.14 ± 0.17	4.26 ± 0.06 ²⁾ (+2.8 %)
Accumulator B liquid temperature (K)	303 ± 3	308 ± 6 ²⁾ (+1.6 %)

(a) If no value is listed, none was specified.

(b) These values were out of specification.

(c) Steam generator liquid level referenced to 2.95 m (116 in.) above top of tube sheet.

TABLE 2.2. Operational setpoints

Event	Specified (s)	Actual (s)
Reactor scram	1.0 ± 0.025	-0.99 ± 0.01
QOBV open	0	0
Primary pumps turned off	1.25 ± 0.25	0.91 ± 0.01
FPMS isolation valve opened	29 ± 2	29.2 ± 0.1
BLCL QOBV closed	49 ± 5	62.5 ± 0.1
FPMS incore isolation valves closed ^(a)	341	340.8 ± 0.05
Accumulator A & B injection started ^(b)	347 ± 1	344.3 ± 0.05
FPMS BLHL isolation valve closed ^(c)	371 ± 2	371.7 ± 0.05
Accumulator injection stopped ^(d)	507 ± 1	506.5 ± 0.5
HPIS injection starts ^(d)	507 ± 1	515.8 ± 0.5
BLHL QOBV closed ^(e)	<527	535 ± 1
QOBV isolation valves closed ^(f)	>527	695 ± 1

(a) Defined as when 3 peripheral thermocouples measured 1037 K (1408 °F).

(b) 5 to 7 s after FPMS incore isolation valves closed.

(c) 30 ± 2 s after FPMS incore isolation valve closure.

(d) 160 s after accumulator injection initiation.

(e) Within 20 s after accumulator injection termination.

(f) After closure of BLHL QOBV.

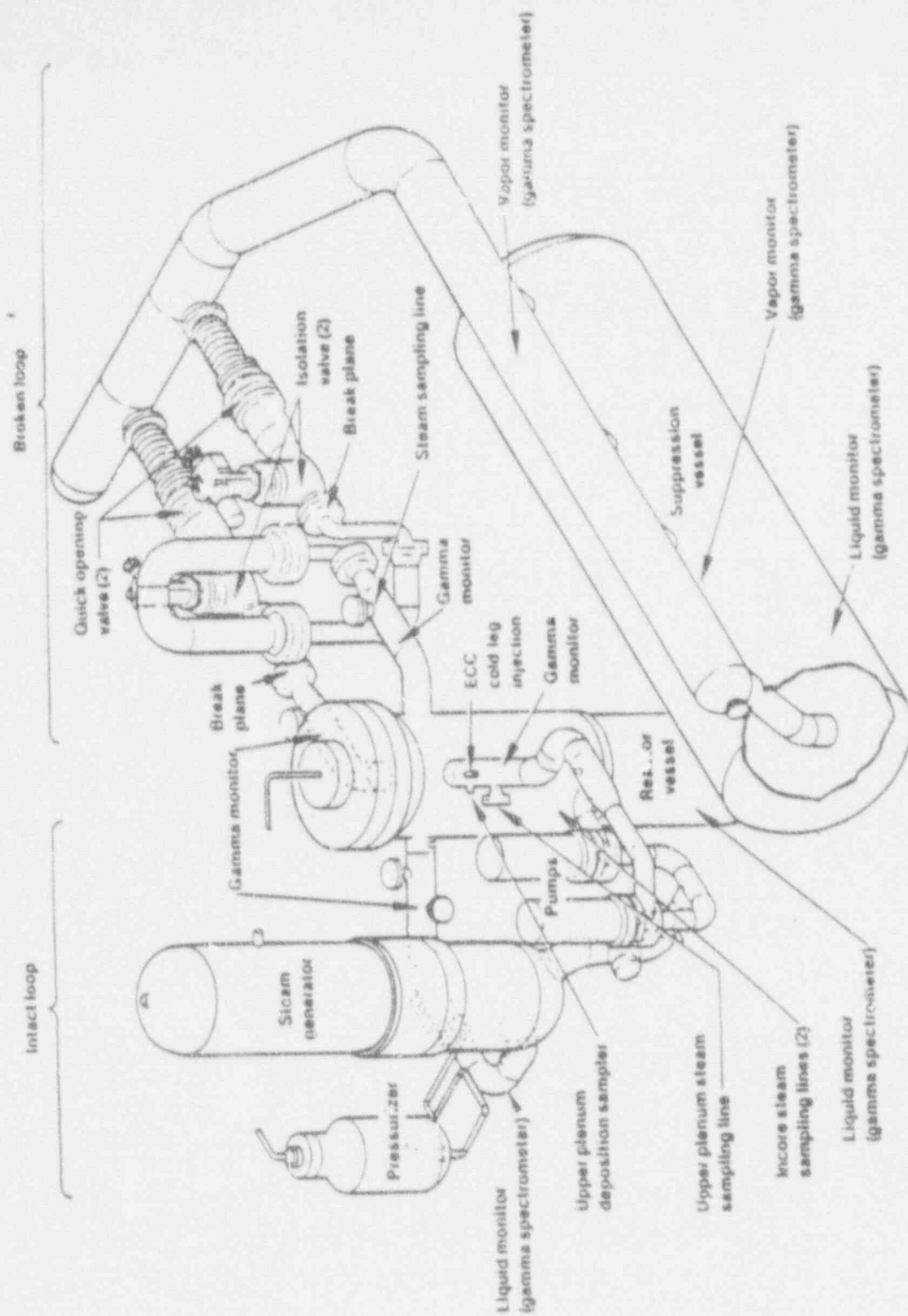


Figure 2.1. Axonometric representation of LOFT system

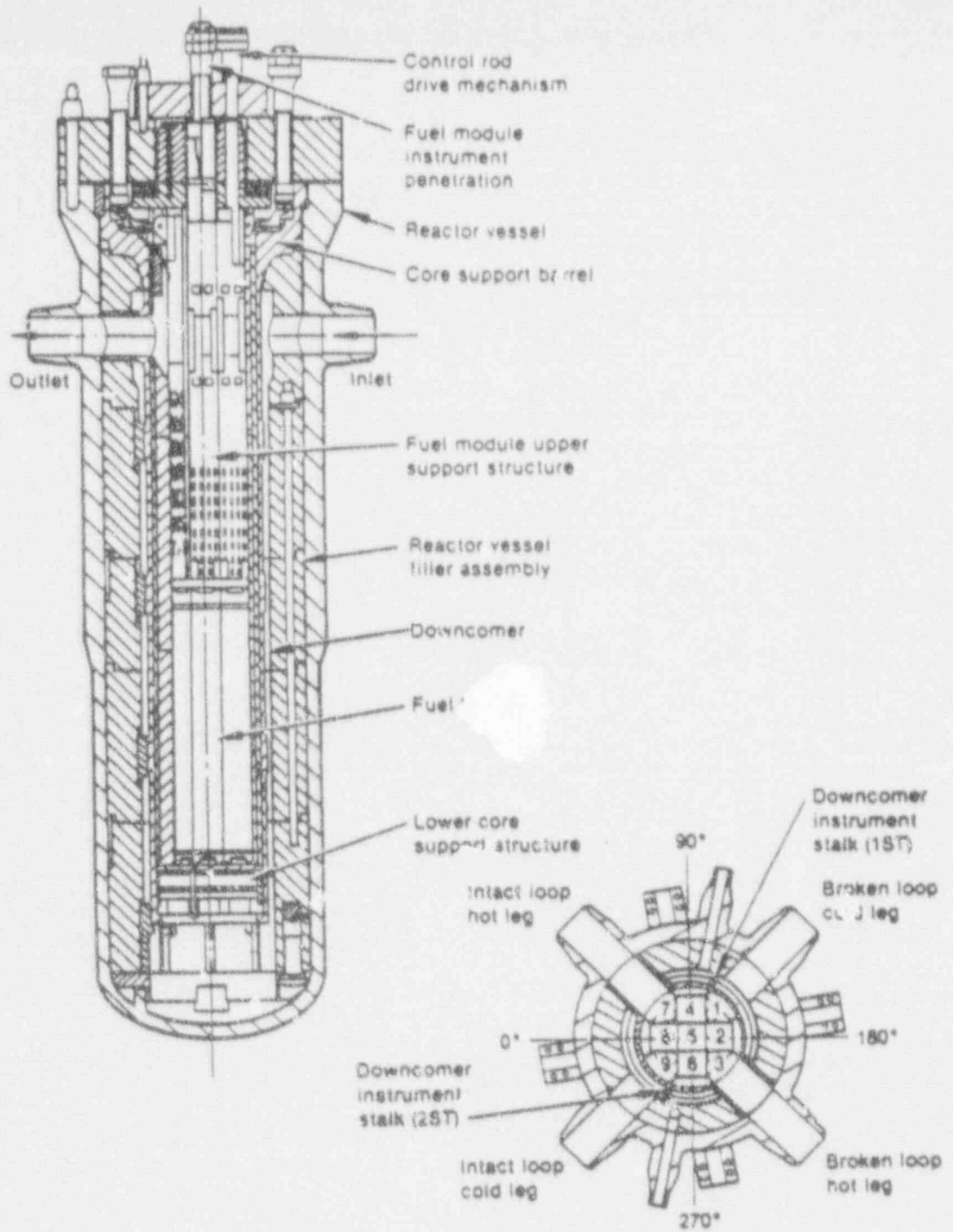


Figure 2.3. LOFT reactor vessel

○ Recorded on PLSS only - low frequency
 ■ Recorded on DDAS/DDAPS - high frequency

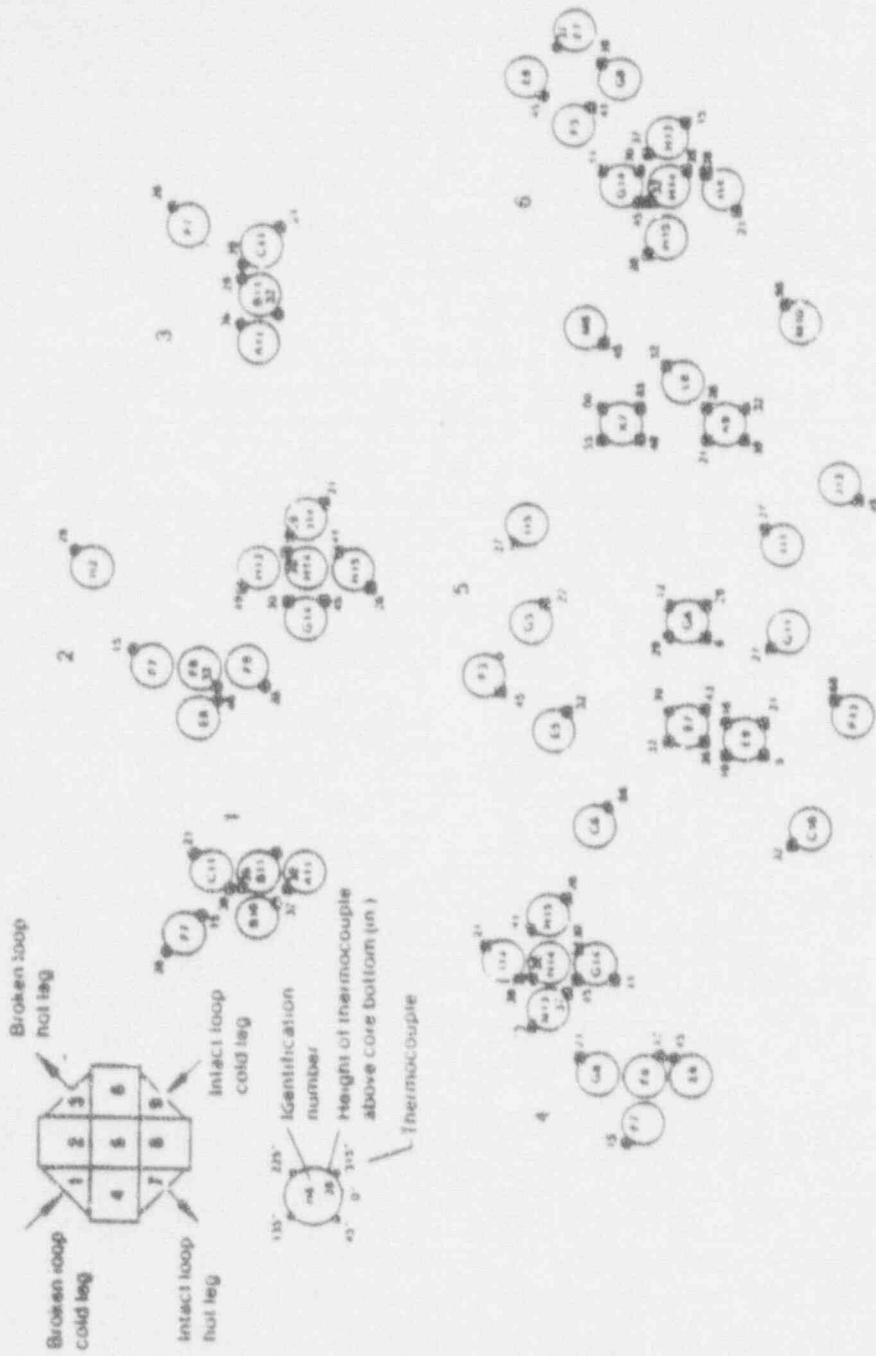


Figure 2.4. Fuel cladding thermocouples in core

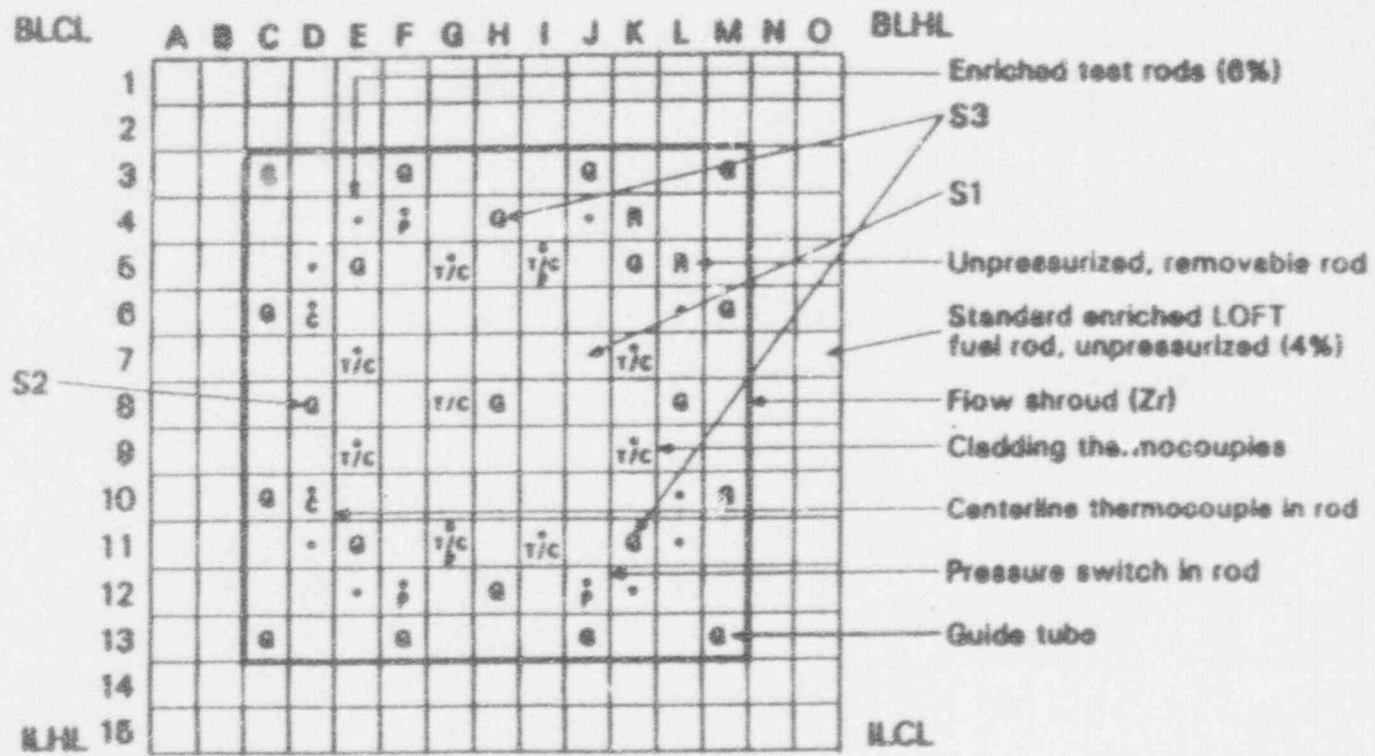
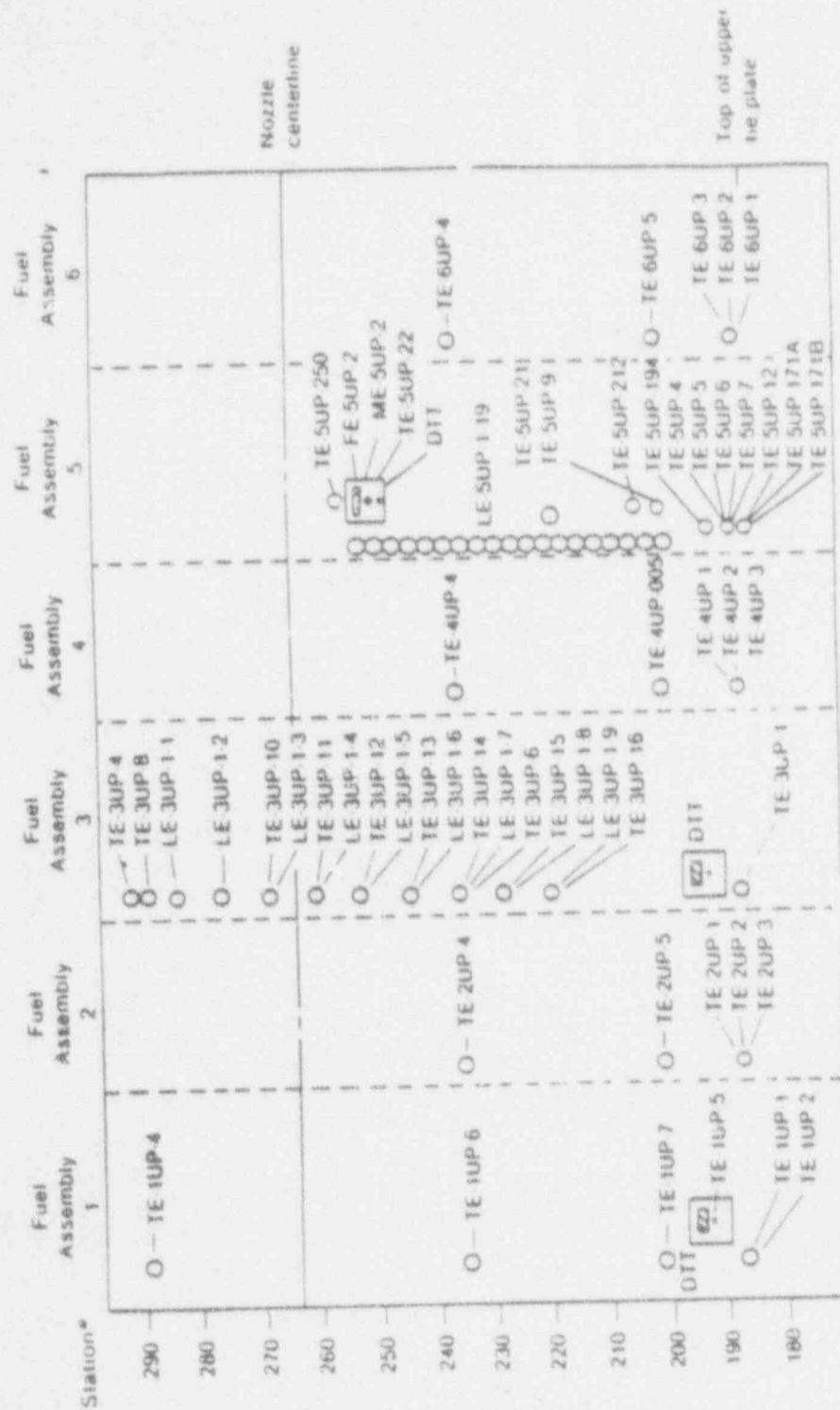


Figure 2.5. Central fuel assembly instrumentation



* Station numbers are a dimensionless relative elevation within the reactor vessel defined at the barrel support ledge inside the reactor vessel flange.

Figure 2.6. Upper plenum thermocouples

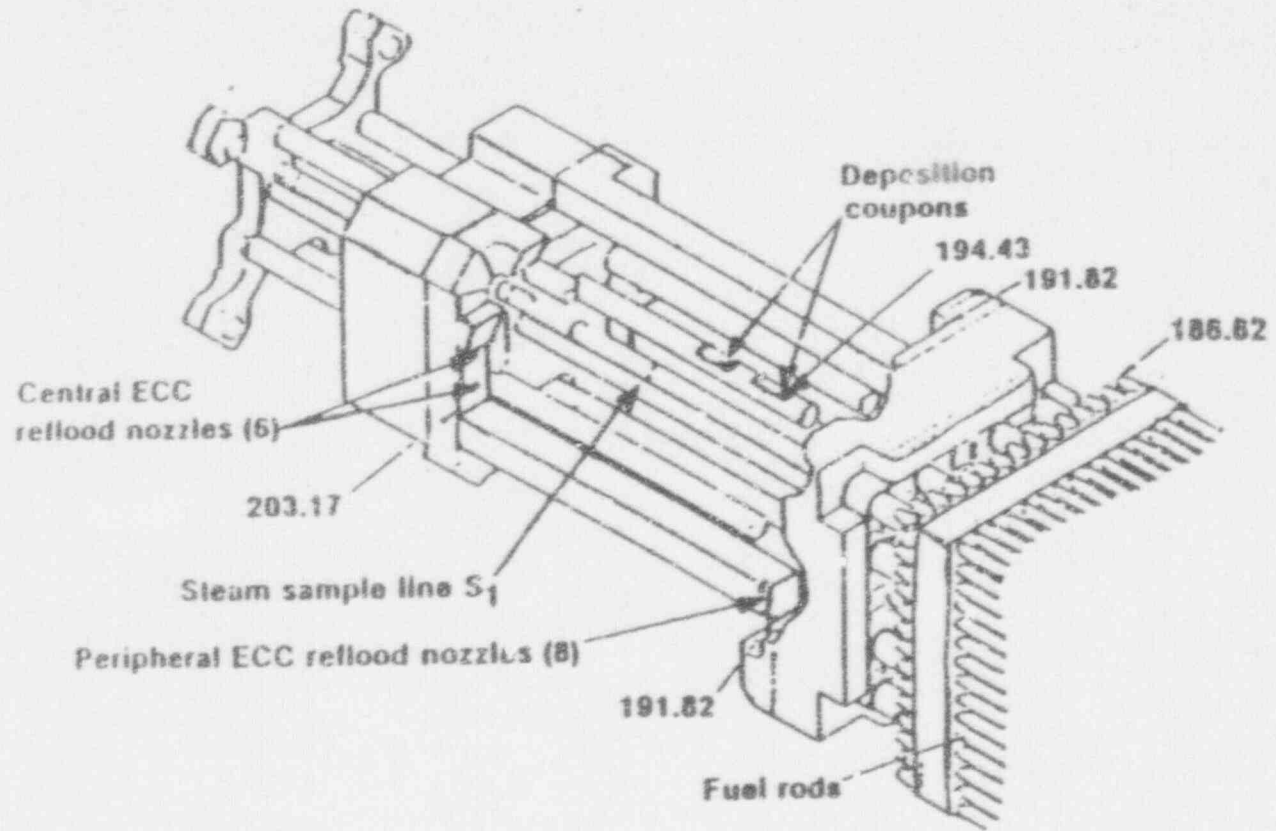


Figure 2.7. Accumulator B upper head Injection

Volumes indicated are approximate values for the volume of the pipe between the indicated point and the upper head injection point.

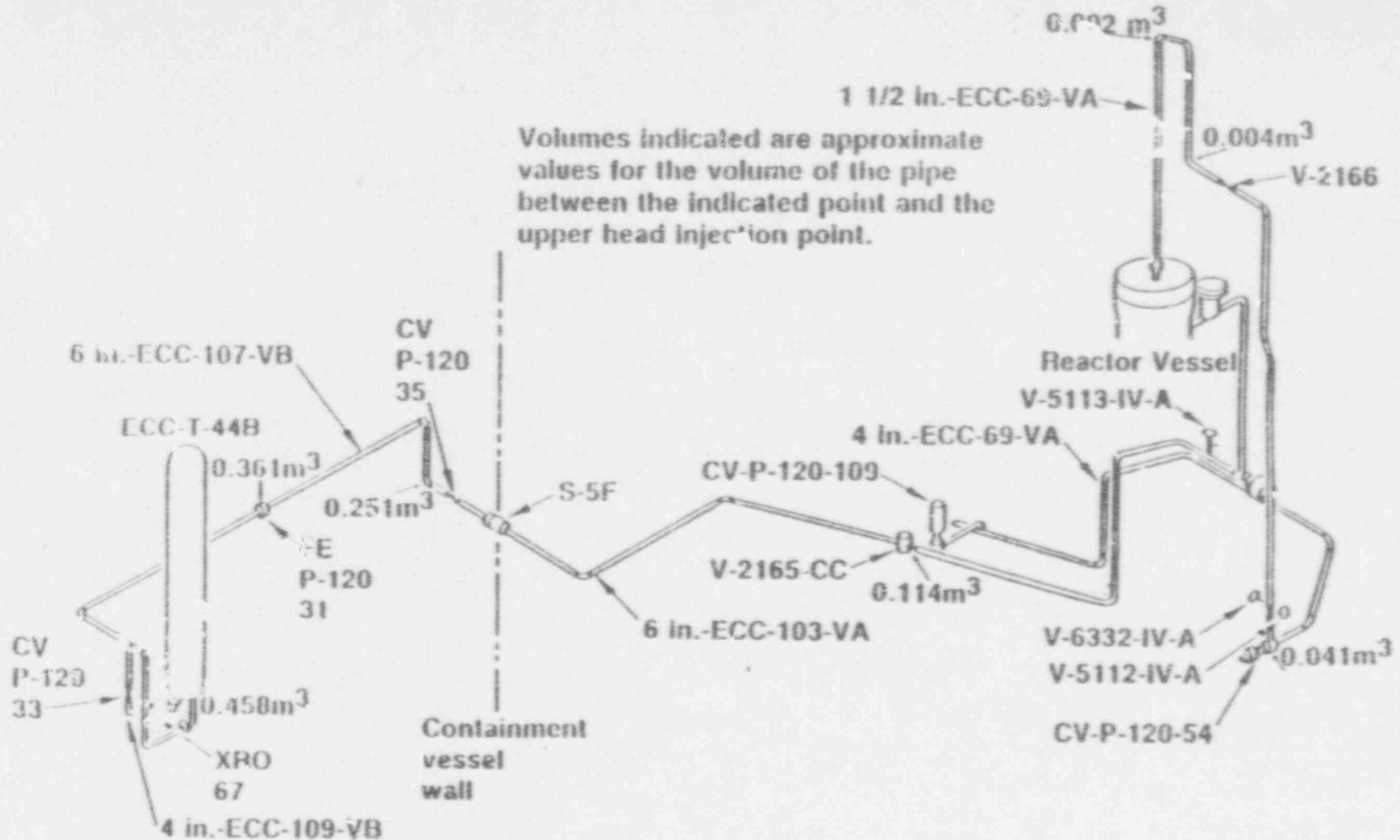


Figure 2.8. Accumulator B injection line

3. INPUT MODEL AND NODALIZATION

3.1 Code

Code used was TRAC-PF1/Mod 1 (version 11.0), installed on CDC Cyber 830.

The Transient Reactor Analysis Code (TRAC serie P) is an advanced best-estimate code for handling PWR accidents, having the capability to make a 3-D model in the reactor vessel. Code uses full two-fluid model with two-steps numerics in the one-dimensional components and may also handle a noncondensable gas field.

TRAC has the capability to treat the following physical phenomena:

1. ECC downcomer penetration and bypass, including the effects of countercurrent flow and hot walls
2. Lower plenum refill with entrainment and phase separation effects
3. Bottom-flood and falling-film reflood quench fronts
4. Multidimensional flow patterns in the core and plenum regions
5. Pool formation and countercurrent flow at the upper core support plate region
6. Pool formation in the upper plenum
7. Steam binding

8. Average rod and hot rod cladding temperature histories
9. Alternate ECC injection systems, including hot leg and upper head injection
10. Direct injection of subcooled ECC water, without artificial mixing zones
11. Critical flow (choking)
12. Liquid carryover during reflood
13. Metal-water reaction
14. Water-hammer effects
15. Wall friction losses
16. Horizontal stratified flow, including reflux cooling

Code has been used without any modification, in models or components. No multiplicative factor for minimum stable film boiling temperature (MSFBT) has been introduced.

3.2 Nodalization

Nodalization of the LOFT system for the FP-1 test may be seen in Figures 3.1 to 3.6 and Table 3.1.

Input deck for determining the plant steady state (actually a first processing by TRAC), is in Table 3.2.

Reactor vessel is modelled as three-dimensional due to the non-homogeneous phenomena registered during the experiment. 3-inner rings represent the core and the 4th downcomer, which extends from level 3 to level 11. Core covers levels 4 to 8 and loops insert at level 11.

First ring simulates the central (11 x 11) fuel assembly and around, a zircaloy shroud. Second and third rings are the internal parts of the peripheral bundles. Vessel is nodalized in 192 cells.

Bypasses have been introduced in the nodalization for getting a better calculation of core liquid fraction (underestimated in pretest calculations). Description and calculations of these bypasses may be found in reference [3]:

- 4 bypasses connecting lower and upper plena, carrying 4.7 % of the flux through the intact loop in the steady state.
- 3 bypasses from downcomer to lower plenum, carrying 4.1 % of the above mentioned flux.

The existence of 1300 rods in the core was simulated using 18 "theoretical" TRAC rods:

- 12 standard rods, representing 4 % enriched fuel rods, one per internal cell.
- 4 rods with peak factor 1.25, simulate the 24 - 6 % fuel rods, one per cell in the central ring.
- 1 rod in cell 8 with peak factor 1.094
- 1 rod in cell 12 with peak factor 1.236

Rod axial dynamic renodalization factor is fixed in a value of 11, instead the initially selected of 60, due to high running times.

Decay heat used has been obtained from the previous power and burn-up histories and may be seen in Table 3.3.

Figure 3.4 shows the intact loop nodalization, including pressurizer, primary side of SG and ECCS with the roots of LPI and HPI systems:

- Accumulator A has been simulated as a PIPE component instead an ACCUM component for avoiding calculation time. Flow rates correspond to those of a 1300 MW scaled KWU reactor.
- Cold leg is fractioned in several cells for helping follow condensation when the accumulator begins to inject.
- Pressurizer has been simulated also as a PIPE for the same reason as before. FILL connected at the upper end represents a relief valve.

Steam generator secondary side is modelled as a STGEN component, including secondary downcomer, main steam line and steam control valve (see Figure 3.5).

broken loop is shown in Fig 3.6. where secondary sides of REFS represent Reflood Assist Bypass Valve, connecting both cold legs, which includes simulators of steam generator and pumps, is nodalized in detail but the cold leg has been defined using the minimum number of nodes, due to the TRAC ability for modelling the choked flow.

Accumulator B has been nodalized as 12 independent FILLS (one for each cell) rooted on the vessel axial node 9, where the upper head injector is located. Each FILL has the same injection history (see Fig 3.7 and Table 3.4) but different weights. History has been defined to be azimuthally symmetric but non-homogeneous from one ring to another. During the blow-down and heatup phases, these weights are:

Ring	Weight	Weight per cell
1	0.33	0.0825
2	0.67	0.1675
3	0.	0.

Planned injection from 345 s on, follows the measured data from accumulators and the corresponding weights are:

Ring	Weight	Weight per cell
1	0.20	0.05
2	0.34	0.085
3	0.46	0.115

Unexpected injection history from accumulator B line has been selected through several parametric studies from different authors and from the data registered by thermocouples

such as TE-5UP-004 (see Fig 3.8), guide tubes and flowmeter FE-P120-31. Main characteristics of the selected injection were:

- Bulk of mass injection starts at 16 s, being preceeded of a slight mass flow of coolant.
- Duration of this injection expands up to 100 s.
- Mass flow doesn't cease during the heatup phase.
- A second injection peak exists at 270 s.
- Total unplanned mass water injected is 400.5 Kg.

Trips defined in TRAC to simulate the events occurred during the experiment, were:

t(s)	Event	Components
0.	SCRAM	50
1.	QOBVs aperture	32,43
2.	Pumps disconnect	4,5
63.5	QOBV (BLHL) closes	43
345.	Reflood begins	15

Accumulator B and BREAKS are inhibited during the plant steady state calculations. When this state is reached, code starts the transient using restart data and the input deck in Table 3.5.

TABLE 3.1. Nodalization elements of LOFT system

	Component Number	Description	Number of Cells	
			Primary	Secondary
Intact	1	Hot leg--TEE	8	3
Loop	2	Steam generator--STGEN	10	5
	3	Steam generator to pump piping--TEE	3	3
	4	Pump--PUMP	2	-
	5	Pump--PUMP	2	-
	6	Pump discharge--TEE	2	1
	7	Cold leg--TEE	9	1
	8	Pressurizer--PRIZER	3	-
	Steam	21	Header-TEE	2
Generator	22	Downcomer--TEE	4	1
Secondary	23	Exit valve--VALVE	6	-
	24	Water inlet--FILL	-	-
	25	Steam exit--BREAK	-	-
Vessel	50	Vessel		
		Axial levels	12	
		Radial segments	4	192
		Azimuthal sectors	4	
Broken	31	Hot leg--TEE ^(a)	26	3
	41	Cold leg--TEE ^(a)	2	2
Loop	32	Hot leg break-BREAK	-	-
	42	Cold leg break--BREAK	-	-
	43	Cold leg break--VALVE	4	-
	Emergency	12	HPI connection and piping--TEE.	1
Core	13	LPI connection and piping--TEE.	1	1
Cooling	14	Accumulator check valve--VALVE.	2	-
Systems	15	Accumulator-ACCUM	3	-
	16	HPI--FILL	1	1
Upper Plenum	81-92	Upper plenum connections, Cells 1 through 12, Vessel Level 9--PIPE	1	-
ECCS	61-72	Upper plenum fills--FILL	-	-

(a) Secondary sides of hot and cold broken loops represent reflood assist bypass lines.

TABLE 3.3. Decay heat in LP-FP-1

t(s)	DH (MW)	t(s)	DH (MW)
0.	37.	4.	1.987
0.3	32.425	6.	1.875
0.9	9.875	8.	1.792
1.28	5.514	10.	1.726
1.38	3.990	15.	1.605
1.40	3.299	20.	1.518
1.46	2.996	30.	1.396
1.52	2.648	40.	1.309
1.59	2.332	60.	1.136
1.61	2.271	100.	1.070
2.	2.155	200.	0.950
3.	2.062	300.	0.840
		10.E4	0.053

TABLE 3.4. Unplanned injection history

t(s)	Mass flow rate (Kg/s)	Integrated flow (Kg)
0.	0.	0.
0.45	1.0	2.9
1.	0.	6.5
2.	0.67	6.8
16.	0.67	16.2
38.	7.2	102.8
40.	5.9	115.9
100.	0.	292.9
175.	0.5	311.6
255.	0.5	351.7
265.	0.	354.2
271.	1.8	359.6
277.	0.5	366.5
345.	0.5	400.5

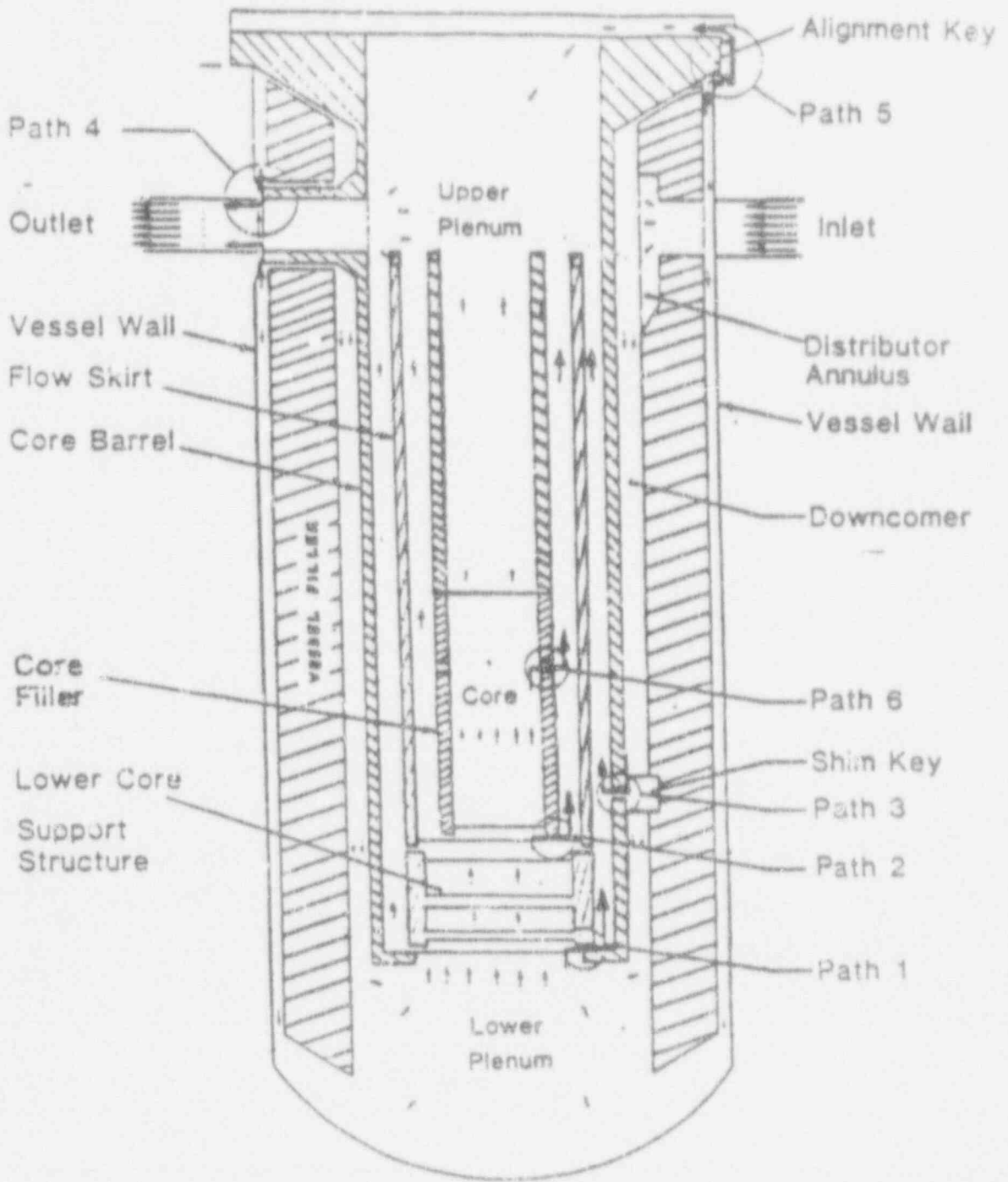


Figure 3.1. Section of LOFT reactor

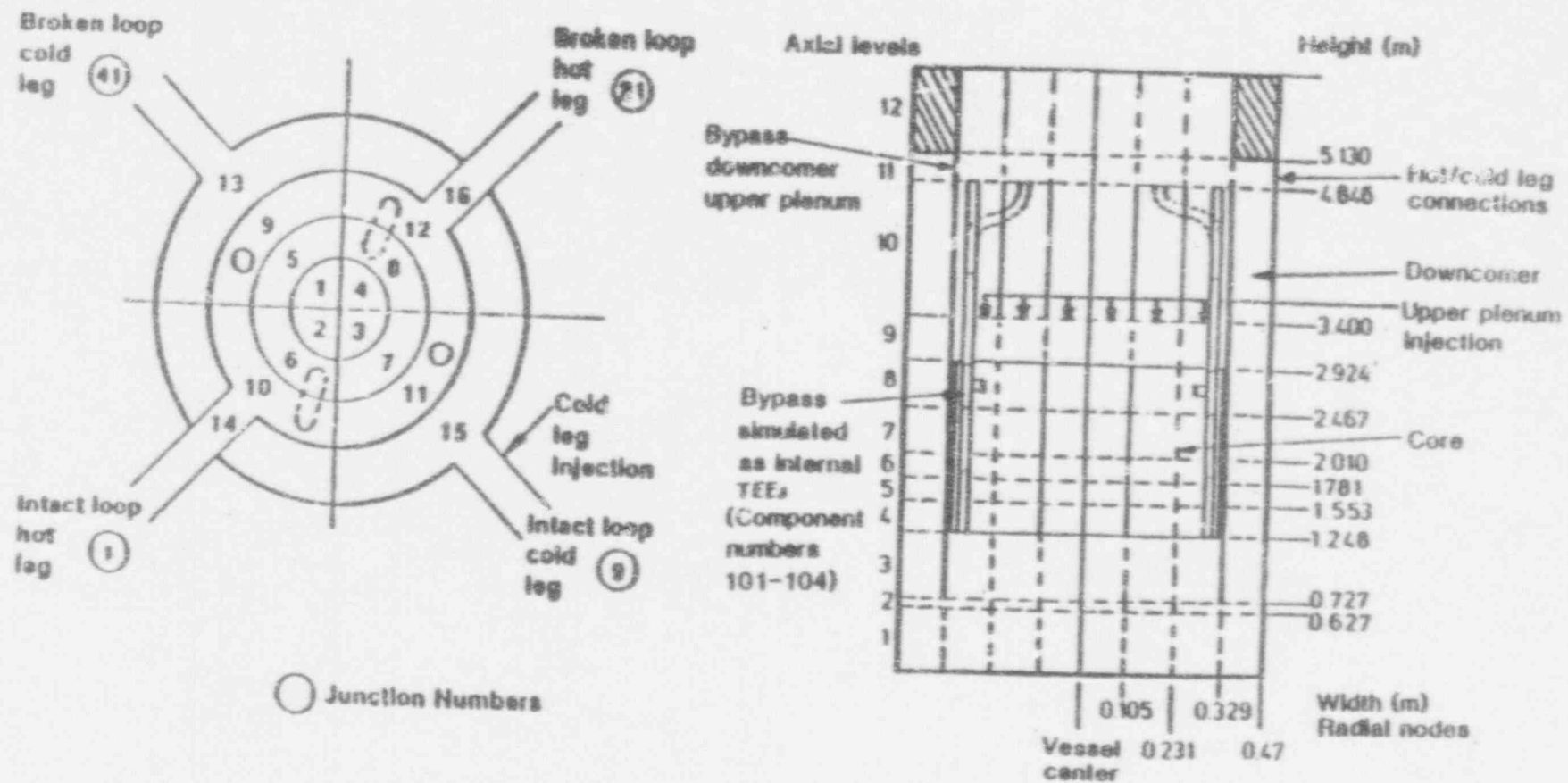


Figure 3.2. Vessel nodalization

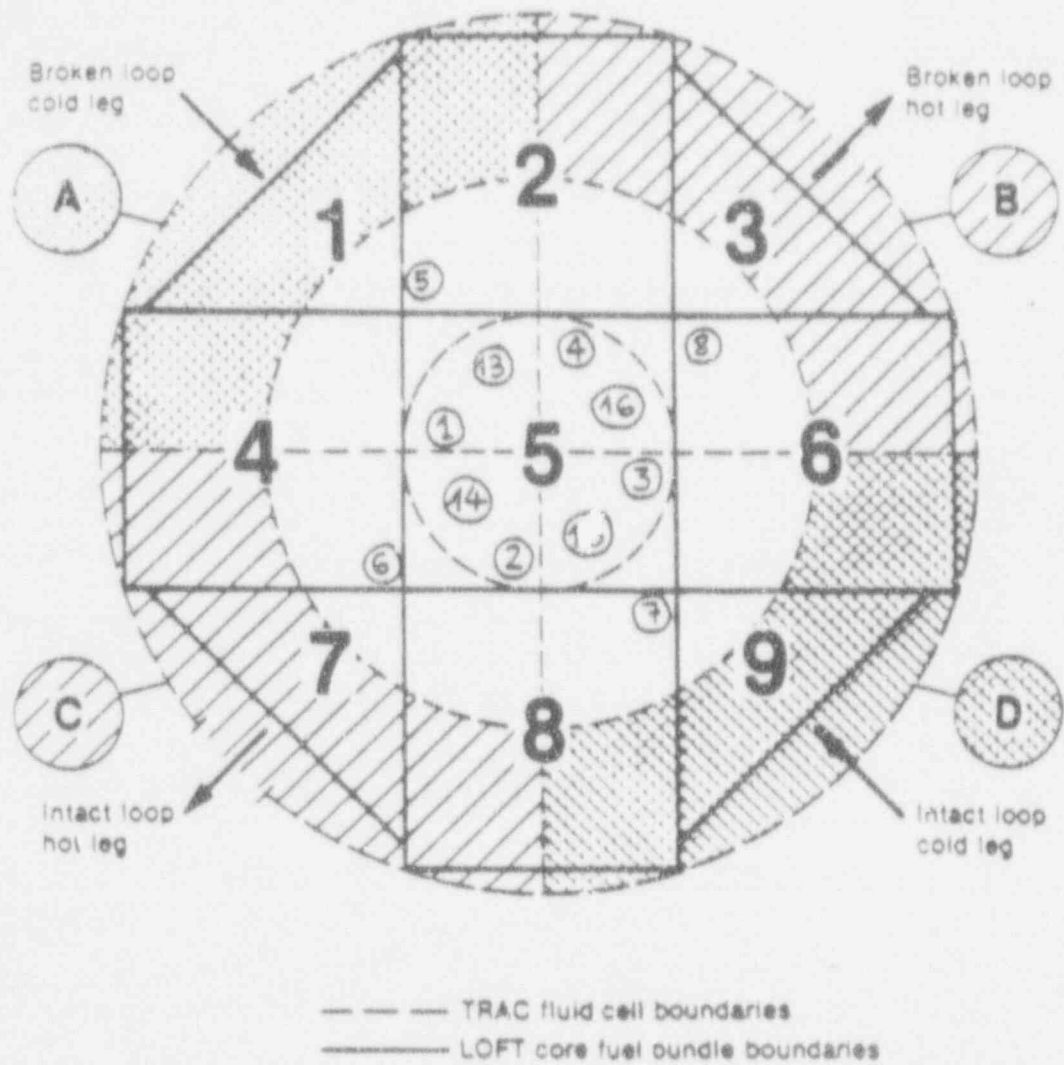


Figure 3.3. Simulated rods location

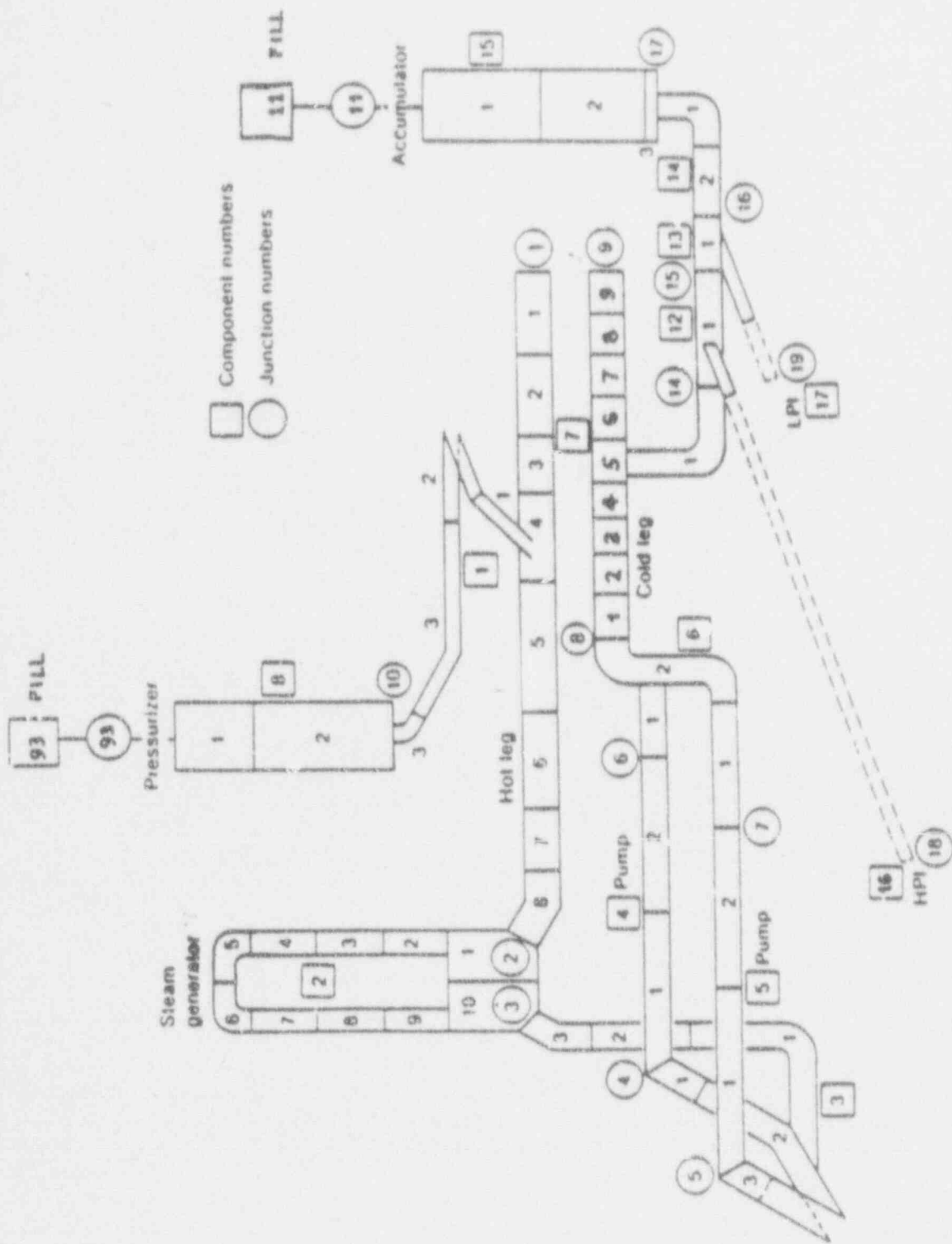


Figure 3.4. Intact loop nodalization

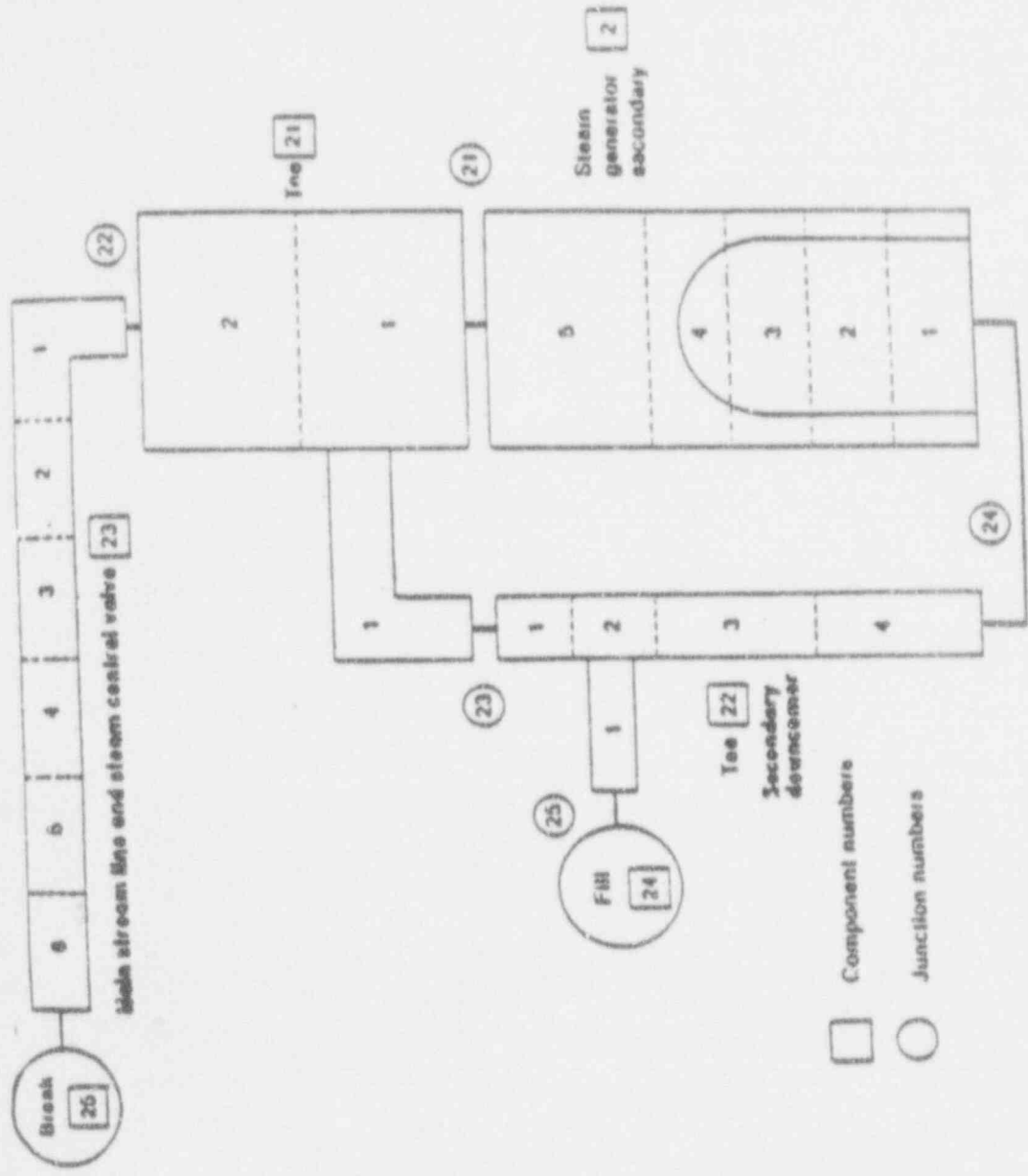


Figure 3.5. Steam generator secondary side nodalization

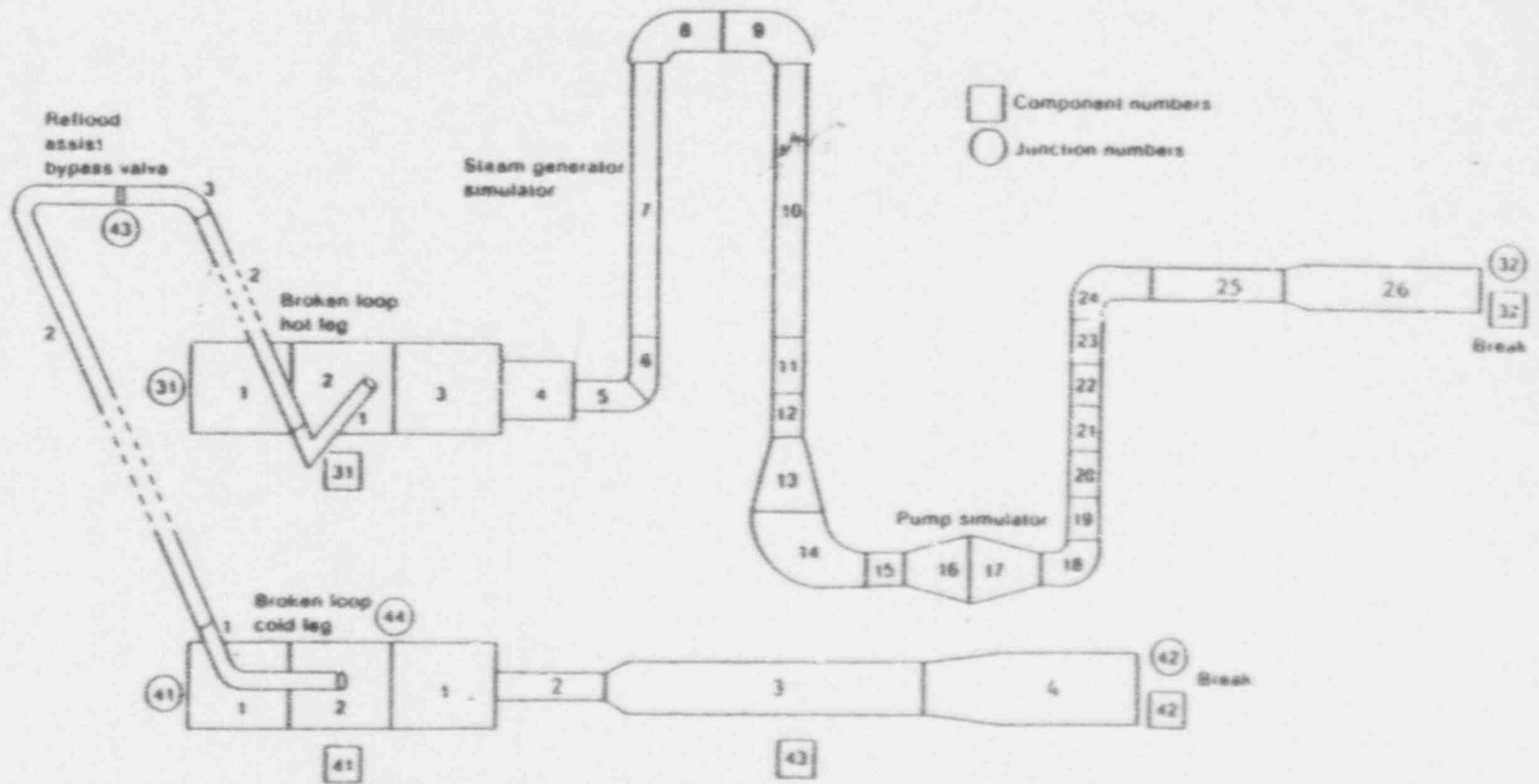


Figure 3.6. Broken loop nodalization

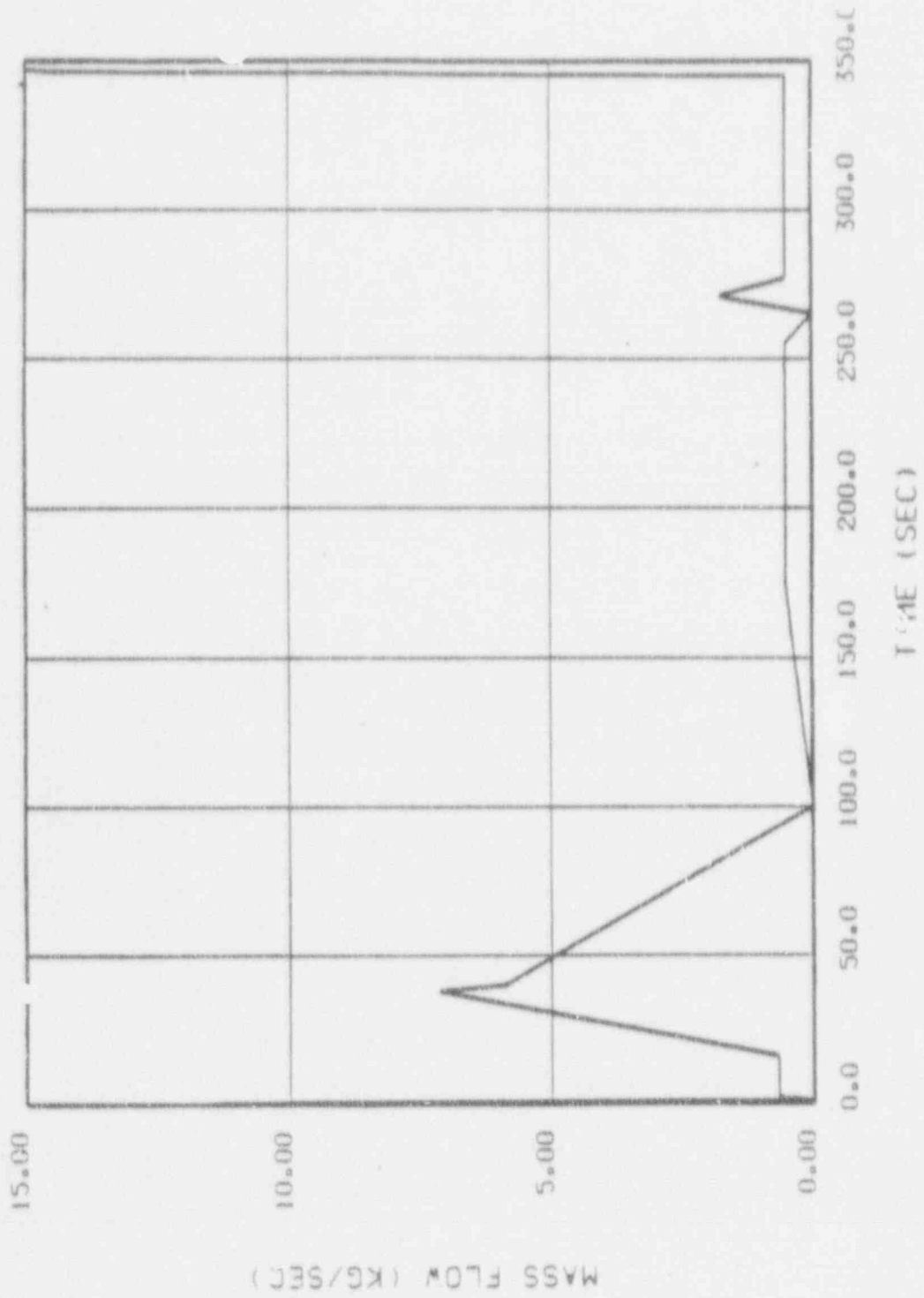


Figure 3.7. Unexpected injection history

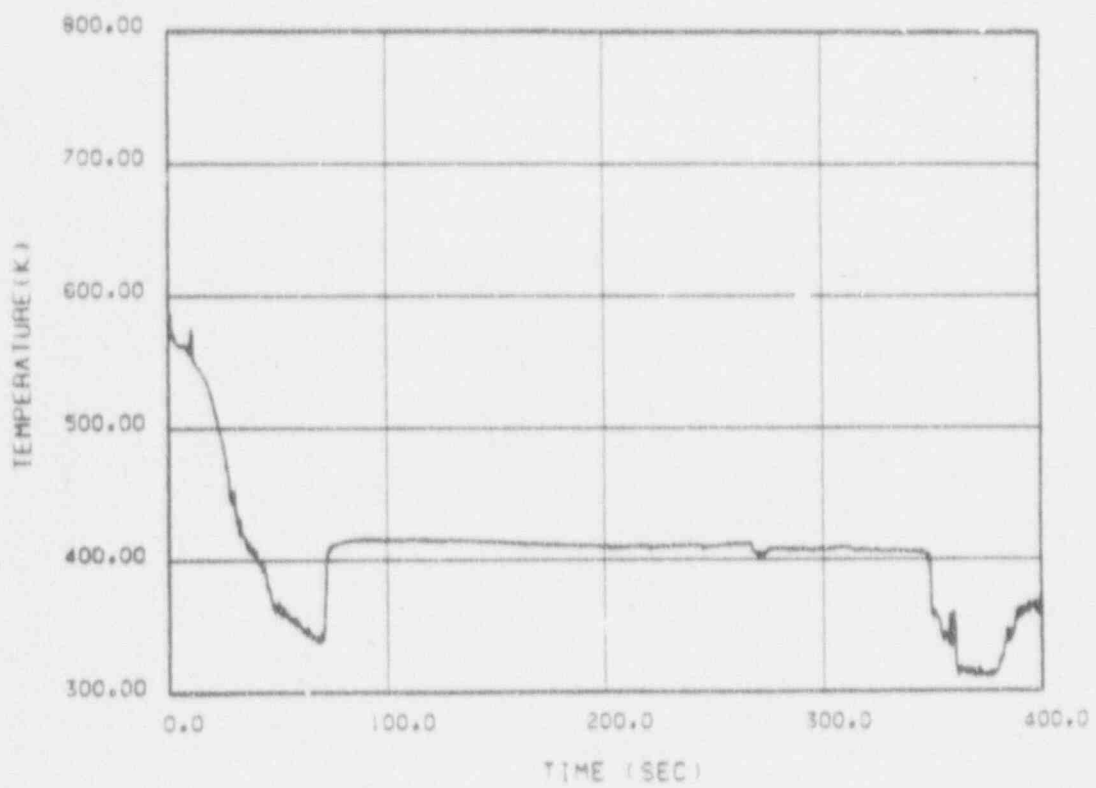
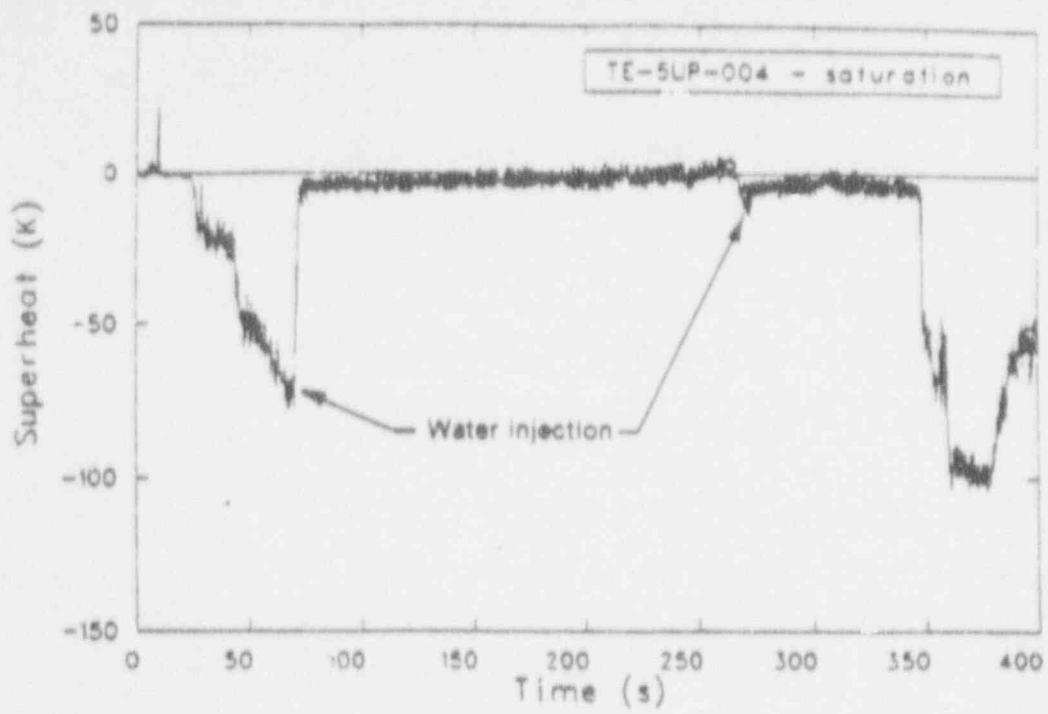


Figure 3.8. TE-5UP-004 measurements

4. RESULTS

4.1 Steady state

Plant steady state conditions have been determined after 52 s of "pseudo-transient" for starting the transient phase calculations, based on the referred input model.

Table 4.1 resumes the final values for a representative set of variables, compared with the equivalent measured ones. The agreement is good in general, except in the case of the steam generator dome pressure, which shows a minor convergence rate. The main consequence of this fact is to have a slightly higher temperature in the intact loop (maintaining differences between hot and cold legs), without influence on the transient evolution.

Convergence criteria used (also in transient) have been:

- Inner convergence : 5.0E-6
- Outer convergence : 5.0E-4
- Steady state convergence : 1.0E-5
- Maximum number of iterations in vessel : 50
- Maximum number of outer iterations : 10
- Maximum number of steady state iterations : 25

Total calculation time for this 52 s of pseudo-transient has been 89400 s of CPU.

4.2 Transient

We analyze in this chapter, results obtained after simulating 400 s of transient, compared with measured data along the experiment. In the case of hydraulic variables, comparison is done between registered data and the variable calculated in the TRAC node related to the detector actual location. For cladding temperatures, code provides information at fixed rod heights; measurements for each thermocouple is compared with the calculations in two adjacent levels and, in some cases, using a cosine law interpolation.

Analysis is mainly directed to explain the asymmetry in the damaged rods distribution and to determine vessel thermal-hydraulic conditions during the fuel rod rupture period (325-345 s), in connection with fission products generation and transport.

Start time of simulation begins at scram time in order to take into account its effects on the plant thermal-hydraulic state, mainly on rod temperatures. From simulation start point through the instant of QOBV apertures, cladding temperatures decrease remarkably, while hydraulic variables remain nearly constant.

4.2.1. Exit flows

When QOBVs open, system pressure drops suddenly due to the subcooled flow through the breaks. Code slightly overestimates ($\sim 7\%$) system pressure up to 16 s, when becomes lower than the observed one, partly because of the unplanned injection existence. The final pressure in the blowdown phase is well calculated (see Fig 4.1).

Figures 4.2 to 4.5 show mass flow rates through the loops, and figures 4.6 to 4.9 the corresponding densities.

Sudden aperture of QOBVs in the broken loop drives the fluid, initially subcooled, to flow out at high velocity, higher in the cold leg, a way with a lower resistance. As pressure continues decreasing, fluid in the broken loop suffer saturation conditions, reaching critical velocity and reducing the mass flow rate. Simultaneously in the intact loop, flow decreases but at lower rate so there is a net positive mass inventory in vessel, causing a bottom-up quench, starting at 4.5-5 s in simulation time (1 s less in real experiment time) (see Fig 4.10 for CORE).

Mass flow rate in the ILHL shows a good agreement with FR-PC-205 detector measurements up to 7 s, when code calculates a back flow from the pressurizer and steam generator. Total mass implied in this flow is about 500 Kg in 18 s, which causes a top-down quench. Fig 4.6 is a plot of the density in ILHL showing two peaks, one for each mentioned back flows (pressurizer and steam generator). First peak is underestimated and delayed, but the second one is simulated properly.

In the ILCL, there is no reference data, because detectors have been removed in this experiment.

Agreement of mass flow rates in 5LHL with experimental data is exceptionally good, matching the peaks caused by the mentioned quenches.

Code underestimates the mass flow rate in the BLCL during the initial phase, causing a greater mass inventory and, consequently, a greater pressure as Fig 4.1 has showed (always in the range of the experimental data uncertainties).

Vessel liquid fraction for upper plenum, core and lower plenum may be seen in Fig 4.10, where all the referred initial hydraulic effects can be observed in timing and relative magnitude.

4.2.2 Initial quenches

Loss of coolant and depressurization have as a direct consequence the interruption of fission processes and a drastic fall in the capability of cooling the fuel rods, from now on producing only decay heat.

Figures 4.11 to 4.14 show the evolution of cladding temperatures for the simulated 6 % fuel rods 13, 14, 15 and 16, at heights 0., 0.305, 0.533, 0.762, 1.219 and 1.676 m, during the blowdown phase. Fig 4.15 to 4.18 show, for the same rods and heights, the evolution in the whole transient (blowdown, heatup and reflood phases).

The explanation of the behaviour in cladding temperatures, can be derived from the comparison between this TRAC calculated variables and the corresponding measurements, such as in figures 4.19 and 4.20.

Code calculates an initial rod dry-out beginning at about 3 s (depending on the level). This first heat-up brings cladding temperatures up to the minimum stable film boiling temperature (MSFBT) or beyond, for almost the whole rod surface. A first (bottom-up) quench stops the rise in temperatures in the bar, but isn't able to destroy the film, as the experiment has showed.

After this slight cooling, temperature grows again (in film boiling regime) through the second quench (top-down at 16 s), which rewets all the bar, remaining yet in the same heat transfer mode, while experimental data show a second quench dropping the cladding temperature to saturation. Code predicts

a maximum temperature 2 or 3 s earlier than in the experiment.

Thermocouples remain at saturation several second, but a third dry-out occurs, irregular in timing and magnitude. An unexpected injection, actually non-homogeneous and asymmetric ends this phase. Code responds to the simulated injection only decreasing slowly cladding temperatures and, in some cases (as the 4 % fuel rods in central ring and 6 % fuel rods in cell 3) quenching the whole rod and getting the saturation temperature in the surface, when the MSFBT is reached, but in times delayed up to 40 s, compared with the measured in the experiment.

4.2.3 Heat-up

After the blowdown phase and under the effects of a decreasing unexpected injection, calculated cladding temperatures for rewetted rods begins to departure from nucleate boiling in time very near to the observed. Several thermocouples - (such as 5G08 or 5I05) undergoes particular quench situations reaching the DNB point very late. Code, of course, cannot predict these special cases because simulated injection is defined to be symmetric.

DNB point is exceptionally well matched in rods 5G08, 5I11, 5E09 and 4C14, all of them starting from saturation.

Calculated mean heating rate, from DNB to reflood point, for 6 % fuel rods is about 3 K/s at peak power elevation, being 4-5 K/s a typical value for the initial rate. Calculated values are very near to measured data.

In those cases when cladding is in film boiling regime, the slope is nearly the same or lower, but starting at temperatures 200-300 K higher (see figure 26).

The effects of a second peak of injected water at 270 s, which provides about 12 Kg of coolant, are seen as a little decrease of 10-15 K in cladding temperatures. Actually, this was distributed in a very chaotic way, such as several thermocouples showed (including those in guide tubes).

Heat-up follows steadily from this point through the simultaneous injection from accumulators A and B at 345 s.

Table 4.2 resumes the maximum cladding temperatures reached in the TRAC simulated rods at peak power elevation (27 inch). Marked values correspond to those rods which remain in film boiling regime during the whole transient. Fig 4.23 to 4.25 show the behaviour of those instrumented 6 % fuel rods which ruptured, compared with the corresponding TRAC calculations. In the case of 5G11, the agreement is exceptionally good, because of heat-up starts from saturation.

For peripheral rods (Fig 4.26), when the simulated rod has descended from film boiling regime, the fitting in the final heat-up phase is successful.

Thermocouples cited above, show successful fits between calculations and measured data along the final heat-up phase. In the case of 5G08 (4 % enriched fuel rod), predicted cladding temperature is lower than the registered during the final heat-up phase, so it's possible that the actual temperature in central element during the rod rupture period were slightly higher than the calculated one. This comment is derived from only one 4 % enriched rod and must be seen as an hypothesis.

4.2.4. T/H conditions during rod rupture period

Results from TRAC shows that all the hydraulic variables were nearly constant during the period in which, eight 6 % fuel rods ruptured (325-345 s).

A small quantity of water from accumulator B line was falling over the element during this phase as some detectors showed (see Fig 3.8 for TE-5UP-004). We are feeding the system with 0.5 Kg/s of coolant in this period, which flows down among the rods, vaporizing partly.

Tables 4.3 to 4.4 resume the mean (ring averaged) vapor and liquid behaviour during the rod rupture period, when eight 6 % fuel rods failed. Fig 4.27 shows the flow patterns (also during rupture period, when 8 - 6 % fuel rods failed. Figure averaged per ring) through the vessel.

One may see two possible and alternative paths for the generated fission products, both starting at peak power elevation (where there is a stagnation point) through BLHL:

- Ascending from this point to the upper plenum
- Descending from peak power elevation to the lower plenum and then, ascending through the peripheral bundles in ring 3.

Vapor in the upper plenum has a very asymmetric behaviour (Fig 4.28 and 4.29), which may be explained by the presence of the hot legs. Those cells near to the cold legs have near identical values.

In second ring (inner parts of peripheral bundles), vapor is nearly stagnant during this period.

4.2.5. Combined injection

From 345 s on, both accumulators inject coolant for system recovery. Injection caused dramatic oscillations in all plant variables, except on cladding temperatures which drop steadily to the moment when the MSFBT is reached and the film is destroyed. Quenching is nearly instantaneous but happens with a great delay respect to the measured final quench times. Enriched fuel rods (6 %) doesn't have completed the rewetting phase at 400 s in TRAC calculations.

Some other characteristics of the reflood period are:

- Core liquid fraction rise from 0. to 0.8 at a rate of 4 Kg/s (see figure 4.30).
- Vapor temperature in the core, decreases at a rate of about 6.5 K/s near the peak power elevation.
- Cooling rates for cladding temperatures are about:

- 7 K/s for 4 % enriched fuel rods in central element.
- 10 K/s for 6 % enriched fuel rods in central element.
- 10 K/s for 4 % enriched fuel rods in peripheral elements.

TABLE 4.1. Plant calculated steady state

	Measured	TRAC/PF1
Hot leg pressure (Mpa)	14.77 + 0.07	14.87
Hot leg temperature (K)	577.6 + 0.8	581.6
Cold leg temperature (K)	563.2 + 1.1	567.2
Mass flow in loop (Kg/s)	486.7 + 2.5	487.5
Steam generator secondary pressure (Mpa)	6.41 + 0.08	6.77
Pressurizer pressure (Mpa)	14.73 + 0.11	14.85
Pressurizer temperature (K)	616.2 + 5.8	614.3
Broken loop cold leg temperature (K)	561.4 + 1.5	562.0
Broken loop hot leg temperature (K)	564.8 + 1.8	565.0

TABLE 4.2. Maximum cladding temperatures during rod rupture phase

	4% Rod	T(K)	6% Rod	T(K)
Ring 1	1	1025	13	1254*
	2	1018	14	1238*
	3	1018	15	1167
	4	1048	16	1192
Ring 2	5	1076*		
	6	1173*		
	7	1165*		
	8	1176*		
Ring 3	10	950		
	11	933		
	12	940		
	13	952		

TABLE 4.3. Vapor axial velocity (m/s) in central ring during rod rupture phase

LEVEL	CELL			
	1	2	3	4
4	-0.75	-0.61	-0.71	-1.36
5	-0.41	-0.30	-0.39	-0.71
6	0.03	0.01	0.03	0.02
7	0.73	0.52	0.70	1.33
8	1.08	0.89	1.06	1.35

TABLE 4.4. Liquid axial velocity (m/s) in central ring during rod rupture phase

LEVEL	CELL			
	1	2	3	4
4	-3.60	-3.60	-3.60	-3.60
5	-3.51	-3.53	-3.51	-3.50
6	-3.45	-3.47	-3.45	-3.40
7	-3.35	-3.39	-3.35	-3.28
8	-3.26	-3.29	-3.26	-3.22

TABLE 4.5. Vapor temperature (K) in central ring during rod rupture phase

LEVEL	CELL			
	1	2	3	4
4	502	498	499	548
5	628	621	625	666
6	640	636	637	660
7	598	596	597	617
8	498	491	497	522

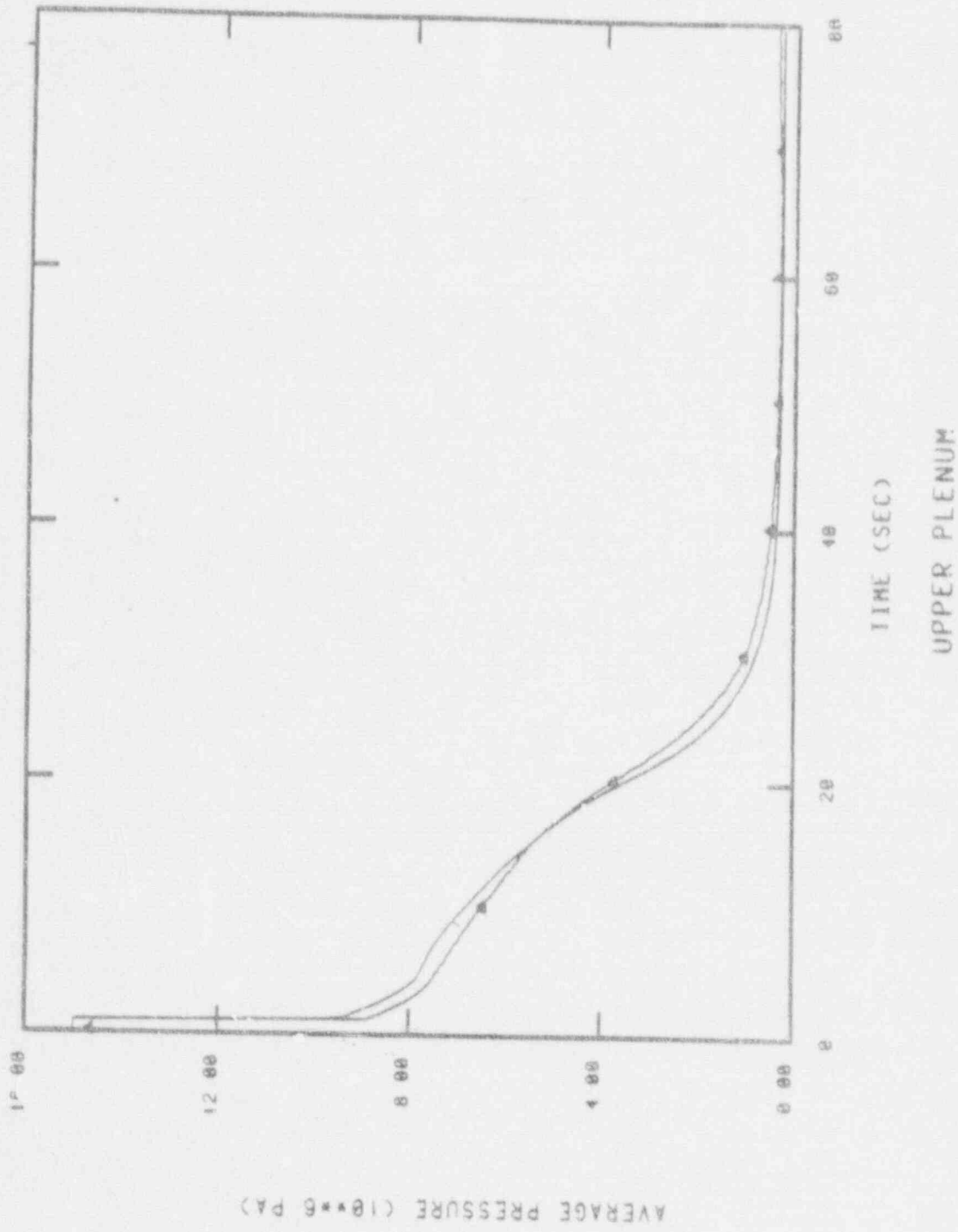


Figure 4.1. Upper plenum pressure

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▲ FR-PC-205

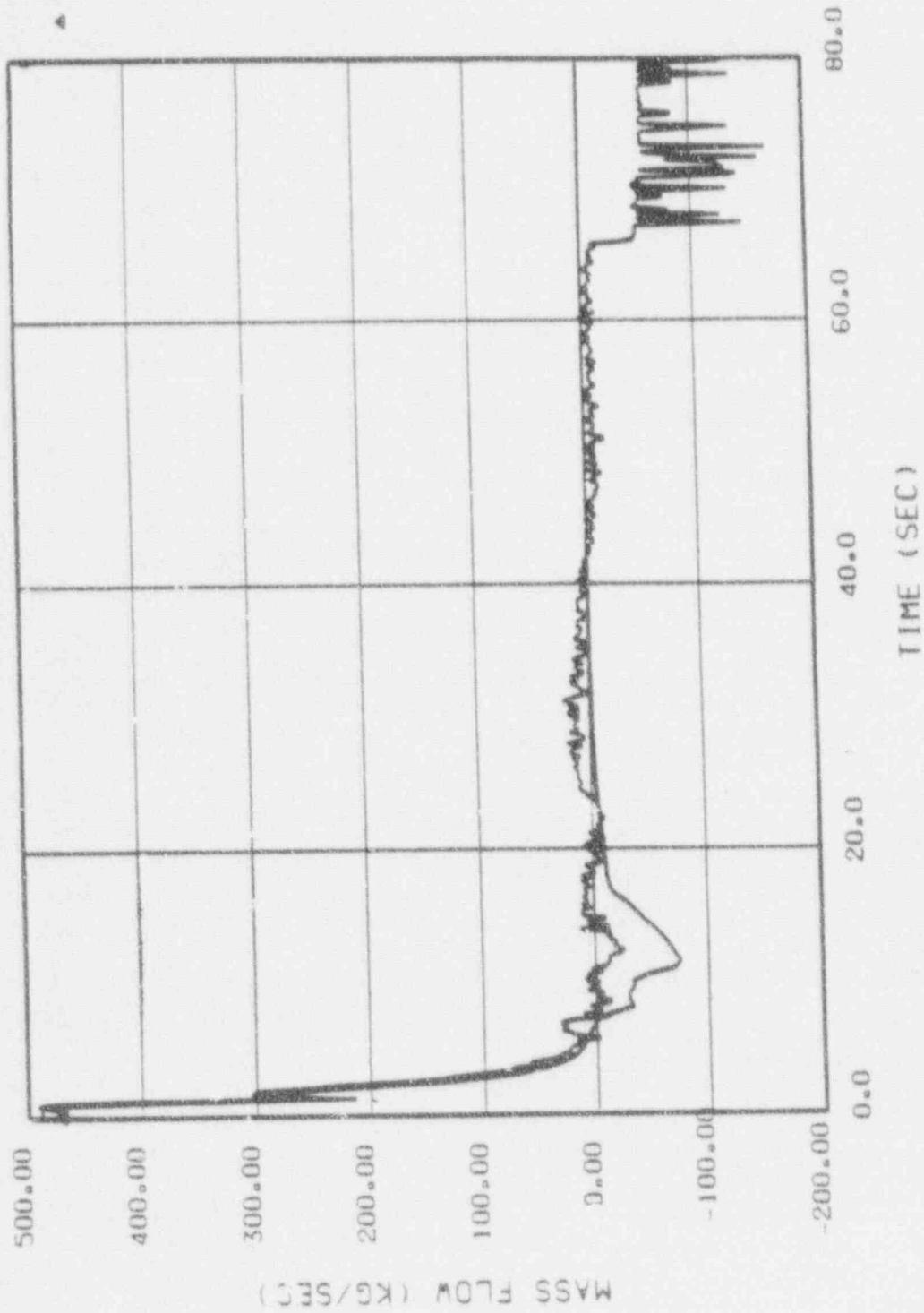


Figure 4.2. Intact loop hot leg (cell 3) mass flow

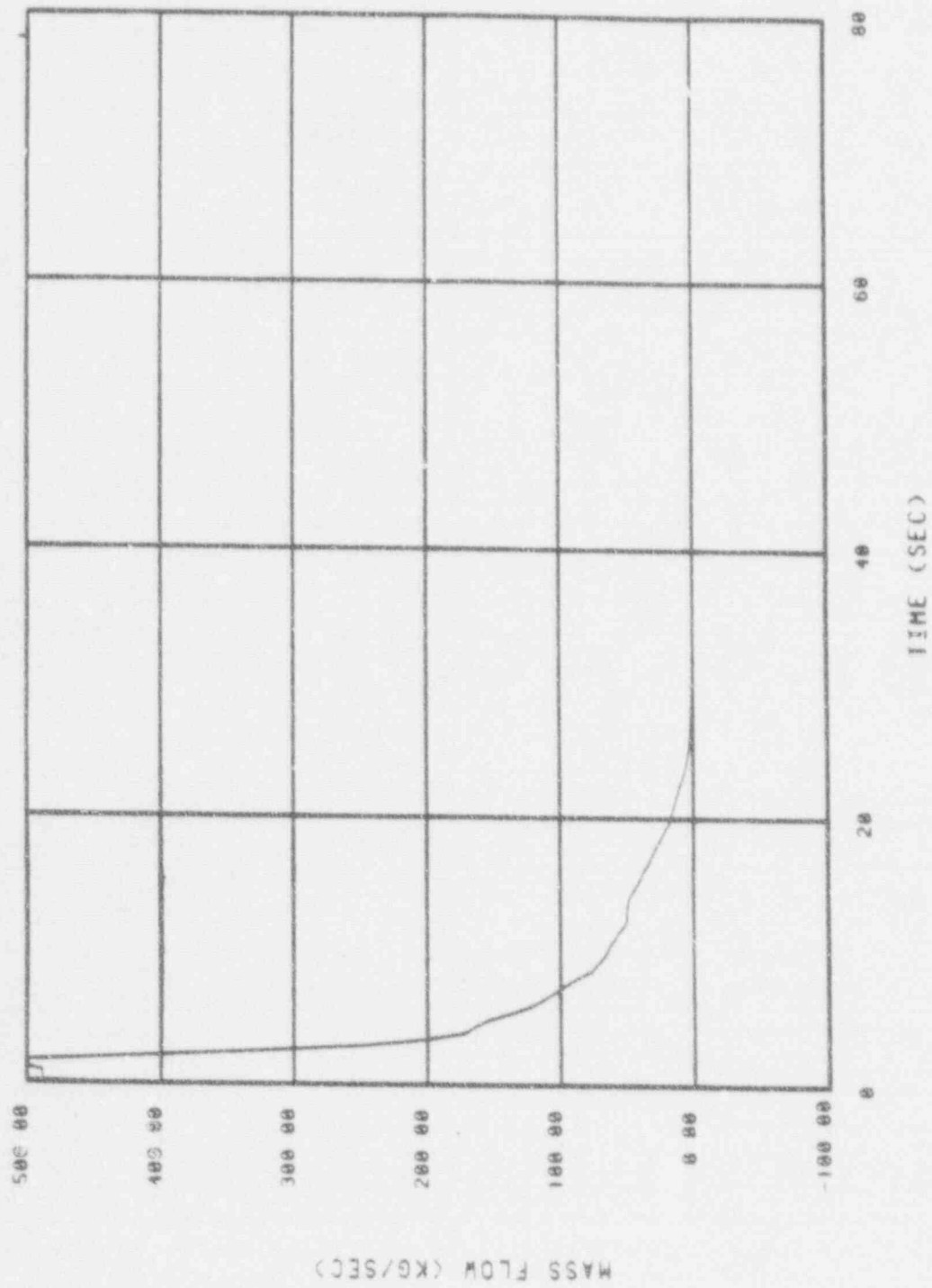


Figure 4.3. Intact loop cold leg (cell 2) mass flow

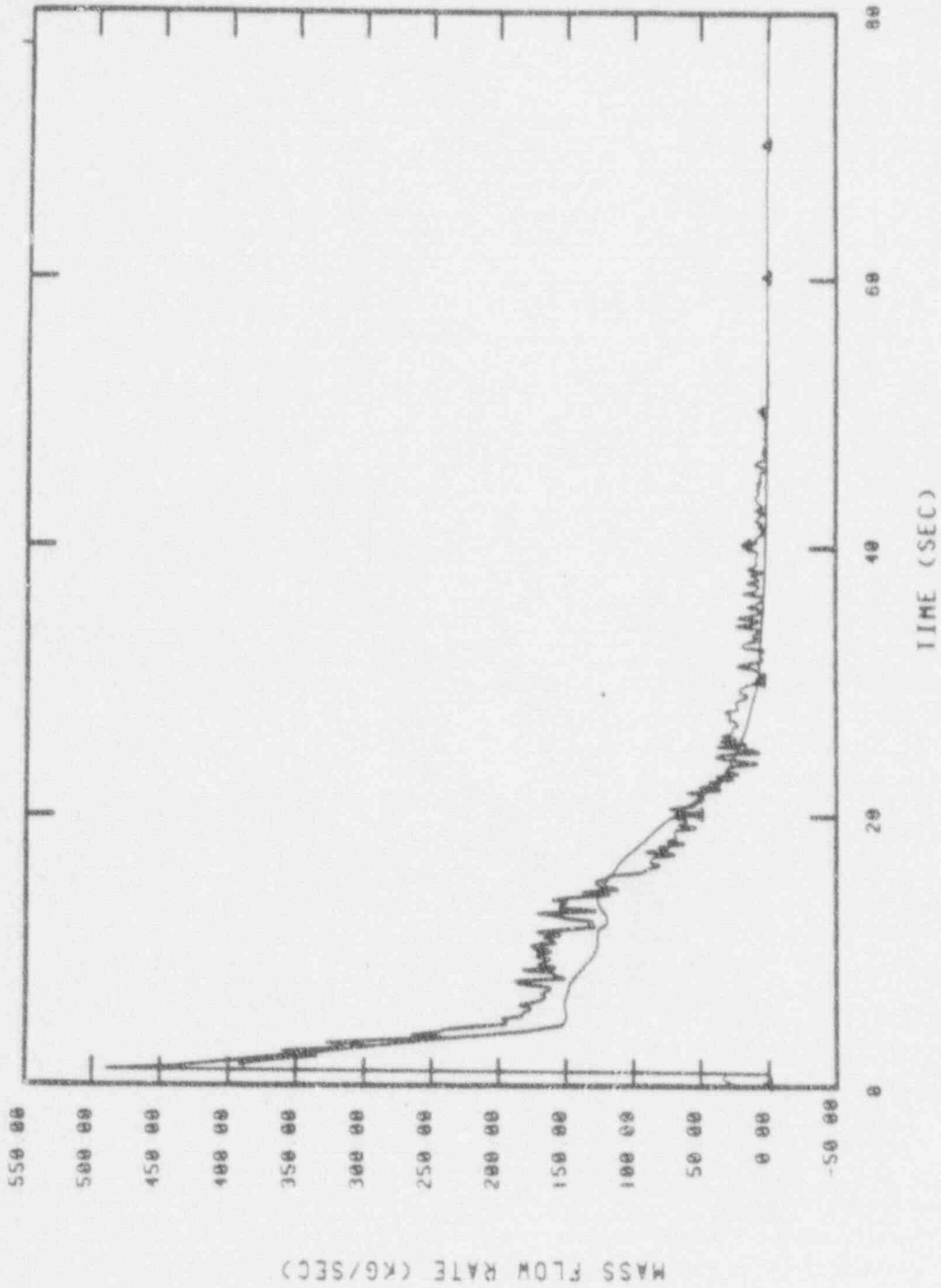


Figure 4.4. Broken loop cold leg (cell 1) mass flow

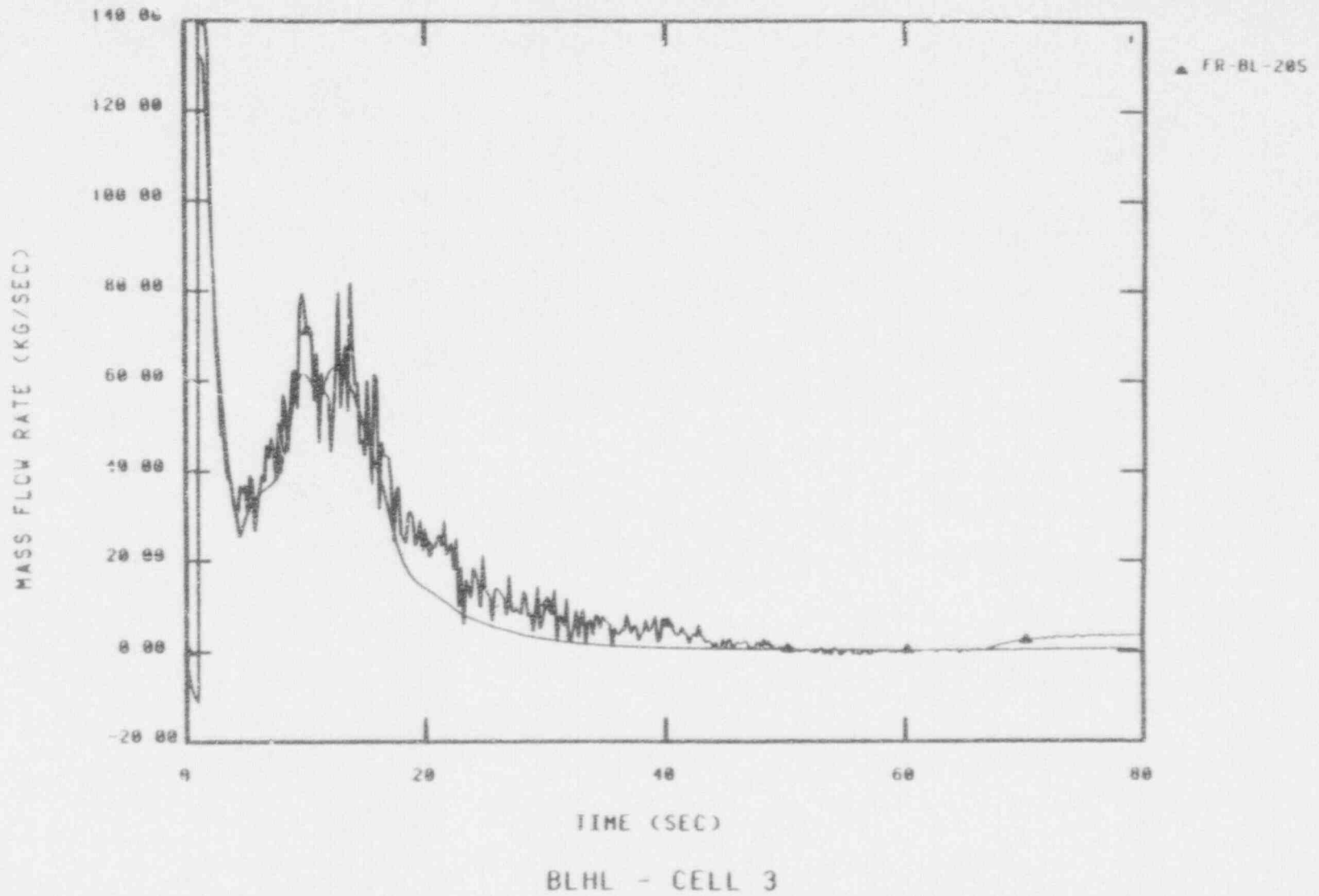
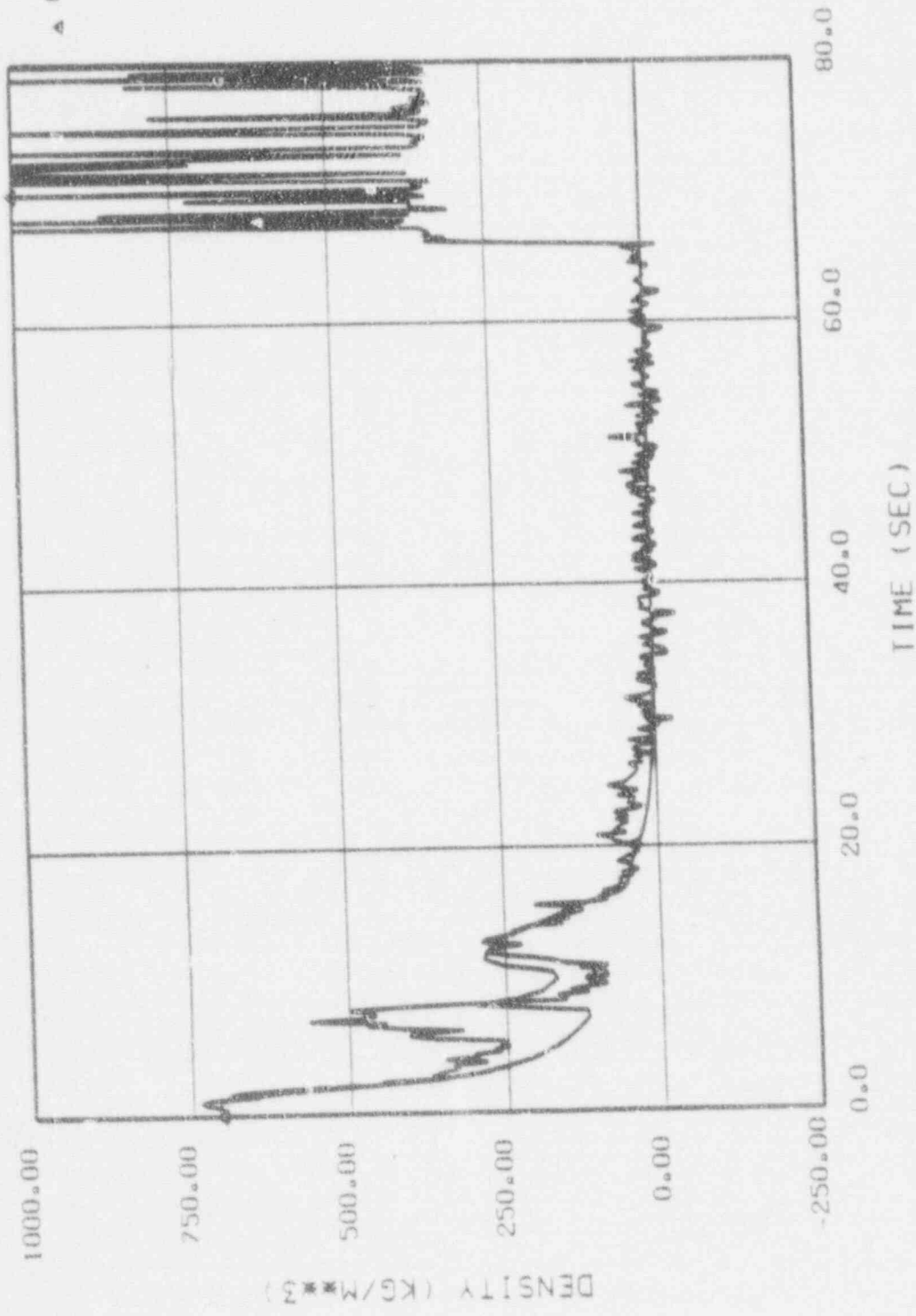


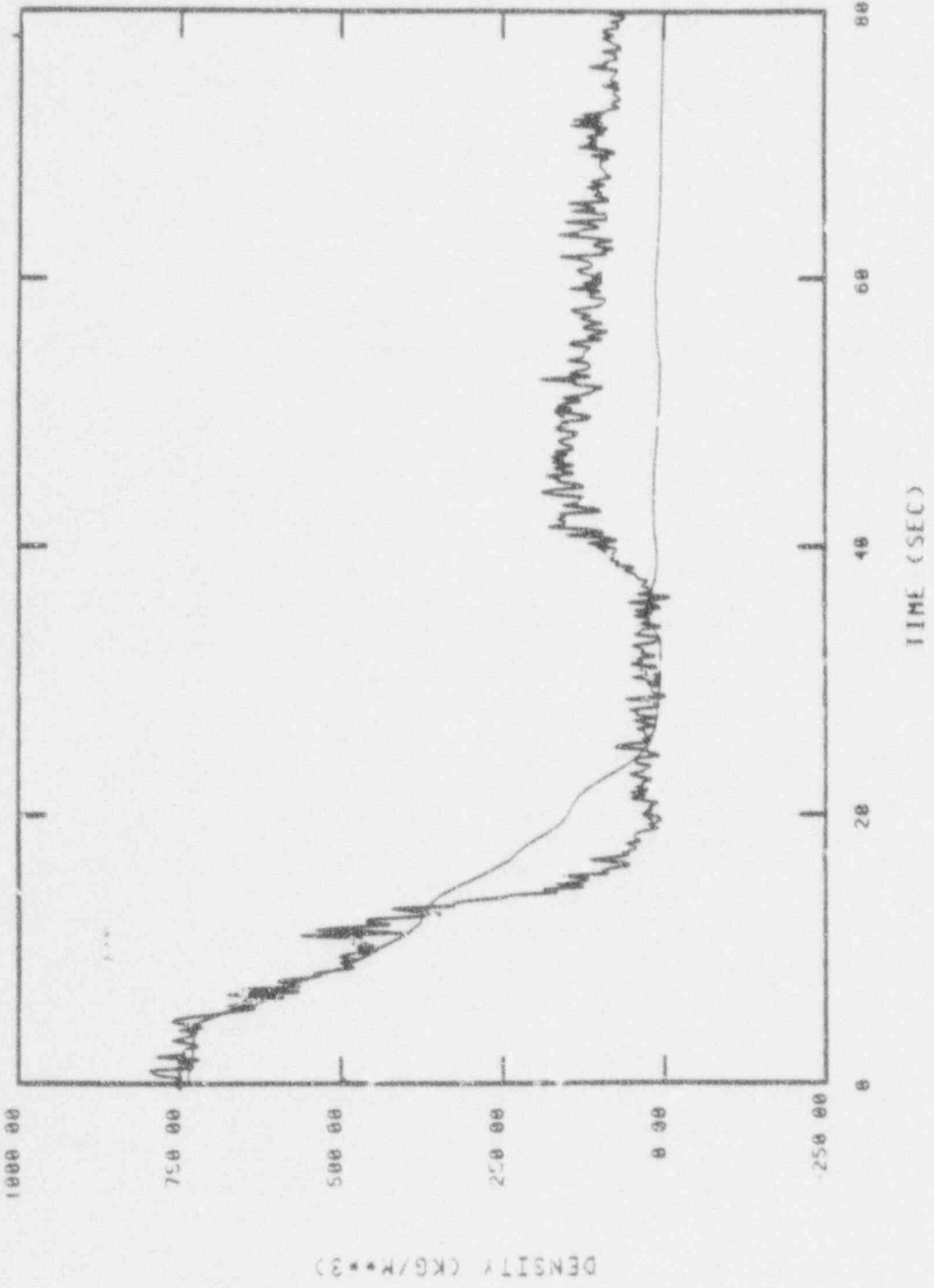
Figure 4.5. Broken loop hot leg (cell 3) mass flow

A DE PC-225



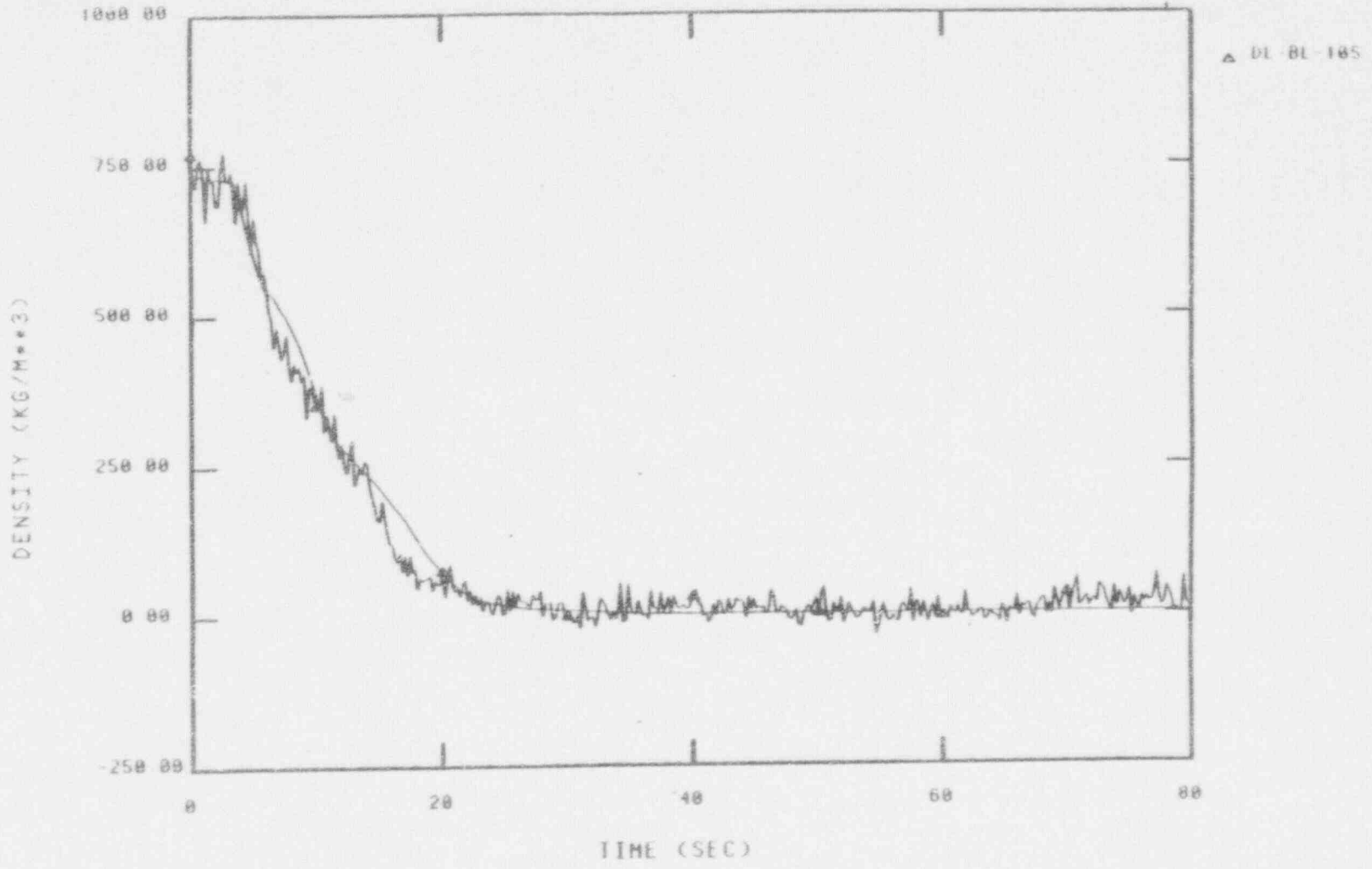
ILHL - CELL 2

Figure 4.6. Intact loop hot leg (cell 2) density



I:CL - CELL 2

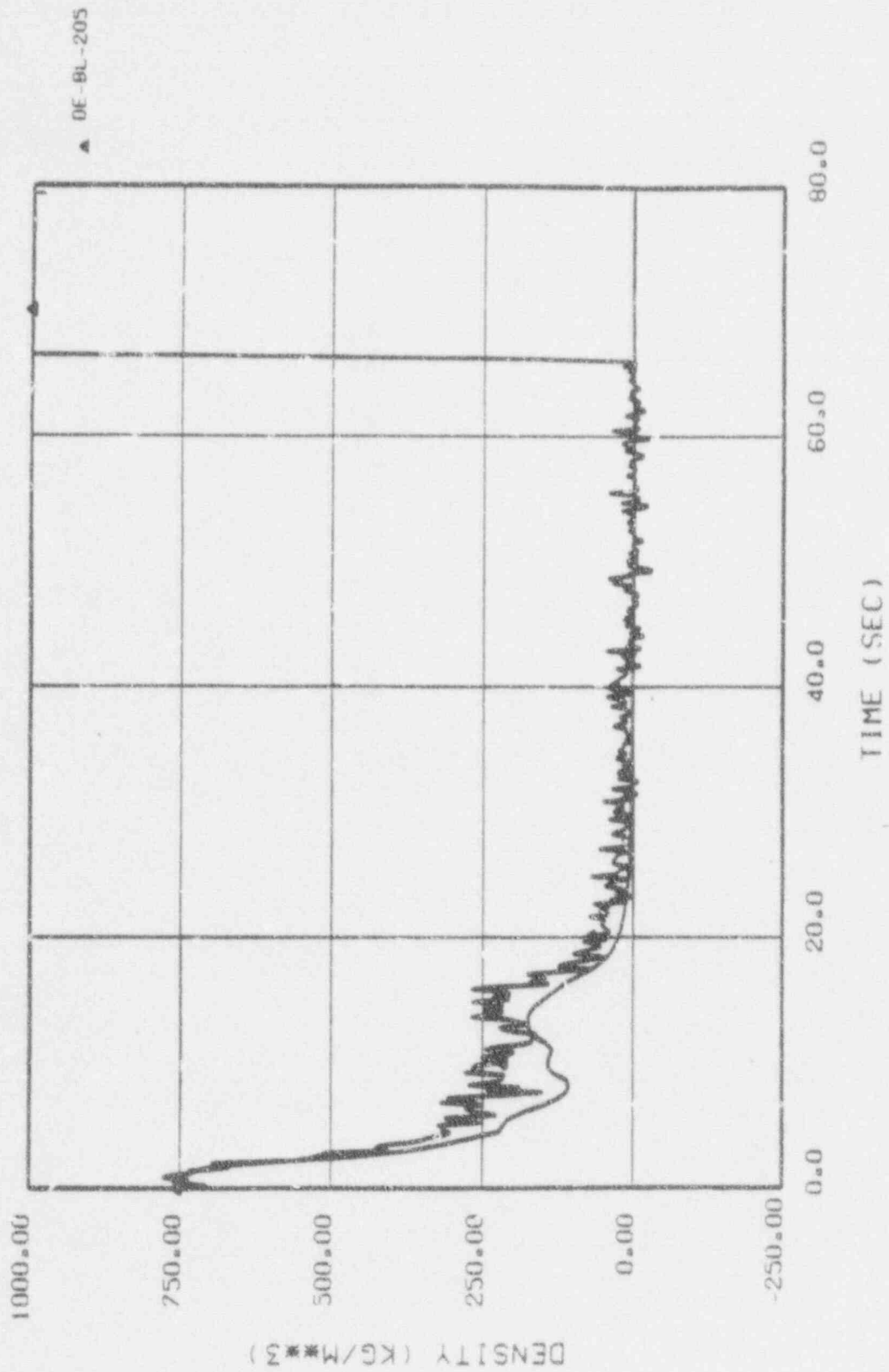
Figure 4.7. Intact loop cold leg (cell 2) density



BLCL - CELL 1

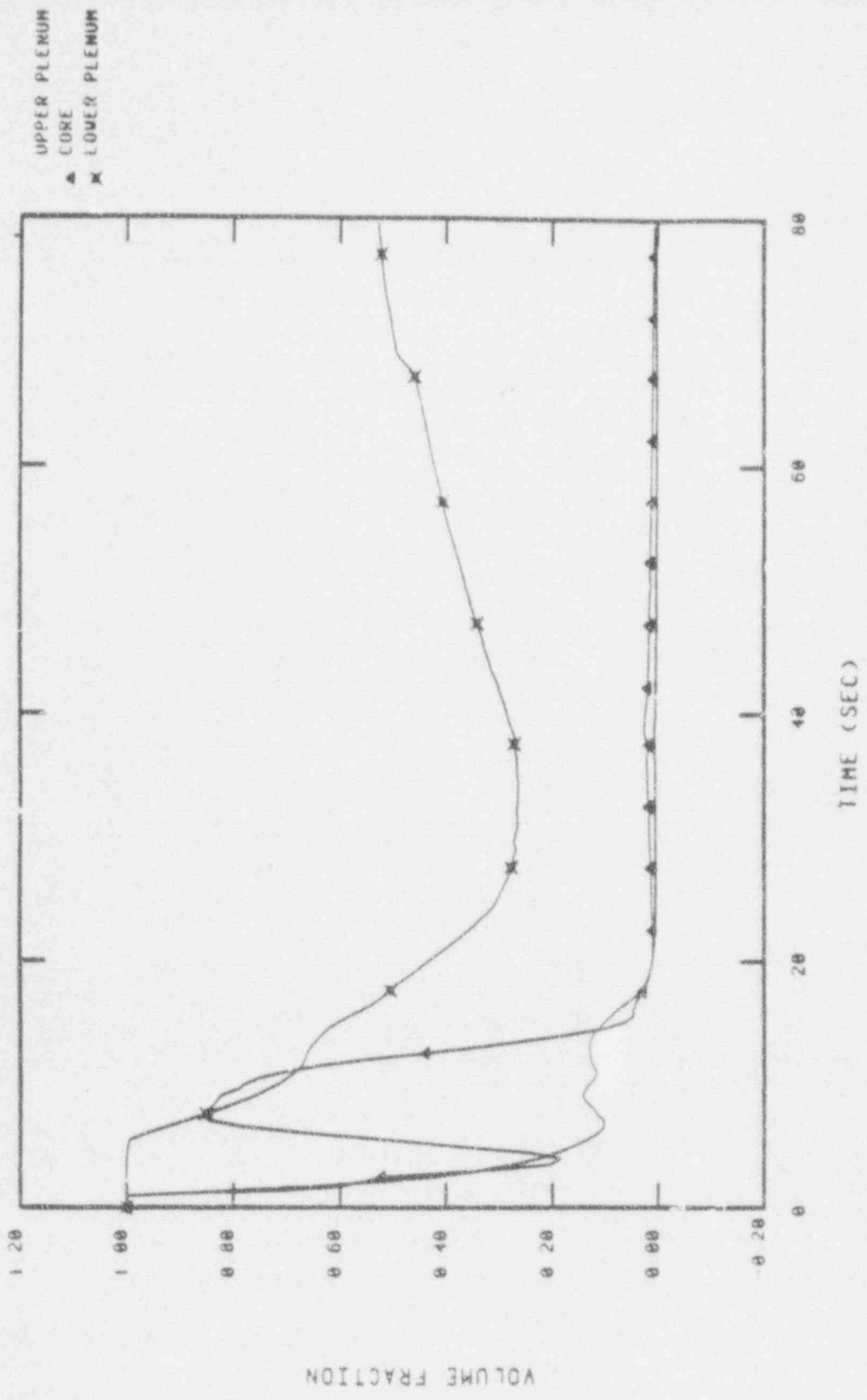
FIGURA

Figure 4.8. Broken loop cold leg (cell 1) density



BLHL - CELL 3

Figure 4.9. Broken loop ..ot 'g (cell 3) density



LIQUID VOLUME FRACTION

Figure 4.10. Vessel liquid fraction

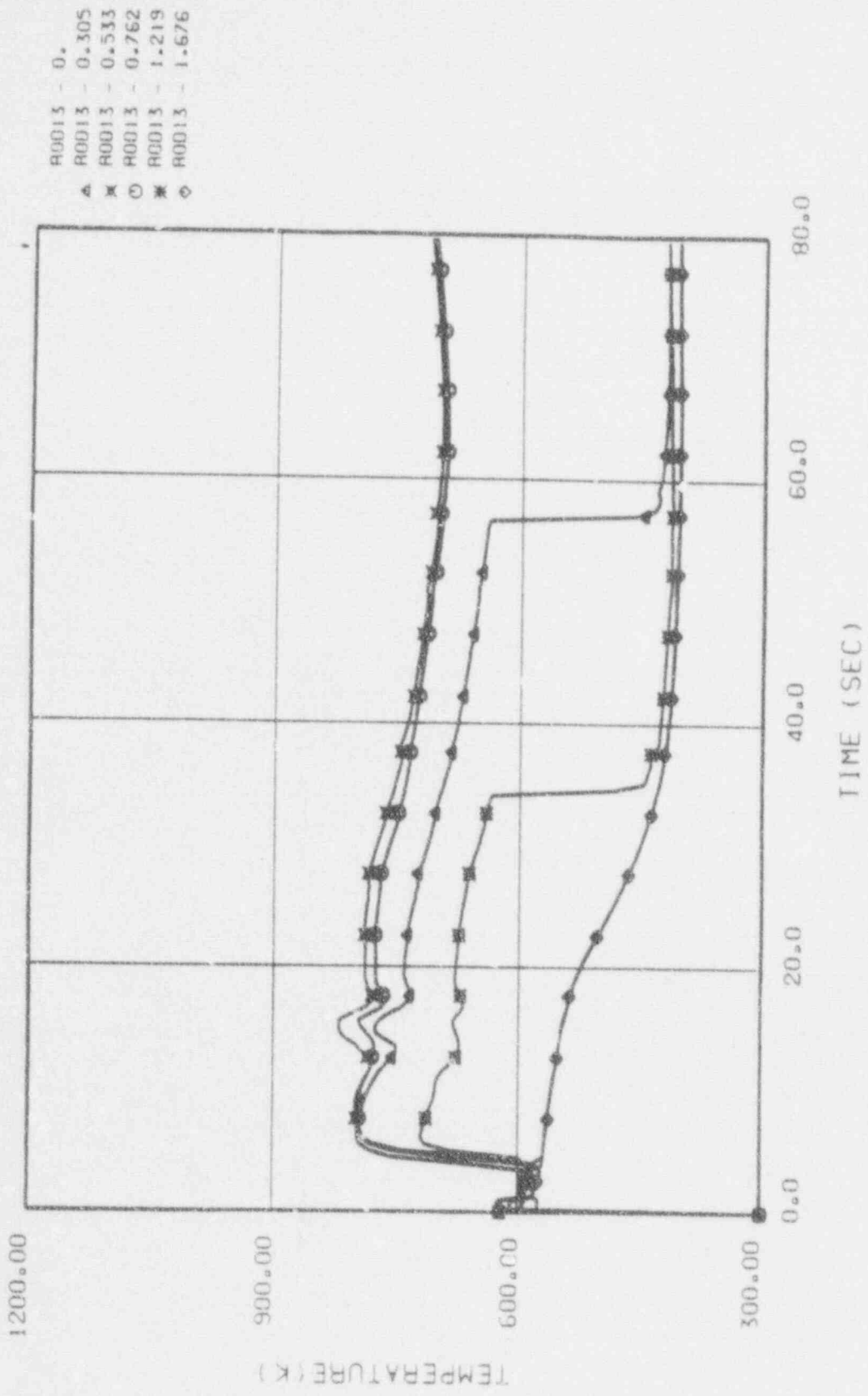


Figure 4.11. Simulated 6% rod 13 at several heights during blowdown phase

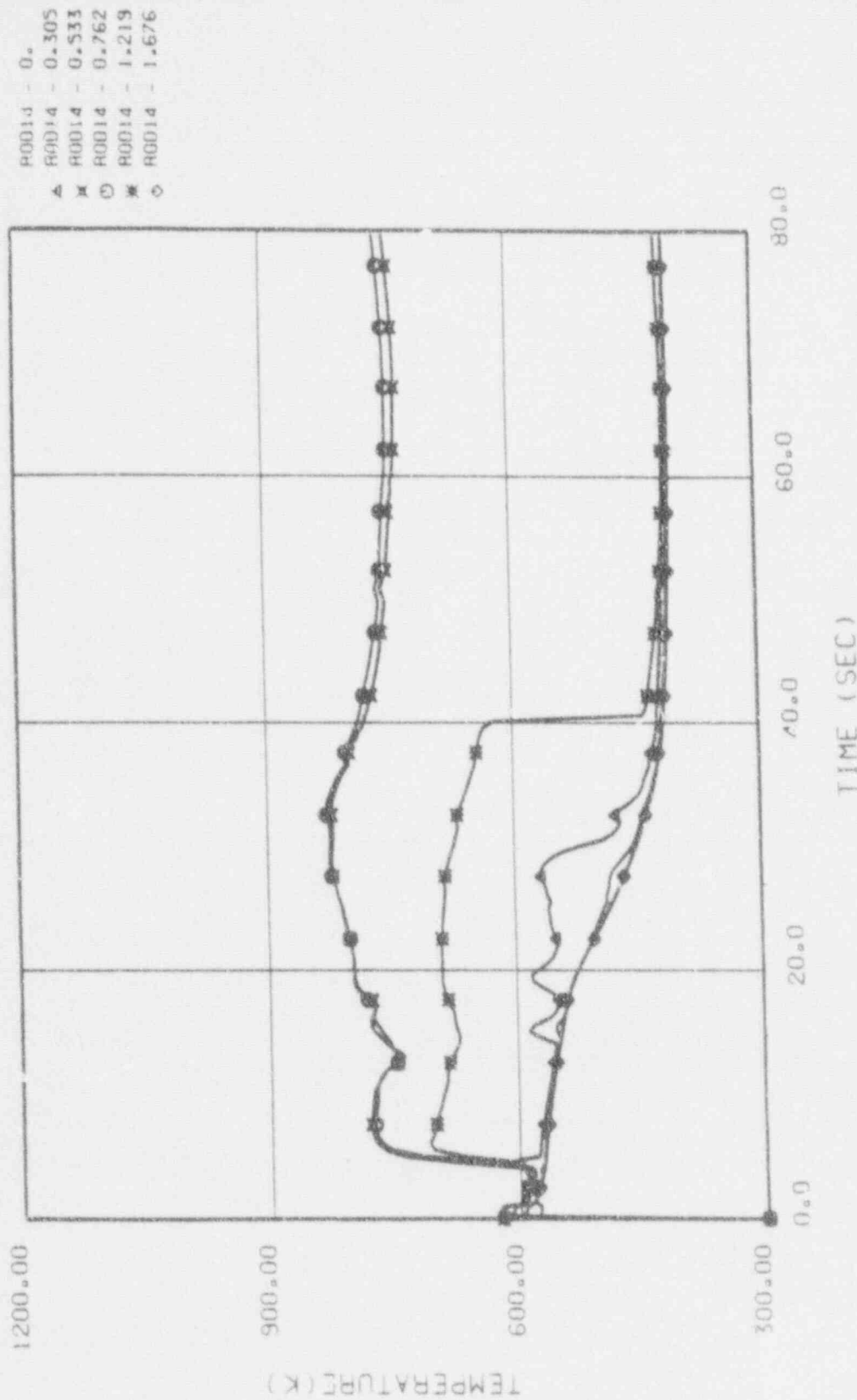


Figure 4.12. Simulated 6% rod 14 at several heights during blowdown phase

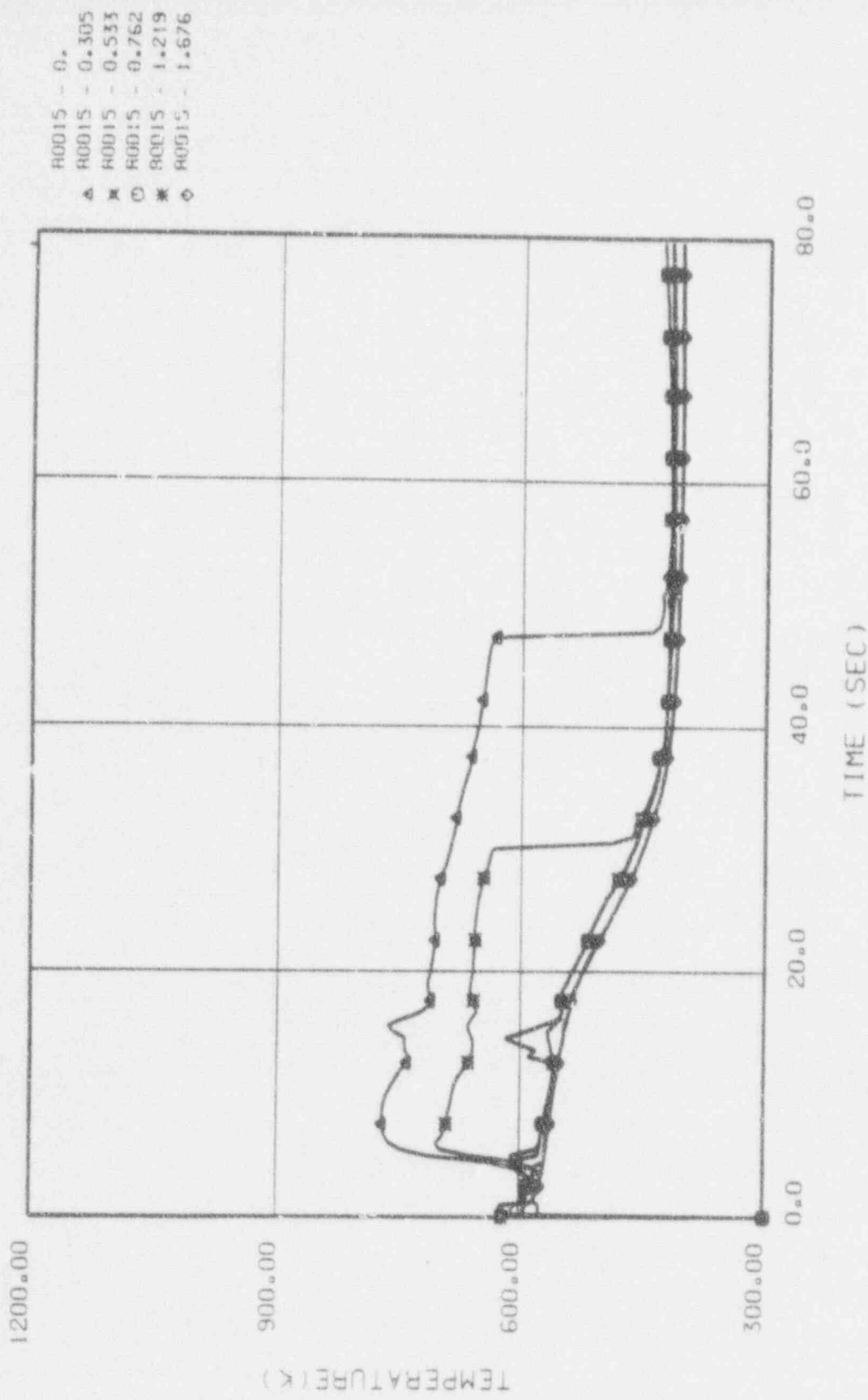


Figure 4.13. Simulated 6% rod 15 at several heights during blowdown phase

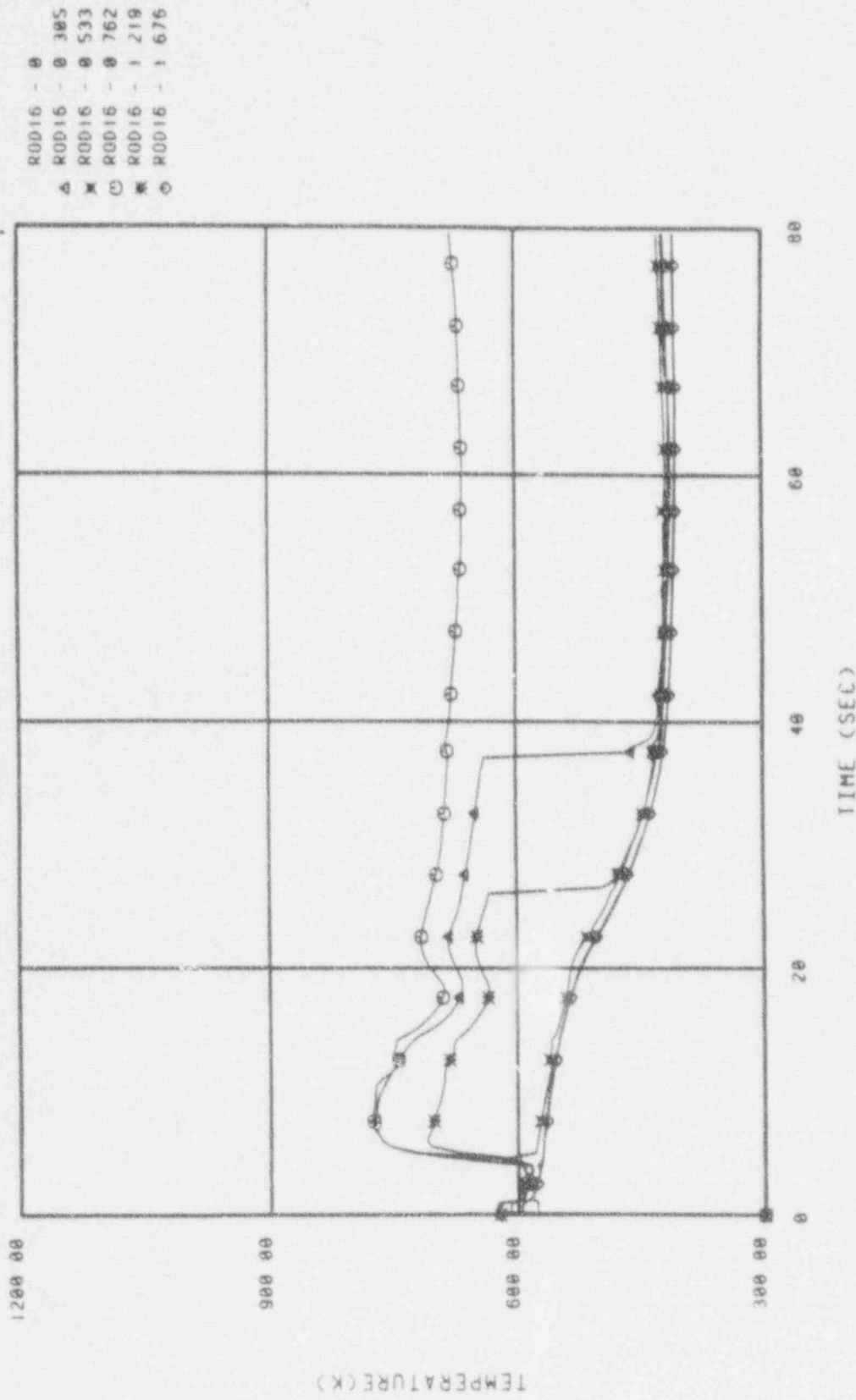


Figure 4.14. Simulated 6 x rod 16 at several heights during blowdown phase

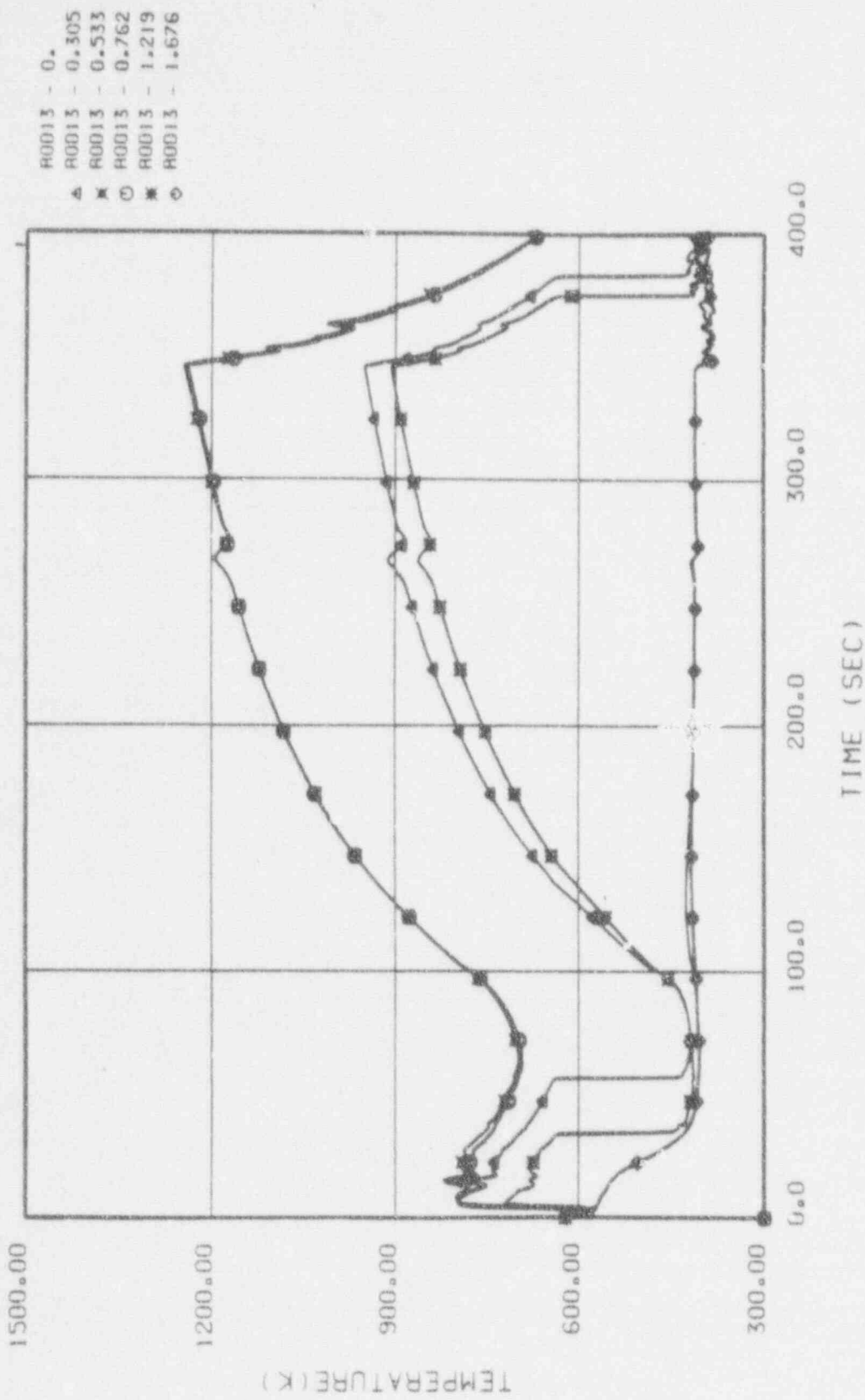


Figure 4.15. Simulated 6 X rod 13 at several heights during the whole transient

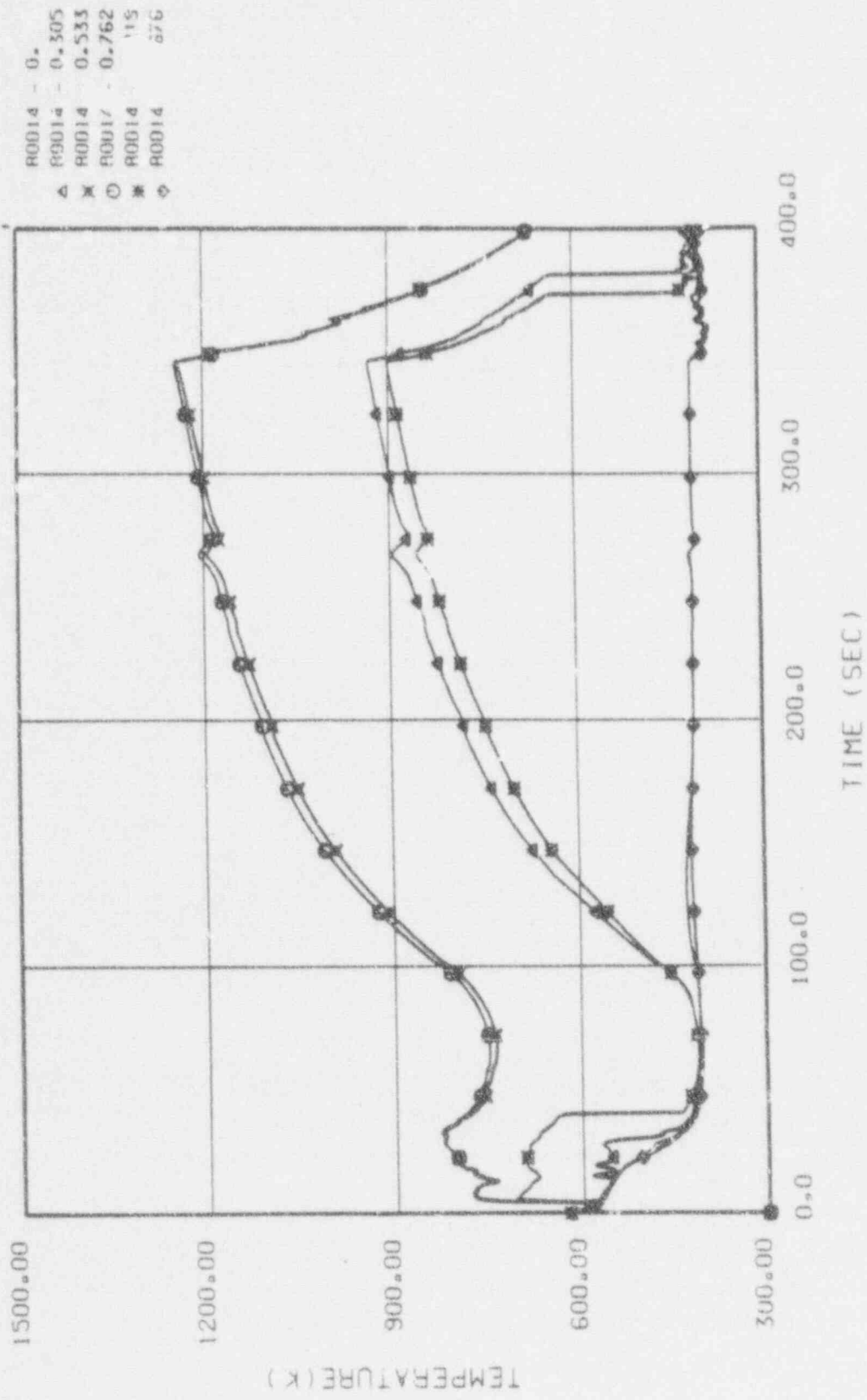


Figure 4.16. Simulated 6 1/2 rod 14 at several heights during the whole transient

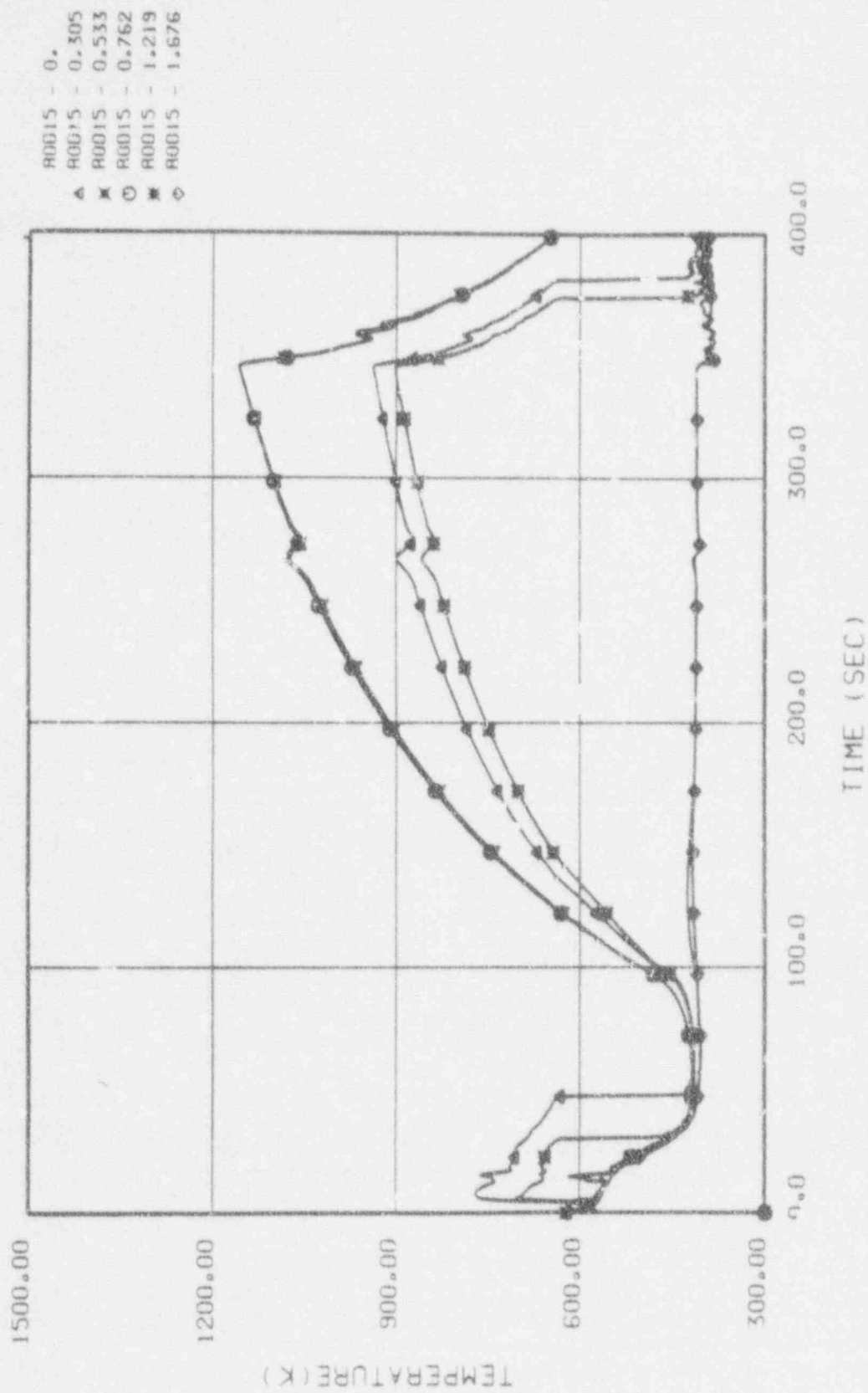


Figure 4.17. Simulated 6 1/2 rod 15 at several heights during the whole transient

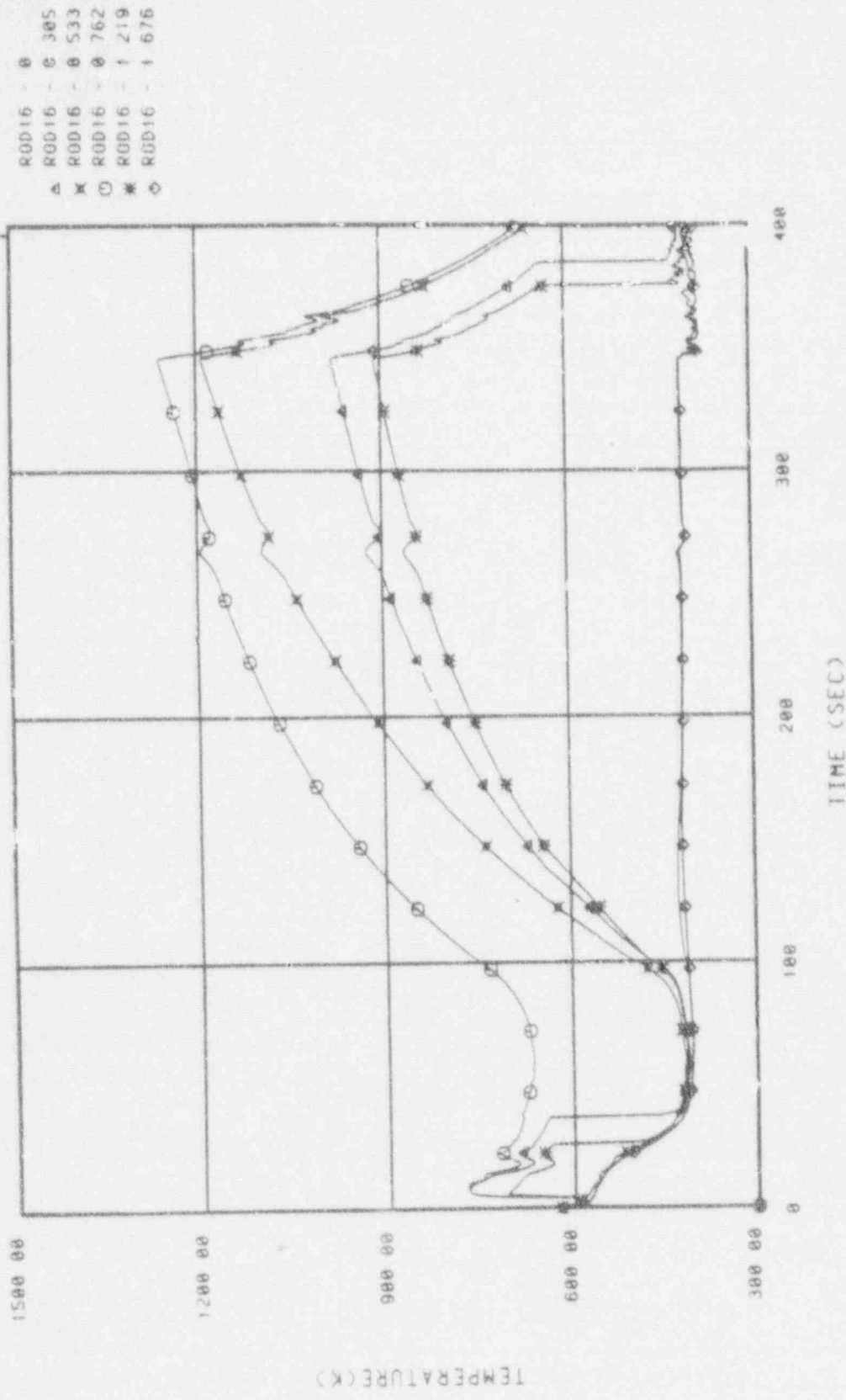


Figure 4.18. Simulated 6 % rod 16 at several heights during the whole transient

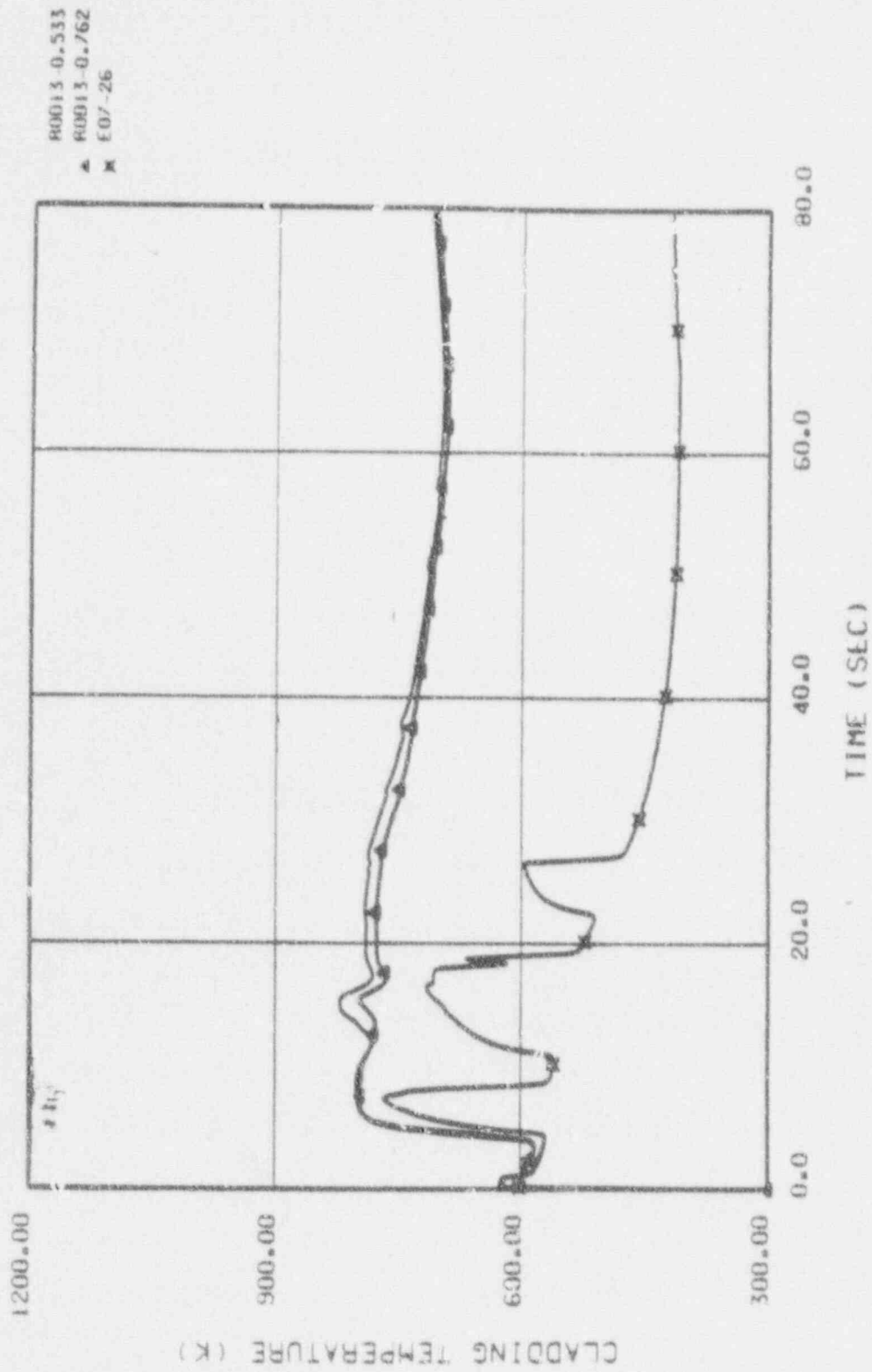


Figure 4.19. Comparison with thermocouple 5E07 (blowdown)

R0013-0.533
R0013-0.752
E07-26

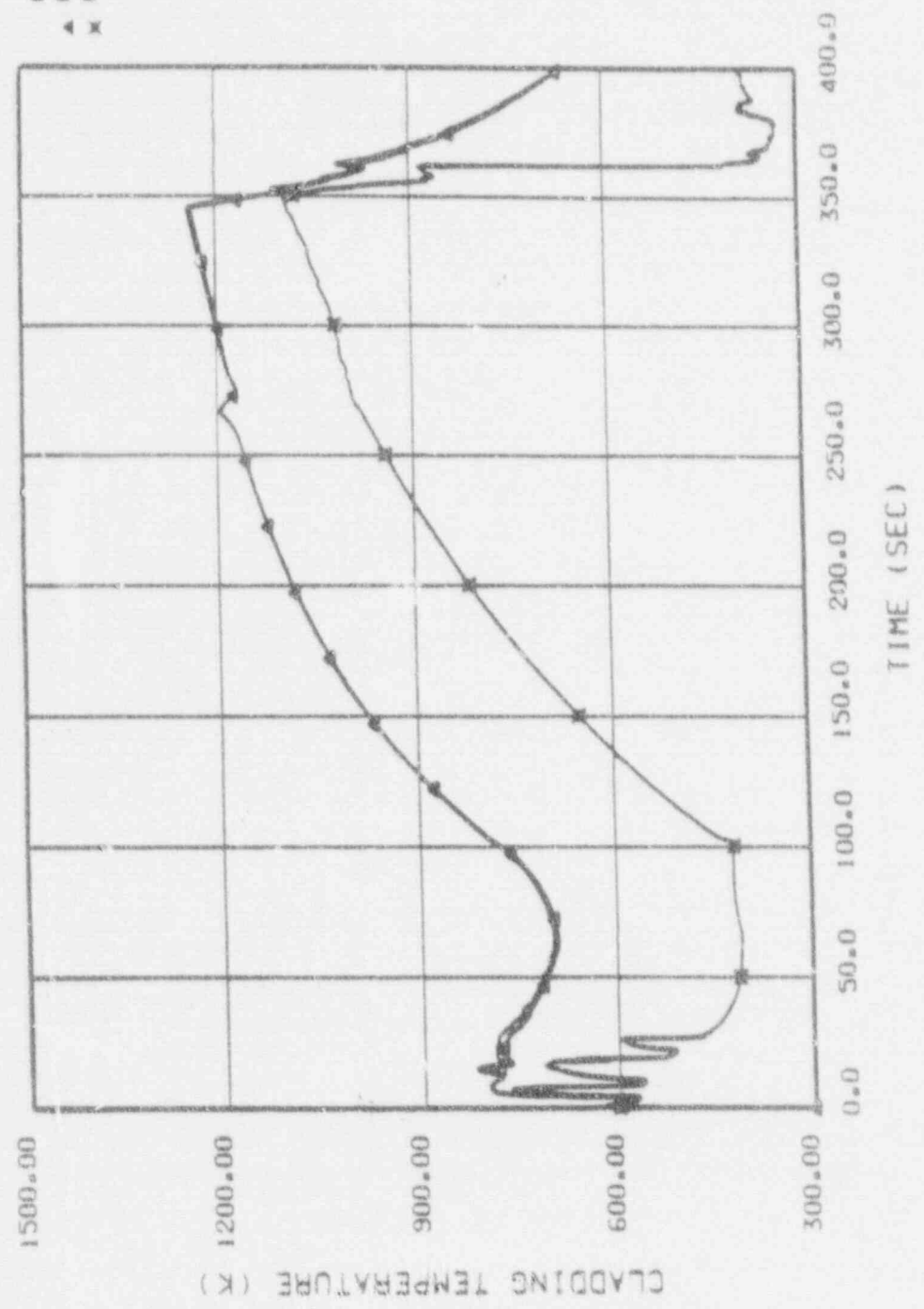


Figure 4.20. Comparison with thermocouple 5E07 (transient)

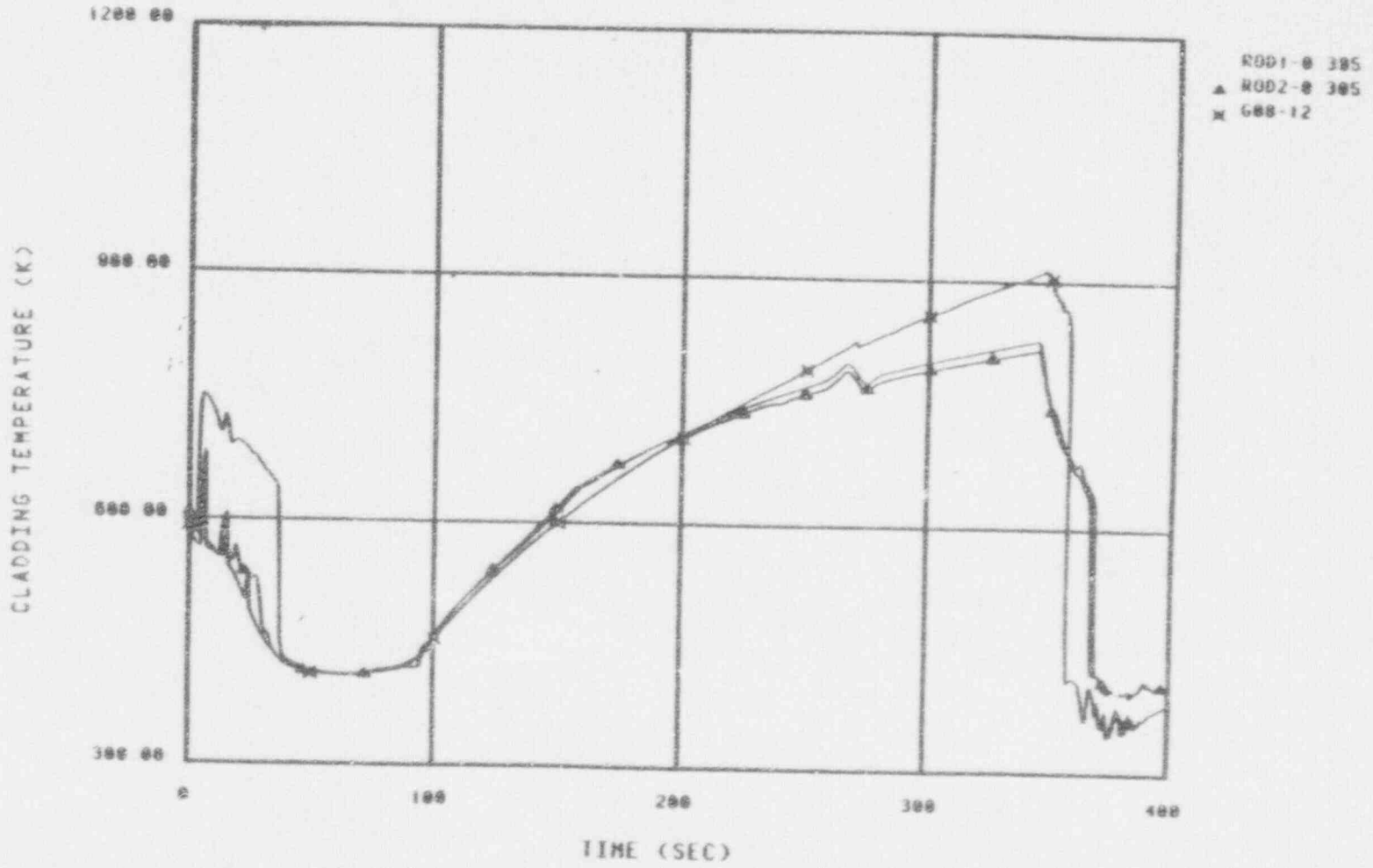


Figure 4.21. Cladding temperatures calculated for 5G08 (4 % fuel rod in central element)

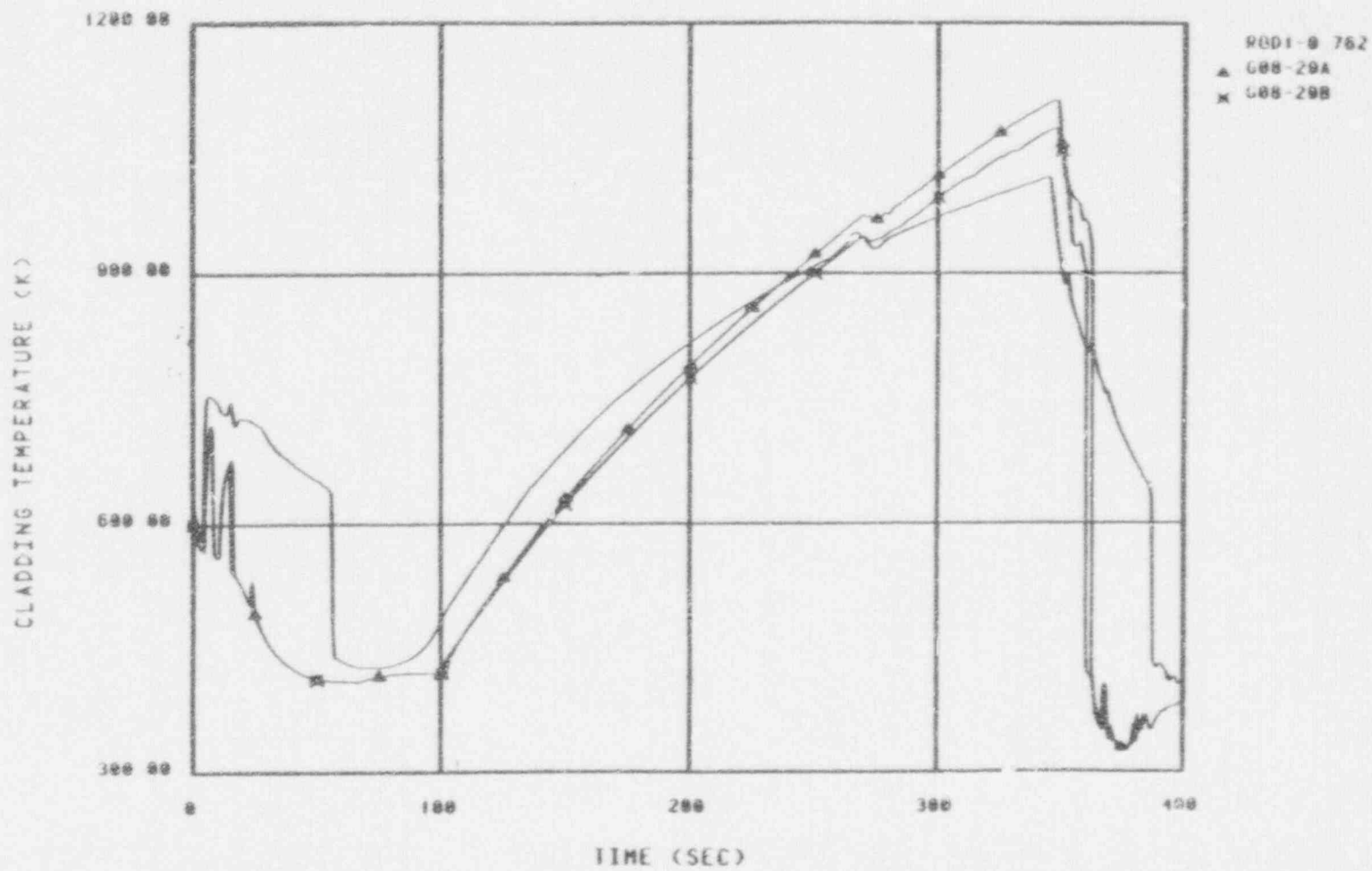


Figure 4.22. Cladding temperatures calculated for 5G08
(4 % fuel rod in central element)

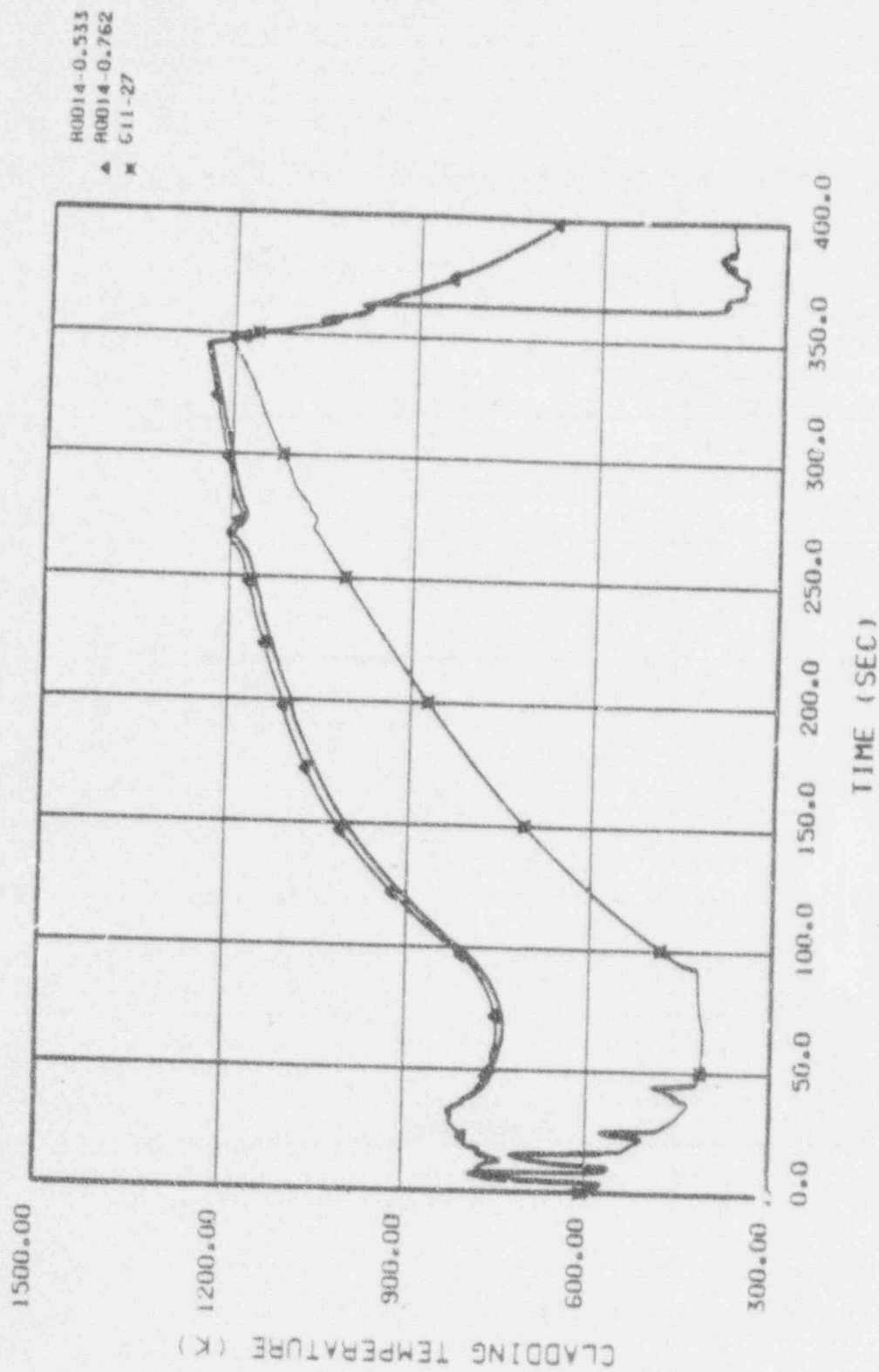


Figure 4.23. Cladding temperatures calculated for 5C11 (6% ruptured fuel rod)

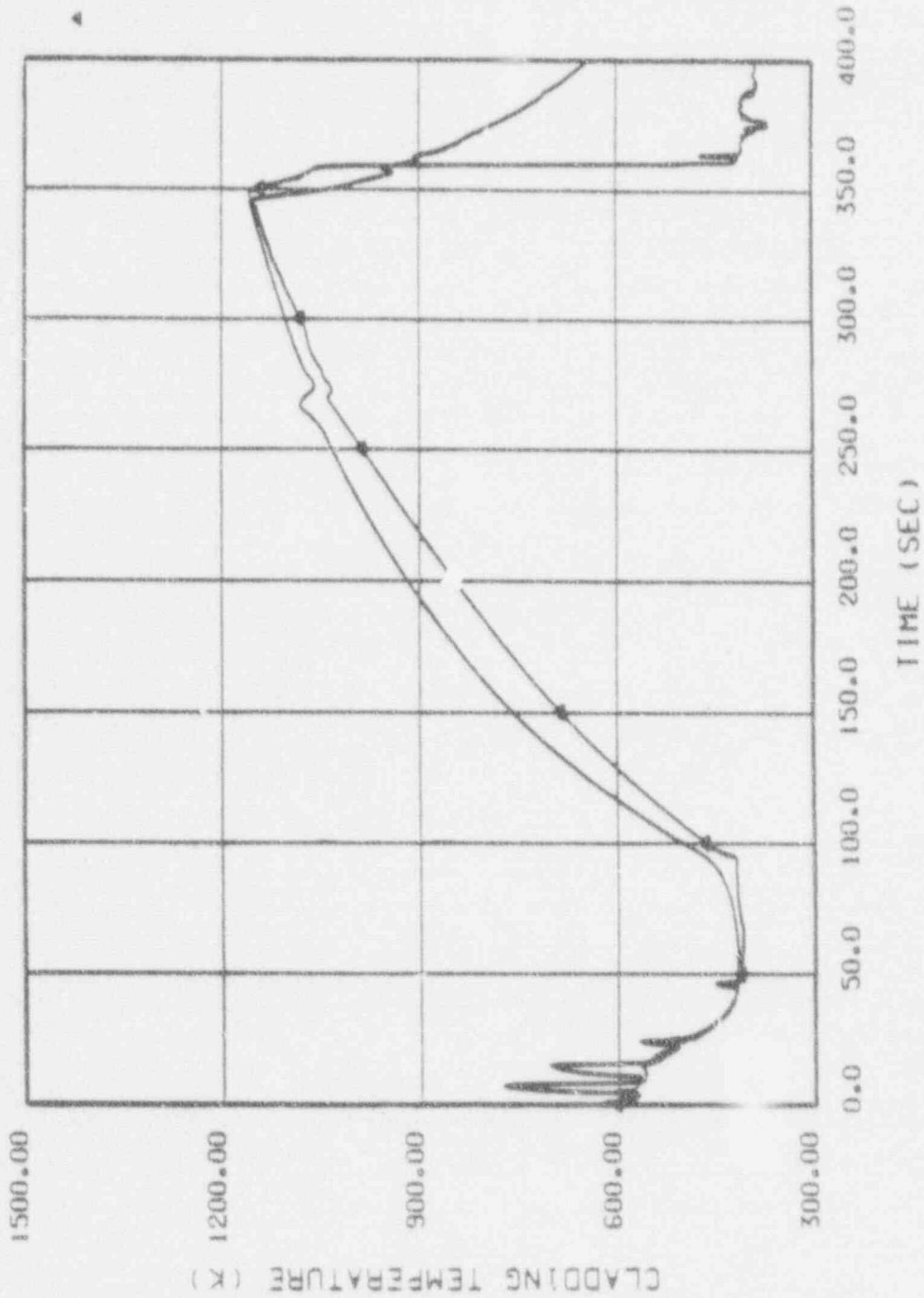


Figure 4.24. Cladding temperatures calculated for 5111 (6% ruptured fuel rod)

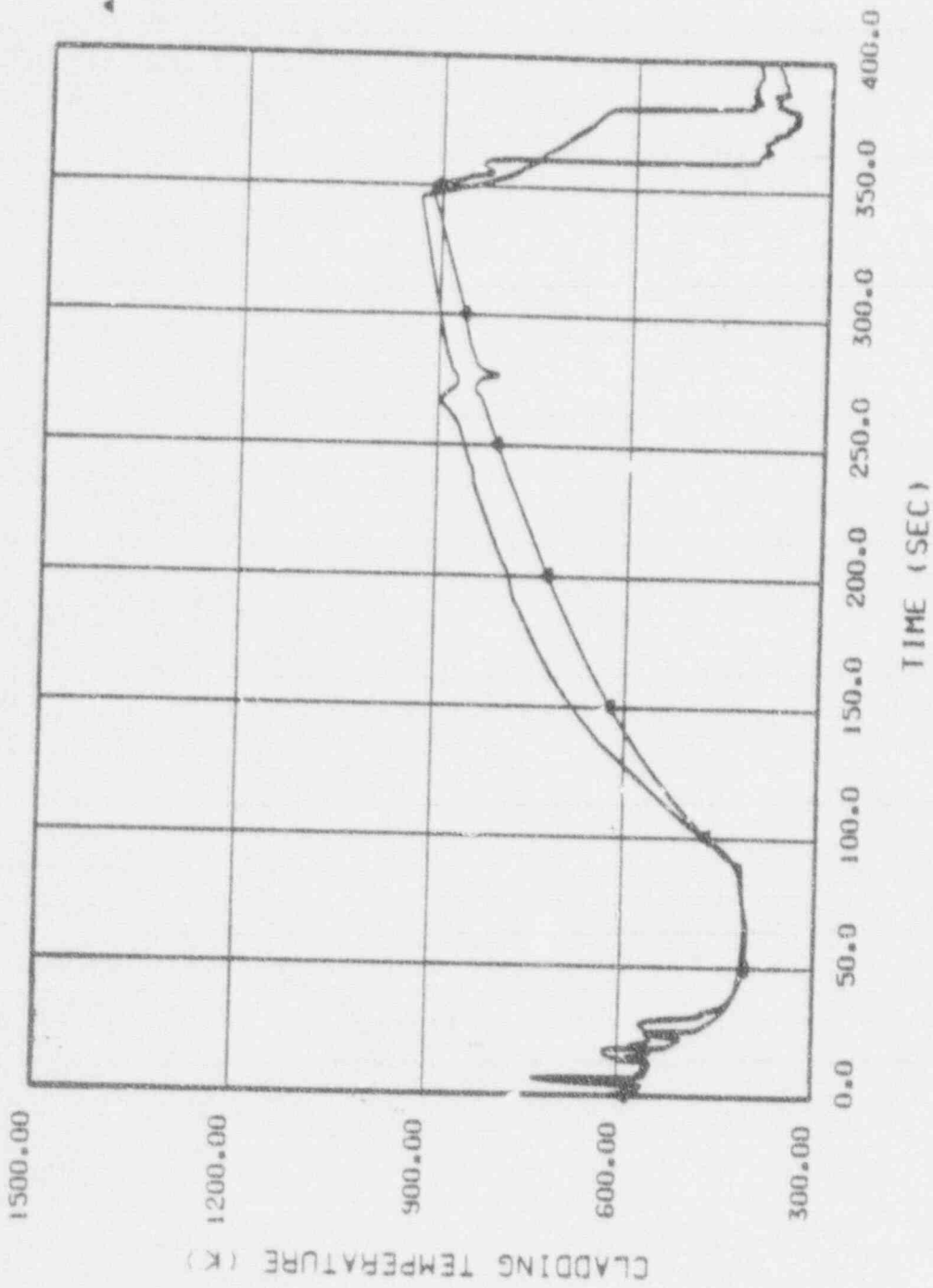


Figure 4.25. Cladding temperatures calculated for 5E09 (6% ruptured fuel rod)

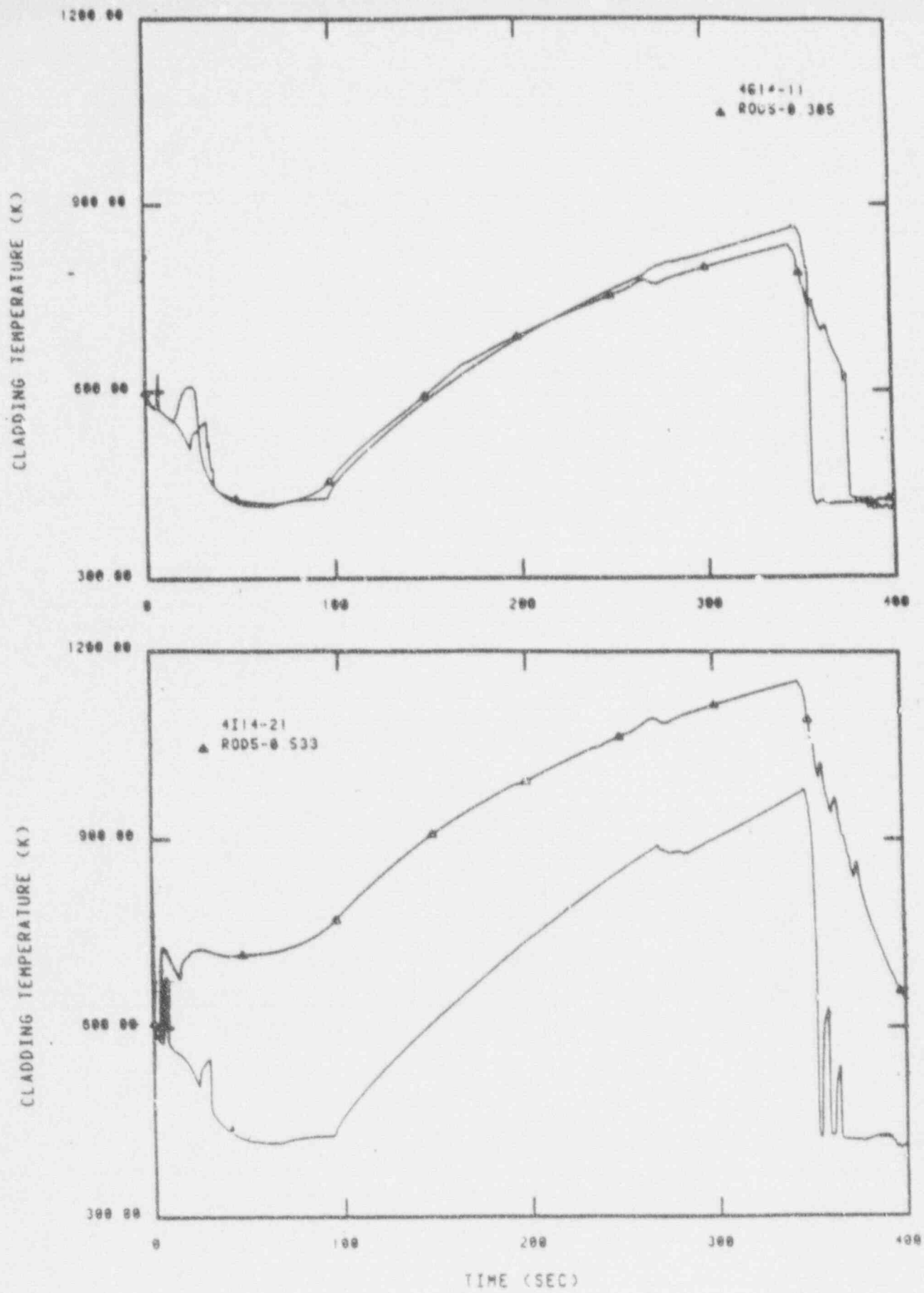


Figure 4.26. Cladding temperatures calculated for fuel rods in peripheral bundles

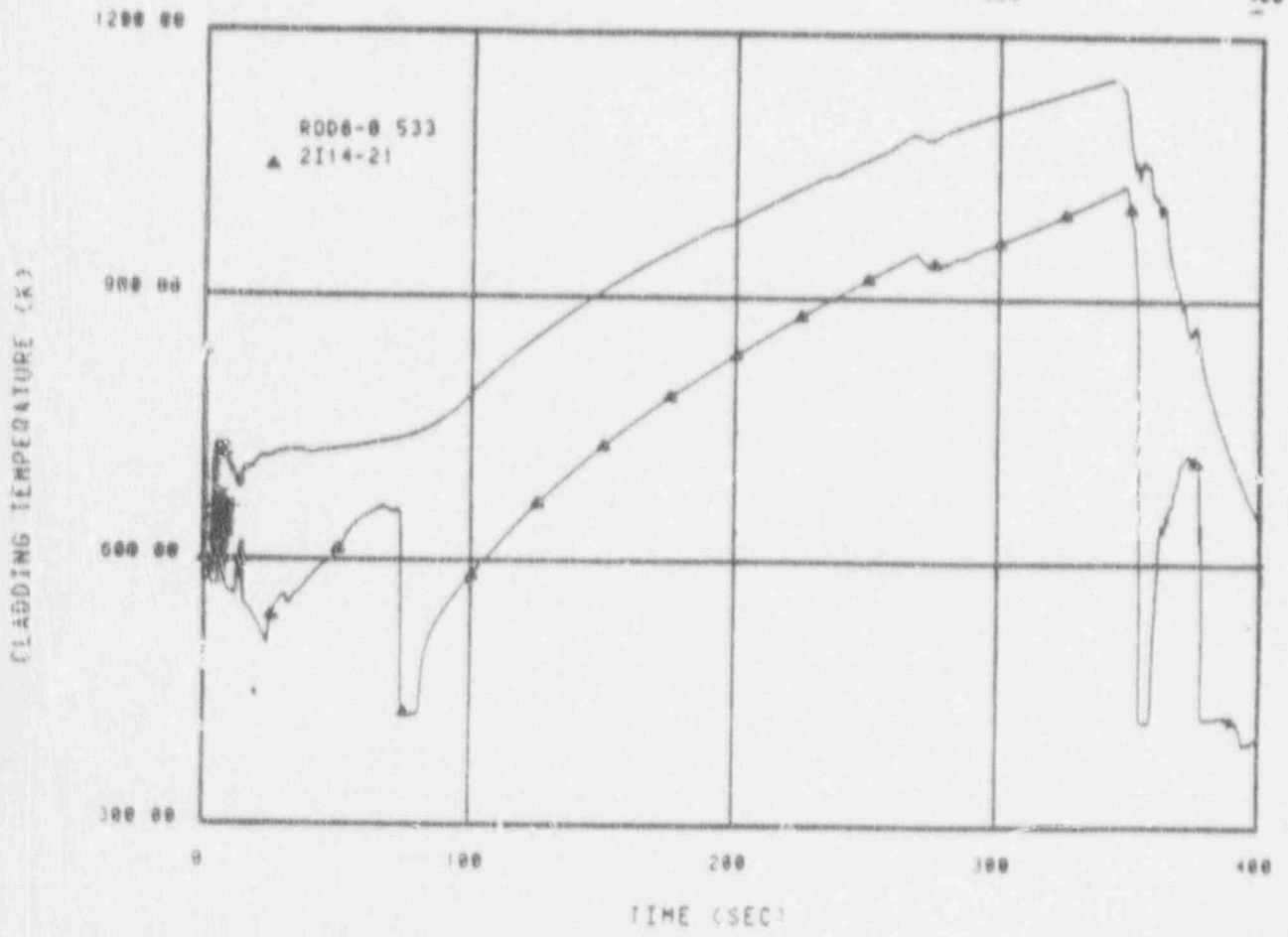
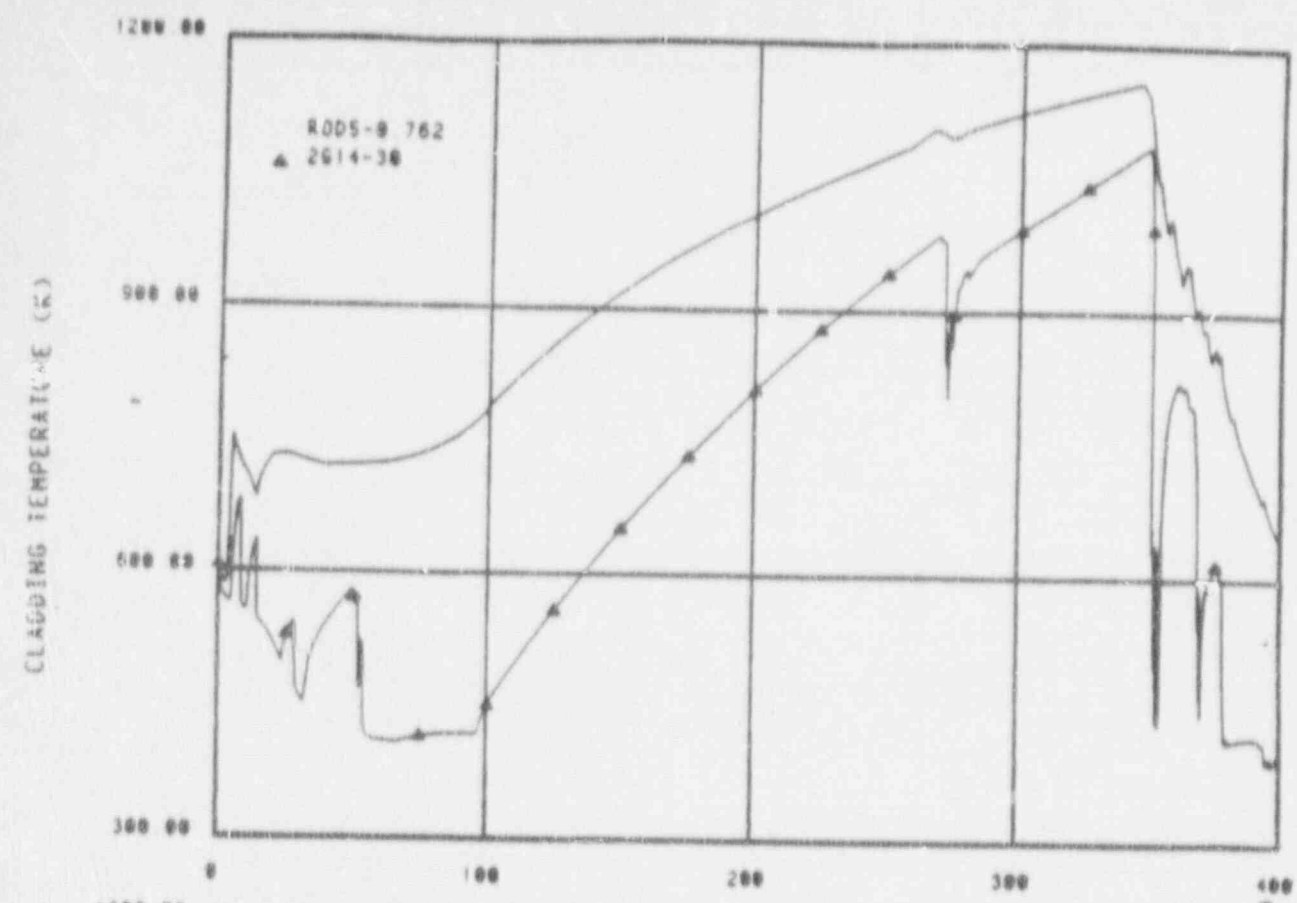


Figure 4.26. Cladding temperatures calculated for fuel rods in peripheral bundle 2

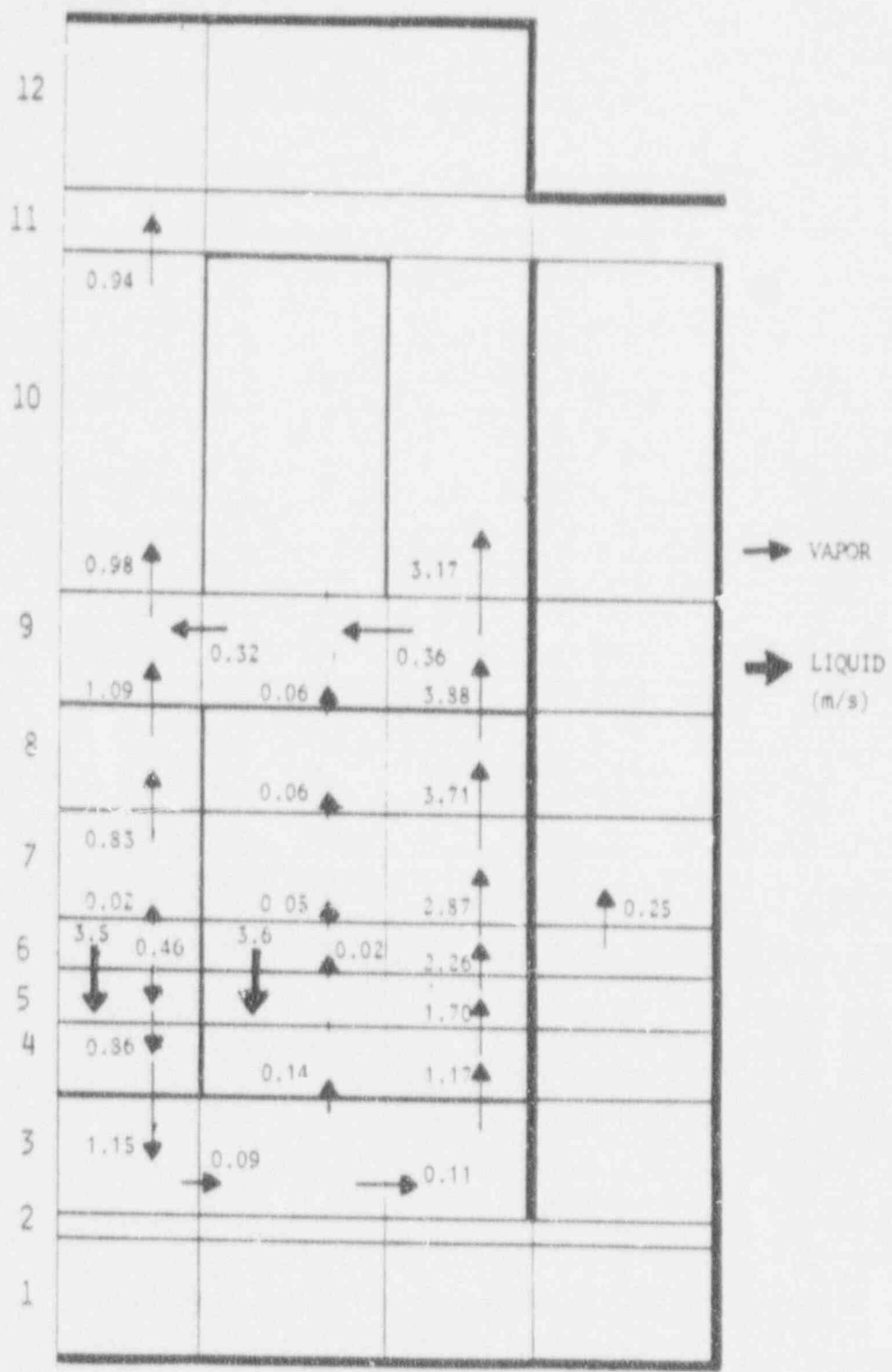


Figure 4.27. Flow patterns in vessel during rupture phase

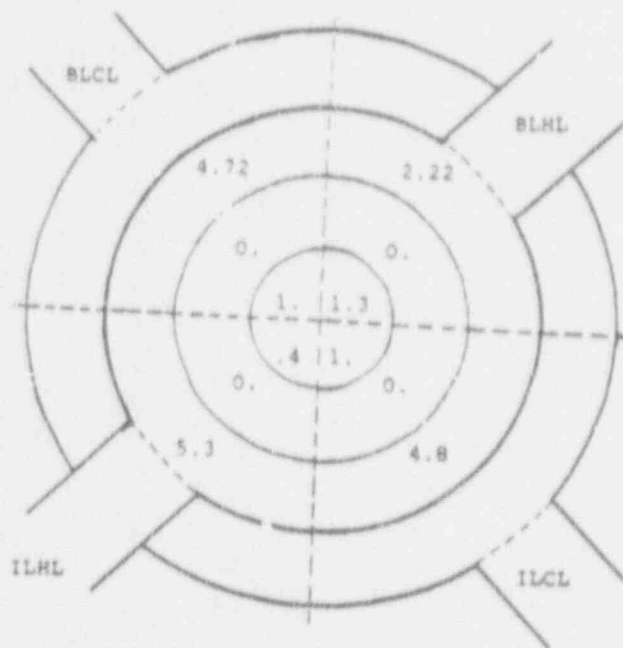


Figure 4.28. Vapor axial velocity (m/s) from level 10 to 11 during rod rupture phase

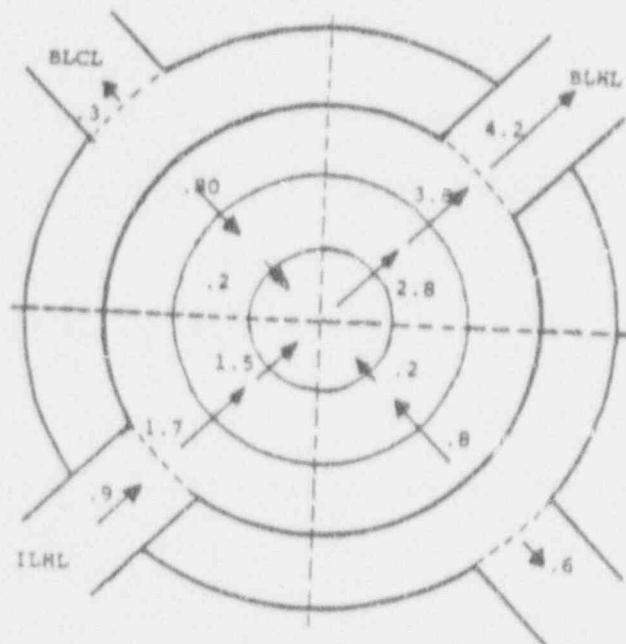
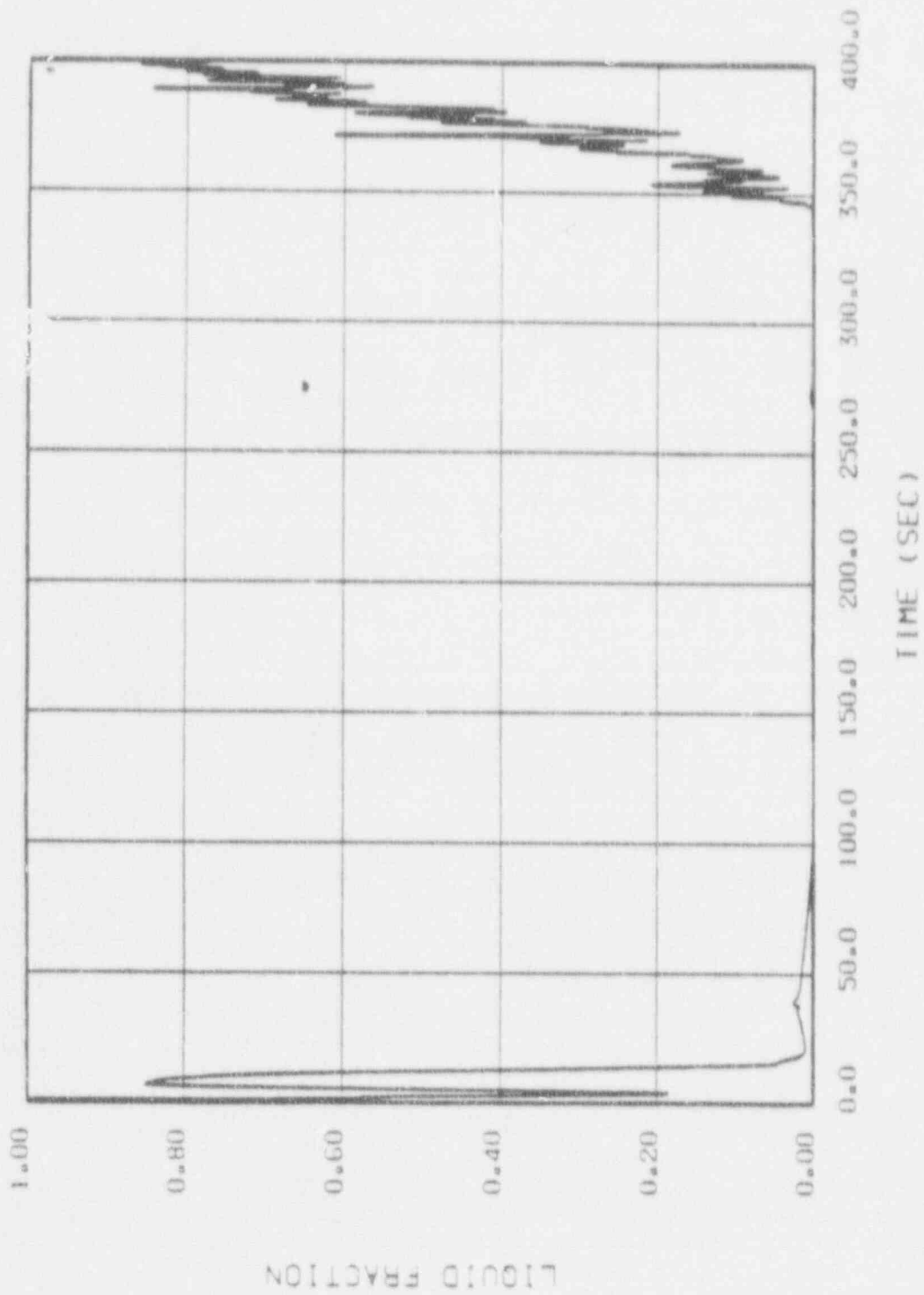


Figure 4.29. Vapor radial velocity (m/s) in level 11 during rod rupture phase



CORE

Figure 4.30. Liquid fraction in core

5. RUN STATISTICS

In the nodalization defined we have used the following
number of cells:

- Vessel and core 192
- Intact loop 54
- Broken loop 37
- Steam generator
 (secondary side) 19

Total number of cells = 302

Minimum and maximum time steps selected were:

Range (s)	DTMIN (s)	DTMAX (s)
0 - 1	1.E-5	1.E-3
1 - 5	1.E-5	1.E-2
5 - 345	1.E-5	1.E-1

These maximum values haven't been reached in any phase as
may be seen in Fig 5.1, where the time step evolution along
the transient is shown.

Figure 5.2 reflects the cumulative CPU time used in calcu-
lating the transient. Clearly, we can distinguish two phases
according to the time steps selected by the code:

Phase	Range (s)	Number steps	CPU time (s)	RS
Blowdown & Heat-up	0 - 345	21500	624E3	96.1
Reflood	345 - 400	16000	576E3	119.2

The last column, named RS, represents the calculated run statistics (CPU time in ms per cell and time step) in units of ms/(cell*step).

Machine used for this calculation was CDC Cyber (operating system NOC-BE) with reserved Core Memory = 376500 and Extended Memory = 500.

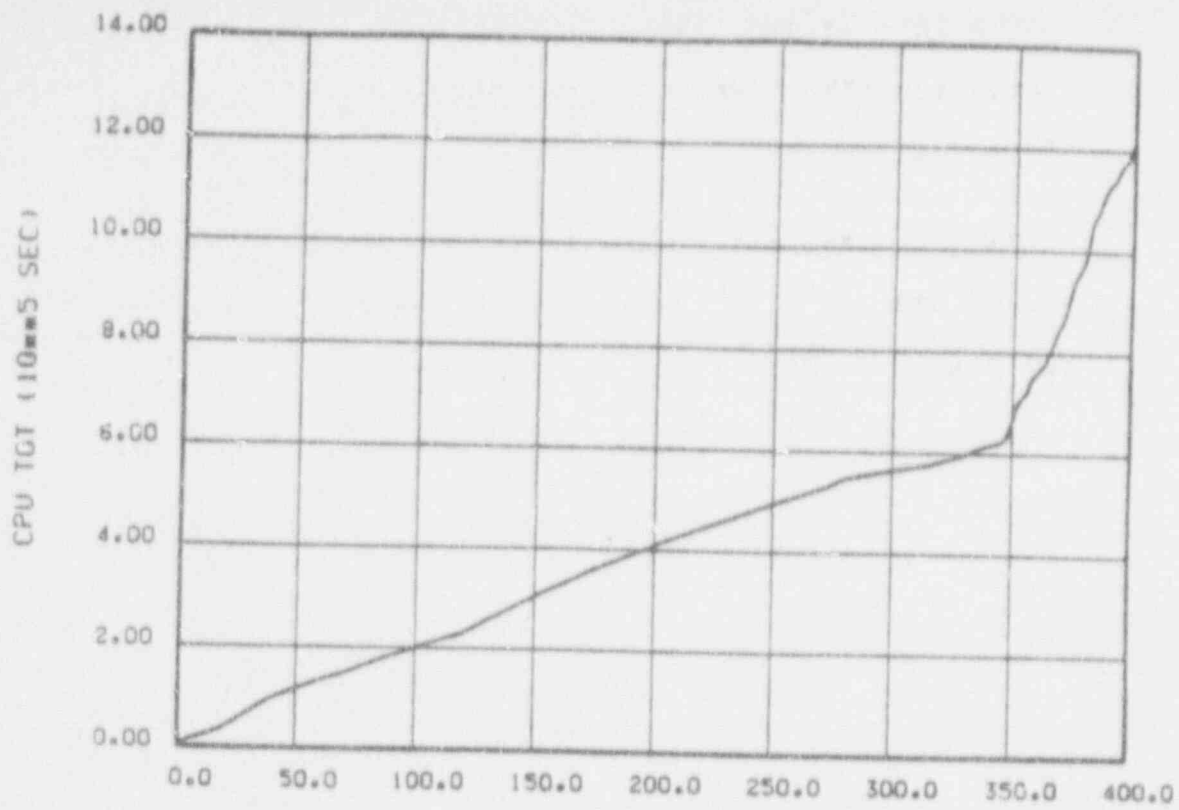


Figure 5.2. Accumulated CPU time

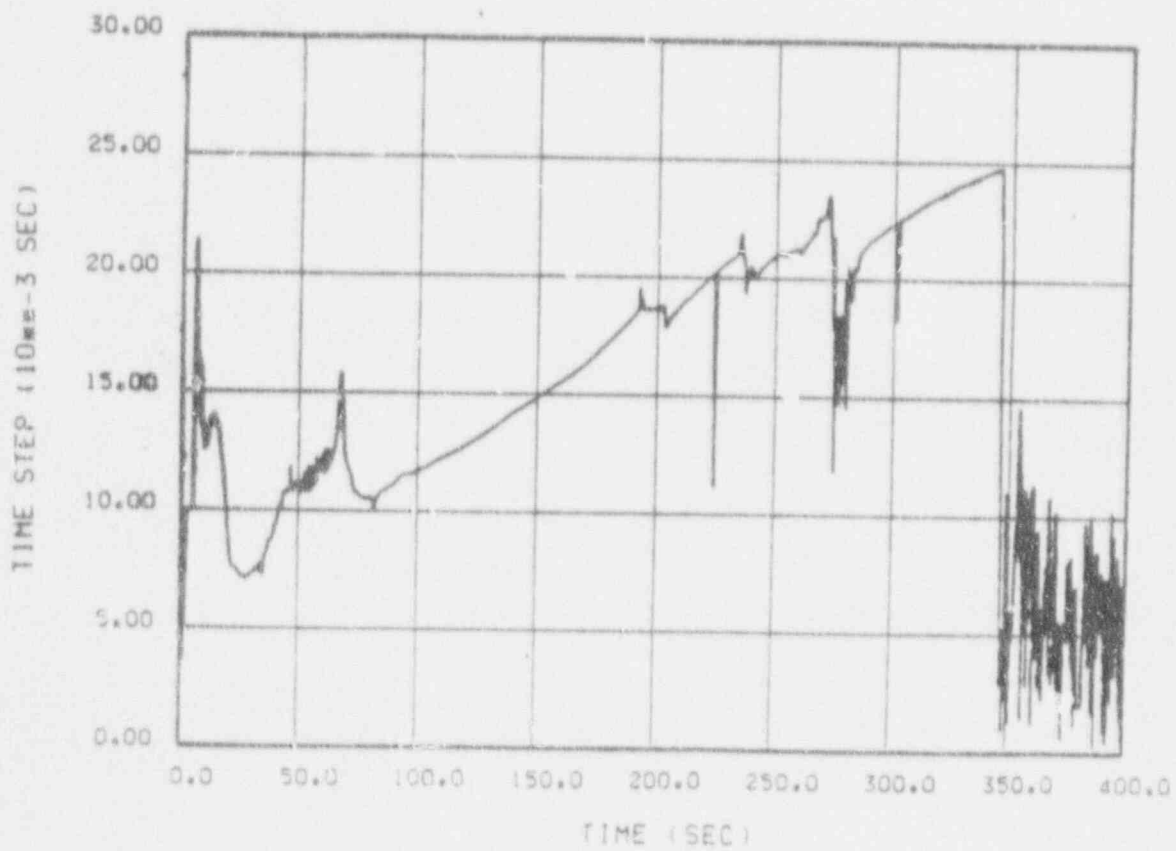


Figure 5.1. Time step evolution

6. CONCLUSIONS

1. Good agreement exists between calculated and experimental hydraulic variables during the blowdown, like pressure, mass flow rates and densities.
2. TRAC-PF1 cannot simulate observed initial quenches and final quench time. If these delays were consequence of an incorrect value of MSFBT, introducing a multiplicative correcting factor greater than 1.12 in the correlation for MSFBT (only for the FP-1 case), the experimental quench time can be reproduced.
3. Good agreement is found between calculated and measured cladding temperatures for the 4 % enriched rods in central fuel assembly.
4. Those simulated 6 % fuel rods which suffer quench during the blowdown phase (such as rod 15 in TRAC, close to ILCL), show the best fitting with thermocouple data. For the remaining 6 % and peripheral rods, higher temperatures are calculated in film boiling transfer regime.
5. Three-dimensional behaviour is calculated, although unplanned upper plenum injection was defined to be azimuthally symmetric within each ring.
6. Flow patterns during rod rupture period show two possible paths for fission products in a non-dry phase.

7. REFERENCES

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APENDIX A. LOFT system instrumentation

This section resumes the instrumentation nomenclature and location in the LOFT facility, contained in reference [5].

Figures show locations for the main instrumentation used for the FP-1 thermal-hydraulic study.

All experimental data plotted in this document are identified using the instrumentation nomenclature explained in Table A.1, which is also used for the related variables. The DIRC report resumed, shows the qualified and failed data in the experiment, recorded at 50 samples per second, except in the cases which are noted.

TABLE A.1. Nomenclature for LOFT instrumentation

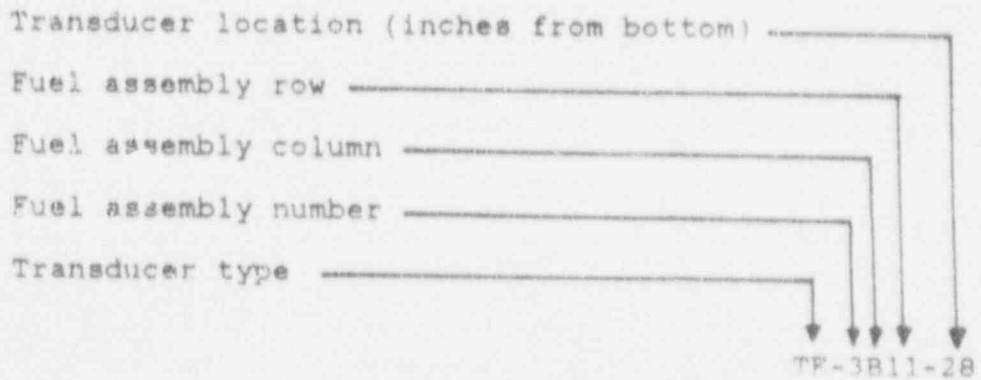
Designation for the different types of transducers

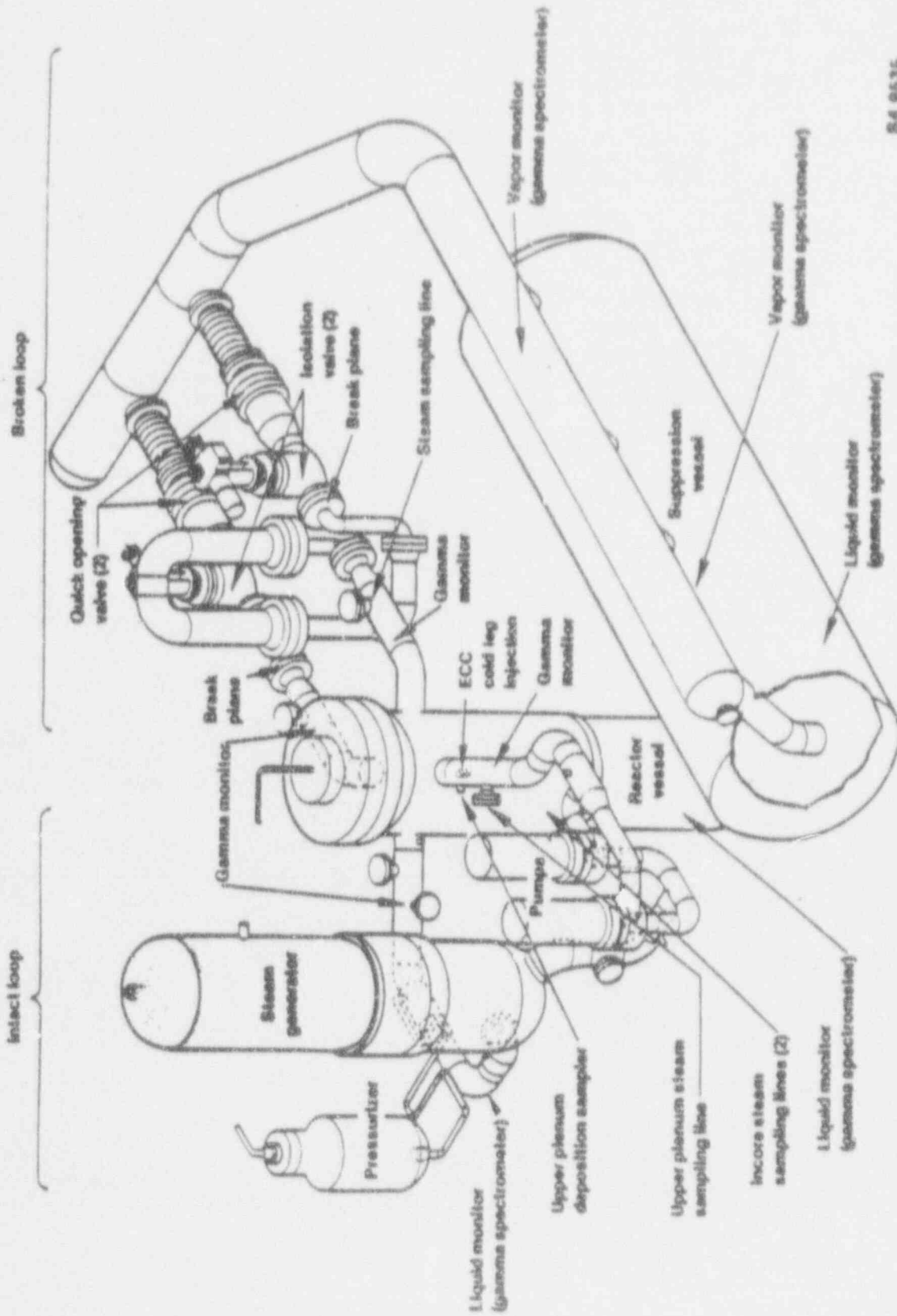
RPE - Pump speed	FE - Coolant flow
PE - Pressure transducer	DE - Densitometer
PdE - Differential pressure	ME - Momentum flux
LE - Coolant level	FT - Flow rate
PS - Pressure switch	TC - Fuel centerline
TE - Thermocouple	

Designation of systems

PC - Primary coolant intact	LP - Lower plenum
BL - Broken loop	ST - Downcomer stalk
RV - Reactor vessel	UP - Upper plenum
P120 - Emergency core coolant system	P128 - Primary coolant addition and control

Designation for Core instrumentation





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Figure A-1. LOFT Major Components

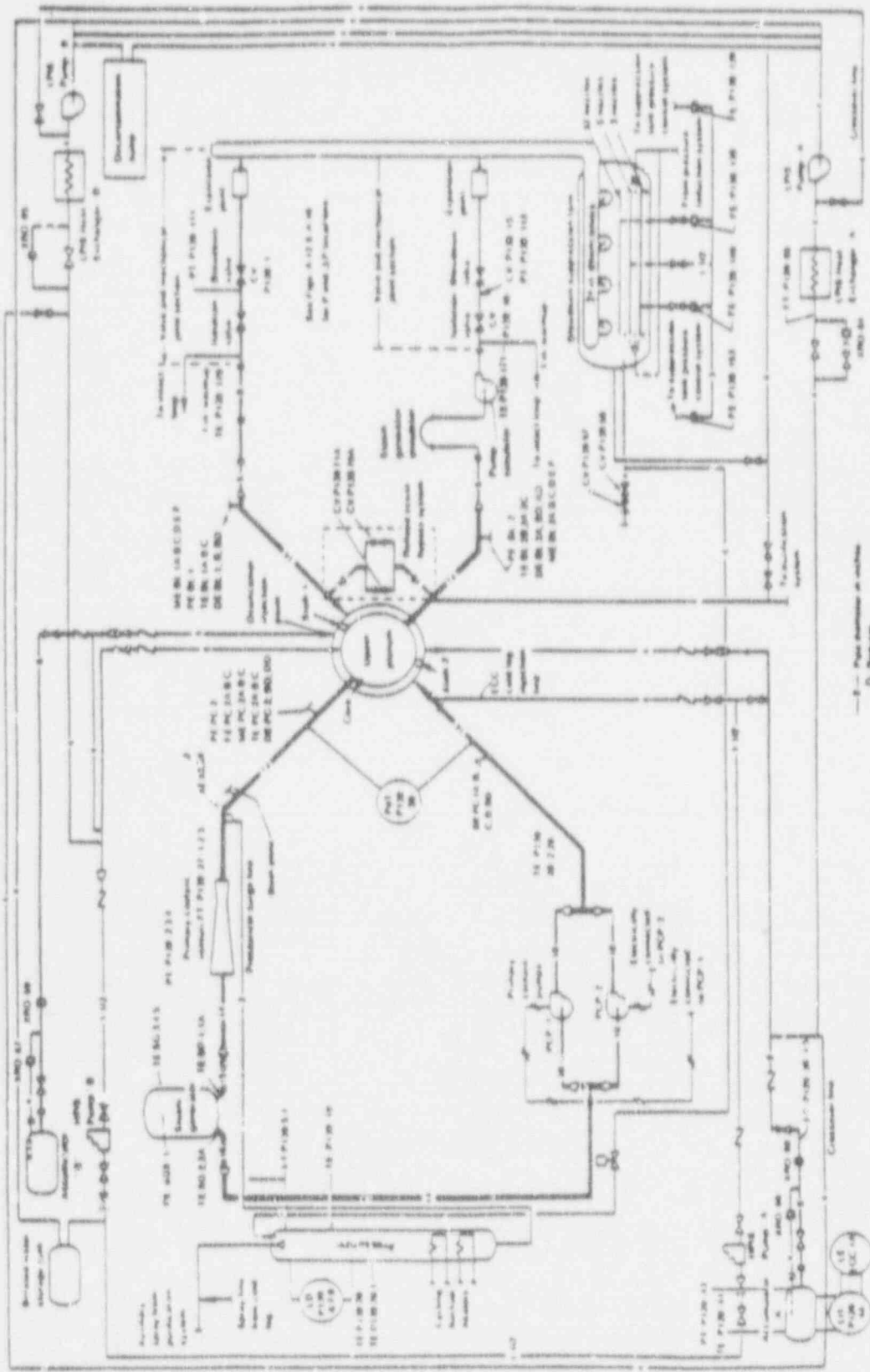


Figure A-2. LOFT Piping Schematic with Instrumentation

Process instrumentation for the containment vessel (not shown) includes containment pressure (PT-P139-41, 42 and 43), containment temperature (TE-T55-2), and hydrogen concentration (AH2E-T55-1,2,3). Specific instrumentation for the pressurizer and steam generator is found on their respective drawings in this set.

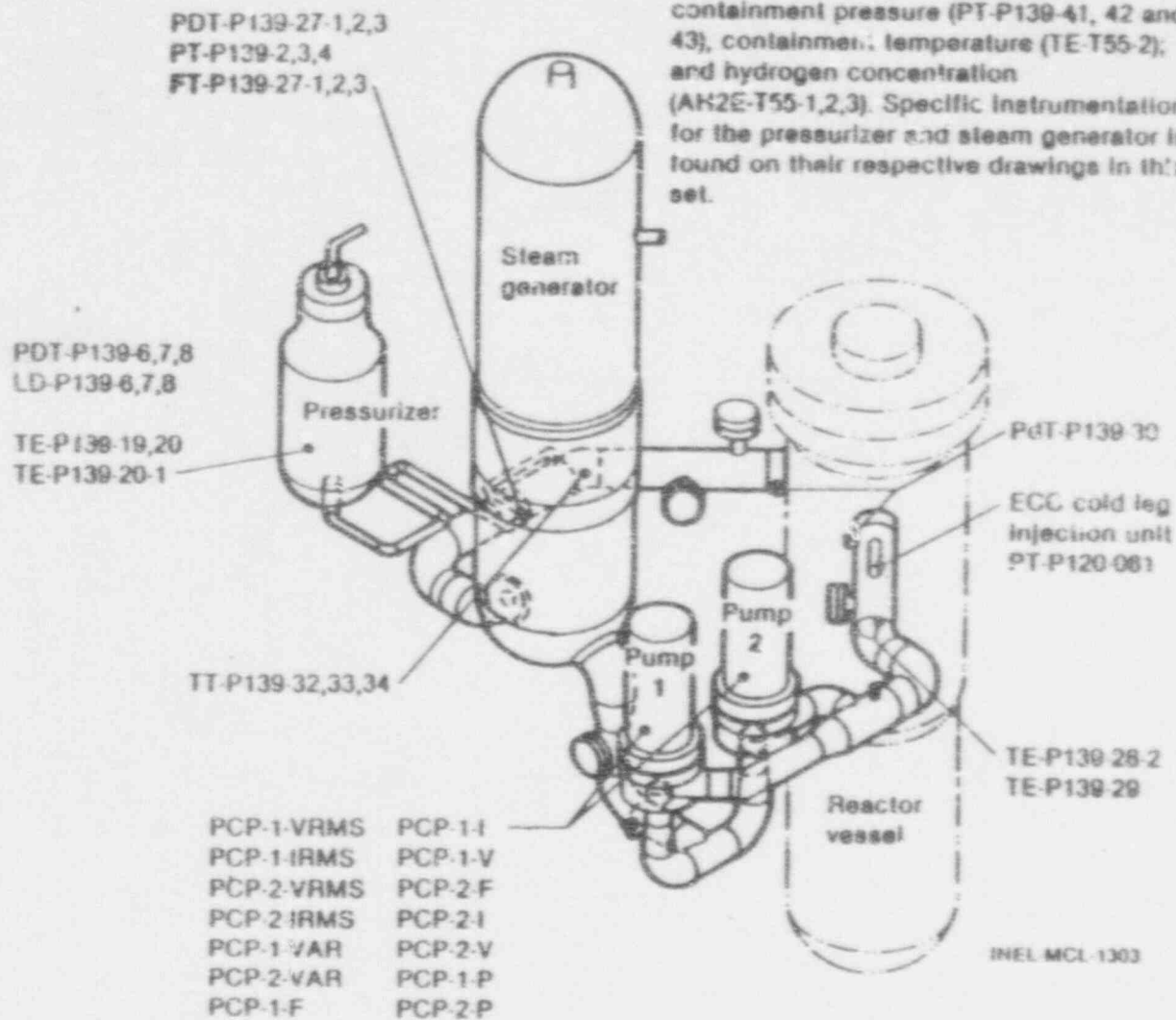


Figure A-3 LOFT Intact Loop Process Instrumentation

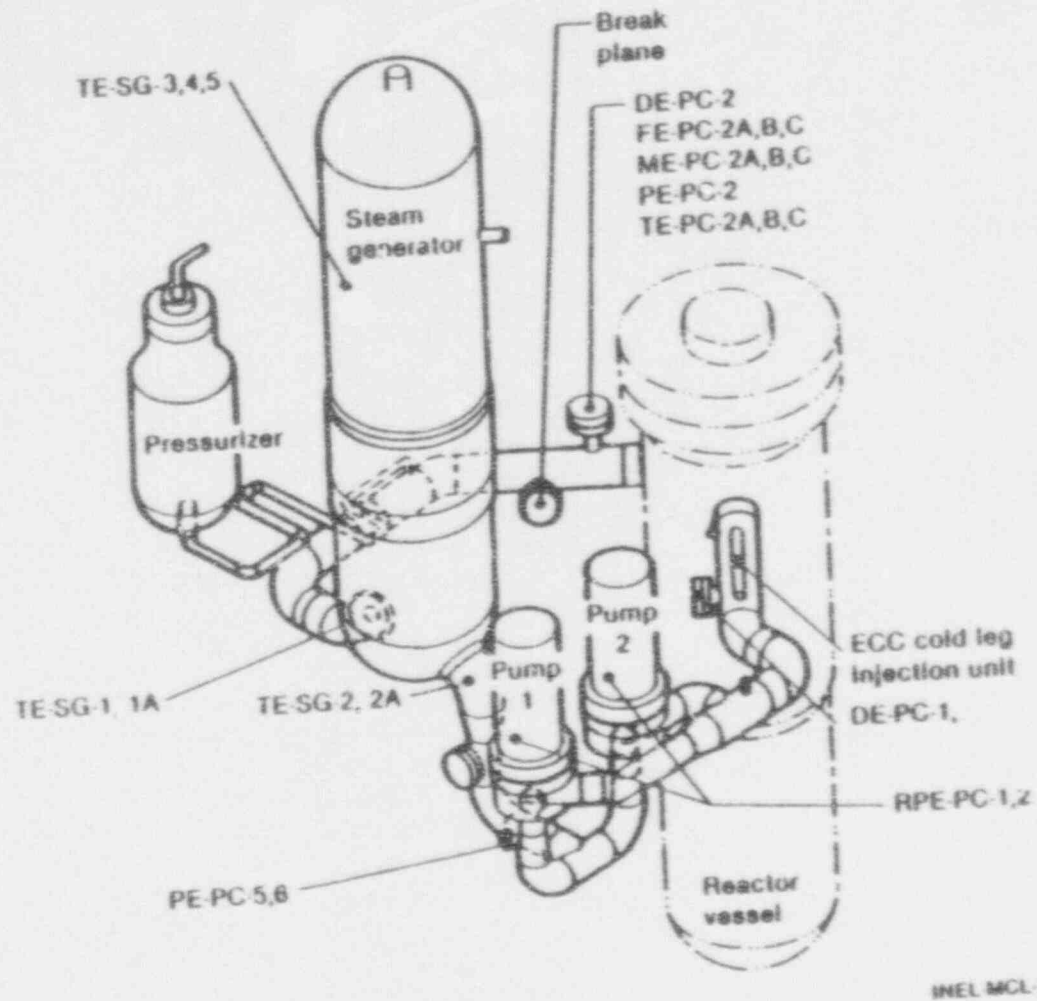
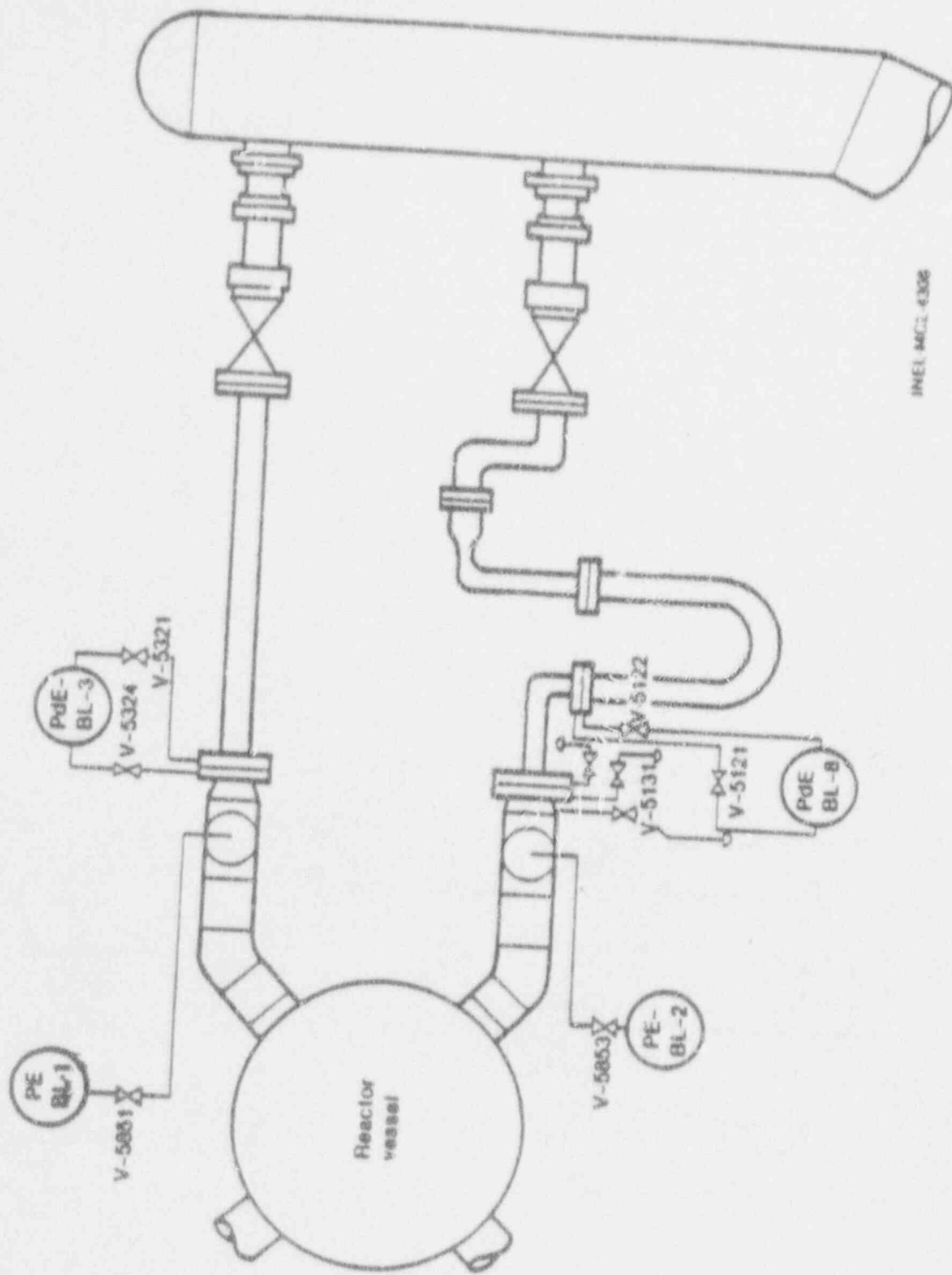


Figure A-4. LOFT Intact Loop Experimental Thermal-Hydraulic Instrumentation



INEL MC/L-6306

Figure A-5. Instrument Locations - Broken Loop Differential Pressure Measurements

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FP-1 FINAL DISC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
REVISION: FINAL
SYSTEM LOCK: FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
CV-P00A-008	VALVE P05-FEEDWATER FLOW CONTROL	01-03-85	QUALIFIED	
CV-P00A-010	VALVE P05-SC3 STEAM FLOW CONTROL	12-31-84	QUALIFIED	
CV-P00A-090	MAIN STEAM BYPASS VALVE	01-03-85	QUALIFIED	
CV-P00A-091	MAIN FUEL BYPASS VALVE	12-31-84	QUALIFIED	
CV-P138-001	VALVE P05-BROKEN LOOP CL 00BV	01-03-85	QUALIFIED	
CV-P138-015	VALVE P05-BROKEN LOOP HL 00BV	12-31-84	QUALIFIED	
CV-P138-070A	VALVE P05-BLOWDOWN SYSTEM RABV CH A	12-31-84	QUALIFIED	
CV-P138-071A	VALVE P05-BLOWDOWN SYSTEM RABV CH B	12-31-84	QUALIFIED	
DE-BL-001A	CHORDAL DENSITY-BROKEN LOOP CL	01-08-85	QUALIFIED	
DE-BL-001B	CHORDAL DENSITY-BROKEN LOOP CL	01-03-85	QUALIFIED	
DE-BL-001C	CHORDAL DENSITY-BROKEN LOOP CL	01-08-85	QUALIFIED	TO 65 SECONDS
DE-BL-002A	CHORDAL DENSITY-BROKEN LOOP HL	01-03-85	QUALIFIED	TO 65 SECONDS
DE-BL-002B	CHORDAL DENSITY-BROKEN LOOP HL	01-03-85	QUALIFIED	TO 65 SECONDS

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FP- FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
REVISION: FINAL
SYSTEM CODE: FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
DE-BL-002C	CHORDAL DENSITY-BROKEN LOOP HL	01-09-85	QUALIFIED	TO 65 SECONDS
DE-BL-002D	GROSS GAMMA BRG/BROKEN LOOP HL	01-29-85	QUALIFIED	TREND DATA ONLY, 80 SAMPLES PER SECOND DATA
DE-BL-105	AVERAGE DENSITY-BROKEN LOOP CL	01-11-85	QUALIFIED	AFTER 12 SECONDS SPURIOUS SPIRES
DE-BL-205	AVERAGE DENSITY-BROKEN LOOP HL	01-11-85	QUALIFIED	TO 65 SECONDS
DE-PC-001A	CHORDAL DENSITY-INTACT LOOP CL	01-08-85	QUALIFIED	SPURIOUS SPIRES
DE-PC-001B	CHORDAL DENSITY-INTACT LOOP CL	01-08-85	QUALIFIED	SPURIOUS SPIRES
DE-PC-001C	CHORDAL DENSITY-INTACT LOOP CL	01-08-85	QUALIFIED	SPURIOUS SPIRES
DE-PC-002A	CHORDAL DENSITY-INTACT LOOP HL	01-09-85	QUALIFIED	DE-PC-001B USED FOR BACKGROUND CORRECTION
DE-PC-002B	CHORDAL DENSITY-INTACT LOOP HL	01-03-85	QUALIFIED	TO 65 SECONDS
DE-PC-002C	CHORDAL DENSITY-INTACT LOOP HL	01-09-85	FAILED	
DE-PC-002D	GROSS GAMMA BRG/INTACT LOOP HL	01-29-85	QUALIFIED	TREND DATA ONLY
DE-PC-105	AVERAGE DENSITY - INTACT LOOP CL	01-11-85	QUALIFIED	
DE-PC-225	WEIGHTED AVG DENSITY IL HL	01-11-85	QUALIFIED	TO 65 SECONDS

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FP-1 FINAL DIRC QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT	
FE-PC-002B	VELOCITY-INTACT LOOP HOT LEG BOTTOM CI-09-85	01-09-85	QUALIFIED	UNIDIRECTIONAL	
FE-PC-002C	VELOCITY-INTACT LOOP HOT LEG MIDDLE CI-09-85	01-09-85	QUALIFIED	UNIDIRECTIONAL	
FE-PC-002D	VELOCITY-INTACT LOOP HOT LEG TOP CI-09-85	01-09-85	QUALIFIED	UNIDIRECTIONAL	
FE-PC-002E	AVERAGE VELOCITY - INTACT LOOP HL CI-22-85	01-22-85	QUALIFIED	UNIDIRECTIONAL	
FE-151-001	VELOCITY DOWNCOMER STALK I CI-09-85	01-09-85	QUALIFIED	UNIDIRECTIONAL	
FE-151-002	VELOCITY DOWNCOMER STALK I LOWER CI-18-85	01-18-85	QUALIFIED	UNIDIRECTIONAL	
FE-SUP-002	VELOCITY-FAS ABOVE UPPER END NOX CI-09-85	01-09-85	QUALIFIED	UNIDIRECTIONAL	
FR-BL-105	AVERAGE FLOWRATE, BROKEN LOOP CL CI-18-85	01-18-85	QUALIFIED	TO 65 SECONDS	
FR-BL-205	AVERAGE FLOWRATE, BROKEN LOOP HL CI-22-85	01-22-85	QUALIFIED	TO 420 SECONDS, MASS FLOW AFTER 65 SECONDS PASSED ON STEAM DENSITY	
FR-PC-205	MASS FLOW RATE HL DD+DENS CI-22-85	01-22-85	QUALIFIED	TO 27 SECONDS, B DRAB DISC SUBSTITUTED FOR C DRAB DISC IN CALCULATION	
FT-P00A-012	FLOWRATE-STEAM FLOW CONDENSER IN CI-03-85	01-03-85	QUALIFIED	INITIAL CONDITIONS ONLY	
FT-P00A-040	VOLUMETRIC FLOW STEAM ULTRASOUND B CI-03-85	01-03-85	QUALIFIED		
FT-P00A-091	VOLUMETRIC FLOW SECONDARY CI-03-85	01-03-85	QUALIFIED		

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FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
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SYSTEM: LDCR FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
FI-P004-72A	FLOWRATE-SCS FEEDWATER	01-09-85	QUALIFIED	INITIAL CONDITION ONLY
FI-P004-72-Z	FLOWRATE-SCS PREHEATER	01-09-85	QUALIFIED	INITIAL CONDITIONS ONLY
FI-P120-07Z	FLOWRATE-LP15 PUMP B DISCHARGE	01-03-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
FI-P120-08S	FLOWRATE-LP15 PUMP A DISCHARGE	01-03-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
FI-P128-08S	FLOWRATE-HP15 PUMP B DISCHARGE	01-09-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
FI-P128-104	FLOWRATE-HP15 PUMP A DISCHARGE	01-18-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
FI-P139-27-1	FLOWRATE-INTACT LOOP COOLANT	01-08-85	QUALIFIED	INITIAL CONDITION ONLY
FI-P139-27-2	FLOWRATE-INTACT LOOP COOLANT	01-08-85	QUALIFIED	INITIAL CONDITION ONLY
FI-P139-27-3	FLOWRATE-INTACT LOOP COOLANT	01-08-85	QUALIFIED	INITIAL CONDITION ONLY
FI-P131-02Z	FLOWRATE-TOTAL PCC	01-03-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
LD-P139-006	LIQUID LEVEL-PRESSURIZER CH A	12-31-84	QUALIFIED	INITIAL CONDITIONS ONLY
LD-P139-007	LIQUID LEVEL-PRESSURIZER CH B	12-31-84	QUALIFIED	INITIAL CONDITIONS ONLY
LD-P139-008	LIQUID LEVEL-PRESSURIZER CH C	12-31-84	FAILED	

FP-1 FINAL DIRC QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT (S)
LEPDE-SV-161	LIQUID LEVEL-8ST	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
LEPDE-SV-261	LIQUID LEVEL-8ST	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
LE-ECC-01A	ACCUMULATOR A LIQUID LEVEL	01-11-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
LE-1F10	COOLANT LEVEL-FUEL ASSY 1 LOC F10	03-03-85	QUALIFIED	FAILED STINGS - 1,4,5,6,7,8,9,11,13,16,18,19
LE-1ST-001	COOLANT LEVEL-INSTA STALK 1 LP	12-27-84	QUALIFIED	
LE-1ST-002	COOLANT LEVEL-INSTA STALK 1 DC	12-27-84	QUALIFIED	FAILED STINGS - 1,2,3
LE-3F10	COOLANT LEVEL-FUEL ASSY 3 LOC F10	12-27-84	QUALIFIED	FAILED STINGS - 2,3,4,5,7,11,16,18,19
LE-3UP-001	COOLANT LEVEL-UPPER PLENUM	01-03-85	QUALIFIED	FAILED STINGS - 1,2,3,4,5,6,9
LE-9E11	COOLANT LEVEL-FUEL ASSY 5 LOC E 11	12-27-84	QUALIFIED	FAILED STING - 17
LE-3UP-001	COOLANT LEVEL-UPPER PLENUM	12-27-84	QUALIFIED	
LIT-P120-030	LIQUID LEVEL-ACCUMULATOR B	01-11-85	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
LTD-P138-033	85T DEWS CORR	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
LTD-P138-038	85T DEWS CORR	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY

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FP-1 FINAL DISC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
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SYSTEM: LOCB FP-1

MEASUREMENT IDENTIFICATION MEASUREMENT DESCRIPTION QUAL DATE QUAL STATUS QUALIFYING STATEMENT(S)

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
LT-P004-008A	STEAM GENERATOR LEVEL NARROW RANGE	01-14-85	QUALIFIED	
LT-P004-042	CONDENSATE RECEIVER LEVEL	12-31-84	QUALIFIED	
LT-P004-084A	STEAM GEN LEVEL NARROW RANGE	01-14-84	QUALIFIED	
LT-P138-033	LIQUID LEVEL A	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
LT-P138-058	LIQUID LEVEL-BST B	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
ME-BL-001A	MON FLUX, BL-1, BOT, HIGH RANGE	01-18-85	QUALIFIED	TO 65 SECONDS
ME-BL-001B	MON FLUX, BL-1, MIDDLE, HIGH RANGE	01-18-85	QUALIFIED	TO 65 SECONDS
ME-BL-001C	MON FLUX, BL-1, TOP, HIGH RANGE	01-18-85	QUALIFIED	TO 65 SECONDS
ME-BL-001	AVERAGE MON FLUX BROKEN LOOP CL	01-18-85	QUALIFIED	TO 65 SECONDS
ME-BL-002A	MOMENTUM FLUX-BROKEN LOOP HL BOTTOM	01-18-85	QUALIFIED	
ME-BL-002B	MOMENTUM FLUX-BROKEN LOOP HL MIDDLE	01-18-85	QUALIFIED	
ME-BL-002C	MOMENTUM FLUX-BROKEN LOOP HL TOP	01-18-85	QUALIFIED	
ME-BL-002	AVERAGE MON FLUX BROKEN LOOP HL	01-18-85	QUALIFIED	

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FP-1 FINAL OIRC QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
RE-PC-002A	MOMENTUM FLUX-INTACT LOOP HL BOTTOM	01-22-85	QUALIFIED	TO 22 SECONDS
RE-PC-002B	MOMENTUM FLUX-INTACT LOOP HL MIDDLE	01-22-85	QUALIFIED	TO 22 SECONDS
RE-PC-002C	MOMENTUM FLUX-INTACT LOOP HL TOP	01-18-85	FAILED	
RE-PC-002	AVE MOMENTUM FLUX-INTACT LOOP HL	01-22-85	QUALIFIED	TO 22 SECONDS, B DRAG DISC SUBSTITUTED FOR C DRAG DISC IN CALCULATION
RE-1SI-001	MOMENTUM FLUX-INSTR STALK 1 DC	01-22-85	FAILED	
RE-1SI-002	MOMENTUM FLUX-INSTR STALK 1 DC	01-22-85	FAILED	
RE-SUP-002	MOMENTUM FLUX-FAS AB UPPER END BOX	01-22-85	QUALIFIED	UNTIL 10 SECS AND AFTER 70 SECONDS UNCOMPENSATED TEMPERATURE SENSITIVITY BETWEEN 10 & 70 SECS.
RE-2HOB-26	NEUTRON DETECTOR IN CORE FAB2	12-31-84	QUALIFIED	
RE-4HOB-26	NEUTRON DETECTOR IN CORE FAB4	12-31-84	QUALIFIED	
RE-6HOB-26	NEUTRON DETECTOR IN CORE FAB6	12-31-84	QUALIFIED	
PE-BL-003	DELTA P-BL COLD LEG BRK PLANE	01-03-85	QUALIFIED	
PE-BL-008	DELTA P-BL ACROSS SG SIM IN FINE	01-03-85	QUALIFIED	
PE-SV-001	SUPPRESSION VESSEL LEVEL	01-18-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY

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PP-1 FINAL DERC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
REVISION: FINAL
SYSTEM: LOCE PP-1

MEASUREMENT IDENTIFICATION DESCRIPTION QUAL DATE QUAL STATUS QUALIFYING STATEMENT(S)

MEASUREMENT IDENTIFICATION	DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
PDE-SV-002	SUPPRESSION VESSEL LEVEL	01-19-85	QUALIFIED	INITIAL AND FINAL CONDITIONS ONLY
POIPI39-27-1	INTACT LOOP MASS FLOW DELTA P	01-08-85	QUALIFIED	INITIAL CONDITION ONLY, TREND THEREAFTER
POIPI39-27-2	INTACT LOOP MASS FLOW DELTA P	01-08-85	QUALIFIED	INITIAL CONDITION ONLY, TREND THEREAFTER
POIPI39-27-3	INTACT LOOP MASS FLOW DELTA P	01-08-85	QUALIFIED	INITIAL CONDITION ONLY, TREND THEREAFTER
POI-PO0A-072	DIFF PRESS FEEDWATER FLOW ORIFICE	01-08-85	QUALIFIED	INITIAL CONDITIONS ONLY
POI-PI39-030A	DELTA P-PRIMARY COOLANT PUMP	01-03-85	QUALIFIED	INITIAL CONDITIONS ONLY
POI-PI39-030B	DELTA P-INTACT LOOP SG	01-08-85	QUALIFIED	INITIAL CONDITION ONLY, TREND THEREAFTER
POI-PI39-030	DELTA P - REACTOR VESSEL	01-03-85	QUALIFIED	UNIDIRECTIONAL
PE-BL-001	PRESSURE-BROKEN LOOP COLD LEG	12-27-84	QUALIFIED	
PE-BL-002	PRESSURE-BROKEN LOOP HOT LEG	12-27-84	QUALIFIED	
PE-PC-002	PRESSURE-INTACT LOOP HOT LEG	12-27-84	QUALIFIED	
PE-PC-003	PRESSURE-INTACT LOOP REF.	12-27-84	QUALIFIED	
PE-PC-006	PRESSURE-INTACT LOOP REF.	12-27-84	QUALIFIED	

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FP-3 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
REVISION: FINAL
SYSTEM: LOCE FP-3

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
PS-5F04-5W	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PS-5F12-5W	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PS-5G11-5W	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PS-5I05-5W	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PS-5J12-5W	PRESSURE SWITCH, FA 05	01-11-85	QUALIFIED	SWITCH ACTIVATES AT ROD INTERNAL PRESSURE OF 450 +/-20 PSI
PT-P004-010A	PRESSURE-SCS 10 INCH LIME FROM 56	12-27-84	QUALIFIED	
PT-P004-022	CONDENSATE RECEIVER PRESSURE	12-27-84	QUALIFIED	
PT-P004-034	PRESSURE-SCS FEEDWATER	12-27-84	QUALIFIED	
PT-P004-085	PRESSURE-SCS 12 INCH CONDENSOR IN	12-27-84	FAILED	
PT-P120-029	PRESSURE-ECCS ACCUMULATOR B	12-27-84	QUALIFIED	
PT-P120-043	PRESSURE-ECCS ACCUMULATOR A	01-10-85	QUALIFIED	
PT-P120-102	AC-P-4B DISCHARGE PRESS	01-08-85	FAILED	
PT-P120-103	AC-P-4C DISCHARGE PRESS	01-09-85	QUALIFIED	

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FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/83
REVISION: FINAL
SYSTEM: LDCB FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFIER'S STATEMENT(S)
PT-P138-055	PRESSURE-BST VAPOR SPACE CH A	01-03-85	QUALIFIED	
PT-P138-056	PRESSURE-BST VAPOR SPACE CH B	01-03-84	QUALIFIED	
PT-P138-057	PRESSURE-BST VAPOR SPACE CH C	01-03-85	QUALIFIED	
PT-P139-002	PRESSURE-INITIAL LOOP HOT LEG CH A	12-31-84	QUALIFIED	RESPONSE LIMITED DURING THE SUB COOLED BLOWDOWN
PT-P139-003	PRESSURE-INITIAL LOOP HOT LEG CH B	12-31-84	QUALIFIED	RESPONSE LIMITED DURING THE SUB COOLED BLOWDOWN
PT-P139-004	PRESSURE-INITIAL LOOP HOT LEG CH C	12-31-84	QUALIFIED	RESPONSE LIMITED DURING THE SUB COOLED BLOWDOWN
PT-P139-041	PRESSURE CONTAINMENT CHAN A	12-27-84	FAILED	
PT-P139-042	PRESSURE CONTAINMENT CHAN B	12-27-84	QUALIFIED	
PT-P139-043	PRESSURE CONTAINMENT CHAN C	12-31-84	QUALIFIED	
PT-P139-051	PRESSURE-PRESSURIZER	12-27-84	QUALIFIED	
RE-T-77-1A2	MIS-POWER RANGE CHANNEL A LEVEL	01-11-85	QUALIFIED	
RE-T-77-2A2	MIS-POWER RANGE CHANNEL B LEVEL	01-11-85	QUALIFIED	
RE-T-77-3A2	MIS-POWER RANGE CHANNEL C LEVEL	01-11-85	QUALIFIED	

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FP-1 FINAL DINC QUALIFICATION REPORT

EFFECTIVE DATE: 03/30/85
REVISION: FINAL
SYSTEM: LOCEB FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
RP-PC-001	PUMP SPEED-PRIMARY COOLANT	11-11-84	QUALIFIED	AFTER 5 SECONDS
RP-PC-002	PUMP SPEED-PRIMARY COOLANT	11-11-84	QUALIFIED	
RP-CRDM2-TC	ROD POS-ROD 2 TURNS COUNTER	12-31-84	QUALIFIED	FOR SCRAM EVENT TIME ONLY
RP-CRDM4-TC	ROD POS-ROD 4 TURNS COUNTER	12-31-84	QUALIFIED	FOR SCRAM EVENT TIME ONLY
RP-CRDM6-TC	ROD POS-ROD 6 TURNS COUNTER	12-31-84	QUALIFIED	FOR SCRAM EVENT TIME ONLY
RP-CRDM8-TC	ROD POS-ROD 8 TURNS COUNTER	12-31-84	QUALIFIED	FOR SCRAM EVENT TIME ONLY
RTP165-S1-10	GROSS GAMMA S1 SAMPLE SYSTEM	01-22-85	QUALIFIED	TREND DATA ONLY
RTP165-S2-10	GROSS GAMMA S2 SAMPLE SYSTEM	01-22-85	FAILED	
RTP165-S3-10	GROSS GAMMA S3 SAMPLE SYSTEM	01-22-85	QUALIFIED	S-3 SAMPLE SYSTEM BLOCKED
RTP165-S4-10	GROSS GAMMA S4 SAMPLE SYSTEM	01-22-84	QUALIFIED	TREND DATA ONLY
SP-BL-001B	SAT PRESSURE BROKEN LOOP CL	01-08-85	QUALIFIED	
SP-BL-002B	SAT PRESSURE BROKEN LOOP HL	01-08-85	QUALIFIED	
SP-PC-002B	SATURATIUM PRESS-INTACT LOOP HL	01-08-85	QUALIFIED	

FP-3 FINAL DIRC QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENTS
SP-56-004	SATURATION PRESSURE, STEAM GEN, FID	01-08-85	QUALIFIED	
SP-157-005	SATURATION PRESS-COMMUNICATOR STALK 1	01-08-85	QUALIFIED	
SP-149-001	SATURATION PRESSURE, UPPER P-ENGR	01-08-85	QUALIFIED	
ST-81-001	SAT TEMPERATURE BROKEN LOOP CL	01-08-85	QUALIFIED	
ST-81-002	SAT TEMPERATURE BROKEN LOOP HL	01-08-85	QUALIFIED	
ST-PC-002	SATURATION TEMP, CONTACT LOOP, HL	01-08-85	QUALIFIED	
ST-PC-605	SATURATION TEMP, INTACT LOOP, CI	01-08-85	QUALIFIED	
ST-P004-010a	SATURATION TEMP - SC5 56 10 IN LINE	01-08-85	QUALIFIED	
TC-5006-27	TEMP FUEL CENTERLINE/FAS PIN D6 Z7	12-27-84	FAILED	
TC-5010-27	TEMP FUEL CENTERLINE/FAS PIN D10 Z7	01-03-85	QUALIFIED	FAILED PRE-LOCE TEST
TE-81-001A	COOLANT TEMP-BROKEN LOOP CL BOTTOM	12-27-84	QUALIFIED	POSSIBLE NOT MALL EFFECTS
TE-81-001B	COOLANT TEMP-BROKEN LOOP CL MIDDLE	12-27-84	QUALIFIED	POSSIBLE NOT MALL EFFECTS
TE-81-001C	COOLANT TEMP-BROKEN LOOP CL TOP	12-27-84	QUALIFIED	POSSIBLE NOT MALL EFFECTS

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FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
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SYSTEM: LOCE FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-BL-002B	COOLANT TEMP- DOWN LOOP HL MIDDLE	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-BL-002C	COOLANT TEMP- DOWN LOOP HL TOP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-PC-002A	TEMP-INTACT LOOP HL BOTTOM	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-PC-002B	TEMP-INTACT LOOP HL MIDDLE	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-PC-002C	TEMP-INTACT LOOP HL TOP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-P00A-05A	CONDENSATE RECEIVER TEMP	12-27-84	QUALIFIED	
TE-P120-001	LIQUID TEMP-BWST	12-27-84	QUALIFIED	
TE-P120-041	LIQUID TEMP-ECCS ACCUM A	01-03-85	QUALIFIED	INITIAL CONDITIONS ONLY
TE-P120-102	LIQUID TEMP-ECCS LPTS MK B OUTLET	12-27-84	QUALIFIED	
TE-P130-019	TEMPERATURE-PRESSURIZER VAPOR	12-31-84	QUALIFIED	INITIAL CONDITIONS ONLY
TE-P130-020	TEMPERATURE-PRESSURIZER LIQUID	12-31-84	QUALIFIED	INITIAL CONDITIONS ONLY
TE-P130-029	COOLANT TEMP-INTACT LOOP COLD LEG	12-27-84	QUALIFIED	INITIAL CONDITIONS ONLY
TE-P130-28-2	TEMPERATURE-INTACT LOOP COLD LEG	12-27-84	QUALIFIED	INITIAL CONDITIONS ONLY

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FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
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MEASUREMENT IDENTIFICATION MEASUREMENT DESCRIPTION QUAL DATE QUAL STATUS QUALIFYING STATEMENTS

INITIAL CONDITIONS ONLY

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENTS
TE-P139-32-1	PRIMARY COOLANT HOT LEG TEMP CHAN A	12-27-84	QUALIFIED	
TE-P141-004	PCCS HEAT EXCH ML TEMP	12-21-84	QUALIFIED	
TE-P141-005	WATER TEMP-COLD LEG OF PCC LOADS	12-27-84	QUALIFIED	
TE-S6-001A	COOLANT TEMP-IL SG INLET PLENUM	01-03-85	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-S6-001	COOLANT TEMP-IL SG INLET PLENUM	12-31-84	FAILED	
TE-S6-002A	COOLANT TEMP-IL SG OUTLET PLENUM	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-S6-002	COOLANT TEMP-IL SG OUTLET PLENUM	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-S6-003	LIQUID TEMP-SCS SG DOWNCOMER	12-27-84	FAILED	
TE-S6-004	LIQUID TEMP-SCS SG DOWNCOMER	12-27-84	QUALIFIED	
TE-S9-001	LIQUID TEMP-BST STALK 1-107.2	12-27-84	QUALIFIED	
TE-S9-006	LIQUID TEMP-BST STALK 1-14.7	12-27-84	QUALIFIED	
TE-S9-007	LIQUID TEMP-BST STALK 2-107.2	12-27-84	QUALIFIED	
TE-S9-011	LIQUID TEMP-BST STALK 2-39.0	12-27-84	QUALIFIED	

MEASUREMENT IDENTIFICATION MEASUREMENT DESCRIPTION QUAL DAY QUAL STATUS QUALIFYING STATEMENTS

TE-SV-012	LIQUID TEMP-BBY STALK 8-14.7	12-27-84	QUALIFIED	
TE-Y053-002	TEMPERATURE-COMTAINMENT AMBIENT	12-27-84	QUALIFIED	NO OTHER MEASUREMENT FOR DIRECT COMPARISON
TE-1A11-030	TEMP-CLADDING/FAL PIN A11 30 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1B10-037	TEMP-CLADDING/FAL PIN B10 37 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1B11-028	TEMP-CLADDING/FAL PIN B11 28 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1B11-032	TEMP-CLADDING/FAL PIN B11 32 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1C11-021	TEMP-CLADDING/FAL PIN C11 21 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1C11-039	TEMP-CLADDING/FAL PIN C11 39 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1F07-015	TEMP-CLADDING/FAL PIN F7 15 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1F07-026	TEMP-CLADDING/FAL PIN F7 26 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-1S7-001	COOLANT TEMP-BV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1S7-002	COOLANT TEMP-BV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1S7-003	COOLANT TEMP-BV INSTR STALK 1 DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

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FP-1 FINAL DARC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/89
REVISION: FINAL
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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-1ST-004	COOLANT TEMP-RV INSTR STALK I DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-005	COOLANT TEMP-RV INSTR STALK I DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-006	COOLANT TEMP-RV INSTR STALK I DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-008	COOLANT TEMP-RV INSTR STALK I LP	12-27-84	FAILED	
TE-1ST-009	COOLANT TEMP-RV INSTR STALK I LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-010	COOLANT TEMP-RV INSTR STALK I LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-011	COOLANT TEMP-RV INSTR STALK I LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-012	COOLANT TEMP-RV INSTR STALK I LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-013	COOLANT TEMP-RV INSTR STALK I LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-014	COOLANT TEMP-RV INSTR STALK I LP	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1ST-015	COOLANT TEMP-RV INSTR STALK I DC	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1UP-001	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1UP-002	COOLANT TEMP-UPPER END BOX	12-31-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

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FP-1 FINAL QIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/89
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SYSTEM: LDC2 FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-1UP-005	COOLANT TEMP-ON DTY FE-1UP-1	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-1UP-006	PISTON TEMP-SUPPORTY COLUMN FA1	12-27-84	QUALIFIED	
TE-1UP-007	METAL TEMP-SUPPORTY COLUMN FA1	12-27-84	QUALIFIED	
TE-2E08-043	TEMP-CLADDING/FA2 PIM E8 45 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2F07-013	TEMP-CLADDING/FA2 PIM F7 15 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2F08-032	TEMP-CLADDING/FA2 PIM F8 32 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2F09-026	TEMP-CLADDING/FA2 PIM F9 26 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2G14-011	TEMP-CLADDING/FA2 PIM G14 11 IN.	12-27-84	QUALIFIED	
TE-2G14-030	TEMP-CLADDING/FA2 PIM G14 30 IN.	12-27-84	QUALIFIED	
TE-2G14-045	TEMP-CLADDING/FA2 PIM G14 45 IN.	12-27-84	QUALIFIED	
TE-2H07-020	TEMP-CLADDING/FA2 PIM H2 26 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-2H13-021	TEMP-CLADDING/FA2 PIM H13 21 IN.	12-27-84	QUALIFIED	
TE-2H13-049	TEMP-CLADDING/FA2 PIM H13 49 IN.	01-03-84	QUALIFIED	

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FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
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SYSTEM: LOCE FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENTS
TE-2H1A-020	TEMP-CLADDING/FAZ PIN H14 26 IN.	12-27-84	QUALIFIED	
TE-2H1A-022	TEMP-CLADDING/FAZ PIN H14 32 IN.	12-27-84	QUALIFIED	
TE-2H1A-026	TEMP-CLADDING/FAZ PIN H15 24 IN.	12-27-84	QUALIFIED	
TE-2H1A-041	TEMP-CLADDING/FAZ PIN H15 13 IN.	12-27-84	QUALIFIED	
TE-2H1A-021	TEMP-CLADDING/FAZ PIN I14 21 IN.	12-27-84	QUALIFIED	
TE-2H1A-039	TEMP-CLADDING/FAZ PIN I14 39 IN.	12-27-84	QUALIFIED	
TE-2LP-001	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2LP-002	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2LP-003	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2UP-001	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2UP-002	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2UP-003	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-2UP-004	METAL TEMP-SUPPORT COLUMN FAZ	12-27-84	QUALIFIED	

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FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-ZUP-005	METAL TEMP-SUPPORT COLUMN FA2	12-27-84	QUALIFIED	
TE-JA11-030	TEMP-CLADDING/FA3 PIM A11 30 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3B11-028	TEMP-CLADDING/FA3 PIM B11 28 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3M11-032	TEMP-CLADDING/FA3 PIM M11 32 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3C11-021	TEMP-CLADDING/FA3 PIM C11 21 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3C11-039	TEMP-CLADDING/FA3 PIM C11 39 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-3F07-026	TEMP-CLADDING/FA3 PIM F7 26 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PE SECOND
TE-3UP-001	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE NOT WALL EFFECTS
TE-3UP-006	METAL TEMP-SUPPORT COLUMN FA3	12-27-84	QUALIFIED	
TE-3UP-008	TEMP-COOLANT LLY ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE NOT WALL EFFECTS
TE-3UP-010	TEMP-COOLANT LLY ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE NOT WALL EFFECTS
TE-3UP-011	TEMP-COOLANT LLY ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE NOT WALL EFFECTS
TE-3UP-012	TEMP-COOLANT LLY ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE NOT WALL EFFECTS

FP-1 FINAL DIRC QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENTS
TE-3UP-013	TEMP-COOLANT LLY ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-014	TEMP-COOLANT LLY ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-015	TEMP-COOLANT LLY ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-3UP-016	TEMP-COOLANT LLY ABOVE FA3	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-4E08-045	TEMP-CLADDING/FA4 PIN E8 47 IM.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-4F07-015	TEMP-CLADDING/FA4 PIN F7 15 IM.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-4F08-032	TEMP-CLADDING/FA4 PIN F8 32 IM.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-4G08-021	TEMP-CLADDING/FA4 PIN G8 21 IM.	12-27-84	QUALIFIED	
TE-4G14-011	TEMP-CLADDING/FA4 PIN G14 11 IM.	12-27-84	QUALIFIED	
TE-4G14-030	TEMP-CLADDING/FA4 PIN G14 30 IM	12-27-84	FAILED	
TE-4G14-045	TEMP-CLADDING/FA4 PIN G14 45 IM.	12-27-84	QUALIFIED	
TE-4H13-015	TEMP-CLADDING/FA4 PIN H13 15 IM.	12-27-84	QUALIFIED	
TE-4H13-037	TEMP-CLADDING/FA4 PIN H13 37 IM.	12-27-84	QUALIFIED	

FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
REVISION: FINAL
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MEASUREMENT IDENTIFICATION MEASUREMENT DESCRIPTION QUAL DATE QUAL STATUS QUALIFYING STATEMENT(S)

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-5E10-032	TEMP-GUIDE TUBE FAS LOC C10 32 IM	12-27-84	QUALIFIED	
TE-5E03-022	TEMP-GUIDE TUBE FAS LOC E5 32 IM	12-27-84	QUALIFIED	
TE-5E07-026	TEMP-CLADDING/FAS PIN E7 F6 IM	12-27-84	QUALIFIED	
TE-5E07-032	TEMP-CLADDING/FAS PIN G1 32 IM	12-27-84	QUALIFIED	
TE-5E07-039	TEMP-CLADDING/FAS PIN E7 39 IM	12-27-84	QUALIFIED	
TE-5E07-043	TEMP-CLADDING/FAS PIN E7 43 IM	12-27-84	QUALIFIED	
TE-5E09-005	TEMP-CLADDING/FAS PIN E9 5 IM	12-27-84	QUALIFIED	
TE-5E09-010	TEMP-CLADDING/FAS PIN E9 10 IM	12-27-84	QUALIFIED	
TE-5E09-016	TEMP-CLADDING/FAS PIN E9 16 IM	12-27-84	QUALIFIED	
TE-5E09-021	TEMP-CLADDING/FAS PIN E9 21 IM	12-27-84	QUALIFIED	
TE-5F03-045	TEMP-GUIDE TUBE FAS LOC F3 45 IM	12-27-84	QUALIFIED	
TE-5F13-068	TEMP-GUIDE TUBE FAS LOC F13 68 IM	12-27-84	QUALIFIED	
TE-5G03-027	TEMP-CLADDING/FAS PIN G3 27 IM	01-03-85	QUALIFIED	

FP-1 FINAL DISC QUALIFICATION REPORT

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MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-5608-006	TEMP-CLADDING/FAS PIN G6 6 IN	12-27-84	QUALIFIED	
TE-5608-012	TEMP-CLADDING/FAS PIN G8 12 IN	12-27-84	QUALIFIED	
TE-5608-029A	TEMP-CLADDING/FAS PIN G8 20 IN	12-27-84	QUALIFIED	
TE-5608-029B	TEMP-CLADDING/FAS PIN G8 28 IN	12-27-84	QUALIFIED	
TE-5611-027	TEMP-CLADDING/FAS PIN G11 27 IN	12-27-84	QUALIFIED	
TE-5103-027	TEMP-CLADDING/FAS PIN I3 27 IN	12-27-84	QUALIFIED	
TE-5111-027	TEMP-CLADDING/FAS PIN I11 27 IN	12-27-84	QUALIFIED	
TE-5J12-045	TEMP-GUIDE TUBE FAS 10C J13 45 IN	12-27-84	QUALIFIED	
TE-5K07-048	TEMP-CLADDING/FAS PIN K7 48 IN	12-27-84	FAILED	
TE-5K07-055	TEMP-CLADDING/FAS PIN K7 55 IN	12-27-84	QUALIFIED	
TE-5K07-060	TEMP-CLADDING/FAS PIN K7 60 IN	12-27-84	QUALIFIED	
TE-5K07-065	TEMP-CLADDING/FAS PIN K7 65 IN	12-27-84	QUALIFIED	
TE-5K09-021	TEMP-CLADDING/FAS PIN K9 21 IN	12-27-84	QUALIFIED	

05/02/01
15.52.31

FP-1 FINAL QIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/89
REVISION: FINAL
SYSTEM: LOC: FP-1

MEASUREMENT IDENTIFICATION MEASUREMENT DESCRIPTION QUAL DATE QUAL STATUS QUALIFYING STATEMENTS:

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENTS
TE-SK09-026	TEMP-CLADDING/FAS PIM R9 26 IM	12-27-84	QUALIFIED	
TE-SK09-032	TEMP-CLADDING/FAS PIM R9 32 IM	12-27-84	QUALIFIED	
TE-SK09-039	TEMP-CLADDING/FAS PIM R9 39 IM	12-27-84	QUALIFIED	
TE-SL08-032	TEMP-GUIDE TUBE FAS LOC L9 32 IM	12-27-84	QUALIFIED	
TE-SM06-045	TEMP-GUIDE TUBE FAS LOC M6 45 IM	12-27-84	QUALIFIED	
TE-SM10-046	TEMP-GUIDE TUBE FAS LOC M10 46 IM	12-27-84	QUALIFIED	
TE-SUP-004	COOLANT TEMP-UPPER EMP BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SUP-005	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SUP-006	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SUP-007	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SUP-009	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SUP-011	COOLANT TEMP-UPPER END BOX	12-31-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SUP-012	COOLANT TEMP-UPPER END BOX	12-31-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

PP-1 FINAL DIRC QUALIFICATION REPORT

85/02/01
 15.52.31

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENT(S)
TE-SUP-021	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SUP-022	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-SUP-171A	METAL SURFACE TEMPERATURE UPPER END	12-27-84	QUALIFIED	
TE-SUP-171B	METAL SURFACE TEMPERATURE UPPER END	12-27-84	QUALIFIED	
TE-SUP-19A	METAL SURFACE TEMPERATURE UPPER END	12-27-84	QUALIFIED	
TE-SUP-212	METAL SURFACE TEMPERATURE UPPER END	12-31-84	QUALIFIED	
TE-SUP-250	METAL SURFACE TEMPERATURE UPPER END	12-27-84	QUALIFIED	
TE-6608-045	TEMP-CLADDING/FAB PIM E6 45 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-6607-037	TEMP-CLADDING/FAB PIM F7 37 IN.	01-22-85	QUALIFIED	SAMPLE RATE IS 2.5 SAMPLES PER SECOND
TE-6609-041	TEMP-CLADDING/FAB PIM F9 41 IN.	01-03-84	QUALIFIED	
TE-6608-039	TEMP-CLADDING/FAB PIM G8 39 IN.	12-27-84	QUALIFIED	
TE-6614-011	TEMP-CLADDING/FAB PIM G14 11 IN.	12-27-84	QUALIFIED	
TE-6614-030	TEMP-CLADDING/FAB PIM G14 30 IN.	12-27-84	QUALIFIED	

15.52.31

FP-1 FINAL DIRC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
REVISION: FINAL
SYSTEM: LOEB FP-1

MEASUREMENT IDENTIFICATION	MEASUREMENT DESCRIPTION	QUAL DATE	QUAL STATUS	QUALIFYING STATEMENTS
TE-661A-044	TEMP-CLADDING/FAB PIN 614 A5 IN.	01-03-85	QUALIFIED	
TE-6M13-015	TEMP-CLADDING/FAB PIN 613 B5 IN.	12-27-84	QUALIFIED	
TE-6M13-037	TEMP-CLADDING/FAB PIN 613 B7 IN.	12-27-84	QUALIFIED	
TE-6M14-028	TEMP-CLADDING/FAB PIN 614 Z8 IN.	12-27-84	QUALIFIED	
TE-6M14-032	TEMP-CLADDING/FAB PIN 614 Z2 IN.	12-27-84	QUALIFIED	
TE-6M15-026	TEMP-CLADDING/FAB PIN 615 Z6 IN.	01-03-85	QUALIFIED	
TE-611A-021	TEMP-CLADDING/FAB PIN 114 I1 IN.	12-27-84	QUALIFIED	
TE-611A-039	TEMP-CLADDING/FAB PIN 114 B9 IN.	12-27-84	QUALIFIED	
TE-6LP-001	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-6LP-002	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-6LP-007	COOLANT TEMP-LOWER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-6UP-001	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS
TE-6UP-002	COOLANT TEMP-UPPER END BOX	12-27-84	QUALIFIED	POSSIBLE HOT WALL EFFECTS

85/02/01
15-52-31

FP-1 FINAL DPC QUALIFICATION REPORT

EFFECTIVE DATE: 01/30/85
REVISION: FINAL
SYSTEM: LOCB FP-1

MEASUREMENT IDENTIFICATION MEASUREMENT DESCRIPTION QUAL DATE QUAL STATUS QUALIFYING STATEMENT(S)

TE-6UP-003 COOLANT TEMP-UPPER END BOX 12-27-84 QUALIFIED POSSIBLE HOT WALL EFFECTS

TE-6UP-004 METAL TEMP-SUPPORT COLUMN FAS 12-27-84 QUALIFIED

TE-6UP-005 METAL TEMP-SUPPORT COLUMN FAS 12-27-84 QUALIFIED

TT-P004-004 LIQUID TEMP-SCS FEEDWATER 12-27-84 QUALIFIED

TT-P120-062 LIQUID TEMP-ECS CL INJECT POINT 01-03-85 QUALIFIED RESPONSE LIMITED

TT-P139-032 COOLANT TEMP-INTACT .OUP HOT LEG 12-27-84 QUALIFIED INITIAL CONDITIONS ONLY

TT-P139-033 COOLANT TEMP-INTACT LOOP HOT LEG 12-27-84 QUALIFIED INITIAL CONDITIONS ONLY

TT-P139-034 COOLANT TEMP-INTACT LOOP HOT LEG 12-27-84 QUALIFIED INITIAL CONDITIONS ONLY

TABLE 3.2. Input deck listing for plant steady state

* Main Pipe

*CH02
T INACT-LDOP HOT LEG
U.O *ICHF* 1

7 4 4

FEF

*****COMPONENT DATA*****

50	FEF	101	101.105.109	CORE BYPASS
51	FEF	102	102.106.110	CORE BYPASS
52	FEF	103	103.107.111	CORE BYPASS
53	FEF	104	104.108.112	CORE BYPASS
49	FILL	72	72	U.PLENUM INJECTION SYSTEM
48	PIPE	92	92.72	U.PLENUM INJECTION SYSTEM
47	FILL	71	71	U.PLENUM INJECTION SYSTEM
46	PIPE	91	91.71	U.PLENUM INJECTION SYSTEM
45	FILL	70	70	U.PLENUM INJECTION SYSTEM
44	PIPE	90	90.70	U.PLENUM INJECTION SYSTEM
43	FILL	69	69	U.PLENUM INJECTION SYSTEM
42	PIPE	89	89.69	U.PLENUM INJECTION SYSTEM
41	FILL	68	68	U.PLENUM INJECTION SYSTEM
40	PIPE	88	88.68	U.PLENUM INJECTION SYSTEM
39	FILL	67	67	U.PLENUM INJECTION SYSTEM
38	PIPE	87	87.67	U.PLENUM INJECTION SYSTEM
37	FILL	66	66	U.PLENUM INJECTION SYSTEM
36	PIPE	86	86.66	U.PLENUM INJECTION SYSTEM
35	FILL	65	65	U.PLENUM INJECTION SYSTEM
34	PIPE	85	85.65	U.PLENUM INJECTION SYSTEM
33	FILL	64	64	U.PLENUM INJECTION SYSTEM
32	PIPE	84	84.64	U.PLENUM INJECTION SYSTEM
31	FILL	63	63	U.PLENUM INJECTION SYSTEM
30	PIPE	83	83.63	U.PLENUM INJECTION SYSTEM
29	FILL	62	62	U.PLENUM INJECTION SYSTEM
28	PIPE	82	82.62	U.PLENUM INJECTION SYSTEM
27	FILL	61	61	U.PLENUM INJECTION SYSTEM
26	PIPE	81	81.61	U.PLENUM INJECTION SYSTEM
25	VALVE	43	44.42	BROKEN - P. COLL. LEG VALVE
24	VALVE	50	1.931.41.81.82	101-112 83.84.85.86.87 88.89.90.91.92
23	FILL	42	42	103.101 WESSE
22	FEF	41	41.44.43	BROKEN-COLD-LEG TERMINAL
21	FILL	32	32	BROKEN-COLD-LEG TERMINAL
20	FEF	31	31.32.43	BROKEN-LDOP HOT LEG
19	FILL	17	17	HPIS INJECTION
18	FILL	18	18	HPIS INJECTION
17	PIPE	19	17.11	ACQUILATOR
16	VALVE	14	14.15	ECC LINE - CHECK VALVE
15	FEF	13	13.15.14	ECC LINE - HPIS
14	FEF	12	12.14.13	ECC LINE - HPIS
13	FILL	11	11	ACQUILATOR OUTLET
12	FILL	93	93	PRESSURIZER OUTLET
11	PIPE	6	10.93	PRESSURIZER
10	FEF	7	8.9.14	INACT-LOOP COLD LEG
9	FEF	5	7.8.4	PUMP DISCHARGE
8	PUMP	5	5.7	PUMP NO. 1
7	PUMP	4	4.5	PUMP NO. 2
6	FILL	3	4.5.3	PUMP SUCTION
5	FEF	29	29	STEAM-GENERATOR WENT

0	0	0	0	0	0	*CN03
0	0	0	0	0	0	*CN04
0.14200	0.03571	0.0	0.0	300.0	0	*CN05
300.0	0.0	0.0	1.0E20	1.0	0	*CN06
0.0	0.0	1.0E20	1.0	0	0	*CN07
						*CN08

* SIDE TUBE

0	0	10	0	0	0	*CN09
0.0233005	0.0086968	0.0	0.0	300.0	0	*CN10
300.0	0.0	0.0	1.0E20	1.0	0	*CN11
0.0	0.0	1.0E20	1.0	0	0	*CN12
						*CN13
						*CN14

* MAIN TUBE

P 2	7.83555E-1	4.42503E-1	7.75839E-15	*DX
	1.12415E+0	0.65752E-1	4.17249E-15	
	5.25324E-1F			
P 2	5.07732E-2	3.20423E-2	5.04812E-25	*VJL
	5.05917E-2	5.52743E-2	3.13808E-25	
	5.71981E-2F			
P 5	5.34253E-2	5.34253E-2	5.34253E-25	*FA
	6.34253E-2	5.15000E-2E		
	0.0F 5	0.0	7.52500E-25	*FRIC VSL-HL FF=-0.28
	0.0	1.70400E-1E		*FRIC HL-SC FF=0.1704
	0.0310R 5	0.0	7.52500E-25	*FRIC REV
	0.0	1.70400E-1E		*FRIC REV
P 8	0.0	5.84737E-1E		*GRAY
P 7	2.84000E-1	2.84000E-1	2.56300E-1E	*HJ
F	0E			*ICFLG
F	1F			*NFF
F	0.0F			*ALP
F	0.0F			*VL
F	0.0F			*VV
F	578.4E			*TL
F	515.0E			*TV
F	148.4E+5E			*P
F	0.0F			*PA
F	0.0F			*QPP
F	7E			*MATID
F	593.0F			*Td
				*CJNC
				*S
				*PJWTR1
				*PJWRF1
				*OP3TR1
				*OP3RF1

* SIDE TUBE

P 1	2.14984E+0	2.64277E+0	2.22169E+0E	*DX
	3.11487E-3	3.54537E-3	5.70588E-3E	*VJL
P 1	1.44227E-3	5.73212E-3E		*FA
	1.65244E-1	5.50315E-3P 2	4.66877E-3F	*FRIC
	1.63298E-1	5.50315E-3R 2	4.66877E-3E	*FRIC REV
	5.45100E-1R 2	0.0	6.04100E-1E	*GRAY
P 3	4.29358E-2	6.54304E-2E		*HJ
F	0E			*ICFLG
F	1F			*NFF
F	0.0F			*ALP
F	0.0F			*VL
F	0.0E			*VV
F	578.4E			*TL
F	515.0F			*TV
F	148.4E+5F			*P
F	0.0F			*PA
F	0.0F			*QPP

F 27
 2 103.4F

*HATIP
 *TW
 *CJYC
 *S
 *P3TR1
 *P3RF1
 *Q3TR1
 *Q3RF1

 * TO MAKE THIS DATA CONSISTENT AT JUNCTION 2
 * THE FOLLOWING CHANGES HAVE BEEN MADE
 * FRICTION CHANGED FROM 0.1183 TO 0.19258
 * LOSS CHANGED FROM 0.4237 TO 0.589737
 * THE NEW VALUES ARE GIVEN IN COMPONENT 1 FROM TRAC-P02 LB1 DECK
 *

STEEN		2	2 STEAM GENERATOR		
	10	0		3	9 *CN 02
	0	1		3	*CN 03
	0	1	29	22	*CN 04
	0	0	0	0.000000	*LN 05
	0	0	5		*CN 06
	17	4			*LN 07
	5.10540E-3	1.24440E-3			*LN 08
PIPE		5	0		*SECONDARY PIPE 20
TEE		4	1		*DOWNCOMER TEE 22
TEE		2	1		*STEAM DOME TEE 21

-----PRIMARY SIDE

	2.63500E-1F01	5.56950E-1	2.63500E-1E		*DX
	3.79507E-1F01	8.57500E-2	3.79500E-1E		*VNL
	5.15000E-2F01	1.91100E-1	5.15000E-2F		*FA
	0.17040 F02	0.000000	0.186100F		*FRIC
	0.17040 F04	0.000000	0.186100E		*FRIC P KE
	0.589737 F04	1.000000	0.000000F04	-1.000000	*URAV
	2.55300E-1F04	1.02110E-2	2.55000E-1E	-0.711500E	*HD
F	UF				*ICFLG
	1F04	1	1E		*NEF
F	0.000000F				*ALP
F	0.000000F				*VL
F	0.000000F				*VV
IJR	567.500000	552.800000L			*TL
IUR	567.500000	552.800000E			*TV
F	14.8400E+1F				*P
F	0.000000F				*PA

-----SECONDARY SIDE

	24	21	0	20 *PIPE 20
R04	5.68950E-1	1.11150E+0E		*UX
R04	4.43562E-1	2.77863E-1E		*VNL
	2.18894E-1F03	7.79615E-1F02	8.27762E-1F	*FA
	2.000000F05	0.000000E		*FRIC
	2.000000F05	0.000000E		*FRIC
	0.000000F05	1.00000E+0E		*URAV
R05	5.33000E-3	1.06910E+0E		*HD
F	OF			*ICFLG
F	1E			*NEF
R04	0.000000	0.258500E		*ALP
F	0.000000F			*VL
F	0.000000E			*VV
F	549.000000F			*TL
F	549.000000F			*TV
F	5.4100E+6E			*P
F	0.000000F			*PA

	23	24	25	22 *TEE 22
R02	7.41000E-1	1.70485E+0	5.68950E-1E	*DX
R02	3.82365E-1	3.73532E-1	1.24544E-1E	*VNL
R02	5.15342E-1F03	2.18898E-1E		*FA
R04	0.000000	2.000000E		*FRIC
R04	0.000000	2.000000F		*FRIC
	-1.37524E-1F03	-1.000000	0.000000F	*URAV
R02	2.54000E-1F02	1.01600E-1	5.35000E-3E	*HD

F 1.000000
 F 0.000000
 F 0.000000
 F 541.571343E
 F 541.571343E
 F 6.4100E+6E
 F 0.000000
 F 0.000000
 F 2.000000
 F 1.52144E-2E
 F 4.10737E-3E
 F 0.000000
 F 0.000000
 F 0.000000
 F 1.01500E-1E
 F 0.000000
 F 0.000000
 F 0.000000
 F 525.000000
 F 525.000000
 F 6.4100E+6E
 F 0.000000

0.776734K02 0.000000F

*ICFLG P
 *IFF P
 *ALP P
 *VL P
 *VV P
 *TL P
 *TV P
 *P P
 *PA P
 *UX S
 *VOL S
 *FA S
 *FRICE S
 *FRICR S
 *GRAY S
 *HO S
 *ICFLG S
 *NFF S
 *ALP S
 *VL S
 *VV S
 *TL S
 *TV S
 *P S
 *PA S

F 1.11157E+0E
 F 0.97867E-1
 F 0.97717E-1
 F 0.000000
 F 0.000000
 F 1.000000
 F 1.05917E+0
 F 0.000000
 F 1.000000
 F 0.000000
 F 0.000000
 F 541.571343E
 F 541.571343E
 F 6.4100E+6E
 F 0.000000
 F 0.000000
 F 7.41000E-1E
 F 3.82966E-1E
 F 5.15347E-1E
 F 0.000000
 F 0.000000
 F -3.77525E-1E
 F 2.54000E-1E
 F 0.000000
 F 1.000000
 F 0.000000
 F 0.000000
 F 541.571343E
 F 541.571343E
 F 6.4100E+6E
 F 0.000000

21 22 23
 1.23045E+0E
 1.58004E+0
 1.0000E+30
 1.0000E+30
 4.63242E-2E
 2.44600E-1E
 2.44600E-1E

21 *TEE 21

*DX P
 *VOL P
 *FA P
 *FRICE P
 *FRICR P
 *GRAY P
 *HO P
 *ICFLG P
 *NFF P
 *ALP P
 *VL P
 *VV P
 *TL P
 *TV P
 *P P
 *PA P
 *UX S
 *VOL S
 *FA S
 *FRICE S
 *FRICR S
 *GRAY S
 *HO S
 *ICFLG S
 *NFF S
 *ALP S
 *VL S
 *VV S
 *TL S
 *TV S
 *P S
 *PA S

HEAT STRUCTURES

R08	0P05	0R06	20R04	22R02	21E	*ICMP
	2	3	4	5	6	*ICELL
	7	6	45			*ICELL
R03	1P02	10S				*ICELL
	1	2	3	4R02	5	*ICELL
	1	2	3	45		*ICELL
	2	3E				*ICELL
R09	20P05	0R06	22R04	0R02	0E	*ICMP

```

      1          2          3          4          5          6          7          8
      2          15         10002        05          15
R03  4P03          3          2          15
R04  4P02          0E
R24  12P06        4P03          8R06          45
R18  4P18          4F
R08  5.12540E-3    0.665800    5.12540E-3    10.000000    0.665800    *RADI6
      5.12540E-3R04  0.644525K02    0.571500P06    0.711200E
R08  1.24467E-3    0.098900    5.18435E-3    0.031750    0.088400    *TH
      5.18435E-3R06  0.012700R06    0.053975E
R      0.000000E
R37  541.571343P12  547.500000P14  552.800000P48  541.571343E
R      0.000000F
R      0.000000E
R      0.000000E
R      0.000000F
R08  33.804952      1.388600    17.287714    0.738780    1.388600    *WA10
      17.287714R04  2.304050    2.550813    2.848253    2.214570    *WA10
      7.311234      7.427232    2.542411    4.956850    4.407864E *WA10
R08  0.000000R02    1.600000    0.000000R02    1.600000R05    0.000000    *HOL6
R05  1.600000F
R08  0.000000R02    1.600000    0.000000R02    1.600000R05    0.000000    *HOL6
R05  1.600000F
R08  0.000000R02  305.370000    0.000000R02  305.370000R06  0.000000    *TOL6
R05  305.370000F
R08  0.000000R02  305.370000    0.000000R02  305.370000R06  0.000000    *TOL6
R05  305.370000F
R08  42.162876      1.568604    38.228926    0.738780    1.568604    *WAUS
      34.228926R04  2.349480    2.719942    2.911549    2.382671    *WAUS
      3.567533      8.206045    2.735352    5.343797    4.742394E *WAUS

```

```

* DATA CHANGED TO AGREE WITH CONTROL LOGIC IN FP-1
* VALVE IS OPEN UNTIL TRIP COMES ON
* THEN VALVE IS CLOSED USING A TABLE (TIME,RELATIVE POSITION)
* TRIP 7 , SV 1

```

```

VALVE          23          23 STEAM LINE VALVE          7
      6          0          22          26          7 *LN 02
      1          0          3          5          0 *CN 03
      7          1          6          0          0 *LN 04
      0          0          0          0          0 *LN 05
      1.0F+20      0.0          0.0          1.0          0 *CN 07
      0.1214      0.0151      1.6          1.6          305.37 *LN 00
      305.37      4.63292E-2    0.242900    0.451          *CN 04
R      5.01191F
R      2.32140E-1F
R      4.63247E-2F
      0.2446 R04    0.0          5.44          0.0E
      0.2446 R04    0.0          6.4          0.0E
      1.0 R06      0.0E
R      0.2429E
R08  0          1          0F
R      1E
R      1.0 E
R      0.0 E
R      0.0 E
R      541.571343E
R      541.571343E
R08  6.4900E+6    2.1500E+6E
R      0.0 E
R
      0.0          0.451          1.0          0.4115    *VMTB1
      2.0          0.350          5.0          0.1665    *VMTB1
      7.5          0.0          1000.0        0.0E      *VMTB1

```

```

* MODIFIED TO AGREE WITH FP-1 DATA
* CONSTANT MASS FLOW UNTIL TRIP ON
* THEN MASS FLOW READ FROM A TABLE (TIME,MASS FLOW)

```

```

* TRIP * 5 * 1
*
FILL          24          24 STEAM GENERATOR FEEDWATER
      25          8          0          *CN 02
      5          1          5          0          *CN
      0.0          1.0E20          0.0          0          *CN
      2.0          1.52146E-2          0.0          482.0          *CN 05
      57.4E+5          0.0          12.800          0.0          482.0          *CN 06
      1.0          1.0          *CN 09
      0.0          12.800          1.0          2.535          *VMTB
      2.0          0.8101          2.67          0.005          *VMTB
      500.          0.004          *VMTB

```

```

-----
BREAK          25          25 STM GEN SEC BRK
      26          0          3          1          0          *CN 02
      5.011910          0.232198          1.0          498.0          21.5E5          *CN 04
      0.0          0.0          1.0E20          21.5F5          0.0          *CN 05

```

```

-----
TEE          3          3 PUMP SUCTION
      2          4          7          0.0          *ICHF 1          *CN02
*
* MAIN TUBE
*
      0          3          4          5          0          *CN03
      0          0          0          0          0          *CN04
      0.14203          0.03571          0.0          0.0          300.0          *CN05
      300.0          0.0          0.0          1.0E20          1.0          *CN06
      0.0          0.0          1.0E20          1.0          *CN07
      1.0E20          *CN08

```

```

* SIDE TUBE
*
      0          3          3          0          *CN09
      0          0          0          0          0          *CN10
      0.14203          0.03571          0.0          0.0          300.0          *CN11
      300.0          0.0          0.0          1.0E20          1.0          *CN12
      0.0          0.0          1.0E20          1.0          *CN14

```

```

* MAIN TUBE
*
      6.35000E-1          1.40340E+0          4.35000E-1E          *NX
      2.74675E-2          1.14380E-1          2.74675E-2E          *VJL
      3.56131E-2P          2 6.34249E-2          3.56131E-2E          *FA
      0.0F          *FRICF
      0.0F          *FRICR
      -5.26590E-1          -5.52200E-1          5.52200E-1S          *GRAY
      5.26590E-1F
      2.15910E-1P          2 2.84174E-1          2.15910E-1E          *HJ
      0E          *ICFLG
      1E          *HFF
      0.0E          *ALP
      0.0E          *V
      0.0E          *VV
      564.3E          *TL
      515.0E          *TY
      148.4E+5E          *P
      0.0E          *PA
      0.0E          *QPPP
      7E          *MATID
      573.0E          *TW
          *CJVC
          *S
          *PJWTR1
          *PJRRF1
          *OP3TR1
          *OP3RF1

```

```

* SIDE TUBE
*

```

```

1.71117E-1 2 1.71117E-1F
7.71717E-2 4.00000E-2 5.00481E-2E
2 5.34243E-2 5.87143E-2 5.16000E-2E
2 3 0.0 1.80100E-1E
2 3 0.0 1.80100E-1E
0.0 6.74400E-1 1.00000E+05
7.11500E-1F
2 2.94174E-1 2.45787E-1 2.56000E-1F
F 0F
F 1E
F 0.0E
F 0.0E
F 0.0E
F 564.3F
F 515.0F
F 144.4E+5E
F 0.0E
F 0.0E
F 7E
F 593.0E
*DX
*VJL
*FA
*FRIC FF=0.1861
*FRIC REV
*GRAV
*HD
*ICFLG
*NEFF
*ALP
*VL
*VV
*TL
*TV
*P
*PA
*QPPP
*MATID
*TW
*CNJC
*S
*P3TRB1
*P3RRF1
*Q3TB1
*Q3RRF1

```

```

*****
PUMP 2 4 PUMP NU. 2
2 4 6 7 *CNU2
*IC4F 1 U 2 1 1 *CNU3
4 U 0 0 0 *CNU4
0 U 0 0 *CNU5
0.10775 0.02856 6.0 6.0 300.0 *CNU5
300.0 1.42 1.3.0 0.0 *CV7
441.54 500.0 0.315 614.0 369.561 *CNU8
363.50 0.0 1.0E20 1.0 0 *CNU9
0.0 0.0 1.0E20 1.0 *CNU10

```

```

* OPTION FOR LEFT PUMP DATA
*
* 2 *CN11

```

```

* ARRAY DATA CAKOS

```

```

F 1.35213E+0E *DX
F 4.95348E+2E *VJL
F 3.45131E-2E *FA
F 0.0E *FRICF
F 0.0E *FRICR
F 5.25570E-1R 2 0.0E *GRAV
F 2.15913E-1E *HD
F 0E *ICFLG
F 1 0 1E *NEFF
F 0.0F *ALP
F 0.0 6.77 0.0E *VL
F 0.0 6.77 0.0E *VV
F 564.3F *TL
F 515.0E *TV
F 148.4E+5E *P
F 0.0F *PA
F 0.0E *QPPP
F 7E *MATID
F 593.0E *TW
*CNJC
*S
*P4PTR
*P4PRF
*Q3TB
*Q3RRF

```

* THE PUMP DATA IS THE SAME AS COMPONENT 4
 * EXCEPT FOR THE JUNCTION NUMBERS IN LUDZ

PUMP	2	4	6	7	8	9
ICHP	1	0	0	2	1	1
	0	0	0	0	0	0
0.10795	0.02858	0.0	0.0	0.0	300.0	0.0
300.0	1.43	1.43	0.0	0.0	0.0	0.0
941.54	500.0	0.319	0.0	0.0	369.551	0.0
1.43	0.0	1.0E20	1.0	1.0	0	0
0.0	0.0	1.0E20	1.0	1.0	0	0

* OPTION FOR LUDZ PUMP DATA

* 2 *CN11

* ALWAY DATA CARDS

F	1.15213E+0E					*DX
F	4.95348E-2E					*VJL
F	3.45131E-2E					*FA
F	0.0E					*FRICF
F	0.0E					*FRICR
F	4.75547E-1E	2	0.0E			*GRAV
F	2.15910E-1E					*HD
F	0E					*ICFLG
F	1	0		1E		*NEF
F	0.0E					*ALP
F	0.0	4.77		0.0E		*V _w
F	0.0	5.7		0.0E		*VV
F	544.3E					*TL
F	515.0E					*TV
F	148.4E+5E					*P
F	0.0E					*PA
F	0.0E					*QPPP
F	7E					*MATID
F	573.0E					*TW
						*CONC
						*S
						*PMPTR
						*PMPRI
						*QP3TP
						*QP3RF

.....

TEE	2	4	6	7	8	9
	0	0	0	0	0	0
0.10795	0.02858	0.0	0.0	0.0	300.0	0.0
300.0	0.0	0.0	0.0	1.0E20	1.0	0.0
0.0	0.0	1.0E20	1.0	1.0	0	0

* MAIN TUB

0	0	0	0	0	0	0
0.10795	0.02858	0.0	0.0	0.0	300.0	0.0
300.0	0.0	0.0	0.0	1.0E20	1.0	0.0
0.0	0.0	1.0E20	1.0	1.0	0	0

* SIDE TUB

0	0	0	0	0	0	0
0.10795	0.02858	0.0	0.0	0.0	300.0	0.0
300.0	0.0	0.0	0.0	1.0E20	1.0	0.0
0.0	0.0	1.0E20	1.0	1.0	0	0

* MAIN TUBE

1.10810E+0	1.11760E+0E					*DX
------------	-------------	--	--	--	--	-----

```

4.74557E+2 1.44017E+06
R 2 3.45131E+2F 1 3.34244E+2F
R 2 0.0 0.0E
R 2 0.0 0.0E
F 0.0F
R 2 2.15910E-1 2.84174E-10
F 0E
F 1E
F 0.0F
F 0.0F
F 0.0F
F 514.3E
F 615.0E
F 148.4E+5E
F 0.0E
F 0.0E
F 7E
F 503.0E

```

```

*VJL
*FA
*FRIC PS=CL 1FR=0.12
*FRIC MEV FR=0.12 ?
*GRAV
*HD
*ICFLG
*NEF
*ALP
*VL
*VV
*TL
*TV
*P
*PA
*OPPP
*MATID
*TW
*CONC
*S
*POWTR1
*POWRF1
*OP3TB1
*OP3RF1

```

```

*
* SIDE TUBE
*

```

```

5.42220E-1E
2.94344E-2F
F 3.45131E+2F
F 0.0E
F 0.0E
F 0.0E
F 2.159 1E
F 0E
F 1F
F 0.0E
F 0.0E
F 0.0E
F 514.3E
F 615.0E
F 148.4E+5E
F 0.0E
F 0.0E
F 7E
F 573.0E

```

```

*DX
*VJL
*FA
*FRICF
*FRICR
*GRAV
*HD
*ICFLG
*NEF
*ALP
*VL
*VV
*TL
*TV
*P
*PA
*OPPP
*MATID
*TW
*CONC
*S
*POWTR1
*POWRF1
*OP3TB1
*OP3RF1

```

```

*****
TEE
5 4 7 7 INTACT-LOOP COLD LEG
0.0 *ICHF* 1 *CN02
*
* MAIN TUBE
*
0 9 8 9 0 *CN03
0 0 0 0 *CN04
0.14209 0.33571 6.0 6.0 300.0 *CN05
300.0 0.0 0.0 1.0E20 1.0 *CN07
0.0 0.0 1.0E20 1.0 *CN08
*
* SIDE TUBE
*
0 1 14 0 *CN09
0 0 0 0 *CN10
0 0 0 0 *CN11

```


	1.117477E+1	1.117477E+1	2.000000E+1P	0.0
	5.748170E-1	5.748170E-1	1.277000E+2E	*VCL
R 3	5.552570E-1	5.732122E-3E		*FA
R 3	0.0	4.66877E-3E		*FKILF
R 3	0.0	4.66877E-3E		*FRICR
R 3	-1.00000E+0	-5.04101E-1E		*GRAV
R 3	4.48367E-1	8.54309E-2E		*H3
R				*ICFLG
R				*NRF
R	0.7174	0.0000	0.0E	*ALP
R	0.0E			*VL
R	0.0E			*VV
R	514.3E			*TL
R	514.3E			*TV
R	148.4E+5	148.361E+5	148.223E+5E	*P
R	0.0E			*P3
R	0.0E			*QPPP
R	7E			*MAT10
R	514.3E			*T4
				*C34C
				*S

 * CONSTANT VELOCITY - SET TO ZERO
 *

FILL	93	93	93	93	93	93 PRESSURISER OUTLET	
	1	1	0	0	0		*CN02
	0.0	1.0E20	0.0	0.0	0.0		*CN03
	4.66877E+1	2.4414E+2	0.0	0.0	550.3		*CN04
	148.4E+5	0.0	0.0	0.0	550.3		*CN05
							*CN06
							*CN07
							*CN08
							*CN09
							*CN10

 * CONSTANT VELOCITY - SET TO ZERO
 *

FILL	11	11	11	11	11	11 ACCUMULATOR TOP	
	1	1	0	0	0		*CN02
	0.0	1.0E20	0.0	0.0	0.0		*CN03
	0.555	0.007	0.0	0.0	300.0		*CN04
	43.0E5	43.0E5	0.0	0.0	300.0		*CN05
							*CN06
							*CN07
							*CN08
							*CN09
							*CN10

 * NOTE THAT MODES*0 GIVING NO WALL-FLUID HEAT TRANSFER
 *

TEE	1	0	12	12	12	12 ECC LINE - HP15	
	1	0	7	0.0	0		*CN02
* MAIN TUBE							
	0	1	15	14	0		*CN03
							*CN04
							*CN05
	0.0436625	0.0134674	0.0	6.0	300.0		*CN06
	300.0	0.0	0.0	1.0E20	1.0		*CN07
							*CN08

* SIDE TUBE							
	0	1	18	0			*CN09
							*CN10
							*CN11
							*CN12
	0.0436625	0.0134674	0.0	6.0	300.0		*CN13
	300.0	0.0	0.0	1.0E20	1.0		*CN14


```

* MAIN TUBE
*
F 1.00000E+0F
F 5.99220E-3E
F 5.99220E-3F
      0.0      0.4941  E
      0.0      0.4941  F
F 0.0F
F 8.73252E-2F
F 0F
F 1E
F 0.0F
F 0.0F
F 0.0E
F 450.0F
F 615.0F
F 148.4E+5F
F 0.0F

```

```

*DX
*VJL
*FA
*FRICF
*FRICR
*GRAY
*HD
*ICFLG
*NEFF
*ALP
*VL
*VV
*TL
*TV
*P
*PA
*QPPP
*MATID
*TW
*CONC
*S
*P3WTB1
*P3WRF1
*Q3TB1
*Q3RF1

```

```

* SIDE TUBE
*
F 5.00000E+0F
F 4.99555E-3F
F 9.07132E-4E
      0.0E
      0.0E
      0.0F
F 3.39952E-2E
      0F
      1E
      0.0E
      0.0E
      0.0F
      450.0F
      615.0E
      148.4E+5F
      0.0E

```

```

*DX
*VJL
*FA
*FRICF
*FRICR
*GRAY
*HD
*ICFLG
*NEFF
*ALP
*VL
*VV
*TL
*TV
*P
*PA
*QPPP
*MATID
*TW
*CONC
*S
*P3WTB1
*P3WRF1
*Q3TB1
*Q3RF1

```

* NOTE THAT NODES=0 GIVING NO WALL-FLUID HEAT TRANSFER

```

*
TEE      1      0      13      13 ECC LINE - LPIS
          1      0      7      0.0      0      *C402
*
* MAIN TUBE
*
          0      1      15      15      0      *C403
          *C404
          *C405
0.7435625  0.0134874  0.0  5.0  300.0  *C406
          300.0  0.0  0.0  1.0E20  1.0  *C407
          *C408

```

1	2	3	4	5	6
5	1	2	0	0	
0	0	0.0	0.0	0.0	
20.0	0.0	0.0	0.0	0.0	
4.35624E-2	1.34674E-2	6.0	6.0	300.0	
300.0	5.547E-2	2.636E-1	0.0	0.0	

*CN04
*CN05
*CN06
*CN07
*CN08
*CN09
*CN10

* ARRAY DATA

F	1.07227E+0E				*DX
F	7.41555E-2E				*VDL
	3.79522E-2E	2	5.54700E-2E		*FA
	0.013521		0.004551	44.5155	*FRICF
	0.013521		0.004551	44.5155	*FRICR
	-1.0E	2	0.0E		*GRAY
	2.04520E-1E	2	2.63500E-1E		*HJ
F	0E				*ICFLG
F	1E				*NFF
F	0.0E				*ALP
F	0.0E				*VL
F	0.0E				*VV
	307.2		400.0E		*TL
	525.6		615.0E		*TV
	43.0E5		148.4E+5E		*P
F	0.0E				

0.0 1.0 10000.0 1.0 E

*CR1
*T2
*R
*OP3TR
*OP3RF

* NOTE THAT NODES 0 GIVING NO WALL-FLUID HEAT TRANSFER
* UNKNOWN VALUES FOR RADII AND THICKNESS OF PIPE

PIPE			15	15	ACCUMULATOR	
	3	0	11	17	0	*CN02
	1	0	1	0		*CN03
	1.0	0.1	0.0	0.0	300.0	*CN04
	300.0	0.0	0.0	1.0E20	1.0	*CN05
						*CN06
						*CN07
						*CN08

* ARRAY DATA

	0.545		0.9516	1.1250CF-2E	*DX
	0.707		1.166	1.4077E-2E	*VDL
F	1.25133E+0		3.26522E-2E		*FA
R	0.0		0.013521	E	*FRICF
R	0.0		0.013521	E	*FRICR
F	-1.0E				*GRAY
R	1.25954E+0		2.04520E-1E		*HJ
F	0E				*ICFLG
F	1E				*NFF
F	1.0		0.0	0.0E	*ALP
F	0.0E				*VL
F	0.0E				*VV
F	307.2E				*TL
F	307.2E				*TV
F	43.0E5				*P
F	43.0E5	R2	0.0	E	*PA
					*QPPP

*RTIP
 *TW
 *CUNC
 *S
 *PJWTR1
 *PJWRF1
 *QP3TR1
 *QP3RF1

 * USES TRIP 2 AND SIGNAL VARIABLE 3
 * CONSTANT VELOCITY UNTIL TRIP ON THEN PRESSURE-VELOCITY TABLE
 *

FILL	15	16	HPIS INJECTION		
18	7	0			*CN02
2	3	4	0	0	*CN03
0.0	1.0E20	0.0	0.0	0	*CN04
5.0	4.53955E-3	0.0	0.0	307.2	*CN05
1.0E+5	0.0	0.0	0.0	307.2	*CN06
					*CN07
					*CN08
1.0	1.0				*CN09
					*CN10

*
 * FILL TABLE = (PRESSURE, VELOCITY)
 * THIS IS FOR L2-R4LB-1 AND FP-1
 *

1.0000E+0	1.76554	0.85013E+5	1.765545	*VNTB
23.589E+5	0.73564	1000.0E+5	0.73564E	

 * USES TRIP 2 AND SIGNAL VARIABLE 1
 * CONSTANT MASS FLOW UNTIL TRIP ON THEN TIME-MASS FLOW TABLE
 *

FILL	17	17	ILCL ACCUMULATOR & INJECTION		
19	8	0			*CN02
3	1	-13	0	0	*CN03
0.0	1.0E20	0.0	0.0	0	*CN04
1.0	4.98920E-3	0.0	0.0	303.0	*CN05
41.4E+5	0.0	0.0	0.0	303.0	*CN06
					*CN07
					*CN08
1.0	1.0				*CN09
					*CN10

*
 * FILL TABLE = (TIME, MASS FLOW)
 * FOR FP-1
 *

0.0	0.0	0.2	3.0 S	*VNTB
2.0	10.8	4.0	13.8 S	
6.0	15.6	8.0	19.8 S	
12.0	15.3	16.0	14.5 S	
28.0	13.0	52.0	11.0 S	
69.0	3.4	70.0	0.0 S	
100.0	0.0E			
78.0	4.6	100.0	8.6 S	
136.0	7.0	145.0	7.4 S	
1070.0	7.4E			

 * RENAMED AS USED IN L2/3 DECK FOR IRAC-PF1(M3D1)
 * ICHP=1
 *

TEE	31	31	BRUKEY-LOOP HOT LEG		
2	4	7	0.0	1	*CN02
	26	31	32	0	*CN03
					*CN04
					*CN05
0	0	0	0	0	*CN06
0.14207	0.03571	0.0	6.0	300.0	

```

      1.0000      0.0      0.0      1.0000      1.0      *C409
      0.0      0.0      1.0000      1.0      *C40A
* SIDE FJHF
      0      0      0      0      *C409
      0      0      0      0      *C410
      0.13795      0.32858      0.0      5.0      100.0      *C412
      300.0      0.0      0.0      1.0000      1.0      *C413
      0.0      0.0      1.0000      1.0      *C414
* MAIN FJHF
*
R 3 5.58490E-1      5.25780E-1      4.47490E-1      5.58510E-1      1.98750E+05 *DX
R 2 1.07720E+0      1.98750E+0      5.10290E-1      5.46290E-1      4.86280E-15 *UX
      7.84000E-1      1.71490E-1      3.00000E-1      2.79400E-1R 2 2.11840E-15 *UX
R4 0.18717      0.24922      0.244476      0.81597R E      *UX
*
R 3 4.24400E-2      4.72800E-3      3.75790E-3      4.55030E-3      1.26860E-15 *VOL
R 2 1.13530E-1      1.76860E-1      4.07280E-3      4.26350E-3      3.17150E-35 *VOL
      2.75000E-2      1.85000E-2      1.84000E-2      6.85060E-3R 2 1.76670E-35 *VOL
R4 0.0018574      0.002492      0.00204496      0.042344R E      *VOL
*
R 3 4.34250E-2      1.34130E-2R 3 0.36470E-3R 3 1.91410E-2R 3 8.36470E-35 *FA
      4.34250E-2R 2 7.46290E-3      5.34250E-25 *FA
R4 4.35470E-3R1 5.14560E-2E *FA
*
      0.0      0 2 2.20351E-1      2.39561E-1      2.54000E-1      0.05 *FRICF
      7.72000E-3R 3 1.40000E-2      1.93000E-2R 3 0.0      1.40000E-15 *FRICF
      1.70000E-1      1.12000E-1R 2 0.0      4.39700E-2R4      0.05 *FRICF
      0.018403R 0.347732      0.0 E *FRICF
      0.035      4 2 2.20351E-1      2.39561E-1      2.54000E-1      0.05 *FRICR
      7.72000E-3R 3 1.40000E-2      1.93000E-2R 3 0.0      1.40000E-15 *FRICR
      1.70000E-1      1.12000E-1R 2 0.0      4.39700E-2R4      0.05 *FRICR
      0.018403R 0.347732      0.0 E *FRICR
*
R 4 0.0      4.71372E-1R 2 1.00000E+0      0.0R 5-1.00000E+05 *GRAV
      -4.45355E-1R 2 0.0      2.91528E-15 *GRAV
R 5 1.00000E+0      0.492407 *3      0.0E *GRAV
*
R 3 2.84000E-1      1.14000E-1R 3 1.03000E+1R 3 1.75000E-2R 3 1.03000E-15 *HD
      2.84000E-1R 2 1.14000E-2      2.84000E-15 *HD
R4 1.03200E-1R1 2.57200E-1E *HD
*
R25 0      2      UF *ICFLG
      1F *NFF
      0.0F *ALP
      0.0E *VL
      0.0E *VV
*
R 2 5.55500E+2      5.55120E+2      5.564770E+2      5.54450E+2      5.564070E+25 *TL
      5.52730E+2      5.52000E+2      5.51280E+2      5.59930E+2      5.59590E+25 *TL
      5.53220E+2      5.56840E+2      5.58720E+2      5.58600E+2      5.58400E+25 *TL
      5.58210E+2      5.58070E+2      5.57920E+2      5.57800E+2      5.57670E+25 *TL
      5.57550E+2      5.57420E+25 *TL
      5.57270E+2      5.57100E+2      5.56760E+2E *TL
*
R      615.0F *TV
      148.4E+5F *P
      0.0F *PA
      0.0E *QPPP
      7F *MATIO
*
R 4 5.65500E+2R 4 5.65120E+2R 4 5.64770E+2R 4 5.64450E+2R 4 5.64070E+25 *TW
R 4 5.62730E+2R 4 5.62000E+2R 4 5.61280E+2R 4 5.59930E+2R 4 5.59590E+25 *TW
R 4 5.53220E+2R 4 5.56890E+2R 4 5.58720E+2R 4 5.58500E+2R 4 5.58400E+25 *TW
R 4 5.58210E+2R 4 5.58070E+2R 4 5.57920E+2R 4 5.57800E+2R 4 5.57670E+25 *TW
R 4 5.57550E+2R 4 5.57420E+25 *TW
R 4 5.57270E+2R 4 5.57100E+2R 4 5.56760E+2E *TW

```

*CJNC
 *S
 *PQWTR1
 *PQWRF1
 *QP3TR1
 *QP3RF1

```

*
* SIDE TUBE
*
1.38707E+0      8.14000E-1      5.10440E+0E      *DX
5.40007E-2      3.14000E-2      1.98700E-1E      *VJL
* 3 3.8800E+2      3.3300E-03E      *FA
* 1 0.0      0.0E      *FRICF
* 1 0.0      0.0E      *FRICR
0.0      2.24200E-1      1.91200E-15      *GRAY
0.0E
* 1 2.22300E-1      65.200E-3E      *HD
* 0E      *ICFLG
* 1E      *NEF
* 0.0E      *ALP
* 0.0E      *VL
* 0.0E      *VV
* 565.5E      *TL
* 515.0E      *TV
* 148.4E+5E      *P
* 0.0E      *PA
* 0.0E      *OPPP
* 7E      *MATID
* 565.5E      *Td
*      *CJNC
*      *S
*      *PQWTR1
*      *PQWRF1
*      *QP3TR1
*      *QP3RF1

```

 * CONSTANT VELOCITY - SET TO ZERO
 *

```

*
* FILL      32      32      32 BROKEN-HOT-LEG TERMINAL
*      32      1      0
*      0.0      1.0E20      0.0      0.0      *CNO2
0.815975  0.0423448  0.0      0.0      555.5      *CNO3
148.4E+5  0.0      0.0      0.0      555.5      *CNO4
*      *CNO5
*      *CNO6
*      *CNO7
*      *CNO8
*      *CNO9
*      *CNO10

```

 * REVISED AS USED IN L2/3 DECK FOR TRAC-PF1(MD01)
 * ICHP=1
 *

```

*
* TEE      2      4      41      41 BROKEN-LOOP COLO LEG TEE
*      2      4      7      0.0      1      *CNO2
*
* MAIN TUBE
*
0      2      41      46      0      *CNO3
0      0      0      0      0      *CNO4
0.14209  0.03571  6.0      6.0      300.0      *CNO5
300.0      0.0      0.0      1.0E20      1.0      *CNO6
0.0      0.0      1.0E20      1.0      *CNO7
*      *CNO8
*
* SIDE TUBE
*
0      2      43      0      *CNO9
0      0      0      0      0      *CNO10
0.10775  0.02666  6.0      6.0      300.0      *CNO11
*      *CNO12

```

* SIDE TRIP

	0	1	19	0		*CNO9
						*CNO10
						*CNO11
						*CNO12
						*CNO13
						*CNO14

* MAIN TRIP

	4.35783E+0F					*DX
	1.04557E-1F					*YJL
	5.54700E-2	5.98920E-3E				*FA
	49.5155		0.0E			*FRICF
	49.5155		0.0E			*FRICR
F	0.0E					*GRAV
	7.43503E-1	8.73252E-2E				*HJ
F	0F					*ICFLG
Z	1E					*NEF
F	0.0E					*A_P
F	0.0F					*V_
F	0.0F					*VV
F	400.0E					*T_
F	615.0F					*TY
F	149.4E+5F					*P
F	0.0E					*PA
						*QPPF
						*MATID
						*TW
						*CJNC
						*S
						*PJWTR1
						*PDWRF1
						*OP3TR1
						*OP3RF1

* SIDE TRIP

	1.0E					*DX
	5.73220E-3E					*YJL
F	5.73220E-3E					*FA
F	0.0F					*FRICF
F	0.0E					*FRICR
F	0.0E					*GRAV
F	8.73252E-2E					*HJ
F	0F					*ICFLG
F	1E					*NEF
F	0.0F					*A_P
F	0.0F					*V_
F	0.0E					*VV
F	400.0E					*T_
F	615.0E					*TY
F	149.4E+5F					*P
F	0.0F					*PA
						*QPPF
						*MATID
						*TW
						*CJNC
						*S
						*PJWTR1
						*PDWRF1
						*OP3TR1
						*OP3RF1

* VALVE IS CONTROLLED BY TRIP 5.

VALVE	2	19	17	16	7	*CNO7
-------	---	----	----	----	---	-------

100.0 0.0 0.0 1.0E20 1.0 10013
 0.0 0.0 1.0E20 1.0 *CN14

* MAIN TUBE

R2	0.00774				E	*DX
R2	0.0512674				E	*YDL
R3	0.053425				L	*FA
	0.0	1.047	0.030579	E	*FRIC YSL-BLCL	-0.17
F	0.1291	1.847	0.033579	E	*FRIC BLCL-YSL	0.129
F	0.0					*GRAY
R3	0.274				E	*HD
R3		0		E		*ICFLG
F		1F				*NEF
F		0.0E				*ALP
F		0.0E				*VL
F		0.0E				*VY
	560.25	562.40			L	*TL
F		516.38E				*TV
F		148.4E+5E				*P
F		0.0E				*PA
F		0.0E				*QPPP
F		7E				*MATID
	560.9	561.01	R2 561.03			*TW
	562.51	R2 562.58E				*TW
						*CONC
						*S
						*PQWTB1
						*POWERF1
						*QP3TB1
						*QP3RF1

* SIDE TUBE

	8.95000E-1	7.28340E+0E			*DX
	3.03300E-2	2.76800E-1E			*YDL
R 2	0.0388	3.3300E-03E			*FA
R 2	0.0	0.0E			*FRIC
R 2	0.0	0.0E			*FRIC
	0.0	1.79000E-1	0.0E		*F'ICP
R 2	2.22300E-1	55.700E+3E			*LAV
F		UF			0
F		1E			ICFLG
F		0.0F			*NEF
F		0.0F			*ALP
F		0.0E			*VL
	553.30	562.88 E			*VY
F		515.0E			*T
F		148.4E+5E			*TV
F		0.0F			*P
F		0.0E			*PA
F		7E			*QPPP
F		553.3E			*MATID
					*TW
					*CONC
					*S
					*PQWTB1
					*POWERF1
					*QP3TB1
					*QP3RF1

 * -- TRIP 200

VALVE	43	43	BROKEN-LOOP	CUL3	LED	VALVE	
	4	4	44	42	7		*CN02
	0	0	3	2	0		*CN03
	207	1	-4	0	0		*CN04
	0	0	0	0	0		*CN05
	0	0					*CN06
	1.0E+20	0.0	0.0	0.0			*CN07
	1.4209E-01	3.5710E-02	6.0	6.0	3.00E+02		*CN08

```

1.0 1.0 1.0 1.0 1.0 1.0
0.0 0.0 0.0 0.0 0.0 0.0
*
* ARRAY DATA
*
0.80774 0.517081 1.145074 1.02234
0.0512576 0.00505142 0.02623801 0.0472489
1.043125 0.013875 0.0083047 0.02352 0.051955
0.010479 0.0 0.1515 0.0460103 0.1717
0.010479 0.0 0.1515 0.0460103 0.1717
0.284 0.13292 0.1032 0.17305 0.2572
R2 0 2 R2 0
R 1
R 0.0
R 0.0
R 0.0
554.53 543.72 551.41 550.35
R 616.39
R 143.4E+5
R 0.0
R 0.0
R 7
R4 554.47 R4 554.0 R4 552.0 R4 551.0
*
0.0 1.0 2.5 0.55
5.0 0.0 1000.0 0.0
*
* *****
* CONSTANT VELOCITY - SET TO ZERO
*
FILL 42 42 42 BROKEN-COLD-LEG TERMINAL
42 1 0 *CNO2
0.0 1.0E20 0.0 0.0 *CNU3
1.07235 0.0472489 0.0 0.0 550.3 *CNO4
143.4E+5 0.0 0.0 0.0 550.3 *CNU5
*CNO6
*CNO7
*CNO8
*CNO9
*CNO10
*
* *****
*
* PIPE 81 81 UPPER PLENUM INJECTION PIPE
1 1 51 81 7 *CNO2
0 0 0 0 *CNO3
3.505200E+02 3.555000E-03 0. 0. 3.072000E+02 *CNO4
3.072000E+02 0.0 0.0 1.0E20 1.0 *CNU5
*CNO6
*CNO7
*CNO8
*
* ARRAY DATA
*
R 2.9000E+00E *DX
R 2.4124E-03E *VCL
R 0.6497E-04E *FA
R 0. *FRIL
R 0. *FRIL
R 1.0000E+00E *GRAY
R 3.5052E-02E *HU
R 0. *ICFLU
R 0. *NKF
R 0. *ALP
R 0. *VL
-2.4327E-05E

```


9.
 F 4.9792E+02F
 F 4.1541E+02F
 F 1.5190E+07E
 F 0.0 E

-7.7177E+05L

* VV
 * TL
 * TV
 * P
 * PA
 * QPPP
 * MATIU
 * TW
 * CONC
 * S
 * POWTB1
 * POWRF1
 * QP3TB1
 * UP3RF1

FILL

61		61 UPPER PLENUM INJECTION		
A1	B	0	0	
1013	1	21	0	
0.0	1.0E20	0.0	0	*CN02
2.500000E+00	2.412430E-03	0.	0.	*CN03
41.400000E+05	0.	0.	3.080000E+02	*CN04
				*CN05
				*CN06
				*CN07
				*CN08
				*CN09
				*CN10
0.0825				
0.0	0.0	1.0	0.05	* VMTB
78.0	7.2	40.0	5.25	
78.0	0.0	100.0	0.05	
200.0	0.67	255.0	0.705	
260.0	0.0	266.0	1.805	
272.0	0.50	349.0	0.505	
347.0	31.0	352.0	30.05	
358.0	20.0	353.0	18.25	
375.0	16.9	400.0	10.05	
445.0	4.0	450.0	0.05	
1000.0	0.0E			

PIPE

82		82 UPPER PLENUM INJECTION PIPE		
1	0	62	82	7
0	0	0	0	
3.505200E-02	3.555000E-03	0.	0.	*CN02
3.072000E+02	0.0	0.0	1.0E20	*CN03
				*CN04
				*CN05
				*CN06
				*CN07
				*CN08

* ARRAY DATA

F 2.5000E+00E
 F 2.4124E-03F
 F 9.6497E-04E
 F 0. E
 F 0. E
 F 1.0000E+00E
 F 3.5052E-02E
 F 0 E
 F 1E
 F 1.8330E-06F
 0.
 0.
 F 5.9792E+02F
 F 4.1535E+02F
 F 1.5200E+07F
 F 0.0 E

-1.2684E-05E
 -1.2684E-05E

* DX
 * VOL
 * FA
 * FRIC
 * FRIC
 * GRAY
 * HD
 * IC+LG
 * NFF
 * ALP
 * VL
 * VV
 * TL
 * TV
 * P
 * PA
 * QPPP
 * MATIU

* YW
 * C2XL
 * S
 * POWTR1
 * POWRF1
 * QP3T81
 * QP3RF1

```

FILL          #G          52 UPPER PLENUM INJECTION          *CN02
          62          0          U          0          0          *CN03
          1010          1          21          0          0          *CN04
          0.0          1.0E20          0.0          0.          0.          *CN05
2.800000E+00  2.412430E-03  0.          0.          3.080000E+02  *CN06
41.400000E+05  0.          0.          *CN07
          *CN08
          0.3875          *CN09
          *CN10
          0.0          0.0          1.0          0.05          * VMTB
          78.0          7.2          40.0          5.95
          78.0          0.0          100.0          0.05
          200.0          0.67          255.0          0.735
          210.0          0.0          268.0          1.835
          272.0          0.40          345.0          0.405
          347.0          31.0          352.0          30.05
          358.0          20.0          363.0          18.25
          375.0          16.9          400.0          10.05
          445.0          4.0          450.0          0.05
          1000.0          0.0E
  
```

```

PIPE          #J          83 UPPER PLENUM INJECTION PIPE          *CN02
          1          0          83          #3          7          *CN03
          0          0          0          0          *CN04
          *CN05
          3.405200E-02  3.555000E-03  0.          0.          3.072000E+02  *CN06
          3.072000E+02  0.0  0.0  1.0E20  1.0          *CN07
          *CN08
  
```

* ARRAY DATA

```

F 2.5000E+00F
F 2.4124E-03F
F 2.5437E-04E
F 0.          E
F 0.          E
F 1.0000E+00F
F 3.4052E-02F
F 0          E
F          1F
F 2.4250E-06F
0.          -1.2657E-05E
0.          -1.2657E-05E
F 5.0791E+02E
F 5.1575E+02E
F 1.5100E+07F
F 0.0          E
  
```

* DX
 * YUL
 * FA
 * FRIC
 * FRIC
 * GRAY
 * HU
 * ICFLG
 * IFF
 * ALP
 * VL
 * VV
 * TL
 * TV
 * P
 * PA
 * QPPP
 * MATIU
 * TW
 * CONC
 * S
 * POWT81
 * POWRF1
 * QP3T81
 * QP3RF1

```

*****
FILL
      63          63          53 UPPER PLENUM INJECTION
      1010          1          0          0          0
      0.0          1.0E20          0.0          0.0          0.0
      2.500000E+00  2.412430E-01  0.0          0.0          3.080000E+02
      41.400000E+05  0.0          0.0          0.0          0.0
      0.0825
      0.0          0.0          1.0          0.05          * VMTB
      78.0          7.2          40.0          5.95
      78.0          0.0          100.0          0.05
      270.0          0.67          255.0          0.705
      250.0          0.0          266.0          1.805
      272.0          0.50          345.0          0.505
      347.0          31.0          352.0          30.05
      358.0          20.0          363.0          18.25
      375.0          16.9          400.0          10.05
      445.0          4.0          450.0          0.05
      1000.0          0.0E

```

```

*****
PIPE
      1          64          64 UPPER PLENUM INJECTION PIPE          7
      0          0          0          64          64          0
      3.505200E-02  3.555000E-03  0.0          0.0          3.072000E+02
      3.072000E+02  0.0          0.0          1.0E20          1.0

```

```

*
* ARRAY DATA
*
F  2.50000E+00F
F  2.4124E-03E
F  3.6497E-04E
F  0.0          E
F  0.0          F
F  1.03000E+00E
F  3.5052E-02E
F  0          E
F  0          1E
F  2.5303E-05E
F  0.0          -1.2758E-05E
F  0.0          -1.2758E-05E
F  5.4791E+02E
F  5.1536E+02E
F  1.5200E+07E
F  0.0          E

```

- * CN02
- * CN03
- * CN04
- * CN05
- * CN06
- * CN07
- * CN08
- * DX
- * YUL
- * FA
- * FRIC
- * FRIC
- * GRAY
- * HD
- * ICFLG
- * NFF
- * ALP
- * VL
- * VV
- * TL
- * TV
- * P
- * PA
- * UPPP
- * HATI
- * TW
- * CONC
- * S
- * POWTE1
- * POWRF1
- * QP3TB1
- * QP3RF1

```

*****
FILL
      64          64          54 UPPER PLENUM INJECTION
      1010          1          0          0          0
      0.0          1.0E20          0.0          0.0          0.0

```

2.50000E+00 2.41243E+03 0. 0. 3.072000E+02 *CN05
 41.40000E+05 0. 0. *CN06
 *CN07
 *CN08
 *CN09
 *CN10

0.0875

0.0	0.0	1.0	0.05	* VMTR
38.0	7.2	40.0	5.95	
78.0	0.0	100.0	0.05	
270.0	0.87	255.0	0.705	
260.0	0.0	266.0	1.805	
272.0	0.50	345.0	0.505	
347.0	31.0	352.0	30.05	
375.0	20.0	363.0	18.25	
375.0	10.9	400.0	10.05	
445.0	4.0	450.0	0.05	
= 1070.0	0.0E			

 *
 *

PIPE 65 65 UPPER PLENUM INJECTION PIPE 65 7 *CN02
 1 U *CN03
 0 U *CN04
 *CN05
 3.505200E+02 3.554000E+03 0. 0. *CN06
 3.072000E+02 0.0 0.0 1.0E20 1.0 *CN07
 *CN08

* BRACKY DATA

2.5000E+00F	* DX
2.4124E+03F	* VOL
2.6497E+04F	* FA
0. F	* FRIC
0. F	* FRIC
1.0000E+00E	* GRAY
3.5052E+02F	* HU
0. E	* ICFLG
0. 1F	* NPF
4.7080E+06F	* ALP
0. -1.2837E+05E	* VL
0. -1.2837E+05E	* VV
6.0791E+02F	* TL
6.1537E+02F	* TV
1.9203E+07F	* P
0.0 F	* PA
	*UPPP
	*MATID
	*TW
	*COND
	*S
	*POWTB1
	*POWRF1
	*QP3TB1
	*QP3RF1

 *
 *

FILL 65 65 UPPER PLENUM INJECTION 65 *CN02
 1010 8 *CN03
 0.0 1.0E20 0.0 0 0 *CN04
 2.500000E+00 2.412430E+03 0. 0. 3.080000E+02 *CN05
 41.40000E+05 0. 0. *CN06
 *CN07
 *CN08
 *CN09
 *CN10
 0.1675
 0.0 0.0 1.0 0.05 * VMTR

375.0	17.7	400.0	10.05
445.0	4.0	450.0	0.05
1070.0	0.0E		

```

*
*****
*
PIPE          87          87 UPPER PLENUM INJECTION PIPE
              1          67          87          7
              0          0          0          0
3.405200E+02 3.455000E+03 0.          0.          3.072000E+02
3.072000E+02 0.0          0.0          1.0E20  1.0

```

```

*
* ARRAY DATA
*
F 2.40000E+00F
F 2.4124E-03F
F 2.6697E-04F
F 0.          E
F 0.          F
F 1.00000E+00E
F 3.40520E-02E
F 0          F
F 0          LE
F 4.9541E-06E
0.          +1.2082E-05E
0.          -1.2082E-05E
F 4.9730E+02E
F 4.1537E+02E
F 1.5203E+07E
F 0.0          E

```

- * DX
- * VOL
- * FA
- * FRIC
- * FRIC
- * GRAY
- * HD
- * ICFLG
- * HFF
- * ALP
- * VL
- * VV
- * TL
- * TV
- * P
- * PA
- * OPFF
- * MATIU
- * TW
- * CDNC
- * S
- * PDWT01
- * PDWRF1
- * QP3TB1
- * UPJRF1

```

*
*****
*
FILL          67          87 UPPER PLENUM INJECTION
              67          8          21          0          0
              1010          1          0.0          0.0
0.0          1.0E20          0.0          0.0          3.080000E+02
2.500000E+00 2.412430E-03 0.          0.          *CN02
41.400000E+05 0.          0.          *CN03
*CN04
*CN05
*CN06
*CN07
*CN08
*CN09
*CN10
0.1675
0.0          0.0          1.0          0.05          * YMTB
30.0          7.2          40.0          5.95
78.0          0.0          100.0          0.05
200.0          0.67          255.0          0.725
260.0          0.0          266.0          1.805
272.0          0.50          345.0          0.505
347.0          31.0          352.0          30.05
356.0          20.0          363.0          18.25
375.0          10.9          400.0          10.05
445.0          4.0          450.0          0.05
1000.0          0.0E

```

```

*
*****
*
PIPE          88          88 UPPER PLENUM INJECTION PIPE

```

1	1	58	88	7	CN02
0	0	0	0	0	CN03
					CN04
					CN05
1.505200E+02	3.555000E+01	0.	0.	3.072000E+02	CN06
3.072000E+02	0.0	0.0	1.0E20	1.0	CN07
					CN08

```

*
* APRAY DATA
*
F 2.50000E+00E
F 2.41245E+03E
F 9.64977E+00E
F 0.
F 0.
F 1.00000E+00E
F 3.50520E+02E
F 0
F 1F
F 4.47215E-06E
D. -1.27405E-05E
D. -1.27405E-05E
F 5.97904E+02E
F 5.15377E+02E
F 1.52030E+07E
F 0.0 E

```

- * DX
- * VOL
- * PA
- * FRIC
- * FRIC
- * GRAY
- * HD
- * TCFLD
- * HFF
- * ALP
- * VL
- * VV
- * TL
- * TV
- * P
- * PA
- * QPPP
- * HATI
- * TW
- * CONC
- * S
- * POWT61
- * POWRF1
- * QP3TB1
- * UP3RF1

```

*****
*
*
FILL

```

	58	88	58 UPPER PLENUM INJECTION						
	1010	1	21	0	0	0			CN02
	0.0	1.0E20	0.0						CN03
2.500000E+00	2.412430E+03	0.	0.			3.080000E+02			CN04
41.400000E+05	0.	0.							CN05
									CN06
									CN07
0.1675									CN08
									CN09
									CN10
0.0	0.0	1.0	0.05	* VMTR					
38.0	7.2	40.0	5.95						
78.0	0.0	100.0	0.05						
200.0	0.47	255.0	0.705						
260.0	0.0	265.0	1.805						
272.0	0.40	345.0	0.505						
347.0	31.0	242.0	30.05						
358.0	20.0	363.0	18.25						
375.0	16.9	400.0	10.05						
445.0	9.0	450.0	0.05						
1000.0	0.0E								

```

*****
*
*
PIPE

```

	84	89	89 UPPER PLENUM INJECTION PIPE						
	1	0	69	89	7				CN02
	0	0	0	0					CN03
									CN04
									CN05
1.505200E+02	3.555000E+03	0.	0.			3.072000E+02			CN06
3.072000E+02	0.0	0.0	1.0E20	1.0					CN07
									CN08

F 0.0 F
 F 1.00000E+00F
 F 3.5052E-02F
 F 0 F
 F 1F
 F 1.7754E-06F
 F 0. -1.2505E+05E
 F 0. -1.2506E-05E
 F 5.0784E+02F
 F 4.1538E+02F
 F 1.5204E+07F
 F 0.0 F

- * R=IL
- * GRAY
- * HD
- * ICFLG
- * NFF
- * ALP
- * VL
- * VV
- * TL
- * TV
- * P
- * PA
- *UPPP
- *MATID
- *TW
- *CDNC
- *S
- *PQWTB1
- *PQWRF1
- *UP3TB1
- *UP3RF1

FILE

70	70	70	70	70	70	70
1010	8	1	21	0	0	0
0.0	1.0170	0.	0.0	0.	0.	3.080000E+02
2.500000E+00	2.412430E+03	0.	0.	0.	0.	0.
41.40000E+05	0.	0.	0.	0.	0.	0.
0.0000						
0.0	0.0	1.0	0.05	* VMTB		
78.0	7.2	40.0	5.95			
78.0	0.0	100.0	0.05			
270.0	0.67	255.0	0.705			
260.0	0.0	266.0	1.805			
272.0	0.50	345.0	0.505			
347.0	31.0	352.0	30.05			
358.0	20.0	363.0	18.25			
375.0	16.4	400.0	10.05			
445.0	4.0	450.0	0.05			
1000.0	0.0F					

- *CN02
- *CN03
- *CN04
- *CN05
- *CN06
- *CN07
- *CN08
- *CN09
- *CN10

PIPE

1	91	91	91	91	91	91
0	0	0	71	0	0	7
0	0	0	0	0	0	0
3.509200E-02	3.555000E-03	0.	0.	0.	0.	3.072000E+02
3.072000E+02	0.0	0.0	1.0E20	1.0	0.	0.

- *CN02
- *CN03
- *CN04
- *CN05
- *CN06
- *CN07
- *CN08

* AKRAY DATA

F 2.5000E+00E
 F 2.4124E-03E
 F 2.6497E-04E
 F 0. F
 F 0. F
 F 1.0000E+00E
 F 3.5052E-02E
 F 0 F
 F 1F
 F 3.7557E-06E
 F 0. -1.0007E-05E

- * DX
- * VDL
- * FA
- * FRIC
- * FRIC
- * GRAY
- * HD
- * ICFLG
- * NFF
- * ALP
- * VL

E 4.0784E+02E
 E 4.1637E+02E
 F 1.5200E+07E
 E 0.0 E

-1.4707E-05

* VV
 * TL
 * TV
 * P
 * PA
 *UPPP
 *MATID
 *TW
 *CONC
 *S
 *PWTB1
 *PWRFF1
 *UP3TB1
 *UP3RF1

*

.....

*

FILL 71 71 71 UPPER PLENUM INJECTION
 71 8 0
 1010 1 21 0 0 *CNO2
 0.0 1.0E20 0.0 *CNO3
 2.500000E+00 2.412430E+03 0. *CNO4
 41.40000E+05 0. 0. 3.080000E+02 *CNO5
 *CNO6
 *CNO7
 *CNO8
 *CNO9
 *CNO10
 0.0000 * VHTB
 0.0 0.0 1.0 0.05
 78.0 7.2 40.0 5.95
 78.0 0.0 100.0 0.05
 270.0 0.67 255.0 0.705
 260.0 0.0 266.0 1.805
 272.0 0.50 345.0 0.505
 347.0 31.0 352.0 30.05
 378.0 20.0 363.0 18.25
 375.0 10.9 400.0 10.05
 445.0 4.0 450.0 0.05
 1070.0 0.0E

*

.....

*

PIPE 72 72 72 UPPER PLENUM INJECTION PIPE
 1 0 72 72 7 *CNO2
 0 0 0 0 *CNO3
 *CNO4
 *CNO5
 *CNO6
 *CNO7
 *CNO8
 3.505200E+02 3.555000E-03 0. 0. 3.072000E+02
 3.072000E+02 0.0 0.0 1.0E20 1.0

*

* APRAT DATA

*

F 2.5000E+00E * DX
 F 2.4124E-03E * VUL
 F 0.5437E-04E * F1
 F 0.0 E * FRIC
 F 0.0 E * FRIC
 F 1.0000E+00E * GRAY
 F 3.5052E-02E * HD
 F 0 E * ICFLG
 F 4.1450E-06E * NFF
 0. -1.2557E-05E * ALP
 0. -1.2557E-05E * VL
 F 3.0785E+02E * VV
 F 4.1637E+02E * TL
 F 1.5200E+07E * TV
 F 0.0 E * P
 * PA
 *UPPP
 *MATID

*1W
 *C0V0
 *S
 *P0WTF1
 *P0WRF1
 *P3TB1
 *P3RF1

```

*****
*
*
FILL          72          72          72 UPPER PLENUM INJECTION
              72          8          0
              1017        1          21          0          0
              0.0          1.0E20      0.0          0          0
2.900000E+00  2.412430E+03  0.          0.          3.080000E+02
41.400000E+05  0.          0.          0.          0.
*
0.0000
0.0          0.0          1.0          0.05      * YMTB
38.0         7.2          40.0         5.95
78.0         0.0          100.0        0.05
270.0        0.47         255.0        0.735
250.0        0.0          260.0        1.805
272.0        0.50         345.0        0.505
347.0        31.0         352.0        30.05
398.0        20.0         363.0        18.25
375.0        16.7         400.0        10.05
445.0        4.0          450.0        0.05
1000.0       0.0E
*
*****

```

*CN02
 *CN03
 *CN04
 *CN05
 *CN06
 *CN07
 *CN08
 *CN09
 *CN10

```

*****
*
*
TEE          101          101          CORE BYPASS
*   JCELL    NJDES      MAT      CUST      ICHE
*   3         4         7         0.0       1          *CN07
*
* MAIN TUBE
*
*   ICUN11    NCELL1     JUN1     JUN2     IPJW1
*   0         0         101     100     0          *CN08
*   IOPTR1    IOPSV1     NOPTB1   NOPSV1   NOPRF1
*   0         0         0         0         0          *CN05
*   RADIN1    TH1      HOURL1   HOJTY1   TOUTL1
*   0.00174   0.04     0.0      0.0     300.0     *CN06
*   TOUTV1    PW1V1     PWOFF1   PPWMX1   PWSCL1
*   300.0     0.0      0.0      1.0E20  1.0       *CN07
*   OPIN1     OPPOFF1   POPMX1   OPSCL1
*   0.0       0.0      1.0E20   1.0     *CN08
*
* SIDE TUBE
*
*   ICUN02    NCELL2     JUN3     IPJW2
*   0         1         109     0          *CN09
*   IOPTR2    IOPSV2     NOPTB2   NOPSV2   NOPRF2
*   0         0         0         0         0          *CN11
*   RADIN2    TH2      HOURL2   HOJTY2   TOUTL2
*   0.00195   0.04     0.0      0.0     300.0     *CN12
*   TOUTV2    PW1V2     PWOFF2   PPWMX2   PWSCL2
*   300.0     0.0      0.0      1.0E20  1.0       *CN13
*   OPIN2     OPPOFF2   POPMX2   OPSCL2
*   0.0       0.0      1.0E20   1.0     *CN14
*
* MAIN TUBE
*
R 2          0.6          0.46E 2          0.97E          *DX1
R 2          2.204E+03      1.603E+03K 2      3.570E+03E      *VJL1
          1.295E+03R 4      5.030E+03          1.295E+03E      *FA1
F          0.0E          *FRIC1F

```

```

*
* 0.0E
* 1.0E
* 1.0E-03 4 1.44E-02 3.440E-03E 1E
* 1E
* 0.0E
* 0.0E
* 0.0E
* 593.0E
* 515.0E
* 148.4E+5E
* 0.0E
* 0.0E
* 7E
* 570.0E

```

```

*FRIC1X
*GRAV1
*H21
*ICFLG1
*HFF1
*ALP1
*V11
*VV1
*TL1
*TV1
*P1
*PA1
*OPPP1
*MATID1
*TW1

```

* SIDE TURF

```

*
* 0.0E
* 2.742E-04E
* 1.341E-03E
* 0.0E
* 0.0E
* 0.0E
* 0.00391E
* 0
* 1E
* 0.0E
* 0.0E
* 0.0E
* 593.0E
* 515.0E
* 148.4E+5E
* 0.0E
* 0.0E
* 7E
* 570.0E

```

```

*DK2
*VCL2
*FA2
*FRIC2F
*FRIC2R
*GRAV2
*H22
*ICFLG2
*HFF2
*ALP2
*V_2
*VV2
*TL2
*TV2
*P2
*PA2
*OPPP2
*MATID2
*TW2

```



TEE	JCELL	NODES	102 PA1	102 CUST	CORE BYPASS ICBF	
*	3	4	7	0.0	1	*CN02
* MAIN TURF						
*	ICUN01	NCELL1	JUN1	JUN2	IPDH1	
	0	5	102	106	0	*CN03
*	IQPTR1	IQPSV1	QPTR1	QPSV1	QPRF1	
	0	0	0	0	0	*CN05
*	RADIV1	TH1	HOUTL1	HOUTV1	TOJTL1	
	0.00174	0.04	0.0	0.0	300.0	*CN06
*	TOUTV1	PWIN1	PWOFF1	RPWMX1	PWSCL1	
	300.0	0.0	0.0	1.0E20	1.0	*CN07
*	QPIV1	QPOFF1	RUPMX1	QPSCL1		*LNUR
	0.0	0.0	1.0E20	1.0		
* SIDE TURF						
*	ICUN02	NCELL2	JUN3	IPDH2		*CN09
	0	1	110	0		
*	IQPTR2	IQPSV2	QPTR2	QPSV2	QPRF2	
	0	0	0	0	0	*CN11
*	RADIV2	TH2	HOUTL2	HOUTV2	TOJTL2	
	0.00195	0.04	0.0	0.0	300.0	*CN12
*	TOUTV2	PWIN2	PWOFF2	RPWMX2	PWSCL2	
	300.0	0.0	0.0	1.0E20	1.0	*CN13
*	QPIV2	QPOFF2	RUPMX2	QPSCL2		*CN14
	0.0	0.0	1.0E20	1.0		

```

* MAIN TUBE
*
R 2 2.200E+03 0.460 2 0.97E *DX1
R 2 1.295E+03 1.673E+03 2 3.570E+03 *VJL1
R 2 1.295E+03 0.030E+03 1.295E+03 *FA1
R 0.0E *FRIC1
R 0.0E *FRIC1
R 1.0E *GRAV1
R 3.480E+03 4 1.44E+02 3.480E+03 *H31
R 1R 4 0 1E *ICFLG1
R 1E *VFF1
R 0.0E *ALP1
R 0.0E *VL1
R 0.0E *VV1
R 593.0E *TL1
R 615.0E *TV1
R 148.4E+5E *P1
R 0.0E *PA1
R 0.0E *OPPP1
R 7E *MATID1
R 570.0E *T#1

```

```

* SIDE TUBE
*
R 0.050E *DX2
R 2.742E+04 *VJL2
R 1.041E+03 *FA2
R 0.0E *FRIC2
R 0.0E *FRIC2
R 0.0E *GRAV2
R 3.00391E *H32
R 0 1E *ICFLG2
R 1E *VFF2
R 0.0E *ALP2
R 0.0E *VL2
R 0.0E *VV2
R 593.0E *TL2
R 615.0E *TV2
R 148.4E+5E *P2
R 0.0E *PA2
R 0.0E *OPPP2
R 7E *MATID2
R 570.0E *T#2

```

```

*****
TE#
* JCELL NNODES 103 103 CORE BYPASS
* J MAT CUST ICHF
* J 4 7 0.0 1 *CN02
*
* MAIN TUBE
* ICUNC1 NCELL1 JUN1 JU42 IPJW1
* 0 5 103 107 0 *CN03
* IDPTR1 IDPSV1 NQPTR1 NQPSV1 VQPRF1
* 0 0 U 0 0 *CN05
* RADIV1 TH1 HOUTL1 HOUTV1 TOUTL1
* 0.00174 0.04 0.0 0.0 300.0 *CN06
* TDJTV1 PWINI PWUFF1 RPWMX1 PWSCL1
* 300.0 0.0 0.0 1.0E20 1.0 *CN07
* DPV1 DPOFF1 RQPMX1 QPSCL1
* 0.0 0.0 1.0E20 1.0 *CN08
*
* SIDE TUBE
* ICUNC2 NCELL2 JUN3 IPOW2
* 0 1 111 0 *CN09
* IDPTR2 IDPSV2 NQPTR2 NQPSV2 VQPRF2
* 0 0 U 0 0 *CN11
* RADIV2 TH2 HOUTL2 HOUTV2 TOUTL2

```

```

* 0.00175      1.028      0.00175      0.00175      1.028
* 1.028      0.00175      0.00175      0.00175      1.028
* 300.0      0.00175      0.00175      0.00175      1.028
* 300.0      0.00175      0.00175      0.00175      1.028
* 0.0      0.0      1.0E20      1.0
*

```

* MAIN TUBE

```

*
* 2      0.0      0.0E02      0.0002      *OX1
* 2      2.20E-03      1.593E-03P 2      3.570E-03F      *VCL1
*      1.295E-03P 4      6.030E-03      1.295E-03F      *FA1
*      0.0F      *FRIC1
*      0.0F      *FRIC1
*      1.0F      *GRAY1
*      3.480E-03P 4      1.44E-02      3.480E-03F      *H01
*      1E 4      0      1E      *ICFLG1
*      1F      *NPF1
*      0.0F      *ALP1
*      0.0F      *V1
*      0.0F      *V2
*      593.0F      *TL1
*      615.0F      *TV1
*      148.4E+0F      *P1
*      0.0F      *PA1
*      0.0F      *QPP1
*      7F      *MATID1
*      570.0F      *TW1
*

```

* SIDE TUBE

```

*
*      0.050F      *OX2
*      2.742E-04F      *VCL2
*      1.341E-03E      *FA2
*      0.0F      *FRIC2
*      0.0F      *FRIC2
*      0.0F      *GRAY2
*      3.00391E      *H02
*      0      1F      *ICFLG2
*      1E      *NPF2
*      0.0F      *ALP2
*      0.0F      *V2
*      0.0F      *V2
*      593.0F      *TL2
*      615.0F      *TV2
*      148.4E+0F      *P2
*      0.0F      *PA2
*      0.0F      *QPP2
*      7F      *MATID2
*      570.0E      *TW2
*

```

```

* TEE      JCELL      NODES      104      104      CORE RYPA/S
*      3      4      MAT      CUST      ICDF      1      *CN02

```

* MAIN TUBE

```

*
* ICUNC1      NCELL1      JUN1      JUN2      IPOW1
*      0      5      104      108      0      *CN03
* IOPTR1      IQPSV1      NQPTB1      NQPSV1      NQPRF1
*      0      0      0      0      0      *CN05
* RADIN1      TH1      HQUTL1      HUUTY1      TOUTL1
* 0.00175      0.04      0.0      0.0      300.0      *CN06
* IOUTV1      FWIN1      RPWFX1      RPWFX1      PWSCL1
* 300.0      0.0      0.0      1.0E20      1.0      *CN07
* OPIN1      OPDFP1      RQPMX1      SPSC11
* 0.0      0.0      1.0E20      1.0      *CN08
*

```

* SIDE TUBE

```

* 170V22  MDELLZ  JUNA  1PDKZ
* 0 1 112 0
* 17PRT1  12PSY2  NQPR1Z  NQPSV2  NQPR2  *CN09
* 0 0 0 0 0
* 17AD12  1HZ  HDUTLZ  HDUTV2  HDUTL2  *CN11
* 0.70126 0.04 0.0 0.0 300.0
* 17UTV2  RWINEZ  RWOFFZ  RWPMXZ  RWSCLEZ  *CN12
* 300.0 0.0 0.0 1.0E20 1.0
* 17PIV2  17OFFZ  RWPMXZ  17SLLZ  *CN13
* 0.0 0.0 1.0E20 1.0 *CN14

```

```
* MAIN TUBE
```

```

R 2 0.0 0.40R 2 0.97F *DX1
R 2 2.228E-03 1.673E-03R 2 3.570E-03E *VCL1
F 1.295E-03R 4 5.030E-03 1.295E-03E *FA1
F 0.0F *FRIC1
F 0.0F *FRIC1
F 1.0F *GRAV1
F 3.480E-03R 4 1.44E-02 3.480E-03E *HD1
F 1R 4 U 1E *ICFLG1
F 1E *NFF1
F 0.0F *ALP1
F 0.0F *VL1
F 0.0E *VV1
F 573.0F *T_1
F 615.0F *TV1
F 148.4E+5E *P1
F 0.0F *PA1
F 0.0F *OPPP1
F 7F *MATID1
F 570.0E *TW1

```

```
* SIDE TUBE
```

```

F 0.050F *DX2
F 2.742E-04F *VCL2
F 1.041E-03E *FA2
F 0.0F *FRIC2
F 0.0F *FRIC2
F 0.0F *GRAV2
F 3.00371E *HD2
F 0 1E *ICFLG2
F 1F *NFF2
F 0.0E *ALP2
F 0.0E *VL2
F 0.0F *VV2
F 503.0E *TL2
F 615.0E *TV2
F 148.4E+5E *P2
F 0.0E *PA2
F 0.0E *OPPP2
F 7F *MATID2
F 570.0E *TW2

```

```
-----
```

```
* - N2MAX SET TO 60 FROM 50
```

```
* THE FOLLOWING APRAYS HAVE BEEN REPLACED BY FP-1 VALUES
```

```
* TAKEN FROM TRAC-PDZ(MOU1) ANALYSIS
```

```

* - CPDWR
* - RPKF
* - ZPWR
* - RADRO
* - PPATP
* - NREX
* - PSAPT

```

```
-----
```

```
VESSEL
```

```
50
```

```
50 VESSEL
```

* BASED ON PROPIA/20A/7L2+3/0417L2+3IND WITH FOLLOWING MODIFICATIONS:

- * OCT/NOV 1982, PTD
- * - INCORPORATE DISTRIBUTED HEAT SLABS
- * - CHANGE INITIAL MESH'S FROM 5x3 K TO 570 X TO HELP INHIBIT FILM BOILING AT START UP STEADY STATE RUN
- * - MINOR CHANGE TO LEVEL 3 DOWNCOMER PART AND 2 (TO .375)
- * DEC 1983, PTD
- * - REVISE AXIAL POWER SHAPE P&P PC L T
- * AUG 1984, ULS
- * - REVISE ELEVATION OF CORE, 0.13 M LOWER
- * SEP 1985, J. BIRCHLEY
- * - INCLUDE FRICTION FACTOR VALUES FOR ENTRY INTO, THROUGH AND EXIT FROM LORE
- * - REVISE FLUID VOLUME AND AREA FRACTIONS

```

*VASK*      12 *IKKX*      4 *NTSX*      4 *HCSR*      28 *IVSSBF*      U *CARD 2
*ICU*       12 *IUCI*      2 *IUCH*      3 *ICPU*      8 *ICRL*      3 *CARD 3
*ICPR*      3 *IUCSP*     0 *IUCSP*     0 *IUHP*      0 *ICDNC*     0 *CARD 4
*VPPA*      0 *VPPA*     0 *VPPA*     0 *VVENT*     0 *CARD 5
*IRPWT*     7 *IRDUX*     0 *IRDUX*     0 *NRTS*      0 *CARD 6
*
*IRPWT*     100 *IRPWSY*   1 *NRPWT*     25 *NRPWSY*   0 *NRPWRP*   0 *CARD 7
*IRPWT*     0 *IRPWSY*   1 *NRPWT*     1 *NRPWSY*   0 *NRPWRP*   0 *CARD 8
*IRPWT*     101 *NRWXX*   1 *NFCL*      1 *NFCL*      1 *NZMAX*    60 *CARD 9
*
*NRDUS*     16 *NUDES*    10 *NUDHS*     4 *IVHSMX*   1 *CARD 10
*PEACT*     0. *INEUT*    0. *XPWDF*=-1.820 *RRPWX*=-1.E30 *RPWSCL* 1.0 *CARD 11
*PPDR1* 0.37 *ZPWIV*    0. *ZPWDF* 0. *ZPWX* 0. *CARD 12
*SHFLV*     0. *FLDR*    0. *PURAT* 1.336 *FUCKAC* 0.7 *HGAPD* 1.0E-3 *CARD 13
*DTVHT(1)*4.0 *DTVHT(2)*50. *DZVHT* 1.0E-3 *CARD 14
*
**SKIPPED** *CARD 15
**SKIPPED** *CARD 16
**SKIPPED** *CARD 17

```

```

0.527          0.727          1.2485          *Z
1.553          1.7815          *Z
2.010          2.467          .9245          *Z
3.400          4.8465          *Z
5.130          5.900E          *Z
0.105          0.231          0.324          0.470E *RADIUS
1.573794377   3.141592654   4.712388981   6.283185308E *THETA
* VESSEL SOURCE LEXOS
11            10            3            1          *ILHL
11            10            3            9          *ILCL
11            12            3            31         *BLHL
11            13            3            41         *BLCL
11            4            -2           105         *BYPS
11            0            -2           105         *BYPS
11            11           -2           107         *BYPS
11            8            -2           108         *BYPS
9             1            2            81         *UPINJ
9             2            2            82         *UPINJ
9             3            2            83         *UPINJ
9             .            2            84         *UPINJ
9             .            2            85         *UPINJ
9             .            2            86         *UPINJ
9             .            2            87         *UPINJ
9             .            2            88         *UPINJ
9             .            2            89         *UPINJ
9             10           2            90         *UPINJ
9             11           2            91         *UPINJ
9             12           2            92         *UPINJ
8             4            3           109         *BYPS
8             10           3           110         *BYPS

```


11	3	111	*UYP5
12	3	112	*BYPS
4	2	101	*HYPS
10	2	102	*BYPS
11	2	103	*BYPS
12	2	104	*BYPS
0.355	0.440	0.4655	*RDPWR
0.775	0.4405		*RDPWR
1.016	1.060R 3	0.000E	*RDPWR

THE FOLLOWING DATA IS FOR FP-1

R 4	1.4856F 4	1.2034 R 4	0.7245E		*COPWR
	1	2	3	45	*IDROD
	8	12E			*IDROD
R 4	1.2803	1.0939	1.2365E		*RPWF
*IDUMM)	1.05				*ZPWTB
	0.1500	1.2541	1.4586 5		*ZPWTB
	1.4995	1.0337	0.0477 E		*7PWTB
R 4	33.10R 4	127.1R 4	154.0E		*PDX
	0.0	7.7449E-4	1.5489E-35		*RADRD
	2.3235E-3	3.0479E-35			*RADRD
	3.1725E-3	4.6470E-3	4.7420E-35		*RADRD
	5.0509E-3	5.3540E-3E			*RADRD
R 5	1	3R 2	2E		*MATRO
	0.0	37.0E6	0.3	32.425E6 5	*RPWTB
	0.4	9.8748E6	1.28	5.5142E6 5	*RPWTB
	1.38	3.0836E6	1.40	3.2985E6 5	*RPWTB
	1.46	2.9450E6	1.52	2.6480E6 5	*RPWTB
	1.59	2.3320E6	1.61	2.2712E6 5	*RPWTB
	2.0	2.1547E6	3.0	2.0515E6 5	*RPWTB
	4.0	1.9873E6	6.0	1.8751E6 5	*RPWTB
	.0	1.7719E6	10.0	1.7251E6 5	*RPWTB
	15.0	1.6047E6	20.0	1.5183E6 5	*RPWTB
	30.0	1.3462E6	40.0	1.3085E6 5	*RPWTB
	60.0	1.1357E6	100.0	1.0700E6 5	*RPWTB
	200.0	0.7500E6	300.0	0.8400E6 5	*RPWTB
	10000.	5.7560E4 E			*RPWTB

LF					*4FAX
0.0E					*FPU02
0.03E					*FTD
9.81010E-1	0.0	1.01030E-2	1.78300E-3	0.0	*GMIX
7.09910E-3	0.05				*GMIX
9.81010E-1	0.0	1.01030E-2	1.78300E-3	0.0	*GMIX
7.09910E-3	0.05				*GMIX
9.81010E-1	0.0	1.01030E-2	1.78300E-3	0.0	*GMIX
7.09910E-3	0.05				*GMIX
9.81010E-1	0.0	1.01030E-2	1.78300E-3	0.0	*GMIX
7.09910E-3	0.05				*GMIX
9.81010E-1	0.0	1.01030E-2	1.78300E-3	0.0	*GMIX
7.09910E-3	0.05				*GMIX
9.81010E-1	0.0	1.01030E-2	1.78300E-3	0.0	*GMIX
7.09910E-3	0.05				*GMIX
9.81010E-1	0.0	1.01030E-2	1.78300E-3	0.0	*GMIX
7.09910E-3	0.05				*GMIX
9.81010E-1	0.0	1.01030E-2	1.78300E-3	0.0	*GMIX
7.09910E-3	0.05				*GMIX
1.0E					*GMLES
R 4	2.4100F+6	K 8	2.1200E+5	E	*PCAPT

	0.0	0.075	0.085	0.0925	*HSX
	0.0	0.075	0.085	0.0925	*HSX
	0.0	0.075	0.085	0.0925	*HSX
	0.0	0.075	0.085	0.0925	*HSX
	0.0	0.075	0.085	0.0925	*HSX
F	0.0F				*CFZL-T
F	0.0F				*CFZL-Z
F	0.0F				*CFZL-R
F	0.0F				*CFZY-T
F	0.0E				*CFZY-Z
F	0.0F				*CFZY-R
F	1.118F				*VDL
F	1.0F				*FA-T
R12	.4099 4	.582E			*FA-Z
R8	1.0 R4 1.0 P4 U.U E				*FA-R
F	.1F				*HD-T
F	.1F				*HD-Z
F	.1E				*HD-R
F	570.0F				*HSTN
F	6F				*MATHS
F	0.0F				*ALPN
F	0.0E				*VYN-T
F	0.0F				*VYN-Z
F	0.0F				*VYN-R
F	0.0E				*VLN-T
F	0.0E				*VLN-Z
F	0.0F				*VLN-R
F	0.15.0F				*TVN
F	573.0E				*TLN
F	14H.4E5E				*PN
F	0.0F				*PAN
*					
*	LEVEL 3				
*					
R 4	0.1341 S				*HSA
R 4	0.5150 S				*HSA
P 4	0.5676 S				*HSE
P 4	2.1207 E				*HSA
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.005	0.010	0.01535	*HSX
	0.0	0.025	0.035	0.0405	*HSX
	0.0	0.025	0.035	0.0405	*HSX
	0.0	0.025	0.035	0.0405	*HSX
	0.0	0.025	0.035	0.0405	*HSX
	0.0	0.025	0.035	0.0405	*HSX
F	0.0F				*CFZL-T
R12	5.5R 4	0.0E		*FF=5.5	*CFZL-Z
F	0.0F				*CFZL-R
F	0.0E				*CFZY-T
R12	5.5R 4	0.0E		*FF=5.5	*CFZY-Z
F	0.0F				*CFZY-R
R12	.656R 4	0.582E			*VDL
R12	.7P 4	.582E			*FA-T
R12	0.448P 4	.582E			*FA-Z
R8	0.7 R4 0.0 P4 U.U E				*FA-R
R12	1.27F-TR 4	0.100E			*HD-T
R12	1.22F-LP 4	0.100E			*HD-Z
R12	1.22E-2P 4	0.100E			*HD-R
F	570.0F				*HSTN
F	6E				*MATHS
F	0.0F				*ALPN

F	0.0F					*CFZL-T
F	0.0F					*CFZV-T
R 4	0.0P 4	1.2K 4		0.5P 4		*CFZV-Z
F	0.0F					*CFZV-R
R12	0.875P 4	.2K2E				*VOL
R12	0.375P 4	.5K2E				*FA-T
R 4	0.75P 4	0.375K 4		0.5820F		*FA-Z
R 4	0.375P 4	0.0 4	0.0 4			*FA-R
R12	1.22E-2P 4	0.100E				*HD-T
R12	1.22E-2P 4	0.100E				*HD-Z
R12	1.22E-2P 4	0.100E				*HD-R
F	570.0E					*HSTN
F	0F					*MATHS
F	0.0F					*ALPN
F	0.0E					*VYN-T
F	0.0F					*VYN-Z
F	0.0F					*VYN-R
F	0.0E					*VLN-T
F	0.0F					*VLN-Z
F	0.0F					*VLN-R
F	515.0F					*TVN
F	503.0E					*TLN
F	148.415E					*PN
F	0.0F					*PAN
* LEVEL 10						
R 4	1.0940 5					*HSA
R 4	4.2010 5					*HSA
R 4	1.7344 5					*HSA
R 4	5.0940 5					*HSA
	0.0	.0010		.002	.003045	*HSX
	0.0	.0010		.002	.003045	*HSX
	0.0	.0010		.002	.003045	*HSX
	0.0	.0010		.002	.003045	*HSX
	0.0	.0010		.002	.003045	*HSX
	0.0	.0010		.002	.003045	*HSX
	0.0	.0010		.002	.003045	*HSX
	0.0	.0010		.002	.003045	*HSX
	0.0	.0200		.030	.034105	*HSX
	0.0	.0200		.030	.034105	*HSX
	0.0	.0200		.030	.034105	*HSX
	0.0	.0200		.030	.034105	*HSX
	0.0	.0250		.035	.04005	*HSX
	0.0	.0250		.035	.04005	*HSX
	0.0	.0250		.035	.04005	*HSX
	0.0	.0250		.035	.04005	*HSX
F	0.0F					*CFZL-T
F	0.0F					*CFZL-Z
F	0.0F					*CFZL-R
F	0.0F					*CFZV-T
F	0.0E					*CFZV-Z
F	0.0E					*CFZV-R
R12	0.885P 4	.715E				*VOL
R 4	1.0P 4	0.0K 4		.7150F		*FA-T
R 4	0.85P 4	0.0K 4		.2505		*FA-Z
R 4	0.981	0.444		0.481	0.449E	*FA-Z
R 4	0.0	0.0	0.0			*FA-R
R12	1.22E-2P 4	0.100E				*HD-T
R12	1.22E-2P 4	0.100E				*HD-Z
R12	1.22E-2P 4	0.100E				*HD-R
F	570.0E					*HSTN
F	0E					*MATHS
F	0.0E					*ALPN
F	0.0F					*VYN-T
F	0.0F					*VYN-Z
F	0.0F					*VYN-R
F	0.0F					*VLN-T
F	0.0F					*VLN-Z
F	0.0F					*VLN-R

	0.0	.0200	.030	.034105	*HSX
	0.0	.0200	.030	.034105	*HSX
	0.0	.0250	.035	.04005	*HSX
	0.0	.0250	.035	.04005	*HSX
	0.0	.0250	.035	.04005	*HSX
	0.0	.0250	.035	.04005	*HSX
F	0.0F				*CFZL-T
F	0.0F				*CFZL-Z
F	0.0F				*CFZL-R
F	0.0F				*CFZY-T
F	0.0E				*CFZY-Z
F	0.0F				*CFZY-R
R12	0.8850 4	0.000E			*YDL
R12	0.3450 4	0.000E			*FA-T
R12	0.0000 4	0.000E			*FA-Z
R8	0.345 4 0.0 4 0.0 E				*FA-R
R12	1.22E-20 4	0.100E			*HD-T
R12	1.22E-20 4	0.100E			*HD-Z
R12	1.22E-20 4	0.100E			*HD-R
F	570.0E				*HSTN
F	0E				*MATHS
F	0.0E				*ALPN
F	0.0F				*VYN-T
F	0.0F				*VYN-Z
F	0.0F				*VYN-R
F	0.0E				*VLN-T
F	0.0F				*VLN-Z
F	0.0F				*VLN-K
F	015.0E				*TVN
F	593.0E				*TLN
F	149.45E				*PN
F	0.0F				*PAN
*					
*	PUN DATA				
*					
F	0.0E				*BURN 1
F	559.0E				*RDTN 1
F	0.0E				*BURN 2
F	559.0E				*RDTN 2
F	0.0E				*BURN 3
F	559.0E				*RDTN 3
F	0.0E				*BURN 4
F	559.0E				*RDTN 4
F	0.0E				*BURN 5
F	559.0E				*RDTN 5
F	0.0E				*BURN 6
F	559.0E				*RDTN 6
F	0.0E				*BURN 7
F	559.0E				*RDTN 7
F	0.0E				*BURN 8
F	559.0E				*RDTN 8
F	0.0E				*BURN 9
F	559.0E				*RDTN 9
F	0.0E				*BURN10
F	559.0E				*RDTN10
F	0.0E				*BURN11
F	559.0E				*RDTN11
F	0.0E				*BURN12
F	559.0E				*RDTN12
F	0.0E				*BURN13
F	559.0E				*RDTN13
F	0.0E				*BURN14
F	559.0E				*RDTN14
F	0.0E				*BURN15
F	559.0E				*RDTN15
F	0.0E				*BURN16
F	559.0E				*RDTN16
F	0.0E				*BURN17
F	559.0E				*RDTN17
F	0.0E				*BURN18

```

# *****
#                               TIME STEP (ATA) *****
#
# 1.0E-5          1.0E+0          3.0E+1          1.0E+1
# 1.0E-5          1.0E+0          0.1E-1          1.0E+1
# 5.0E+0          1.0E-1          1.0E+0          1.0E+0
# -1.0

```

TABLE 3.5. Input deck listing for transient

0.0	1.0E-5	1.0	1.0E-5	S
1.7191	1.0E-5	3.0	1.61E5	S
7.0	1.71E5	21.3	2.79E5	S
24.4	2.88E5	74.8	2.00E5	S
140.0	2.01E5	269.0	2.60E5	S
285.0	2.15E5	357.0	2.64E5	S
491.0	2.694E5	401.0	2.66E5	S
857.0	3.06E5	500.0	3.04E5	E
* 2.0	3.5E5	6.0	2.3E5	S
* 33.0	3.6E5	53.0	3.34E5	S
* 70.0	3.17E5	100.0	3.0E5	S
* 110.0	2.7E5	500.0	2.7E5	E

END

*****TIME STEP DATA*****				
1.0E-5	5.0E-3	1.0	10.0	
1.0	0.2	2.0	0.5	
1.0E-5	1.0E-2	5.0	10.0	
1.0	0.5	2.0	1.0	
1.0E-5	0.1	345.0	10.0	
5.0	0.5	5.0	5.0	
* 1.0E-5	1.0E-2	500.0	10.0	
* 5.0	0.5	5.0	5.0	
-1.0				

END

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(See instructions on the reverse)

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10. SUPPLEMENTARY NOTES

11. ABSTRACT *(200 words or less)*

This report assesses thermal-hydraulic aspects of LOFT LP-FP-1 experiment making use of TRAC-PF1/MOD1. LP-FP-1 experiment studies the system thermal-hydraulic and core thermal response for initial and boundary conditions similar to a large-break design basis LOCA leading to fission product release from the fuel cladding gap region. It also assesses the fission product retention effectiveness of the PWR-ECCS in best estimate conditions.

12. KEY WORDS/DESCRIPTORS *(List words or phrases that will assist researchers in locating the report.)*

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TRAC-PF1/MOD1
LP-FP-1 Experiment

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