RCS Leakage Detection Instrumentation 3.4.15

1

CONDITION		REQUIRED ACTION	COMPLETION TIME	
 Required containment atmosphere radioactivity monitor inoperable. AND 	Ĕ.1	Restore required containment atmosphere radioactivity monitor to OPERABLE status.	30 days	
Required containment air cooler condensate flow rate monitor inoperable.	OR E	Restore required containment air cooler condensate flow rate monitor to OPERABLE status.	30 days	
 Required Action and associated Completion Time not met. 	F Z.1	Be in MODE 3.	6 hours	
	AND F.2	Be in MODE 5.	36 hours	
(Teakage detection systems)	G			
F. All required monitors inoperable.	1.1	Enter LCO 3.0.3.	Immediately	

SURVEILLANCE REQUIREMENTS

LCV-0603-

	SURVEILLANCE	FREQUENCY
SR 3.4.15.X	Perform CHANNEL CHECK of the required containment atmosphere radioactivity monitor.	12 hours
SR 3.4.15.1	Perform CHANNEL CHECK of containment normal sumps level and reactor cavity sump levelmonitors.	(continued) 12 hours
400 513 WOB 513 Vortle Units	424 DR 3.4-41 -) Rev. 0, 09/28/

LCV-0603-E For the purpose of this Condition the leakage detection systems consist RCS Leakage Detection Instrumentation of the three systems described below in items 0, b, and C, respectively: 8 3.4.15 a. the containment normal sumps level and reactor cavity sump manitors, BASES b. one cuntain ment atmosphere radioactivity ACTIONS E.1 and E.2 (continued) monitor (gaseous or particulate); and required plant conditions from full power conditions in an orderly manner and without challenging plant systems. C. either the containment air cooler condensate G flow rate or a 1.1 containment othosphere leakage detection systems) goseous or particulate radioactivity monitoring With all required monitors inoperable, no automatic means of system not token credit monitoring leakage are available, and immediate plant for in item b. shutdown in accordance with LCO 3.0.3 is required. SR 3.4.15.1 and SR 3.4.15.2 5 SURVEILLANCE REQUIREMENTS SR 3.4.15.1 requires the performance of a CHANNEL CHECK of These SRs are the required containment atmosphere radioactivity monitor, The check gives reasonable confidence that the channel is operating properly. The Frequency of 12 hours is based on instrument reliability and is reasonable for detecting off normal conditions. and containment sump monitors SR 3.4.15.Z SR 3.4.15.2 requires the performance of a COT on the required containment atmosphere radioactivity monitor. The test ensures that the monitor can perform its function in the desired manner. The test verifies the alarm setpoint and relative accuracy of the instrument string. The Frequency of of days considers instrument reliability, and operating experience has shown that it is proper for detecting degradation. WOG-09 -92 C4 3.4.15.4. an 3.4.15.2 DSR SR and SR 3.4.15.50 These SRs require the performance of a CHANNEL CALIBRATION for each of the RCS leakage detection instrumentation channels. The calibration verifies the accuracy of the instrument string, including the instruments located inside containment. The Frequency of [18] months is a typical refueling cycle and considers channel reliability. Again, operating experience has proven that this Frequency is acceptable. (continued)

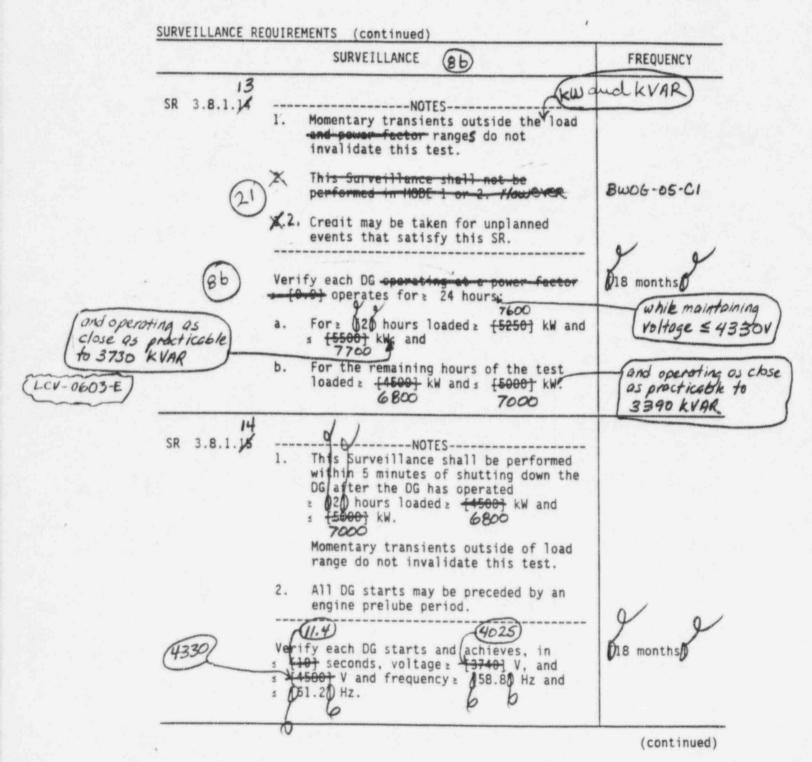
B 3.4-90

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Vogile Units 1 and 2

Rev. 0, 09/28/92

AC Sources - Operating 3.8.1



a KVEP had as close as practicable to 3730 kvar while loaded = 7600 KW and LCV-0603-E. AC Sources - Operating ETTOOKW and 3390 KVAR while loaded B 3.8.1 26800 KW and 57000 KW for the remaining hours of the test, while BASES maintaining voltage ≤ 4330 V SR 3.8.1.14 (Scontinued) SURVEILLANCE REQUIREMENTS KVAR load possible, testing must be performed using a power factor of $\leq [0.9]$. This power factor is chosen to be representative The voltage limit of 4330 V is required to of the actual design basis inductive loading that the DG would experience. I The load band is provided to avoid prevent operation routine overloading of the DG. Routine overloading may of any loads at result in more frequent teardown inspections in accordance orabove the maximum with vendor recommendations in order to maintain DG design voltage, OPERABILITY. The 18 month Frequency is consistent with the recommendations of Regulatory Guide 1.108 (Ref. 9), paragraph 2.a.(3), takes into consideration unit conditions required to perform the Surveillance, and is intended to be consistent with expected fuel cycle lengths. KVAR load two This Surveillance is modified by three Notes. [Note 1 states that momentary transients due to changing bus/loads do not invalidate this test. Similarly, momentary power factor transients above the power factor limit will not invalidate the test. The reason for Note 2 is that during operation with the reactor critical, performance of this Surveillance could cause perturbations to the electrical distribution systems that could challenge continued steady state / operation/and, as a result, unit safely stems. Note 3-2 acknowledges that credit may be taken for unplanned events that satisfy this SR. K BWR-25-1 INSERT SR 3.8.1 11.4 This Surveillance demonstrates that the diesel engine can restart from a hot condition, such as subsequent to shutdown from normal Surveillances, and achieve the required voltage and frequency within [10] seconds. The [40] secondy time is derived from the requirements of the accident analysis to respond to a design basis large break LOCA. The 218 months Frequency is consistent with the recommendations of Regulatory Guide 1.108 (Ref. 9), paragraph 2.a.(5). This SR is modified by two Notes. Note 1 ensures that the test is performed with the diesel sufficiently hot. The load band is provided to avoid routine overloading of the DG. Routine overloads may result in more frequent teardown inspections in accordance with vendor recommendations in

(continued)

Rev. 0, 09/28/92

Fo(Z) (Fo Methodology 8 3.2.18 TSC ACTIONS A.2 of RTP (continued) A reduction of the Power Range Neutron Flux - High trip setpoints by $\ge 1\%$ for each 1% by which FS(Z) exceeds its Steady State limit, is a conservative action for protection against the consequences of severe transients with unanalyzed power distributions. The Completion Time of 8 hours is sufficient . 6.1 considering the small likelihood of a severe transient in this time period and the preceding prompt reduction in LCV-0603-E THERMAL POWER in accordance with Required Action A.1 (In 96RTP value of K A.3 Reduction in the Overpower ΔT trip setpoints by $\geq 1\%$ for each 1% by which $F_{0}^{S}(Z)$ exceeds its limit, is a conservative action for protection against the consequences of severe transients with unanalyzed power distributions. The Completion Time of 72 hours is sufficient considering the small likelihood of a severe transient in this time period.

A.4

Verification that $F_{0}(Z)$ has been restored to within its limit, by performing SR 3.2.1.1 prior to increasing THERMAL POWER above the limit imposed by Required Action A.1. ensures that core conditions during operation at higher power levels are consistent with safety analyses assumptions.

and the preceding prompt reduction in THERMAL POWER in

accordance with Required Action A.1.

limit B.1 If it is found that the maximum calculated - Fo(Z) that can secur during normal maneumener Fi(2), expeeds its transient opecified limits, there exists a potential for Fo(Z) to become excessively high if a normal operational transient transient occurs. Reducing the AFD by $\geq 1\%$ for each 1% by which $F_0(Z)$ exceeds its limits within the allowed Completion Time of 2 hours, restricts the axial flux distribution such that even if a transient occurred, core peaking factors are not exceeded, INSERT FOR REQUIRED ACTION B.1 BASES (REF.5) (continued)

BASES

Vertilation

Diesel Fuel Oil, Lube Oil, and Starting Air, and B 3.8.3

SURVEILLANCE

BASES

SR 3.8.3.4 (continued)

intended to reflect the lowest value at which the five starts can be accomplished. (PI-9060, PI9061, PI-9064, PI-965)

The 31 day Frequency takes into account the capacity, capability, redundancy, and diversity of the AC sources and other indications available in the control room, including alarms, to alert the operator to below normal air start pressure.

SR 3.8.3.5

Microbiological fouling is a major cause of fuel oil degradation. There are numerous/bacteria that can grow in fuel oil and cause fouling, but all must have a water environment in order to survive! Removal of water from the fuel storage tanks once every \$310 days eliminates the necessary environment for bacterial survival. This is the most effective means of controlling microbiological fouling. In addition, it eliminates the potential for water entraigment in the fuel oil during DG operation. Water may come from any of several sources, including condensation. ground water, rain water, and contaminated fuel oil, and from breakdown of the fuel oil by bacteria. Frequent checking for and removal of accumulated water minimizes fouling and provides data regarding the watertight integrity of the fuel oil system. The Surveillance Frequencies are established by Regulatory Guide 1.137 (Ref. 2). This SR is for preventive maintenance. The presence of water does not necessarily represent failure of this SR, provided the accumulated water is removed during performance of the Surveillance.

SR 3.8.3.87

Draining of the fuel oil stored in the supply tanks, removal of accumulated sediment, and tank cleaning are required at 10 year intervals by Regulatory Guide 1.137 (Ref. 2), paragraph 2.f. This SP also requires the performance of the ASME Code, Section XI (Ref. 8), examinations of the tanks. To preclude the introduction of surfactants in the fuel oil system, the cleaning should be accomplished using sodium hypochlorite solutions, or their equivalent, rather than

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LCV-0603-E

Rev. 0, 09/28/92

Ventilation-Diesel Fuel Oil, Lube Oil, and Starting Air, and B 3.8.3 BASES 7 SURVEILLANCE SR 3.8.3.8 (continued) REQUIREMENTS soap or detergents. This SR is for preventive maintenance. The presence of sediment does not necessarily represent a failure of this SR, provided that accumulated sediment is removed during performance of the Surveillance. > REFERENCES FSAR, Section 19.5.4.21. 1. 2. Regulatory Guide 1.137. 3. ANSI N195-1976, Appendix B. FSAR, Chapter /161. 4. FSAR, Chapter 115 5. WOG-13-11 D405X-681 0: D975-681 0: D4176-ASTM Standards: 6. D1522-0790; D2622-0820; D2276 7. ASTM Standards, D975, Table 1. 8. ASME, Beitor and Presser Verset Code LCV-0603-E Deleted The SR is modified by a note that excepts the performance of this SR when the associated DG is required OPERABLE by LCO 3.8.2. This exception is consistent with the SR performance exceptions in LCO 3.8.2 for SRs that might impact the OPERABility of the DGs. 9. Southern Company Services Calculation number X4C2403VID, Emergency Diesel Generator Fuel Oil Storage Technical Specification Values. 10, Southern Company Services Calculation number X 4C2403VII, Emergency Diesel Ger. ator Lube oil Inventory Technical Specification Values. 11. Southern Company Services Calculation number X4C2403V09, Emergency Diesel Generator Starting Air Pressure Technical Specification Value. Rev. 0. 09/28/92 WOG STS

CHAPTER 3.7 PLANT SYSTEMS

INSERT 28 FOR CST LCO BASES PAGE B 3.7- 34

LCV-0603-E

In order for a single CST to meet the LCO requirements stated above, design modifications are required. The design modifications are planned for each anit, during 1996s to allow alignment of the AFW pumps mini-flow lines to the CST to which the pump suction is aligned. Prior to the implementation of the design modification, LCO 3.7.6a shall be applicable. Prior to completion of the design modification the volume of water required to satisfy the safety analyses for a unit is 420,000 gallons LCO 3.7.6a requires an unmodified unit to maintain both CSTs OPERABLE with a combined safety-related volume of ≥420,000 gallons. In addition, LCO 3.7.6a requires the CST that supplies the AFW pumps to contain a safety-related volume of ≥340,000 gallons. The volume specified for the CST supplying the AFW System is based on the need to ensure sufficient time exists for the operator action required to switch the AFW pump suction supply to the other CST. If the combined safety-related volume or the safetyrelated volume required for the AFW supply is not as specified, LCO 3.7.6a contains Actions to restore the volume(s) to within limit or to place the unit in a MODE where the CSTs are no longer required OPERABLE. LCO 3.7.6a is no longer required and may be deleted when both units have completed the required modifications.

5.5 Programs and Manuals (continued)

and a second

5.5.10 Secondary Water Chemistry Program

This program provides controls for monitoring secondary water chemistry to inhibit SG tube degradation and low proceure turbing disc stress correction cracking. The program shall include:

- Identification of a sampling schedule for the critical variables and control points for these variables;
- Identification of the procedures used to measure the values of the critical variables;

 Identification of process sampling points; which shall include monitoring the discharge of the condensate pumps for evidence of condenser in leakage;

- Procedures for the recording and management of data;
- Procedures defining corrective actions for all off control point chemistry conditions; and
- f. A procedure identifying the authority responsible for the interpretation of the data and the sequence and timing of administrative events, which is required to initiate corrective action.

5.5.11 Ventilation Filter Testing Program (VFTP)

A program shall be established to implement the following required testing of Engineered Safety Feature (ESF) filter ventilation systems at the frequencies specified in [Regulatory Guide], in accordance with Regulatory Guide 1.52, Revision 2x and ASME N510-1989, and AG-1]. 1980 Demonstrate for each of the ESF systems that an inplace test а. of the high efficiency particulate air (HEPA) filters shows a penetration and system by pass $\leq 10.05\%$ when tested in 1CV-0603-E accordance with Regulatory Guide 1.52, Revision 2, and ASME N510-1989] at the system flowrate specified below (1 10%). 1980 Flowrate ESF Ventilation System CREFS P.P.ng Penetration Area filtration and Exhaust, 19,000 CFM (continued) WOG STS 5.0-12 Rev. 11/16/94

5.5 Programs and Manuals

1 1 4 V B

5.5.11 Ventilation Filter Testing Program (VFTP) (continued) Demonstrate for each of the ESF systems that an inplace test b. of the charcoal adsorber shows a penetration and system bypass $\leq 10.05\%$ when tested in accordance with ORegulatory 1980 Guide 1.52, Revision 2, and ASME N510-1989 at the system flowrate specified below $d \pm 10\%$ ESF Nentilation System Powrate 19,000 CFM CREFS PPAFES 15,500 CFM (oregual to) Demonstrate for each of the ESF systems that a laboratory с. test of a sample of the charcoal adsorber, when obtained as described in Regulatory Guide 1.52, Revision 20, shows the LCV-0603-E methyl iodide penetration less than the value specified below when tested in accordance with MASTM D3803-19890 at a temperature of \$3030°C and greater than or equal to the relative humidity specified below. ESP Ventilation System Benetration RH CREFS PPAFES Reviewer's Note: Allowable penetration = [100% methyl iodide efficiency for charcoal credited in staff safety evaluation]/ (safety factor) afety factor = [5] for systems with heaters. [7] for systems without heaters. Demonstrate for each of the ESF systems that the pressure d. drop across the combined HEPA filters, the prefilters, and the charcoal adsorbers, is less than the value specified below when tested in adcordance with Aregulatory Guide 1.52, - and CREFS cooling coils

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Rev. 11/16/94